

SMITHSONIAN
MISCELLANEOUS COLLECTIONS

VOL. 88



"EVERY MAN IS A VALUABLE MEMBER OF SOCIETY WHO, BY HIS OBSERVATIONS, RESEARCHES,
AND EXPERIMENTS, PROCURES KNOWLEDGE FOR MEN"—SMITHSON

(PUBLICATION 3240)

CITY OF WASHINGTON
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C. G. ABBOT,
Secretary of the Smithsonian Institution.

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SMITHSONIAN MISCELLANEOUS COLLECTIONS

VOLUME 88
(WHOLE VOLUME)

SMITHSONIAN PHYSICAL TABLES

EIGHTH REVISED EDITION

PREPARED BY

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(PUBLICATION 3171)

CITY OF WASHINGTON
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In connection with the system of meteorological observations established by the Smithsonian Institution about 1850, a series of meteorological tables was compiled by Dr. Arnold Guyot, at the request of Secretary Henry, and the first edition was published in 1852. Though primarily designed for meteorological observers reporting to the Smithsonian Institution, the tables were so widely used by physicists that it seemed desirable to recast the work entirely. It was decided to publish three sets of tables, each representative of the latest knowledge in its field, and independent of one another, but forming a homogeneous series. The first of the new series, Meteorological Tables, was published in 1893, the second, Geographical Tables, in 1894, and the third, Physical Tables, in 1896. In 1909 and 1922, respectively, two further volumes were added, so that the series now comprises: Smithsonian Meteorological Tables, Smithsonian Geographical Tables, Smithsonian Physical Tables, Smithsonian Mathematical Tables, Smithsonian Mathematical Formulae.

The 14 years which had elapsed in 1910 since the publication of the first edition of the Physical Tables, prepared by Prof. Thomas Gray, made imperative a radical revision for the fifth and sixth revised editions published in 1910 and 1914. The latter edition was reprinted thrice. The seventh revision was issued in 1919 and was reprinted thrice. The present eighth edition results from a further extensive revision.

Inconsistencies that will be noted in minor points of style, such as abbreviations, etc., arise from the fact that many of the tables are printed from electrotype plates; to change them to agree with present usages would involve too great expense.

CHARLES G. ABBOT,
Secretary, Smithsonian Institution.

March, 1932.

PREFACE TO 8TH REVISED EDITION

The present edition of the Smithsonian Physical Tables entails a considerable enlargement. Besides the insertion of new data in the older tables, about 270 new ones have been added. Their scope has been further broadened to include many new tables relating to astrophysics, geophysics, meteorology, geochemistry, atmospheric electricity, wireless, molecular and atomic data, etc.

Many suggestions and data have been received: from the Bureau of Standards, the Coast and Geodetic Survey (magnetic data), the Geophysical Laboratory, Naval Research Laboratory, Department of Terrestrial Magnetism, Harvard College Observatory, Eastman Kodak Co. (photographic data), National Research Council (International Critical Tables); from Messrs. Adams, White (Geophysical Laboratory), R. T. Birge, Briggs, Dellinger, Deming (Bureau of Chemistry and Soils), Dorsey (I. C. T.), Fleming, Forsythe, Hulburt, Lovejoy and Loomis (Eastman Kodak Co.), Kimball, Menzel, van Maanen, Russell, Shapley, St. John, Wells, Wherry, and many others whose names generally will be found with the corresponding data furnished. To all these we are indebted.

The changes in the domain of physics and allied branches have been so radical and extensive that it has been difficult to do justice to the advances. Further, it has been deemed essential to keep this volume in handy size, referring the reader to the more extensive International Critical Tables or to Landolt-Börnstein's *Physikalisch-chemische Tabellen* for more extensive data. It has been inadvisable to delay the tables for revision in many places. We will be grateful for criticisms, the notification of errors, and new data.

FREDERICK EUGENE FOWLE.

ASTROPHYSICAL OBSERVATORY,
SMITHSONIAN INSTITUTION,
March, 1932.

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INTRODUCTION

UNITS OF MEASUREMENT

The quantitative measure of anything is expressed by two factors, — one, a certain definite amount of the kind of physical quantity measured, called the unit, the other, the number of times this unit is taken. A distance is stated as 5 meters. The purpose in such a statement is to convey an idea of this distance in terms of some familiar or standard unit distance. Similarly quantity of matter is referred to as so many grams; of time, as so many seconds, or minutes, or hours.

The numerical factor definitive of the magnitude of any quantity must depend on the size of the unit in terms of which the quantity is measured. For example, let the magnitude factor be 5 for a certain distance when the mile is used as the unit of measurement. A mile equals 1760 yards or 5280 feet. The numerical factor evidently becomes 8800 and 26400, respectively, when the yard or the foot is used as the unit. Hence, to obtain the magnitude factor for a quantity in terms of a new unit, multiply the old magnitude factor by the ratio of the magnitudes of the old and new units; that is, by the number of the new units required to make one of the old.

The different kinds of quantities measured by physicists fall fairly definitely into two classes. In one class the magnitudes may be called extensive, — in the other, intensive. To decide to which class a quantity belongs, it is often helpful to note the effect of the addition of two equal quantities of the kind in question. If twice the quantity results, then the quantity has extensive (additive) magnitude. For instance, two pieces of platinum, each weighing 5 grams, added together, weigh 10 grams; on the other hand, the addition of one piece of platinum at 100°C to another at 100°C does not result in a system at 200°C . Volume, entropy, energy may be taken as typical of extensive, — density, temperature and magnetic permeability, of intensive magnitudes.

The measurement of quantities having extensive magnitude is a comparatively direct process. Those having intensive magnitude must be correlated with phenomena which may be measured extensively. In the case of temperature, a typical quantity with intensive magnitude, various methods of measurement have been devised, such as the correlation of magnitudes of temperature with the varying lengths of a thread of mercury.

Fundamental Units. — It is desirable that the fewest possible fundamental unit quantities should be chosen. Simplicity should regulate the choice, — simplicity 1st, psychologically, in that they should be easy to grasp mentally, and 2nd, physically, in permitting as straightforward and simple definition as

possible of the complex relationships involving them. Further it seems desirable that the units should be extensive in nature. It has been found possible to express all measurable physical quantities in terms of five such units: 1st, geometrical considerations — length, surface, etc., — lead to the need of a length; 2nd, kinematical considerations — velocity, acceleration, etc., — introduce time; 3rd, mechanics — treating of masses instead of immaterial points — introduces matter with the need of a fundamental unit of mass; 4th, electrical, and 5th, thermal considerations require two more such quantities. The discovery of new classes of phenomena may require further additions.

As to the first three fundamental quantities, simplicity and good use sanction the choice of a length, L , a time interval, T , and a mass, M . For the measurement of electrical quantities, good use has sanctioned two fundamental quantities, — the dielectric constant, K , the basis of the “electrostatic” system and the magnetic permeability, μ , the basis of the “electromagnetic” system. Besides these two systems involving electrical considerations, there is in common use a third one called the “international” system which will be referred to later. For the fifth, or thermal fundamental unit, temperature is generally chosen.¹

Derived Units. — Having selected the fundamental or basic units, — namely, a measure of length, of time, of mass, of permeability or of the dielectric constant, and of temperature, — it remains to express all other units for physical quantities in terms of these. Units depending on powers greater than unity of the basic units are called “derived units.” Thus, the unit volume is the volume of a cube having each edge a unit of length. Suppose that the capacity of some volume is expressed in terms of the foot as fundamental unit and the volume number is wished when the yard is taken as the unit. The yard is three times as long as the foot and therefore the volume of a cube whose edge is a yard is $3 \times 3 \times 3$ times as great as that whose edge is a foot. Thus the given volume will contain only $1/27$ as many units of volume when the yard is the unit of length as it will contain when the foot is the unit. To transform from the foot as old unit to the yard as new unit, the old volume number must be multiplied by $1/27$, or by the ratio of the magnitude of the old to that of the new unit of volume. This is the same rule as already given, but it is usually more convenient to express the transformations in terms of the fundamental units directly. In the present case, since, with the method of measurement here adopted, a volume number is the cube of a length-number, the ratio of two units of volume is the cube of the ratio of the intrinsic values of the two units of length. Hence, if l is the ratio of the magnitude of the old to that of the new unit of length, the ratio of the corresponding units of volume is l^3 . Similarly the ratio of two units of area would be l^2 , and so on for other quantities.

¹ Because of its greater psychological and physical simplicity, and the desirability that the unit chosen should have extensive magnitude, it has been proposed to choose as the fourth fundamental quantity, a quantity of electrical charge, e . The standard unit of electrical charge would then be the electronic charge. For thermal needs, entropy has been proposed. While not generally so psychologically easy to grasp as temperature, entropy is of fundamental importance in thermodynamics and has extensive magnitude. (R. C. Tolman, *The Measurable Quantities of Physics*, Physical Review, 9, p. 237, 1917.)

CONVERSION FACTORS AND DIMENSIONAL FORMULAE

For the ratios of length, mass, time, temperature, dielectric constant and permeability units the small bracketed letters, $[l]$, $[m]$, $[t]$, $[\theta]$, $[k]$, and $[\mu]$ will be adopted. These symbols will always represent simple numbers, but the magnitude of the number will depend on the relative magnitudes of the units the ratios of which they represent. When the values of the numbers represented by these small bracketed letters as well as the powers of them involved in any particular unit are known, the factor for the transformation is at once obtained. Thus, in the above example, the value of l was $1/3$, and the power involved in the expression for volume was 3; hence the factor for transforming from cubic feet to cubic yards was l^3 or $1/3^3$ or $1/27$. These factors will be called *conversion factors*.

To find the symbolic expression for the conversion factor for any physical quantity, it is sufficient to determine the degree to which the quantities length, mass, time, etc., are involved. Thus a velocity is expressed by the ratio of the number representing a length to that representing an interval of time, or $[L/T]$, and acceleration by a velocity number divided by an interval-of-time number, or $[L/T^2]$, and so on, and the corresponding ratios of units must therefore enter in precisely the same degree. The factors would thus be for the just stated cases, $[l/t]$ and $[l/t^2]$. Equations of the form above given for velocity and acceleration which show the dimensions of the quantity in terms of the fundamental units are called *dimensional equations*. Thus $[E] = [ML^2T^{-2}]$ will be found to be the dimensional equation for energy, and $[ML^2T^{-2}]$ the dimensional formula for it. These expressions will be distinguished from the conversion factors by the use of bracketed capital letters.

In general, if we have an equation for a physical quantity,

$$Q = CL^a M^b T^c,$$

where C is a constant and L , M , T represent length, mass, and time in terms of one set of units, and it is desired to transform to another set of units in terms of which the length, mass, and time are L_i , M_i , T_i , we have to find the value of L_i/L , M_i/M , T_i/T , which, in accordance with the convention adopted above, will be l , m , t , or the ratios of the magnitudes of the old to those of the new units.

Thus $L_i = Ll$, $M_i = Mm$, $T_i = Tt$, and if Q_i be the new quantity number,

$$\begin{aligned} Q_i &= CL_i^a M_i^b T_i^c, \\ &= CL^a l^a M^b m^b T^c t^c = Ql^a m^b t^c, \end{aligned}$$

or the conversion factor is $[l^a m^b t^c]$, a quantity precisely of the same form as the dimension formula $[L^a M^b T^c]$.

Dimensional equations are useful for checking the validity of physical equations. Since physical equations must be homogeneous, each term appearing in them must be dimensionally equivalent. For example, the distance moved by a uniformly accelerated body is $s = v_0 t + \frac{1}{2} a t^2$. The corresponding dimensional equation is $[L] = [(L/T)T] + [(L/T^2)T^2]$, each term reducing to $[L]$.

Dimensional considerations may often give insight into the laws regulating physical phenomena.¹ For instance Lord Rayleigh, in discussing the intensity

¹ See "On Physically Similar Systems; Illustrations of the Use of Dimensional Equations." E. Buckingham, *Physical Review*, (2) 4, 345, 1914; also *Phil. Mag.* 42, 696, 1921.

of light scattered from small particles, in so far as it depends upon the wave length, reasons as follows: ¹

"The object is to compare the intensities of the incident and scattered ray; for these will clearly be proportional. The number (*i*) expressing the ratio of the two amplitudes is a function of the following quantities:— *T*, the volume of the disturbing particle; *r*, the distance of the point under consideration from it; λ , the wave length; *b*, the velocity of propagation of light; *D* and *D'*, the original and altered densities: of which the first three depend only on space, the fourth on space and time, while the fifth and sixth introduce the consideration of mass. Other elements of the problem there are none, except mere numbers and angles, which do not depend upon the fundamental measurements of space, time, and mass. Since the ratio *i*, whose expression we seek, is of no dimensions in mass, it follows at once that *D* and *D'* occur only under the form *D*:*D'*, which is a simple number and may therefore be omitted. It remains to find how *i* varies with *T*, *r*, λ , *b*.

"Now, of these quantities, *b* is the only one depending on time; and therefore, as *i* is of no dimensions in time, *b* cannot occur in its expression. We are left, then, with *T*, *r*, and λ ; and from what we know of the dynamics of the question, we may be sure that *i* varies directly as *T* and inversely as *r*, and must therefore be proportional to $T \div \lambda^2 r$, *T* being of three dimensions in space. In passing from one part of the spectrum to another λ is the only quantity which varies, and we have the important law:

"When light is scattered by particles which are very small compared with any of the wave lengths, the ratio of the amplitudes of the vibrations of the scattered and incident light varies inversely as the square of the wave length, and the intensity of the lights themselves as the inverse fourth power."

The dimensional and conversion-factor formulae for the more commonly occurring derived units will now be developed.

GEOMETRICAL AND MECHANICAL UNITS

Area is referred to a unit square whose side is the unit of length. The area of a surface is expressed as

$$S = CL^2,$$

where the constant *C* depends on the contour of the surface and *L* is a linear dimension. If the surface is a square and *L* the length of a side, *C* is unity; if a circle and *L* its diameter, *C* is $\pi/4$. The dimensional formula is therefore $[L^2]$ and the conversion factor $[l^2]$. (Since the conversion factors are always of the same dimensions as the dimensional formulae they will be omitted in the subsequent discussions. A table of them will be found on page 3.)

Volume is referred to a unit cube whose edge is the unit of length. The volume of a body is expressed as

$$V = CL^3.$$

The constant *C* depends on the shape of the bounding surfaces. The dimensional formula is $[L^3]$.

Density is the quantity of matter per unit volume. The dimensional formula is $[M/V]$ or $[ML^{-3}]$.

Ex.—The density of a body is 150 pd. per cu. ft.: required the density in grains per cu. in. Here *m*, the number of grains in a pd., = 7000; *l*, the number of in. in a ft., = 12; $ml^{-3} = 7000/12^3 = 4.051$. The density is $150 \times 4.051 = 607.6$ grains/cu. in.

The specific gravity of a body is the ratio of a density to the density of a standard substance. The dimensional formula and conversion factor are both unity.

¹Philos. Mag., (4) 41, p. 107, 1871. See also Robertson, Dimensional analysis, Gen. Elec. Rev., 33, 207, 1930.

Velocity, v , of a body is dL/dt , or the ratio of a length to a time. The dimensional formula is $[LT^{-1}]$.

Angle is measured by the ratio of the length of an arc to its radius. The dimensional formula is unity.

Angular Velocity is the ratio of the angle described in a given time to that time. The dimensional formula is $[T^{-1}]$.

Linear Acceleration is the rate of change of velocity or $a = dv/dt$. The dimensional formula is $[L^1T^{-2}]$ or $[LT^{-2}]$.

Ex. — A body acquires velocity at a uniform rate and at the end of one minute moves at the rate of 20 kilometers per hour: what is the acceleration in centimeters per second per second? Since the velocity gained was 20 km per hour in one minute, the acceleration was 1200 km per hour per hour. $l = 100000$, $t = 3600$, $lt^{-2} = 100000/3600^2 = 0.00771$; the acceleration = $.00771 \times 1200 = 9.26$ cm/sec.

Angular Acceleration is rate of change of angular velocity. The dimensional formula is $[(\text{angular velocity})/T]$ or $[T^{-2}]$.

Momentum, the quantity of motion in the Newtonian sense, is measured by the product of the mass and velocity of the body. The dimensional formula is $[MV]$ or $[MLT^{-1}]$.

Moment of Momentum of a body with reference to a point is the product of its momentum by the distance of its line of motion from the point. The dimensional formula is $[ML^2T^{-1}]$.

Moment of Inertia of a body round an axis is expressed by the formula $\sum mr^2$, where m is the mass of any particle of the body and r its distance from the axis. The dimensional formula for the sum is the same as for each element and is $[ML^2]$.

Angular Momentum of a body is the product of its moment of inertia and angular velocity. The dimensional formula is $[ML^2T^{-1}]$.

Force is measured by the rate of change of momentum it can produce. The dimensional formulae for force and "time rate of change of momentum" are therefore the same, the ratio of a momentum to a time $[MLT^{-2}]$.

Ex. — When mass is expressed in lbs., length in ft., and time in secs., the unit force is called the poundal. When grams, cms, and secs. are the corresponding units, the unit of force is called the dyne. Find the number of dynes in 25 poundals. Here $m = 453.59$, $l = 30.48$, $t = 1$; $mlt^{-2} = 453.59 \times 30.48 = 13825$ nearly. The number of dynes is $13825 \times 25 = 345625$ approximately.

Moment of Couple, Torque, or Twisting Motive can be expressed as the product of a force and a length. The dimensional formula is $[FL]$ or $[ML^2T^{-2}]$.

Intensity of Stress is the ratio of the total stress to the area over which the stress is distributed. The dimensional formula is $[FL^{-2}]$ or $[ML^{-1}T^{-2}]$.

Intensity of Attraction, or "Force at a Point," is the force of attraction per unit mass on a body placed at the point. The dimensional formula is $[FM^{-1}]$ or $[LT^{-2}]$, the same as acceleration.

Absolute Force of a Center of Attraction, or "**Strength of a Center**," is the intensity of force at unit distance from the center, and is the force per unit mass at any point multiplied by the square of the distance from the center. The dimensional formula is $[FL^2M^{-1}]$ or $[L^3T^{-2}]$.

Modulus of Elasticity is the ratio of stress intensity to percentage strain. The dimensional of percentage strain, a length divided by a length, is unity. Hence the dimensional formula of a modulus of elasticity is that of stress intensity $[ML^{-1}T^{-2}]$.

Work is done by a force when the point of application of the force, acting on a body, moves in the direction of the force. It is measured by the product of the force and the displacement. The dimensional formula is $[FL]$ or $[ML^2T^{-2}]$.

Energy. — The work done by the force produces either a change in the velocity of the body or a change of its shape or configuration, or both. In the first case it produces a change of kinetic energy, in the second, of potential energy. The dimensional formulae of energy and work, representing quantities of the same kind, are identical $[ML^2T^{-2}]$.

Resilience is the work done per unit volume of a body in distorting it to the elastic limit or in producing rupture. The dimensional formula is $[ML^2T^{-2}L^{-3}]$ or $[ML^{-1}T^{-2}]$.

Power or Activity is the time rate of doing work, or if W represents work and P power, $P = dw/dt$. The dimensional formula is $[WT^{-1}]$ or $[ML^2T^{-3}]$, or for problems in gravitation units more conveniently $[FLT^{-1}]$, where F stands for the force factor.

Exs. — Find the number of gram-cms in one ft.-pd. Here the units of force are the attraction of the earth on the pound and the gram of matter. (In problems like this the terms "grams" and "pd." refer to force and not to mass.) The conversion factor is $[f/l]$, where f is 453.59 and l is 30.48. The answer is $453.59 \times 30.48 = 13825$.

Find the number of ft.-poundals in 1000000 cm.-dynes. Here $m = 1/453.59$, $l = 1/30.48$, $t = 1$; $ml^2t^{-2} = 1/453.59 \times 30.48^2$, and $10^6 ml^2t^{-2} = 10^6/453.59 \times 30.48^2 = 2.373$.

If gravity produces an acceleration of 32.2 ft./sec./sec., how many watts are required to make one horsepower? One horsepower is 550 ft.-pds. per sec., or $550 \times 32.2 = 17710$ ft.-poundals per second. One watt is 10^7 ergs per sec., that is, 10^7 dyne-cms per sec. The conversion factor is $[ml^2t^{-3}]$, where m is 453.59, l is 30.48, and t is 1, and the result has to be divided by 10^7 , the number of dyne-cms per sec. in the watt. $17710 ml^2t^{-3}/10^7 = 17710 \times 453.59 \times 30.48^2/10^7 = 746.3$.

HEAT UNITS

Quantity of Heat, measured in dynamical units, has the same dimensions as energy $[ML^2T^{-2}]$. Ordinary measurements, however, are made in *thermal units*, that is, in terms of the amount of heat required to raise the temperature of a unit mass of water one degree of temperature at some stated temperature. This involves the unit of mass and some unit of temperature. If we denote temperature numbers by Θ , the dimensional formula for quantity of heat, H , will be $[M\Theta]$. Unit volume is sometimes used instead of unit mass in the measurement of heat, the units being called *thermometric units*. The dimensional formula now changed by the substitution of volume for mass is $[L^3\Theta]$.

Specific Heat is the relative amount of heat, compared with water as standard substance, required to raise unit mass of different substances one degree in temperature and is a simple number.

Coefficient of Thermal Expansion of a substance is the ratio of the change of length per unit length (linear), or change of volume per unit volume (voluminal), to the change of temperature. These ratios are simple numbers, and the change of temperature varies inversely as the magnitude of the unit of temperature. The dimensional formula is $[\Theta^{-1}]$.

Thermal Conductivity, or **Specific Conductance**, is the quantity of heat, H , transmitted per unit of time per unit of surface per unit of temperature gradient. The equation for conductivity is therefore $K = H/L^2T\Theta/L$, and the dimensional formula $[H/\Theta LT] = [ML^{-1}T^{-1}]$ in thermal units. In thermometric units the formula becomes $[L^2T^{-1}]$, which properly represents diffusivity, and in dynamical units $[MLT^{-3}\Theta^{-1}]$.

Thermal Capacity is mass times the specific heat. The dimensional formula is $[M]$.

Latent Heat is the quantity of heat required to change the state of a body divided by the quantity of matter. The dimensional formula is $[M\Theta/M]$ or $[\Theta]$; in dynamical units it is $[L^2T^{-2}]$.

NOTE.—When Θ is given the dimensional formula $[L^2T^{-2}]$, the formulae in thermal and dynamical units are identical.

Joule's Equivalent, J , is connected with the quantity of heat by the equation $ML^2T^{-2} = JH$ or $JM\Theta$. The dimensional formula of J is $[L^2T^{-2}\Theta^{-1}]$. In dynamical units J is a simple number.

Entropy of a body is directly proportional to the quantity of heat it contains and inversely proportional to its temperature. The dimensional formula is $[M\Theta/\Theta]$ or $[M]$. In dynamical units the formula is $[ML^2T^{-2}\Theta^{-1}]$.

Exs.—Find the relation between the British thermal unit, the large or kilogram-calorie and the small or gram-calorie, sometimes called the “therm.” Referring all the units to the same temperature of the standard substance, the *British thermal unit* is the amount of heat required to warm one pound of water 1°F. , the *large calorie*, 1 kilogram of water, 1°C. , the *small calorie* or *therm*, 1 gram, 1°C. (1) To find the number of kg-cals. in one British thermal unit. $m = .45359$, $\theta = 5/9$; $m\theta = .45359 \times 5/9 = .25199$. (2) To find the number therms in one kg-cal. $m = 1000$, and $\theta = 1$; $m\theta = 1000$. (3) Hence the number of small calories or therms in one British thermal unit is $1000 \times .25199 = 251.99$.

ELECTRIC AND MAGNETIC UNITS

A system of units of electric and magnetic quantities requires four fundamental quantities. A system in which length, mass, and time constitute three of the fundamental quantities is known as an “absolute” system. There are two absolute systems of electric and magnetic units. One is called the electrostatic, in which the fourth fundamental quantity is the dielectric constant, and one is called the electromagnetic, in which the fourth fundamental quantity is magnetic permeability. Besides these two systems there will be described a third in common use called the “international” system.

In the electrostatic system, unit quantity of electricity, Q , is the quantity which exerts unit mechanical force upon an equal quantity a unit distance from it in a vacuum. From this definition the dimensions and the units of all the other electric and magnetic quantities follow through the equations of the mathematical theory of electromagnetism. The mechanical force between two quantities of electricity in any medium is

$$F = \frac{QQ'}{Kr^2},$$

where K is the dielectric constant, characteristic of the medium, and r the distance between the two points at which the quantities Q and Q' are located. K is the fourth quantity entering into dimensional expressions in the electrostatic system. Since the dimensional formula for force is $[MLT^{-2}]$, that for Q is $[M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-1}K^{\frac{1}{2}}]$.

The electromagnetic system is based upon the unit of the magnetic pole strength. The dimensions and the units of the other quantities are built up from this in the same manner as for the electrostatic system. The mechanical force between two magnetic poles in any medium is

$$F = \frac{mm'}{\mu r^2},$$

in which μ is the permeability of the medium and r is the distance between two poles having the strengths m and m' . μ is the fourth quantity entering into dimensional expressions in the electromagnetic system. It follows that the dimensional expression for magnetic pole strength is $[M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-1}\mu^{\frac{1}{2}}]$.

The symbols K and μ are sometimes omitted in the dimensional formulae so that only three fundamental quantities appear. There are a number of objections to this. Such formulae give no information as to the relative magnitudes of the units in the two systems. The omission is equivalent to assuming some relation between mechanical and electrical quantities, or to a mechanical explanation of electricity. Such a relation or explanation is not known.

The properties K and μ are connected by the equation $1/\sqrt{K\mu} = v$, where v is the velocity of an electromagnetic wave. For empty space or for air, K and μ being measured in the same units, $1/\sqrt{K\mu} = c$, where c is the velocity of light in vacuo, 3×10^{10} cm per sec. It is sometimes forgotten that the omission of the dimensions of K or μ is merely conventional. For instance, magnetic field intensity and magnetic induction apparently have the same dimensions when μ is omitted. This results in confusion and difficulty in understanding the theory of magnetism. The suppression of μ has also led to the use of the "centimeter" as a unit of capacity and of inductance; neither is physically the same as length.

ELECTROSTATIC SYSTEM

Quantity of Electricity has the dimensional formula $[M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-1}K^{\frac{1}{2}}]$, as shown above.

Electric Surface Density of an electrical distribution at any point on a surface is measured by the quantity per unit area. The dimensional formula is the ratio of the formulae for quantity of electricity and for area or $[M^{\frac{1}{2}}L^{-\frac{1}{2}}T^{-1}K^{\frac{1}{2}}]$.

Electric Field Intensity is measured by the ratio of the force on a quantity of electricity at a point to the quantity of electricity. The dimensional formula is therefore the ratio of the formulae for force and electric quantity or $[MLT^{-2}/M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-1}K^{\frac{1}{2}}]$ or $[M^{\frac{1}{2}}L^{-\frac{1}{2}}T^{-1}K^{-\frac{1}{2}}]$.

Electric Potential and Electromotive Force. — Change of potential is proportional to the work done per unit of electricity in producing the change. The dimensional formula is the ratio of the formulae for work and electrical quantity or $[MLL^2T^{-2}/M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-1}K^{\frac{1}{2}}]$ or $[M^{\frac{1}{2}}L^{\frac{1}{2}}T^{-1}K^{-\frac{1}{2}}]$.

Capacity of an Insulated Conductor is proportional to the ratio of the quantity of electricity in a charge to the potential of the charge. The dimensional formula is the ratio of the two formulae for electric quantity and potential or $[M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-1}K^{\frac{1}{2}}/M^{\frac{1}{2}}L^{\frac{1}{2}}T^{-1}K^{-\frac{1}{2}}]$ or $[LK]$.

Specific Inductive Capacity is the ratio of the inductive capacity of the substance to that of a standard substance and therefore is a number.

Electric Current is quantity of electricity flowing past a point per unit of time. The dimensional formula is the ratio of the formulae for electric quantity and for time or $[M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-1}K^{\frac{1}{2}}/T]$ or $[M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-2}K^{\frac{1}{2}}]$.

Electrical Conductivity, like the corresponding term for heat, is quantity per unit area per unit potential gradient per unit of time. The dimensional formula is $[M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-1}K^{\frac{1}{2}}/L^2(M^{\frac{1}{2}}L^{\frac{1}{2}}T^{-1}K^{-\frac{1}{2}}/L)T]$ or $[T^{-1}K]$.

Resistivity is the reciprocal of conductivity. The dimensional formula is $[TK^{-1}]$.

Conductance of any part of an electric circuit, not containing a source of electromotive force, is the ratio of the current flowing through it to the difference of potential between its ends. The dimensional formula is the ratio of the formulae for current and potential or $[M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-2}K^{\frac{1}{2}}/M^{\frac{1}{2}}L^{\frac{1}{2}}T^{-1}K^{-\frac{1}{2}}]$ or $[LT^{-1}K]$.

Resistance is the reciprocal of conductance. The dimensional formula is $[L^{-1}TK^{-1}]$.

Exs. — Find the factor for converting quantity of electricity expressed in ft.-grain-sec. units to the same expressed in c.g.s. units. The formula is $[m^{\frac{1}{2}}l^{\frac{3}{2}}t^{-1}k^{\frac{1}{2}}]$, in which $m=0.0648$, $l=30.48$, $t=1$, $k=1$; the factor is $0.0648^{\frac{1}{2}} \times 30.48^{\frac{3}{2}}$, or 42.8.

Find the factor required to convert electric potential from mm.-mg.-sec. units to c.g.s. units. The formula is $[m^{\frac{1}{2}}lt^{-1}k^{-\frac{1}{2}}]$, in which $m=0.001$, $l=0.1$, $t=1$, $k=1$; the factor is $0.001^{\frac{1}{2}} \times 0.1$, or 0.01.

Find the factor required to convert electrostatic capacity from ft.-grain-sec. and specific inductive capacity 6 units to c.g.s. units. The formula is $[lk]$ in which $l=30.48$, $k=6$; the factor is 30.48×6 , or 182.88.

ELECTROMAGNETIC SYSTEM

Many of the magnetic quantities are analogues of certain electric quantities. The dimensions of such quantities in the electromagnetic system differ from those of the corresponding electrostatic quantities in the electrostatic system only in the substitution of permeability μ for K .

Magnetic Pole Strength or **Quantity of Magnetism** has already been shown to have the dimensional formula $[M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-1}\mu^{\frac{1}{2}}]$.

Magnetic Flux characterizes the magnetized state of a magnetic circuit. Through a surface inclosing a magnetic pole it is proportional to the magnetic pole strength. The dimensional formula is that for magnetic pole strength.

Magnetic Field Intensity or **Magnetizing Force** is the ratio of the force on a magnetic pole placed at the point and the magnetic pole strength. The dimensional formula is therefore the ratio of the formulae for a force and magnetic quantity, or $[MLT^{-2}/M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-1}\mu^{\frac{1}{2}}]$ or $[M^{\frac{1}{2}}L^{-\frac{1}{2}}T^{-1}\mu^{-\frac{1}{2}}]$.

Magnetic Potential or **Magnetomotive Force** at a point is measured by the work which is required to bring unit quantity of positive magnetism from zero potential to the point. The dimensional formula is the ratio of the formulae for work and magnetic quantity, $[ML^2T^{-2}/M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-1}\mu^{\frac{1}{2}}]$ or $[M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-1}\mu^{-\frac{1}{2}}]$.

Magnetic Moment is the product of the pole strength by the length of the magnet. The dimensional formula is $[M^{\frac{1}{2}}L^{\frac{5}{2}}T^{-1}\mu^{\frac{1}{2}}]$.

Intensity of Magnetization of any portion of a magnetized body is the ratio of the magnetic moment of that portion and its volume. The dimensional formula is $[M^{\frac{1}{2}}L^{\frac{5}{2}}T^{-1}\mu^{\frac{1}{2}}/L^3]$ or $[M^{\frac{1}{2}}L^{-\frac{1}{2}}T^{-1}\mu^{\frac{1}{2}}]$.

Magnetic Induction is the magnetic flux per unit of area taken perpendicular to the direction of the magnetic flux. The dimensional formula is $[M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-1}\mu^{\frac{1}{2}}/L^2]$ or $[M^{\frac{1}{2}}L^{-\frac{1}{2}}T^{-1}\mu^{\frac{1}{2}}]$.

Magnetic Susceptibility is the ratio of intensity of magnetization produced and the intensity of the magnetic field producing it. The dimensional formula is $[M^{\frac{1}{2}}L^{-\frac{1}{2}}T^{-1}\mu^{\frac{1}{2}}/M^{\frac{1}{2}}L^{-\frac{1}{2}}T^{-1}\mu^{-\frac{1}{2}}]$ or $[\mu]$.

Current, I , flowing in circle, radius r , creates magnetic field at its center, $2\pi I/r$. Dimensional formula is product of formulae for magnetic field intensity and length or $[M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-1}\mu^{-\frac{1}{2}}]$.

Quantity of Electricity is the product of the current and time. The dimensional formula is $[M^{\frac{1}{2}}L^{\frac{3}{2}}\mu^{-\frac{1}{2}}]$.

Electric Potential, or **Electromotive Force**, as in the electrostatic system, is the ratio of work to quantity of electricity. The dimensional formula is $[ML^2T^{-2}/M^{\frac{1}{2}}L^{\frac{3}{2}}\mu^{-\frac{1}{2}}]$ or $[M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-2}\mu^{\frac{1}{2}}]$.

Electrostatic Capacity is the ratio of quantity of electricity to difference of potential. The dimensional formula is $[L^{-1}T^2\mu^{-1}]$.

Resistance of a Conductor is the ratio of the difference of potential between its ends and the constant current flowing. The dimensional formula is $[M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-2}\mu^{\frac{1}{2}}/M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-1}\mu^{-\frac{1}{2}}]$ or $[LT^{-1}\mu]$.

Conductance is the reciprocal of resistance, and the dimensional formula is $[L^{-1}T\mu^{-1}]$.

Conductivity is the quantity of electricity transmitted per unit area per unit potential gradient per unit of time. The dimensional formula is $[M^{\frac{1}{2}}L^{\frac{3}{2}}\mu^{-\frac{1}{2}}/L^2(M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-2}\mu^{\frac{1}{2}}/L)T]$ or $[L^{-2}T\mu^{-1}]$.

Resistivity is the reciprocal of conductivity as just defined. The dimensional formula is $[L^2T^{-1}\mu]$.

Self-inductance is for any circuit the electromotive force produced in it by unit rate of variation of the current through it. The dimensional formula is the product of the formulæ for electromotive force and time divided by that for current or $[M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-2}\mu^{\frac{1}{2}} \times T \div M^{\frac{1}{2}}L^{\frac{1}{2}}T^{-1}\mu^{-\frac{1}{2}}]$ or $[L\mu]$.

Mutual Inductance of two circuits is the electromotive force produced in one per unit rate of variation of the current in the other. The dimensional formula is the same as for self-inductance.

Electric Field Intensity is the ratio of electric potential or electromotive force and length. The dimensional formula is $[M^{\frac{1}{2}}L^{\frac{1}{2}}T^{-2}\mu^{\frac{1}{2}}]$.

Magnetic Reluctance is the ratio of magnetic potential difference to magnetic flux. The dimensional formula is $[L^{-1}\mu^{-1}]$.

Thermoelectric Power is measured by the ratio of electromotive force and temperature. The dimensional formula is $[M^{\frac{1}{2}}L^{\frac{1}{2}}T^{-2}\mu^{\frac{1}{2}}\Theta^{-1}]$.

Coefficient of Peltier Effect is measured by the ratio of the quantity of heat and quantity of electricity. The dimensional formula is $[ML^2T^{-2}/M^{\frac{1}{2}}L^{\frac{1}{2}}\mu^{-\frac{1}{2}}]$ or $[M^{\frac{1}{2}}L^{\frac{3}{2}}T^{-2}\mu^{\frac{1}{2}}]$, the same as for electromotive force.

Exs. — Find the factor required to convert intensity of magnetic field from ft.-grain-min. units to c.g.s. units. The formula is $[m^{\frac{1}{2}}l^{-\frac{1}{2}}t^{-1}\mu^{-\frac{1}{2}}]$; $m = 0.0648$, $l = 30.48$, $t = 60$, and $\mu = 1$; the factor is $0.0648^{\frac{1}{2}} \times 30.48^{-\frac{1}{2}}$, or 0.046108 .

How many c.g.s. units of magnetic moment make one ft.-grain-sec. unit of the same quantity? The formula is $[m^{\frac{1}{2}}l^{\frac{1}{2}}t^{-1}\mu^{\frac{1}{2}}]$; $m = 0.0648$, $l = 30.48$, $t = 1$, and $\mu = 1$; the number is $0.0648^{\frac{1}{2}} \times 30.48^{\frac{1}{2}}$, or 1305.6 .

If the intensity of magnetization of a steel bar is 700 in c.g.s. units, what will it be in mm-gram-sec. units? The formula is $[m^{\frac{1}{2}}l^{\frac{1}{2}}t^{-1}\mu^{\frac{1}{2}}]$; $m = 1000$, $l = 10$, $t = 1$, $\mu = 1$; the intensity is $700 \times 1000^{\frac{1}{2}} \times 10^{\frac{1}{2}}$, or 70000 .

Find the factor required to convert current from c.g.s. units to earth-quadrant- 10^{-11} gram-sec. units. The formula is $[m^{\frac{1}{2}}l^{\frac{1}{2}}t^{-1}\mu^{-\frac{1}{2}}]$; $m = 10^{11}$, $l = 10^{-9}$, $\mu = 1$; the factor is $10^{11} \times 10^{-\frac{9}{2}}$, or 10 .

Find the factor required to convert resistance expressed in c.g.s. units into the same expressed in earth-quadrant- 10^{-11} gram-sec. units. The formula is $[lt^{-1}\mu]$; $l = 10^{-9}$, $t = 1$, $\mu = 1$; the factor is 10^{-9} .

FUNDAMENTAL STANDARDS

The choice of the nature of the fundamental quantities already made does not sufficiently define the system for measurements. Some definite unit or arbitrarily chosen standard must next be taken for each of the fundamental quantities. This fundamental standard should have the qualities of permanence, reproducibility and availability and be suitable for accurate measures. Once chosen and made it is called the primary standard and is generally kept at some central bureau, — for instance, the International Bureau of Weights and Measures at Sèvres, France. A primary standard may also be chosen and made for derived units (e.g., the international ohm standard), when it is simply a standard closely representing the unit and accepted for practical purposes, its value having been fixed by certain measuring processes. Secondary or refer-

ence standards are accurately compared copies, not necessarily duplicates, of the primaries for use in the work of standardizing laboratories and the production of working standards for everyday use.

Standard of Length. — The primary standard of length which now almost universally serves as the basis for physical measurements is the meter. It is defined as the distance between two lines at 0°C on a platinum-iridium bar deposited at the International Bureau of Weights and Measures. This bar is known as the International Prototype Meter, and its length was derived from the "mètre des Archives," which was made by Borda. Borda, Delambre, Laplace, and others, acting as a committee of the French Academy, recommended that the standard unit of length should be the ten-millionth part of the length, from the equator to the pole, of the meridian passing through Paris. In 1795 the French Republic passed a decree making this the legal standard of length, and an arc of the meridian extending from Dunkirk to Barcelona was measured by Delambre and Mechain for the purpose of realizing the standard. From the results of that measurement the meter bar was made by Borda. The meter is now defined as above and not in terms of the meridian length; hence subsequent measures of the length of the meridian have not affected the length of the meter.

Standard of Mass. — The primary standard of mass now almost universally used as the basis for physical measurements is the kilogram. It is defined as the mass of a certain piece of platinum-iridium deposited at the International Bureau of Weights and Measures. This standard is known as the International Prototype Kilogram. Its mass is equal to that of the older standard, the "kilogram des Archives," made by Borda and intended to have the same mass as a cubic decimeter of distilled water at the temperature of 4°C .

Copies of the International Prototype Meter and Kilogram are possessed by the various governments and are called National Prototypes.

Standard of Time. — The unit of time universally used is the mean solar second, or the 86400th part of the mean solar day. It is based on the average time of one rotation of the earth on its axis relatively to the sun as a point of reference $= 1.002\,737\,91$ sidereal second.

Standard of Temperature. — The standard scale of temperature as adopted by the International Committee of Weights and Measures (1887) depends on the constant-volume hydrogen thermometer. The hydrogen is taken at an initial pressure at 0°C of one meter of mercury, 0°C , sea-level at latitude 45° . The scale is defined by designating the temperature of melting ice as 0° and of condensing steam as 100° under standard atmospheric pressure. This is known as the Centigrade scale (abbreviated C).

A scale independent of the properties of any particular substance, and called the thermodynamic, or absolute scale, was proposed in 1848 by Lord Kelvin. In it the temperature is proportional to the average kinetic energy per molecule of a perfect gas. The temperature of melting ice is taken as 273.18° , that of the boiling point, 373.18° . The scale of the hydrogen thermometer varies from it only in the sense that the behavior of hydrogen departs from that of a perfect gas. It is customary to refer to this scale as the Kelvin scale (abbreviated K.)

NUMERICALLY DIFFERENT SYSTEMS OF UNITS

The fundamental physical quantities which form the basis of a system for measurements have been chosen and the fundamental standards selected and made. Custom has not however generally used these standards for the measurement of the magnitudes of quantities but rather multiples or submultiples of them. For instance, for very small quantities the micron (μ) or one-millionth of a meter is often used. The following table ¹ gives some of the systems proposed, all built upon the fundamental standards already described. The centimeter-gram-second (cm-g-sec. or c.g.s.) system proposed by Kelvin is the only one generally accepted.

TABLE I.
PROPOSED SYSTEMS OF UNITS.

| | Weber and Gauss | Kelvin c.g.s. | Moon 1891 | Giorgi MKS (Prim. Stds.) | France 1914 | B. A. Com., 1863 | Practical (B. A. Com., 1873) | Strout 1891 |
|--------|-----------------------|------------------|--------------------------|-----------------------------------|----------------|------------------------|---------------------------------------|----------------|
| Length | mm | cm | dm | m | m | m | 10^9 cm | 10^9 cm |
| Mass | mg | g | Kg | Kg | 10^6 g | g | 10^{-11} g | 10^{-9} g |
| Time | sec. | sec. | $\frac{\text{sec.}}{10}$ | sec. | sec. | sec. | sec. | sec. |

Further the choice of a set of fundamental physical quantities to form the basis of a system does not necessarily determine how that system shall be used in measurements. In fact, upon any sufficient set of fundamental quantities, a great many different systems of units may be built. The electrostatic and electromagnetic systems are really systems of electric quantities rather than units. They were based upon the relationships $F = QQ'/Kr^2$ and $mm'/\mu r^2$, respectively. Systems of units built upon a chosen set of fundamental physical quantities may differ in two ways: (1) the units chosen for the fundamental quantities may be different; (2) the defining equations by which the system is built may be different.

The electrostatic system generally used is based on the centimeter, gram, second, and dielectric constant of a vacuum. Other systems have appeared, differing from this in the first way, — for instance using the foot, grain and second in place of the centimeter, gram and second. A system differing from it in the second way is that of Heaviside which introduces the factor 4π at different places than is usual in the equations. There are similarly several systems of electromagnetic units in use.

Gaussian Systems. — “The complexity of the interrelations of the units is increased by the fact that not one of the systems is used as a whole, consistently for all electromagnetic quantities. The ‘systems’ at present used are therefore combinations of certain of the systems of units.

¹ Circular 60 of the Bureau of Standards, Electric Units and Standards, 1916. The subsequent matter in this introduction is based upon this circular.

"Some writers ¹ on the theory of electricity prefer to use what is called a Gaussian system, a combination of electrostatic units for purely electrical quantities and electromagnetic units for magnetic quantities. There are two such Gaussian systems in vogue, — one a combination of c.g.s. electrostatic and c.g.s. electromagnetic systems, and the other a combination of the two corresponding Heaviside systems.

"When a Gaussian system is used, caution is necessary when an equation contains both electric and magnetic quantities. A factor expressing the ratio between the electrostatic and electromagnetic units of one of the quantities has to be introduced. This factor is the first or second power of c , the number of electrostatic units of electric charge in one electromagnetic unit of the same. There is sometimes a question as to whether electric current is to be expressed in electrostatic or electromagnetic units, since it has both electric and magnetic attributes. It is usually expressed in electrostatic units in the Gaussian system."

It may be observed from the dimensions of K given in Table 1 that $[1/K\mu] = [L^2/T^2]$ which has the dimensions of a square of a velocity. This velocity was found experimentally to be equal to that of light, when K and μ were expressed in the same system of units. Maxwell proved theoretically that $1/\sqrt{K\mu}$ is the velocity of any electromagnetic wave. This was subsequently proved experimentally. When a Gaussian system is used, this equation becomes $c/\sqrt{K\mu} = v$. For the ether $K = 1$ in electrostatic units and $\mu = 1$ in electromagnetic units. Hence $c = v$ for the ether, or the velocity of an electromagnetic wave in the ether is equal to the ratio of the c.g.s. electromagnetic to the c.g.s. electrostatic unit of electric charge. This constant c is of primary importance in electrical theory. Its most probable value is 2.9979×10^{10} centimeters per second.

"Practical" Electromagnetic System. — This electromagnetic system is based upon the units of 10^9 cm, 10^{-11} gram, the sec. and μ of the ether. It is never used as a complete system of units but is of interest as the historical basis of the present International System. The principal quantities are the resistance unit, the ohm = 10^9 c.g.s. units; the current unit, the ampere = 10^{-1} c.g.s. units; and the electromotive force unit, the volt = 10^8 c.g.s. units.

The International Electric Units. — The units used in practical measurements, however, are the "International Units." They were derived from the "practical" system just described, or as the latter is sometimes called, the "absolute" system. These international units are based upon certain concrete standards presently to be defined and described. With such standards electrical comparisons can be more accurately and readily made than could absolute measurements in terms of the fundamental units. Two electric units, the international ohm and the international ampere, were chosen and made as nearly equal as possible to the ohm and ampere of the "practical" or "absolute" system.

¹ For example, A. G. Webster, "Theory of Electricity and Magnetism," 1897; J. H. Jeans, "Electricity and Magnetism," 1911; H. A. Lorentz, "The Theory of Electrons," 1909; and O. W. Richardson, "The Electron Theory of Matter," 1914.

This system of units, sufficiently near to the "absolute" system for the purpose of electrical measurements and as a basis for legislation, was defined as follows:

"1. The *International Ohm* is the resistance offered to an unvarying electric current by a column of mercury at the temperature of melting ice, 14.4521 grams in mass, of a constant cross-sectional area and of a length of 106.300 centimeters.

"2. The *International Ampere* is the unvarying electric current which, when passed through a solution of nitrate of silver in water, in accordance with specification II attached to these Resolutions, deposits silver at the rate of 0.00111800 of a gram per second.

"3. The *International Volt* is the electrical pressure which, when steadily applied to a conductor the resistance of which is one international ohm will produce a current of one international ampere.

"4. The *International Watt* is the energy expended per second by an unvarying electric current of one international ampere under the pressure of one international volt."

In accordance with these definitions, a value was established for the electromotive force of the recognized standard of electromotive force, the Weston normal cell, as the result of international coöperative experiments in 1910. The value was 1.0183 international volts at 20° C.

The definitions by the 1908 International Conference supersede certain definitions adopted by the International Electrical Congress at Chicago in 1893. Certain of the units retain their Chicago definitions, however. They are as follows:

"*Coulomb*. As a unit of quantity, the *International Coulomb*, which is the quantity of electricity transferred by a current of one international ampere in one second.

"*Farad*. As a unit of capacity, the *International Farad*, which is the capacity of a condenser, charged to be a potential of one international volt by one international coulomb of electricity.

"*Joule*. As a unit of work, the *Joule*, which is equal to 10^7 units of work in the c.g.s. system, and which is represented sufficiently well for practical use by the energy expended in one second by an international ampere in an international ohm.

"*Henry*. As the unit of induction, the *Henry*, which is the induction in a circuit when the electromotive force induced in this circuit is one international volt, while the inducing current varies at the rate of one ampere per second."

"The choice of the ohm and ampere as fundamental was purely arbitrary. These are the two quantities directly measured in absolute electrical measurements. The ohm and volt have been urged as more suitable for definition in terms of arbitrary standards, because the primary standard of electromotive force (standard cell) has greater simplicity than the primary standard of current (silver voltameter). The standard cell is in fact used, together with resistance standards, for the actual maintenance of the units, rather than the silver voltameter and resistance standards. Again, the volt and ampere have some claim

for consideration for fundamental definition, both being units of quantities more fundamental in electrical theory than resistance."

For all practical purposes the "international" and the "practical" or "absolute" units are the same. Experimental determination of the ratios of the corresponding units in the two systems have been made and the mean results are given in Table 463. These ratios represent the accuracy with which it was possible to fix the values of the international ohm and ampere at the time they were defined (London Conference of 1908). It is unlikely that the definitions of the international units will be changed in the near future to make the agreement any closer. An act approved July 12, 1894, makes the International units as above defined the legal units in the United States of America.

THE STANDARDS OF THE INTERNATIONAL ELECTRICAL UNITS

RESISTANCE

The definition of the international ohm adopted by the London Conference in 1908 is accepted practically everywhere.

Mercury Standards. — Mercury standards conforming to the definition were constructed in England, France, Germany, Japan, Russia and the United States. Their mean resistances agree to about two parts in 100,000. To attain this accuracy, elaborate and painstaking experiments were necessary. Tubes are never quite uniform in cross-section; the accurate measurement of the mass of mercury filling the tube is difficult, partly because of a surface film on the walls of the tube; the greatest refinements are necessary in determining the length of the tube. In the electrical comparison of the resistance with wire standards, the largest source of error is in the filling of the tube. These and other sources of error necessitated a certain uniformity in the setting up of mercury standards and at the London Conference the following specifications were drawn up:

SPECIFICATION RELATING TO MERCURY STANDARDS OF RESISTANCE

The glass tubes used for mercury standards of resistance must be made of a glass such that the dimensions may remain as constant as possible. The tubes must be well annealed and straight. The bore must be as nearly as possible uniform and circular, and the area of cross-section of the bore must be approximately one square millimeter. The mercury must have a resistance of approximately one ohm.

Each of the tubes must be accurately calibrated. The correction to be applied to allow for the area of the cross-section of the bore not being exactly the same at all parts of the tube must not exceed 5 parts in 10,000.

The mercury filling the tube must be considered as bounded by plane surfaces placed in contact with the ends of the tube.

The length of the axis of the tube, the mass of mercury the tube contains, and the electrical resistance of the mercury are to be determined at a temperature as near to 0°C as possible. The measurements are to be corrected to 0°C .

For the purpose of the electrical measurements, end vessels carrying connections for the current and potential terminals are to be fitted on to the tube. These end vessels are to be spherical in shape (of a diameter of approximately four centimeters) and should have cylindrical pieces attached to make connections with the tubes. The outside edge of each end of the tube

is to be coincident with the inner surface of the corresponding end vessel. The leads which make contact with the mercury are to be of thin platinum wire fused into glass. The point of entry of the current lead and the end of the tube are to be at opposite ends of a diameter of the bulb; the potential lead is to be midway between these two points. All the leads must be so thin that no error in the resistance is introduced through conduction of heat to the mercury. The filling of the tube with mercury for the purpose of the resistance measurements must be carried out under the same conditions as the filling for the determination of the mass.

The resistance which has to be added to the resistance of the tube to allow for the effect of the end vessels is to be calculated by the formula

$$A = \frac{0.80}{1063\pi} \left(\frac{1}{r_1} + \frac{1}{r_2} \right) \text{ ohm},$$

where r_1 and r_2 are the radii in millimeters of the end sections of the bore of the tube.

The mean of the calculated resistances of at least five tubes shall be taken to determine the value of the unit of resistance.

For the purpose of the comparison of resistances with a mercury tube the measurements shall be made with at least three separate fillings of the tube.

Secondary Standards. — Secondary standards, derived from the mercury standards and used to give values to working standards, are certain coils of manganin wire kept in the national laboratories. Their resistances are adjusted to correspond to the unit or its decimal multiples or submultiples. The values assigned to these coils are checked from time to time with the similar coils of the other countries. The value now in use is based on the comparison made at the U. S. Bureau of Standards in 1910 and may be called the "1910 ohm." Later measurements on various mercury standards checked the value then used within 2 parts in 100,000. Thus the basis of resistance measurement is maintained not by the mercury standards of a single laboratory, but by all the mercury standards of the various national laboratories; it is furthermore the same in all countries, except for very slight outstanding discrepancies due to the errors of measurement and variations of the standards with time.

Resistance Standards in Practice. — In ordinary measurements, working standards of resistance are usually coils of manganin wire (approximately 84 per cent Cu + 12 per cent Mn + 4 per cent Ni). They are generally used in oil which carries away the heat developed by the current and facilitates regulation and measurement of the temperature. The best type is inclosed in a sealed case for protection against atmospheric humidity. Varying humidity changes the resistance of open coils often to several parts in 10,000 higher in summer than in winter. While sealed 1 ohm and 0.1 ohm coils may remain constant to about 1 part in 100,000.

Absolute Ohm. — The absolute measurement of resistance involves the precise determination of a length and a time (usually an angular velocity) in a medium of unit permeability. Since the dimensional formula of resistance in the electromagnetic system is $[L\mu/T]$, such an absolute measurement gives R not in cm/sec. but in $\text{cm} \times \mu/\text{sec}$. The definitions of the ohm, ampere and volt by the 1908 London conference tacitly assume a permeability equal to unity. The relation of the international ohm to the absolute ohm has been measured in different ways involving revolving coil, revolving disk, and alter-

nate current methods. Probably the most accurate value is that given by Birge (see p. 77).

1 international ohm = 1.00051 ± 0.00002 absolute ohms,

or, in other words, while one international ohm is represented by a mercury column 106.300 cm long as specified above, one absolute ohm requires a similar column 106.246 cm long.

CURRENT

The Silver Voltmeter. — The silver voltmeter is a concrete means of measuring current in accordance with the definition of the international ampere. As used for the realization of the international ampere "it consists of a platinum cathode in the form of a cup holding the silver nitrate solution, a silver anode partly or wholly immersed in the solution, and some means to prevent anode slime and particles of silver mechanically detached from the anode from reaching the cathode. As a standard representing the international ampere, the silver voltmeter includes also the chronometer used to measure time. The degree of purity and the mode of preparation of the various parts of the voltmeter affect the mass of the deposit. There are numerous sources of error, and the suitability of the silver voltmeter as a primary standard of current has been under investigation since 1893. Differences of as much as 0.1 per cent or more may be obtained by different procedures, the larger differences being mainly due to impurities produced in the electrolyte (by filter paper, for instance). Hence, in order that the definition of current be precise, it must be accompanied by *specifications* for using the voltmeter."

The original specifications were recognized to be inadequate and an international committee on electrical units and standards was appointed to complete the specifications. It was also recognized that in practice standard cells would replace secondary current standards so that a value must be fixed for the electromotive force of the Weston normal cell. This was attempted in 1910 at the Bureau of Standards by representatives of that institution together with one delegate each from the Physikalische-Technische Reichsanstalt, The National Physical Laboratory and the Laboratoire Central d'Electricité. Voltmeters from all four institutions were put in series under a variety of experimental conditions. Standard Weston cells and resistance standards of the four laboratories were also intercompared. From the joint comparison of standard cells and silver voltmeters particular values were assigned to the standard cells from each laboratory. The different countries thus have a common basis of measurement maintained by the aid of standard cells and resistance standards derived from the international voltmeter investigation of 1910.

It was not found possible to draw up satisfactory and final specifications for the silver voltmeter. Provisional specifications were submitted by the U. S. Bureau of Standards and more complete specifications have been proposed in correspondence between the national laboratories and members of the inter-

national committee since 1910, but no agreement upon final specifications has yet been reached.

Resistance Standards Used in Current Measurements. — Precise measurements of currents require a potentiometer, a standard cell and a resistance standard. The resistance must be so designed as to carry the maximum current without undue heating and consequent change of resistance. Accordingly the resistance metal must have a small temperature resistance coefficient and a sufficient area in contact with the air, oil, or other cooling fluid. It must have a small thermal electromotive force against copper. Manganin satisfies these conditions and is usually used. The terminals of the standard must have sufficient contact area so that there shall be no undue heating at contacts.¹ It must be so designed that the current distribution does not depend upon the mode of connection to the circuit.

Absolute Ampere. — The absolute ampere (10^{-1} c.g.s. electromagnetic units) differs by a negligible amount from the international ampere. Since the dimensional formula of the current in the electromagnetic system is $[L^{\frac{1}{2}}M^{\frac{1}{2}}/T\mu^{\frac{1}{2}}]$ which is equivalent to $[F^{\frac{1}{2}}/\mu^{\frac{1}{2}}]$, the absolute measurement of current involves fundamentally the measurement of a force in a medium of unit permeability. In most measurements of high precision an electro-dynamometer has been used of the form known as a current balance.

The best value may be taken as (Birge, 1930)

$$1 \text{ international ampere} = 0.99995 \pm 0.00005 \text{ absolute ampere.}$$

The result may also be expressed in terms of the electrochemical equivalent of silver, and thus equals 0.00111805 g per absolute coulomb. The value is 0.00111800 g per international coulomb.

ELECTROMOTIVE FORCE

International Volt. — “The international volt is derived from the international ohm and ampere by Ohm’s law. Its value is maintained by the aid of the Weston normal cell. The national standardizing laboratories have groups of such cells, to which values in terms of the international ohm and ampere have been assigned by international experiments, and thus form a basis of reference for the standardization of the standard cells used in practical measurements.”

Weston Normal Cell. — The Weston normal cell is the standard used to maintain the international volt and, in conjunction with resistance standards, to maintain the international ampere. The cell is a simple voltaic combination

¹ See “Report to the International Committee on Electrical Units and Standards,” 1912, p. 199. For the Bureau of Standards investigations see Bull. Bureau of Standards, 9, pp. 209, 493; 10, p. 475, 1912-14; 13, p. 147, 1915; 9, p. 151, 1912; 13, pp. 447, 479, 1916.

having its anode or negative electrode of cadmium amalgam, consisting of 10 per cent by weight of cadmium and 90 per cent mercury. The cathode, or positive electrode, is pure mercury covered with a paste consisting of mercurous sulphate, cadmium-sulphate crystals, and solution. The electrolyte is cadmium-sulphate solution in contact with an excess of cadmium-sulphate crystals. The containing vessel is of glass, usually in the H form. Connection is made to the electrodes by platinum wires sealed into the glass. The cells are sealed, preferably hermetically, and in use are submerged in a constant-temperature oil bath. The resistance of a cell is about 600 to 1000 ohms. The Weston cell used with potentiometers is not the Weston normal cell, but differs from it only slightly, the cadmium-sulphate solution not being saturated. It is described in the next section below.

One of the great advantages of the Weston normal cell is its small change of electromotive force with change of temperature. At any temperature, t (centigrade), between 0° and 40° , $E_t = E_{20} - 0.0000406 (t - 20) - 0.00000095 (t - 20)^2 + 0.00000001 (t - 20)^3$. This temperature formula was adopted by the London conference of 1908. That this formula may apply, the cell must be of a strictly uniform temperature throughout. One leg of the cell has a large positive and the other leg a large negative temperature coefficient. If the temperature of one leg changes faster than the other, the formula does not hold.

When the best of care is taken as to purity of materials and mode of procedure, Weston normal cells are reproducible within 1 part in 100,000. The source of the greatest variations has probably been in the mercurous sulphate. Cells using the best samples of this material have an electromotive force the constancy of which over a period of one year is about 1 part in 100,000. Only very meager specifications for the cell have as yet been agreed upon internationally, however, and the procedures in various laboratories differ in some respects.¹

The basis of measurements of electromotive force is the same in all countries as the result of the joint international experiments of 1910. As already stated, a large number of observations were made at that time with the silver voltameter, and a considerable number of Weston normal cells from the national laboratories of England, France, Germany and the United States were compared. From the results of these voltameter experiments and from resistance measurements, the value

$$1.0183 \text{ international volts at } 20^\circ \text{ C}$$

was assigned to the Weston normal cell. A mean of the groups of cells from the four laboratories was taken as most accurately representing the Weston normal

¹ For the preliminary specifications which have been issued and the reports of the various investigations on the standard cells see the following references: Preliminary specifications, Wolff and Waters, Bull. B. of S. 3, p. 623, 1907; Clark and Weston Standard Cells, Wolff and Waters, ditto, 4, p. 1, 1907; Temperature formula of Weston Standard Cell, ditto, 5, p. 309, 1908; The materials, reproducibility, etc., of the Weston Cell, Helett, Phys. Rev. 22, p. 321, 1906; 23, p. 166, 1906; 27, pp. 33, 337, 1908; Mercurous sulphate, etc., Steinwehr, Zs. für Electroch. 12, p. 578, 1906; German value of cell, Jaeger and Steinwehr, ditto, 28, p. 367, 1908; National Physical Laboratory researches, Smith, Phil. Trans. 207, p. 393, 1908; On the Weston Cell, Haga and Boerema, Arch. Neerland, des Sci. Exactes, 3, p. 324, 1913.

cell. Each laboratory has means of preserving the unit. Any discrepancies between the bases of the different countries at the present time would be due only to possible variations in the reference cells of the national laboratories. Such discrepancies are probably less than 2 parts in 100,000.

The figure 1.0183 has been in use since January 1, 1911. The value used in the United States before 1911, 1.019126 at 20° C or 1.0189 at 25° C, was assigned to a certain group of cells maintained as the standard of electromotive force at the Bureau of Standards. The high value is partly due to the use of commercial mercurous sulphate in the cells. The old and the new values, 1.01926 and 1.0183, thus apply to different groups of cells. The group of cells to which the value 1.019126 was assigned before 1910 differed by 26 microvolts from the mean of the international group, such that the international group to which the value 1.0183 is now assigned had the value $1.019126 + 0.000026$, or 1.019152, in terms of the old United States basis. The difference between 1.019152 and 1.0183 is 0.000852.

The electromotive force of any Weston cell as now given is therefore 0.000852 volt smaller than on the old United States basis, i.e., the present international volt is 84 parts in 100,000 larger than the old international volt of the United States.

Upon the new international basis the Clark cell set up according to the old United States legal specifications has an e.m.f of 1.4328₀ international volts at 15° C. The Clark cell set up (with specially purified mercurous sulphate) according to improved specifications used at the Bureau of Standards has an e.m.f of 1.4325₀ international volts at 15° C or 1.4263₇ at 20° C.

Weston Portable Cell. — The standard cell used in practice is the Weston portable cell. It is like the Weston normal cell except that the cadmium-sulphate solution at ordinary temperatures is unsaturated. As usually made, the cadmium-sulphate solution is saturated at about 4° C; at higher temperatures the crystals are dissolved. Plugs of asbestos or other material hold the chemicals in place. Its resistance is usually about 200 to 311 ohms. The change of e.m.f. wholly negligible in most electrical measurements, is less than 0.00001 volt per degree C. The two legs of the cell have large and opposite temperature coefficients so that care must be taken that the temperature of the cell is kept uniform and the cell must be protected from draughts or large changes of temperature. The electromotive force of a portable cell ranges from 1.0181 to 1.0191 international volts and must be determined by comparison with standards. It decreases very slightly with time, usually less than 0.0001 volt per year.

Absolute and Semi-absolute Volt. — Since the direct determination of the volt in absolute measure presents great difficulties, it is derived by Ohm's law from the absolute measures of the ohm and ampere. From the absolute values of these,

$$1 \text{ international volt} = 1.00046 \pm 0.00005 \text{ absolute volts.}$$

The electromotive force of the Weston normal cell at 20° C is 1.0183₀ international volts and 1.0187₇ absolute volts. A semi-absolute volt is that potential

difference which exists between the terminals of a resistance of one *international* ohm when the latter carries a current of one *absolute* ampere. The e.m.f of the Weston normal cell may be taken as 1.01821 semi-absolute volts at 20° C.

QUANTITY OF ELECTRICITY

The international unit of quantity of electricity is the coulomb. The faraday is the quantity of electricity necessary to liberate 1 gram equivalent in electrolysis. It is equivalent to 96494 international coulombs = 96489 absolute coulombs (Birge).

Standards. — There are no standards of electric quantity. The silver voltameter may be used for its measurement since under ideal conditions the mass of metal deposited is proportional to the amount of electricity which has flowed.

CAPACITY

The unit generally used for capacity is the international microfarad or the one-millionth of the international farad. Capacities are commonly measured by comparison with standard capacities. The values of the standards are determined by measurement in terms of resistance and time. The standard is some form of condenser consisting of two sets of metal plates separated by a dielectric. The condenser should be surrounded by a metal shield connected to one set of plates rendering the capacity independent of the surroundings. An ideal condenser would have a constant capacity under all circumstances, with zero resistance in its leads and plates, and no absorption in the dielectric. Actual condensers vary with the temperature, atmospheric pressure, and the voltage, frequency, and time of charge and discharge. A well-constructed air condenser with heavy metal plates and suitable insulating supports is practically free from these effects and is used as a standard of capacity.

Practically air condenser plates must be separated by 1 mm or more and so cannot be of great capacity. The more the capacity is increased by approaching the plates, the less the mechanical stability and the less constant the capacity. Condensers of great capacity use solid dielectrics, preferably mica sheets with conducting plates of tinfoil. At constant temperature the best mica condensers are excellent standards. The dielectric absorption is small but not quite zero, so that the capacity of these standards with different methods of measurement must be carefully determined.

INDUCTANCE

The henry, the unit of self-inductance, is also the unit of mutual inductance. The henry has been known as the "quadrant" and the "secohm." The length of a quadrant or quarter of the earth's circumference is approximately 10^9 cms. and a henry is 10^9 cms. of inductance. Secohm is a contraction of second and ohm; the dimensions of inductance are $[TR]$ and this unit is based on the second and ohm.

Inductance Standards. — Inductance standards are measured in international units in terms of resistance and time or resistance and capacity by alternate-

current bridge methods. Inductances calculated from dimensions are in absolute electromagnetic units. The ratio of the international to the absolute henry is the same as the ratio of the corresponding ohms.

Since inductance is measured in terms of capacity and resistance by the bridge method about as simply and as conveniently as by comparison with standard inductances, it is not necessary to maintain standard inductances. They are however of value in magnetic, alternating-current, and absolute electrical measurements. A standard inductance is a circuit so wound that when used in a circuit it adds a definite amount of inductance. It must have either such a form or so great an inductance that the mutual inductance of the rest of the circuit upon it may be negligible. It usually is a wire coil wound all in the same direction to make self-induction a maximum. A standard, the inductance of which may be calculated from its dimensions, should be a single layer coil of very simple geometrical form. Standards of very small inductance, calculable from their dimensions, are of some simple device, such as a pair of parallel wires or a single turn of wire. With such standards great care must be used that the mutual inductance upon them of the leads and other parts of the circuit is negligible. Any inductance standard should be separated by long leads from the measuring bridge or other apparatus. It must be wound so that the distributed capacity between its turns is negligible; otherwise the apparent inductance will vary with the frequency.

POWER AND ENERGY

Power and energy, although mechanical and not primarily electrical quantities, are measurable with greater precision by electrical methods than in any other way. The watt and the electric units were so chosen in terms of the c.g.s. units that the product of the current in amperes by the electromotive force in volts gives the power in watts (for continuous or instantaneous values). The international watt, defined as "the energy expended per second by an unvarying electric current of one international ampere under an electric pressure of one international volt," differs but little from the absolute watt.

Standards and Measurements. — No standard is maintained for power or energy. Measurements are always made in electrical practice in terms of some of the purely electrical quantities represented by standards.

MAGNETIC UNITS

C.g.s. units are generally used for magnetic quantities. American practice is fairly uniform in names for these units: the c.g.s. unit of magnetomotive force is called the "gilbert," of reluctance, the "oersted," following the provisional definitions of the American Institute of Electrical Engineers (1894). The c.g.s. unit of flux is called the "maxwell" as defined by the 1900 Paris conference. The name "gauss" is used unfortunately both for the unit of induction (A.I.E.E. 1894) and for the unit of magnetic field intensity or magnetizing force. "This double usage, recently sanctioned by engineering societies, is based upon the mathematical convenience of defining both induction and magnetizing force

as the force on a unit magnetic pole in a narrow cavity in the material, the cavity being in one case perpendicular, in the other parallel, to the direction of the magnetization: this definition however applies only in the ordinary electro-magnetic units. There are a number of reasons for considering induction and magnetizing force as two physically distinct quantities, just as electromotive force and current are physically different."

In the United States "gauss" has been used much more for the c.g.s. unit of induction than for the unit of magnetizing force. The longer name of "maxwell per cm²" is also sometimes used for this unit when it is desired to distinguish clearly between the two quantities. The c.g.s. unit of magnetizing force is usually called the "gilbert per cm."

A unit frequently used is the ampere-turn. It is a convenient unit since it eliminates 4π in certain calculations. It is derived from the "ampere turn per cm." The following table shows the relations between a system built on the ampere-turn and the ordinary magnetic units.¹

TABLE II.
THE ORDINARY AND THE AMPERE-TURN MAGNETIC UNITS.

| Quantity | | Ordinary magnetic units. | Ampere-turn units. | Ordinary units in 1 ampere-turn unit |
|-------------------------|---------------|-------------------------------------|-------------------------------------|--------------------------------------|
| Magnetomotive force | \mathcal{F} | Gilbert | Ampere-turn | $4\pi/10$ |
| Magnetizing force | H | Gilbert per cm | Ampere-turn per cm | $4\pi/10$ |
| Magnetic flux | Φ | Maxwell | Maxwell | 1 |
| Magnetic induction | B | { Maxwell per cm ² Gauss | { Maxwell per cm ² Gauss | 1 |
| Permeability | μ | | | 1 |
| Reluctance | R | Oersted | { Ampere-turn per Maxwell | $4\pi/10$ |
| Magnetization intensity | J | | Maxwell per cm ² | $1/4\pi$ |
| Magnetic susceptibility | κ | | | $1/4\pi$ |
| Magnetic pole strength | m | | Maxwell | $1/4\pi$ |

¹ Dellinger, International System of Electric and Magnetic Units, Bull. Bureau of Standards, 13, p. 599, 1916.

PHYSICAL TABLES

SPELLING AND ABBREVIATIONS OF THE COMMON UNITS OF WEIGHT AND MEASURE

The spelling of the metric units is that adopted by the International Committee on Weights and Measures and given in the law legalizing the metric system in the United States (1866). The period is omitted after the metric abbreviations but not after those of the customary system. The exponents "²" and "³" are used to signify area and volume respectively in the metric units. The use of the same abbreviation for singular and plural is recommended. It is also suggested that only small letters be used for abbreviations except in the case of A. for acre, where the use of the capital letter is general. The following list is taken from circular 47 of the U. S. Bureau of Standards.

| Unit. | Abbreviation. | Unit. | Abbreviation. |
|---------------------|---------------------------|------------------------|---------------------------|
| acre | A | kilogram | kg |
| are | a | kiloliter | kl |
| avoirdupois | av. | kilometer | km |
| barrel | bbl. | link | li. |
| board foot | bd. ft. | liquid | liq. |
| bushel | bu. | liter | l |
| carat, metric | c | meter | m |
| centare | ca | metric ton | t |
| centigram | cg | micron | μ |
| centiliter | cl | mile | mi. |
| centimeter | cm | milligram | mg |
| chain | ch. | milliliter | ml |
| cubic centimeter | cm ³ | millimeter | mm |
| cubic decimeter | dm ³ | millimicron | m μ |
| cubic dekameter | dkm ³ | minim | min. or m |
| cubic foot | cu. ft. | ounce | oz. |
| cubic hectometer | hm ³ | ounce, apothecaries' | oz. ap. or \mathfrak{z} |
| cubic inch | cu. in. | ounce, avoirdupois | oz. av. |
| cubic kilometer | km ³ | ounce, fluid | fl. oz. |
| cubic meter | m ³ | ounce, troy | oz. t. |
| cubic mile | cu. mi. | peck | pk. |
| cubic millimeter | mm ³ | pennyweight | dwt. |
| cubic yard | cu. yd. | pint | pt. |
| decigram | dg | pound | lb. |
| deciliter | dl | pound, apothecaries' | lb. ap. |
| decimeter | dm | pound, avoirdupois | lb. av. |
| decistere | ds | pound, troy | lb. t. |
| dekagram | dkg | quart | qt. |
| dekaliter | dkl | rod | rd. |
| dekameter | dkm | scruple, apothecaries' | s. ap. or \mathfrak{d} |
| dekastere | dks | square centimeter | cm ² |
| dram | dr. | square chain | sq. ch. |
| dram, apothecaries' | dr. ap. or \mathfrak{r} | square decimeter | dm ² |
| dram, avoirdupois | dr. av. | square dekameter | dkm ² |
| dram, fluid | fl. dr. | square foot | sq. ft. |
| fathom | fath. | square hectometer | hm ² |
| foot | ft. | square inch | sq. in. |
| firkin | fir. | square kilometer | km ² |
| furlong | fur. | square meter | m ² |
| gallon | gal. | square mile | sq. mi. |
| grain | gr. | square millimeter | mm ² |
| gram | g | square rod | sq. rd. |
| hectare | ha | square yard | sq. yd. |
| hectogram | hg | stere | s |
| hectoliter | hl | ton | tn. |
| hectometer | hm | ton, metric | t |
| hogshead | hhd. | troy | t. |
| hundredweight | cwt. | yard | yd. |
| inch | in. | | |

FUNDAMENTAL AND DERIVED UNITS

Conversion Factors

To change a quantity from one system of units to another: substitute in the corresponding conversion factor from the following table the ratios of the magnitudes of the *old* units to the *new* and multiply the old quantity by the resulting number. For example: to reduce velocity in miles per hour to feet per second, the conversion factor is l^{-1} ; $l = 5280/1$, $t = 3600/1$, and the factor is $5280/3600$ or 1.467 . Or we may proceed as follows: e. g., to find the equivalent of 1 c.g.s. unit of angular momentum in the pd.ft.m unit, from the Table $1 \text{ g cm}^2/\text{sec.} = x \text{ lb. ft.}^2/\text{min.}$ where x is the factor sought. Solving, $x = 1 \text{ g/lb.} \times \text{cm}^2/\text{ft.}^2 \times \text{min.}/\text{sec.} = 1 \times .002205 \times .001076 \times 60 = .0001425$.

The dimensional formulæ lack one quality which is needed for completeness, an indication of their vector characteristics; such characteristics distinguish plane and solid angle, torque and energy, illumination and brightness.

(a) FUNDAMENTAL UNITS

The fundamental units and conversion factors in the systems of units most commonly used are: Length [l]; Mass [m]; Time [t]; Temperature [θ]; and for the electrostatic system, Dielectric Constant [k]; for the electromagnetic system, Permeability [μ]. The formulæ will also be given for the International System of electric and magnetic units based on the units length, resistance [r], current [i], and time.

(b) DERIVED UNITS

| Name of unit. (Geometrical and dynamical.) | Conversion factor. [$m^x l^y t^z$] | | | Name of units. (Heat and light.) | Conversion factor. [$m^x l^y t^z \theta^r$] | | | |
|---|---|----|----|--|--|----|----|----|
| | x | y | z | | x | y | z | r |
| Area, surface..... | 0 | 2 | 0 | Quantity of heat: | | | | |
| Volume..... | 0 | 3 | 0 | thermal units..... | 1 | 0 | 0 | 1 |
| Angle..... | 0 | 0 | 0 | thermometric units..... | 0 | 3 | 0 | 1 |
| | | | | dynamical units..... | 1 | 2 | -2 | 0 |
| Solid angle..... | 0 | 0 | 0 | | | | | |
| Curvature..... | 0 | -1 | 0 | Coefficient of thermal expansion..... | 0 | 0 | 0 | -1 |
| Angular velocity..... | 0 | 0 | -1 | | | | | |
| Linear velocity..... | 0 | 1 | -1 | Thermal conductivity: | | | | |
| Angular acceleration..... | 0 | 0 | -2 | thermal units..... | 1 | -1 | -1 | 0 |
| Linear acceleration..... | 0 | 1 | -2 | thermometric units or diffusivity..... | 0 | 2 | -1 | 0 |
| | | | | dynamical units..... | 1 | 1 | -3 | -1 |
| Density..... | 1 | -3 | 0 | Thermal capacity..... | 1 | 0 | 0 | 0 |
| Moment of inertia..... | 1 | 2 | 0 | | | | | |
| Intensity of attraction..... | 0 | 1 | -2 | Latent heat: | | | | |
| | | | | thermal units..... | 0 | 0 | 0 | 1 |
| Momentum..... | 1 | 1 | -1 | dynamical units..... | 0 | 2 | -2 | 0 |
| Moment of momentum..... | 1 | 2 | -1 | | | | | |
| Angular momentum..... | 1 | 2 | -1 | Joule's equivalent..... | 0 | 2 | -2 | 1 |
| Force..... | 1 | 1 | -2 | | | | | |
| Moment of couple, torque..... | 1 | 2 | -2 | Entropy: | | | | |
| Work, energy..... | 1 | 2 | -2 | heat in thermal units..... | 1 | 0 | 0 | 0 |
| | | | | heat in dynamical units..... | 1 | 2 | -2 | 1 |
| Power, activity..... | 1 | 2 | -3 | | | | | |
| Intensity of stress..... | 1 | -1 | -2 | Luminous intensity.... | 0 | 0 | 0 | 1* |
| Modulus of elasticity..... | 1 | -1 | -2 | Illumination..... | 0 | -2 | 0 | 1* |
| | | | | Brightness..... | 0 | -2 | 0 | 1* |
| Compressibility..... | -1 | 1 | 2 | Visibility..... | -1 | -2 | 3 | 1* |
| Resilience..... | 1 | -1 | -2 | Luminous efficiency.... | -1 | -2 | 3 | 1* |
| Viscosity..... | 1 | -1 | -1 | | | | | |

* For these formulæ the numbers in the last column are the exponents of F where F refers to the luminous flux. For definitions of these quantities see Table 348, page 333.

FUNDAMENTAL AND DERIVED UNITS

Conversion Factors

(b) DERIVED UNITS

| NAME OF UNIT. (Electric and magnetic.) | Sym- bol.* | CONVERSION FACTOR. | | | | | | | | | | | | | | | | |
|---|---------------|--------------------------|---------------|----|----------------|----------------------------|---------------|----|----------------|------------------|--------------------------|---|----|----|---|---|---|---|
| | | Electrostatic system. | | | | Electromagnetic system. | | | | emu esu † | International system. | | | | x | y | z | v |
| | | $m^2l^2t^2k^2$ | | | | $m^2l^2t^2\mu^2$ | | | | | $r^2i^2t^2v^2$ | | | | | | | |
| | | x | y | z | v | x | y | z | v | | x | y | z | v | | | | |
| Quantity of electricity..... | Q | $\frac{1}{2}$ | $\frac{3}{2}$ | -1 | $\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{1}{2}$ | 0 | $-\frac{1}{2}$ | C | 0 | 1 | 0 | 1 | | | | |
| Electric displacement..... | D | $\frac{1}{2}$ | $\frac{1}{2}$ | -1 | $\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{1}{2}$ | 0 | $-\frac{1}{2}$ | C | 0 | 1 | -2 | 1 | | | | |
| Electric surface density..... | D | $\frac{1}{2}$ | $\frac{1}{2}$ | -1 | $\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{1}{2}$ | 0 | $-\frac{1}{2}$ | C | 0 | 1 | -2 | 1 | | | | |
| Electric field intensity..... | E | $\frac{1}{2}$ | $\frac{1}{2}$ | -1 | $\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{1}{2}$ | -2 | $\frac{1}{2}$ | 1/C | 1 | 1 | 1 | 0 | | | | |
| Electric potential..... | V | $\frac{1}{2}$ | $\frac{1}{2}$ | -1 | $\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{1}{2}$ | -2 | $\frac{1}{2}$ | 1/C | 1 | 1 | 0 | 0 | | | | |
| Electromotive force..... | E | $\frac{1}{2}$ | $\frac{1}{2}$ | -1 | $\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{1}{2}$ | -2 | $\frac{1}{2}$ | 1/C | 1 | 1 | 0 | 0 | | | | |
| Electrostatic capacity..... | C | 0 | 1 | 0 | 1 | 0 | -1 | 2 | -1 | C ² | -1 | 0 | 0 | 0 | | | | |
| Dielectric constant..... | K | 0 | 0 | 0 | 1 | 0 | -2 | 2 | -1 | C ² | -1 | 0 | -1 | 1 | | | | |
| Specific inductive capacity..... | — | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | | | |
| Current..... | I | $\frac{1}{2}$ | $\frac{3}{2}$ | -2 | $\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{1}{2}$ | -1 | $-\frac{1}{2}$ | C | 0 | 1 | 0 | 0 | | | | |
| Electric conductivity..... | γ | 0 | 0 | -1 | 1 | 0 | -2 | 1 | -1 | C ² | -1 | 0 | -1 | 0 | | | | |
| Resistivity..... | ρ | 0 | 0 | 1 | -1 | 0 | 2 | -1 | 1 | 1/C ² | 1 | 0 | 1 | 0 | | | | |
| Conductance..... | g | 0 | 1 | -1 | 1 | 0 | -1 | 1 | -1 | C ² | -1 | 0 | 0 | 0 | | | | |
| Resistance..... | R | 0 | -1 | 1 | -1 | 0 | 1 | -1 | 1 | 1/C ² | 1 | 0 | 0 | 0 | | | | |
| Magnetic pole strength..... | m | $\frac{1}{2}$ | $\frac{1}{2}$ | 0 | $-\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{3}{2}$ | -1 | $\frac{1}{2}$ | 1/C | 1 | 1 | 0 | 1 | | | | |
| Quantity of magnetism..... | m | $\frac{1}{2}$ | $\frac{1}{2}$ | 0 | $-\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{3}{2}$ | -1 | $\frac{1}{2}$ | 1/C | 1 | 1 | 0 | 1 | | | | |
| Magnetic flux..... | Φ | $\frac{1}{2}$ | $\frac{1}{2}$ | 0 | $-\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{3}{2}$ | -1 | $\frac{1}{2}$ | 1/C | 1 | 1 | 0 | 1 | | | | |
| Magnetic field intensity..... | H | $\frac{1}{2}$ | $\frac{1}{2}$ | -2 | $\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{1}{2}$ | -1 | $-\frac{1}{2}$ | C | 0 | 0 | -1 | 0 | | | | |
| Magnetizing force..... | H | $\frac{1}{2}$ | $\frac{1}{2}$ | -2 | $\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{1}{2}$ | -1 | $-\frac{1}{2}$ | C | 0 | 0 | -1 | 0 | | | | |
| Magnetic potential..... | Ω | $\frac{1}{2}$ | $\frac{1}{2}$ | -2 | $\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{1}{2}$ | -1 | $-\frac{1}{2}$ | C | 0 | 1 | 0 | 0 | | | | |
| Magnetomotive force..... | \mathcal{F} | $\frac{1}{2}$ | $\frac{1}{2}$ | -2 | $\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{1}{2}$ | -1 | $-\frac{1}{2}$ | C | 0 | 1 | 0 | 0 | | | | |
| Magnetic moment..... | — | $\frac{1}{2}$ | $\frac{1}{2}$ | 0 | $-\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{3}{2}$ | -1 | $\frac{1}{2}$ | 1/C | 1 | 1 | 1 | 1 | | | | |
| Intensity magnetization..... | — | $\frac{1}{2}$ | $\frac{1}{2}$ | 0 | $-\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{3}{2}$ | -1 | $\frac{1}{2}$ | 1/C | 1 | 1 | -2 | 1 | | | | |
| Magnetic induction..... | B | $\frac{1}{2}$ | $\frac{1}{2}$ | 0 | $-\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{3}{2}$ | -1 | $\frac{1}{2}$ | 1/C | 1 | 1 | -2 | 1 | | | | |
| Magnetic susceptibility..... | κ | 0 | -2 | 2 | -1 | 0 | 0 | 0 | 1 | 1/C ² | 1 | 0 | -1 | 1 | | | | |
| Magnetic permeability..... | μ | 0 | -2 | 2 | -1 | 0 | 0 | 0 | 1 | 1/C ² | 1 | 0 | -1 | 1 | | | | |
| Current density..... | — | $\frac{1}{2}$ | $\frac{1}{2}$ | -2 | $\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{1}{2}$ | -1 | -2 | C | 0 | 1 | -2 | 0 | | | | |
| Self-inductance..... | \mathcal{L} | 0 | -1 | 2 | -1 | 0 | 1 | 0 | 1 | 1/C ² | 1 | 0 | 0 | 1 | | | | |
| Mutual inductance..... | \mathcal{M} | 0 | -1 | 2 | -1 | 0 | 1 | 0 | 1 | 1/C ² | 1 | 0 | 0 | 1 | | | | |
| Magnetic reluctance..... | \mathcal{R} | 0 | 1 | -2 | 1 | 0 | -1 | 0 | -1 | C ² | -1 | 0 | 0 | -1 | | | | |
| Thermoelectric power†..... | — | $\frac{1}{2}$ | $\frac{1}{2}$ | -1 | $-\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{3}{2}$ | -2 | $\frac{1}{2}$ | 1/C | 1 | 1 | 0 | 0 | | | | |
| Peltier coefficient†..... | — | $\frac{1}{2}$ | $\frac{1}{2}$ | -1 | $-\frac{1}{2}$ | $\frac{1}{2}$ | $\frac{3}{2}$ | -2 | $\frac{1}{2}$ | 1/C | 1 | 1 | 0 | 0 | | | | |

* As adopted by American Institute of Electrical Engineers, 1915.

† c is the velocity of an electromagnetic wave in the ether = 3×10^{10} approximately.

‡ This conversion factor should include $[\theta^{-1}]$.

* As adopted by American Institute of Electrical Engineers, 1915.

† c is the velocity of an electromagnetic wave in the ether = 3×10^{10} approximately.‡ This conversion factor should include $[10^{-1}]$.

TABLES FOR CONVERTING U. S. WEIGHTS AND MEASURES*

(1) CUSTOMARY TO METRIC

| LINEAR. | | | | | CAPACITY. | | | | |
|---------|--------------------------------------|-----------------------------------|--------------------------------|-------------------------|--|--|------------------------------|----------------------------------|-----------------------|
| | Inches to millimeters. | Feet to meters. | Yards to meters. | Miles to kilometers. | | Fluid drams to milliliters or cubic centimeters. | Fluid ounces to milliliters. | Liquid quarts to liters. | Gallons to liters. |
| 1 | 25.4001 | 0.304801 | 0.914402 | 1.60935 | 1 | 3.70 | 29.57 | 0.94633 | 3.78533 |
| 2 | 50.8001 | 0.609601 | 1.828804 | 3.21869 | 2 | 7.39 | 59.15 | 1.89267 | 7.57066 |
| 3 | 76.2002 | 0.914402 | 2.743205 | 4.82804 | 3 | 11.09 | 88.72 | 2.83900 | 11.35000 |
| 4 | 101.6002 | 1.219202 | 3.657607 | 6.43739 | 4 | 14.79 | 118.29 | 3.78533 | 15.14133 |
| 5 | 127.0003 | 1.524003 | 4.572009 | 8.04674 | 5 | 18.48 | 147.87 | 4.73167 | 18.92066 |
| 6 | 152.4003 | 1.828804 | 5.486411 | 9.65608 | 6 | 22.18 | 177.44 | 5.67800 | 22.71199 |
| 7 | 177.8004 | 2.133605 | 6.400813 | 11.26543 | 7 | 25.88 | 207.01 | 6.62433 | 26.49733 |
| 8 | 203.2004 | 2.438405 | 7.315215 | 12.87478 | 8 | 29.57 | 236.58 | 7.57066 | 30.28266 |
| 9 | 228.6005 | 2.743205 | 8.229616 | 14.48412 | 9 | 33.27 | 266.16 | 8.51700 | 34.06799 |
| SQUARE. | | | | | WEIGHT. | | | | |
| | Square inches to square centimeters. | Square feet to square decimeters. | Square yards to square meters. | Acres to hectares. | | Grains to milligrams. | Avoirdupois ounces to grams. | Avoirdupois pounds to kilograms. | Troy ounces to grams. |
| 1 | 6.452 | 9.290 | 0.836 | 0.4047 | 1 | 64.7989 | 28.3495 | 0.45359 | 31.10348 |
| 2 | 12.903 | 18.581 | 1.672 | 0.8094 | 2 | 129.5978 | 56.6991 | 0.90718 | 62.20696 |
| 3 | 19.355 | 27.871 | 2.508 | 1.2141 | 3 | 194.3968 | 85.0486 | 1.36078 | 93.31044 |
| 4 | 25.807 | 37.161 | 3.345 | 1.6187 | 4 | 259.1957 | 113.3981 | 1.81437 | 124.41392 |
| 5 | 32.258 | 46.452 | 4.181 | 2.0234 | 5 | 323.9946 | 141.7476 | 2.26796 | 155.51740 |
| 6 | 38.710 | 55.742 | 5.017 | 2.4281 | 6 | 388.7935 | 170.0972 | 2.72155 | 186.62088 |
| 7 | 45.161 | 65.032 | 5.853 | 2.8328 | 7 | 453.5924 | 198.4467 | 3.17515 | 217.72437 |
| 8 | 51.613 | 74.323 | 6.689 | 3.2375 | 8 | 518.3913 | 226.7962 | 3.62874 | 248.82785 |
| 9 | 58.065 | 83.613 | 7.525 | 3.6422 | 9 | 583.1903 | 255.1457 | 4.08233 | 279.93133 |
| CUBIC. | | | | | | | | | |
| | Cubic inches to cubic centimeters. | Cubic feet to cubic meters. | Cubic yards to cubic meters. | Bushels to hectoliters. | | | | | |
| 1 | 16.387 | 0.02832 | 0.765 | 0.35239 | 1 Gunter's chain = 20.1168 meters. | | | | |
| 2 | 32.774 | 0.05663 | 1.529 | 0.70479 | 1 sq. statute mile = 259.000 hectares. | | | | |
| 3 | 49.161 | 0.08495 | 2.294 | 1.05718 | 1 fathom = 1.829 meters. | | | | |
| 4 | 65.549 | 0.11327 | 3.058 | 1.40957 | 1 nautical mile = 1853.25 meters. | | | | |
| 5 | 81.936 | 0.14159 | 3.823 | 1.76196 | 1 foot = 0.304801 meter. | | | | |
| 6 | 98.323 | 0.16990 | 4.587 | 2.11436 | 1 avoirdupois pound = 453.5924277 grams. | | | | |
| 7 | 114.710 | 0.19822 | 5.352 | 2.46675 | 15432.35639 grains = 1.000 kilogram. | | | | |
| 8 | 131.097 | 0.22654 | 6.116 | 2.81914 | | | | | |
| 9 | 147.484 | 0.25485 | 6.881 | 3.17154 | | | | | |

According to an executive order dated April 15, 1893, the United States yard is defined as 3600/3937 meter, and the avoirdupois pound as 1/2.20462 kilogram.

1 meter (international prototype) = 1553164.13 times the wave length of the red Cd. line. Benoit, Fabry and Perot. C. R. 144, 1907 differs only in the decimal portion from the measure of Michelson and Benoit 14 years earlier.

The length of the nautical mile given above and adopted by the U. S. Coast and Geodetic Survey many years ago, is defined as that of a minute of arc of a great circle of a sphere whose surface equals that of the earth (Clarke's Spheroid of 1866).

* Quoted from sheets issued by the United States Bureau of Standards.

TABLES FOR CONVERTING U. S. WEIGHTS AND MEASURES
(2) METRIC TO CUSTOMARY

| LINEAR. | | | | | CAPACITY. | | | | | |
|---------|-------------------|-----------------|------------------|----------------------|-----------|---|-------------------------------|-------------------|-------------------------|--------------------------|
| | Meters to inches. | Meters to feet. | Meters to yards. | Kilometers to miles. | | Milli-liters or cubic centimeters to fluid drams. | Centi-liters to fluid ounces. | Liters to quarts. | Deca-liters to gallons. | Hecto-liters to bushels. |
| 1 | 39.3700 | 3.28083 | 1.093611 | 0.62137 | 1 | 0.27 | 0.338 | 1.0567 | 2.6418 | 2.8378 |
| 2 | 78.7400 | 6.56167 | 2.187222 | 1.24274 | 2 | 0.54 | 0.676 | 2.1134 | 5.2836 | 5.6756 |
| 3 | 118.1100 | 9.84250 | 3.280833 | 1.86411 | 3 | 0.81 | 1.014 | 3.1701 | 7.9253 | 8.5135 |
| 4 | 157.4800 | 13.12333 | 4.374444 | 2.48548 | 4 | 1.08 | 1.353 | 4.2268 | 10.5671 | 11.3512 |
| 5 | 196.8500 | 16.40417 | 5.468056 | 3.10685 | 5 | 1.35 | 1.691 | 5.2836 | 13.2089 | 14.1891 |
| 6 | 236.2200 | 19.68500 | 6.561667 | 3.72822 | 6 | 1.62 | 2.029 | 6.3403 | 15.8507 | 17.0269 |
| 7 | 275.5900 | 22.96583 | 7.655278 | 4.34959 | 7 | 1.89 | 2.367 | 7.3970 | 18.4924 | 19.8647 |
| 8 | 314.9600 | 26.24667 | 8.748889 | 4.97096 | 8 | 2.16 | 2.705 | 8.4537 | 21.1342 | 22.7026 |
| 9 | 354.3300 | 29.52750 | 9.842500 | 5.59233 | 9 | 2.43 | 3.043 | 9.5104 | 23.7760 | 25.5404 |

| SQUARE. | | | | | WEIGHT. | | | | |
|---------|--------------------------------------|-------------------------------|--------------------------------|--------------------|---------|------------------------|-----------------------|------------------------------------|-----------------------------------|
| | Square centimeters to square inches. | Square meters to square feet. | Square meters to square yards. | Hectares to acres. | | Milli-grams to grains. | Kilo-grams to grains. | Hecto-grams to ounces avoirdupois. | Kilo-grams to pounds avoirdupois. |
| 1 | 0.1550 | 10.764 | 1.196 | 2.471 | 1 | 0.01543 | 15432.36 | 3.5274 | 2.20462 |
| 2 | 0.3100 | 21.528 | 2.392 | 4.942 | 2 | 0.03086 | 30864.71 | 7.0548 | 4.40924 |
| 3 | 0.4650 | 32.292 | 3.588 | 7.413 | 3 | 0.04630 | 46297.07 | 10.5822 | 6.61387 |
| 4 | 0.6200 | 43.055 | 4.784 | 9.884 | 4 | 0.06173 | 61729.43 | 14.1096 | 8.81849 |
| 5 | 0.7750 | 53.819 | 5.980 | 12.355 | 5 | 0.07716 | 77161.78 | 17.6370 | 11.02311 |
| 6 | 0.9300 | 64.583 | 7.176 | 14.826 | 6 | 0.09259 | 92594.14 | 21.1644 | 13.22773 |
| 7 | 1.0850 | 75.347 | 8.372 | 17.297 | 7 | 0.10803 | 108026.49 | 24.6918 | 15.43236 |
| 8 | 1.2400 | 86.111 | 9.568 | 19.768 | 8 | 0.12346 | 123458.85 | 28.2192 | 17.63668 |
| 9 | 1.3950 | 96.875 | 10.764 | 22.239 | 9 | 0.13889 | 138891.21 | 31.7466 | 19.84160 |

| CUBIC. | | | | | WEIGHT. | | | |
|--------|------------------------------------|-----------------------------------|-----------------------------|------------------------------|---------|------------------------|----------------------------------|---------------------------|
| | Cubic centimeters to cubic inches. | Cubic decimeters to cubic inches. | Cubic meters to cubic feet. | Cubic meters to cubic yards. | | Quintals to pounds av. | Milliers or tonnes to pounds av. | Kilograms to ounces Troy. |
| 1 | 0.0610 | 61.023 | 35.314 | 1.308 | 1 | 220.46 | 2204.6 | 32.1507 |
| 2 | 0.1220 | 122.047 | 70.609 | 2.616 | 2 | 440.92 | 4409.2 | 64.3015 |
| 3 | 0.1831 | 183.070 | 105.943 | 3.924 | 3 | 661.39 | 6613.9 | 96.4522 |
| 4 | 0.2441 | 244.094 | 141.258 | 5.232 | 4 | 881.85 | 8818.5 | 128.6030 |
| 5 | 0.3051 | 305.117 | 176.572 | 6.540 | 5 | 1102.31 | 11023.1 | 160.7537 |
| 6 | 0.3661 | 366.140 | 211.887 | 7.848 | 6 | 1322.77 | 13227.7 | 192.9045 |
| 7 | 0.4272 | 427.164 | 247.201 | 9.156 | 7 | 1543.24 | 15432.4 | 225.0552 |
| 8 | 0.4882 | 488.187 | 282.516 | 10.464 | 8 | 1763.70 | 17637.0 | 257.2059 |
| 9 | 0.5492 | 549.210 | 317.830 | 11.771 | 9 | 1984.16 | 19841.6 | 289.3567 |

By the concurrent action of the principal governments of the world an International Bureau of Weights and Measures has been established near Paris. Under the direction of the International Committee, two ingots were cast of pure platinum-iridium in the proportion of 9 parts of the former to 1 of the latter metal. From one of these a certain number of kilograms were prepared, from the other a definite number of meter bars. These standards of weight and length were intercompared, without preference, and certain ones were selected as International prototype standards. The others were distributed by lot, in September, 1889, to the different governments, and are called National prototype standards. Those apportioned to the United States were received in 1890, and are kept at the Bureau of Standards in Washington, D. C.

The metric system was legalized in the United States in 1866.

The International Standard Meter is derived from the Mètre des Archives, and its length is defined by the distance between two lines at 0° Centigrade, on a platinum-iridium bar deposited at the International Bureau of Weights and Measures.

The International Standard Kilogram is a mass of platinum-iridium deposited at the same place, and its weight in vacuo is the same as that of the Kilogram des Archives.

The liter is equal to the quantity of pure water at 4° C. (760 mm Hg. pressure) which weighs 1 kilogram and = 1.000027 cu. dm. (Trav. et Mem. Bureau Intern. des P. et M. 14, 1910, Benoit.)

MISCELLANEOUS EQUIVALENTS OF U. S. AND METRIC WEIGHTS AND MEASURES *

(For other equivalents than those below, see Table 3.)

LINEAR MEASURES.

| |
|--|
| 1 mil (.001 in.) = 25.4001 μ |
| 1 in. = .000015783 mile |
| 1 hand (4 in.) = 10.16002 cm |
| 1 link (.66 ft.) = 20.11684 cm |
| 1 span (9 in.) = 22.86005 cm |
| 1 fathom (6 ft.) = 1.828804 m |
| 1 rod (25 links) = 5.020210 m |
| 1 chain (4 rods) = 20.11684 m |
| 1 light year (9.5×10^{12} km) = 5.9×10^{12} miles |
| 1 parsec (31×10^{12} km) = 19×10^{12} miles |
| $\frac{1}{4}$ in. = .397 mm $\frac{1}{8}$ in. = .704 mm |
| $\frac{1}{16}$ in. = 1.588 mm $\frac{1}{4}$ in. = 3.175 mm |
| $\frac{1}{8}$ in. = 6.350 mm $\frac{1}{2}$ in. = 12.700 mm |
| 1 Angstrom unit = .0000000001 m |
| 1 micron (μ) = .000001 m = .00003937 in. |
| 1 millimicron (m μ) = .000000001 m |
| 1 m = 4.970960 links = 1.093611 yds. |
| = .198838 rod = .0497096 chain |

SQUARE MEASURES.

| |
|---|
| 1 sq. link (62.7264 sq. in.) = 404.6873 cm ² |
| 1 sq. rod (625 sq. links) = 25.29295 m ² |
| 1 sq. chain (16 sq. rods) = 404.6873 m ² |
| 1 acre (10 sq. chains) = 4046.873 m ² |
| 1 sq. mile (640 acres) = 2.580998 km ² |
| 1 km ² = .3861006 sq. mile |
| 1 m ² = 24.7104 sq. links = 10.76387 sq. ft. |
| = .039537 sq. rod = .00247104 sq. chain |

CUBIC MEASURES.

| |
|---|
| 1 board foot (144 cu. in.) = 2359.8 cm ³ |
| 1 cord (128 cu. ft.) = 3.625 m ³ |

CAPACITY MEASURES.

| |
|---|
| 1 minim (M) = .0616102 ml |
| 1 fl. dram (60M) = 3.69661 ml |
| 1 fl. oz. (8 fl. dr.) = 1.80469 cu. in. |
| = 29.5729 ml |
| 1 gill (4 fl. oz.) = 7.21875 cu. in. = 118.292 ml |
| 1 liq. pt. (28.875 cu. in.) = .473167 l |
| 1 liq. qt. (57.75 cu. in.) = .946333 l |
| 1 gallon (4 qt., 231 cu. in.) = 3.785332 l |
| 1 dry pt. (33.6003125 cu. in.) = .550590 l |
| 1 dry qt. (67.200625 cu. in.) = 1.101198 l |
| 1 pk. (8 dry qt., 537.605 cu. in.) = 8.80958 l |
| 1 bu. (4 pk., 2150.42 cu. in.) = 35.2383 l |
| 1 firkin (9 gallons) = 34.06799 l |
| 1 liter = .264178 gal. = 1.05671 liq. qt. |
| = 33.8147 fl. oz. = 270.518 fl. dr. |
| 1 ml = 16.2311 minims. |
| 1 dkl = 18.620 dry pt. = 9.08102 dry qt. |
| = 1.13513 pk. = .28378 bu. |

MASS MEASURES.

Avoirdupois weights.

| |
|---|
| 1 grain = .064708918 g |
| 1 dram av. (27.34375 gr.) = 1.771845 g |
| 1 oz. av. (16 dr. av.) = 28.340527 g |
| 1 lb. av. (16 oz. av. or 7000 gr.) |
| = 14.583333 oz. ap. ($\frac{3}{4}$) or oz. t. |
| = 1.2152778 or 7000/5760 lb. ap. |
| or t. |
| = 453.5924277 g |
| 1 kg = 2.204622341 lb. av. |
| 1 g = 15.432356 gr. = .5643833 dr. av. |
| = .03527396 oz. av. |
| 1 short hundred weight (100 lb.) |
| = 45.359243 kg |
| 1 long hundred weight (112 lb.) |
| = 50.802352 kg |
| 1 short ton (2000 lb.) |
| = 907.18486 kg |
| 1 long ton (2240 lb.) |
| = 1016.04704 kg |
| 1 metric ton = 0.08420640 long ton |
| = 1.1023112 short tons |

Troy weights.

| |
|--|
| 1 pennyweight (dwt., 24 gr.) = 1.555174 g; |
| gr., oz., pd. are same as apothecary |

Apothecaries' weights.

| |
|--------------------------------------|
| 1 gr. = 64.708918 mg |
| 1 scruple (℥, 20 gr.) = 1.2059784 g |
| 1 dram (℥, 3 ℥) = 3.8879351 g |
| 1 oz. (℥, 8 ℥) = 31.103481 g |
| 1 lb. (12 ℥, 5760 gr.) = 373.24177 g |
| 1 g = 15.432356 gr. = 0.771618 ℥ |
| = 0.2572059 ℥ = .03215074 ℥ |
| 1 kg = 32.150742 ℥ = 2.6792285 lb. |

| |
|---|
| 1 metric carat = 200 mg = 3.0864712 gr. |
|---|

U. S. $\frac{1}{2}$ dollar should weigh 12.5 g and the smaller silver coins in proportion.

* Taken from Circular 47 of the U. S. Bureau of Standards, 1915, which see for more complete tables.

EQUIVALENTS OF METRIC AND BRITISH IMPERIAL WEIGHTS AND MEASURES*

(1) METRIC TO IMPERIAL

(For U. S. Weights and Measures, see Table 3)

LINEAR MEASURE.

| | |
|-------------------------|------------------------|
| 1 millimeter (mm) | } = 0.03937 in. |
| (.001 m) | |
| 1 centimeter (.01 m) | = 0.39370 " |
| 1 decimeter (.1 m) | = 3.93701 " |
| 1 METER (m) | . . . = { 39.370113 " |
| | { 3.280843 ft. |
| | { 1.09361425 yds. |
| 1 dekameter (10 m) | } . . = 10.93614 " |
| 1 hectometer (100 m) | } . . = 109.361425 " |
| 1 kilometer (1,000 m) | } . . = 0.62137 mile. |
| 1 myriameter (10,000 m) | } . . = 6.21372 miles. |
| 1 micron | = 0.001 mm. |

SQUARE MEASURE.

| | |
|--------------------------------------|---------------------|
| 1 sq. centimeter . . | = 0.1550 sq. in. |
| 1 sq. decimeter (100 sq. cm) | } = 15.500 sq. in. |
| 1 sq. meter or centiare (100 sq. dm) | = { 10.7639 sq. ft. |
| | { 1.1960 sq. yds. |
| 1 ARE (100 sq. m) | = 119.60 sq. yds. |
| 1 hectare (100 ares or 10,000 sq. m) | } = 2.4711 acres. |

CUBIC MEASURE.

| | |
|---|---------------------------|
| 1 cu. centimeter (cc) (1,000 cubic millimeters) | } = 0.0610 cu. in. |
| 1 cu. decimeter (cd) (1,000 cubic centimeters) | } = 61.024 " " |
| 1 CU. METER or stere (1,000 cd) | } . . = { 35.3148 cu. ft. |
| | { 1.307954 cu. yds. |

MEASURE OF CAPACITY.

| | |
|--|--------------------|
| 1 milliliter (ml) (.001 liter) | } = 0.0610 cu. in. |
| 1 centiliter (.01 liter) | = { 0.61024 " " |
| | { 0.070 gill. |
| 1 deciliter (.1 liter) | = 0.176 pint. |
| 1 LITER (1,000 cu. centimeters or 1 cu. decimeter) | } = 1.75980 pints. |
| 1 dekaliter (10 liters) | = 2.200 gallons. |
| 1 hectoliter (100 ") | = 2.75 bushels. |
| 1 kiloliter (1,000 ") | = 3.437 quarters. |

APOTHECARIES' MEASURE.

| | |
|---------------------------------|---------------------------|
| 1 cubic centimeter (1 gram w't) | = { 0.03520 fluid ounce. |
| | { 0.28157 fluid drachm. |
| 1 cu. millimeter | = 15.43236 grains weight. |
| | = 0.01693 minim. |

AVOIRDUPOIS WEIGHT.

| | |
|-------------------------------|----------------------|
| 1 milligram (mg) | . . = 0.01543 grain. |
| 1 centigram (.01 gram) | = 0.15432 " |
| 1 decigram (.1 ") | = 1.54324 grains. |
| 1 GRAM | = 15.43236 " |
| 1 dekagram (10 grams) | = 5.64383 drams. |
| 1 hectogram (100 ") | = 3.52739 oz. |
| 1 KILOGRAM (1,000 ") | = { 2.2046223 lb. |
| | { 15432.3564 grains. |
| 1 myriagram (10 kg) | = 22.04622 lbs. |
| 1 quintal (100 ") | = 1.96841 cwt. |
| 1 millier or tonne (1,000 kg) | } . . = 0.9842 ton. |

TROY WEIGHT.

| | |
|------------------|------------------------|
| 1 GRAM | = { 0.03215 oz. Troy. |
| | { 0.64301 pennyweight. |
| | { 15.43236 grains. |

APOTHECARIES' WEIGHT.

| | |
|------------------|---------------------|
| 1 GRAM | = { 0.25721 drachm. |
| | { 0.77162 scruple. |
| | { 15.43236 grains. |

NOTE.—The METER is the length, at the temperature of 0° C, of the platinum-iridium bar deposited at the International Bureau of Weights and Measures at Sèvres, near Paris, France.

The present legal equivalent of the meter is 39.370113 inches, as above stated.

The KILOGRAM is the mass of a platinum-iridium weight deposited at the same place.

The LITER contains one kilogram weight of distilled water at its maximum density (4° C), the barometer being at 760 millimeters.

* In accordance with the schedule adopted under the Weights and Measures (metric system) Act, 1897.

EQUIVALENTS OF METRIC AND BRITISH IMPERIAL WEIGHTS AND MEASURES

(2) METRIC TO IMPERIAL, MULTIPLES

(For U. S. Weights and Measures, see Table 3)

| LINEAR MEASURE. | | | | | MEASURE OF CAPACITY. | | | | |
|-----------------|------------------------------|-----------------------|------------------------|------------------------------|----------------------|------------------------|------------------------------|-------------------------------|-------------------------------|
| | Millimeters to inches. | Meters to feet. | Meters to yards. | Kilo- meters to miles. | | Liters to pints. | Dekaliters to gallons. | Hectoliters to bushels. | Kiloliters to quarters. |
| 1 | 0.03937011 | 3.28084 | 1.09361 | 0.62137 | 1 | 1.75980 | 2.19975 | 2.74969 | 3.43712 |
| 2 | 0.07874023 | 6.56169 | 2.18723 | 1.24274 | 2 | 3.51961 | 4.39951 | 5.49938 | 6.87423 |
| 3 | 0.11811034 | 9.84253 | 3.28084 | 1.86412 | 3 | 5.27941 | 6.59926 | 8.24908 | 10.31135 |
| 4 | 0.15748045 | 13.12337 | 4.37440 | 2.48540 | 4 | 7.03921 | 8.79902 | 10.99877 | 13.74840 |
| 5 | 0.19685056 | 16.40421 | 5.46807 | 3.10686 | 5 | 8.79902 | 10.99877 | 13.74846 | 17.18558 |
| 6 | 0.23622068 | 19.68506 | 6.56169 | 3.72823 | 6 | 10.55882 | 13.19852 | 16.49815 | 20.62269 |
| 7 | 0.27559079 | 22.06590 | 7.05530 | 4.34960 | 7 | 12.31862 | 15.39828 | 19.24785 | 24.05981 |
| 8 | 0.31496090 | 26.24674 | 8.74891 | 4.97097 | 8 | 14.07842 | 17.59803 | 21.99754 | 27.49692 |
| 9 | 0.35433102 | 29.52758 | 9.84253 | 5.59235 | 9 | 15.83823 | 19.79778 | 24.74723 | 30.93404 |

| SQUARE MEASURE. | | | | | WEIGHT (AVOIRDUPOIS). | | | | |
|-----------------|---|--|---|-----------------------|-----------------------|----------------------------------|-------------------------|---------------------------------|--|
| | Square centimeters to square inches. | Square meters to square feet. | Square meters to square yards. | Hectares to acres. | | Milli- grams to grains. | Kilograms to grains. | Kilo- grams to pounds. | Quintals to hundred- weights. |
| 1 | 0.15500 | 10.76393 | 1.19599 | 2.4711 | 1 | 0.01543 | 15432.356 | 2.20462 | 1.96841 |
| 2 | 0.31000 | 21.52786 | 2.39198 | 4.9421 | 2 | 0.03086 | 30864.713 | 4.40924 | 3.93683 |
| 3 | 0.46500 | 32.29179 | 3.58798 | 7.4132 | 3 | 0.04630 | 46297.069 | 6.61387 | 5.90524 |
| 4 | 0.62000 | 43.05572 | 4.78397 | 9.8842 | 4 | 0.06173 | 61729.426 | 8.81849 | 7.87365 |
| 5 | 0.77500 | 53.81965 | 5.97996 | 12.3553 | 5 | 0.07716 | 77161.782 | 11.02311 | 9.84206 |
| 6 | 0.93000 | 64.58357 | 7.17595 | 14.8263 | 6 | 0.09259 | 92504.138 | 13.22773 | 11.81048 |
| 7 | 1.08500 | 75.34750 | 8.37194 | 17.2974 | 7 | 0.10803 | 108026.495 | 15.43236 | 13.77889 |
| 8 | 1.24000 | 86.11143 | 9.56794 | 19.7685 | 8 | 0.12346 | 123458.851 | 17.63668 | 15.74730 |
| 9 | 1.39501 | 96.87536 | 10.76393 | 22.2395 | 9 | 0.13889 | 138891.268 | 19.84160 | 17.71572 |

| CUBIC MEASURE. | | | | | APOTHE- CARIES' MEASURE. | AVOIRDUPOIS (cont.) | | TROY WEIGHT. | APOTHE- CARIES' WEIGHT. |
|----------------|--|--------------------------------------|---------------------------------------|---|--------------------------------|-----------------------------------|-----------------------------|--------------------------------|-------------------------------|
| | Cubic decimeters to cubic inches. | Cubic meters to cubic feet. | Cubic meters to cubic yards. | Cub. cen- timeters to fluid drachms. | | Milliers or tonnes to tons. | Grams to ounces Troy. | Grams to penny- weights. | Grams to scruples. |
| 1 | 61.02390 | 35.31476 | 1.30795 | 0.28157 | 1 | 0.98421 | 0.03215 | 0.64301 | 0.77162 |
| 2 | 122.04781 | 70.62952 | 2.61591 | 0.56314 | 2 | 1.96841 | 0.06430 | 1.28603 | 1.54324 |
| 3 | 183.07171 | 105.94428 | 3.92386 | 0.84471 | 3 | 2.95262 | 0.09645 | 1.92904 | 2.31485 |
| 4 | 244.09561 | 141.25904 | 5.23182 | 1.12627 | 4 | 3.93683 | 0.12860 | 2.57206 | 3.08647 |
| 5 | 305.11952 | 176.57379 | 6.53977 | 1.40784 | 5 | 4.92103 | 0.16075 | 3.21507 | 3.85809 |
| 6 | 366.14342 | 211.88855 | 7.84777 | 1.68941 | 6 | 5.90524 | 0.19290 | 3.85800 | 4.62971 |
| 7 | 427.16732 | 247.20331 | 9.15568 | 1.97098 | 7 | 6.88944 | 0.22506 | 4.50110 | 5.40132 |
| 8 | 488.19123 | 282.51807 | 10.46363 | 2.25255 | 8 | 7.87365 | 0.25721 | 5.14412 | 6.17204 |
| 9 | 549.21513 | 317.83283 | 11.77159 | 2.53412 | 9 | 8.85786 | 0.28936 | 5.78713 | 6.94456 |

EQUIVALENTS OF BRITISH IMPERIAL AND METRIC WEIGHTS AND MEASURES

(3) IMPERIAL TO METRIC

(For U. S. Weights and Measures, see Table 3)

LINEAR MEASURE.

| | | |
|------------------------------------|-----------|---|
| 1 inch | = | $\left\{ \begin{array}{l} 25.400 \text{ milli-} \\ \text{meters.} \end{array} \right.$ |
| 1 foot (12 in.) | = | 0.30480 meter. |
| 1 YARD (3 ft.) | = | 0.914399 " |
| 1 pole (5½ yd.) | = | 5.0292 meters. |
| 1 chain (22 yd. or } 100 links) | = | 20.1168 " |
| 1 furlong (220 yd.) = | 201.168 " | |
| 1 mile (1,760 yd.) | = | $\left\{ \begin{array}{l} 1.6093 \text{ kilo-} \\ \text{meters.} \end{array} \right.$ |
| 1 yard | = | $\left\{ \begin{array}{l} 1420210. \times \text{Cd.}\lambda. \\ \text{(Tutton 1932)} \end{array} \right.$ |

SQUARE MEASURE.

| | | |
|---------------------------|---|--|
| 1 square inch | = | $\left\{ \begin{array}{l} 6.4516 \text{ sq. cen-} \\ \text{timeters.} \end{array} \right.$ |
| 1 sq. ft. (144 sq. in.) = | $\left\{ \begin{array}{l} 9.2903 \text{ sq. deci-} \\ \text{meters.} \end{array} \right.$ | |
| 1 SQ. YARD (9 sq. ft.) = | $\left\{ \begin{array}{l} 0.836126 \text{ sq.} \\ \text{meters.} \end{array} \right.$ | |
| 1 perch (30¼ sq. yd.) = | $\left\{ \begin{array}{l} 25.293 \text{ sq. me-} \\ \text{ters.} \end{array} \right.$ | |
| 1 rood (40 perches) = | 10.117 ares. | |
| 1 ACRE (4840 sq. yd.) = | 0.40468 hectare. | |
| 1 sq. mile (640 acres) = | 259.00 hectares. | |

CUBIC MEASURE.

| | |
|--------------------------------|---|
| 1 cu. inch = | 16.387 cu. centimeters. |
| 1 cu. foot (1728 } cu. in.) | = $\left\{ \begin{array}{l} 0.028317 \text{ cu. me-} \\ \text{ter, or } 28.317 \\ \text{cu. decimeters.} \end{array} \right.$ |
| 1 CU. YARD (27 } cu. ft.) | = 0.76455 cu. meter. |

APOTHECARIES' MEASURE.

| | | |
|---|---|---|
| 1 gallon (8 pints or } 160 fluid ounces) | = | 4.5459631 liters. |
| 1 fluid ounce, f 3 } (8 drachms) | = | $\left\{ \begin{array}{l} 28.4123 \text{ cubic} \\ \text{centimeters.} \end{array} \right.$ |
| 1 fluid drachm, f 5 } (60 minims) | = | $\left\{ \begin{array}{l} 3.5515 \text{ cubic} \\ \text{centimeters.} \end{array} \right.$ |
| 1 minim, m (0.01146 } grain weight) | = | $\left\{ \begin{array}{l} 0.05919 \text{ cubic} \\ \text{centimeters.} \end{array} \right.$ |

NOTE.—The Apothecaries' gallon is of the same capacity as the Imperial gallon.

MEASURE OF CAPACITY.

| | | |
|-----------------------------|--------------------|-------------------|
| 1 gill | = | 1.42 deciliters. |
| 1 pint (4 gills) | = | 0.568 liter. |
| 1 quart (2 pints) | = | 1.136 liters. |
| 1 GALLON (4 quarts) = | 4.5459631 " | |
| 1 peck (2 gal.) | = | 9.092 " |
| 1 bushel (8 gal.) | = | 3.637 dekaliters. |
| 1 quarter (8 bushels) = | 2.909 hectoliters. | |

AVOIRDUPOIS WEIGHT.

| | | |
|---------------------------------------|---|--|
| 1 grain | = | $\left\{ \begin{array}{l} 64.8 \text{ milli-} \\ \text{grams.} \end{array} \right.$ |
| 1 dram | = | 1.772 grams. |
| 1 ounce (16 dr.) | = | 28.350 " |
| 1 POUND (16 oz. or } 7,000 grains) | = | 0.45359243 kg. |
| 1 stone (14 lb.) | = | 6.350 " |
| 1 quarter (28 lb.) | = | 12.70 " |
| 1 hundredweight { (112 lb.) | = | $\left\{ \begin{array}{l} 50.80 \\ 0.5080 \text{ quintal.} \end{array} \right.$ |
| 1 ton (20 cwt.) | = | $\left\{ \begin{array}{l} 1.0160 \text{ tonnes} \\ \text{or } 1016 \text{ kilo-} \\ \text{grams.} \end{array} \right.$ |

TROY WEIGHT.

| | | |
|------------------------------------|---|----------------|
| 1 TROY OUNCE (480 } grains av.) | = | 31.1035 grams. |
| 1 pennyweight (24 } grains) | = | 1.5552 " |

NOTE.—The Troy grain is of the same weight as the Avoirdupois grain.

APOTHECARIES' WEIGHT.

| | |
|-----------------------------------|----------------|
| 1 ounce (8 drachms) = | 31.1035 grams. |
| 1 drachm, 3i (3 scrup- } ples) | = 3.888 " |
| 1 scruple, ʒi (20 } grains) | = 1.296 " |

NOTE.—The Apothecaries' ounce is of the same weight as the Troy ounce. The Apothecaries' grain is also of the same weight as the Avoirdupois grain.

NOTE.—The YARD is the length at 62° F., marked on a bronze bar deposited with the Board of Trade. The POUND is the weight of a piece of platinum weighed in vacuo at the temperature of 0° C., and which is also deposited with the Board of Trade. The GALLON contains 10 lb. weight of distilled water at the temperature of 62° F., the barometer being at 30 inches.

TABLE 5 (concluded)

11

EQUIVALENTS OF BRITISH IMPERIAL AND METRIC WEIGHTS AND MEASURES

(4) IMPERIAL TO METRIC, MULTIPLES

(For U. S. Weights and Measures, see Table 3)

| LINEAR MEASURE. | | | | | MEASURE OF CAPACITY. | | | | |
|------------------------|---|--|---|---|-----------------------|-----------------------------------|--------------------------|--------------------------------|-------------------------------------|
| | Inches to centimeters. | Feet to meters. | Yards to meters. | Miles to kilo- meters. | | Quarts to liters. | Gallons to liters. | Bushels to dekaliters. | Quarters to hectoliters. |
| 1 | 2.539998 | 0.30480 | 0.91440 | 1.60934 | 1 | 1.13649 | 4.54596 | 3.63677 | 2.90942 |
| 2 | 5.079996 | 0.60960 | 1.82880 | 3.21869 | 2 | 2.27298 | 9.09193 | 7.27354 | 5.81883 |
| 3 | 7.619993 | 0.91440 | 2.74320 | 4.82803 | 3 | 3.40947 | 13.63789 | 10.91031 | 8.72825 |
| 4 | 10.159991 | 1.21920 | 3.65760 | 6.43737 | 4 | 4.54596 | 18.18385 | 14.54708 | 11.63767 |
| 5 | 12.699989 | 1.52400 | 4.57200 | 8.04671 | 5 | 5.68245 | 22.72982 | 18.18385 | 14.54708 |
| 6 | 15.239987 | 1.82880 | 5.48640 | 9.65606 | 6 | 6.81894 | 27.27578 | 21.82062 | 17.45650 |
| 7 | 17.779984 | 2.13360 | 6.40080 | 11.26540 | 7 | 7.95544 | 31.82174 | 25.45739 | 20.36591 |
| 8 | 20.319982 | 2.43840 | 7.31519 | 12.87474 | 8 | 9.09193 | 36.36770 | 29.09416 | 23.27533 |
| 9 | 22.859980 | 2.74320 | 8.22959 | 14.48408 | 9 | 10.22842 | 40.91367 | 32.73993 | 26.18475 |
| SQUARE MEASURE. | | | | | WEIGHT (AVOIRDUPOIS). | | | | |
| | Square inches to square centimeters. | Square feet to square decimeters. | Square yards to square meters. | Acres to hectares. | | Grains to milli- grams. | Ounces to grams. | Pounds to kilo- grams. | Hundred- weights to quintals. |
| 1 | 6.45159 | 9.29029 | 0.83613 | 0.40468 | 1 | 64.79892 | 28.34953 | 0.45359 | 0.50802 |
| 2 | 12.90318 | 18.58058 | 1.67225 | 0.80937 | 2 | 129.59784 | 56.69905 | 0.90718 | 1.01605 |
| 3 | 19.35477 | 27.87086 | 2.50838 | 1.21405 | 3 | 194.39675 | 85.04858 | 1.36078 | 1.52407 |
| 4 | 25.80636 | 37.16115 | 3.34450 | 1.61874 | 4 | 259.19567 | 113.39811 | 1.81437 | 2.03209 |
| 5 | 32.25794 | 46.45144 | 4.18063 | 2.02342 | 5 | 323.99459 | 141.74763 | 2.26796 | 2.54012 |
| 6 | 38.70953 | 55.74173 | 5.01676 | 2.42811 | 6 | 388.79351 | 170.09716 | 2.72155 | 3.04814 |
| 7 | 45.16112 | 65.03201 | 5.85288 | 2.83279 | 7 | 453.59243 | 198.44669 | 3.17515 | 3.55616 |
| 8 | 51.61271 | 74.32230 | 6.68901 | 3.23748 | 8 | 518.39135 | 226.79621 | 3.62874 | 4.06419 |
| 9 | 58.06430 | 83.61259 | 7.52513 | 3.64216 | 9 | 583.19026 | 255.14574 | 4.08233 | 4.57221 |
| CUBIC MEASURE. | | | | | TROY WEIGHT | | | | |
| | Cubic inches to cubic centimeters. | Cubic feet to cubic meters. | Cubic yards to cubic meters. | Fluid drachms to cubic centi- meters. | | Tons to milliers or tonnes. | Ounces to grams. | Penny- weights to grams. | Scruples to grams. |
| 1 | 16.38702 | 0.02832 | 0.76455 | 3.55153 | 1 | 1.01605 | 31.10348 | 1.55517 | 1.29598 |
| 2 | 32.77404 | 0.05663 | 1.52911 | 7.10307 | 2 | 2.03209 | 62.20696 | 3.11035 | 2.59196 |
| 3 | 49.16106 | 0.08495 | 2.29366 | 10.65460 | 3 | 3.04814 | 93.31044 | 4.66552 | 3.88794 |
| 4 | 65.54808 | 0.11327 | 3.05821 | 14.20613 | 4 | 4.06419 | 124.41392 | 6.22070 | 5.18391 |
| 5 | 81.93511 | 0.14158 | 3.82276 | 17.75767 | 5 | 5.08024 | 155.51740 | 7.77587 | 6.47989 |
| 6 | 98.32213 | 0.16990 | 4.58732 | 21.30920 | 6 | 6.09628 | 186.62088 | 9.33104 | 7.77587 |
| 7 | 114.70915 | 0.19822 | 5.35187 | 24.86074 | 7 | 7.11233 | 217.72437 | 10.88622 | 9.07185 |
| 8 | 131.09617 | 0.22653 | 6.11642 | 28.41227 | 8 | 8.12838 | 248.82785 | 12.44139 | 10.36783 |
| 9 | 147.48319 | 0.25485 | 6.88098 | 31.96380 | 9 | 9.14442 | 279.93133 | 13.99657 | 11.66381 |
| APOTHECARIES' MEASURE. | | | | | APOTHECARIES' WEIGHT | | | | |
| | | | | | | | | | |

SMITHSONIAN TABLES.

DERIVATIVES AND INTEGRALS *

| | | | |
|--------------------------------|---|------------------------------------|---|
| $d ax$ | $= a dx$ | $\int x^n dx$ | $= \frac{x^{n+1}}{n+1}$, unless $n = -1$ |
| $d uv$ | $= \left(u \frac{dv}{dx} + v \frac{du}{dx} \right) dx$ | $\int \frac{dx}{x}$ | $= \log x$ |
| $d \frac{u}{v}$ | $= \left(\frac{v \frac{du}{dx} - u \frac{dv}{dx}}{v^2} \right) dx$ | $\int e^x dx$ | $= e^x$ |
| $d x^n$ | $= nx^{n-1} dx$ | $\int e^{ax} dx$ | $= \frac{1}{a} e^{ax}$ |
| $d f(u)$ | $= d \frac{f(u)}{du} \cdot \frac{du}{dx} dx$ | $\int x^m e^{ax} dx$ | $= \frac{x^m e^{ax}}{a} - \frac{m}{a} \int x^{m-1} e^{ax} dx$ |
| $d e^x$ | $= e^x dx$ | $\int \log x dx$ | $= x \log x - x$ |
| $d e^{ax}$ | $= a e^{ax} dx$ | $\int u dv$ | $= u v - \int v du$ |
| $d \log_e x$ | $= \frac{1}{x} dx$ | $\int (a+bx)^n dx$ | $= \frac{(a+bx)^{n+1}}{(n+1)b}$ |
| $d x^x$ | $= x^x (1 + \log_e x) dx$ | $\int (a^2+x^2)^{-1} dx$ | $= \frac{1}{a} \tan^{-1} \frac{x}{a} =$ $\frac{1}{a} \sin^{-1} \frac{x}{\sqrt{x^2+a^2}}$ |
| $d \sin x$ | $= \cos x dx$ | $\int (a^2-x^2)^{-1} dx$ | $= \frac{1}{2a} \log \frac{a+x}{a-x}$ |
| $d \cos x$ | $= -\sin x dx$ | $\int (a^2-x^2)^{-\frac{1}{2}} dx$ | $= \sin^{-1} \frac{x}{a}$, or $-\cos^{-1} \frac{x}{a}$ |
| $d \tan x$ | $= \sec^2 x dx$ | $\int x(a^2 \pm x^2)^{-1} dx$ | $= \pm (a^2 \pm x^2)^{-\frac{1}{2}}$ |
| $d \cot x$ | $= -\csc^2 x dx$ | $\int \sin^2 x dx$ | $= -\frac{1}{2} \cos x \sin x + \frac{1}{2} x$ |
| $d \sec x$ | $= \tan x \sec x dx$ | $\int \cos^2 x dx$ | $= \frac{1}{2} \sin x \cos x + \frac{1}{2} x$ |
| $d \csc x$ | $= -\cot x \csc x dx$ | $\int \sin x \cos x dx$ | $= \frac{1}{2} \sin^2 x$ |
| $d \sin^{-1} x$ | $= (1-x^2)^{-\frac{1}{2}} dx$ | $\int (\sin x \cos x)^{-1} dx$ | $= \log \tan x$ |
| $d \cos^{-1} x$ | $= -(1-x^2)^{-\frac{1}{2}} dx$ | $\int \tan x dx$ | $= -\log \cos x$ |
| $d \tan^{-1} x$ | $= (1+x^2)^{-1} dx$ | $\int \tan^2 x dx$ | $= \tan x - x$ |
| $d \cot^{-1} x$ | $= -(1+x^2)^{-1} dx$ | $\int \cot x dx$ | $= \log \sin x$ |
| $d \sec^{-1} x$ | $= x^{-1} (x^2-1)^{-\frac{1}{2}} dx$ | $\int \cot^2 x dx$ | $= -\cot x - x$ |
| $d \csc^{-1} x$ | $= -x^{-1} (x^2-1)^{-\frac{1}{2}} dx$ | $\int \csc x dx$ | $= \log \tan \frac{1}{2} x$ |
| $d \sinh x$ | $= \cosh x dx$ | $\int x \sin x dx$ | $= \sin x - x \cos x$ |
| $d \cosh x$ | $= \sinh x dx$ | $\int x \cos x dx$ | $= \cos x + x \sin x$ |
| $d \tanh x$ | $= \operatorname{sech}^2 x dx$ | $\int \tanh x dx$ | $= \log \cosh x$ |
| $d \coth x$ | $= -\operatorname{csch}^2 x dx$ | $\int \coth x dx$ | $= \log \sinh x$ |
| $d \operatorname{sech} x$ | $= -\operatorname{sech} x \tanh x dx$ | $\int \operatorname{sech} x dx$ | $= 2 \tan^{-1} e^x = \operatorname{gd} u$ |
| $d \operatorname{csch} x$ | $= -\operatorname{csch} x \cdot \coth x dx$ | $\int \operatorname{csch} x dx$ | $= \log \tanh \frac{x}{2}$ |
| $d \sinh^{-1} x$ | $= (x^2+1)^{-\frac{1}{2}} dx$ | $\int x \sinh x dx$ | $= x \cosh x - \sinh x$ |
| $d \cosh^{-1} x$ | $= (x^2-1)^{-\frac{1}{2}} dx$ | $\int x \cosh x dx$ | $= x \sinh x - \cosh x$ |
| $d \tanh^{-1} x$ | $= (1-x^2)^{-1} dx$ | $\int \sinh^2 x dx$ | $= \frac{1}{2} (\sinh x \cosh x - x)$ |
| $d \coth^{-1} x$ | $= (1-x^2)^{-1} dx$ | $\int \cosh^2 x dx$ | $= \frac{1}{2} (\sinh x \cosh x + x)$ |
| $d \operatorname{sech}^{-1} x$ | $= -x^{-1} (1-x^2)^{-\frac{1}{2}} dx$ | $\int \sinh x \cosh x dx$ | $= \frac{1}{4} \cosh (2x)$ |
| $d \operatorname{csch}^{-1} x$ | $= -x^{-1} (x^2+1)^{-\frac{1}{2}} dx$ | | |

* See also accompanying table of derivatives. For example: $\int \cos_x x dx = \sin_x x + \text{constant}$.

$$(x+y)^n = x^n + \frac{n}{1} x^{n-1} y + \frac{n(n-1)}{2!} x^{n-2} y^2 + \dots$$

$$\frac{n(n-1) \dots (n-m+1)}{m!} x^{n-m} y^m + \dots \quad (y^2 < x^2)$$

$$(1 \pm x)^n = 1 \pm nx + \frac{n(n-1)x^2}{2!} \pm \frac{n(n-1)(n-2)x^3}{3!} + \dots + \frac{(\pm 1)^k n! x^k}{(n-k)! k!} + \dots \quad (x^2 < 1)$$

$$(1 \pm x)^{-n} = 1 \mp nx + \frac{n(n+1)}{2!} x^2 \mp \frac{n(n+1)(n+2)x^3}{3!} + \dots$$

$$(\mp 1)^k \frac{(n+k-1)x^k}{(n-1)! k!} + \dots \quad (x^2 < 1)$$

$$(1 \pm x)^{-1} = 1 \mp x + x^2 \mp x^3 + x^4 \mp x^5 + \dots \quad (x^2 < 1)$$

$$(1 \pm x)^{-2} = 1 \mp 2x + 3x^2 \mp 4x^3 + 5x^4 \mp 6x^5 + \dots \quad (x^2 < 1)$$

$$f(x+h) = f(x) + hf'(x) + \frac{h^2}{2!} f''(x) + \dots + \frac{h^n}{n!} f^{(n)}(x) + \dots$$

Taylor's series.

$$f(x) = f(0) + \frac{x}{1} f'(0) + \frac{x^2}{2!} f''(0) + \dots + \frac{x^n}{n!} f^{(n)}(0) + \dots$$

Maclaurin's series.

$$e = \lim \left(1 + \frac{1}{n} \right)^n = 1 + \frac{1}{1!} + \frac{1}{2!} + \frac{1}{3!} + \frac{1}{4!} + \dots$$

$$e^x = 1 + x + \frac{x^2}{2!} + \frac{x^3}{3!} + \frac{x^4}{4!} + \dots \quad (x^2 < x)$$

$$a^x = 1 + x \log a + \frac{(x \log a)^2}{2!} + \frac{(x \log a)^3}{3!} + \dots \quad (x^2 < x)$$

$$\log x = \frac{x-1}{x} + \frac{1}{2} \left(\frac{x-1}{x} \right)^2 + \frac{1}{3} \left(\frac{x-1}{x} \right)^3 + \dots \quad (x > \frac{1}{2})$$

$$= (x-1) - \frac{1}{2} (x-1)^2 + \frac{1}{3} (x-1)^3 - \dots \quad (2 > x > 0)$$

$$= 2 \left[\frac{x-1}{x+1} + \frac{1}{3} \left(\frac{x-1}{x+1} \right)^3 + \frac{1}{5} \left(\frac{x-1}{x+1} \right)^5 + \dots \right] \quad (x > 0)$$

$$\log(1+x) = x - \frac{1}{2} x^2 + \frac{1}{3} x^3 - \frac{1}{4} x^4 + \dots \quad (x^2 < 1)$$

$$\sin x = \frac{1}{2i} (e^{ix} - e^{-ix}) = x - \frac{x^3}{3!} + \frac{x^5}{5!} - \frac{x^7}{7!} + \dots \quad (x^2 < x)$$

$$\cos x = \frac{1}{2} (e^{ix} + e^{-ix}) = 1 - \frac{x^2}{2!} + \frac{x^4}{4!} - \frac{x^6}{6!} + \dots = 1 - \text{versin } x \quad (x^2 < x)$$

$$\tan x = x + \frac{x^3}{3} + \frac{2x^5}{15} + \frac{17x^7}{315} + \frac{62}{2835} x^9 + \dots \quad \left(x^2 < \frac{\pi^2}{4} \right)$$

$$\sin^{-1} x = \frac{\pi}{2} - \cos^{-1} x = x + \frac{x^3}{6} + \frac{1}{2} \cdot \frac{3}{4} \cdot \frac{x^5}{5} + \frac{1}{2} \cdot \frac{3}{4} \cdot \frac{5}{6} \cdot \frac{x^7}{7} + \dots \quad (x^2 < 1)$$

$$\tan^{-1} x = \frac{\pi}{2} - \cot^{-1} x = x - \frac{1}{3} x^3 + \frac{1}{5} x^5 - \frac{1}{7} x^7 + \dots \quad (x^2 < 1)$$

$$= \frac{\pi}{2} - \frac{1}{x} + \frac{1}{3x^3} - \frac{1}{5x^5} + \dots \quad (x^2 > 1)$$

$$\sinh x = \frac{1}{2} (e^x - e^{-x}) = x + \frac{x^3}{3!} + \frac{x^5}{5!} + \frac{x^7}{7!} + \dots \quad (x^2 < x)$$

TABLES 7 (continued) AND 8
TABLE 7 (continued)—SERIES

$$\cosh x = \frac{1}{2} (e^x + e^{-x}) = 1 + \frac{x^2}{2!} + \frac{x^4}{4!} + \frac{x^6}{6!} + \dots \quad (x^2 < \infty)$$

$$\tanh x = x - \frac{1}{3} x^3 + \frac{2}{15} x^5 - \frac{17}{315} x^7 + \dots \quad (x^2 < \frac{1}{4} \pi^2)$$

$$\sinh^{-1} x = x - \frac{1}{2} \frac{x^3}{3} + \frac{1}{2} \cdot \frac{3}{4} \cdot \frac{x^5}{5} - \frac{1}{2} \cdot \frac{3}{4} \cdot \frac{5}{6} \frac{x^7}{7} + \dots \quad (x^2 < 1)$$

$$= \log 2x + \frac{1}{2} \frac{1}{2x^2} - \frac{1}{2} \frac{3}{4} \frac{1}{4x^4} + \frac{1}{2} \frac{3}{4} \frac{5}{6} \frac{1}{6x^6} - \dots \quad (x^2 > 1)$$

$$\cosh^{-1} x = \log 2x - \frac{1}{2} \frac{1}{2x^2} - \frac{1}{2} \frac{3}{4} \frac{1}{4x^4} - \frac{1}{2} \frac{3}{4} \frac{5}{6} \frac{1}{6x^6} - \dots \quad (x^2 > 1)$$

$$\tanh^{-1} x = x + \frac{1}{3} x^3 + \frac{1}{5} x^5 + \frac{1}{7} x^7 + \dots \quad (x^2 < 1)$$

$$\operatorname{gd} x = \phi = x - \frac{1}{6} x^3 + \frac{1}{24} x^5 - \frac{61}{5040} x^7 + \dots \quad (x \text{ small})$$

$$= \frac{\pi}{2} - \operatorname{sech} x - \frac{1}{2} \frac{\operatorname{sech}^3 x}{3} - \frac{1}{2} \frac{3}{4} \frac{\operatorname{sech}^5 x}{5} - \dots \quad (x \text{ large})$$

$$x = \operatorname{gd}^{-1} \phi = \phi + \frac{1}{6} \phi^3 + \frac{1}{24} \phi^5 + \frac{61}{5040} \phi^7 + \dots \quad \left(\phi < \frac{\pi}{2} \right)$$

$$f(x) = \frac{1}{2} b_0 + b_1 \cos \frac{\pi x}{c} + b_2 \cos \frac{2\pi x}{c} + \dots$$

$$+ a_1 \sin \frac{\pi x}{c} + a_2 \cos \frac{2\pi x}{c} + \dots \quad (-c < x < c)$$

$$a_m = \frac{1}{c} \int_{-c}^{+c} f(x) \sin \frac{m\pi x}{c} dx$$

$$b_m = \frac{1}{c} \int_{-c}^{+c} f(x) \cos \frac{m\pi x}{c} dx$$

TABLE 8.—MATHEMATICAL CONSTANTS

| | Numbers. | Logarithms. |
|---|---|-------------------|
| $e = 2.71828 \ 18285$ | $\pi = 3.14159 \ 26536$ | $0.49714 \ 98727$ |
| $e^{-1} = 0.36787 \ 94412$ | $\pi^2 = 9.86960 \ 44011$ | $0.99429 \ 97454$ |
| $M = \log_{10} e = 0.43429 \ 44819$ | $\frac{1}{\pi} = 0.31830 \ 98862$ | $9.50285 \ 01273$ |
| $(M)^{-1} = \log_e 10 = 2.30258 \ 50930$ | $\sqrt{\pi} = 1.77245 \ 38509$ | $0.24857 \ 49363$ |
| $\log_{10} \log_{10} e = 9.63778 \ 43113$ | $\frac{\sqrt{\pi}}{2} = 0.88622 \ 69255$ | $9.94754 \ 49407$ |
| $\log_{10} 2 = 0.30102 \ 99957$ | $\frac{1}{\sqrt{\pi}} = 0.56418 \ 95835$ | $9.75142 \ 50637$ |
| $\log_e 2 = 0.69314 \ 71806$ | $\frac{2}{\sqrt{\pi}} = 1.12837 \ 91671$ | $0.05245 \ 50593$ |
| $\log_{10} x = M \cdot \log_e x$ | $\sqrt{\frac{\pi}{2}} = 1.25331 \ 41373$ | $0.09805 \ 99385$ |
| $\log_B x = \log_e x \cdot \log_e B$ | $\sqrt{\frac{2}{\pi}} = 0.79788 \ 45608$ | $9.90194 \ 00615$ |
| $= \log_e x \div \log_e B$ | $\frac{\pi}{4} = 0.78539 \ 81634$ | $9.89508 \ 98814$ |
| $\log_e \pi = 1.14472 \ 98858$ | $\frac{\sqrt{\pi}}{4} = 0.44311 \ 34627$ | $9.64651 \ 49450$ |
| $\rho = 0.47693 \ 62762$ | $\frac{4}{3} \pi = 4.18879 \ 02048$ | $0.62208 \ 86093$ |
| $\log \rho = 9.67846 \ 03565$ | $\frac{e}{\sqrt{2\pi}} = 1.08443 \ 75514$ | $0.03520 \ 45477$ |

VALUES OF RECIPROCAL, SQUARES, CUBES, AND SQUARE ROOTS
OF NATURAL NUMBERS

| n | $1000 \cdot \frac{1}{n}$ | n^2 | n^3 | \sqrt{n} | n | $1000 \cdot \frac{1}{n}$ | n^2 | n^3 | \sqrt{n} |
|-----|--------------------------|-------|--------|------------|-----|--------------------------|-------|---------|------------|
| 10 | 100.000 | 100 | 1000 | 3.1623 | 65 | 15.3846 | 4225 | 274625 | 8.0623 |
| 11 | 90.9091 | 121 | 1331 | 3.3166 | 66 | 15.1515 | 4356 | 287496 | 8.1240 |
| 12 | 83.3333 | 144 | 1728 | 3.4641 | 67 | 14.9254 | 4489 | 300763 | 8.1854 |
| 13 | 76.9231 | 169 | 2197 | 3.6056 | 68 | 14.7059 | 4624 | 314432 | 8.2462 |
| 14 | 71.4286 | 196 | 2744 | 3.7417 | 69 | 14.4928 | 4761 | 328509 | 8.3066 |
| 15 | 66.6667 | 225 | 3375 | 3.8730 | 70 | 14.2857 | 4900 | 343000 | 8.3666 |
| 16 | 62.5000 | 256 | 4096 | 4.0000 | 71 | 14.0845 | 5041 | 357911 | 8.4261 |
| 17 | 58.8235 | 289 | 4913 | 4.1231 | 72 | 13.8889 | 5184 | 373248 | 8.4853 |
| 18 | 55.5556 | 324 | 5832 | 4.2426 | 73 | 13.6986 | 5329 | 389017 | 8.5440 |
| 19 | 52.6316 | 361 | 6859 | 4.3589 | 74 | 13.5135 | 5476 | 405224 | 8.6023 |
| 20 | 50.0000 | 400 | 8000 | 4.4721 | 75 | 13.3333 | 5625 | 421875 | 8.6603 |
| 21 | 47.6190 | 441 | 9261 | 4.5826 | 76 | 13.1579 | 5776 | 438976 | 8.7178 |
| 22 | 45.4545 | 484 | 10648 | 4.6904 | 77 | 12.9870 | 5929 | 456533 | 8.7750 |
| 23 | 43.4783 | 529 | 12167 | 4.7958 | 78 | 12.8205 | 6084 | 474552 | 8.8318 |
| 24 | 41.6667 | 576 | 13824 | 4.8990 | 79 | 12.6582 | 6241 | 493039 | 8.8882 |
| 25 | 40.0000 | 625 | 15625 | 5.0000 | 80 | 12.5000 | 6400 | 512000 | 8.9443 |
| 26 | 38.4615 | 676 | 17576 | 5.0990 | 81 | 12.3457 | 6561 | 531441 | 9.0000 |
| 27 | 37.0370 | 729 | 19683 | 5.1962 | 82 | 12.1951 | 6724 | 551368 | 9.0554 |
| 28 | 35.7143 | 784 | 21952 | 5.2915 | 83 | 12.0482 | 6889 | 571787 | 9.1104 |
| 29 | 34.4828 | 841 | 24389 | 5.3852 | 84 | 11.9048 | 7056 | 592704 | 9.1652 |
| 30 | 33.3333 | 900 | 27000 | 5.4772 | 85 | 11.7647 | 7225 | 614125 | 9.2195 |
| 31 | 32.2581 | 961 | 29791 | 5.5678 | 86 | 11.6279 | 7396 | 636056 | 9.2736 |
| 32 | 31.2500 | 1024 | 32768 | 5.6569 | 87 | 11.4943 | 7569 | 658503 | 9.3274 |
| 33 | 30.3030 | 1089 | 35937 | 5.7446 | 88 | 11.3636 | 7744 | 681472 | 9.3808 |
| 34 | 29.4118 | 1156 | 39304 | 5.8310 | 89 | 11.2360 | 7921 | 704969 | 9.4340 |
| 35 | 28.5714 | 1225 | 42875 | 5.9161 | 90 | 11.1111 | 8100 | 729000 | 9.4868 |
| 36 | 27.7778 | 1296 | 46656 | 6.0000 | 91 | 10.9890 | 8281 | 753571 | 9.5394 |
| 37 | 27.0270 | 1369 | 50653 | 6.0828 | 92 | 10.8696 | 8464 | 778688 | 9.5917 |
| 38 | 26.3158 | 1444 | 54872 | 6.1644 | 93 | 10.7527 | 8649 | 804357 | 9.6437 |
| 39 | 25.6410 | 1521 | 59319 | 6.2450 | 94 | 10.6383 | 8836 | 830584 | 9.6954 |
| 40 | 25.0000 | 1600 | 64000 | 6.3246 | 95 | 10.5263 | 9025 | 857375 | 9.7468 |
| 41 | 24.3902 | 1681 | 68921 | 6.4031 | 96 | 10.4167 | 9216 | 884736 | 9.7980 |
| 42 | 23.8095 | 1764 | 74088 | 6.4807 | 97 | 10.3093 | 9409 | 912673 | 9.8489 |
| 43 | 23.2558 | 1849 | 79507 | 6.5574 | 98 | 10.2041 | 9604 | 941192 | 9.8995 |
| 44 | 22.7273 | 1936 | 85184 | 6.6332 | 99 | 10.1010 | 9801 | 970299 | 9.9499 |
| 45 | 22.2222 | 2025 | 91125 | 6.7082 | 100 | 10.0000 | 10000 | 1000000 | 10.0000 |
| 46 | 21.7391 | 2116 | 97336 | 6.7823 | 101 | 9.90099 | 10201 | 1030301 | 10.0499 |
| 47 | 21.2766 | 2209 | 103823 | 6.8557 | 102 | 9.80392 | 10404 | 1061208 | 10.0995 |
| 48 | 20.8333 | 2304 | 110592 | 6.9282 | 103 | 9.70874 | 10609 | 1092727 | 10.1489 |
| 49 | 20.4082 | 2401 | 117649 | 7.0000 | 104 | 9.61538 | 10816 | 1124864 | 10.1980 |
| 50 | 20.0000 | 2500 | 125000 | 7.0711 | 105 | 9.52381 | 11025 | 1157625 | 10.2470 |
| 51 | 19.6078 | 2601 | 132651 | 7.1414 | 106 | 9.43396 | 11236 | 1191016 | 10.2956 |
| 52 | 19.2308 | 2704 | 140608 | 7.2111 | 107 | 9.34579 | 11449 | 1225043 | 10.3441 |
| 53 | 18.8679 | 2809 | 148877 | 7.2801 | 108 | 9.25926 | 11664 | 1259712 | 10.3923 |
| 54 | 18.5185 | 2916 | 157464 | 7.3485 | 109 | 9.17431 | 11881 | 1295029 | 10.4403 |
| 55 | 18.1818 | 3025 | 166375 | 7.4162 | 110 | 9.09091 | 12100 | 1331000 | 10.4881 |
| 56 | 17.8571 | 3136 | 175616 | 7.4833 | 111 | 9.00901 | 12321 | 1367631 | 10.5357 |
| 57 | 17.5439 | 3249 | 185193 | 7.5498 | 112 | 8.92857 | 12544 | 1404028 | 10.5830 |
| 58 | 17.2414 | 3364 | 195112 | 7.6158 | 113 | 8.84956 | 12769 | 1442867 | 10.6301 |
| 59 | 16.9492 | 3481 | 205379 | 7.6811 | 114 | 8.77193 | 12996 | 1481544 | 10.6771 |
| 60 | 16.6667 | 3600 | 216000 | 7.7460 | 115 | 8.69565 | 13225 | 1520875 | 10.7238 |
| 61 | 16.3934 | 3721 | 226981 | 7.8102 | 116 | 8.62069 | 13456 | 1560806 | 10.7703 |
| 62 | 16.1290 | 3844 | 238328 | 7.8740 | 117 | 8.54701 | 13689 | 1601613 | 10.8167 |
| 63 | 15.8730 | 3969 | 250047 | 7.9373 | 118 | 8.47458 | 13924 | 1643332 | 10.8628 |
| 64 | 15.6250 | 4096 | 262144 | 8.0000 | 119 | 8.40336 | 14161 | 1685159 | 10.9087 |

VALUES OF RECIPROCAL, SQUARES, CUBES, AND SQUARE ROOTS OF NATURAL NUMBERS

| n | $1000 \cdot \frac{1}{n}$ | n^2 | n^3 | \sqrt{n} | n | $1000 \cdot \frac{1}{n}$ | n^2 | n^3 | \sqrt{n} |
|-----|--------------------------|-------|---------|------------|-----|--------------------------|-------|----------|------------|
| 120 | 8.33333 | 14400 | 1728000 | 10.9545 | 175 | 5.71429 | 30625 | 5359375 | 13.2288 |
| 121 | 8.26446 | 14641 | 1771561 | 11.0000 | 176 | 5.68182 | 30976 | 5451776 | 13.2665 |
| 122 | 8.19672 | 14884 | 1815848 | 11.0454 | 177 | 5.64972 | 31329 | 5545233 | 13.3041 |
| 123 | 8.13008 | 15129 | 1860867 | 11.0905 | 178 | 5.61798 | 31684 | 5639752 | 13.3417 |
| 124 | 8.06452 | 15376 | 1906624 | 11.1355 | 179 | 5.58659 | 32041 | 5735339 | 13.3791 |
| 125 | 8.00000 | 15625 | 1953125 | 11.1803 | 180 | 5.55556 | 32400 | 5832000 | 13.4164 |
| 126 | 7.93651 | 15876 | 2000376 | 11.2250 | 181 | 5.52486 | 32761 | 5929741 | 13.4536 |
| 127 | 7.87402 | 16129 | 2048383 | 11.2694 | 182 | 5.49451 | 33124 | 6028568 | 13.4907 |
| 128 | 7.81250 | 16384 | 2097152 | 11.3137 | 183 | 5.46448 | 33489 | 6128487 | 13.5277 |
| 129 | 7.75194 | 16641 | 2146689 | 11.3578 | 184 | 5.43478 | 33856 | 6229504 | 13.5647 |
| 130 | 7.69231 | 16900 | 2197000 | 11.4018 | 185 | 5.40511 | 34225 | 6331625 | 13.6015 |
| 131 | 7.63339 | 17161 | 2248091 | 11.4455 | 186 | 5.37634 | 34596 | 6434856 | 13.6382 |
| 132 | 7.57576 | 17424 | 2299968 | 11.4891 | 187 | 5.34759 | 34969 | 6539203 | 13.6748 |
| 133 | 7.51880 | 17689 | 2352637 | 11.5326 | 188 | 5.31915 | 35344 | 6644672 | 13.7113 |
| 134 | 7.46269 | 17956 | 2406104 | 11.5758 | 189 | 5.29101 | 35721 | 6751269 | 13.7477 |
| 135 | 7.40741 | 18225 | 2460375 | 11.6190 | 190 | 5.26316 | 36100 | 6859000 | 13.7840 |
| 136 | 7.35294 | 18496 | 2515456 | 11.6619 | 191 | 5.23560 | 36481 | 6967871 | 13.8203 |
| 137 | 7.29927 | 18769 | 2571353 | 11.7047 | 192 | 5.20833 | 36864 | 7077888 | 13.8564 |
| 138 | 7.24638 | 19044 | 2628072 | 11.7473 | 193 | 5.18135 | 37249 | 7189057 | 13.8924 |
| 139 | 7.19424 | 19321 | 2685619 | 11.7898 | 194 | 5.15464 | 37636 | 7301384 | 13.9284 |
| 140 | 7.14286 | 19600 | 2744000 | 11.8322 | 195 | 5.12821 | 38025 | 7414875 | 13.9642 |
| 141 | 7.09220 | 19881 | 2803221 | 11.8743 | 196 | 5.10204 | 38416 | 7529536 | 14.0000 |
| 142 | 7.04225 | 20164 | 2863288 | 11.9164 | 197 | 5.07614 | 38809 | 7645373 | 14.0357 |
| 143 | 6.99301 | 20449 | 2924207 | 11.9583 | 198 | 5.05051 | 39204 | 7762392 | 14.0712 |
| 144 | 6.94444 | 20736 | 2985984 | 12.0000 | 199 | 5.02513 | 39601 | 7880599 | 14.1067 |
| 145 | 6.89655 | 21025 | 3048625 | 12.0416 | 200 | 5.00000 | 40000 | 8000000 | 14.1421 |
| 146 | 6.84932 | 21316 | 3112136 | 12.0830 | 201 | 4.97512 | 40401 | 8120601 | 14.1774 |
| 147 | 6.80272 | 21609 | 3176523 | 12.1244 | 202 | 4.95050 | 40804 | 8242408 | 14.2127 |
| 148 | 6.75676 | 21904 | 3241792 | 12.1655 | 203 | 4.92611 | 41209 | 8365427 | 14.2478 |
| 149 | 6.71141 | 22201 | 3307949 | 12.2066 | 204 | 4.90196 | 41616 | 8489664 | 14.2829 |
| 150 | 6.66667 | 22500 | 3375000 | 12.2474 | 205 | 4.87805 | 42025 | 8615125 | 14.3178 |
| 151 | 6.62252 | 22801 | 3442951 | 12.2882 | 206 | 4.85437 | 42436 | 8741816 | 14.3527 |
| 152 | 6.57895 | 23104 | 3511808 | 12.3288 | 207 | 4.83092 | 42849 | 8869743 | 14.3875 |
| 153 | 6.53595 | 23409 | 3581577 | 12.3693 | 208 | 4.80769 | 43264 | 8998912 | 14.4222 |
| 154 | 6.49351 | 23716 | 3652204 | 12.4097 | 209 | 4.78469 | 43681 | 9129329 | 14.4568 |
| 155 | 6.45161 | 24025 | 3723875 | 12.4499 | 210 | 4.76190 | 44100 | 9261000 | 14.4914 |
| 156 | 6.41026 | 24336 | 3796416 | 12.4900 | 211 | 4.73934 | 44521 | 9393931 | 14.5258 |
| 157 | 6.36943 | 24649 | 3869893 | 12.5300 | 212 | 4.71698 | 44944 | 9528128 | 14.5602 |
| 158 | 6.32911 | 24964 | 3944312 | 12.5698 | 213 | 4.69484 | 45369 | 9663597 | 14.5945 |
| 159 | 6.28931 | 25281 | 4019679 | 12.6095 | 214 | 4.67290 | 45796 | 9800344 | 14.6287 |
| 160 | 6.25000 | 25600 | 4096000 | 12.6491 | 215 | 4.65116 | 46225 | 9938375 | 14.6629 |
| 161 | 6.21118 | 25921 | 4173281 | 12.6886 | 216 | 4.62963 | 46656 | 10077696 | 14.6969 |
| 162 | 6.17284 | 26244 | 4251528 | 12.7279 | 217 | 4.60829 | 47089 | 10218313 | 14.7309 |
| 163 | 6.13497 | 26569 | 4330747 | 12.7671 | 218 | 4.58716 | 47524 | 10360232 | 14.7648 |
| 164 | 6.09756 | 26896 | 4410944 | 12.8062 | 219 | 4.56621 | 47961 | 10503459 | 14.7986 |
| 165 | 6.06061 | 27225 | 4492125 | 12.8452 | 220 | 4.54545 | 48400 | 10648000 | 14.8324 |
| 166 | 6.02410 | 27556 | 4574296 | 12.8841 | 221 | 4.52489 | 48841 | 10793861 | 14.8661 |
| 167 | 5.98802 | 27889 | 4657463 | 12.9228 | 222 | 4.50450 | 49284 | 10941048 | 14.8997 |
| 168 | 5.95238 | 28224 | 4741632 | 12.9615 | 223 | 4.48430 | 49729 | 11089567 | 14.9332 |
| 169 | 5.91716 | 28561 | 4826809 | 13.0000 | 224 | 4.46429 | 50176 | 11239424 | 14.9666 |
| 170 | 5.88235 | 28900 | 4913000 | 13.0384 | 225 | 4.44444 | 50625 | 11390625 | 15.0000 |
| 171 | 5.84795 | 29241 | 5000211 | 13.0767 | 226 | 4.42478 | 51076 | 11543176 | 15.0333 |
| 172 | 5.81395 | 29584 | 5088448 | 13.1149 | 227 | 4.40529 | 51529 | 11697083 | 15.0665 |
| 173 | 5.78035 | 29929 | 5177717 | 13.1529 | 228 | 4.38596 | 51984 | 11852532 | 15.0997 |
| 174 | 5.74713 | 30276 | 5268024 | 13.1909 | 229 | 4.36681 | 52441 | 12008989 | 15.1327 |

VALUES OF RECIPROCAL, SQUARES, CUBES, AND SQUARE ROOTS OF
NATURAL NUMBERS

| n | $1000 \cdot \frac{1}{n}$ | n^2 | n^3 | \sqrt{n} | n | $1000 \cdot \frac{1}{n}$ | n^2 | n^3 | \sqrt{n} |
|-----|--------------------------|-------|----------|------------|-----|--------------------------|--------|----------|------------|
| 230 | 4.34783 | 52900 | 12167000 | 15.1658 | 285 | 3.50877 | 81225 | 23149125 | 16.8819 |
| 231 | 4.32900 | 53361 | 12326391 | 15.1987 | 286 | 3.49650 | 81796 | 23393656 | 16.9115 |
| 232 | 4.31034 | 53824 | 12487168 | 15.2315 | 287 | 3.48432 | 82369 | 23639903 | 16.9411 |
| 233 | 4.29185 | 54289 | 12649337 | 15.2643 | 288 | 3.47222 | 82944 | 23887872 | 16.9706 |
| 234 | 4.27350 | 54756 | 12812904 | 15.2971 | 289 | 3.46021 | 83521 | 24137569 | 17.0000 |
| 235 | 4.25532 | 55225 | 12977875 | 15.3297 | 290 | 3.44828 | 84100 | 24389000 | 17.0294 |
| 236 | 4.23729 | 55696 | 13144256 | 15.3623 | 291 | 3.43643 | 84681 | 24642171 | 17.0587 |
| 237 | 4.21941 | 56169 | 13312053 | 15.3948 | 292 | 3.42466 | 85264 | 24897088 | 17.0880 |
| 238 | 4.20168 | 56644 | 13481272 | 15.4272 | 293 | 3.41297 | 85849 | 25153757 | 17.1172 |
| 239 | 4.18410 | 57121 | 13651919 | 15.4596 | 294 | 3.40136 | 86436 | 25412184 | 17.1464 |
| 240 | 4.16667 | 57600 | 13824000 | 15.4919 | 295 | 3.38983 | 87025 | 25672375 | 17.1756 |
| 241 | 4.14938 | 58081 | 13997521 | 15.5242 | 296 | 3.37838 | 87616 | 25934336 | 17.2047 |
| 242 | 4.13223 | 58564 | 14172488 | 15.5563 | 297 | 3.36700 | 88209 | 26198073 | 17.2337 |
| 243 | 4.11523 | 59049 | 14348907 | 15.5885 | 298 | 3.35570 | 88804 | 26463592 | 17.2627 |
| 244 | 4.09836 | 59536 | 14526784 | 15.6205 | 299 | 3.34448 | 89401 | 26730899 | 17.2916 |
| 245 | 4.08163 | 60025 | 14706125 | 15.6525 | 300 | 3.33333 | 90000 | 27000000 | 17.3205 |
| 246 | 4.06504 | 60516 | 14886936 | 15.6844 | 301 | 3.32226 | 90601 | 27270901 | 17.3494 |
| 247 | 4.04858 | 61009 | 15069223 | 15.7162 | 302 | 3.31126 | 91204 | 27543608 | 17.3781 |
| 248 | 4.03226 | 61504 | 15252992 | 15.7480 | 303 | 3.30033 | 91809 | 27818127 | 17.4069 |
| 249 | 4.01606 | 62001 | 15438249 | 15.7797 | 304 | 3.28947 | 92416 | 28094464 | 17.4356 |
| 250 | 4.00000 | 62500 | 15625000 | 15.8114 | 305 | 3.27869 | 93025 | 28372625 | 17.4642 |
| 251 | 3.98406 | 63001 | 15813251 | 15.8430 | 306 | 3.26797 | 93636 | 28652616 | 17.4929 |
| 252 | 3.96825 | 63504 | 16003008 | 15.8745 | 307 | 3.25733 | 94249 | 28934443 | 17.5214 |
| 253 | 3.95257 | 64009 | 16194277 | 15.9060 | 308 | 3.24675 | 94864 | 29218112 | 17.5499 |
| 254 | 3.93701 | 64516 | 16387064 | 15.9374 | 309 | 3.23625 | 95481 | 29503629 | 17.5784 |
| 255 | 3.92157 | 65025 | 16581375 | 15.9687 | 310 | 3.22581 | 96100 | 29791000 | 17.6068 |
| 256 | 3.90625 | 65536 | 16777216 | 16.0000 | 311 | 3.21543 | 96721 | 30080231 | 17.6352 |
| 257 | 3.89105 | 66049 | 16974593 | 16.0312 | 312 | 3.20513 | 97344 | 30371328 | 17.6635 |
| 258 | 3.87597 | 66564 | 17173512 | 16.0624 | 313 | 3.19489 | 97969 | 30664297 | 17.6918 |
| 259 | 3.86100 | 67081 | 17373979 | 16.0935 | 314 | 3.18471 | 98596 | 30959144 | 17.7200 |
| 260 | 3.84615 | 67600 | 17576000 | 16.1245 | 315 | 3.17460 | 99225 | 31255875 | 17.7482 |
| 261 | 3.83142 | 68121 | 17779581 | 16.1555 | 316 | 3.16456 | 99856 | 31554496 | 17.7764 |
| 262 | 3.81679 | 68644 | 17984728 | 16.1864 | 317 | 3.15457 | 100489 | 31855013 | 17.8045 |
| 263 | 3.80228 | 69169 | 18191447 | 16.2173 | 318 | 3.14465 | 101124 | 32157432 | 17.8326 |
| 264 | 3.78788 | 69696 | 18399744 | 16.2481 | 319 | 3.13480 | 101761 | 32461759 | 17.8606 |
| 265 | 3.77358 | 70225 | 18609625 | 16.2788 | 320 | 3.12500 | 102400 | 32768000 | 17.8885 |
| 266 | 3.75940 | 70756 | 18821096 | 16.3095 | 321 | 3.11526 | 103041 | 33076161 | 17.9165 |
| 267 | 3.74532 | 71289 | 19034163 | 16.3401 | 322 | 3.10559 | 103684 | 33386248 | 17.9444 |
| 268 | 3.73134 | 71824 | 19248832 | 16.3707 | 323 | 3.09598 | 104329 | 33698267 | 17.9722 |
| 269 | 3.71747 | 72361 | 19465109 | 16.4012 | 324 | 3.08642 | 104976 | 34012224 | 18.0000 |
| 270 | 3.70370 | 72900 | 19683000 | 16.4317 | 325 | 3.07692 | 105625 | 34328125 | 18.0278 |
| 271 | 3.69004 | 73441 | 19902511 | 16.4621 | 326 | 3.06748 | 106276 | 34645976 | 18.0555 |
| 272 | 3.67647 | 73984 | 20123648 | 16.4924 | 327 | 3.05810 | 106929 | 34965783 | 18.0831 |
| 273 | 3.66300 | 74529 | 20346417 | 16.5227 | 328 | 3.04878 | 107584 | 35287552 | 18.1108 |
| 274 | 3.64964 | 75076 | 20570824 | 16.5529 | 329 | 3.03951 | 108241 | 35611289 | 18.1384 |
| 275 | 3.63636 | 75625 | 20796875 | 16.5831 | 330 | 3.03030 | 108900 | 35937000 | 18.1659 |
| 276 | 3.62319 | 76176 | 21024576 | 16.6132 | 331 | 3.02115 | 109561 | 36264601 | 18.1934 |
| 277 | 3.61011 | 76729 | 21253933 | 16.6433 | 332 | 3.01205 | 110224 | 36594368 | 18.2209 |
| 278 | 3.59712 | 77284 | 21484952 | 16.6733 | 333 | 3.00300 | 110889 | 36926037 | 18.2483 |
| 279 | 3.58423 | 77841 | 21717639 | 16.7033 | 334 | 2.99401 | 111556 | 37259704 | 18.2757 |
| 280 | 3.57143 | 78400 | 21952000 | 16.7332 | 335 | 2.98507 | 112225 | 37595375 | 18.3030 |
| 281 | 3.55872 | 78961 | 22188041 | 16.7631 | 336 | 2.97619 | 112896 | 37933056 | 18.3303 |
| 282 | 3.54610 | 79524 | 22425768 | 16.7929 | 337 | 2.96736 | 113569 | 38272753 | 18.3576 |
| 283 | 3.53357 | 80089 | 22665187 | 16.8226 | 338 | 2.95858 | 114244 | 38614472 | 18.3848 |
| 284 | 3.52113 | 80656 | 22906304 | 16.8523 | 339 | 2.94985 | 114921 | 38958219 | 18.4120 |

VALUES OF RECIPROALS, SQUARES, CUBES, AND SQUARE ROOTS
OF NATURAL NUMBERS

| n | $1000 \cdot \frac{1}{n}$ | n^2 | n^3 | \sqrt{n} | n | $1000 \cdot \frac{1}{n}$ | n^2 | n^3 | \sqrt{n} |
|-----|--------------------------|--------|----------|------------|-----|--------------------------|--------|----------|------------|
| 340 | 2.94118 | 115600 | 39304000 | 18.4391 | 395 | 2.53165 | 156025 | 61629875 | 19.8746 |
| 341 | 2.93255 | 116281 | 39651821 | 18.4662 | 396 | 2.52525 | 156816 | 62099136 | 19.8997 |
| 342 | 2.92398 | 116964 | 40001688 | 18.4932 | 397 | 2.51889 | 157609 | 62570773 | 19.9249 |
| 343 | 2.91545 | 117649 | 40353607 | 18.5203 | 398 | 2.51256 | 158404 | 63044792 | 19.9499 |
| 344 | 2.90698 | 118336 | 40707384 | 18.5472 | 399 | 2.50627 | 159201 | 63521199 | 19.9750 |
| 345 | 2.89855 | 119025 | 41063625 | 18.5742 | 400 | 2.50000 | 160000 | 64000000 | 20.0000 |
| 346 | 2.89017 | 119716 | 41421736 | 18.6011 | 401 | 2.49377 | 160801 | 64481201 | 20.0250 |
| 347 | 2.88184 | 120409 | 41781923 | 18.6279 | 402 | 2.48756 | 161604 | 64964808 | 20.0499 |
| 348 | 2.87356 | 121104 | 42144192 | 18.6548 | 403 | 2.48139 | 162409 | 65450827 | 20.0749 |
| 349 | 2.86533 | 121801 | 42508549 | 18.6815 | 404 | 2.47525 | 163216 | 65939264 | 20.0998 |
| 350 | 2.85714 | 122500 | 42875000 | 18.7083 | 405 | 2.46914 | 164025 | 66430125 | 20.1246 |
| 351 | 2.84900 | 123201 | 43243551 | 18.7350 | 406 | 2.46305 | 164836 | 66923416 | 20.1494 |
| 352 | 2.84091 | 123904 | 43614208 | 18.7617 | 407 | 2.45690 | 165649 | 67419143 | 20.1742 |
| 353 | 2.83286 | 124609 | 43986977 | 18.7883 | 408 | 2.45098 | 166464 | 67917312 | 20.1990 |
| 354 | 2.82486 | 125316 | 44361864 | 18.8149 | 409 | 2.44499 | 167281 | 68417929 | 20.2237 |
| 355 | 2.81690 | 126025 | 44738875 | 18.8414 | 410 | 2.43902 | 168100 | 68921000 | 20.2485 |
| 356 | 2.80899 | 126736 | 45118016 | 18.8680 | 411 | 2.43309 | 168921 | 69426531 | 20.2731 |
| 357 | 2.80112 | 127449 | 45499293 | 18.8944 | 412 | 2.42718 | 169744 | 69934528 | 20.2978 |
| 358 | 2.79330 | 128164 | 45882712 | 18.9209 | 413 | 2.42131 | 170569 | 70444997 | 20.3224 |
| 359 | 2.78552 | 128881 | 46268279 | 18.9473 | 414 | 2.41546 | 171396 | 70957944 | 20.3470 |
| 360 | 2.77778 | 129600 | 46656000 | 18.9737 | 415 | 2.40964 | 172225 | 71473375 | 20.3715 |
| 361 | 2.77008 | 130321 | 47045881 | 19.0000 | 416 | 2.40385 | 173056 | 71991296 | 20.3961 |
| 362 | 2.76243 | 131044 | 47437928 | 19.0263 | 417 | 2.39808 | 173889 | 72511713 | 20.4206 |
| 363 | 2.75482 | 131769 | 47832147 | 19.0526 | 418 | 2.39234 | 174724 | 73034632 | 20.4450 |
| 364 | 2.74725 | 132496 | 48228544 | 19.0788 | 419 | 2.38663 | 175561 | 73560059 | 20.4695 |
| 365 | 2.73973 | 133225 | 48627125 | 19.1050 | 420 | 2.38095 | 176400 | 74088000 | 20.4939 |
| 366 | 2.73224 | 133956 | 49027896 | 19.1311 | 421 | 2.37530 | 177241 | 74618461 | 20.5183 |
| 367 | 2.72480 | 134689 | 49430863 | 19.1572 | 422 | 2.36967 | 178084 | 75151448 | 20.5426 |
| 368 | 2.71739 | 135424 | 49836032 | 19.1833 | 423 | 2.36407 | 178929 | 75686967 | 20.5670 |
| 369 | 2.71003 | 136161 | 50243409 | 19.2094 | 424 | 2.35849 | 179776 | 76225024 | 20.5913 |
| 370 | 2.70270 | 136900 | 50653000 | 19.2354 | 425 | 2.35294 | 180625 | 76765625 | 20.6155 |
| 371 | 2.69542 | 137641 | 51064811 | 19.2614 | 426 | 2.34742 | 181476 | 77308776 | 20.6398 |
| 372 | 2.68817 | 138384 | 51478848 | 19.2873 | 427 | 2.34192 | 182329 | 77854483 | 20.6640 |
| 373 | 2.68097 | 139129 | 51895117 | 19.3132 | 428 | 2.33645 | 183184 | 78402752 | 20.6882 |
| 374 | 2.67380 | 139876 | 52313624 | 19.3391 | 429 | 2.33100 | 184041 | 78953589 | 20.7123 |
| 375 | 2.66667 | 140625 | 52734375 | 19.3649 | 430 | 2.32558 | 184900 | 79507000 | 20.7364 |
| 376 | 2.65957 | 141376 | 53157376 | 19.3907 | 431 | 2.32019 | 185761 | 80062991 | 20.7605 |
| 377 | 2.65252 | 142129 | 53582633 | 19.4165 | 432 | 2.31481 | 186624 | 80621568 | 20.7846 |
| 378 | 2.64550 | 142884 | 54010152 | 19.4422 | 433 | 2.30947 | 187489 | 81182737 | 20.8087 |
| 379 | 2.63852 | 143641 | 54439939 | 19.4679 | 434 | 2.30415 | 188356 | 81746504 | 20.8327 |
| 380 | 2.63158 | 144400 | 54872000 | 19.4936 | 435 | 2.29885 | 189225 | 82312875 | 20.8567 |
| 381 | 2.62467 | 145161 | 55306341 | 19.5192 | 436 | 2.29358 | 190096 | 82881856 | 20.8806 |
| 382 | 2.61780 | 145924 | 55742968 | 19.5448 | 437 | 2.28833 | 190969 | 83453453 | 20.9045 |
| 383 | 2.61097 | 146689 | 56181887 | 19.5704 | 438 | 2.28311 | 191844 | 84027672 | 20.9284 |
| 384 | 2.60417 | 147456 | 56623104 | 19.5959 | 439 | 2.27790 | 192721 | 84604519 | 20.9523 |
| 385 | 2.59740 | 148225 | 57066625 | 19.6214 | 440 | 2.27273 | 193600 | 85184000 | 20.9762 |
| 386 | 2.59067 | 148996 | 57512456 | 19.6469 | 441 | 2.26757 | 194481 | 85766121 | 21.0000 |
| 387 | 2.58398 | 149769 | 57960603 | 19.6723 | 442 | 2.26244 | 195364 | 86350888 | 21.0238 |
| 388 | 2.57732 | 150544 | 58411072 | 19.6977 | 443 | 2.25734 | 196249 | 86938307 | 21.0476 |
| 389 | 2.57069 | 151321 | 58863869 | 19.7231 | 444 | 2.25225 | 197136 | 87528384 | 21.0713 |
| 390 | 2.56410 | 152100 | 59319000 | 19.7484 | 445 | 2.24719 | 198025 | 88121125 | 21.0950 |
| 391 | 2.55754 | 152881 | 59776471 | 19.7737 | 446 | 2.24215 | 198916 | 88716536 | 21.1187 |
| 392 | 2.55102 | 153664 | 60236288 | 19.7990 | 447 | 2.23714 | 199809 | 89314623 | 21.1424 |
| 393 | 2.54453 | 154449 | 60698457 | 19.8242 | 448 | 2.23214 | 200704 | 89915392 | 21.1660 |
| 394 | 2.53807 | 155236 | 61162984 | 19.8494 | 449 | 2.22717 | 201601 | 90518849 | 21.1896 |

VALUES OF RECIPROCAL, SQUARES, CUBES, AND SQUARE ROOTS
OF NATURAL NUMBERS

| n | $1000 \cdot \frac{1}{n}$ | n^2 | n^3 | \sqrt{n} | n | $1000 \cdot \frac{1}{n}$ | n^2 | n^3 | \sqrt{n} |
|-----|--------------------------|--------|-----------|------------|-----|--------------------------|--------|-----------|------------|
| 450 | 2.22222 | 202500 | 91125000 | 21.2132 | 505 | 1.98020 | 255025 | 128787625 | 22.4722 |
| 451 | 2.21729 | 203401 | 91733851 | 21.2368 | 506 | 1.97628 | 256036 | 129554216 | 22.4944 |
| 452 | 2.21239 | 204304 | 92345408 | 21.2603 | 507 | 1.97239 | 257049 | 130323843 | 22.5167 |
| 453 | 2.20751 | 205209 | 92959677 | 21.2838 | 508 | 1.96850 | 258064 | 131096512 | 22.5389 |
| 454 | 2.20264 | 206116 | 93577064 | 21.3073 | 509 | 1.96464 | 259081 | 131872229 | 22.5610 |
| 455 | 2.19780 | 207025 | 94196375 | 21.3307 | 510 | 1.96078 | 260100 | 132651000 | 22.5832 |
| 456 | 2.19298 | 207936 | 94818816 | 21.3542 | 511 | 1.95695 | 261121 | 133432831 | 22.6053 |
| 457 | 2.18818 | 208849 | 95443993 | 21.3776 | 512 | 1.95312 | 262144 | 134217728 | 22.6274 |
| 458 | 2.18341 | 209764 | 96071912 | 21.4009 | 513 | 1.94932 | 263169 | 135005697 | 22.6495 |
| 459 | 2.17865 | 210681 | 96702579 | 21.4243 | 514 | 1.94553 | 264196 | 135796744 | 22.6716 |
| 460 | 2.17391 | 211600 | 97336000 | 21.4476 | 515 | 1.94175 | 265225 | 136590875 | 22.6936 |
| 461 | 2.16920 | 212521 | 97972181 | 21.4709 | 516 | 1.93798 | 266256 | 137388096 | 22.7156 |
| 462 | 2.16450 | 213444 | 98611128 | 21.4942 | 517 | 1.93424 | 267289 | 138188413 | 22.7376 |
| 463 | 2.15983 | 214369 | 99252847 | 21.5174 | 518 | 1.93050 | 268324 | 138991832 | 22.7596 |
| 464 | 2.15517 | 215296 | 99897344 | 21.5407 | 519 | 1.92678 | 269361 | 139798359 | 22.7816 |
| 465 | 2.15054 | 216225 | 100544625 | 21.5639 | 520 | 1.92308 | 270400 | 140608000 | 22.8035 |
| 466 | 2.14592 | 217156 | 101194696 | 21.5870 | 521 | 1.91939 | 271441 | 141420701 | 22.8254 |
| 467 | 2.14133 | 218089 | 101847563 | 21.6102 | 522 | 1.91571 | 272484 | 142236648 | 22.8473 |
| 468 | 2.13675 | 219024 | 102503232 | 21.6333 | 523 | 1.91205 | 273529 | 143055667 | 22.8692 |
| 469 | 2.13220 | 219961 | 103161709 | 21.6564 | 524 | 1.90840 | 274576 | 143877824 | 22.8910 |
| 470 | 2.12766 | 220900 | 103823000 | 21.6795 | 525 | 1.90476 | 275625 | 144703125 | 22.9129 |
| 471 | 2.12314 | 221841 | 104487111 | 21.7025 | 526 | 1.90114 | 276676 | 145531576 | 22.9347 |
| 472 | 2.11864 | 222784 | 105154048 | 21.7256 | 527 | 1.89753 | 277729 | 146363183 | 22.9565 |
| 473 | 2.11416 | 223729 | 105823817 | 21.7486 | 528 | 1.89394 | 278784 | 147197952 | 22.9783 |
| 474 | 2.10970 | 224676 | 106496424 | 21.7715 | 529 | 1.89036 | 279841 | 148035889 | 23.0000 |
| 475 | 2.10526 | 225625 | 107171875 | 21.7945 | 530 | 1.88679 | 280900 | 148877000 | 23.0217 |
| 476 | 2.10084 | 226576 | 107850176 | 21.8174 | 531 | 1.88324 | 281961 | 149721291 | 23.0434 |
| 477 | 2.09644 | 227529 | 108531333 | 21.8403 | 532 | 1.87970 | 283024 | 150568768 | 23.0651 |
| 478 | 2.09205 | 228484 | 109215352 | 21.8632 | 533 | 1.87617 | 284089 | 151419437 | 23.0868 |
| 479 | 2.08768 | 229441 | 109902239 | 21.8861 | 534 | 1.87266 | 285156 | 152273304 | 23.1084 |
| 480 | 2.08333 | 230400 | 110592000 | 21.9089 | 535 | 1.86916 | 286225 | 153130375 | 23.1301 |
| 481 | 2.07900 | 231361 | 111284641 | 21.9317 | 536 | 1.86567 | 287296 | 153990656 | 23.1517 |
| 482 | 2.07469 | 232324 | 111980168 | 21.9545 | 537 | 1.86220 | 288369 | 154854153 | 23.1733 |
| 483 | 2.07039 | 233289 | 112678567 | 21.9773 | 538 | 1.85874 | 289444 | 155720872 | 23.1948 |
| 484 | 2.06612 | 234256 | 113379904 | 22.0000 | 539 | 1.85529 | 290521 | 156590819 | 23.2164 |
| 485 | 2.06186 | 235225 | 114084125 | 22.0227 | 540 | 1.85185 | 291600 | 157464000 | 23.2379 |
| 486 | 2.05761 | 236196 | 114791256 | 22.0454 | 541 | 1.84843 | 292681 | 158340421 | 23.2594 |
| 487 | 2.05339 | 237169 | 115501303 | 22.0681 | 542 | 1.84502 | 293764 | 159220088 | 23.2809 |
| 488 | 2.04918 | 238144 | 116214272 | 22.0907 | 543 | 1.84162 | 294849 | 160103007 | 23.3024 |
| 489 | 2.04499 | 239121 | 116930169 | 22.1133 | 544 | 1.83824 | 295936 | 160989184 | 23.3238 |
| 490 | 2.04082 | 240100 | 117649000 | 22.1359 | 545 | 1.83486 | 297025 | 161878625 | 23.3452 |
| 491 | 2.03666 | 241081 | 118370771 | 22.1585 | 546 | 1.83150 | 298116 | 162771336 | 23.3666 |
| 492 | 2.03252 | 242064 | 119095488 | 22.1811 | 547 | 1.82815 | 299209 | 163667323 | 23.3880 |
| 493 | 2.02840 | 243049 | 119823157 | 22.2036 | 548 | 1.82482 | 300304 | 164566592 | 23.4094 |
| 494 | 2.02429 | 244036 | 120553784 | 22.2261 | 549 | 1.82149 | 301401 | 165469149 | 23.4307 |
| 495 | 2.02020 | 245025 | 121287375 | 22.2486 | 550 | 1.81818 | 302500 | 166375000 | 23.4521 |
| 496 | 2.01613 | 246016 | 122023936 | 22.2711 | 551 | 1.81488 | 303601 | 167284151 | 23.4734 |
| 497 | 2.01207 | 247009 | 122763473 | 22.2935 | 552 | 1.81159 | 304704 | 168196668 | 23.4947 |
| 498 | 2.00803 | 248004 | 123506000 | 22.3159 | 553 | 1.80832 | 305809 | 169112377 | 23.5160 |
| 499 | 2.00401 | 249001 | 124251499 | 22.3383 | 554 | 1.80505 | 306916 | 170031464 | 23.5372 |
| 500 | 2.00000 | 250000 | 125000000 | 22.3607 | 555 | 1.80180 | 308025 | 170953875 | 23.5584 |
| 501 | 1.99601 | 251001 | 125751501 | 22.3830 | 556 | 1.79856 | 309136 | 171879616 | 23.5797 |
| 502 | 1.99203 | 252004 | 126506008 | 22.4054 | 557 | 1.79533 | 310249 | 172808693 | 23.6008 |
| 503 | 1.98807 | 253009 | 127263527 | 22.4277 | 558 | 1.79211 | 311364 | 173741112 | 23.6220 |
| 504 | 1.98413 | 254016 | 128024064 | 22.4499 | 559 | 1.78891 | 312481 | 174676879 | 23.6432 |

VALUES OF RECIPROCAL, SQUARES, CUBES, AND SQUARE ROOTS OF NATURAL NUMBERS

| n | $1000 \cdot \frac{1}{n}$ | n^2 | n^3 | \sqrt{n} | n | $1000 \cdot \frac{1}{n}$ | n^2 | n^3 | \sqrt{n} |
|-----|--------------------------|--------|-----------|------------|-----|--------------------------|--------|-----------|------------|
| 560 | 1.78571 | 313600 | 175616000 | 23.6643 | 615 | 1.62602 | 378225 | 232608375 | 24.7992 |
| 561 | 1.78253 | 314721 | 176558481 | 23.6854 | 616 | 1.62338 | 379456 | 233744896 | 24.8193 |
| 562 | 1.77930 | 315844 | 177504328 | 23.7065 | 617 | 1.62075 | 380689 | 234885113 | 24.8395 |
| 563 | 1.77620 | 316969 | 178453547 | 23.7276 | 618 | 1.61812 | 381924 | 236029032 | 24.8596 |
| 564 | 1.77305 | 318096 | 179406144 | 23.7487 | 619 | 1.61551 | 383161 | 237176659 | 24.8797 |
| 565 | 1.76991 | 319225 | 180362125 | 23.7697 | 620 | 1.61290 | 384400 | 238328000 | 24.8998 |
| 566 | 1.76678 | 320356 | 181321496 | 23.7908 | 621 | 1.61031 | 385641 | 239483061 | 24.9199 |
| 567 | 1.76367 | 321489 | 182284263 | 23.8118 | 622 | 1.60772 | 386884 | 240641848 | 24.9399 |
| 568 | 1.76056 | 322624 | 183250432 | 23.8328 | 623 | 1.60514 | 388129 | 241804367 | 24.9600 |
| 569 | 1.75747 | 323761 | 184220009 | 23.8537 | 624 | 1.60256 | 389376 | 242970624 | 24.9800 |
| 570 | 1.75439 | 324900 | 185193000 | 23.8747 | 625 | 1.60000 | 390625 | 244140625 | 25.0000 |
| 571 | 1.75131 | 326041 | 186169411 | 23.8956 | 626 | 1.59744 | 391876 | 245314376 | 25.0200 |
| 572 | 1.74825 | 327184 | 187149248 | 23.9165 | 627 | 1.59490 | 393129 | 246491883 | 25.0400 |
| 573 | 1.74520 | 328329 | 188132517 | 23.9374 | 628 | 1.59236 | 394384 | 247673152 | 25.0599 |
| 574 | 1.74216 | 329476 | 189119224 | 23.9583 | 629 | 1.58983 | 395641 | 248858189 | 25.0799 |
| 575 | 1.73913 | 330625 | 190109375 | 23.9792 | 630 | 1.58730 | 396900 | 250047000 | 25.0998 |
| 576 | 1.73611 | 331776 | 191102976 | 24.0000 | 631 | 1.58479 | 398161 | 251239591 | 25.1197 |
| 577 | 1.73310 | 332929 | 192100033 | 24.0208 | 632 | 1.58228 | 399424 | 252435968 | 25.1396 |
| 578 | 1.73010 | 334084 | 193100552 | 24.0416 | 633 | 1.57978 | 400689 | 253636137 | 25.1595 |
| 579 | 1.72712 | 335241 | 194104539 | 24.0624 | 634 | 1.57729 | 401956 | 254840104 | 25.1794 |
| 580 | 1.72414 | 336400 | 195112000 | 24.0832 | 635 | 1.57480 | 403225 | 256047875 | 25.1992 |
| 581 | 1.72117 | 337561 | 196122941 | 24.1039 | 636 | 1.57233 | 404496 | 257259456 | 25.2190 |
| 582 | 1.71821 | 338724 | 197137368 | 24.1247 | 637 | 1.56986 | 405769 | 258474853 | 25.2389 |
| 583 | 1.71527 | 339889 | 198155287 | 24.1454 | 638 | 1.56740 | 407044 | 259694072 | 25.2587 |
| 584 | 1.71233 | 341056 | 199176704 | 24.1661 | 639 | 1.56495 | 408321 | 260917119 | 25.2784 |
| 585 | 1.70940 | 342225 | 200201625 | 24.1868 | 640 | 1.56250 | 409600 | 262144000 | 25.2982 |
| 586 | 1.70648 | 343396 | 201230056 | 24.2074 | 641 | 1.56006 | 410881 | 263374721 | 25.3180 |
| 587 | 1.70358 | 344569 | 202262003 | 24.2281 | 642 | 1.55763 | 412164 | 264609288 | 25.3378 |
| 588 | 1.70068 | 345744 | 203297472 | 24.2487 | 643 | 1.55521 | 413449 | 265847707 | 25.3574 |
| 589 | 1.69779 | 346921 | 204336469 | 24.2693 | 644 | 1.55280 | 414736 | 267089984 | 25.3772 |
| 590 | 1.69492 | 348100 | 205379000 | 24.2899 | 645 | 1.55039 | 416025 | 268336125 | 25.3969 |
| 591 | 1.69205 | 349281 | 206425071 | 24.3105 | 646 | 1.54799 | 417316 | 269586136 | 25.4165 |
| 592 | 1.68919 | 350464 | 207474688 | 24.3311 | 647 | 1.54560 | 418609 | 270840023 | 25.4362 |
| 593 | 1.68634 | 351649 | 208527857 | 24.3516 | 648 | 1.54321 | 419904 | 272097792 | 25.4558 |
| 594 | 1.68350 | 352836 | 209584584 | 24.3721 | 649 | 1.54083 | 421201 | 273359449 | 25.4755 |
| 595 | 1.68067 | 354025 | 210644875 | 24.3926 | 650 | 1.53846 | 422500 | 274625000 | 25.4951 |
| 596 | 1.67785 | 355216 | 211708736 | 24.4131 | 651 | 1.53610 | 423801 | 275894451 | 25.5147 |
| 597 | 1.67504 | 356409 | 212776173 | 24.4336 | 652 | 1.53374 | 425104 | 277167808 | 25.5343 |
| 598 | 1.67224 | 357604 | 213847192 | 24.4540 | 653 | 1.53139 | 426409 | 278445077 | 25.5539 |
| 599 | 1.66945 | 358801 | 214921799 | 24.4745 | 654 | 1.52905 | 427716 | 279726264 | 25.5734 |
| 600 | 1.66667 | 360000 | 216000000 | 24.4949 | 655 | 1.52672 | 429025 | 281011375 | 25.5930 |
| 601 | 1.66389 | 361201 | 217081801 | 24.5153 | 656 | 1.52439 | 430336 | 282300416 | 25.6125 |
| 602 | 1.66113 | 362404 | 218167208 | 24.5357 | 657 | 1.52207 | 431649 | 283593393 | 25.6320 |
| 603 | 1.65837 | 363609 | 219256227 | 24.5561 | 658 | 1.51976 | 432964 | 284890312 | 25.6515 |
| 604 | 1.65563 | 364816 | 220348864 | 24.5764 | 659 | 1.51745 | 434281 | 286191179 | 25.6710 |
| 605 | 1.65289 | 366025 | 221445125 | 24.5967 | 660 | 1.51515 | 435600 | 287496000 | 25.6905 |
| 606 | 1.65017 | 367236 | 222545016 | 24.6171 | 661 | 1.51286 | 436921 | 288804781 | 25.7099 |
| 607 | 1.64745 | 368449 | 223648543 | 24.6374 | 662 | 1.51057 | 438244 | 290117528 | 25.7294 |
| 608 | 1.64474 | 369664 | 224755712 | 24.6577 | 663 | 1.50830 | 439569 | 291434247 | 25.7488 |
| 609 | 1.64204 | 370881 | 225866529 | 24.6779 | 664 | 1.50602 | 440896 | 292754944 | 25.7682 |
| 610 | 1.63934 | 372100 | 226981000 | 24.6982 | 665 | 1.50376 | 442225 | 294079625 | 25.7876 |
| 611 | 1.63666 | 373321 | 228099131 | 24.7184 | 666 | 1.50150 | 443556 | 295408296 | 25.8070 |
| 612 | 1.63399 | 374544 | 229220928 | 24.7386 | 667 | 1.49925 | 444889 | 296740963 | 25.8263 |
| 613 | 1.63132 | 375769 | 230346397 | 24.7588 | 668 | 1.49701 | 446224 | 298077632 | 25.8457 |
| 614 | 1.62866 | 376996 | 231475544 | 24.7790 | 669 | 1.49477 | 447561 | 299418309 | 25.8650 |

VALUES OF RECIPROALS, SQUARES, CUBES, AND SQUARE ROOTS
OF NATURAL NUMBERS

| n | $1000 \cdot \frac{1}{n}$ | n^2 | n^3 | \sqrt{n} | n | $1000 \cdot \frac{1}{n}$ | n^2 | n^3 | \sqrt{n} |
|-----|--------------------------|--------|-----------|------------|-----|--------------------------|--------|-----------|------------|
| 670 | 1.49254 | 448900 | 300763000 | 25.8844 | 725 | 1.37931 | 525625 | 381078125 | 26.9258 |
| 671 | 1.49031 | 450241 | 302111711 | 25.9037 | 726 | 1.37741 | 529076 | 382657176 | 26.9444 |
| 672 | 1.48810 | 451584 | 303464448 | 25.9230 | 727 | 1.37552 | 532529 | 384240583 | 26.9629 |
| 673 | 1.48588 | 452929 | 304821217 | 25.9422 | 728 | 1.37303 | 529984 | 385828352 | 26.9815 |
| 674 | 1.48368 | 454276 | 306182024 | 25.9615 | 729 | 1.37174 | 531441 | 387420489 | 27.0000 |
| 675 | 1.48148 | 455625 | 307546875 | 25.9808 | 730 | 1.36986 | 532900 | 389017000 | 27.0185 |
| 676 | 1.47929 | 456976 | 308915776 | 26.0000 | 731 | 1.36799 | 534361 | 390617891 | 27.0370 |
| 677 | 1.47710 | 458329 | 310288733 | 26.0192 | 732 | 1.36612 | 535824 | 392223108 | 27.0555 |
| 678 | 1.47493 | 459684 | 311665752 | 26.0384 | 733 | 1.36426 | 537289 | 393832837 | 27.0740 |
| 679 | 1.47275 | 461041 | 313046839 | 26.0576 | 734 | 1.36240 | 538756 | 395446904 | 27.0924 |
| 680 | 1.47059 | 462400 | 314432000 | 26.0768 | 735 | 1.36054 | 540225 | 397065375 | 27.1109 |
| 681 | 1.46843 | 463761 | 315821241 | 26.0960 | 736 | 1.35870 | 541696 | 398688256 | 27.1293 |
| 682 | 1.46628 | 465124 | 317214568 | 26.1151 | 737 | 1.35685 | 543169 | 400315553 | 27.1477 |
| 683 | 1.46413 | 466489 | 318611987 | 26.1343 | 738 | 1.35501 | 544644 | 401944722 | 27.1660 |
| 684 | 1.46199 | 467856 | 320013504 | 26.1534 | 739 | 1.35318 | 546121 | 403583419 | 27.1846 |
| 685 | 1.45985 | 469225 | 321419125 | 26.1725 | 740 | 1.35135 | 547600 | 405224000 | 27.2029 |
| 686 | 1.45773 | 470596 | 322828856 | 26.1916 | 741 | 1.34953 | 549081 | 406869021 | 27.2213 |
| 687 | 1.45560 | 471969 | 324242703 | 26.2107 | 742 | 1.34771 | 550504 | 408518488 | 27.2397 |
| 688 | 1.45349 | 473344 | 325660662 | 26.2298 | 743 | 1.34590 | 552049 | 410172407 | 27.2580 |
| 689 | 1.45138 | 474721 | 327082769 | 26.2488 | 744 | 1.34409 | 553536 | 411830784 | 27.2764 |
| 690 | 1.44928 | 476100 | 328509000 | 26.2679 | 745 | 1.34228 | 555025 | 413493625 | 27.2947 |
| 691 | 1.44718 | 477481 | 329939371 | 26.2869 | 746 | 1.34048 | 556516 | 415160936 | 27.3130 |
| 692 | 1.44509 | 478864 | 331373888 | 26.3059 | 747 | 1.33869 | 558009 | 416832723 | 27.3313 |
| 693 | 1.44300 | 480249 | 332812557 | 26.3249 | 748 | 1.33690 | 559504 | 418508992 | 27.3496 |
| 694 | 1.44092 | 481636 | 334255384 | 26.3439 | 749 | 1.33511 | 561001 | 420189749 | 27.3679 |
| 695 | 1.43885 | 483025 | 335702375 | 26.3629 | 750 | 1.33333 | 562500 | 421875000 | 27.3861 |
| 696 | 1.43678 | 484416 | 337153536 | 26.3818 | 751 | 1.33156 | 564001 | 423564751 | 27.4044 |
| 697 | 1.43472 | 485809 | 338608873 | 26.4008 | 752 | 1.32979 | 565504 | 425259008 | 27.4226 |
| 698 | 1.43266 | 487204 | 340068392 | 26.4197 | 753 | 1.32802 | 567009 | 426957777 | 27.4408 |
| 699 | 1.43062 | 488601 | 341532099 | 26.4386 | 754 | 1.32626 | 568516 | 428661064 | 27.4591 |
| 700 | 1.42857 | 490000 | 343000000 | 26.4575 | 755 | 1.32450 | 570025 | 430368875 | 27.4773 |
| 701 | 1.42653 | 491401 | 344472101 | 26.4764 | 756 | 1.32275 | 571536 | 432081216 | 27.4955 |
| 702 | 1.42450 | 492804 | 345948408 | 26.4953 | 757 | 1.32100 | 573049 | 433798093 | 27.5136 |
| 703 | 1.42248 | 494209 | 347428927 | 26.5141 | 758 | 1.31926 | 574564 | 435519512 | 27.5318 |
| 704 | 1.42045 | 495616 | 348913664 | 26.5330 | 759 | 1.31752 | 576081 | 437245479 | 27.5500 |
| 705 | 1.41844 | 497025 | 350402625 | 26.5518 | 760 | 1.31579 | 577600 | 438976000 | 27.5681 |
| 706 | 1.41643 | 498436 | 351895816 | 26.5707 | 761 | 1.31406 | 579121 | 440711081 | 27.5862 |
| 707 | 1.41443 | 499849 | 353393243 | 26.5895 | 762 | 1.31234 | 580644 | 442450728 | 27.6043 |
| 708 | 1.41243 | 501264 | 354894912 | 26.6083 | 763 | 1.31062 | 582169 | 444194947 | 27.6225 |
| 709 | 1.41044 | 502681 | 356400829 | 26.6271 | 764 | 1.30890 | 583696 | 445943744 | 27.6405 |
| 710 | 1.40845 | 504100 | 357911000 | 26.6458 | 765 | 1.30719 | 585225 | 447697125 | 27.6586 |
| 711 | 1.40647 | 505521 | 359425431 | 26.6646 | 766 | 1.30548 | 586756 | 449455096 | 27.6767 |
| 712 | 1.40449 | 506944 | 360944128 | 26.6833 | 767 | 1.30378 | 588289 | 451217603 | 27.6948 |
| 713 | 1.40252 | 508369 | 362467097 | 26.7021 | 768 | 1.30208 | 589824 | 452984832 | 27.7128 |
| 714 | 1.40056 | 509796 | 363994344 | 26.7208 | 769 | 1.30039 | 591361 | 454756609 | 27.7308 |
| 715 | 1.39860 | 511225 | 365525875 | 26.7395 | 770 | 1.29870 | 592900 | 456533000 | 27.7489 |
| 716 | 1.39665 | 512656 | 367061696 | 26.7582 | 771 | 1.29702 | 594441 | 458314011 | 27.7669 |
| 717 | 1.39470 | 514089 | 368601813 | 26.7769 | 772 | 1.29534 | 595984 | 460099648 | 27.7849 |
| 718 | 1.39276 | 515524 | 370146232 | 26.7955 | 773 | 1.29366 | 597529 | 461889917 | 27.8029 |
| 719 | 1.39082 | 516961 | 371694959 | 26.8142 | 774 | 1.29199 | 599076 | 463684824 | 27.8209 |
| 720 | 1.38889 | 518400 | 373248000 | 26.8328 | 775 | 1.29032 | 600625 | 465484375 | 27.8388 |
| 721 | 1.38696 | 519841 | 374805361 | 26.8514 | 776 | 1.28866 | 602176 | 467288576 | 27.8568 |
| 722 | 1.38504 | 521284 | 376367048 | 26.8701 | 777 | 1.28700 | 603729 | 469097433 | 27.8747 |
| 723 | 1.38313 | 522729 | 377933067 | 26.8887 | 778 | 1.28535 | 605284 | 470910952 | 27.8927 |
| 724 | 1.38122 | 524176 | 379503424 | 26.9072 | 779 | 1.28370 | 606841 | 472720139 | 27.9106 |

VALUES OF RECIPROCAL, SQUARES, CUBES, AND SQUARE ROOTS OF NATURAL NUMBERS

| n | $1000 \cdot \frac{1}{n}$ | n^2 | n^3 | \sqrt{n} | n | $1000 \cdot \frac{1}{n}$ | n^2 | n^3 | \sqrt{n} |
|-----|--------------------------|--------|-----------|------------|-----|--------------------------|--------|-----------|------------|
| 780 | 1.28205 | 608400 | 474552000 | 27.9285 | 835 | 1.19760 | 697225 | 582182875 | 28.8964 |
| 781 | 1.28041 | 609961 | 476379541 | 27.9464 | 836 | 1.19617 | 698896 | 584277056 | 28.9137 |
| 782 | 1.27877 | 611524 | 478211768 | 27.9643 | 837 | 1.19474 | 700569 | 586376253 | 28.9310 |
| 783 | 1.27714 | 613089 | 480048637 | 27.9821 | 838 | 1.19332 | 702244 | 588480472 | 28.9482 |
| 784 | 1.27551 | 614656 | 481890304 | 28.0000 | 839 | 1.19190 | 703921 | 590589719 | 28.9655 |
| 785 | 1.27389 | 616225 | 483736625 | 28.0179 | 840 | 1.19048 | 705600 | 592704000 | 28.9828 |
| 786 | 1.27226 | 617796 | 485587636 | 28.0357 | 841 | 1.18906 | 707281 | 594823321 | 29.0000 |
| 787 | 1.27065 | 619369 | 487443403 | 28.0535 | 842 | 1.18765 | 708964 | 596947688 | 29.0172 |
| 788 | 1.26904 | 620944 | 489303872 | 28.0713 | 843 | 1.18624 | 710649 | 599077107 | 29.0345 |
| 789 | 1.26743 | 622521 | 491169069 | 28.0891 | 844 | 1.18483 | 712336 | 601211584 | 29.0517 |
| 790 | 1.26582 | 624100 | 493039000 | 28.1069 | 845 | 1.18343 | 714025 | 603351125 | 29.0689 |
| 791 | 1.26422 | 625681 | 494913671 | 28.1247 | 846 | 1.18203 | 715716 | 605495736 | 29.0861 |
| 792 | 1.26263 | 627264 | 496793088 | 28.1425 | 847 | 1.18064 | 717409 | 607645423 | 29.1033 |
| 793 | 1.26103 | 628849 | 498677257 | 28.1603 | 848 | 1.17925 | 719104 | 609800192 | 29.1204 |
| 794 | 1.25945 | 630436 | 500566184 | 28.1780 | 849 | 1.17786 | 720801 | 611960049 | 29.1376 |
| 795 | 1.25786 | 632025 | 502459875 | 28.1957 | 850 | 1.17647 | 722500 | 614125000 | 29.1548 |
| 796 | 1.25628 | 633616 | 504358336 | 28.2135 | 851 | 1.17509 | 724201 | 616295051 | 29.1719 |
| 797 | 1.25471 | 635209 | 506261573 | 28.2312 | 852 | 1.17371 | 725904 | 618470208 | 29.1890 |
| 798 | 1.25313 | 636804 | 508169592 | 28.2489 | 853 | 1.17233 | 727609 | 620650477 | 29.2062 |
| 799 | 1.25156 | 638401 | 510082399 | 28.2666 | 854 | 1.17096 | 729316 | 622835864 | 29.2233 |
| 800 | 1.25000 | 640000 | 512000000 | 28.2843 | 855 | 1.16959 | 731025 | 625026375 | 29.2404 |
| 801 | 1.24844 | 641601 | 513922401 | 28.3019 | 856 | 1.16822 | 732736 | 627222016 | 29.2575 |
| 802 | 1.24688 | 643204 | 515849608 | 28.3196 | 857 | 1.16686 | 734449 | 629422793 | 29.2746 |
| 803 | 1.24533 | 644809 | 517781627 | 28.3373 | 858 | 1.16550 | 736164 | 631628712 | 29.2916 |
| 804 | 1.24378 | 646416 | 519718464 | 28.3549 | 859 | 1.16414 | 737881 | 633839779 | 29.3087 |
| 805 | 1.24224 | 648025 | 521660125 | 28.3725 | 860 | 1.16279 | 739600 | 636056000 | 29.3258 |
| 806 | 1.24069 | 649636 | 523606616 | 28.3901 | 861 | 1.16144 | 741321 | 638277381 | 29.3428 |
| 807 | 1.23916 | 651249 | 525557943 | 28.4077 | 862 | 1.16009 | 743044 | 640503928 | 29.3598 |
| 808 | 1.23762 | 652864 | 527514112 | 28.4253 | 863 | 1.15875 | 744769 | 642735647 | 29.3769 |
| 809 | 1.23609 | 654481 | 529475129 | 28.4429 | 864 | 1.15741 | 746496 | 644972544 | 29.3939 |
| 810 | 1.23457 | 656100 | 531441000 | 28.4605 | 865 | 1.15607 | 748225 | 647214625 | 29.4109 |
| 811 | 1.23305 | 657721 | 533411731 | 28.4781 | 866 | 1.15473 | 749956 | 649461896 | 29.4279 |
| 812 | 1.23153 | 659344 | 535387328 | 28.4956 | 867 | 1.15340 | 751689 | 651714363 | 29.4449 |
| 813 | 1.23001 | 660969 | 537367797 | 28.5132 | 868 | 1.15207 | 753424 | 653972032 | 29.4618 |
| 814 | 1.22850 | 662596 | 539353144 | 28.5307 | 869 | 1.15075 | 755161 | 656234909 | 29.4788 |
| 815 | 1.22699 | 664225 | 541343375 | 28.5482 | 870 | 1.14943 | 756900 | 658503000 | 29.4958 |
| 816 | 1.22549 | 665856 | 543338496 | 28.5657 | 871 | 1.14811 | 758641 | 660776311 | 29.5127 |
| 817 | 1.22399 | 667489 | 545338513 | 28.5832 | 872 | 1.14679 | 760384 | 663054848 | 29.5296 |
| 818 | 1.22249 | 669124 | 547343432 | 28.6007 | 873 | 1.14548 | 762129 | 665338617 | 29.5466 |
| 819 | 1.22100 | 670761 | 549353259 | 28.6182 | 874 | 1.14416 | 763876 | 667627624 | 29.5635 |
| 820 | 1.21951 | 672400 | 551368000 | 28.6356 | 875 | 1.14286 | 765625 | 669921875 | 29.5804 |
| 821 | 1.21803 | 674041 | 553387661 | 28.6531 | 876 | 1.14155 | 767376 | 672221376 | 29.5973 |
| 822 | 1.21655 | 675684 | 555412248 | 28.6705 | 877 | 1.14025 | 769129 | 674526133 | 29.6142 |
| 823 | 1.21507 | 677329 | 557441767 | 28.6880 | 878 | 1.13895 | 770884 | 676836152 | 29.6311 |
| 824 | 1.21359 | 678976 | 559476224 | 28.7054 | 879 | 1.13766 | 772641 | 679151439 | 29.6479 |
| 825 | 1.21212 | 680625 | 561515625 | 28.7228 | 880 | 1.13636 | 774400 | 681472000 | 29.6648 |
| 826 | 1.21065 | 682276 | 563559976 | 28.7402 | 881 | 1.13507 | 776161 | 683797841 | 29.6816 |
| 827 | 1.20919 | 683929 | 565609283 | 28.7576 | 882 | 1.13379 | 777924 | 686128968 | 29.6985 |
| 828 | 1.20773 | 685584 | 567663552 | 28.7750 | 883 | 1.13250 | 779689 | 688465387 | 29.7153 |
| 829 | 1.20627 | 687241 | 569722789 | 28.7924 | 884 | 1.13122 | 781456 | 690807104 | 29.7321 |
| 830 | 1.20482 | 688900 | 571787000 | 28.8097 | 885 | 1.12994 | 783225 | 693154125 | 29.7489 |
| 831 | 1.20337 | 690561 | 573856191 | 28.8271 | 886 | 1.12867 | 784996 | 695506456 | 29.7658 |
| 832 | 1.20192 | 692224 | 575930368 | 28.8444 | 887 | 1.12740 | 786769 | 697864103 | 29.7825 |
| 833 | 1.20048 | 693889 | 578009537 | 28.8617 | 888 | 1.12613 | 788544 | 700227072 | 29.7993 |
| 834 | 1.19904 | 695556 | 580093704 | 28.8791 | 889 | 1.12486 | 790321 | 702595369 | 29.8161 |

VALUES OF RECIPROCAL, SQUARES, CUBES, AND SQUARE ROOTS
OF NATURAL NUMBERS

| n | $1000 \cdot \frac{1}{n}$ | n^2 | n^3 | \sqrt{n} | n | $1000 \cdot \frac{1}{n}$ | n^2 | n^3 | \sqrt{n} |
|-----|--------------------------|--------|-----------|------------|-----|--------------------------|--------|------------|------------|
| 890 | 1.12360 | 792100 | 704969000 | 29.8329 | 945 | 1.05820 | 893025 | 843908625 | 30.7409 |
| 891 | 1.12233 | 793881 | 707347971 | 29.8496 | 946 | 1.05708 | 894916 | 846590536 | 30.7571 |
| 892 | 1.12108 | 795664 | 709732288 | 29.8664 | 947 | 1.05597 | 896809 | 849278123 | 30.7734 |
| 893 | 1.11982 | 797449 | 712121057 | 29.8831 | 948 | 1.05485 | 898704 | 851971392 | 30.7896 |
| 894 | 1.11857 | 799236 | 714516984 | 29.8998 | 949 | 1.05374 | 900601 | 854670349 | 30.8058 |
| 895 | 1.11732 | 801025 | 716917375 | 29.9166 | 950 | 1.05263 | 902500 | 857375000 | 30.8221 |
| 896 | 1.11607 | 802816 | 719323136 | 29.9333 | 951 | 1.05152 | 904401 | 860085351 | 30.8383 |
| 897 | 1.11483 | 804609 | 721734273 | 29.9500 | 952 | 1.05042 | 906304 | 862801408 | 30.8545 |
| 898 | 1.11359 | 806404 | 724150792 | 29.9666 | 953 | 1.04932 | 908209 | 865523177 | 30.8707 |
| 899 | 1.11235 | 808201 | 726572099 | 29.9833 | 954 | 1.04822 | 910116 | 868250664 | 30.8869 |
| 900 | 1.11111 | 810000 | 729000000 | 30.0000 | 955 | 1.04712 | 912025 | 870983875 | 30.9031 |
| 901 | 1.10988 | 811801 | 731432701 | 30.0167 | 956 | 1.04603 | 913936 | 873722816 | 30.9192 |
| 902 | 1.10865 | 813604 | 733870808 | 30.0333 | 957 | 1.04493 | 915849 | 876467493 | 30.9354 |
| 903 | 1.10742 | 815409 | 736314327 | 30.0500 | 958 | 1.04384 | 917764 | 879217912 | 30.9516 |
| 904 | 1.10619 | 817216 | 738763204 | 30.0666 | 959 | 1.04275 | 919681 | 881974079 | 30.9677 |
| 905 | 1.10497 | 819025 | 741217625 | 30.0832 | 960 | 1.04167 | 921600 | 884736000 | 30.9839 |
| 906 | 1.10375 | 820836 | 743677416 | 30.0998 | 961 | 1.04058 | 923521 | 887503681 | 31.0000 |
| 907 | 1.10254 | 822649 | 746142043 | 30.1164 | 962 | 1.03950 | 925444 | 890277128 | 31.0161 |
| 908 | 1.10132 | 824464 | 748613312 | 30.1330 | 963 | 1.03842 | 927369 | 893056347 | 31.0322 |
| 909 | 1.10011 | 826281 | 751089429 | 30.1496 | 964 | 1.03734 | 929296 | 895841344 | 31.0483 |
| 910 | 1.09890 | 828100 | 753571000 | 30.1662 | 965 | 1.03627 | 931225 | 898632125 | 31.0644 |
| 911 | 1.09769 | 829921 | 756058031 | 30.1828 | 966 | 1.03520 | 933156 | 901428696 | 31.0805 |
| 912 | 1.09649 | 831744 | 758550528 | 30.1993 | 967 | 1.03413 | 935089 | 904231063 | 31.0966 |
| 913 | 1.09529 | 833569 | 761048497 | 30.2159 | 968 | 1.03306 | 937024 | 907039232 | 31.1127 |
| 914 | 1.09409 | 835396 | 763551944 | 30.2324 | 969 | 1.03199 | 938961 | 909853209 | 31.1288 |
| 915 | 1.09290 | 837225 | 766060875 | 30.2490 | 970 | 1.03093 | 940900 | 912673000 | 31.1448 |
| 916 | 1.09170 | 839056 | 768575296 | 30.2655 | 971 | 1.02987 | 942841 | 915498611 | 31.1609 |
| 917 | 1.09051 | 840889 | 771095213 | 30.2820 | 972 | 1.02881 | 944784 | 918330048 | 31.1769 |
| 918 | 1.08932 | 842724 | 773620632 | 30.2985 | 973 | 1.02775 | 946729 | 921167317 | 31.1929 |
| 919 | 1.08814 | 844561 | 776151559 | 30.3150 | 974 | 1.02669 | 948676 | 924010424 | 31.2090 |
| 920 | 1.08696 | 846400 | 778688000 | 30.3315 | 975 | 1.02564 | 950625 | 926859375 | 31.2250 |
| 921 | 1.08578 | 848241 | 781229961 | 30.3480 | 976 | 1.02459 | 952576 | 929714176 | 31.2410 |
| 922 | 1.08460 | 850084 | 783777448 | 30.3645 | 977 | 1.02354 | 954529 | 932574833 | 31.2570 |
| 923 | 1.08342 | 851929 | 786330467 | 30.3809 | 978 | 1.02249 | 956484 | 935441352 | 31.2730 |
| 924 | 1.08225 | 853776 | 788889024 | 30.3974 | 979 | 1.02145 | 958441 | 938313739 | 31.2890 |
| 925 | 1.08108 | 855625 | 791453125 | 30.4138 | 980 | 1.02041 | 960400 | 941192000 | 31.3050 |
| 926 | 1.07991 | 857476 | 794022776 | 30.4302 | 981 | 1.01937 | 962361 | 944076141 | 31.3209 |
| 927 | 1.07875 | 859329 | 796597983 | 30.4467 | 982 | 1.01833 | 964324 | 946966168 | 31.3369 |
| 928 | 1.07759 | 861184 | 799178752 | 30.4631 | 983 | 1.01729 | 966289 | 949862087 | 31.3528 |
| 929 | 1.07643 | 863041 | 801765089 | 30.4795 | 984 | 1.01626 | 968256 | 9527673904 | 31.3688 |
| 930 | 1.07527 | 864900 | 804357000 | 30.4959 | 985 | 1.01523 | 970225 | 955671625 | 31.3847 |
| 931 | 1.07411 | 866761 | 806954491 | 30.5123 | 986 | 1.01420 | 972196 | 958585256 | 31.4006 |
| 932 | 1.07296 | 868624 | 809557568 | 30.5287 | 987 | 1.01317 | 974169 | 961504803 | 31.4166 |
| 933 | 1.07181 | 870489 | 812166237 | 30.5450 | 988 | 1.01215 | 976144 | 964430272 | 31.4325 |
| 934 | 1.07066 | 872356 | 814780504 | 30.5614 | 989 | 1.01112 | 978121 | 967361669 | 31.4484 |
| 935 | 1.06952 | 874225 | 817400375 | 30.5778 | 990 | 1.01010 | 980100 | 970299000 | 31.4643 |
| 936 | 1.06838 | 876096 | 820025856 | 30.5941 | 991 | 1.00908 | 982081 | 973242271 | 31.4802 |
| 937 | 1.06724 | 877969 | 822656953 | 30.6105 | 992 | 1.00806 | 984064 | 976191488 | 31.4960 |
| 938 | 1.06610 | 879844 | 825293672 | 30.6268 | 993 | 1.00705 | 986049 | 979146657 | 31.5119 |
| 939 | 1.06496 | 881721 | 827936019 | 30.6431 | 994 | 1.00604 | 988036 | 982107784 | 31.5278 |
| 940 | 1.06383 | 883600 | 830584000 | 30.6594 | 995 | 1.00503 | 990025 | 985074875 | 31.5436 |
| 941 | 1.06270 | 885481 | 833237621 | 30.6757 | 996 | 1.00402 | 992016 | 988047936 | 31.5595 |
| 942 | 1.06157 | 887364 | 835896888 | 30.6920 | 997 | 1.00301 | 994009 | 991026973 | 31.5753 |
| 943 | 1.06045 | 889249 | 838561807 | 30.7083 | 998 | 1.00200 | 996004 | 994011992 | 31.5911 |
| 944 | 1.05932 | 891136 | 841232384 | 30.7246 | 999 | 1.00100 | 998001 | 997002999 | 31.6070 |

TABLE 10
LOGARITHMS

| N. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|-----|------|------|------|------|------|------|------|------|------|------|------|
| 100 | 0000 | 0004 | 0009 | 0013 | 0017 | 0022 | 0026 | 0030 | 0035 | 0039 | 0043 |
| 101 | 0043 | 0048 | 0052 | 0056 | 0060 | 0065 | 0069 | 0073 | 0077 | 0082 | 0086 |
| 102 | 0086 | 0090 | 0095 | 0099 | 0103 | 0107 | 0111 | 0116 | 0120 | 0124 | 0128 |
| 103 | 0128 | 0133 | 0137 | 0141 | 0145 | 0149 | 0154 | 0158 | 0162 | 0166 | 0170 |
| 104 | 0170 | 0175 | 0179 | 0183 | 0187 | 0191 | 0195 | 0199 | 0204 | 0208 | 0212 |
| 105 | 0212 | 0216 | 0220 | 0224 | 0228 | 0233 | 0237 | 0241 | 0245 | 0249 | 0253 |
| 106 | 0253 | 0257 | 0261 | 0265 | 0269 | 0273 | 0278 | 0282 | 0286 | 0290 | 0294 |
| 107 | 0294 | 0298 | 0302 | 0306 | 0310 | 0314 | 0318 | 0322 | 0326 | 0330 | 0334 |
| 108 | 0334 | 0338 | 0342 | 0346 | 0350 | 0354 | 0358 | 0362 | 0366 | 0370 | 0374 |
| 109 | 0374 | 0378 | 0382 | 0386 | 0390 | 0394 | 0398 | 0402 | 0406 | 0410 | 0414 |
| 110 | 0414 | 0418 | 0422 | 0426 | 0430 | 0434 | 0438 | 0441 | 0445 | 0449 | 0453 |
| 111 | 0453 | 0457 | 0461 | 0465 | 0469 | 0473 | 0477 | 0481 | 0484 | 0488 | 0492 |
| 112 | 0492 | 0496 | 0500 | 0504 | 0508 | 0512 | 0515 | 0519 | 0523 | 0527 | 0531 |
| 113 | 0531 | 0535 | 0538 | 0542 | 0546 | 0550 | 0554 | 0558 | 0561 | 0565 | 0569 |
| 114 | 0569 | 0573 | 0577 | 0580 | 0584 | 0588 | 0592 | 0596 | 0599 | 0603 | 0607 |
| 115 | 0607 | 0611 | 0615 | 0618 | 0622 | 0626 | 0630 | 0633 | 0637 | 0641 | 0645 |
| 116 | 0645 | 0648 | 0652 | 0656 | 0660 | 0663 | 0667 | 0671 | 0674 | 0678 | 0682 |
| 117 | 0682 | 0686 | 0689 | 0693 | 0697 | 0700 | 0704 | 0708 | 0711 | 0715 | 0719 |
| 118 | 0719 | 0722 | 0726 | 0730 | 0734 | 0737 | 0741 | 0745 | 0748 | 0752 | 0755 |
| 119 | 0755 | 0759 | 0763 | 0766 | 0770 | 0774 | 0777 | 0781 | 0785 | 0788 | 0792 |
| 120 | 0792 | 0795 | 0799 | 0803 | 0806 | 0810 | 0813 | 0817 | 0821 | 0824 | 0828 |
| 121 | 0828 | 0831 | 0835 | 0839 | 0842 | 0846 | 0849 | 0853 | 0856 | 0860 | 0864 |
| 122 | 0864 | 0867 | 0871 | 0874 | 0878 | 0881 | 0885 | 0888 | 0892 | 0896 | 0899 |
| 123 | 0899 | 0903 | 0906 | 0910 | 0913 | 0917 | 0920 | 0924 | 0927 | 0931 | 0934 |
| 124 | 0934 | 0938 | 0941 | 0945 | 0948 | 0952 | 0955 | 0959 | 0962 | 0966 | 0969 |
| 125 | 0969 | 0973 | 0976 | 0980 | 0983 | 0986 | 0990 | 0993 | 0997 | 1000 | 1004 |
| 126 | 1004 | 1007 | 1011 | 1014 | 1017 | 1021 | 1024 | 1028 | 1031 | 1035 | 1038 |
| 127 | 1038 | 1041 | 1045 | 1048 | 1052 | 1055 | 1059 | 1062 | 1065 | 1069 | 1072 |
| 128 | 1072 | 1075 | 1079 | 1082 | 1086 | 1089 | 1092 | 1096 | 1099 | 1103 | 1106 |
| 129 | 1106 | 1109 | 1113 | 1116 | 1119 | 1123 | 1126 | 1129 | 1133 | 1136 | 1139 |
| 130 | 1139 | 1143 | 1146 | 1149 | 1153 | 1156 | 1159 | 1163 | 1166 | 1169 | 1173 |
| 131 | 1173 | 1176 | 1179 | 1183 | 1186 | 1189 | 1193 | 1196 | 1199 | 1202 | 1206 |
| 132 | 1206 | 1209 | 1212 | 1216 | 1219 | 1222 | 1225 | 1229 | 1232 | 1235 | 1239 |
| 133 | 1239 | 1242 | 1245 | 1248 | 1252 | 1255 | 1258 | 1261 | 1265 | 1268 | 1271 |
| 134 | 1271 | 1274 | 1278 | 1281 | 1284 | 1287 | 1290 | 1294 | 1297 | 1300 | 1303 |
| 135 | 1303 | 1307 | 1310 | 1313 | 1316 | 1319 | 1323 | 1326 | 1329 | 1332 | 1335 |
| 136 | 1335 | 1339 | 1342 | 1345 | 1348 | 1351 | 1355 | 1358 | 1361 | 1364 | 1367 |
| 137 | 1367 | 1370 | 1374 | 1377 | 1380 | 1383 | 1386 | 1389 | 1392 | 1396 | 1399 |
| 138 | 1399 | 1402 | 1405 | 1408 | 1411 | 1414 | 1418 | 1421 | 1424 | 1427 | 1430 |
| 139 | 1430 | 1433 | 1436 | 1440 | 1443 | 1446 | 1449 | 1452 | 1455 | 1458 | 1461 |
| 140 | 1461 | 1464 | 1467 | 1471 | 1474 | 1477 | 1480 | 1483 | 1486 | 1489 | 1492 |
| 141 | 1492 | 1495 | 1498 | 1501 | 1504 | 1508 | 1511 | 1514 | 1517 | 1520 | 1523 |
| 142 | 1523 | 1526 | 1529 | 1532 | 1535 | 1538 | 1541 | 1544 | 1547 | 1550 | 1553 |
| 143 | 1553 | 1556 | 1559 | 1562 | 1565 | 1569 | 1572 | 1575 | 1578 | 1581 | 1584 |
| 144 | 1584 | 1587 | 1590 | 1593 | 1596 | 1599 | 1602 | 1605 | 1608 | 1611 | 1614 |
| 145 | 1614 | 1617 | 1620 | 1623 | 1626 | 1629 | 1632 | 1635 | 1638 | 1641 | 1644 |
| 146 | 1644 | 1647 | 1649 | 1652 | 1655 | 1658 | 1661 | 1664 | 1667 | 1670 | 1673 |
| 147 | 1673 | 1676 | 1679 | 1682 | 1685 | 1688 | 1691 | 1694 | 1697 | 1700 | 1703 |
| 148 | 1703 | 1706 | 1708 | 1711 | 1714 | 1717 | 1720 | 1723 | 1726 | 1729 | 1732 |
| 149 | 1732 | 1735 | 1738 | 1741 | 1744 | 1746 | 1749 | 1752 | 1755 | 1758 | 1761 |

LOGARITHMS

| N. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|-----|------|------|------|------|------|------|------|------|------|------|------|
| 150 | 1761 | 1764 | 1767 | 1770 | 1772 | 1775 | 1778 | 1781 | 1784 | 1787 | 1790 |
| 151 | 1790 | 1793 | 1796 | 1798 | 1801 | 1804 | 1807 | 1810 | 1813 | 1816 | 1818 |
| 152 | 1818 | 1821 | 1824 | 1827 | 1830 | 1833 | 1836 | 1838 | 1841 | 1844 | 1847 |
| 153 | 1847 | 1850 | 1853 | 1855 | 1858 | 1861 | 1864 | 1867 | 1870 | 1872 | 1875 |
| 154 | 1875 | 1878 | 1881 | 1884 | 1886 | 1889 | 1892 | 1895 | 1898 | 1901 | 1903 |
| 155 | 1903 | 1906 | 1909 | 1912 | 1915 | 1917 | 1920 | 1923 | 1926 | 1928 | 1931 |
| 156 | 1931 | 1934 | 1937 | 1940 | 1942 | 1945 | 1948 | 1951 | 1953 | 1956 | 1959 |
| 157 | 1959 | 1962 | 1965 | 1967 | 1970 | 1973 | 1976 | 1978 | 1981 | 1984 | 1987 |
| 158 | 1987 | 1989 | 1992 | 1995 | 1998 | 2000 | 2003 | 2006 | 2009 | 2011 | 2014 |
| 159 | 2014 | 2017 | 2019 | 2022 | 2025 | 2028 | 2030 | 2033 | 2036 | 2038 | 2041 |
| 160 | 2041 | 2044 | 2047 | 2049 | 2052 | 2055 | 2057 | 2060 | 2063 | 2066 | 2068 |
| 161 | 2068 | 2071 | 2074 | 2076 | 2079 | 2082 | 2084 | 2087 | 2090 | 2092 | 2095 |
| 162 | 2095 | 2098 | 2101 | 2103 | 2106 | 2109 | 2111 | 2114 | 2117 | 2119 | 2122 |
| 163 | 2122 | 2125 | 2127 | 2130 | 2133 | 2135 | 2138 | 2140 | 2143 | 2146 | 2148 |
| 164 | 2148 | 2151 | 2154 | 2156 | 2159 | 2162 | 2164 | 2167 | 2170 | 2172 | 2175 |
| 165 | 2175 | 2177 | 2180 | 2183 | 2185 | 2188 | 2191 | 2193 | 2196 | 2198 | 2201 |
| 166 | 2201 | 2204 | 2206 | 2209 | 2212 | 2214 | 2217 | 2219 | 2222 | 2225 | 2227 |
| 167 | 2227 | 2230 | 2232 | 2235 | 2238 | 2240 | 2243 | 2245 | 2248 | 2251 | 2253 |
| 168 | 2253 | 2256 | 2258 | 2261 | 2263 | 2266 | 2269 | 2271 | 2274 | 2276 | 2279 |
| 169 | 2279 | 2281 | 2284 | 2287 | 2289 | 2292 | 2294 | 2297 | 2299 | 2302 | 2304 |
| 170 | 2304 | 2307 | 2310 | 2312 | 2315 | 2317 | 2320 | 2322 | 2325 | 2327 | 2330 |
| 171 | 2330 | 2333 | 2335 | 2338 | 2340 | 2343 | 2345 | 2348 | 2350 | 2353 | 2355 |
| 172 | 2355 | 2358 | 2360 | 2363 | 2365 | 2368 | 2370 | 2373 | 2375 | 2378 | 2380 |
| 173 | 2380 | 2383 | 2385 | 2388 | 2390 | 2393 | 2395 | 2398 | 2400 | 2403 | 2405 |
| 174 | 2405 | 2408 | 2410 | 2413 | 2415 | 2418 | 2420 | 2423 | 2425 | 2428 | 2430 |
| 175 | 2430 | 2433 | 2435 | 2438 | 2440 | 2443 | 2445 | 2448 | 2450 | 2453 | 2455 |
| 176 | 2455 | 2458 | 2460 | 2463 | 2465 | 2467 | 2470 | 2472 | 2475 | 2477 | 2480 |
| 177 | 2480 | 2482 | 2485 | 2487 | 2490 | 2492 | 2494 | 2497 | 2499 | 2502 | 2504 |
| 178 | 2504 | 2507 | 2509 | 2512 | 2514 | 2516 | 2519 | 2521 | 2524 | 2526 | 2529 |
| 179 | 2529 | 2531 | 2533 | 2536 | 2538 | 2541 | 2543 | 2545 | 2548 | 2550 | 2553 |
| 180 | 2553 | 2555 | 2558 | 2560 | 2562 | 2565 | 2567 | 2570 | 2572 | 2574 | 2577 |
| 181 | 2577 | 2579 | 2582 | 2584 | 2586 | 2589 | 2591 | 2594 | 2596 | 2598 | 2601 |
| 182 | 2601 | 2603 | 2605 | 2608 | 2610 | 2613 | 2615 | 2617 | 2620 | 2622 | 2625 |
| 183 | 2625 | 2627 | 2629 | 2632 | 2634 | 2636 | 2639 | 2641 | 2643 | 2646 | 2648 |
| 184 | 2648 | 2651 | 2653 | 2655 | 2658 | 2660 | 2662 | 2665 | 2667 | 2669 | 2672 |
| 185 | 2672 | 2674 | 2676 | 2679 | 2681 | 2683 | 2686 | 2688 | 2690 | 2693 | 2695 |
| 186 | 2695 | 2697 | 2700 | 2702 | 2704 | 2707 | 2709 | 2711 | 2714 | 2716 | 2718 |
| 187 | 2718 | 2721 | 2723 | 2725 | 2728 | 2730 | 2732 | 2735 | 2737 | 2739 | 2742 |
| 188 | 2742 | 2744 | 2746 | 2749 | 2751 | 2753 | 2755 | 2758 | 2760 | 2762 | 2765 |
| 189 | 2765 | 2767 | 2769 | 2772 | 2774 | 2776 | 2778 | 2781 | 2783 | 2785 | 2788 |
| 190 | 2788 | 2790 | 2792 | 2794 | 2797 | 2799 | 2801 | 2804 | 2806 | 2808 | 2810 |
| 191 | 2810 | 2813 | 2815 | 2817 | 2819 | 2822 | 2824 | 2826 | 2828 | 2831 | 2833 |
| 192 | 2833 | 2835 | 2838 | 2840 | 2842 | 2844 | 2847 | 2849 | 2851 | 2853 | 2856 |
| 193 | 2856 | 2858 | 2860 | 2862 | 2865 | 2867 | 2869 | 2871 | 2874 | 2876 | 2878 |
| 194 | 2878 | 2880 | 2882 | 2885 | 2887 | 2889 | 2891 | 2894 | 2896 | 2898 | 2900 |
| 195 | 2900 | 2903 | 2905 | 2907 | 2909 | 2911 | 2914 | 2916 | 2918 | 2920 | 2923 |
| 196 | 2923 | 2925 | 2927 | 2929 | 2931 | 2934 | 2936 | 2938 | 2940 | 2942 | 2945 |
| 197 | 2945 | 2947 | 2949 | 2951 | 2953 | 2956 | 2958 | 2960 | 2962 | 2964 | 2967 |
| 198 | 2967 | 2969 | 2971 | 2973 | 2975 | 2978 | 2980 | 2982 | 2984 | 2986 | 2989 |
| 199 | 2989 | 2991 | 2993 | 2995 | 2997 | 2999 | 3002 | 3004 | 3006 | 3008 | 3010 |

TABLE 11
LOGARITHMS

| N | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | P. P. | | | | |
|----|------|------|------|------|------|------|------|------|------|------|-------|---|----|----|----|
| | | | | | | | | | | | 1 | 2 | 3 | 4 | 5 |
| 10 | 0000 | 0043 | 0086 | 0128 | 0170 | 0212 | 0253 | 0294 | 0334 | 0374 | 4 | 8 | 12 | 17 | 21 |
| 11 | 0414 | 0453 | 0492 | 0531 | 0569 | 0607 | 0645 | 0682 | 0719 | 0755 | 4 | 8 | 11 | 15 | 19 |
| 12 | 0792 | 0828 | 0864 | 0899 | 0934 | 0969 | 1004 | 1038 | 1072 | 1106 | 3 | 7 | 10 | 14 | 17 |
| 13 | 1139 | 1173 | 1206 | 1239 | 1271 | 1303 | 1335 | 1367 | 1399 | 1430 | 3 | 6 | 10 | 13 | 16 |
| 14 | 1461 | 1492 | 1523 | 1553 | 1584 | 1614 | 1644 | 1673 | 1703 | 1732 | 3 | 6 | 9 | 12 | 15 |
| 15 | 1761 | 1790 | 1818 | 1847 | 1875 | 1903 | 1931 | 1959 | 1987 | 2014 | 3 | 6 | 8 | 11 | 14 |
| 16 | 2041 | 2068 | 2095 | 2122 | 2148 | 2175 | 2201 | 2227 | 2253 | 2279 | 3 | 5 | 8 | 11 | 13 |
| 17 | 2304 | 2330 | 2355 | 2380 | 2405 | 2430 | 2455 | 2480 | 2504 | 2529 | 2 | 5 | 7 | 10 | 12 |
| 18 | 2553 | 2577 | 2601 | 2625 | 2648 | 2672 | 2695 | 2718 | 2742 | 2765 | 2 | 5 | 7 | 9 | 12 |
| 19 | 2788 | 2810 | 2833 | 2856 | 2878 | 2900 | 2923 | 2945 | 2967 | 2989 | 2 | 4 | 7 | 9 | 11 |
| 20 | 3010 | 3032 | 3054 | 3075 | 3096 | 3118 | 3139 | 3160 | 3181 | 3201 | 2 | 4 | 6 | 8 | 11 |
| 21 | 3222 | 3243 | 3263 | 3284 | 3304 | 3324 | 3345 | 3365 | 3385 | 3404 | 2 | 4 | 6 | 8 | 10 |
| 22 | 3424 | 3444 | 3464 | 3483 | 3502 | 3522 | 3541 | 3560 | 3579 | 3598 | 2 | 4 | 6 | 8 | 10 |
| 23 | 3617 | 3636 | 3655 | 3674 | 3692 | 3711 | 3729 | 3747 | 3766 | 3784 | 2 | 4 | 5 | 7 | 9 |
| 24 | 3802 | 3820 | 3838 | 3856 | 3874 | 3892 | 3909 | 3927 | 3945 | 3962 | 2 | 4 | 5 | 7 | 9 |
| 25 | 3979 | 3997 | 4014 | 4031 | 4048 | 4065 | 4082 | 4099 | 4116 | 4133 | 2 | 3 | 5 | 7 | 9 |
| 26 | 4150 | 4166 | 4183 | 4200 | 4216 | 4232 | 4249 | 4265 | 4281 | 4298 | 2 | 3 | 5 | 7 | 8 |
| 27 | 4314 | 4330 | 4346 | 4362 | 4378 | 4393 | 4409 | 4425 | 4440 | 4456 | 2 | 3 | 5 | 6 | 8 |
| 28 | 4472 | 4487 | 4502 | 4518 | 4533 | 4548 | 4564 | 4579 | 4594 | 4609 | 2 | 3 | 5 | 6 | 8 |
| 29 | 4624 | 4639 | 4654 | 4669 | 4683 | 4698 | 4713 | 4728 | 4742 | 4757 | 1 | 3 | 4 | 6 | 7 |
| 30 | 4771 | 4786 | 4800 | 4814 | 4829 | 4843 | 4857 | 4871 | 4886 | 4900 | 1 | 3 | 4 | 6 | 7 |
| 31 | 4914 | 4928 | 4942 | 4955 | 4969 | 4983 | 4997 | 5011 | 5024 | 5038 | 1 | 3 | 4 | 6 | 7 |
| 32 | 5051 | 5065 | 5079 | 5092 | 5105 | 5119 | 5132 | 5145 | 5159 | 5172 | 1 | 3 | 4 | 5 | 7 |
| 33 | 5185 | 5198 | 5211 | 5224 | 5237 | 5250 | 5263 | 5276 | 5289 | 5302 | 1 | 3 | 4 | 5 | 6 |
| 34 | 5315 | 5328 | 5340 | 5353 | 5366 | 5378 | 5391 | 5403 | 5416 | 5428 | 1 | 3 | 4 | 5 | 6 |
| 35 | 5441 | 5453 | 5465 | 5478 | 5490 | 5502 | 5514 | 5527 | 5539 | 5551 | 1 | 2 | 4 | 5 | 6 |
| 36 | 5563 | 5575 | 5587 | 5599 | 5611 | 5623 | 5635 | 5647 | 5658 | 5670 | 1 | 2 | 4 | 5 | 6 |
| 37 | 5682 | 5694 | 5705 | 5717 | 5729 | 5740 | 5752 | 5763 | 5775 | 5786 | 1 | 2 | 3 | 5 | 6 |
| 38 | 5798 | 5809 | 5821 | 5832 | 5843 | 5855 | 5866 | 5877 | 5888 | 5899 | 1 | 2 | 3 | 5 | 6 |
| 39 | 5911 | 5922 | 5933 | 5944 | 5955 | 5966 | 5977 | 5988 | 5999 | 6010 | 1 | 2 | 3 | 4 | 6 |
| 40 | 6021 | 6031 | 6042 | 6053 | 6064 | 6075 | 6085 | 6096 | 6107 | 6117 | 1 | 2 | 3 | 4 | 5 |
| 41 | 6128 | 6138 | 6149 | 6160 | 6170 | 6180 | 6191 | 6201 | 6212 | 6222 | 1 | 2 | 3 | 4 | 5 |
| 42 | 6232 | 6243 | 6253 | 6263 | 6274 | 6284 | 6294 | 6304 | 6314 | 6325 | 1 | 2 | 3 | 4 | 5 |
| 43 | 6335 | 6345 | 6355 | 6365 | 6375 | 6385 | 6395 | 6405 | 6415 | 6425 | 1 | 2 | 3 | 4 | 5 |
| 44 | 6435 | 6444 | 6454 | 6464 | 6474 | 6484 | 6493 | 6503 | 6513 | 6522 | 1 | 2 | 3 | 4 | 5 |
| 45 | 6532 | 6542 | 6551 | 6561 | 6571 | 6580 | 6590 | 6599 | 6609 | 6618 | 1 | 2 | 3 | 4 | 5 |
| 46 | 6628 | 6637 | 6646 | 6656 | 6665 | 6675 | 6684 | 6693 | 6702 | 6712 | 1 | 2 | 3 | 4 | 5 |
| 47 | 6721 | 6730 | 6739 | 6749 | 6758 | 6767 | 6776 | 6785 | 6794 | 6803 | 1 | 2 | 3 | 4 | 5 |
| 48 | 6812 | 6821 | 6830 | 6839 | 6848 | 6857 | 6866 | 6875 | 6884 | 6893 | 1 | 2 | 3 | 4 | 4 |
| 49 | 6902 | 6911 | 6920 | 6928 | 6937 | 6946 | 6955 | 6964 | 6972 | 6981 | 1 | 2 | 3 | 4 | 4 |
| 50 | 6990 | 6998 | 7007 | 7016 | 7024 | 7033 | 7042 | 7050 | 7059 | 7067 | 1 | 2 | 3 | 3 | 4 |
| 51 | 7076 | 7084 | 7093 | 7101 | 7110 | 7118 | 7126 | 7135 | 7143 | 7152 | 1 | 2 | 3 | 3 | 4 |
| 52 | 7160 | 7168 | 7177 | 7185 | 7193 | 7202 | 7210 | 7218 | 7226 | 7235 | 1 | 2 | 2 | 3 | 4 |
| 53 | 7243 | 7251 | 7259 | 7267 | 7275 | 7284 | 7292 | 7300 | 7308 | 7316 | 1 | 2 | 2 | 3 | 4 |
| 54 | 7324 | 7332 | 7340 | 7348 | 7356 | 7364 | 7372 | 7380 | 7388 | 7396 | 1 | 2 | 2 | 3 | 4 |

LOGARITHMS

| N. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | P. P. | | | | |
|----|------|------|------|------|------|------|------|------|------|------|-------|---|---|---|---|
| | | | | | | | | | | | 1 | 2 | 3 | 4 | 5 |
| 55 | 7404 | 7412 | 7419 | 7427 | 7435 | 7443 | 7451 | 7459 | 7466 | 7474 | 1 | 2 | 2 | 3 | 4 |
| 56 | 7482 | 7490 | 7497 | 7505 | 7513 | 7520 | 7528 | 7536 | 7543 | 7551 | 1 | 2 | 2 | 3 | 4 |
| 57 | 7559 | 7566 | 7574 | 7582 | 7589 | 7597 | 7604 | 7612 | 7619 | 7627 | 1 | 2 | 2 | 3 | 4 |
| 58 | 7634 | 7642 | 7649 | 7657 | 7664 | 7672 | 7679 | 7686 | 7694 | 7701 | 1 | 1 | 2 | 3 | 4 |
| 59 | 7709 | 7716 | 7723 | 7731 | 7738 | 7745 | 7752 | 7760 | 7767 | 7774 | 1 | 1 | 2 | 3 | 4 |
| 60 | 7782 | 7789 | 7796 | 7803 | 7810 | 7818 | 7825 | 7832 | 7839 | 7846 | 1 | 1 | 2 | 3 | 4 |
| 61 | 7853 | 7860 | 7868 | 7875 | 7882 | 7889 | 7896 | 7903 | 7910 | 7917 | 1 | 1 | 2 | 3 | 4 |
| 62 | 7924 | 7931 | 7938 | 7945 | 7952 | 7959 | 7966 | 7973 | 7980 | 7987 | 1 | 1 | 2 | 3 | 3 |
| 63 | 7993 | 8000 | 8007 | 8014 | 8021 | 8028 | 8035 | 8041 | 8048 | 8055 | 1 | 1 | 2 | 3 | 3 |
| 64 | 8062 | 8069 | 8075 | 8082 | 8089 | 8096 | 8102 | 8109 | 8116 | 8122 | 1 | 1 | 2 | 3 | 3 |
| 65 | 8129 | 8136 | 8142 | 8149 | 8156 | 8162 | 8169 | 8176 | 8182 | 8189 | 1 | 1 | 2 | 3 | 3 |
| 66 | 8195 | 8202 | 8209 | 8215 | 8222 | 8228 | 8235 | 8241 | 8248 | 8254 | 1 | 1 | 2 | 3 | 3 |
| 67 | 8261 | 8267 | 8274 | 8280 | 8287 | 8293 | 8299 | 8306 | 8312 | 8319 | 1 | 1 | 2 | 3 | 3 |
| 68 | 8325 | 8331 | 8338 | 8344 | 8351 | 8357 | 8363 | 8370 | 8376 | 8382 | 1 | 1 | 2 | 3 | 3 |
| 69 | 8388 | 8395 | 8401 | 8407 | 8414 | 8420 | 8426 | 8432 | 8439 | 8445 | 1 | 1 | 2 | 3 | 3 |
| 70 | 8451 | 8457 | 8463 | 8470 | 8476 | 8482 | 8488 | 8494 | 8500 | 8506 | 1 | 1 | 2 | 2 | 3 |
| 71 | 8513 | 8519 | 8525 | 8531 | 8537 | 8543 | 8549 | 8555 | 8561 | 8567 | 1 | 1 | 2 | 2 | 3 |
| 72 | 8573 | 8579 | 8585 | 8591 | 8597 | 8603 | 8609 | 8615 | 8621 | 8627 | 1 | 1 | 2 | 2 | 3 |
| 73 | 8633 | 8639 | 8645 | 8651 | 8657 | 8663 | 8669 | 8675 | 8681 | 8686 | 1 | 1 | 2 | 2 | 3 |
| 74 | 8692 | 8698 | 8704 | 8710 | 8716 | 8722 | 8727 | 8733 | 8739 | 8745 | 1 | 1 | 2 | 2 | 3 |
| 75 | 8751 | 8756 | 8762 | 8768 | 8774 | 8779 | 8785 | 8791 | 8797 | 8802 | 1 | 1 | 2 | 2 | 3 |
| 76 | 8808 | 8814 | 8820 | 8825 | 8831 | 8837 | 8842 | 8848 | 8854 | 8859 | 1 | 1 | 2 | 2 | 3 |
| 77 | 8865 | 8871 | 8876 | 8882 | 8887 | 8893 | 8899 | 8904 | 8910 | 8915 | 1 | 1 | 2 | 2 | 3 |
| 78 | 8921 | 8927 | 8932 | 8938 | 8943 | 8949 | 8954 | 8960 | 8965 | 8971 | 1 | 1 | 2 | 2 | 3 |
| 79 | 8976 | 8982 | 8987 | 8993 | 8998 | 9004 | 9009 | 9015 | 9020 | 9025 | 1 | 1 | 2 | 2 | 3 |
| 80 | 9031 | 9036 | 9042 | 9047 | 9053 | 9058 | 9063 | 9069 | 9074 | 9079 | 1 | 1 | 2 | 2 | 3 |
| 81 | 9085 | 9090 | 9096 | 9101 | 9106 | 9112 | 9117 | 9122 | 9128 | 9133 | 1 | 1 | 2 | 2 | 3 |
| 82 | 9138 | 9143 | 9149 | 9154 | 9159 | 9165 | 9170 | 9175 | 9180 | 9186 | 1 | 1 | 2 | 2 | 3 |
| 83 | 9191 | 9196 | 9201 | 9206 | 9212 | 9217 | 9222 | 9227 | 9232 | 9238 | 1 | 1 | 2 | 2 | 3 |
| 84 | 9243 | 9248 | 9253 | 9258 | 9263 | 9269 | 9274 | 9279 | 9284 | 9289 | 1 | 1 | 2 | 2 | 3 |
| 85 | 9294 | 9299 | 9304 | 9309 | 9315 | 9320 | 9325 | 9330 | 9335 | 9340 | 1 | 1 | 2 | 2 | 3 |
| 86 | 9345 | 9350 | 9355 | 9360 | 9365 | 9370 | 9375 | 9380 | 9385 | 9390 | 1 | 1 | 2 | 2 | 3 |
| 87 | 9395 | 9400 | 9405 | 9410 | 9415 | 9420 | 9425 | 9430 | 9435 | 9440 | 0 | 1 | 1 | 2 | 2 |
| 88 | 9445 | 9450 | 9455 | 9460 | 9465 | 9469 | 9474 | 9479 | 9484 | 9489 | 0 | 1 | 1 | 2 | 2 |
| 89 | 9494 | 9499 | 9504 | 9509 | 9513 | 9518 | 9523 | 9528 | 9533 | 9538 | 0 | 1 | 1 | 2 | 2 |
| 90 | 9542 | 9547 | 9552 | 9557 | 9562 | 9566 | 9571 | 9576 | 9581 | 9586 | 0 | 1 | 1 | 2 | 2 |
| 91 | 9590 | 9595 | 9600 | 9605 | 9609 | 9614 | 9619 | 9624 | 9628 | 9633 | 0 | 1 | 1 | 2 | 2 |
| 92 | 9638 | 9643 | 9647 | 9652 | 9657 | 9661 | 9666 | 9671 | 9675 | 9680 | 0 | 1 | 1 | 2 | 2 |
| 93 | 9685 | 9689 | 9694 | 9699 | 9703 | 9708 | 9713 | 9717 | 9722 | 9727 | 0 | 1 | 1 | 2 | 2 |
| 94 | 9731 | 9736 | 9741 | 9745 | 9750 | 9754 | 9759 | 9763 | 9768 | 9773 | 0 | 1 | 1 | 2 | 2 |
| 95 | 9777 | 9782 | 9786 | 9791 | 9795 | 9800 | 9805 | 9809 | 9814 | 9818 | 0 | 1 | 1 | 2 | 2 |
| 96 | 9823 | 9827 | 9832 | 9836 | 9841 | 9845 | 9850 | 9854 | 9859 | 9863 | 0 | 1 | 1 | 2 | 2 |
| 97 | 9868 | 9872 | 9877 | 9881 | 9886 | 9890 | 9894 | 9899 | 9903 | 9908 | 0 | 1 | 1 | 2 | 2 |
| 98 | 9912 | 9917 | 9921 | 9926 | 9930 | 9934 | 9939 | 9943 | 9948 | 9952 | 0 | 1 | 1 | 2 | 2 |
| 99 | 9956 | 9961 | 9965 | 9969 | 9974 | 9978 | 9983 | 9987 | 9991 | 9996 | 0 | 1 | 1 | 2 | 2 |

TABLE 12
ANTILOGARITHMS

| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | P. P. | | | | |
|-----|------|------|------|------|------|------|------|------|------|------|-------|---|---|---|---|
| | | | | | | | | | | | 1 | 2 | 3 | 4 | 5 |
| .00 | 1000 | 1002 | 1005 | 1007 | 1009 | 1012 | 1014 | 1016 | 1019 | 1021 | 0 | 0 | 1 | 1 | 1 |
| .01 | 1023 | 1026 | 1028 | 1030 | 1033 | 1035 | 1038 | 1040 | 1042 | 1045 | 0 | 0 | 1 | 1 | 1 |
| .02 | 1047 | 1050 | 1052 | 1054 | 1057 | 1059 | 1062 | 1064 | 1067 | 1069 | 0 | 0 | 1 | 1 | 1 |
| .03 | 1072 | 1074 | 1076 | 1079 | 1081 | 1084 | 1086 | 1089 | 1091 | 1094 | 0 | 0 | 1 | 1 | 1 |
| .04 | 1096 | 1099 | 1102 | 1104 | 1107 | 1109 | 1112 | 1114 | 1117 | 1119 | 0 | 1 | 1 | 1 | 1 |
| .05 | 1122 | 1125 | 1127 | 1130 | 1132 | 1135 | 1138 | 1140 | 1143 | 1146 | 0 | 1 | 1 | 1 | 1 |
| .06 | 1148 | 1151 | 1153 | 1156 | 1159 | 1161 | 1164 | 1167 | 1169 | 1172 | 0 | 1 | 1 | 1 | 1 |
| .07 | 1175 | 1178 | 1180 | 1183 | 1186 | 1189 | 1191 | 1194 | 1197 | 1199 | 0 | 1 | 1 | 1 | 1 |
| .08 | 1202 | 1205 | 1208 | 1211 | 1213 | 1216 | 1219 | 1222 | 1225 | 1227 | 0 | 1 | 1 | 1 | 1 |
| .09 | 1230 | 1233 | 1236 | 1239 | 1242 | 1245 | 1247 | 1250 | 1253 | 1256 | 0 | 1 | 1 | 1 | 1 |
| .10 | 1259 | 1262 | 1265 | 1268 | 1271 | 1274 | 1276 | 1279 | 1282 | 1285 | 0 | 1 | 1 | 1 | 1 |
| .11 | 1288 | 1291 | 1294 | 1297 | 1300 | 1303 | 1306 | 1309 | 1312 | 1315 | 0 | 1 | 1 | 1 | 2 |
| .12 | 1318 | 1321 | 1324 | 1327 | 1330 | 1334 | 1337 | 1340 | 1343 | 1346 | 0 | 1 | 1 | 1 | 2 |
| .13 | 1349 | 1352 | 1355 | 1358 | 1361 | 1365 | 1368 | 1371 | 1374 | 1377 | 0 | 1 | 1 | 1 | 2 |
| .14 | 1380 | 1384 | 1387 | 1390 | 1393 | 1396 | 1400 | 1403 | 1406 | 1409 | 0 | 1 | 1 | 1 | 2 |
| .15 | 1413 | 1416 | 1419 | 1422 | 1426 | 1429 | 1432 | 1435 | 1439 | 1442 | 0 | 1 | 1 | 1 | 2 |
| .16 | 1445 | 1449 | 1452 | 1455 | 1459 | 1462 | 1466 | 1469 | 1472 | 1476 | 0 | 1 | 1 | 1 | 2 |
| .17 | 1479 | 1483 | 1486 | 1489 | 1493 | 1496 | 1500 | 1503 | 1507 | 1510 | 0 | 1 | 1 | 1 | 2 |
| .18 | 1514 | 1517 | 1521 | 1524 | 1528 | 1531 | 1535 | 1538 | 1542 | 1545 | 0 | 1 | 1 | 1 | 2 |
| .19 | 1549 | 1552 | 1556 | 1560 | 1563 | 1567 | 1570 | 1574 | 1578 | 1581 | 0 | 1 | 1 | 1 | 2 |
| .20 | 1585 | 1589 | 1592 | 1596 | 1600 | 1603 | 1607 | 1611 | 1614 | 1618 | 0 | 1 | 1 | 1 | 2 |
| .21 | 1622 | 1626 | 1629 | 1633 | 1637 | 1641 | 1644 | 1648 | 1652 | 1656 | 0 | 1 | 1 | 1 | 2 |
| .22 | 1660 | 1663 | 1667 | 1671 | 1675 | 1679 | 1683 | 1687 | 1690 | 1694 | 0 | 1 | 1 | 1 | 2 |
| .23 | 1698 | 1702 | 1706 | 1710 | 1714 | 1718 | 1722 | 1726 | 1730 | 1734 | 0 | 1 | 1 | 1 | 2 |
| .24 | 1738 | 1742 | 1746 | 1750 | 1754 | 1758 | 1762 | 1766 | 1770 | 1774 | 0 | 1 | 1 | 1 | 2 |
| .25 | 1778 | 1782 | 1786 | 1791 | 1795 | 1799 | 1803 | 1807 | 1811 | 1816 | 0 | 1 | 1 | 1 | 2 |
| .26 | 1820 | 1824 | 1828 | 1832 | 1837 | 1841 | 1845 | 1849 | 1854 | 1858 | 0 | 1 | 1 | 1 | 2 |
| .27 | 1862 | 1866 | 1871 | 1875 | 1879 | 1884 | 1888 | 1892 | 1897 | 1901 | 0 | 1 | 1 | 1 | 2 |
| .28 | 1905 | 1910 | 1914 | 1919 | 1923 | 1928 | 1932 | 1936 | 1941 | 1945 | 0 | 1 | 1 | 1 | 2 |
| .29 | 1950 | 1954 | 1959 | 1963 | 1968 | 1972 | 1977 | 1982 | 1986 | 1991 | 0 | 1 | 1 | 1 | 2 |
| .30 | 1995 | 2000 | 2004 | 2009 | 2014 | 2018 | 2023 | 2028 | 2032 | 2037 | 0 | 1 | 1 | 1 | 2 |
| .31 | 2042 | 2046 | 2051 | 2056 | 2061 | 2065 | 2070 | 2075 | 2080 | 2084 | 0 | 1 | 1 | 1 | 2 |
| .32 | 2089 | 2094 | 2099 | 2104 | 2109 | 2113 | 2118 | 2123 | 2128 | 2133 | 0 | 1 | 1 | 1 | 2 |
| .33 | 2138 | 2143 | 2148 | 2153 | 2158 | 2163 | 2168 | 2173 | 2178 | 2183 | 0 | 1 | 1 | 1 | 2 |
| .34 | 2188 | 2193 | 2198 | 2203 | 2208 | 2213 | 2218 | 2223 | 2228 | 2234 | 1 | 1 | 1 | 1 | 2 |
| .35 | 2239 | 2244 | 2249 | 2254 | 2259 | 2265 | 2270 | 2275 | 2280 | 2286 | 1 | 1 | 1 | 1 | 2 |
| .36 | 2291 | 2296 | 2301 | 2307 | 2312 | 2317 | 2323 | 2328 | 2333 | 2339 | 1 | 1 | 1 | 1 | 2 |
| .37 | 2344 | 2350 | 2355 | 2360 | 2366 | 2371 | 2377 | 2382 | 2388 | 2393 | 1 | 1 | 1 | 1 | 2 |
| .38 | 2399 | 2404 | 2410 | 2415 | 2421 | 2427 | 2432 | 2438 | 2443 | 2449 | 1 | 1 | 1 | 1 | 2 |
| .39 | 2455 | 2460 | 2466 | 2472 | 2477 | 2483 | 2489 | 2495 | 2500 | 2506 | 1 | 1 | 1 | 1 | 2 |
| .40 | 2512 | 2518 | 2523 | 2529 | 2535 | 2541 | 2547 | 2553 | 2559 | 2564 | 1 | 1 | 1 | 1 | 2 |
| .41 | 2570 | 2576 | 2582 | 2588 | 2594 | 2600 | 2606 | 2612 | 2618 | 2624 | 1 | 1 | 1 | 1 | 2 |
| .42 | 2630 | 2636 | 2642 | 2649 | 2655 | 2661 | 2667 | 2673 | 2679 | 2685 | 1 | 1 | 1 | 1 | 2 |
| .43 | 2692 | 2698 | 2704 | 2710 | 2716 | 2723 | 2729 | 2735 | 2742 | 2748 | 1 | 1 | 1 | 1 | 2 |
| .44 | 2754 | 2761 | 2767 | 2773 | 2780 | 2786 | 2793 | 2799 | 2805 | 2812 | 1 | 1 | 1 | 1 | 2 |
| .45 | 2818 | 2825 | 2831 | 2838 | 2844 | 2851 | 2858 | 2864 | 2871 | 2877 | 1 | 1 | 1 | 1 | 2 |
| .46 | 2884 | 2891 | 2897 | 2904 | 2911 | 2917 | 2924 | 2931 | 2938 | 2944 | 1 | 1 | 1 | 1 | 2 |
| .47 | 2951 | 2958 | 2965 | 2972 | 2979 | 2985 | 2992 | 2999 | 3006 | 3013 | 1 | 1 | 1 | 1 | 2 |
| .48 | 3020 | 3027 | 3034 | 3041 | 3048 | 3055 | 3062 | 3069 | 3076 | 3083 | 1 | 1 | 1 | 1 | 2 |
| .49 | 3090 | 3097 | 3105 | 3112 | 3119 | 3126 | 3133 | 3141 | 3148 | 3155 | 1 | 1 | 1 | 1 | 2 |

ANTILOGARITHMS

| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | P. P. | | | | |
|-----|------|------|------|------|------|------|------|------|------|------|-------|---|---|---|----|
| | | | | | | | | | | | 1 | 2 | 3 | 4 | 5 |
| .50 | 3162 | 3170 | 3177 | 3184 | 3192 | 3199 | 3206 | 3214 | 3221 | 3228 | 1 | 1 | 2 | 3 | 4 |
| .51 | 3236 | 3243 | 3251 | 3258 | 3266 | 3273 | 3281 | 3289 | 3296 | 3304 | 1 | 2 | 2 | 3 | 4 |
| .52 | 3311 | 3319 | 3327 | 3334 | 3342 | 3350 | 3357 | 3365 | 3373 | 3381 | 1 | 2 | 2 | 3 | 4 |
| .53 | 3388 | 3396 | 3404 | 3412 | 3420 | 3428 | 3436 | 3443 | 3451 | 3459 | 1 | 2 | 2 | 3 | 4 |
| .54 | 3467 | 3475 | 3483 | 3491 | 3499 | 3508 | 3516 | 3524 | 3532 | 3540 | 1 | 2 | 2 | 3 | 4 |
| .55 | 3548 | 3556 | 3565 | 3573 | 3581 | 3589 | 3597 | 3606 | 3614 | 3622 | 1 | 2 | 2 | 3 | 4 |
| .56 | 3631 | 3639 | 3648 | 3656 | 3664 | 3673 | 3681 | 3690 | 3698 | 3707 | 1 | 2 | 3 | 3 | 4 |
| .57 | 3715 | 3724 | 3733 | 3741 | 3750 | 3758 | 3767 | 3776 | 3784 | 3793 | 1 | 2 | 3 | 3 | 4 |
| .58 | 3802 | 3811 | 3819 | 3828 | 3837 | 3846 | 3855 | 3864 | 3873 | 3882 | 1 | 2 | 3 | 4 | 4 |
| .59 | 3890 | 3899 | 3908 | 3917 | 3926 | 3936 | 3945 | 3954 | 3963 | 3972 | 1 | 2 | 3 | 4 | 5 |
| .60 | 3981 | 3990 | 3999 | 4009 | 4018 | 4027 | 4036 | 4046 | 4055 | 4064 | 1 | 2 | 3 | 4 | 5 |
| .61 | 4074 | 4083 | 4093 | 4102 | 4111 | 4121 | 4130 | 4140 | 4150 | 4159 | 1 | 2 | 3 | 4 | 5 |
| .62 | 4169 | 4178 | 4188 | 4198 | 4207 | 4217 | 4227 | 4236 | 4246 | 4256 | 1 | 2 | 3 | 4 | 5 |
| .63 | 4266 | 4276 | 4285 | 4295 | 4305 | 4315 | 4325 | 4335 | 4345 | 4355 | 1 | 2 | 3 | 4 | 5 |
| .64 | 4365 | 4375 | 4385 | 4395 | 4406 | 4416 | 4426 | 4436 | 4446 | 4457 | 1 | 2 | 3 | 4 | 5 |
| .65 | 4467 | 4477 | 4487 | 4498 | 4508 | 4519 | 4529 | 4539 | 4550 | 4560 | 1 | 2 | 3 | 4 | 5 |
| .66 | 4571 | 4581 | 4592 | 4603 | 4613 | 4624 | 4634 | 4645 | 4656 | 4667 | 1 | 2 | 3 | 4 | 5 |
| .67 | 4677 | 4688 | 4699 | 4710 | 4721 | 4732 | 4742 | 4753 | 4764 | 4775 | 1 | 2 | 3 | 4 | 5 |
| .68 | 4786 | 4797 | 4808 | 4819 | 4831 | 4842 | 4853 | 4864 | 4875 | 4887 | 1 | 2 | 3 | 4 | 6 |
| .69 | 4898 | 4909 | 4920 | 4932 | 4943 | 4955 | 4966 | 4977 | 4989 | 5000 | 1 | 2 | 3 | 5 | 6 |
| .70 | 5012 | 5023 | 5035 | 5047 | 5058 | 5070 | 5082 | 5093 | 5105 | 5117 | 1 | 2 | 4 | 5 | 6 |
| .71 | 5129 | 5140 | 5152 | 5164 | 5176 | 5188 | 5200 | 5212 | 5224 | 5236 | 1 | 2 | 4 | 5 | 6 |
| .72 | 5248 | 5260 | 5272 | 5284 | 5297 | 5309 | 5321 | 5333 | 5346 | 5358 | 1 | 2 | 4 | 5 | 6 |
| .73 | 5370 | 5383 | 5395 | 5408 | 5420 | 5433 | 5445 | 5458 | 5470 | 5483 | 1 | 3 | 4 | 5 | 6 |
| .74 | 5495 | 5508 | 5521 | 5534 | 5546 | 5559 | 5572 | 5585 | 5598 | 5610 | 1 | 3 | 4 | 5 | 6 |
| .75 | 5623 | 5636 | 5649 | 5662 | 5675 | 5689 | 5702 | 5715 | 5728 | 5741 | 1 | 3 | 4 | 5 | 7 |
| .76 | 5754 | 5768 | 5781 | 5794 | 5808 | 5821 | 5834 | 5848 | 5861 | 5875 | 1 | 3 | 4 | 5 | 7 |
| .77 | 5888 | 5902 | 5916 | 5929 | 5943 | 5957 | 5970 | 5984 | 5998 | 6012 | 1 | 3 | 4 | 5 | 7 |
| .78 | 6026 | 6039 | 6053 | 6067 | 6081 | 6095 | 6109 | 6124 | 6138 | 6152 | 1 | 3 | 4 | 6 | 7 |
| .79 | 6166 | 6180 | 6194 | 6209 | 6223 | 6237 | 6252 | 6266 | 6281 | 6295 | 1 | 3 | 4 | 6 | 7 |
| .80 | 6310 | 6324 | 6339 | 6353 | 6368 | 6383 | 6397 | 6412 | 6427 | 6442 | 1 | 3 | 4 | 6 | 7 |
| .81 | 6457 | 6471 | 6486 | 6501 | 6516 | 6531 | 6546 | 6561 | 6577 | 6592 | 2 | 3 | 5 | 6 | 8 |
| .82 | 6607 | 6622 | 6637 | 6653 | 6668 | 6683 | 6699 | 6714 | 6730 | 6745 | 2 | 3 | 5 | 6 | 8 |
| .83 | 6761 | 6776 | 6792 | 6808 | 6823 | 6839 | 6855 | 6871 | 6887 | 6902 | 2 | 3 | 5 | 6 | 8 |
| .84 | 6918 | 6934 | 6950 | 6966 | 6982 | 6998 | 7015 | 7031 | 7047 | 7063 | 2 | 3 | 5 | 6 | 8 |
| .85 | 7079 | 7096 | 7112 | 7129 | 7145 | 7161 | 7178 | 7194 | 7211 | 7228 | 2 | 3 | 5 | 7 | 8 |
| .86 | 7244 | 7261 | 7278 | 7295 | 7311 | 7328 | 7345 | 7362 | 7379 | 7396 | 2 | 3 | 5 | 7 | 8 |
| .87 | 7413 | 7430 | 7447 | 7464 | 7482 | 7499 | 7516 | 7534 | 7551 | 7568 | 2 | 3 | 5 | 7 | 9 |
| .88 | 7586 | 7603 | 7621 | 7638 | 7656 | 7674 | 7691 | 7709 | 7727 | 7745 | 2 | 4 | 5 | 7 | 9 |
| .89 | 7762 | 7780 | 7798 | 7816 | 7834 | 7852 | 7870 | 7889 | 7907 | 7925 | 2 | 4 | 5 | 7 | 9 |
| .90 | 7943 | 7962 | 7980 | 7998 | 8017 | 8035 | 8054 | 8072 | 8091 | 8110 | 2 | 4 | 6 | 7 | 9 |
| .91 | 8128 | 8147 | 8166 | 8185 | 8204 | 8222 | 8241 | 8260 | 8279 | 8299 | 2 | 4 | 6 | 8 | 9 |
| .92 | 8318 | 8337 | 8356 | 8375 | 8395 | 8414 | 8433 | 8453 | 8472 | 8492 | 2 | 4 | 6 | 8 | 10 |
| .93 | 8511 | 8531 | 8551 | 8570 | 8590 | 8610 | 8630 | 8650 | 8670 | 8690 | 2 | 4 | 6 | 8 | 10 |
| .94 | 8710 | 8730 | 8750 | 8770 | 8790 | 8810 | 8831 | 8851 | 8872 | 8892 | 2 | 4 | 6 | 8 | 10 |
| .95 | 8913 | 8933 | 8954 | 8974 | 8995 | 9016 | 9036 | 9057 | 9078 | 9099 | 2 | 4 | 6 | 8 | 10 |
| .96 | 9120 | 9141 | 9162 | 9183 | 9204 | 9226 | 9247 | 9268 | 9290 | 9311 | 2 | 4 | 6 | 8 | 11 |
| .97 | 9333 | 9354 | 9376 | 9397 | 9419 | 9441 | 9462 | 9484 | 9506 | 9528 | 2 | 4 | 7 | 9 | 11 |
| .98 | 9550 | 9572 | 9594 | 9616 | 9638 | 9661 | 9683 | 9705 | 9727 | 9750 | 2 | 4 | 7 | 9 | 11 |
| .99 | 9772 | 9795 | 9817 | 9840 | 9863 | 9886 | 9908 | 9931 | 9954 | 9977 | 2 | 5 | 7 | 9 | 11 |

TABLE 13
ANTILOGARITHMS

| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|-------------|------|------|------|------|------|------|------|------|------|------|------|
| .900 | 7943 | 7945 | 7947 | 7949 | 7951 | 7952 | 7954 | 7956 | 7958 | 7960 | 7962 |
| .901 | 7962 | 7963 | 7965 | 7967 | 7969 | 7971 | 7973 | 7974 | 7976 | 7978 | 7980 |
| .902 | 7980 | 7982 | 7984 | 7985 | 7987 | 7989 | 7991 | 7993 | 7995 | 7997 | 7998 |
| .903 | 7998 | 8000 | 8002 | 8004 | 8006 | 8008 | 8009 | 8011 | 8013 | 8015 | 8017 |
| .904 | 8017 | 8019 | 8020 | 8022 | 8024 | 8026 | 8028 | 8030 | 8032 | 8033 | 8035 |
| .905 | 8035 | 8037 | 8039 | 8041 | 8043 | 8045 | 8046 | 8048 | 8050 | 8052 | 8054 |
| .906 | 8054 | 8056 | 8057 | 8059 | 8061 | 8063 | 8065 | 8067 | 8069 | 8070 | 8072 |
| .907 | 8072 | 8074 | 8076 | 8078 | 8080 | 8082 | 8084 | 8085 | 8087 | 8089 | 8091 |
| .908 | 8091 | 8093 | 8095 | 8097 | 8098 | 8100 | 8102 | 8104 | 8106 | 8108 | 8110 |
| .909 | 8110 | 8111 | 8113 | 8115 | 8117 | 8119 | 8121 | 8123 | 8125 | 8126 | 8128 |
| .910 | 8128 | 8130 | 8132 | 8134 | 8136 | 8138 | 8140 | 8141 | 8143 | 8145 | 8147 |
| .911 | 8147 | 8149 | 8151 | 8153 | 8155 | 8156 | 8158 | 8160 | 8162 | 8164 | 8166 |
| .912 | 8166 | 8168 | 8170 | 8171 | 8173 | 8175 | 8177 | 8179 | 8181 | 8183 | 8185 |
| .913 | 8185 | 8187 | 8188 | 8190 | 8192 | 8194 | 8196 | 8198 | 8200 | 8202 | 8204 |
| .914 | 8204 | 8205 | 8207 | 8209 | 8211 | 8213 | 8215 | 8217 | 8219 | 8221 | 8222 |
| .915 | 8222 | 8224 | 8226 | 8228 | 8230 | 8232 | 8234 | 8236 | 8238 | 8239 | 8241 |
| .916 | 8241 | 8243 | 8245 | 8247 | 8249 | 8251 | 8253 | 8255 | 8257 | 8258 | 8260 |
| .917 | 8260 | 8262 | 8264 | 8266 | 8268 | 8270 | 8272 | 8274 | 8276 | 8278 | 8279 |
| .918 | 8279 | 8281 | 8283 | 8285 | 8287 | 8289 | 8291 | 8293 | 8295 | 8297 | 8299 |
| .919 | 8299 | 8300 | 8302 | 8304 | 8306 | 8308 | 8310 | 8312 | 8314 | 8316 | 8318 |
| .920 | 8318 | 8320 | 8321 | 8323 | 8325 | 8327 | 8329 | 8331 | 8333 | 8335 | 8337 |
| .921 | 8337 | 8339 | 8341 | 8343 | 8344 | 8346 | 8348 | 8350 | 8352 | 8354 | 8356 |
| .922 | 8356 | 8358 | 8360 | 8362 | 8364 | 8366 | 8368 | 8370 | 8371 | 8373 | 8375 |
| .923 | 8375 | 8377 | 8379 | 8381 | 8383 | 8385 | 8387 | 8389 | 8391 | 8393 | 8395 |
| .924 | 8395 | 8397 | 8398 | 8400 | 8402 | 8404 | 8406 | 8408 | 8410 | 8412 | 8414 |
| .925 | 8414 | 8416 | 8418 | 8420 | 8422 | 8424 | 8426 | 8428 | 8429 | 8431 | 8433 |
| .926 | 8433 | 8435 | 8437 | 8439 | 8441 | 8443 | 8445 | 8447 | 8449 | 8451 | 8453 |
| .927 | 8453 | 8455 | 8457 | 8459 | 8461 | 8463 | 8464 | 8466 | 8468 | 8470 | 8472 |
| .928 | 8472 | 8474 | 8476 | 8478 | 8480 | 8482 | 8484 | 8486 | 8488 | 8490 | 8492 |
| .929 | 8492 | 8494 | 8496 | 8498 | 8500 | 8502 | 8504 | 8506 | 8507 | 8509 | 8511 |
| .930 | 8511 | 8513 | 8515 | 8517 | 8519 | 8521 | 8523 | 8525 | 8527 | 8529 | 8531 |
| .931 | 8531 | 8533 | 8535 | 8537 | 8539 | 8541 | 8543 | 8545 | 8547 | 8549 | 8551 |
| .932 | 8551 | 8553 | 8555 | 8557 | 8559 | 8561 | 8562 | 8564 | 8566 | 8568 | 8570 |
| .933 | 8570 | 8572 | 8574 | 8576 | 8578 | 8580 | 8582 | 8584 | 8586 | 8588 | 8590 |
| .934 | 8590 | 8592 | 8594 | 8596 | 8598 | 8600 | 8602 | 8604 | 8606 | 8608 | 8610 |
| .935 | 8610 | 8612 | 8614 | 8616 | 8618 | 8620 | 8622 | 8624 | 8626 | 8628 | 8630 |
| .936 | 8630 | 8632 | 8634 | 8636 | 8638 | 8640 | 8642 | 8644 | 8646 | 8648 | 8650 |
| .937 | 8650 | 8652 | 8654 | 8656 | 8658 | 8660 | 8662 | 8664 | 8666 | 8668 | 8670 |
| .938 | 8670 | 8672 | 8674 | 8676 | 8678 | 8680 | 8682 | 8684 | 8686 | 8688 | 8690 |
| .939 | 8690 | 8692 | 8694 | 8696 | 8698 | 8700 | 8702 | 8704 | 8706 | 8708 | 8710 |
| .940 | 8710 | 8712 | 8714 | 8716 | 8718 | 8720 | 8722 | 8724 | 8726 | 8728 | 8730 |
| .941 | 8730 | 8732 | 8734 | 8736 | 8738 | 8740 | 8742 | 8744 | 8746 | 8748 | 8750 |
| .942 | 8750 | 8752 | 8754 | 8756 | 8758 | 8760 | 8762 | 8764 | 8766 | 8768 | 8770 |
| .943 | 8770 | 8772 | 8774 | 8776 | 8778 | 8780 | 8782 | 8784 | 8786 | 8788 | 8790 |
| .944 | 8790 | 8792 | 8794 | 8796 | 8798 | 8800 | 8802 | 8804 | 8806 | 8808 | 8810 |
| .945 | 8810 | 8813 | 8815 | 8817 | 8819 | 8821 | 8823 | 8825 | 8827 | 8829 | 8831 |
| .946 | 8831 | 8833 | 8835 | 8837 | 8839 | 8841 | 8843 | 8845 | 8847 | 8849 | 8851 |
| .947 | 8851 | 8853 | 8855 | 8857 | 8859 | 8861 | 8863 | 8865 | 8867 | 8870 | 8872 |
| .948 | 8872 | 8874 | 8876 | 8878 | 8880 | 8882 | 8884 | 8886 | 8888 | 8890 | 8892 |
| .949 | 8892 | 8894 | 8896 | 8898 | 8900 | 8902 | 8904 | 8906 | 8908 | 8910 | 8913 |

ANTILOGARITHMS

| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|-------------|------|------|------|------|------|------|------|------|------|------|------|
| .950 | 8913 | 8915 | 8917 | 8919 | 8921 | 8923 | 8925 | 8927 | 8929 | 8931 | 8933 |
| .951 | 8933 | 8935 | 8937 | 8939 | 8941 | 8943 | 8945 | 8947 | 8950 | 8952 | 8954 |
| .952 | 8954 | 8956 | 8958 | 8960 | 8962 | 8964 | 8966 | 8968 | 8970 | 8972 | 8974 |
| .953 | 8974 | 8976 | 8978 | 8980 | 8983 | 8985 | 8987 | 8989 | 8991 | 8993 | 8995 |
| .954 | 8995 | 8997 | 8999 | 9001 | 9003 | 9005 | 9007 | 9009 | 9012 | 9014 | 9016 |
| .955 | 9016 | 9018 | 9020 | 9022 | 9024 | 9026 | 9028 | 9030 | 9032 | 9034 | 9036 |
| .956 | 9036 | 9039 | 9041 | 9043 | 9045 | 9047 | 9049 | 9051 | 9053 | 9055 | 9057 |
| .957 | 9057 | 9059 | 9061 | 9064 | 9066 | 9068 | 9070 | 9072 | 9074 | 9076 | 9078 |
| .958 | 9078 | 9080 | 9082 | 9084 | 9087 | 9089 | 9091 | 9093 | 9095 | 9097 | 9099 |
| .959 | 9099 | 9101 | 9103 | 9105 | 9108 | 9110 | 9112 | 9114 | 9116 | 9118 | 9120 |
| .960 | 9120 | 9122 | 9124 | 9126 | 9129 | 9131 | 9133 | 9135 | 9137 | 9139 | 9141 |
| .961 | 9141 | 9143 | 9145 | 9147 | 9150 | 9152 | 9154 | 9156 | 9158 | 9160 | 9162 |
| .962 | 9162 | 9164 | 9166 | 9169 | 9171 | 9173 | 9175 | 9177 | 9179 | 9181 | 9183 |
| .963 | 9183 | 9185 | 9188 | 9190 | 9192 | 9194 | 9196 | 9198 | 9200 | 9202 | 9204 |
| .964 | 9204 | 9207 | 9209 | 9211 | 9213 | 9215 | 9217 | 9219 | 9221 | 9224 | 9226 |
| .965 | 9226 | 9228 | 9230 | 9232 | 9234 | 9236 | 9238 | 9241 | 9243 | 9245 | 9247 |
| .966 | 9247 | 9249 | 9251 | 9253 | 9256 | 9258 | 9260 | 9262 | 9264 | 9266 | 9268 |
| .967 | 9268 | 9270 | 9273 | 9275 | 9277 | 9279 | 9281 | 9283 | 9285 | 9288 | 9290 |
| .968 | 9290 | 9292 | 9294 | 9296 | 9298 | 9300 | 9303 | 9305 | 9307 | 9309 | 9311 |
| .969 | 9311 | 9313 | 9315 | 9318 | 9320 | 9322 | 9324 | 9326 | 9328 | 9330 | 9333 |
| .970 | 9333 | 9335 | 9337 | 9339 | 9341 | 9343 | 9345 | 9348 | 9350 | 9352 | 9354 |
| .971 | 9354 | 9356 | 9358 | 9361 | 9363 | 9365 | 9367 | 9369 | 9371 | 9373 | 9376 |
| .972 | 9376 | 9378 | 9380 | 9382 | 9384 | 9386 | 9389 | 9391 | 9393 | 9395 | 9397 |
| .973 | 9397 | 9399 | 9402 | 9404 | 9406 | 9408 | 9410 | 9412 | 9415 | 9417 | 9419 |
| .974 | 9419 | 9421 | 9423 | 9425 | 9428 | 9430 | 9432 | 9434 | 9436 | 9438 | 9441 |
| .975 | 9441 | 9443 | 9445 | 9447 | 9449 | 9451 | 9454 | 9456 | 9458 | 9460 | 9462 |
| .976 | 9462 | 9465 | 9467 | 9469 | 9471 | 9473 | 9475 | 9478 | 9480 | 9482 | 9484 |
| .977 | 9484 | 9486 | 9489 | 9491 | 9493 | 9495 | 9497 | 9499 | 9502 | 9504 | 9506 |
| .978 | 9506 | 9508 | 9510 | 9513 | 9515 | 9517 | 9519 | 9521 | 9524 | 9526 | 9528 |
| .979 | 9528 | 9530 | 9532 | 9535 | 9537 | 9539 | 9541 | 9543 | 9546 | 9548 | 9550 |
| .980 | 9550 | 9552 | 9554 | 9557 | 9559 | 9561 | 9563 | 9565 | 9568 | 9570 | 9572 |
| .981 | 9572 | 9574 | 9576 | 9579 | 9581 | 9583 | 9585 | 9587 | 9590 | 9592 | 9594 |
| .982 | 9594 | 9596 | 9598 | 9601 | 9603 | 9605 | 9607 | 9609 | 9612 | 9614 | 9616 |
| .983 | 9616 | 9618 | 9621 | 9623 | 9625 | 9627 | 9629 | 9632 | 9634 | 9636 | 9638 |
| .984 | 9638 | 9641 | 9643 | 9645 | 9647 | 9649 | 9652 | 9654 | 9656 | 9658 | 9661 |
| .985 | 9661 | 9663 | 9665 | 9667 | 9669 | 9672 | 9674 | 9676 | 9678 | 9681 | 9683 |
| .986 | 9683 | 9685 | 9687 | 9689 | 9692 | 9694 | 9696 | 9698 | 9701 | 9703 | 9705 |
| .987 | 9705 | 9707 | 9710 | 9712 | 9714 | 9716 | 9719 | 9721 | 9723 | 9725 | 9727 |
| .988 | 9727 | 9730 | 9732 | 9734 | 9736 | 9739 | 9741 | 9743 | 9745 | 9748 | 9750 |
| .989 | 9750 | 9752 | 9754 | 9757 | 9759 | 9761 | 9763 | 9766 | 9768 | 9770 | 9772 |
| .990 | 9772 | 9775 | 9777 | 9779 | 9781 | 9784 | 9786 | 9788 | 9790 | 9793 | 9795 |
| .991 | 9795 | 9797 | 9799 | 9802 | 9804 | 9806 | 9808 | 9811 | 9813 | 9815 | 9817 |
| .992 | 9817 | 9820 | 9822 | 9824 | 9827 | 9829 | 9831 | 9833 | 9836 | 9838 | 9840 |
| .993 | 9840 | 9842 | 9845 | 9847 | 9849 | 9851 | 9854 | 9856 | 9858 | 9861 | 9863 |
| .994 | 9863 | 9865 | 9867 | 9870 | 9872 | 9874 | 9876 | 9879 | 9881 | 9883 | 9886 |
| .995 | 9886 | 9888 | 9890 | 9892 | 9895 | 9897 | 9899 | 9901 | 9904 | 9906 | 9908 |
| .996 | 9908 | 9911 | 9913 | 9915 | 9917 | 9920 | 9922 | 9924 | 9927 | 9929 | 9931 |
| .997 | 9931 | 9933 | 9936 | 9938 | 9940 | 9943 | 9945 | 9947 | 9949 | 9952 | 9954 |
| .998 | 9954 | 9956 | 9959 | 9961 | 9963 | 9966 | 9968 | 9970 | 9972 | 9975 | 9977 |
| .999 | 9977 | 9979 | 9982 | 9984 | 9986 | 9988 | 9991 | 9993 | 9995 | 9998 | 0000 |

CIRCULAR (TRIGONOMETRIC) FUNCTIONS

(Taken from B. O. Peirce's "Short Table of Integrals," Ginn & Co.)

| RADIAN- S. | DE- GREES. | SINES. | | COSINES. | | TANGENTS. | | COTANGENTS. | | | |
|---------------|---------------|----------|--------|----------|--------|------------------|--------|-------------|--------|---------------|---------------|
| | | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | | |
| 0.0000 | 0°00' | .0000 | ∞ | 1.0000 | 0.0000 | .0000 | ∞ | ∞ | ∞ | 90°00' | 1.5708 |
| 0.0029 | 10 | .0029 | 7.4637 | 1.0000 | .0000 | .0029 | 7.4637 | 343.77 | 2.5363 | 50 | 1.5679 |
| 0.0058 | 20 | .0058 | .7648 | 1.0000 | .0000 | .0058 | .7648 | 171.89 | .2352 | 40 | 1.5650 |
| 0.0087 | 30 | .0087 | .9408 | 1.0000 | .0000 | .0087 | .9409 | 114.59 | .0591 | 30 | 1.5621 |
| 0.0116 | 40 | .0116 | 8.0658 | .9999 | .0000 | .0116 | 8.0658 | 85.940 | 1.9342 | 20 | 1.5592 |
| 0.0145 | 50 | .0145 | .1627 | .9999 | .0000 | .0145 | .1627 | 68.750 | .8373 | 10 | 1.5563 |
| 0.0175 | 1°00' | .0175 | 8.2419 | .9998 | 9.9999 | .0175 | 8.2419 | 57.290 | 1.7581 | 89°00' | 1.5533 |
| 0.0204 | 10 | .0204 | .3088 | .9998 | .9999 | .0204 | .3089 | 49.104 | .6911 | 50 | 1.5504 |
| 0.0233 | 20 | .0233 | .3668 | .9997 | .9999 | .0233 | .3669 | 42.964 | .6331 | 40 | 1.5475 |
| 0.0262 | 30 | .0262 | .4179 | .9997 | .9999 | .0262 | .4181 | 38.188 | .5819 | 30 | 1.5446 |
| 0.0291 | 40 | .0291 | .4637 | .9996 | .9998 | .0291 | .4638 | 34.368 | .5362 | 20 | 1.5417 |
| 0.0320 | 50 | .0320 | .5050 | .9995 | .9998 | .0320 | .5053 | 31.242 | .4947 | 10 | 1.5388 |
| 0.0349 | 2°00' | .0349 | 8.5428 | .9994 | 9.9997 | .0349 | 8.5431 | 28.636 | 1.4569 | 88°00' | 1.5359 |
| 0.0378 | 10 | .0378 | .5776 | .9993 | .9997 | .0378 | .5779 | 26.432 | .4221 | 50 | 1.5330 |
| 0.0407 | 20 | .0407 | .6097 | .9992 | .9996 | .0407 | .6101 | 24.542 | .3899 | 40 | 1.5301 |
| 0.0436 | 30 | .0436 | .6397 | .9990 | .9996 | .0437 | .6401 | 22.904 | .3599 | 30 | 1.5272 |
| 0.0465 | 40 | .0465 | .6677 | .9989 | .9995 | .0466 | .6682 | 21.470 | .3318 | 20 | 1.5243 |
| 0.0495 | 50 | .0494 | .6940 | .9988 | .9995 | .0495 | .6945 | 20.206 | .3055 | 10 | 1.5213 |
| 0.0524 | 3°00' | .0523 | 8.7188 | .9986 | 9.9994 | .0524 | 8.7194 | 19.081 | 1.2806 | 87°00' | 1.5184 |
| 0.0553 | 10 | .0552 | .7423 | .9985 | .9993 | .0553 | .7429 | 18.075 | .2571 | 50 | 1.5155 |
| 0.0582 | 20 | .0581 | .7645 | .9983 | .9993 | .0582 | .7652 | 17.169 | .2348 | 40 | 1.5126 |
| 0.0611 | 30 | .0610 | .7857 | .9981 | .9992 | .0612 | .7865 | 16.350 | .2135 | 30 | 1.5097 |
| 0.0640 | 40 | .0640 | .8059 | .9980 | .9991 | .0641 | .8067 | 15.605 | .1933 | 20 | 1.5068 |
| 0.0669 | 50 | .0669 | .8251 | .9978 | .9990 | .0670 | .8261 | 14.924 | .1739 | 10 | 1.5039 |
| 0.0698 | 4°00' | .0698 | 8.8436 | .9976 | 9.9989 | .0699 | 8.8446 | 14.301 | 1.1554 | 86°00' | 1.5010 |
| 0.0727 | 10 | .0727 | .8613 | .9974 | .9989 | .0729 | .8624 | 13.727 | .1376 | 50 | 1.4981 |
| 0.0756 | 20 | .0756 | .8783 | .9971 | .9988 | .0758 | .8795 | 13.197 | .1205 | 40 | 1.4952 |
| 0.0785 | 30 | .0785 | .8946 | .9969 | .9987 | .0787 | .8960 | 12.706 | .1040 | 30 | 1.4923 |
| 0.0814 | 40 | .0814 | .9104 | .9967 | .9986 | .0816 | .9118 | 12.251 | .0882 | 20 | 1.4893 |
| 0.0844 | 50 | .0843 | .9256 | .9964 | .9985 | .0846 | .9272 | 11.826 | .0728 | 10 | 1.4864 |
| 0.0873 | 5°00' | .0872 | 8.9403 | .9962 | 9.9983 | .0875 | 8.9420 | 11.430 | 1.0580 | 85°00' | 1.4835 |
| 0.0902 | 10 | .0901 | .9545 | .9959 | .9982 | .0904 | .9563 | 11.059 | .0437 | 50 | 1.4806 |
| 0.0931 | 20 | .0929 | .9682 | .9957 | .9981 | .0934 | .9701 | 10.712 | .0299 | 40 | 1.4777 |
| 0.0960 | 30 | .0958 | .9816 | .9954 | .9980 | .0963 | .9836 | 10.385 | .0164 | 30 | 1.4748 |
| 0.0989 | 40 | .0987 | .9945 | .9951 | .9979 | .0992 | .9966 | 10.078 | .0034 | 20 | 1.4719 |
| 0.1018 | 50 | .1016 | 9.0070 | .9948 | .9977 | .1022 | 9.0093 | 9.7882 | 0.9907 | 10 | 1.4690 |
| 0.1047 | 6°00' | .1045 | 9.0192 | .9945 | 9.9976 | .1051 | 9.0216 | 9.5144 | 0.9784 | 84°00' | 1.4661 |
| 0.1076 | 10 | .1074 | .0311 | .9942 | .9975 | .1080 | .0336 | 9.2553 | .9664 | 50 | 1.4632 |
| 0.1105 | 20 | .1103 | .0426 | .9939 | .9973 | .1110 | .0453 | 9.0098 | .9547 | 40 | 1.4603 |
| 0.1134 | 30 | .1132 | .0539 | .9936 | .9972 | .1139 | .0567 | 8.7769 | .9433 | 30 | 1.4574 |
| 0.1164 | 40 | .1161 | .0648 | .9932 | .9971 | .1169 | .0678 | 8.5555 | .9322 | 20 | 1.4544 |
| 0.1193 | 50 | .1190 | .0755 | .9929 | .9969 | .1198 | .0786 | 8.3450 | .9214 | 10 | 1.4515 |
| 0.1222 | 7°00' | .1219 | 9.0859 | .9925 | 9.9968 | .1228 | 9.0891 | 8.1443 | 0.9109 | 83°00' | 1.4486 |
| 0.1251 | 10 | .1248 | .0961 | .9922 | .9966 | .1257 | .0995 | 7.9530 | .9005 | 50 | 1.4457 |
| 0.1280 | 20 | .1276 | .1060 | .9918 | .9964 | .1287 | .1096 | 7.7704 | .8904 | 40 | 1.4428 |
| 0.1309 | 30 | .1305 | .1157 | .9914 | .9963 | .1317 | .1194 | 7.5958 | .8806 | 30 | 1.4399 |
| 0.1338 | 40 | .1334 | .1252 | .9911 | .9961 | .1346 | .1291 | 7.4287 | .8709 | 20 | 1.4370 |
| 0.1367 | 50 | .1363 | .1345 | .9907 | .9959 | .1376 | .1385 | 7.2687 | .8615 | 10 | 1.4341 |
| 0.1396 | 8°00' | .1392 | 9.1436 | .9903 | 9.9958 | .1405 | 9.1478 | 7.1154 | 0.8522 | 82°00' | 1.4312 |
| 0.1425 | 10 | .1421 | .1525 | .9899 | .9956 | .1435 | .1560 | 6.9682 | .8431 | 50 | 1.4283 |
| 0.1454 | 20 | .1449 | .1612 | .9894 | .9954 | .1465 | .1658 | 6.8269 | .8342 | 40 | 1.4254 |
| 0.1483 | 30 | .1478 | .1697 | .9890 | .9952 | .1495 | .1745 | 6.6912 | .8255 | 30 | 1.4224 |
| 0.1513 | 40 | .1507 | .1781 | .9886 | .9950 | .1524 | .1831 | 6.5606 | .8169 | 20 | 1.4195 |
| 0.1542 | 50 | .1536 | .1863 | .9881 | .9948 | .1554 | .1915 | 6.4348 | .8085 | 10 | 1.4166 |
| 0.1571 | 9°00' | .1564 | 9.1943 | .9877 | 9.9946 | .1584 | 9.1997 | 6.3138 | 0.8003 | 81°00' | 1.4137 |
| | | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | DE- GREES. | RADI- ANS. |
| | | COSINES. | | SINES. | | COTAN- GENTS. | | TANGENTS. | | | |

CIRCULAR (TRIGONOMETRIC) FUNCTIONS

| RADIAN- S. | DE- GREES. | SINES. | | COSINES. | | TANGENTS. | | COTANGENTS. | | | |
|---------------|---------------|----------|--------|----------|--------|------------------|--------|-------------|--------|---------------|---------------|
| | | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | | |
| 0.1571 | 9°00' | .1564 | 9.1943 | .9877 | 9.9946 | .1584 | 9.1997 | 6.3138 | 0.8003 | 81°00' | 1.4137 |
| 0.1600 | 10 | .1593 | .2022 | .9872 | .9944 | .1614 | .2078 | 6.1970 | .7922 | 50 | 1.4108 |
| 0.1629 | 20 | .1622 | .2100 | .9868 | .9942 | .1644 | .2158 | 6.0844 | .7842 | 40 | 1.4079 |
| 0.1658 | 30 | .1650 | .2176 | .9863 | .9940 | .1673 | .2236 | 5.9758 | .7764 | 30 | 1.4050 |
| 0.1687 | 40 | .1679 | .2251 | .9858 | .9938 | .1703 | .2313 | 5.8708 | .7687 | 20 | 1.4021 |
| 0.1716 | 50 | .1708 | .2324 | .9853 | .9936 | .1733 | .2389 | 5.7694 | .7611 | 10 | 1.3992 |
| 0.1745 | 10°00' | .1736 | 9.2397 | .9848 | 9.9934 | .1763 | 9.2463 | 5.6713 | 0.7537 | 80°00' | 1.3963 |
| 0.1774 | 10 | .1765 | .2468 | .9843 | .9931 | .1793 | .2536 | 5.5764 | .7464 | 50 | 1.3934 |
| 0.1804 | 20 | .1794 | .2538 | .9838 | .9929 | .1823 | .2609 | 5.4845 | .7391 | 40 | 1.3904 |
| 0.1833 | 30 | .1822 | .2606 | .9833 | .9927 | .1853 | .2680 | 5.3955 | .7320 | 30 | 1.3875 |
| 0.1862 | 40 | .1851 | .2674 | .9827 | .9924 | .1883 | .2750 | 5.3093 | .7250 | 20 | 1.3846 |
| 0.1891 | 50 | .1880 | .2740 | .9822 | .9922 | .1914 | .2819 | 5.2257 | .7181 | 10 | 1.3817 |
| 0.1920 | 11°00' | .1908 | 9.2806 | .9816 | 9.9919 | .1944 | 9.2887 | 5.1446 | 0.7113 | 79°00' | 1.3788 |
| 0.1949 | 10 | .1937 | .2870 | .9811 | .9917 | .1974 | .2953 | 5.0658 | .7047 | 50 | 1.3759 |
| 0.1978 | 20 | .1965 | .2934 | .9805 | .9914 | .2004 | .3020 | 4.9894 | .6980 | 40 | 1.3730 |
| 0.2007 | 30 | .1994 | .2997 | .9799 | .9912 | .2035 | .3085 | 4.9152 | .6915 | 30 | 1.3701 |
| 0.2036 | 40 | .2022 | .3058 | .9793 | .9909 | .2065 | .3149 | 4.8430 | .6851 | 20 | 1.3672 |
| 0.2065 | 50 | .2051 | .3119 | .9787 | .9907 | .2095 | .3212 | 4.7729 | .6788 | 10 | 1.3643 |
| 0.2094 | 12°00' | .2079 | 9.3179 | .9781 | 9.9904 | .2126 | 9.3275 | 4.7046 | 0.6725 | 78°00' | 1.3614 |
| 0.2123 | 10 | .2108 | .3238 | .9775 | .9901 | .2156 | .3336 | 4.6382 | .6664 | 50 | 1.3584 |
| 0.2153 | 20 | .2136 | .3296 | .9769 | .9899 | .2186 | .3397 | 4.5736 | .6603 | 40 | 1.3555 |
| 0.2182 | 30 | .2164 | .3353 | .9763 | .9896 | .2217 | .3458 | 4.5107 | .6542 | 30 | 1.3526 |
| 0.2211 | 40 | .2193 | .3410 | .9757 | .9893 | .2247 | .3517 | 4.4494 | .6483 | 20 | 1.3497 |
| 0.2240 | 50 | .2221 | .3466 | .9750 | .9890 | .2278 | .3576 | 4.3897 | .6424 | 10 | 1.3468 |
| 0.2269 | 13°00' | .2250 | 9.3521 | .9744 | 9.9887 | .2309 | 9.3634 | 4.3315 | 0.6366 | 77°00' | 1.3439 |
| 0.2298 | 10 | .2278 | .3575 | .9737 | .9884 | .2339 | .3691 | 4.2747 | .6309 | 50 | 1.3410 |
| 0.2327 | 20 | .2306 | .3629 | .9730 | .9881 | .2370 | .3748 | 4.2193 | .6252 | 40 | 1.3381 |
| 0.2356 | 30 | .2334 | .3682 | .9724 | .9878 | .2401 | .3804 | 4.1653 | .6196 | 30 | 1.3352 |
| 0.2385 | 40 | .2363 | .3734 | .9717 | .9875 | .2432 | .3859 | 4.1126 | .6141 | 20 | 1.3323 |
| 0.2414 | 50 | .2391 | .3786 | .9710 | .9872 | .2462 | .3914 | 4.0611 | .6086 | 10 | 1.3294 |
| 0.2443 | 14°00' | .2419 | 9.3837 | .9703 | 9.9869 | .2493 | 9.3968 | 4.0108 | 0.6032 | 76°00' | 1.3265 |
| 0.2473 | 10 | .2447 | .3887 | .9696 | .9866 | .2524 | .4021 | 3.9617 | .5979 | 50 | 1.3235 |
| 0.2502 | 20 | .2476 | .3937 | .9689 | .9863 | .2555 | .4074 | 3.9136 | .5926 | 40 | 1.3206 |
| 0.2531 | 30 | .2504 | .3986 | .9681 | .9859 | .2586 | .4127 | 3.8667 | .5873 | 30 | 1.3177 |
| 0.2560 | 40 | .2532 | .4035 | .9674 | .9856 | .2617 | .4178 | 3.8208 | .5822 | 20 | 1.3148 |
| 0.2589 | 50 | .2560 | .4083 | .9667 | .9853 | .2648 | .4230 | 3.7760 | .5770 | 10 | 1.3119 |
| 0.2618 | 15°00' | .2588 | 9.4130 | .9659 | 9.9849 | .2679 | 9.4281 | 3.7321 | 0.5719 | 75°00' | 1.3090 |
| 0.2647 | 10 | .2616 | .4177 | .9652 | .9846 | .2711 | .4331 | 3.6891 | .5669 | 50 | 1.3061 |
| 0.2676 | 20 | .2644 | .4223 | .9644 | .9843 | .2742 | .4381 | 3.6470 | .5619 | 40 | 1.3032 |
| 0.2705 | 30 | .2672 | .4269 | .9636 | .9839 | .2773 | .4430 | 3.6059 | .5570 | 30 | 1.3003 |
| 0.2734 | 40 | .2700 | .4314 | .9628 | .9836 | .2805 | .4479 | 3.5656 | .5521 | 20 | 1.2974 |
| 0.2763 | 50 | .2728 | .4359 | .9621 | .9832 | .2836 | .4527 | 3.5261 | .5473 | 10 | 1.2945 |
| 0.2793 | 16°00' | .2756 | 9.4403 | .9613 | 9.9828 | .2867 | 9.4575 | 3.4874 | 0.5425 | 74°00' | 1.2915 |
| 0.2822 | 10 | .2784 | .4447 | .9605 | .9825 | .2899 | .4622 | 3.4495 | .5378 | 50 | 1.2886 |
| 0.2851 | 20 | .2812 | .4491 | .9596 | .9821 | .2931 | .4669 | 3.4124 | .5331 | 40 | 1.2857 |
| 0.2880 | 30 | .2840 | .4533 | .9588 | .9817 | .2962 | .4716 | 3.3759 | .5284 | 30 | 1.2828 |
| 0.2909 | 40 | .2868 | .4576 | .9580 | .9814 | .2994 | .4762 | 3.3402 | .5238 | 20 | 1.2799 |
| 0.2938 | 50 | .2896 | .4618 | .9572 | .9810 | .3026 | .4808 | 3.3052 | .5192 | 10 | 1.2770 |
| 0.2967 | 17°00' | .2924 | 9.4659 | .9563 | 9.9806 | .3057 | 9.4853 | 3.2709 | 0.5147 | 73°00' | 1.2741 |
| 0.2996 | 10 | .2952 | .4700 | .9555 | .9802 | .3089 | .4898 | 3.2371 | .5102 | 50 | 1.2712 |
| 0.3025 | 20 | .2979 | .4741 | .9546 | .9798 | .3121 | .4943 | 3.2041 | .5057 | 40 | 1.2683 |
| 0.3054 | 30 | .3007 | .4781 | .9537 | .9794 | .3153 | .4987 | 3.1716 | .5013 | 30 | 1.2654 |
| 0.3083 | 40 | .3035 | .4821 | .9528 | .9790 | .3185 | .5031 | 3.1397 | .4969 | 20 | 1.2625 |
| 0.3113 | 50 | .3062 | .4861 | .9520 | .9786 | .3217 | .5075 | 3.1084 | .4925 | 10 | 1.2595 |
| 0.3142 | 18°00' | .3090 | 9.4900 | .9511 | 9.9782 | .3249 | 9.5118 | 3.0777 | 0.4882 | 72°00' | 1.2566 |
| | | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | DE- GREES. | RADI- ANS. |
| | | COSINES. | | SINES. | | COTAN- GENTS. | | TANGENTS. | | | |

CIRCULAR (TRIGONOMETRIC) FUNCTIONS

| RADI- ANS. | DE- GREES. | SINES. | | COSINES | | TANGENTS. | | COTANGENTS. | | | |
|---------------|---------------|----------|--------|---------|--------|------------------|--------|-------------|--------|---------------|---------------|
| | | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | | |
| 0.3142 | 18°00' | .3090 | 9.4900 | .9511 | 9.9782 | .3249 | 9.5118 | 3.0777 | 0.4882 | 72°00' | 1.2566 |
| 0.3171 | 10 | .3118 | .4939 | .9502 | .9778 | .3281 | .5161 | 3.0475 | .4839 | 50 | 1.2537 |
| 0.3200 | 20 | .3145 | .4977 | .9492 | .9774 | .3314 | .5203 | 3.0178 | .4797 | 40 | 1.2508 |
| 0.3229 | 30 | .3173 | .5015 | .9483 | .9770 | .3346 | .5245 | 2.9887 | .4755 | 30 | 1.2479 |
| 0.3258 | 40 | .3201 | .5052 | .9474 | .9765 | .3378 | .5287 | 2.9600 | .4713 | 20 | 1.2450 |
| 0.3287 | 50 | .3228 | .5090 | .9465 | .9761 | .3411 | .5329 | 2.9319 | .4671 | 10 | 1.2421 |
| 0.3316 | 19°00' | .3256 | 9.5126 | .9455 | 9.9757 | .3443 | 9.5370 | 2.9042 | 0.4630 | 71°00' | 1.2392 |
| 0.3345 | 10 | .3283 | .5163 | .9446 | .9752 | .3476 | .5411 | 2.8770 | .4589 | 50 | 1.2363 |
| 0.3374 | 20 | .3311 | .5199 | .9436 | .9748 | .3508 | .5451 | 2.8502 | .4549 | 40 | 1.2334 |
| 0.3403 | 30 | .3338 | .5235 | .9426 | .9743 | .3541 | .5491 | 2.8239 | .4509 | 30 | 1.2305 |
| 0.3432 | 40 | .3365 | .5270 | .9417 | .9739 | .3574 | .5531 | 2.7980 | .4469 | 20 | 1.2275 |
| 0.3462 | 50 | .3393 | .5306 | .9407 | .9734 | .3607 | .5571 | 2.7725 | .4429 | 10 | 1.2246 |
| 0.3491 | 20°00' | .3420 | 9.5341 | .9397 | 9.9730 | .3640 | 9.5611 | 2.7475 | 0.4389 | 70°00' | 1.2217 |
| 0.3520 | 10 | .3448 | .5375 | .9387 | .9725 | .3673 | .5650 | 2.7228 | .4350 | 50 | 1.2188 |
| 0.3549 | 20 | .3475 | .5409 | .9377 | .9721 | .3706 | .5689 | 2.6985 | .4311 | 40 | 1.2159 |
| 0.3578 | 30 | .3502 | .5443 | .9367 | .9716 | .3739 | .5727 | 2.6746 | .4273 | 30 | 1.2130 |
| 0.3607 | 40 | .3529 | .5477 | .9356 | .9711 | .3772 | .5766 | 2.6511 | .4234 | 20 | 1.2101 |
| 0.3636 | 50 | .3557 | .5510 | .9346 | .9706 | .3805 | .5804 | 2.6279 | .4196 | 10 | 1.2072 |
| 0.3665 | 21°00' | .3584 | 9.5543 | .9336 | 9.9702 | .3839 | 9.5842 | 2.6051 | 0.4158 | 69°00' | 1.2043 |
| 0.3694 | 10 | .3611 | .5576 | .9325 | .9697 | .3872 | .5879 | 2.5826 | .4121 | 50 | 1.2014 |
| 0.3723 | 20 | .3638 | .5609 | .9315 | .9692 | .3906 | .5917 | 2.5605 | .4083 | 40 | 1.1985 |
| 0.3752 | 30 | .3665 | .5641 | .9304 | .9687 | .3939 | .5954 | 2.5386 | .4046 | 30 | 1.1956 |
| 0.3782 | 40 | .3692 | .5673 | .9293 | .9682 | .3973 | .5991 | 2.5172 | .4009 | 20 | 1.1926 |
| 0.3811 | 50 | .3719 | .5704 | .9283 | .9677 | .4006 | .6028 | 2.4960 | .3972 | 10 | 1.1897 |
| 0.3840 | 22°00' | .3746 | 9.5736 | .9272 | 9.9672 | .4040 | 9.6064 | 2.4751 | 0.3936 | 68°00' | 1.1868 |
| 0.3869 | 10 | .3773 | .5767 | .9261 | .9667 | .4074 | .6100 | 2.4545 | .3900 | 50 | 1.1839 |
| 0.3898 | 20 | .3800 | .5798 | .9250 | .9661 | .4108 | .6136 | 2.4342 | .3864 | 40 | 1.1810 |
| 0.3927 | 30 | .3827 | .5828 | .9239 | .9656 | .4142 | .6172 | 2.4142 | .3828 | 30 | 1.1781 |
| 0.3956 | 40 | .3854 | .5859 | .9228 | .9651 | .4176 | .6208 | 2.3945 | .3792 | 20 | 1.1752 |
| 0.3985 | 50 | .3881 | .5889 | .9216 | .9646 | .4210 | .6243 | 2.3750 | .3757 | 10 | 1.1723 |
| 0.4014 | 23°00' | .3907 | 9.5919 | .9205 | 9.9640 | .4245 | 9.6279 | 2.3559 | 0.3721 | 67°00' | 1.1694 |
| 0.4043 | 10 | .3934 | .5948 | .9194 | .9635 | .4279 | .6314 | 2.3369 | .3686 | 50 | 1.1665 |
| 0.4072 | 20 | .3961 | .5978 | .9182 | .9629 | .4314 | .6348 | 2.3183 | .3652 | 40 | 1.1636 |
| 0.4102 | 30 | .3987 | .6007 | .9171 | .9624 | .4348 | .6383 | 2.2998 | .3617 | 30 | 1.1606 |
| 0.4131 | 40 | .4014 | .6036 | .9159 | .9618 | .4383 | .6417 | 2.2817 | .3583 | 20 | 1.1577 |
| 0.4160 | 50 | .4041 | .6065 | .9147 | .9613 | .4417 | .6452 | 2.2637 | .3548 | 10 | 1.1548 |
| 0.4189 | 24°00' | .4067 | 9.6093 | .9135 | 9.9607 | .4452 | 9.6486 | 2.2460 | 0.3514 | 66°00' | 1.1519 |
| 0.4218 | 10 | .4094 | .6121 | .9124 | .9602 | .4487 | .6520 | 2.2286 | .3480 | 50 | 1.1490 |
| 0.4247 | 20 | .4120 | .6149 | .9112 | .9596 | .4522 | .6553 | 2.2113 | .3447 | 40 | 1.1461 |
| 0.4276 | 30 | .4147 | .6177 | .9100 | .9590 | .4557 | .6587 | 2.1943 | .3413 | 30 | 1.1432 |
| 0.4305 | 40 | .4173 | .6205 | .9088 | .9584 | .4592 | .6620 | 2.1775 | .3380 | 20 | 1.1403 |
| 0.4334 | 50 | .4200 | .6232 | .9075 | .9579 | .4628 | .6654 | 2.1609 | .3346 | 10 | 1.1374 |
| 0.4363 | 25°00' | .4226 | 9.6259 | .9063 | 9.9573 | .4663 | 9.6687 | 2.1445 | 0.3313 | 65°00' | 1.1345 |
| 0.4392 | 10 | .4253 | .6286 | .9051 | .9567 | .4699 | .6720 | 2.1283 | .3280 | 50 | 1.1316 |
| 0.4422 | 20 | .4279 | .6313 | .9038 | .9561 | .4734 | .6752 | 2.1123 | .3248 | 40 | 1.1286 |
| 0.4451 | 30 | .4305 | .6340 | .9026 | .9555 | .4770 | .6785 | 2.0965 | .3215 | 30 | 1.1257 |
| 0.4480 | 40 | .4331 | .6366 | .9013 | .9549 | .4806 | .6817 | 2.0809 | .3183 | 20 | 1.1228 |
| 0.4509 | 50 | .4358 | .6392 | .9001 | .9543 | .4841 | .6850 | 2.0655 | .3150 | 10 | 1.1199 |
| 0.4538 | 26°00' | .4384 | 9.6418 | .8988 | 9.9537 | .4877 | 9.6882 | 2.0503 | 0.3118 | 64°00' | 1.1170 |
| 0.4567 | 10 | .4410 | .6444 | .8975 | .9530 | .4913 | .6914 | 2.0353 | .3086 | 50 | 1.1141 |
| 0.4596 | 20 | .4436 | .6470 | .8962 | .9524 | .4950 | .6946 | 2.0204 | .3054 | 40 | 1.1112 |
| 0.4625 | 30 | .4462 | .6495 | .8949 | .9518 | .4986 | .6977 | 2.0057 | .3023 | 30 | 1.1083 |
| 0.4654 | 40 | .4488 | .6521 | .8936 | .9512 | .5022 | .7009 | 1.9912 | .2991 | 20 | 1.1054 |
| 0.4683 | 50 | .4514 | .6546 | .8923 | .9505 | .5059 | .7040 | 1.9768 | .2960 | 10 | 1.1025 |
| 0.4712 | 27°00' | .4540 | 9.6570 | .8910 | 9.9499 | .5095 | 9.7072 | 1.9626 | 0.2928 | 63°00' | 1.0996 |
| | | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | DE- GREES. | RADI- ANS. |
| | | COSINES. | | SINES. | | COTAN- GENTS. | | TANGENTS | | | |

CIRCULAR (TRIGONOMETRIC) FUNCTIONS

| RADI- ANS. | DE- GREES | SINES. | | COSINES. | | TANGENTS. | | COTANGENTS. | | | |
|---------------|--------------|----------|--------|----------|--------|------------------|--------|-------------|--------|---------------|---------------|
| | | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | | |
| 0.4712 | 27°00' | .4540 | 9.6570 | .8910 | 9.9499 | .5095 | 9.7072 | 1.9626 | 0.2928 | 63°00' | 1.0996 |
| 0.4741 | 10 | .4566 | .6595 | .8897 | .9492 | .5132 | .7103 | 1.9486 | .2897 | 50 | 1.0966 |
| 0.4771 | 20 | .4592 | .6620 | .8884 | .9486 | .5169 | .7134 | 1.9347 | .2866 | 40 | 1.0937 |
| 0.4800 | 30 | .4617 | .6644 | .8870 | .9479 | .5206 | .7165 | 1.9210 | .2835 | 30 | 1.0908 |
| 0.4829 | 40 | .4643 | .6668 | .8857 | .9473 | .5243 | .7196 | 1.9074 | .2804 | 20 | 1.0879 |
| 0.4858 | 50 | .4669 | .6692 | .8843 | .9466 | .5280 | .7226 | 1.8940 | .2774 | 10 | 1.0850 |
| 0.4887 | 28°00' | .4695 | 9.6716 | .8829 | 9.9459 | .5317 | 9.7257 | 1.8807 | 0.2743 | 62°00' | 1.0821 |
| 0.4916 | 10 | .4720 | .6740 | .8816 | .9453 | .5354 | .7287 | 1.8676 | .2713 | 50 | 1.0792 |
| 0.4945 | 20 | .4746 | .6763 | .8802 | .9446 | .5392 | .7317 | 1.8546 | .2683 | 40 | 1.0763 |
| 0.4974 | 30 | .4772 | .6787 | .8788 | .9439 | .5430 | .7348 | 1.8418 | .2652 | 30 | 1.0734 |
| 0.5003 | 40 | .4797 | .6810 | .8774 | .9432 | .5467 | .7378 | 1.8291 | .2622 | 20 | 1.0705 |
| 0.5032 | 50 | .4823 | .6833 | .8760 | .9425 | .5505 | .7408 | 1.8165 | .2592 | 10 | 1.0676 |
| 0.5061 | 29°00' | .4848 | 9.6856 | .8746 | 9.9418 | .5543 | 9.7438 | 1.8040 | 0.2562 | 61°00' | 1.0647 |
| 0.5091 | 10 | .4874 | .6878 | .8732 | .9411 | .5581 | .7467 | 1.7917 | .2533 | 50 | 1.0617 |
| 0.5120 | 20 | .4899 | .6901 | .8718 | .9404 | .5619 | .7497 | 1.7796 | .2503 | 40 | 1.0588 |
| 0.5149 | 30 | .4924 | .6923 | .8704 | .9397 | .5658 | .7526 | 1.7675 | .2474 | 30 | 1.0559 |
| 0.5178 | 40 | .4950 | .6946 | .8689 | .9390 | .5696 | .7556 | 1.7556 | .2444 | 20 | 1.0530 |
| 0.5207 | 50 | .4975 | .6968 | .8675 | .9383 | .5735 | .7585 | 1.7437 | .2415 | 10 | 1.0501 |
| 0.5236 | 30°00' | .5000 | 9.6990 | .8660 | 9.9375 | .5774 | 9.7614 | 1.7321 | 0.2386 | 60°00' | 1.0472 |
| 0.5265 | 10 | .5025 | .7012 | .8646 | .9368 | .5812 | .7644 | 1.7205 | .2356 | 50 | 1.0443 |
| 0.5294 | 20 | .5050 | .7033 | .8631 | .9361 | .5851 | .7673 | 1.7090 | .2327 | 40 | 1.0414 |
| 0.5323 | 30 | .5075 | .7055 | .8616 | .9353 | .5890 | .7701 | 1.6977 | .2299 | 30 | 1.0385 |
| 0.5352 | 40 | .5100 | .7076 | .8601 | .9346 | .5930 | .7730 | 1.6864 | .2270 | 20 | 1.0356 |
| 0.5381 | 50 | .5125 | .7097 | .8587 | .9338 | .5969 | .7759 | 1.6753 | .2241 | 10 | 1.0327 |
| 0.5411 | 31°00' | .5150 | 9.7118 | .8572 | 9.9331 | .6009 | 9.7788 | 1.6643 | 0.2212 | 59°00' | 1.0297 |
| 0.5440 | 10 | .5175 | .7139 | .8557 | .9323 | .6048 | .7816 | 1.6534 | .2184 | 50 | 1.0268 |
| 0.5469 | 20 | .5200 | .7160 | .8542 | .9315 | .6088 | .7845 | 1.6426 | .2155 | 40 | 1.0239 |
| 0.5498 | 30 | .5225 | .7181 | .8526 | .9308 | .6128 | .7873 | 1.6319 | .2127 | 30 | 1.0210 |
| 0.5527 | 40 | .5250 | .7201 | .8511 | .9300 | .6168 | .7902 | 1.6212 | .2098 | 20 | 1.0181 |
| 0.5556 | 50 | .5275 | .7222 | .8496 | .9292 | .6208 | .7930 | 1.6107 | .2070 | 10 | 1.0152 |
| 0.5585 | 32°00' | .5299 | 9.7242 | .8480 | 9.9284 | .6249 | 9.7958 | 1.6003 | 0.2042 | 58°00' | 1.0123 |
| 0.5614 | 10 | .5324 | .7262 | .8465 | .9276 | .6289 | .7986 | 1.5900 | .2014 | 50 | 1.0094 |
| 0.5643 | 20 | .5348 | .7282 | .8450 | .9268 | .6330 | .8014 | 1.5798 | .1986 | 40 | 1.0065 |
| 0.5672 | 30 | .5373 | .7302 | .8434 | .9260 | .6371 | .8042 | 1.5697 | .1958 | 30 | 1.0036 |
| 0.5701 | 40 | .5398 | .7322 | .8418 | .9252 | .6412 | .8070 | 1.5597 | .1930 | 20 | 1.0007 |
| 0.5730 | 50 | .5422 | .7342 | .8403 | .9244 | .6453 | .8097 | 1.5497 | .1903 | 10 | 0.9977 |
| 0.5760 | 33°00' | .5446 | 9.7361 | .8387 | 9.9236 | .6494 | 9.8125 | 1.5399 | 0.1875 | 57°00' | 0.9948 |
| 0.5789 | 10 | .5471 | .7380 | .8371 | .9228 | .6536 | .8153 | 1.5301 | .1847 | 50 | 0.9919 |
| 0.5818 | 20 | .5495 | .7400 | .8355 | .9219 | .6577 | .8180 | 1.5204 | .1820 | 40 | 0.9890 |
| 0.5847 | 30 | .5519 | .7419 | .8339 | .9211 | .6619 | .8208 | 1.5108 | .1792 | 30 | 0.9861 |
| 0.5876 | 40 | .5544 | .7438 | .8323 | .9203 | .6661 | .8235 | 1.5013 | .1765 | 20 | 0.9832 |
| 0.5905 | 50 | .5568 | .7457 | .8307 | .9194 | .6703 | .8263 | 1.4919 | .1737 | 10 | 0.9803 |
| 0.5934 | 34°00' | .5592 | 9.7476 | .8290 | 9.9186 | .6745 | 9.8290 | 1.4826 | 0.1710 | 56°00' | 0.9774 |
| 0.5963 | 10 | .5616 | .7494 | .8274 | .9177 | .6787 | .8317 | 1.4733 | .1683 | 50 | 0.9745 |
| 0.5992 | 20 | .5640 | .7513 | .8258 | .9169 | .6830 | .8344 | 1.4641 | .1656 | 40 | 0.9716 |
| 0.6021 | 30 | .5664 | .7531 | .8241 | .9160 | .6873 | .8371 | 1.4550 | .1629 | 30 | 0.9687 |
| 0.6050 | 40 | .5688 | .7550 | .8225 | .9151 | .6916 | .8398 | 1.4460 | .1602 | 20 | 0.9657 |
| 0.6080 | 50 | .5712 | .7568 | .8208 | .9142 | .6959 | .8425 | 1.4370 | .1575 | 10 | 0.9628 |
| 0.6109 | 35°00' | .5736 | 9.7586 | .8192 | 9.9134 | .7002 | 9.8452 | 1.4281 | 0.1548 | 55°00' | 0.9599 |
| 0.6138 | 10 | .5760 | .7604 | .8175 | .9125 | .7046 | .8479 | 1.4193 | .1521 | 50 | 0.9570 |
| 0.6167 | 20 | .5783 | .7622 | .8158 | .9116 | .7089 | .8506 | 1.4106 | .1494 | 40 | 0.9541 |
| 0.6196 | 30 | .5807 | .7640 | .8141 | .9107 | .7133 | .8533 | 1.4019 | .1467 | 30 | 0.9512 |
| 0.6225 | 40 | .5831 | .7657 | .8124 | .9098 | .7177 | .8559 | 1.3934 | .1441 | 20 | 0.9483 |
| 0.6254 | 50 | .5854 | .7675 | .8107 | .9089 | .7221 | .8586 | 1.3848 | .1414 | 10 | 0.9454 |
| 0.6283 | 36°00' | .5878 | 9.7692 | .8090 | 9.9080 | .7265 | 9.8613 | 1.3764 | 0.1387 | 54°00' | 0.9425 |
| | | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | DE- GREES. | RADI- ANS. |
| | | COSINES. | | SINES. | | COTAN- GENTS. | | TANGENTS. | | | |

CIRCULAR (TRIGONOMETRIC) FUNCTIONS

| RADIAN. ANS. | DE- GREES. | SINES. | | COSINES. | | TANGENTS. | | COTANGENTS. | | | |
|-----------------|---------------|----------|--------|----------|--------|------------------|--------|-------------|--------|---------------|---------------|
| | | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | | |
| 0.6283 | 36°00' | .5878 | 9.7692 | .8090 | 9.9080 | .7265 | 9.8613 | 1.3764 | 0.1387 | 54°00' | 0.9425 |
| 0.6312 | 10 | .5901 | .7710 | .8073 | .9070 | .7310 | .8639 | 1.3680 | .1361 | 50 | 0.9396 |
| 0.6341 | 20 | .5925 | .7727 | .8056 | .9061 | .7355 | .8666 | 1.3597 | .1334 | 40 | 0.9367 |
| 0.6370 | 30 | .5948 | .7744 | .8039 | .9052 | .7400 | .8692 | 1.3514 | .1308 | 30 | 0.9338 |
| 0.6400 | 40 | .5972 | .7761 | .8021 | .9042 | .7445 | .8718 | 1.3432 | .1282 | 20 | 0.9308 |
| 0.6429 | 50 | .5995 | .7778 | .8004 | .9033 | .7490 | .8745 | 1.3351 | .1255 | 10 | 0.9279 |
| 0.6458 | 37°00' | .6018 | 9.7795 | .7986 | 9.9023 | .7536 | 9.8771 | 1.3270 | 0.1229 | 53°00' | 0.9250 |
| 0.6487 | 10 | .6041 | .7811 | .7969 | .9014 | .7581 | .8797 | 1.3190 | .1203 | 50 | 0.9221 |
| 0.6516 | 20 | .6065 | .7828 | .7951 | .9004 | .7627 | .8824 | 1.3111 | .1176 | 40 | 0.9192 |
| 0.6545 | 30 | .6088 | .7844 | .7934 | .8995 | .7673 | .8850 | 1.3032 | .1150 | 30 | 0.9163 |
| 0.6574 | 40 | .6111 | .7861 | .7916 | .8985 | .7720 | .8876 | 1.2954 | .1124 | 20 | 0.9134 |
| 0.6603 | 50 | .6134 | .7877 | .7898 | .8975 | .7766 | .8902 | 1.2876 | .1098 | 10 | 0.9105 |
| 0.6632 | 38°00' | .6157 | 9.7893 | .7880 | 9.8965 | .7813 | 9.8928 | 1.2799 | 0.1072 | 52°00' | 0.9076 |
| 0.6661 | 10 | .6180 | .7910 | .7862 | .8955 | .7860 | .8954 | 1.2723 | .1046 | 50 | 0.9047 |
| 0.6690 | 20 | .6202 | .7926 | .7844 | .8945 | .7907 | .8980 | 1.2647 | .1020 | 40 | 0.9018 |
| 0.6720 | 30 | .6225 | .7941 | .7826 | .8935 | .7954 | .9006 | 1.2572 | .0994 | 30 | 0.8988 |
| 0.6749 | 40 | .6248 | .7957 | .7808 | .8925 | .8002 | .9032 | 1.2497 | .0968 | 20 | 0.8959 |
| 0.6778 | 50 | .6271 | .7973 | .7790 | .8915 | .8050 | .9058 | 1.2423 | .0942 | 10 | 0.8930 |
| 0.6807 | 39°00' | .6293 | 9.7989 | .7771 | 9.8905 | .8098 | 9.9084 | 1.2349 | 0.0916 | 51°00' | 0.8901 |
| 0.6836 | 10 | .6316 | .8004 | .7753 | .8895 | .8146 | .9110 | 1.2276 | .0890 | 50 | 0.8872 |
| 0.6865 | 20 | .6338 | .8020 | .7735 | .8884 | .8195 | .9135 | 1.2203 | .0865 | 40 | 0.8843 |
| 0.6894 | 30 | .6361 | .8035 | .7716 | .8874 | .8243 | .9161 | 1.2131 | .0839 | 30 | 0.8814 |
| 0.6923 | 40 | .6383 | .8050 | .7698 | .8864 | .8292 | .9187 | 1.2059 | .0813 | 20 | 0.8785 |
| 0.6952 | 50 | .6406 | .8066 | .7679 | .8853 | .8342 | .9212 | 1.1988 | .0788 | 10 | 0.8756 |
| 0.6981 | 40°00' | .6428 | 9.8081 | .7660 | 9.8843 | .8391 | 9.9238 | 1.1918 | 0.0762 | 50°00' | 0.8727 |
| 0.7010 | 10 | .6450 | .8096 | .7642 | .8832 | .8441 | .9264 | 1.1847 | .0736 | 50 | 0.8698 |
| 0.7039 | 20 | .6472 | .8111 | .7623 | .8821 | .8491 | .9289 | 1.1778 | .0711 | 40 | 0.8668 |
| 0.7069 | 30 | .6494 | .8125 | .7604 | .8810 | .8541 | .9315 | 1.1708 | .0685 | 30 | 0.8639 |
| 0.7098 | 40 | .6517 | .8140 | .7585 | .8800 | .8591 | .9341 | 1.1640 | .0659 | 20 | 0.8610 |
| 0.7127 | 50 | .6539 | .8155 | .7566 | .8789 | .8642 | .9366 | 1.1571 | .0634 | 10 | 0.8581 |
| 0.7156 | 41°00' | .6561 | 9.8169 | .7547 | 9.8778 | .8693 | 9.9392 | 1.1504 | 0.0608 | 49°00' | 0.8552 |
| 0.7185 | 10 | .6583 | .8184 | .7528 | .8767 | .8744 | .9417 | 1.1436 | .0583 | 50 | 0.8523 |
| 0.7214 | 20 | .6604 | .8198 | .7509 | .8756 | .8796 | .9443 | 1.1369 | .0557 | 40 | 0.8494 |
| 0.7243 | 30 | .6626 | .8213 | .7490 | .8745 | .8847 | .9468 | 1.1303 | .0532 | 30 | 0.8465 |
| 0.7272 | 40 | .6648 | .8227 | .7470 | .8733 | .8899 | .9494 | 1.1237 | .0506 | 20 | 0.8436 |
| 0.7301 | 50 | .6670 | .8241 | .7451 | .8722 | .8952 | .9519 | 1.1171 | .0481 | 10 | 0.8407 |
| 0.7330 | 42°00' | .6691 | 9.8255 | .7431 | 9.8711 | .9004 | 9.9544 | 1.1106 | 0.0456 | 48°00' | 0.8378 |
| 0.7359 | 10 | .6713 | .8269 | .7412 | .8699 | .9057 | .9570 | 1.1041 | .0430 | 50 | 0.8348 |
| 0.7389 | 20 | .6734 | .8283 | .7392 | .8688 | .9110 | .9595 | 1.0977 | .0405 | 40 | 0.8319 |
| 0.7418 | 30 | .6756 | .8297 | .7373 | .8676 | .9163 | .9621 | 1.0913 | .0379 | 30 | 0.8290 |
| 0.7447 | 40 | .6777 | .8311 | .7353 | .8665 | .9217 | .9646 | 1.0850 | .0354 | 20 | 0.8261 |
| 0.7476 | 50 | .6799 | .8324 | .7333 | .8653 | .9271 | .9671 | 1.0786 | .0329 | 10 | 0.8232 |
| 0.7505 | 43°00' | .6820 | 9.8338 | .7314 | 9.8641 | .9325 | 9.9697 | 1.0724 | 0.0303 | 47°00' | 0.8203 |
| 0.7534 | 10 | .6841 | .8351 | .7294 | .8629 | .9380 | .9722 | 1.0661 | .0278 | 50 | 0.8174 |
| 0.7563 | 20 | .6862 | .8365 | .7274 | .8618 | .9435 | .9747 | 1.0599 | .0253 | 40 | 0.8145 |
| 0.7592 | 30 | .6884 | .8378 | .7254 | .8606 | .9490 | .9772 | 1.0538 | .0228 | 30 | 0.8116 |
| 0.7621 | 40 | .6905 | .8391 | .7234 | .8594 | .9545 | .9798 | 1.0477 | .0202 | 20 | 0.8087 |
| 0.7650 | 50 | .6926 | .8405 | .7214 | .8582 | .9601 | .9823 | 1.0416 | .0177 | 10 | 0.8058 |
| 0.7679 | 44°00' | .6947 | 9.8418 | .7193 | 9.8569 | .9657 | 9.9848 | 1.0355 | 0.0152 | 46°00' | 0.8029 |
| 0.7709 | 10 | .6967 | .8431 | .7173 | .8557 | .9713 | .9874 | 1.0295 | .0126 | 50 | 0.7999 |
| 0.7738 | 20 | .6988 | .8444 | .7153 | .8545 | .9770 | .9899 | 1.0235 | .0101 | 40 | 0.7970 |
| 0.7767 | 30 | .7009 | .8457 | .7133 | .8532 | .9827 | .9924 | 1.0176 | .0076 | 30 | 0.7941 |
| 0.7796 | 40 | .7030 | .8469 | .7112 | .8520 | .9884 | .9949 | 1.0117 | .0051 | 20 | 0.7912 |
| 0.7825 | 50 | .7050 | .8482 | .7092 | .8507 | .9942 | .9975 | 1.0058 | .0025 | 10 | 0.7883 |
| 0.7854 | 45°00' | .7071 | 9.8495 | .7071 | 9.8495 | 1.0000 | 0.0000 | 1.0000 | 0.0000 | 45°00' | 0.7854 |
| | | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | DE- GREES. | RADI- ANS. |
| | | COSINES. | | SINES. | | COTAN- GENTS. | | TANGENTS. | | | |

TABLE 15
CIRCULAR (TRIGONOMETRIC) FUNCTIONS

| RADIAN. | SINES. | | COSINES. | | TANGENTS. | | COTANGENTS. | | DEGREES. |
|---------|---------|---------|----------|---------|-----------|---------|-------------|---------|----------|
| | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | |
| 0.00 | 0.00000 | — ∞ | 1.00000 | 0.00000 | — ∞ | — ∞ | ∞ | ∞ | 00°00' |
| .01 | .01000 | 7.99999 | 0.99995 | 9.99998 | 0.01000 | 8.00001 | 99.997 | 1.99999 | 00 34 |
| .02 | .02000 | 8.30100 | .99980 | .99991 | .02000 | .30109 | 49.993 | .69891 | 01 09 |
| .03 | .03000 | .47706 | .99955 | .99980 | .03001 | .47725 | 33.323 | .52275 | 01 43 |
| .04 | .03999 | .60194 | .99920 | .99965 | .04002 | .60229 | 24.987 | .39771 | 02 18 |
| 0.05 | 0.04998 | 8.69879 | 0.99875 | 9.99946 | 0.05004 | 8.69933 | 19.983 | 1.30067 | 02°52' |
| .06 | .05996 | .77789 | .99820 | .99922 | .06007 | .77807 | 16.647 | .22133 | 03 26 |
| .07 | .06994 | .84474 | .99755 | .99894 | .07011 | .84581 | 14.262 | .15419 | 04 01 |
| .08 | .07991 | .90263 | .99680 | .99861 | .08017 | .90402 | 12.473 | .09598 | 04 35 |
| .09 | .08988 | .95366 | .99595 | .99824 | .09024 | .95542 | 11.081 | .04458 | 05 09 |
| 0.10 | 0.09983 | 8.99928 | 0.99500 | 9.99782 | 0.10033 | 9.00145 | 9.9666 | 0.99855 | 05°44' |
| .11 | .10978 | 9.04052 | .99396 | .99737 | .11045 | .04315 | 9.0542 | .95685 | 06 18 |
| .12 | .11971 | .07814 | .99281 | .99687 | .12058 | .08127 | 8.2933 | .91873 | 06 53 |
| .13 | .12963 | .11272 | .99156 | .99632 | .13074 | .11640 | 7.6489 | .88360 | 07 27 |
| .14 | .13954 | .14471 | .99022 | .99573 | .14092 | .14898 | 7.0961 | .85102 | 08 01 |
| 0.15 | 0.14944 | 9.17446 | 0.98877 | 9.99510 | 0.15114 | 9.17937 | 6.6166 | 0.82063 | 08°36' |
| .16 | .15932 | .20227 | .98723 | .99442 | .16138 | .20785 | 6.1966 | .79215 | 09 10 |
| .17 | .16918 | .22836 | .98558 | .99369 | .17166 | .23466 | 5.8256 | .76534 | 09 44 |
| .18 | .17903 | .25292 | .98384 | .99293 | .18197 | .26000 | 5.4954 | .74000 | 10 19 |
| .19 | .18886 | .27614 | .98200 | .99211 | .19232 | .28402 | 5.1997 | .71598 | 10 53 |
| 0.20 | 0.19867 | 9.29813 | 0.98007 | 9.99126 | 0.20271 | 9.30688 | 4.9332 | 0.69312 | 11°28' |
| .21 | .20846 | .31902 | .97803 | .99035 | .21314 | .32867 | 4.6917 | .67133 | 12 02 |
| .22 | .21823 | .33891 | .97590 | .98940 | .22362 | .34951 | 4.4719 | .65049 | 12 36 |
| .23 | .22798 | .35789 | .97367 | .98841 | .23414 | .36948 | 4.2709 | .63052 | 13 11 |
| .24 | .23770 | .37603 | .97134 | .98737 | .24472 | .38866 | 4.0864 | .61134 | 13 45 |
| 0.25 | 0.24740 | 9.39341 | 0.96891 | 9.98628 | 0.25534 | 9.40712 | 3.9163 | 0.59288 | 14°19' |
| .26 | .25708 | .41007 | .96639 | .98515 | .26602 | .42491 | 3.7592 | .57590 | 14 54 |
| .27 | .26673 | .42607 | .96377 | .98397 | .27676 | .44210 | 3.6133 | .55799 | 15 28 |
| .28 | .27636 | .44147 | .96106 | .98275 | .28755 | .45872 | 3.4776 | .54128 | 16 03 |
| .29 | .28595 | .45629 | .95824 | .98148 | .29841 | .47482 | 3.3511 | .52518 | 16 37 |
| 0.30 | 0.29552 | 9.47059 | 0.95534 | 9.98016 | 0.30934 | 9.49043 | 3.2327 | 0.50957 | 17°11' |
| .31 | .30506 | .48438 | .95233 | .97879 | .32033 | .50559 | 3.1218 | .49441 | 17 46 |
| .32 | .31457 | .49771 | .94924 | .97737 | .33139 | .52034 | 3.0176 | .47966 | 18 20 |
| .33 | .32404 | .51060 | .94604 | .97591 | .34252 | .53469 | 2.9195 | .46531 | 18 54 |
| .34 | .33349 | .52308 | .94275 | .97440 | .35374 | .54868 | 2.8270 | .45132 | 19 29 |
| 0.35 | 0.34290 | 9.53516 | 0.93937 | 9.97284 | 0.36503 | 9.56233 | 2.7395 | 0.43767 | 20°03' |
| .36 | .35227 | .54688 | .93590 | .97123 | .37640 | .57565 | 2.6567 | .42435 | 20 38 |
| .37 | .36162 | .55825 | .93233 | .96957 | .38786 | .58868 | 2.5782 | .41132 | 21 12 |
| .38 | .37092 | .56928 | .92866 | .96786 | .39941 | .60142 | 2.5037 | .39858 | 21 46 |
| .39 | .38019 | .58000 | .92491 | .96610 | .41105 | .61390 | 2.4328 | .38610 | 22 21 |
| 0.40 | 0.38942 | 9.59042 | 0.92106 | 9.96429 | 0.42279 | 9.62613 | 2.3652 | 0.37387 | 22°55' |
| .41 | .39861 | .60055 | .91712 | .96243 | .43463 | .63812 | 2.3008 | .36188 | 23 29 |
| .42 | .40776 | .61041 | .91309 | .96051 | .44657 | .64989 | 2.2393 | .35011 | 24 04 |
| .43 | .41687 | .62000 | .90897 | .95855 | .45862 | .66145 | 2.1804 | .33855 | 24 38 |
| .44 | .42594 | .62935 | .90475 | .95653 | .47078 | .67282 | 2.1241 | .32718 | 25 13 |
| 0.45 | 0.43497 | 9.63845 | 0.90045 | 9.95446 | 0.48306 | 9.68400 | 2.0702 | 0.31600 | 25°47' |
| .46 | .44395 | .64733 | .89605 | .95233 | .49545 | .69500 | 2.0184 | .30500 | 26 21 |
| .47 | .45289 | .65599 | .89157 | .95015 | .50797 | .70583 | 1.9686 | .29417 | 26 56 |
| .48 | .46178 | .66443 | .88699 | .94792 | .52061 | .71651 | 1.9208 | .28349 | 27 30 |
| .49 | .47063 | .67268 | .88233 | .94563 | .53339 | .72704 | 1.8748 | .27296 | 28 04 |
| 0 50 | 0.47943 | 9.68072 | 0.87758 | 9.94329 | 0.54630 | 9.73743 | 1.8305 | 0.26257 | 28°39' |

CIRCULAR (TRIGONOMETRIC) FUNCTIONS

| RADIANs | SINES. | | COSINES. | | TANGENTS | | COTANGENTS. | | DEGREEs |
|---------|---------|---------|----------|---------|----------|---------|-------------|---------|---------|
| | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | |
| 0.50 | 0.47943 | 9.68072 | 0.87758 | 9.94329 | 0.51630 | 9.73743 | 1.8305 | 0.26257 | 28°39' |
| .51 | .48818 | .68858 | .87274 | .94089 | .55936 | .74769 | .7878 | .25231 | 29 13 |
| .52 | .49688 | .69625 | .86782 | .93843 | .57256 | .75782 | .7465 | .24218 | 29 48 |
| .53 | .50553 | .70375 | .86281 | .93591 | .58592 | .76784 | .7067 | .23216 | 30 22 |
| .54 | .51414 | .71108 | .85771 | .93334 | .59943 | .77774 | .6683 | .22226 | 30 56 |
| 0.55 | 0.52269 | 9.71824 | 0.85252 | 9.93071 | 0.61311 | 9.78754 | 1.6310 | 0.21246 | 31°31' |
| .56 | .53119 | .72525 | .84726 | .92801 | .62695 | .79723 | .5950 | .20277 | 32 05 |
| .57 | .53963 | .73210 | .84190 | .92526 | .64097 | .80684 | .5601 | .19316 | 32 40 |
| .58 | .54802 | .73880 | .83646 | .92245 | .65517 | .81635 | .5263 | .18365 | 33 14 |
| .59 | .55636 | .74536 | .83094 | .91957 | .66956 | .82579 | .4935 | .17421 | 33 48 |
| 0.60 | 0.56464 | 9.75177 | 0.82534 | 9.91663 | 0.68414 | 9.83514 | 1.4617 | 0.16486 | 34°23' |
| .61 | .57287 | .75805 | .81965 | .91363 | .69892 | .84443 | .4308 | .15557 | 34 57 |
| .62 | .58104 | .76420 | .81388 | .91056 | .71391 | .85364 | .4007 | .14636 | 35 31 |
| .63 | .58924 | .77022 | .80803 | .90743 | .72911 | .86280 | .3715 | .13720 | 36 06 |
| .64 | .59720 | .77612 | .80210 | .90423 | .74454 | .87189 | .3431 | .12811 | 36 40 |
| 0.65 | 0.60519 | 9.78189 | 0.79608 | 9.90096 | 0.76020 | 9.88093 | 1.3154 | 0.11907 | 37°15' |
| .66 | .61312 | .78754 | .78999 | .89762 | .77610 | .88902 | .2885 | .11008 | 37 49 |
| .67 | .62099 | .79308 | .78382 | .89422 | .79225 | .89886 | .2622 | .10114 | 38 23 |
| .68 | .62879 | .79851 | .77757 | .89074 | .80866 | .90777 | .2366 | .09223 | 38 58 |
| .69 | .63654 | .80382 | .77125 | .88719 | .82534 | .91663 | .2116 | .08337 | 39 32 |
| 0.70 | 0.64422 | 9.80903 | 0.76484 | 9.88357 | 0.84229 | 9.92546 | 1.1872 | 0.07454 | 40°06' |
| .71 | .65183 | .81414 | .75836 | .87988 | .85953 | .93426 | .1634 | .06574 | 40 41 |
| .72 | .65938 | .81914 | .75181 | .87611 | .87707 | .94303 | .1402 | .05697 | 41 15 |
| .73 | .66687 | .82404 | .74517 | .87226 | .89492 | .95178 | .1174 | .04822 | 41 50 |
| .74 | .67429 | .82885 | .73847 | .86833 | .91309 | .96051 | .0952 | .03949 | 42 24 |
| 0.75 | 0.68164 | 9.83355 | 0.73169 | 9.86433 | 0.93160 | 9.96923 | 1.0734 | 0.03077 | 42°58' |
| .76 | .68892 | .83817 | .72484 | .86024 | .95045 | .97793 | .0521 | .02207 | 43 33 |
| .77 | .69614 | .84269 | .71791 | .85607 | .96967 | .98662 | .0313 | .01338 | 44 07 |
| .78 | .70328 | .84713 | .71091 | .85182 | .98926 | .99953 | 1.0109 | .00469 | 44 41 |
| .79 | .71035 | .85147 | .70385 | .84748 | 1.0092 | 0.00400 | 0.99084 | 9.99600 | 45 16 |
| 0.80 | 0.71736 | 9.85573 | 0.69671 | 9.84305 | 1.0296 | 0.01268 | 0.97121 | 9.98732 | 45°50' |
| .81 | .72429 | .85991 | .68950 | .83853 | .0505 | .02138 | .95197 | .97862 | 46 25 |
| .82 | .73115 | .86400 | .68222 | .83393 | .0717 | .03008 | .93309 | .96092 | 46 59 |
| .83 | .73793 | .86802 | .67488 | .82922 | .0934 | .03879 | .91455 | .94121 | 47 33 |
| .84 | .74464 | .87195 | .66746 | .82443 | .1156 | .04752 | .89635 | .92248 | 48 08 |
| 0.85 | 0.75128 | 9.87580 | 0.65998 | 9.81953 | 1.1383 | 0.05627 | 0.87848 | 9.94373 | 48°42' |
| .86 | .75784 | .87958 | .65244 | .81454 | .1616 | .06504 | .86091 | .93496 | 49 16 |
| .87 | .76433 | .88328 | .64483 | .80944 | .1853 | .07384 | .84365 | .92616 | 49 51 |
| .88 | .77074 | .88691 | .63715 | .80424 | .2097 | .08266 | .82668 | .91734 | 50 25 |
| .89 | .77707 | .89046 | .62941 | .79894 | .2346 | .09153 | .80998 | .90847 | 51 00 |
| 0.90 | 0.78333 | 9.89394 | 0.62161 | 9.79352 | 1.2602 | 0.10043 | 0.79355 | 9.89957 | 51°34' |
| .91 | .78950 | .89735 | .61375 | .78799 | .2864 | .10937 | .77738 | .89063 | 52 08 |
| .92 | .79560 | .90070 | .60582 | .78234 | .3133 | .11835 | .76146 | .88165 | 52 43 |
| .93 | .80162 | .90397 | .59783 | .77658 | .3409 | .12739 | .74578 | .87261 | 53 17 |
| .94 | .80756 | .90717 | .58979 | .77070 | .3692 | .13648 | .73034 | .86352 | 53 51 |
| 0.95 | 0.81342 | 9.91031 | 0.58168 | 9.76469 | 1.3984 | 0.14563 | 0.71511 | 9.85437 | 54°26' |
| .96 | .81919 | .91339 | .57352 | .75855 | .4284 | .15484 | .70010 | .84516 | 55 00 |
| .97 | .82489 | .91639 | .56530 | .75228 | .4592 | .16412 | .68531 | .83588 | 55 35 |
| .98 | .83050 | .91934 | .55702 | .74587 | .4910 | .17347 | .67071 | .82653 | 56 09 |
| .99 | .83603 | .92222 | .54869 | .73933 | .5237 | .18289 | .65631 | .81711 | 56 43 |
| 1.00 | 0.84147 | 9.92504 | 0.54030 | 9.73264 | 1.5574 | 0.19240 | 0.64209 | 9.80760 | 57°18' |

CIRCULAR (TRIGONOMETRIC) FUNCTIONS

| RADIAN. | SINES. | | COSINES. | | TANGENTS. | | COTANGENTS. | | DEGREES. |
|---------|---------|---------|----------|---------|-----------|---------|-------------|---------|----------|
| | Nat. | Log | Nat. | Log. | Nat. | Log. | Nat. | Log. | |
| 1.00 | 0.84147 | 9.92504 | 0.54030 | 9.73264 | 1.5574 | 0.19240 | 0.64209 | 9.80760 | 57°18' |
| .01 | .84683 | .92780 | .53186 | .72580 | .5922 | .20200 | .62806 | .79800 | 57 52 |
| .02 | .85211 | .93049 | .52337 | .71881 | .6281 | .21169 | .61420 | .78831 | 58 27 |
| .03 | .85730 | .93313 | .51482 | .71165 | .6652 | .22148 | .60051 | .77852 | 59 01 |
| .04 | .86240 | .93571 | .50622 | .70434 | .7036 | .23137 | .58699 | .76863 | 59 35 |
| 1.05 | 0.86742 | 9.93823 | 0.49757 | 9.69686 | 1.7433 | 0.24138 | 0.57362 | 9.75862 | 60°10' |
| .06 | .87236 | .94069 | .48887 | .68920 | .7844 | .25150 | .56040 | .74850 | 60 44 |
| .07 | .87720 | .94310 | .48012 | .68135 | .8270 | .26175 | .54734 | .73825 | 61 18 |
| .08 | .88196 | .94545 | .47133 | .67332 | .8712 | .27212 | .53441 | .72788 | 61 53 |
| .09 | .88663 | .94774 | .46249 | .66510 | .9171 | .28264 | .52162 | .71736 | 62 27 |
| 1.10 | 0.89121 | 9.94998 | 0.45360 | 9.65667 | 1.9648 | 0.29331 | 0.50897 | 9.70669 | 63°02' |
| .11 | .89570 | .95216 | .44466 | .64803 | 2.0143 | .30413 | .49644 | .69587 | 63 36 |
| .12 | .90010 | .95429 | .43568 | .63917 | .0660 | .31512 | .48404 | .68488 | 64 10 |
| .13 | .90441 | .95637 | .42666 | .63008 | .1198 | .32628 | .47175 | .67372 | 64 45 |
| .14 | .90863 | .95839 | .41759 | .62075 | .1759 | .33763 | .45959 | .66237 | 65 19 |
| 1.15 | 0.91276 | 9.96036 | 0.40849 | 9.61118 | 2.2345 | 0.34918 | 0.44753 | 9.65082 | 65°53' |
| .16 | .91680 | .96228 | .39934 | .60134 | .2958 | .36093 | .43558 | .63907 | 66 28 |
| .17 | .92075 | .96414 | .39015 | .59123 | .3600 | .37291 | .42373 | .62709 | 67 02 |
| .18 | .92461 | .96596 | .38092 | .58084 | .4273 | .38512 | .41199 | .61488 | 67 37 |
| .19 | .92837 | .96772 | .37166 | .57015 | .4979 | .39757 | .40034 | .60243 | 68 11 |
| 1.20 | 0.93204 | 9.96943 | 0.36236 | 9.55914 | 2.5722 | 0.41030 | 0.38878 | 9.58970 | 68°45' |
| .21 | .93562 | .97110 | .35302 | .54780 | .6503 | .42330 | .37731 | .57670 | 69 20 |
| .22 | .93910 | .97271 | .34365 | .53611 | .7328 | .43600 | .36593 | .56340 | 69 54 |
| .23 | .94249 | .97428 | .33424 | .52406 | .8198 | .44922 | .35463 | .54978 | 70 28 |
| .24 | .94578 | .97579 | .32480 | .51161 | .9119 | .46218 | .34341 | .53582 | 71 03 |
| 1.25 | 0.94998 | 9.97726 | 0.31532 | 9.49875 | 3.0096 | 0.47850 | 0.33227 | 9.52150 | 71°37' |
| .26 | .95209 | .97868 | .30582 | .48546 | .1133 | .49322 | .32121 | .50678 | 72 12 |
| .27 | .95510 | .98005 | .29628 | .47170 | .2236 | .50835 | .31021 | .49165 | 72 46 |
| .28 | .95802 | .98137 | .28672 | .45745 | .3413 | .52392 | .29928 | .47608 | 73 20 |
| .29 | .96084 | .98265 | .27712 | .44267 | .4672 | .53998 | .28842 | .46002 | 73 55 |
| 1.30 | 0.96356 | 9.98388 | 0.26750 | 9.42732 | 3.6021 | 0.55656 | 0.27762 | 9.44344 | 74°29' |
| .31 | .96618 | .98506 | .25785 | .41137 | .7471 | .57309 | .26687 | .42631 | 75 03 |
| .32 | .96872 | .98620 | .24818 | .39476 | .9033 | .59144 | .25619 | .40856 | 75 38 |
| .33 | .97115 | .98729 | .23848 | .37744 | 4.0723 | .60984 | .24556 | .39016 | 76 12 |
| .34 | .97348 | .98833 | .22875 | .35937 | .2556 | .62896 | .23498 | .37104 | 76 47 |
| 1.35 | 0.97572 | 9.98933 | 0.21901 | 9.34046 | 4.4552 | 0.64887 | 0.22446 | 9.35113 | 77°21' |
| .36 | .97786 | .99028 | .20924 | .32064 | .6734 | .66664 | .21398 | .33036 | 77 55 |
| .37 | .97991 | .99119 | .19945 | .29983 | .9131 | .69135 | .20354 | .30865 | 78 30 |
| .38 | .98185 | .99205 | .18964 | .27793 | 5.1774 | .71411 | .19315 | .28589 | 79 04 |
| .39 | .98370 | .99286 | .17981 | .25482 | .4707 | .73804 | .18279 | .26196 | 79 38 |
| 1.40 | 0.98545 | 9.99363 | 0.16997 | 9.23036 | 5.7979 | 0.76327 | 0.17248 | 9.23673 | 80°13' |
| .41 | .98710 | .99436 | .16010 | .20440 | 6.1654 | .78996 | .16220 | .21004 | 80 47 |
| .42 | .98865 | .99504 | .15023 | .17674 | 6.5811 | .81830 | .15195 | .18170 | 81 22 |
| .43 | .99010 | .99568 | .14033 | .14716 | 7.0555 | .84853 | .14173 | .15147 | 81 56 |
| .44 | .99146 | .99627 | .13042 | .11536 | 7.6018 | .88092 | .13155 | .11908 | 82 30 |
| 1.45 | 0.99271 | 9.99682 | 0.12050 | 9.08100 | 8.2381 | 0.91583 | 0.12139 | 9.08417 | 83°05' |
| .46 | .99387 | .99733 | .11057 | .04364 | 8.9886 | .95369 | .11125 | .04631 | 83 39 |
| .47 | .99492 | .99779 | .10063 | .00271 | 9.8874 | .99508 | .10114 | .00492 | 84 13 |
| .48 | .99588 | .99821 | .09067 | .895747 | 10.983 | 1.04074 | .09105 | .895926 | 84 48 |
| .49 | .99674 | .99858 | .08071 | .90692 | 12.350 | .09166 | .08097 | .90834 | 85 22 |
| 1.50 | 0.99749 | 9.99891 | 0.07074 | 8.84965 | 14.101 | 1.14026 | 0.07091 | 8.85074 | 85°57' |

CIRCULAR FUNCTIONS AND FACTORIALS

TABLE 15 (concluded).—Circular (Trigonometric) Functions

| RADIAN. | SINES. | | COSINES. | | TANGENTS | | COTANGENTS. | | DEGREES. |
|---------|---------|---------|----------|----------|----------|---------|-------------|----------|----------|
| | Nat. | Log | Nat. | Log | Nat. | Log. | Nat. | Log. | |
| 1.50 | 0.99749 | 9.99891 | 0.07074 | 8.84965 | 14.101 | 1.14926 | 0.07091 | 8.85074 | 85° 57' |
| .51 | .99815 | .99920 | .06076 | .78361 | 16.428 | .21559 | .06087 | .78441 | 86 31 |
| .52 | .99871 | .99944 | .05077 | .70365 | 19.070 | .29379 | .05084 | .70021 | 87 05 |
| .53 | .99917 | .99964 | .04079 | .61050 | 24.498 | .38714 | .04082 | .61086 | 87 40 |
| .54 | .99953 | .99979 | .03079 | .48843 | 32.461 | .51136 | .03081 | .48864 | 88 14 |
| 1.55 | 0.99978 | 9.99991 | 0.02079 | 8.31796 | 48.078 | 1.68195 | 0.02080 | 8.31805 | 88° 49' |
| .56 | 0.99994 | 9.99997 | .01080 | 8.03327 | 92.621 | 1.96671 | .01080 | 8.03329 | 89 23 |
| .57 | 1.00000 | 0.00000 | .00080 | 6.90109 | 1255.8 | 3.09891 | .00080 | 6.90109 | 89 57 |
| .58 | 0.99996 | 9.99998 | -.00020 | 7.96396n | 108.65 | 2.03603 | -.00020 | 7.96397n | 90 32 |
| .59 | 0.99982 | 9.99992 | -.01920 | 8.28336n | 52.067 | 1.71656 | -.01921 | 8.28344n | 91 06 |
| 1.60 | 0.99957 | 9.99981 | -0.02920 | 8.46538n | 34.233 | 1.53444 | -0.02921 | 8.46556n | 91° 40' |

90° = 1.570 7963 radians.

TABLE 16.—Logarithmic Factorials

Logarithms of the products 1.2.3. n , n from 1 to 100.

See Table 18 for Factorials 1 to 20.

See Table 33 for $\log \Gamma(n+1)$, values of n between 1 and 2.

| n . | $\log(n!)$ | n . | $\log(n!)$ | n . | $\log(n!)$ | n . | $\log(n!)$ |
|-------|------------|-------|------------|-------|------------|-------|------------|
| 1 | 0.000000 | 26 | 26.605619 | 51 | 66.190645 | 76 | 111.275425 |
| 2 | 0.301030 | 27 | 28.036983 | 52 | 67.906648 | 77 | 113.161916 |
| 3 | 0.778151 | 28 | 29.484141 | 53 | 69.630924 | 78 | 115.054011 |
| 4 | 1.380211 | 29 | 30.946539 | 54 | 71.363318 | 79 | 116.951638 |
| 5 | 2.079181 | 30 | 32.423660 | 55 | 73.103681 | 80 | 118.854728 |
| 6 | 2.857332 | 31 | 33.915022 | 56 | 74.851869 | 81 | 120.763213 |
| 7 | 3.702431 | 32 | 35.420172 | 57 | 76.607744 | 82 | 122.677027 |
| 8 | 4.605521 | 33 | 36.938686 | 58 | 78.371172 | 83 | 124.596105 |
| 9 | 5.559763 | 34 | 38.470165 | 59 | 80.142024 | 84 | 126.520384 |
| 10 | 6.559763 | 35 | 40.014233 | 60 | 81.920175 | 85 | 128.449803 |
| 11 | 7.601156 | 36 | 41.570535 | 61 | 83.705505 | 86 | 130.384301 |
| 12 | 8.680337 | 37 | 43.138737 | 62 | 85.497896 | 87 | 132.323821 |
| 13 | 9.794280 | 38 | 44.718520 | 63 | 87.297237 | 88 | 134.268303 |
| 14 | 10.940408 | 39 | 46.309585 | 64 | 89.103417 | 89 | 136.217693 |
| 15 | 12.116500 | 40 | 47.911645 | 65 | 90.916330 | 90 | 138.171936 |
| 16 | 13.320620 | 41 | 49.524429 | 66 | 92.735874 | 91 | 140.130977 |
| 17 | 14.551069 | 42 | 51.147678 | 67 | 94.561949 | 92 | 142.094765 |
| 18 | 15.800341 | 43 | 52.781147 | 68 | 96.394458 | 93 | 144.063248 |
| 19 | 17.085095 | 44 | 54.424599 | 69 | 98.233307 | 94 | 146.036376 |
| 20 | 18.386125 | 45 | 56.077812 | 70 | 100.078405 | 95 | 148.014099 |
| 21 | 19.708344 | 46 | 57.740570 | 71 | 101.929663 | 96 | 149.996371 |
| 22 | 21.050767 | 47 | 59.412668 | 72 | 103.786996 | 97 | 151.983142 |
| 23 | 22.412494 | 48 | 61.093909 | 73 | 105.650319 | 98 | 153.974368 |
| 24 | 23.792706 | 49 | 62.784105 | 74 | 107.519550 | 99 | 155.970004 |
| 25 | 25.190646 | 50 | 64.483075 | 75 | 109.394612 | 100 | 157.970004 |

TABLE 17
HYPERBOLIC FUNCTIONS

| u | sinh u | | cosh u | | tanh u | | coth u | | gd u |
|------|---------|---------|---------|---------|---------|---------|---------|---------|--------|
| | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | |
| 0.00 | 0.00000 | — π | 1.00000 | 0.00000 | 0.00000 | — π | π | π | 00°00' |
| .01 | .01000 | 8.00001 | .00005 | .00002 | .01000 | 7.99999 | 100.003 | 2.00001 | 0 34 |
| .02 | .02000 | .30106 | .00020 | .00009 | .02000 | 8.30007 | 50.007 | 1.69903 | 1 09 |
| .03 | .03000 | .47719 | .00045 | .00020 | .02999 | .47699 | 33.343 | 1.52301 | 1 43 |
| .04 | .04001 | .60218 | .00080 | .00035 | .03998 | .60183 | 25.013 | 1.39817 | 2 17 |
| 0.05 | 0.05002 | 8.69915 | 1.00125 | 0.00054 | 0.04996 | 8.69861 | 20.017 | 1.30139 | 2 52 |
| .06 | .06004 | .77841 | .00180 | .00078 | .05993 | .77763 | 16.687 | .22237 | 3 26 |
| .07 | .07006 | .84545 | .00245 | .00106 | .06989 | .84439 | 14.309 | .15561 | 4 00 |
| .08 | .08009 | .90355 | .00320 | .00139 | .07983 | .90216 | 12.527 | .09784 | 4 35 |
| .09 | .09012 | .95483 | .00405 | .00176 | .08976 | .95307 | 11.141 | .04693 | 5 09 |
| 0.10 | 0.10017 | 9.00072 | 1.00500 | 0.00217 | 0.09967 | 8.99856 | 10.0333 | 1.00144 | 5 43 |
| .11 | .11022 | .04227 | .00606 | .00262 | .10956 | 9.03965 | 9.1275 | 0.90035 | 6 17 |
| .12 | .12029 | .08022 | .00721 | .00312 | .11943 | .07710 | 8.3733 | .92290 | 6 52 |
| .13 | .13037 | .11517 | .00846 | .00366 | .12927 | .11151 | 7.7356 | .88849 | 7 26 |
| .14 | .14046 | .14755 | .00982 | .00424 | .13909 | .14330 | 7.1895 | .85670 | 8 00 |
| 0.15 | 0.15056 | 9.17772 | 1.01127 | 0.00487 | 0.14889 | 9.17285 | 6.7166 | 0.82715 | 8 34 |
| .16 | .16068 | .20597 | .01283 | .00551 | .15865 | .20044 | 6.3032 | .79956 | 9 08 |
| .17 | .17082 | .23254 | .01448 | .00625 | .16838 | .22629 | 5.9389 | .77371 | 9 42 |
| .18 | .18097 | .25762 | .01624 | .00700 | .17808 | .25062 | 5.6154 | .74938 | 10 15 |
| .19 | .19115 | .28136 | .01810 | .00779 | .18775 | .27357 | 5.3263 | .72643 | 10 49 |
| 0.20 | 0.20134 | 9.30392 | 1.02007 | 0.00863 | 0.19738 | 9.29529 | 5.0665 | 0.70471 | 11 23 |
| .21 | .21155 | .32541 | .02213 | .00951 | .20697 | .31590 | 4.8317 | .68410 | 11 57 |
| .22 | .22178 | .34592 | .02430 | .01043 | .21652 | .33549 | 4.6186 | .66451 | 12 30 |
| .23 | .23203 | .36555 | .02657 | .01139 | .22603 | .35416 | 4.4242 | .64584 | 13 04 |
| .24 | .24231 | .38437 | .02894 | .01239 | .23550 | .37198 | 4.2404 | .62802 | 13 37 |
| 0.25 | 0.25261 | 9.40245 | 1.03141 | 0.01343 | 0.24492 | 9.38902 | 4.0830 | 0.61098 | 14 11 |
| .26 | .26294 | .41986 | .03399 | .01452 | .25430 | .40534 | 3.9324 | .59466 | 14 44 |
| .27 | .27329 | .43663 | .03667 | .01504 | .26362 | .42099 | 3.7933 | .57901 | 15 17 |
| .28 | .28367 | .45282 | .03946 | .01681 | .27291 | .43601 | 3.6643 | .56399 | 15 50 |
| .29 | .29408 | .46847 | .04235 | .01801 | .28213 | .45046 | 3.5444 | .54954 | 16 23 |
| 0.30 | 0.30452 | 9.48362 | 1.04534 | 0.01926 | 0.29131 | 9.46436 | 3.4327 | 0.53564 | 16 56 |
| .31 | .31499 | .49830 | .04844 | .02054 | .30044 | .47775 | .3285 | .52225 | 17 29 |
| .32 | .32549 | .51254 | .05164 | .02187 | .30951 | .49067 | .2309 | .50933 | 18 02 |
| .33 | .33602 | .52637 | .05495 | .02323 | .31852 | .50314 | .1395 | .49686 | 18 34 |
| .34 | .34659 | .53981 | .05836 | .02463 | .32748 | .51518 | .0536 | .48482 | 19 07 |
| 0.35 | 0.35719 | 9.55290 | 1.06188 | 0.02607 | 0.33638 | 9.52682 | 2.9729 | 0.47318 | 19 39 |
| .36 | .36783 | .56364 | .06550 | .02755 | .34521 | .53809 | .8968 | .46191 | 20 12 |
| .37 | .37850 | .57807 | .06923 | .02907 | .35399 | .54899 | .8249 | .45101 | 20 44 |
| .38 | .38921 | .59019 | .07307 | .03063 | .36271 | .55956 | .7570 | .44044 | 21 16 |
| .39 | .39996 | .60202 | .07702 | .03222 | .37136 | .56980 | .6928 | .43020 | 21 48 |
| 0.40 | 0.41075 | 9.61358 | 1.08107 | 0.03385 | 0.37995 | 9.57973 | 2.6319 | 0.42027 | 22 20 |
| .41 | .42158 | .62488 | .08523 | .03552 | .38847 | .58936 | .5742 | .41064 | 22 52 |
| .42 | .43246 | .63594 | .08950 | .03723 | .39693 | .59871 | .5193 | .40120 | 23 23 |
| .43 | .44337 | .64677 | .09388 | .03897 | .40532 | .60780 | .4672 | .39220 | 23 55 |
| .44 | .45434 | .65738 | .09837 | .04075 | .41364 | .61663 | .4175 | .38337 | 24 26 |
| 0.45 | 0.46534 | 9.66777 | 1.10290 | 0.04256 | 0.42190 | 9.62521 | 2.3702 | 0.37479 | 24 57 |
| .46 | .47640 | .67797 | .10768 | .04441 | .43008 | .63355 | .3251 | .36645 | 25 28 |
| .47 | .48750 | .68797 | .11250 | .04630 | .43820 | .64167 | .2821 | .35833 | 25 59 |
| .48 | .49865 | .69779 | .11743 | .04822 | .44624 | .64957 | .2400 | .35043 | 26 30 |
| .49 | .50984 | .70744 | .12247 | .05018 | .45422 | .65726 | .2016 | .34274 | 27 01 |
| 0.50 | 0.52110 | 9.71692 | 1.12763 | 0.05217 | 0.46212 | 9.66475 | 2.1640 | 0.33525 | 27 31 |

| u | sinh u | | cosh u | | tanh u | | coth u | | gd u |
|------|---------|---------|---------|---------|---------|---------|--------|---------|--------|
| | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | |
| 0.50 | 0.52110 | 9.71692 | 1.12763 | 0.05217 | 0.46212 | 9.66475 | 2.1640 | 0.33525 | 27°31' |
| .51 | .53240 | .72624 | .13289 | .05419 | .46995 | .67205 | .1279 | .32795 | 28 02 |
| .52 | .54375 | .73540 | .13827 | .05625 | .47770 | .67916 | .0934 | .32084 | 28 32 |
| .53 | .55516 | .74442 | .14377 | .05834 | .48538 | .68608 | .0602 | .31392 | 29 02 |
| .54 | .56663 | .75330 | .14938 | .06046 | .49299 | .69284 | .0284 | .30716 | 29 32 |
| 0.55 | 0.57815 | 9.76204 | 1.15510 | 0.06262 | 0.50052 | 9.69942 | 1.9979 | 0.30058 | 30 02 |
| .56 | .58973 | .77065 | .16094 | .06481 | .50798 | .70584 | .9686 | .29416 | 30 32 |
| .57 | .60137 | .77914 | .16690 | .06703 | .51536 | .71211 | .9404 | .28789 | 31 01 |
| .58 | .61307 | .78751 | .17297 | .06929 | .52267 | .71822 | .9133 | .28178 | 31 31 |
| .59 | .62483 | .79576 | .17916 | .07157 | .52990 | .72419 | .8872 | .27581 | 32 00 |
| 0.60 | 0.63665 | 9.80390 | 1.18547 | 0.07389 | 0.53705 | 9.73001 | 1.8620 | 0.26999 | 32 29 |
| .61 | .64854 | .81194 | .19189 | .07624 | .54413 | .73570 | .8378 | .26430 | 32 58 |
| .62 | .66049 | .81987 | .19844 | .07861 | .55113 | .74125 | .8145 | .25875 | 33 27 |
| .63 | .67251 | .82770 | .20510 | .08102 | .55805 | .74667 | .7919 | .25333 | 33 55 |
| .64 | .68459 | .83543 | .21189 | .08346 | .56490 | .75197 | .7702 | .24803 | 34 24 |
| 0.65 | 0.69675 | 9.84308 | 1.21879 | 0.08593 | 0.57167 | 9.75715 | 1.7493 | 0.24285 | 34 52 |
| .66 | .70897 | .85063 | .22582 | .08843 | .57836 | .76220 | .7290 | .23780 | 35 20 |
| .67 | .72126 | .85809 | .23297 | .09095 | .58498 | .76714 | .7095 | .23286 | 35 48 |
| .68 | .73363 | .86548 | .24025 | .09351 | .59152 | .77197 | .6906 | .22803 | 36 16 |
| .69 | .74607 | .87278 | .24765 | .09609 | .59798 | .77669 | .6723 | .22331 | 36 44 |
| 0.70 | 0.75858 | 9.88000 | 1.25517 | 0.09870 | 0.60437 | 9.78130 | 1.6546 | 0.21870 | 37 11 |
| .71 | .77117 | .88715 | .26282 | .10134 | .61068 | .78581 | .6375 | .21419 | 37 38 |
| .72 | .78384 | .89423 | .27059 | .10401 | .61691 | .79022 | .6210 | .20978 | 38 05 |
| .73 | .79659 | .90123 | .27849 | .10670 | .62307 | .79453 | .6050 | .20547 | 38 32 |
| .74 | .80941 | .90817 | .28652 | .10942 | .62915 | .79875 | .5895 | .20125 | 38 59 |
| 0.75 | 0.82232 | 9.91504 | 1.29468 | 0.11216 | 0.63515 | 9.80288 | 1.5744 | 0.19712 | 39 26 |
| .76 | .83530 | .92185 | .30297 | .11493 | .64108 | .80691 | .5599 | .19309 | 39 52 |
| .77 | .84838 | .92859 | .31139 | .11773 | .64693 | .81086 | .5458 | .18914 | 40 19 |
| .78 | .86153 | .93527 | .31994 | .12055 | .65271 | .81472 | .5321 | .18528 | 40 45 |
| .79 | .87478 | .94190 | .32862 | .12340 | .65841 | .81850 | .5188 | .18150 | 41 11 |
| 0.80 | 0.88811 | 9.94846 | 1.33743 | 0.12627 | 0.66404 | 9.82219 | 1.5059 | 0.17781 | 41 37 |
| .81 | .90152 | .95498 | .34638 | .12917 | .66959 | .82581 | .4935 | .17419 | 42 02 |
| .82 | .91503 | .96144 | .35547 | .13209 | .67507 | .82935 | .4813 | .17065 | 42 28 |
| .83 | .92863 | .96784 | .36468 | .13503 | .68048 | .83281 | .4696 | .16719 | 42 53 |
| .84 | .94233 | .97420 | .37404 | .13800 | .68581 | .83620 | .4581 | .16380 | 43 18 |
| 0.85 | 0.95612 | 9.98051 | 1.38353 | 0.14099 | 0.69107 | 9.83952 | 1.4470 | 0.16048 | 43 43 |
| .86 | .97000 | .98677 | .39316 | .14400 | .69626 | .84277 | .4362 | .15723 | 44 08 |
| .87 | .98398 | .99299 | .40293 | .14704 | .70137 | .84595 | .4258 | .15405 | 44 32 |
| .88 | .99806 | .99916 | .41284 | .15009 | .70642 | .84906 | .4156 | .15094 | 44 57 |
| .89 | 1.01224 | 0.00528 | .42289 | .15317 | .71139 | .85211 | .4057 | .14789 | 45 21 |
| 0.90 | 1.02652 | 0.01137 | 1.43309 | 0.15627 | 0.71630 | 9.85509 | 1.3961 | 0.14491 | 45 45 |
| .91 | .04090 | .01741 | .44342 | .15939 | .72113 | .85801 | .3867 | .14199 | 46 09 |
| .92 | .05539 | .02341 | .45390 | .16254 | .72590 | .86088 | .3776 | .13912 | 46 33 |
| .93 | .06998 | .02937 | .46453 | .16570 | .73059 | .86368 | .3687 | .13632 | 46 56 |
| .94 | .08468 | .03530 | .47530 | .16888 | .73522 | .86642 | .3601 | .13358 | 47 20 |
| 0.95 | 1.09948 | 0.04119 | 1.48623 | 0.17208 | 0.73978 | 9.86910 | 1.3517 | 0.13090 | 47 43 |
| .96 | .11440 | .04704 | .49729 | .17531 | .74428 | .87173 | .3436 | .12827 | 48 06 |
| .97 | .12943 | .05286 | .50851 | .17855 | .74870 | .87431 | .3356 | .12569 | 48 29 |
| .98 | .14457 | .05864 | .51988 | .18181 | .75307 | .87683 | .3279 | .12317 | 48 51 |
| .99 | .15983 | .06439 | .53141 | .18509 | .75736 | .87930 | .3204 | .12070 | 49 14 |
| 1.00 | 1.17520 | 0.07011 | 1.54308 | 0.18839 | 0.76159 | 9.88172 | 1.3130 | 0.11828 | 49 36 |

HYPERBOLIC FUNCTIONS

| u | sinh u | | cosh u | | tanh u | | coth u | | gd u |
|------|---------|---------|---------|---------|---------|---------|--------|---------|---------|
| | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | |
| 1.00 | 1.17520 | 0.07011 | 1.54308 | 0.18839 | 0.76159 | 9.88172 | 1.3130 | 0.11828 | 49° 36' |
| .01 | .19069 | .07580 | .55491 | .19171 | .76576 | .88409 | .3059 | .11591 | 49 58 |
| .02 | .20630 | .08146 | .56689 | .19504 | .76987 | .88642 | .2989 | .11358 | 50 21 |
| .03 | .22203 | .08708 | .57904 | .19839 | .77391 | .88809 | .2921 | .11131 | 50 42 |
| .04 | .23788 | .09268 | .59134 | .20176 | .77789 | .88992 | .2855 | .10908 | 51 04 |
| 1.05 | 1.25386 | 0.09825 | 1.60379 | 0.20515 | 0.78181 | 9.89310 | 1.2791 | 0.10690 | 51 26 |
| .06 | .26996 | .10379 | .61641 | .20855 | .78566 | .89524 | .2728 | .10476 | 51 47 |
| .07 | .28619 | .10930 | .62919 | .21197 | .78946 | .89733 | .2667 | .10267 | 52 08 |
| .08 | .30254 | .11479 | .64214 | .21541 | .79320 | .89938 | .2607 | .10062 | 52 29 |
| .09 | .31903 | .12025 | .65525 | .21886 | .79688 | .90139 | .2549 | .09861 | 52 50 |
| 1.10 | 1.33565 | 0.12569 | 1.66852 | 0.22233 | 0.80050 | 9.90336 | 1.2492 | 0.09664 | 53 11 |
| .11 | .35240 | .13111 | .68196 | .22582 | .80406 | .90529 | .2437 | .09471 | 53 31 |
| .12 | .36929 | .13649 | .69557 | .22931 | .80757 | .90718 | .2383 | .09282 | 53 52 |
| .13 | .38631 | .14186 | .70934 | .23283 | .81102 | .90903 | .2330 | .09097 | 54 12 |
| .14 | .40347 | .14720 | .72329 | .23636 | .81441 | .91085 | .2279 | .08915 | 54 32 |
| 1.15 | 1.42078 | 0.15253 | 1.73741 | 0.23990 | 0.81775 | 9.91262 | 1.2229 | 0.08738 | 54 52 |
| .16 | .43822 | .15783 | .75171 | .24346 | .82104 | .91436 | .2180 | .08564 | 55 11 |
| .17 | .45581 | .16311 | .76618 | .24703 | .82427 | .91607 | .2132 | .08393 | 55 31 |
| .18 | .47355 | .16836 | .78083 | .25062 | .82745 | .91774 | .2085 | .08226 | 55 50 |
| .19 | .49143 | .17360 | .79565 | .25422 | .83058 | .91938 | .2040 | .08062 | 56 09 |
| 1.20 | 1.50946 | 0.17882 | 1.81066 | 0.25784 | 0.83365 | 9.92099 | 1.1995 | 0.07901 | 56 29 |
| .21 | .52764 | .18402 | .82584 | .26146 | .83668 | .92256 | .1952 | .07744 | 56 47 |
| .22 | .54598 | .18920 | .84121 | .26510 | .83965 | .92410 | .1910 | .07590 | 57 06 |
| .23 | .56447 | .19437 | .85676 | .26876 | .84258 | .92561 | .1868 | .07439 | 57 25 |
| .24 | .58311 | .19951 | .87250 | .27242 | .84546 | .92709 | .1828 | .07291 | 57 43 |
| 1.25 | 1.60192 | 0.20464 | 1.88842 | 0.27610 | 0.84828 | 9.92854 | 1.1789 | 0.07146 | 58 02 |
| .26 | .62088 | .20975 | .90454 | .27979 | .85106 | .92996 | .1750 | .07004 | 58 20 |
| .27 | .64001 | .21485 | .92084 | .28349 | .85380 | .93135 | .1712 | .06865 | 58 38 |
| .28 | .65930 | .21993 | .93734 | .28721 | .85648 | .93272 | .1676 | .06728 | 58 55 |
| .29 | .67876 | .22499 | .95403 | .29093 | .85913 | .93406 | .1640 | .06594 | 59 13 |
| 1.30 | 1.69838 | 0.23004 | 1.97091 | 0.29467 | 0.86172 | 9.93537 | 1.1605 | 0.06463 | 59 31 |
| .31 | .71818 | .23507 | .98800 | .29842 | .86428 | .93665 | .1570 | .06335 | 59 48 |
| .32 | .73814 | .24009 | 2.00528 | .30217 | .86678 | .93791 | .1537 | .06209 | 60 05 |
| .33 | .75828 | .24509 | .02276 | .30594 | .86925 | .93914 | .1504 | .06086 | 60 22 |
| .34 | .77860 | .25008 | .04044 | .30972 | .87167 | .94035 | .1472 | .05965 | 60 39 |
| 1.35 | 1.79909 | 0.25505 | 2.05833 | 0.31352 | 0.87405 | 9.94154 | 1.1441 | 0.05846 | 60 56 |
| .36 | .81977 | .26002 | .07643 | .31732 | .87639 | .94270 | .1410 | .05730 | 61 13 |
| .37 | .84062 | .26496 | .09473 | .32113 | .87869 | .94384 | .1381 | .05616 | 61 29 |
| .38 | .86166 | .26990 | .11324 | .32495 | .88095 | .94495 | .1351 | .05505 | 61 45 |
| .39 | .88289 | .27482 | .13196 | .32878 | .88317 | .94604 | .1323 | .05396 | 62 02 |
| 1.40 | 1.90430 | 0.27974 | 2.15090 | 0.33262 | 0.88535 | 9.94712 | 1.1295 | 0.05288 | 62 18 |
| .41 | .92591 | .28464 | .17005 | .33647 | .88749 | .94817 | .1268 | .05183 | 62 34 |
| .42 | .94770 | .28952 | .18942 | .34033 | .88960 | .94919 | .1241 | .05081 | 62 49 |
| .43 | .96970 | .29440 | .20900 | .34420 | .89167 | .95020 | .1215 | .04980 | 63 05 |
| .44 | .99188 | .29926 | .22881 | .34807 | .89370 | .95119 | .1189 | .04881 | 63 20 |
| 1.45 | 2.01427 | 0.30412 | 2.24884 | 0.35196 | 0.89569 | 9.95216 | 1.1165 | 0.04784 | 63 36 |
| .46 | .03686 | .30896 | .26910 | .35585 | .89765 | .95311 | .1140 | .04689 | 63 51 |
| .47 | .05965 | .31379 | .28958 | .35976 | .89958 | .95404 | .1116 | .04596 | 64 06 |
| .48 | .08265 | .31862 | .31029 | .36367 | .90147 | .95495 | .1093 | .04505 | 64 21 |
| .49 | .10586 | .32343 | .33123 | .36759 | .90332 | .95584 | .1070 | .04416 | 64 36 |
| 1.50 | 2.12928 | 0.32823 | 2.35241 | 0.37151 | 0.90515 | 9.95672 | 1.1048 | 0.04328 | 64 51 |

TABLE 17 (continued)
HYPERBOLIC FUNCTIONS

| u | sinh u | | cosh u | | tanh u | | coth u | | gd u |
|------|---------|---------|---------|---------|---------|---------|--------|---------|---------|
| | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | |
| 1.50 | 2.12928 | 0.32823 | 2.35241 | 0.37151 | 0.90515 | 9.95672 | 1.1048 | 0.04328 | 64° 51' |
| .51 | .15291 | .33303 | .37382 | .37545 | .90694 | .95758 | .1026 | .04242 | 65 05 |
| .52 | .17676 | .33781 | .39547 | .37939 | .90870 | .95842 | .1005 | .04158 | 65 20 |
| .53 | .20082 | .34258 | .41736 | .38334 | .91042 | .95924 | .0984 | .04076 | 65 34 |
| .54 | .22510 | .34735 | .43949 | .38730 | .91212 | .96005 | .0963 | .03995 | 65 48 |
| 1.55 | 2.24961 | 0.35211 | 2.46186 | 0.39126 | 0.91379 | 9.96084 | 1.0943 | 0.03916 | 66 02 |
| .50 | .27434 | .35686 | .48448 | .39524 | .91542 | .96162 | .0924 | .03838 | 66 16 |
| .57 | .29930 | .36160 | .50735 | .39921 | .91703 | .96238 | .0905 | .03762 | 66 30 |
| .58 | .32449 | .36633 | .53047 | .40320 | .91860 | .96313 | .0886 | .03687 | 66 43 |
| .59 | .34991 | .37105 | .55384 | .40719 | .92015 | .96386 | .0868 | .03614 | 66 57 |
| 1.60 | 2.37557 | 0.37577 | 2.57746 | 0.41119 | 0.92167 | 9.96457 | 1.0850 | 0.03543 | 67 10 |
| .61 | .40146 | .38048 | .60135 | .41520 | .92316 | .96528 | .0832 | .03472 | 67 24 |
| .62 | .42760 | .38518 | .62549 | .41921 | .92462 | .96597 | .0815 | .03403 | 67 37 |
| .63 | .45397 | .38987 | .64990 | .42323 | .92606 | .96664 | .0798 | .03336 | 67 50 |
| .64 | .48059 | .39456 | .67457 | .42725 | .92747 | .96730 | .0782 | .03270 | 68 03 |
| 1.65 | 2.50746 | 0.39923 | 2.69951 | 0.43129 | 0.92886 | 9.96795 | 1.0766 | 0.03205 | 68 15 |
| .66 | .53459 | .40391 | .72472 | .43532 | .93022 | .96858 | .0750 | .03142 | 68 28 |
| .67 | .56196 | .40857 | .75021 | .43937 | .93155 | .96921 | .0735 | .03079 | 68 41 |
| .68 | .58959 | .41323 | .77596 | .44341 | .93286 | .96982 | .0720 | .03018 | 68 53 |
| .69 | .61748 | .41788 | .80200 | .44747 | .93415 | .97042 | .0705 | .02958 | 69 05 |
| 1.70 | 2.64563 | 0.42253 | 2.82832 | 0.45153 | 0.93541 | 9.97100 | 1.0691 | 0.02900 | 69 18 |
| .71 | .67405 | .42717 | .85491 | .45559 | .93665 | .97158 | .0676 | .02842 | 69 30 |
| .72 | .70273 | .43180 | .88180 | .45966 | .93786 | .97214 | .0663 | .02786 | 69 42 |
| .73 | .73168 | .43643 | .90897 | .46374 | .93906 | .97269 | .0649 | .02731 | 69 54 |
| .74 | .76091 | .44105 | .93643 | .46782 | .94023 | .97323 | .0636 | .02677 | 70 05 |
| 1.75 | 2.79041 | 0.44567 | 2.96419 | 0.47191 | 0.94138 | 9.97376 | 1.0623 | 0.02624 | 70 17 |
| .76 | .82020 | .45028 | .99224 | .47600 | .94250 | .97428 | .0610 | .02572 | 70 29 |
| .77 | .85026 | .45488 | 3.02059 | .48009 | .94361 | .97479 | .0598 | .02521 | 70 40 |
| .78 | .88061 | .45948 | .04925 | .48419 | .94470 | .97529 | .0585 | .02471 | 70 51 |
| .79 | .91125 | .46408 | .07821 | .48830 | .94576 | .97578 | .0574 | .02422 | 71 03 |
| 1.80 | 2.94217 | 0.46867 | 3.10747 | 0.49241 | 0.94681 | 9.97626 | 1.0562 | 0.02374 | 71 14 |
| .81 | .97340 | .47325 | .13705 | .49652 | .94783 | .97673 | .0550 | .02327 | 71 25 |
| .82 | 3.00492 | .47783 | .16094 | .50064 | .94884 | .97719 | .0539 | .02281 | 71 36 |
| .83 | .03674 | .48241 | .19715 | .50476 | .94983 | .97764 | .0528 | .02236 | 71 46 |
| .84 | .06886 | .48698 | .22768 | .50889 | .95080 | .97809 | .0518 | .02191 | 71 57 |
| 1.85 | 3.10129 | 0.49154 | 3.25853 | 0.51302 | 0.95175 | 9.97852 | 1.0507 | 0.02148 | 72 08 |
| .86 | .13403 | .49610 | .28970 | .51716 | .95268 | .97895 | .0497 | .02105 | 72 18 |
| .87 | .16709 | .50066 | .32121 | .52130 | .95359 | .97936 | .0487 | .02064 | 72 29 |
| .88 | .20046 | .50521 | .35305 | .52544 | .95449 | .97977 | .0477 | .02023 | 72 39 |
| .89 | .23415 | .50976 | .38522 | .52959 | .95537 | .98017 | .0467 | .01983 | 72 49 |
| 1.90 | 3.26816 | 0.51430 | 3.41773 | 0.53374 | 0.95624 | 9.98057 | 1.0458 | 0.01943 | 72 59 |
| .91 | .30250 | .51884 | .45058 | .53789 | .95709 | .98095 | .0448 | .01905 | 73 09 |
| .92 | .33718 | .52338 | .48378 | .54205 | .95792 | .98133 | .0439 | .01867 | 73 19 |
| .93 | .37218 | .52791 | .51733 | .54621 | .95873 | .98170 | .0430 | .01830 | 73 29 |
| .94 | .40752 | .53244 | .55123 | .55038 | .95953 | .98206 | .0422 | .01794 | 73 39 |
| 1.95 | 3.44321 | 0.53696 | 3.58548 | 0.55455 | 0.96032 | 9.98242 | 1.0413 | 0.01758 | 73 48 |
| .96 | .47923 | .54148 | .62009 | .55872 | .96109 | .98276 | .0405 | .01724 | 73 58 |
| .97 | .51561 | .54600 | .65507 | .56290 | .96185 | .98311 | .0397 | .01689 | 74 07 |
| .98 | .55234 | .55051 | .69041 | .56707 | .96259 | .98344 | .0389 | .01656 | 74 17 |
| .99 | .58942 | .55502 | .72611 | .57126 | .96331 | .98377 | .0381 | .01623 | 74 26 |
| 2.00 | 3.62686 | 0.55953 | 3.76220 | 0.57544 | 0.96403 | 9.98409 | 1.0373 | 0.01591 | 74 35 |

TABLE 17 (continued)
HYPERBOLIC FUNCTIONS

| u | sinh u | | cosh u | | tanh u | | coth u | | gd u |
|------|---------|---------|---------|---------|---------|---------|--------|---------|---------|
| | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | |
| 2.00 | 3.62686 | 0.55953 | 3.76220 | 0.57544 | 0.96403 | 9.98409 | 1.0373 | 0.01591 | 74° 35' |
| .01 | .66466 | .56403 | .79865 | .57963 | .96473 | .98440 | .0366 | .01560 | 74 44 |
| .02 | .70283 | .56853 | .83549 | .58382 | .96541 | .98471 | .0358 | .01529 | 74 53 |
| .03 | .74138 | .57303 | .87271 | .58802 | .96609 | .98502 | .0351 | .01498 | 75 02 |
| .04 | .78029 | .57753 | .91032 | .59221 | .96675 | .98531 | .0344 | .01469 | 75 11 |
| 2.05 | 3.81958 | 0.58202 | 3.94832 | 0.59641 | 0.96740 | 9.98560 | 1.0337 | 0.01440 | 75 20 |
| .06 | .85926 | .58650 | .98671 | .60061 | .96803 | .98589 | .0330 | .01411 | 75 28 |
| .07 | .89932 | .59099 | 4.02550 | .60482 | .96865 | .98617 | .0324 | .01383 | 75 37 |
| .08 | .93977 | .59547 | .60470 | .60903 | .96926 | .98644 | .0317 | .01356 | 75 45 |
| .09 | .98061 | .59995 | .10430 | .61324 | .96986 | .98671 | .0311 | .01329 | 75 54 |
| 2.10 | 4.02186 | 0.60443 | 4.14431 | 0.61745 | 0.97045 | 9.98697 | 1.0304 | 0.01303 | 76 02 |
| .11 | .06350 | .60890 | .18474 | .62167 | .97103 | .98723 | .0298 | .01277 | 76 10 |
| .12 | .10555 | .61337 | .22558 | .62589 | .97159 | .98748 | .0292 | .01252 | 76 19 |
| .13 | .14801 | .61784 | .26685 | .63011 | .97215 | .98773 | .0286 | .01227 | 76 27 |
| .14 | .19089 | .62231 | .30855 | .63433 | .97269 | .98798 | .0281 | .01202 | 76 35 |
| 2.15 | 4.23419 | 0.62677 | 4.35067 | 0.63856 | 0.97323 | 9.98821 | 1.0275 | 0.01179 | 76 43 |
| .16 | .27791 | .63123 | .39323 | .64278 | .97375 | .98845 | .0270 | .01155 | 76 51 |
| .17 | .32205 | .63569 | .43623 | .64701 | .97426 | .98868 | .0264 | .01132 | 76 58 |
| .18 | .36663 | .64015 | .47967 | .65125 | .97477 | .98890 | .0259 | .01110 | 77 06 |
| .19 | .41165 | .64460 | .52356 | .65548 | .97526 | .98912 | .0254 | .01088 | 77 14 |
| 2.20 | 4.45711 | 0.64905 | 4.56791 | 0.65972 | 0.97574 | 9.98934 | 1.0249 | 0.01066 | 77 21 |
| .21 | .50301 | .65350 | .61271 | .66396 | .97622 | .98955 | .0244 | .01045 | 77 29 |
| .22 | .54936 | .65795 | .65797 | .66820 | .97668 | .98975 | .0239 | .01025 | 77 36 |
| .23 | .59617 | .66240 | .70370 | .67244 | .97714 | .98996 | .0234 | .01004 | 77 44 |
| .24 | .64344 | .66684 | .74989 | .67668 | .97759 | .99016 | .0229 | .00984 | 77 51 |
| 2.25 | 4.69117 | 0.67128 | 4.79657 | 0.68093 | 0.97803 | 9.99035 | 1.0225 | 0.00965 | 77 58 |
| .26 | .73937 | .67572 | .84372 | .68518 | .97846 | .99054 | .0220 | .00946 | 78 05 |
| .27 | .78804 | .68016 | .89136 | .68943 | .97888 | .99073 | .0216 | .00927 | 78 12 |
| .28 | .83720 | .68459 | .93948 | .69368 | .97929 | .99091 | .0211 | .00909 | 78 19 |
| .29 | .88684 | .68903 | .98810 | .69794 | .97970 | .99109 | .0207 | .00891 | 78 26 |
| 2.30 | 4.93696 | 0.69346 | 5.03722 | 0.70219 | 0.98010 | 9.99127 | 1.0203 | 0.00873 | 78 33 |
| .31 | .98758 | .69789 | .08684 | .70645 | .98049 | .99144 | .0199 | .00856 | 78 40 |
| .32 | 5.03870 | .70232 | .13697 | .71071 | .98087 | .99161 | .0195 | .00839 | 78 46 |
| .33 | .09032 | .70675 | .18762 | .71497 | .98124 | .99178 | .0191 | .00822 | 78 53 |
| .34 | .14245 | .71117 | .23878 | .71923 | .98161 | .99194 | .0187 | .00806 | 79 00 |
| 2.35 | 5.19510 | 0.71559 | 5.29047 | 0.72349 | 0.98197 | 9.99210 | 1.0184 | 0.00790 | 79 06 |
| .36 | .24827 | .72002 | .34269 | .72776 | .98233 | .99226 | .0180 | .00774 | 79 13 |
| .37 | .30196 | .72444 | .39544 | .73203 | .98267 | .99241 | .0176 | .00759 | 79 19 |
| .38 | .35618 | .72885 | .44873 | .73630 | .98301 | .99256 | .0173 | .00744 | 79 25 |
| .39 | .41093 | .73327 | .50256 | .74056 | .98335 | .99271 | .0169 | .00729 | 79 32 |
| 2.40 | 5.46623 | 0.73769 | 5.55695 | 0.74484 | 0.98367 | 9.99285 | 1.0166 | 0.00715 | 79 38 |
| .41 | .52207 | .74210 | .61189 | .74911 | .98400 | .99299 | .0163 | .00701 | 79 44 |
| .42 | .57847 | .74652 | .66739 | .75338 | .98431 | .99313 | .0159 | .00687 | 79 50 |
| .43 | .63542 | .75093 | .72346 | .75766 | .98462 | .99327 | .0156 | .00673 | 79 56 |
| .44 | .69294 | .75534 | .78010 | .76194 | .98492 | .99340 | .0153 | .00660 | 80 02 |
| 2.45 | 5.75103 | 0.75975 | 5.83732 | 0.76621 | 0.98522 | 9.99353 | 1.0150 | 0.00647 | 80 08 |
| .46 | .80069 | .76415 | .89512 | .77049 | .98551 | .99366 | .0147 | .00634 | 80 14 |
| .47 | .86803 | .76856 | .95352 | .77477 | .98579 | .99379 | .0144 | .00621 | 80 20 |
| .48 | .92876 | .77296 | 6.01250 | .77906 | .98607 | .99391 | .0141 | .00609 | 80 26 |
| .49 | .98918 | .77737 | .07209 | .78334 | .98635 | .99403 | .0138 | .00597 | 80 31 |
| 2.50 | 6.05020 | 0.78177 | 6.13229 | 0.78762 | 0.98661 | 9.99415 | 1.0136 | 0.00585 | 80 37 |

TABLE 17 (continued)
HYPERBOLIC FUNCTIONS

| u | sinh u | | cosh u | | tanh u | | coth u | | gd u |
|------|----------|---------|----------|---------|---------|---------|--------|---------|---------|
| | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | |
| 2.50 | 6.05020 | 0.78177 | 6.13229 | 0.78762 | 0.98661 | 9.99415 | 1.0136 | 0.00585 | 80° 37' |
| .51 | .11183 | .78617 | .19310 | .79191 | .98688 | .99426 | .0133 | .00574 | 80 42 |
| .52 | .17407 | .79057 | .25453 | .79619 | .98714 | .99438 | .0130 | .00562 | 80 48 |
| .53 | .23692 | .79497 | .31658 | .80048 | .98739 | .99449 | .0128 | .00551 | 80 53 |
| .54 | .30040 | .79937 | .37927 | .80477 | .98764 | .99460 | .0125 | .00540 | 80 59 |
| 2.55 | 6.36451 | 0.80377 | 6.44259 | 0.80906 | 0.98788 | 9.99470 | 1.0123 | 0.00530 | 81 04 |
| .56 | .42926 | .80816 | .50650 | .81335 | .98812 | .99481 | .0120 | .00519 | 81 10 |
| .57 | .49464 | .81256 | .57118 | .81764 | .98835 | .99491 | .0118 | .00509 | 81 15 |
| .58 | .56068 | .81695 | .63646 | .82194 | .98858 | .99501 | .0115 | .00499 | 81 20 |
| .59 | .62738 | .82134 | .70240 | .82623 | .98881 | .99511 | .0113 | .00489 | 81 25 |
| 2.60 | 6.69473 | 0.82573 | 6.76901 | 0.83052 | 0.98903 | 9.99521 | 1.0111 | 0.00479 | 81 30 |
| .61 | .76276 | .83012 | .83629 | .83482 | .98924 | .99530 | .0109 | .00470 | 81 35 |
| .62 | .83146 | .83451 | .90426 | .83912 | .98946 | .99540 | .0107 | .00460 | 81 40 |
| .63 | .90085 | .83890 | .97292 | .84341 | .98966 | .99549 | .0104 | .00451 | 81 45 |
| .64 | .97092 | .84329 | 7.04228 | .84771 | .98987 | .99558 | .0102 | .00442 | 81 50 |
| 2.65 | 7.04169 | 0.84768 | 7.11234 | 0.85201 | 0.99007 | 9.99566 | 1.0100 | 0.00434 | 81 55 |
| .66 | .11317 | .85206 | .18312 | .85631 | .99026 | .99575 | .0098 | .00425 | 82 00 |
| .67 | .18536 | .85645 | .25461 | .86061 | .99045 | .99583 | .0096 | .00417 | 82 05 |
| .68 | .25827 | .86083 | .32683 | .86492 | .99064 | .99592 | .0094 | .00408 | 82 09 |
| .69 | .33190 | .86522 | .39978 | .86922 | .99083 | .99600 | .0093 | .00400 | 82 14 |
| 2.70 | 7.40626 | 0.86960 | 7.47347 | 0.87352 | 0.99101 | 9.99608 | 1.0091 | 0.00392 | 82 19 |
| .71 | .48137 | .87398 | .54791 | .87783 | .99118 | .99615 | .0089 | .00385 | 82 23 |
| .72 | .55722 | .87836 | .62310 | .88213 | .99136 | .99623 | .0087 | .00377 | 82 28 |
| .73 | .63383 | .88274 | .69905 | .88644 | .99153 | .99631 | .0085 | .00369 | 82 32 |
| .74 | .71121 | .88712 | .77578 | .89074 | .99170 | .99638 | .0084 | .00362 | 82 37 |
| 2.75 | 7.78935 | 0.89150 | 7.85328 | 0.89505 | 0.99186 | 9.99645 | 1.0082 | 0.00355 | 82 41 |
| .76 | .86828 | .89588 | .93157 | .89936 | .99202 | .99652 | .0080 | .00348 | 82 45 |
| .77 | .94799 | .90026 | 8.01065 | .90367 | .99218 | .99659 | .0079 | .00341 | 82 50 |
| .78 | 8.02849 | .90463 | .09053 | .90798 | .99233 | .99666 | .0077 | .00334 | 82 54 |
| .79 | .10980 | .90901 | .17122 | .91229 | .99248 | .99672 | .0076 | .00328 | 82 58 |
| 2.80 | 8.19192 | 0.91339 | 8.25273 | 0.91660 | 0.99263 | 9.99679 | 1.0074 | 0.00321 | 83 02 |
| .81 | .27486 | .91776 | .33506 | .92091 | .99278 | .99685 | .0073 | .00315 | 83 07 |
| .82 | .35862 | .92213 | .41823 | .92522 | .99292 | .99691 | .0071 | .00309 | 83 11 |
| .83 | .44322 | .92651 | .50224 | .92953 | .99306 | .99698 | .0070 | .00302 | 83 15 |
| .84 | .52867 | .93088 | .58710 | .93385 | .99320 | .99704 | .0069 | .00296 | 83 19 |
| 2.85 | 8.61497 | 0.93525 | 8.67281 | 0.93816 | 0.99333 | 9.99709 | 1.0067 | 0.00291 | 83 23 |
| .86 | .70213 | .93963 | .75940 | .94247 | .99346 | .99715 | .0066 | .00285 | 83 27 |
| .87 | .79016 | .94400 | .84686 | .94679 | .99359 | .99721 | .0065 | .00279 | 83 31 |
| .88 | .87907 | .94837 | .93520 | .95110 | .99372 | .99726 | .0063 | .00274 | 83 34 |
| .89 | .96887 | .95274 | 9.02444 | .95542 | .99384 | .99732 | .0062 | .00268 | 83 38 |
| 2.90 | 9.05956 | 0.95711 | 9.11458 | 0.95974 | 0.99396 | 9.99737 | 1.0061 | 0.00263 | 83 42 |
| .91 | .15116 | .96148 | .20564 | .96405 | .99408 | .99742 | .0060 | .00258 | 83 46 |
| .92 | .24368 | .96584 | .29761 | .96837 | .99420 | .99747 | .0058 | .00253 | 83 50 |
| .93 | .33712 | .97021 | .39051 | .97269 | .99431 | .99752 | .0057 | .00248 | 83 53 |
| .94 | .43149 | .97458 | .48436 | .97701 | .99443 | .99757 | .0056 | .00243 | 83 57 |
| 2.95 | 9.52681 | 0.97895 | 9.57915 | 0.98133 | 0.99454 | 9.99762 | 1.0055 | 0.00238 | 84 00 |
| .96 | .62308 | .98331 | .67490 | .98565 | .99464 | .99767 | .0054 | .00233 | 84 04 |
| .97 | .72031 | .98768 | .77161 | .98997 | .99475 | .99771 | .0053 | .00229 | 84 08 |
| .98 | .81851 | .99205 | .86930 | .99429 | .99485 | .99776 | .0052 | .00224 | 84 11 |
| .99 | .91770 | .99641 | .96798 | .99861 | .99496 | .99780 | .0051 | .00220 | 84 15 |
| 3.00 | 10.01787 | 1.00078 | 10.06766 | 1.00293 | 0.99505 | 9.99785 | 1.0050 | 0.00215 | 84 18 |

TABLE 17 (concluded).—HYPERBOLIC FUNCTIONS

| u | sinh u | | cosh u | | tanh u | | coth u | | gd u |
|-----|---------|---------|---------|---------|---------|---------|--------|---------|---------|
| | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. | |
| 3.0 | 10.0179 | 1.00078 | 10.0677 | 1.00293 | 0.99505 | 9.99785 | 1.0050 | 0.00215 | 84° 18' |
| .1 | 11.0765 | .04440 | 11.1215 | .04616 | .99595 | .99824 | .0041 | .00176 | 84 50 |
| .2 | 12.2459 | .08799 | 12.2866 | .08943 | .99668 | .99856 | .0033 | .00144 | 85 20 |
| .3 | 13.5379 | .13155 | 13.5748 | .13273 | .99728 | .99882 | .0027 | .00118 | 85 47 |
| .4 | 14.9654 | .17509 | 14.9987 | .17605 | .99777 | .99903 | .0022 | .00097 | 86 11 |
| 3.5 | 16.5426 | 1.21860 | 16.5728 | 1.21940 | 0.99818 | 9.99921 | 1.0018 | 0.00079 | 86 32 |
| .6 | 18.2855 | .26211 | 18.3128 | .26275 | .99851 | .99935 | .0015 | .00065 | 86 52 |
| .7 | 20.2113 | .30559 | 20.2360 | .30612 | .99878 | .99947 | .0012 | .00053 | 87 10 |
| .8 | 22.3394 | .34907 | 22.3618 | .34951 | .99900 | .99957 | .0010 | .00043 | 87 26 |
| .9 | 24.6911 | .39254 | 24.7113 | .39290 | .99918 | .99964 | .0008 | .00036 | 87 41 |
| 4.0 | 27.2899 | 1.43600 | 27.3082 | 1.43629 | 0.99933 | 9.99971 | 1.0007 | 0.00029 | 87 54 |
| .1 | 30.1619 | .47946 | 30.1784 | .47970 | .99945 | .99976 | .0005 | .00024 | 88 06 |
| .2 | 33.3357 | .52291 | 33.3597 | .52310 | .99955 | .99980 | .0004 | .00020 | 88 17 |
| .3 | 36.8431 | .56636 | 36.8567 | .56652 | .99963 | .99984 | .0004 | .00016 | 88 27 |
| .4 | 40.7193 | .60980 | 40.7316 | .60993 | .99970 | .99987 | .0003 | .00013 | 88 36 |
| 4.5 | 45.0030 | 1.65324 | 45.0141 | 1.65335 | 0.99975 | 9.99989 | 1.0002 | 0.00011 | 88 44 |
| .6 | 49.7371 | .66668 | 49.7472 | .66677 | .99980 | .99991 | .0002 | .00009 | 88 51 |
| .7 | 54.9690 | .74012 | 54.9781 | .74019 | .99983 | .99993 | .0002 | .00007 | 88 57 |
| .8 | 60.7511 | .78355 | 60.7593 | .78361 | .99986 | .99994 | .0001 | .00006 | 89 03 |
| .9 | 67.1412 | .82699 | 67.1486 | .82704 | .99989 | .99995 | .0001 | .00005 | 89 09 |
| 5.0 | 74.2032 | 1.87042 | 74.2099 | 1.87046 | 0.99991 | 9.99996 | 1.0001 | 0.00004 | 89 14 |

TABLE 18.—Factorials

See Table 16 for logarithms of the products $1.2.3. \dots n$ from 1 to 100.See Table 33 for log. $\Gamma(n+1)$ for values of n between 1.000 and 2.000.

| n | $\frac{1}{n!}$ | | | | | n: = 1. 2. 3. 4. . . n | n |
|----|----------------|-------|-------|-------|-------|------------------------|----|
| 1 | 1. | | | | | 1 | 1 |
| 2 | 0.5 | | | | | 2 | 2 |
| 3 | .16666 | 66666 | 66666 | 66666 | 66667 | 6 | 3 |
| 4 | .04166 | 66666 | 66666 | 66666 | 66667 | 24 | 4 |
| 5 | .00833 | 33333 | 33333 | 33333 | 33333 | 120 | 5 |
| 6 | 0.00138 | 88888 | 88888 | 88888 | 88889 | 720 | 6 |
| 7 | .00019 | 84126 | 98412 | 69841 | 26984 | 5040 | 7 |
| 8 | .00002 | 48015 | 87301 | 58730 | 15873 | 40320 | 8 |
| 9 | .00000 | 27557 | 31922 | 39858 | 90653 | 3 62880 | 9 |
| 10 | .00000 | 02755 | 73192 | 23985 | 89065 | 36 28800 | 10 |
| 11 | 0.00000 | 00250 | 52108 | 38544 | 17188 | 399 16800 | 11 |
| 12 | .00000 | 00020 | 87675 | 69878 | 68099 | 4790 01600 | 12 |
| 13 | .00000 | 00001 | 60590 | 43836 | 82161 | 62270 20800 | 13 |
| 14 | .00000 | 00000 | 11470 | 74559 | 77297 | 8 71782 91200 | 14 |
| 15 | .00000 | 00000 | 00764 | 71037 | 31820 | 130 76743 68000 | 15 |
| 16 | 0.00000 | 00000 | 00047 | 79477 | 33239 | 2092 27808 88000 | 16 |
| 17 | .00000 | 00000 | 00002 | 81145 | 72543 | 35568 74280 96000 | 17 |
| 18 | .00000 | 00000 | 00000 | 15619 | 20697 | 6 40237 37057 28000 | 18 |
| 19 | .00000 | 00000 | 00000 | 00822 | 06352 | 121 64510 04088 32000 | 19 |
| 20 | .00000 | 00000 | 00000 | 00041 | 10318 | 2432 90200 81766 40000 | 20 |

TABLE 19
EXPONENTIAL FUNCTIONS

| x | $\log_{10}(e^x)$ | e^x | e^{-x} | x | $\log_{10}(e^x)$ | e^x | e^{-x} |
|------|------------------|--------|----------|------|------------------|--------|----------|
| 0.00 | 0.00000 | 1.0000 | 1.000000 | 0.50 | 0.21715 | 1.6487 | 0.606531 |
| .01 | .00434 | .0101 | 0.990050 | .51 | .22149 | .6653 | .600496 |
| .02 | .00869 | .0202 | .980109 | .52 | .22583 | .6820 | .594521 |
| .03 | .01303 | .0305 | .970446 | .53 | .23018 | .6989 | .588605 |
| .04 | .01737 | .0408 | .960789 | .54 | .23452 | .7160 | .582748 |
| 0.05 | 0.02171 | 1.0513 | 0.951229 | 0.55 | 0.23886 | 1.7333 | 0.576950 |
| .06 | .02606 | .0618 | .941765 | .56 | .24320 | .7507 | .571209 |
| .07 | .03040 | .0725 | .932394 | .57 | .24755 | .7683 | .565525 |
| .08 | .03474 | .0833 | .923116 | .58 | .25189 | .7860 | .559898 |
| .09 | .03909 | .0942 | .913931 | .59 | .25623 | .8040 | .554327 |
| 0.10 | 0.04343 | 1.1052 | 0.904837 | 0.60 | 0.26058 | 1.8221 | 0.548812 |
| .11 | .04777 | .1163 | .895834 | .61 | .26492 | .8404 | .543351 |
| .12 | .05212 | .1275 | .886920 | .62 | .26926 | .8589 | .537944 |
| .13 | .05646 | .1388 | .878095 | .63 | .27361 | .8776 | .532592 |
| .14 | .06080 | .1503 | .869358 | .64 | .27795 | .8965 | .527292 |
| 0.15 | 0.06514 | 1.1618 | 0.860708 | 0.65 | 0.28229 | 1.9155 | 0.522046 |
| .16 | .06949 | .1735 | .852144 | .66 | .28663 | .9348 | .516851 |
| .17 | .07383 | .1853 | .843665 | .67 | .29098 | .9542 | .511709 |
| .18 | .07817 | .1972 | .835270 | .68 | .29532 | .9739 | .506617 |
| .19 | .08252 | .2092 | .826959 | .69 | .29966 | .9937 | .501576 |
| 0.20 | 0.08686 | 1.2214 | 0.818731 | 0.70 | 0.30401 | 2.0138 | 0.496585 |
| .21 | .09120 | .2337 | .810584 | .71 | .30835 | .9340 | .491644 |
| .22 | .09554 | .2461 | .802519 | .72 | .31269 | .9544 | .486752 |
| .23 | .09989 | .2586 | .794534 | .73 | .31703 | .9751 | .481909 |
| .24 | .10423 | .2712 | .786628 | .74 | .32138 | .9959 | .477114 |
| 0.25 | 0.10857 | 1.2840 | 0.778801 | 0.75 | 0.32572 | 2.1170 | 0.472367 |
| .26 | .11292 | .2969 | .771052 | .76 | .33006 | .1383 | .467666 |
| .27 | .11726 | .3100 | .763379 | .77 | .33441 | .1598 | .463013 |
| .28 | .12160 | .3231 | .755784 | .78 | .33875 | .1815 | .458406 |
| .29 | .12595 | .3364 | .748264 | .79 | .34309 | .2034 | .453845 |
| 0.30 | 0.13029 | 1.3499 | 0.740818 | 0.80 | 0.34744 | 2.2255 | 0.449329 |
| .31 | .13463 | .3634 | .733447 | .81 | .35178 | .2479 | .444858 |
| .32 | .13897 | .3771 | .726149 | .82 | .35612 | .2705 | .440432 |
| .33 | .14332 | .3910 | .718924 | .83 | .36046 | .2933 | .436049 |
| .34 | .14766 | .4049 | .711770 | .84 | .36481 | .3164 | .431711 |
| 0.35 | 0.15200 | 1.4191 | 0.704688 | 0.85 | 0.36915 | 2.3396 | 0.427415 |
| .36 | .15635 | .4333 | .697676 | .86 | .37349 | .3632 | .423162 |
| .37 | .16069 | .4477 | .690734 | .87 | .37784 | .3869 | .418952 |
| .38 | .16503 | .4623 | .683861 | .88 | .38218 | .4109 | .414783 |
| .39 | .16937 | .4770 | .677057 | .89 | .38652 | .4351 | .410656 |
| 0.40 | 0.17372 | 1.4918 | 0.670320 | 0.90 | 0.39087 | 2.4596 | 0.406570 |
| .41 | .17806 | .5068 | .663650 | .91 | .39521 | .4843 | .402524 |
| .42 | .18240 | .5220 | .657047 | .92 | .39955 | .5093 | .398519 |
| .43 | .18675 | .5373 | .650509 | .93 | .40389 | .5345 | .394554 |
| .44 | .19109 | .5527 | .644036 | .94 | .40824 | .5600 | .390628 |
| 0.45 | 0.19543 | 1.5683 | 0.637628 | 0.95 | 0.41258 | 2.5857 | 0.386741 |
| .46 | .19978 | .5841 | .631284 | .96 | .41692 | .6117 | .382893 |
| .47 | .20412 | .6000 | .625002 | .97 | .42127 | .6379 | .379083 |
| .48 | .20846 | .6161 | .618783 | .98 | .42561 | .6645 | .375311 |
| .49 | .21280 | .6323 | .612626 | .99 | .42995 | .6912 | .371577 |
| 0.50 | 0.21715 | 1.6487 | 0.606531 | 1.00 | 0.43429 | 2.7183 | 0.367879 |

TABLE 19 (*continued*)
EXPONENTIAL FUNCTIONS

| x | $\log_{10}(e^x)$ | e^x | e^{-x} | x | $\log_{10}(e^x)$ | e^x | e^{-x} |
|------|------------------|--------|----------|------|------------------|--------|----------|
| 1.00 | 0.43429 | 2.7183 | 0.367879 | 1.50 | 0.65144 | 4.4817 | 0.223130 |
| .01 | .43864 | .7456 | .364219 | .51 | .65578 | .5267 | .220910 |
| .02 | .44298 | .7732 | .360595 | .52 | .66013 | .5722 | .218712 |
| .03 | .44732 | .8011 | .357007 | .53 | .66447 | .6182 | .216536 |
| .04 | .45167 | .8292 | .353455 | .54 | .66881 | .6646 | .214381 |
| 1.05 | 0.45601 | 2.8577 | 0.349938 | 1.55 | 0.67316 | 4.7115 | 0.212248 |
| .06 | .46035 | .8864 | .346456 | .56 | .67750 | .7588 | .210136 |
| .07 | .46470 | .9154 | .343009 | .57 | .68184 | .8066 | .208045 |
| .08 | .46904 | .9447 | .339596 | .58 | .68619 | .8550 | .205975 |
| .09 | .47338 | .9743 | .336216 | .59 | .69053 | .9037 | .203926 |
| 1.10 | 0.47772 | 3.0042 | 0.332871 | 1.60 | 0.69487 | 4.9530 | 0.201897 |
| .11 | .48207 | .0344 | .329559 | .61 | .69921 | 5.0028 | .199888 |
| .12 | .48641 | .0649 | .326280 | .62 | .70356 | .0531 | .197899 |
| .13 | .49075 | .0957 | .323033 | .63 | .70790 | .1039 | .195930 |
| .14 | .49510 | .1268 | .319819 | .64 | .71224 | .1552 | .193980 |
| 1.15 | 0.49944 | 3.1582 | 0.316637 | 1.65 | 0.71659 | 5.2070 | 0.192050 |
| .16 | .50378 | .1899 | .313486 | .66 | .72093 | .2593 | .190139 |
| .17 | .50812 | .2220 | .310367 | .67 | .72527 | .3122 | .188247 |
| .18 | .51247 | .2544 | .307279 | .68 | .72961 | .3656 | .186374 |
| .19 | .51681 | .2871 | .304221 | .69 | .73396 | .4195 | .184520 |
| 1.20 | 0.52115 | 3.3201 | 0.301194 | 1.70 | 0.73830 | 5.4739 | 0.182684 |
| .21 | .52550 | .3535 | .298197 | .71 | .74264 | .5290 | .180866 |
| .22 | .52984 | .3872 | .295230 | .72 | .74699 | .5845 | .179066 |
| .23 | .53418 | .4212 | .292293 | .73 | .75133 | .6407 | .177284 |
| .24 | .53853 | .4556 | .289384 | .74 | .75567 | .6973 | .175520 |
| 1.25 | 0.54287 | 3.4903 | 0.286505 | 1.75 | 0.76002 | 5.7546 | 0.173774 |
| .26 | .54721 | .5254 | .283654 | .76 | .76436 | .8124 | .172045 |
| .27 | .55155 | .5609 | .280832 | .77 | .76870 | .8709 | .170333 |
| .28 | .55590 | .5966 | .278037 | .78 | .77304 | .9299 | .168638 |
| .29 | .56024 | .6328 | .275271 | .79 | .77739 | .9895 | .166960 |
| 1.30 | 0.56458 | 3.6693 | 0.272532 | 1.80 | 0.78173 | 6.0496 | 0.165299 |
| .31 | .56893 | .7062 | .269820 | .81 | .78607 | .1104 | .163654 |
| .32 | .57327 | .7434 | .267135 | .82 | .79042 | .1719 | .162026 |
| .33 | .57761 | .7810 | .264477 | .83 | .79476 | .2339 | .160414 |
| .34 | .58195 | .8190 | .261846 | .84 | .79910 | .2965 | .158817 |
| 1.35 | 0.58630 | 3.8574 | 0.259240 | 1.85 | 0.80344 | 6.3598 | 0.157237 |
| .36 | .59064 | .8962 | .256661 | .86 | .80779 | .4237 | .155673 |
| .37 | .59498 | .9354 | .254107 | .87 | .81213 | .4883 | .154124 |
| .38 | .59933 | .9749 | .251579 | .88 | .81647 | .5535 | .152590 |
| .39 | .60367 | 4.0149 | .249075 | .89 | .82082 | .6194 | .151072 |
| 1.40 | 0.60801 | 4.0552 | 0.246597 | 1.90 | 0.82516 | 6.6859 | 0.149569 |
| .41 | .61236 | .0960 | .244143 | .91 | .82950 | .7531 | .148080 |
| .42 | .61670 | .1371 | .241714 | .92 | .83385 | .8210 | .146607 |
| .43 | .62104 | .1787 | .239309 | .93 | .83819 | .8895 | .145148 |
| .44 | .62538 | .2207 | .236928 | .94 | .84253 | .9588 | .143704 |
| 1.45 | 0.62973 | 4.2631 | 0.234570 | 1.95 | 0.84687 | 7.0287 | 0.142274 |
| .46 | .63407 | .3060 | .232236 | .96 | .85122 | .0993 | .140858 |
| .47 | .63841 | .3492 | .229925 | .97 | .85556 | .1707 | .139457 |
| .48 | .64276 | .3929 | .227638 | .98 | .85990 | .2427 | .138069 |
| .49 | .64710 | .4371 | .225373 | .99 | .86425 | .3155 | .136695 |
| 1.50 | 0.65144 | 4.4817 | 0.223130 | 2.00 | 0.86859 | 7.3891 | 0.135335 |

TABLE 19 (continued)
EXPONENTIAL FUNCTIONS

| x | $\log_{10}(e^x)$ | e^x | e^{-x} | x | $\log_{10}(e^x)$ | e^x | e^{-x} |
|------|------------------|--------|----------|------|------------------|--------|----------|
| 2.00 | 0.86859 | 7.3891 | 0.135335 | 2.50 | 1.08574 | 12.182 | 0.082085 |
| .01 | .87293 | .4633 | .133989 | .51 | .09008 | .305 | .081268 |
| .02 | .87727 | .5383 | .132655 | .52 | .09442 | .429 | .080460 |
| .03 | .88162 | .6141 | .131336 | .53 | .09877 | .554 | .079659 |
| .04 | .88596 | .6906 | .130029 | .54 | .10311 | .680 | .078866 |
| 2.05 | 0.89030 | 7.7679 | 0.128735 | 2.55 | 1.10745 | 12.807 | 0.078082 |
| .06 | .89465 | .8460 | .127454 | .56 | .11179 | .936 | .077305 |
| .07 | .89899 | .9248 | .126186 | .57 | .11614 | 13.066 | .076536 |
| .08 | .90333 | 8.0045 | .124930 | .58 | .12048 | .197 | .075774 |
| .09 | .90768 | .0849 | .123687 | .59 | .12482 | .330 | .075020 |
| 2.10 | 0.91202 | 8.1662 | 0.122456 | 2.60 | 1.12917 | 13.464 | 0.074274 |
| .11 | .91636 | .2482 | .121238 | .61 | .13351 | .599 | .073535 |
| .12 | .92070 | .3311 | .120032 | .62 | .13785 | .736 | .072803 |
| .13 | .92505 | .4149 | .118837 | .63 | .14219 | .874 | .072078 |
| .14 | .92939 | .4994 | .117655 | .64 | .14654 | 14.013 | .071361 |
| 2.15 | 0.93373 | 8.5849 | 0.116484 | 2.65 | 1.15088 | 14.154 | 0.070651 |
| .16 | .93808 | .6711 | .115325 | .66 | .15522 | .296 | .069948 |
| .17 | .94242 | .7583 | .114178 | .67 | .15957 | .440 | .069252 |
| .18 | .94676 | .8463 | .113042 | .68 | .16391 | .585 | .068563 |
| .19 | .95110 | .9352 | .111917 | .69 | .16825 | .732 | .067881 |
| 2.20 | 0.95545 | 9.0250 | 0.110803 | 2.70 | 1.17260 | 14.880 | 0.067206 |
| .21 | .95979 | .1157 | .109701 | .71 | .17694 | 15.029 | .066537 |
| .22 | .96413 | .2073 | .108609 | .72 | .18128 | .180 | .065875 |
| .23 | .96848 | .2999 | .107528 | .73 | .18562 | .333 | .065219 |
| .24 | .97282 | .3933 | .106459 | .74 | .18997 | .487 | .064570 |
| 2.25 | 0.97716 | 9.4877 | 0.105399 | 2.75 | 1.19431 | 15.643 | 0.063928 |
| .26 | .98151 | .5831 | .104350 | .76 | .19865 | .800 | .063292 |
| .27 | .98585 | .6794 | .103312 | .77 | .20300 | .959 | .062662 |
| .28 | .99019 | .7767 | .102284 | .78 | .20734 | 16.119 | .062039 |
| .29 | .99453 | .8749 | .101266 | .79 | .21168 | .281 | .061421 |
| 2.30 | 0.99888 | 9.9742 | 0.100259 | 2.80 | 1.21602 | 16.445 | 0.060810 |
| .31 | 1.00322 | 10.074 | .099261 | .81 | .22037 | .610 | .060205 |
| .32 | .00756 | .176 | .098274 | .82 | .22471 | .777 | .059606 |
| .33 | .01191 | .278 | .097296 | .83 | .22905 | .945 | .059013 |
| .34 | .01625 | .381 | .096328 | .84 | .23340 | 17.116 | .058426 |
| 2.35 | 1.02059 | 10.486 | 0.095369 | 2.85 | 1.23774 | 17.288 | 0.057844 |
| .36 | .02493 | .591 | .094420 | .86 | .24208 | .462 | .057269 |
| .37 | .02928 | .697 | .093481 | .87 | .24643 | .637 | .056699 |
| .38 | .03362 | .805 | .092551 | .88 | .25077 | .814 | .056135 |
| .39 | .03796 | .913 | .091630 | .89 | .25511 | .993 | .055576 |
| 2.40 | 1.04231 | 11.023 | 0.090718 | 2.90 | 1.25945 | 18.174 | 0.055023 |
| .41 | .04665 | .134 | .089815 | .91 | .26380 | .357 | .054476 |
| .42 | .05099 | .246 | .088922 | .92 | .26814 | .541 | .053934 |
| .43 | .05534 | .359 | .088037 | .93 | .27248 | .728 | .053397 |
| .44 | .05968 | .473 | .087161 | .94 | .27683 | .916 | .052866 |
| 2.45 | 1.06402 | 11.588 | 0.086294 | 2.95 | 1.28117 | 19.106 | 0.052340 |
| .46 | .06836 | .705 | .085435 | .96 | .28551 | .298 | .051819 |
| .47 | .07271 | .822 | .084585 | .97 | .28985 | .492 | .051303 |
| .48 | .07705 | .941 | .083743 | .98 | .29420 | .688 | .050793 |
| .49 | .08139 | 12.061 | .082910 | .99 | .29854 | .886 | .050287 |
| 2.50 | 1.08574 | 12.182 | 0.082085 | 3.00 | 1.30288 | 20.086 | 0.049787 |

TABLE 19 (continued)
EXPONENTIAL FUNCTIONS

| x | $\log_{10}(e^x)$ | e^x | e^{-x} | x | $\log_{10}(e^x)$ | e^x | e^{-x} |
|------|------------------|--------|----------|------|------------------|--------|----------|
| 3.00 | 1.30288 | 20.086 | 0.049787 | 3.50 | 1.52003 | 33.115 | 0.030197 |
| .01 | .30723 | .287 | .049292 | .51 | .52437 | .448 | .029897 |
| .02 | .31157 | .491 | .048801 | .52 | .52872 | .784 | .029599 |
| .03 | .31591 | .697 | .048316 | .53 | .53306 | 34.124 | .029305 |
| .04 | .32026 | .905 | .047835 | .54 | .53740 | .467 | .029013 |
| 3.05 | 1.32460 | 21.115 | 0.047359 | 3.55 | 1.54175 | 34.813 | 0.028725 |
| .06 | .32894 | .328 | .046888 | .56 | .54609 | 35.163 | .028439 |
| .07 | .33328 | .542 | .046421 | .57 | .55043 | .517 | .028156 |
| .08 | .33763 | .758 | .045959 | .58 | .55477 | .874 | .027876 |
| .09 | .34197 | .977 | .045502 | .59 | .55912 | 36.234 | .027598 |
| 3.10 | 1.34631 | 22.198 | 0.045049 | 3.60 | 1.56346 | 36.598 | 0.027324 |
| .11 | .35066 | .421 | .044601 | .61 | .56780 | .066 | .027052 |
| .12 | .35500 | .646 | .044157 | .62 | .57215 | 37.338 | .026783 |
| .13 | .35934 | .874 | .043718 | .63 | .57649 | .713 | .026516 |
| .14 | .36368 | 23.104 | .043283 | .64 | .58083 | 38.092 | .026252 |
| 3.15 | 1.36803 | 23.336 | 0.042852 | 3.65 | 1.58517 | 38.475 | 0.025991 |
| .16 | .37237 | .571 | .042426 | .66 | .58952 | .861 | .025733 |
| .17 | .37671 | .807 | .042004 | .67 | .59386 | 39.252 | .025476 |
| .18 | .38106 | 24.047 | .041586 | .68 | .59820 | .646 | .025223 |
| .19 | .38540 | .288 | .041172 | .69 | .60255 | 40.045 | .024972 |
| 3.20 | 1.38974 | 24.533 | 0.040762 | 3.70 | 1.60689 | 40.447 | 0.024724 |
| .21 | .39409 | .779 | .040357 | .71 | .61123 | .854 | .024478 |
| .22 | .39843 | 25.028 | .039955 | .72 | .61558 | 41.264 | .024234 |
| .23 | .40277 | .280 | .039557 | .73 | .61992 | .679 | .023993 |
| .24 | .40711 | .534 | .039164 | .74 | .62426 | 42.098 | .023754 |
| 3.25 | 1.41146 | 25.790 | 0.038774 | 3.75 | 1.62860 | 42.521 | 0.023518 |
| .26 | .41580 | 26.050 | .038388 | .76 | .63295 | .048 | .023284 |
| .27 | .42014 | .311 | .038006 | .77 | .63729 | 43.380 | .023052 |
| .28 | .42449 | .576 | .037628 | .78 | .64163 | .816 | .022823 |
| .29 | .42883 | .843 | .037254 | .79 | .64598 | 44.256 | .022596 |
| 3.30 | 1.43317 | 27.113 | 0.036883 | 3.80 | 1.65032 | 44.701 | 0.022371 |
| .31 | .43751 | .385 | .036516 | .81 | .65466 | 45.150 | .022148 |
| .32 | .44186 | .660 | .036153 | .82 | .65900 | .604 | .021928 |
| .33 | .44620 | .938 | .035793 | .83 | .66335 | 46.063 | .021710 |
| .34 | .45054 | 28.219 | .035437 | .84 | .66769 | .525 | .021494 |
| 3.35 | 1.45489 | 28.503 | 0.035084 | 3.85 | 1.67203 | 46.993 | 0.021280 |
| .36 | .45923 | .789 | .034735 | .86 | .67638 | 47.465 | .021068 |
| .37 | .46357 | 29.079 | .034390 | .87 | .68072 | .942 | .020858 |
| .38 | .46792 | .371 | .034047 | .88 | .68506 | 48.424 | .020651 |
| .39 | .47226 | .666 | .033709 | .89 | .68941 | .911 | .020445 |
| 3.40 | 1.47660 | 29.964 | 0.033373 | 3.90 | 1.69375 | 49.402 | 0.020242 |
| .41 | .48094 | 30.265 | .033041 | .91 | .69809 | .899 | .020041 |
| .42 | .48529 | .569 | .032712 | .92 | .70243 | 50.400 | .019841 |
| .43 | .48963 | .877 | .032387 | .93 | .70678 | .907 | .019644 |
| .44 | .49397 | 31.187 | .032065 | .94 | .71112 | 51.419 | .019448 |
| 3.45 | 1.49832 | 31.500 | 0.031746 | 3.95 | 1.71546 | 51.935 | 0.019255 |
| .46 | .50266 | .817 | .031430 | .96 | .71981 | 52.457 | .019063 |
| .47 | .50700 | 32.137 | .031117 | .97 | .72415 | .985 | .018873 |
| .48 | .51134 | .460 | .030807 | .98 | .72849 | 53.517 | .018686 |
| .49 | .51569 | .786 | .030501 | .99 | .73283 | 54.055 | .018500 |
| 3.50 | 1.52003 | 33.115 | 0.030197 | 4.00 | 1.73718 | 54.598 | 0.018316 |

TABLE 19 (continued)
EXPONENTIAL FUNCTIONS

| x | $\log_{10}(e^x)$ | e^x | e^{-x} | x | $\log_{10}(e^x)$ | e^x | e^{-x} |
|------|------------------|--------|----------|------|------------------|--------|----------|
| 4.00 | 1.73718 | 54.598 | 0.018316 | 4.50 | 1.95433 | 90.017 | 0.011109 |
| .01 | .74152 | 55.147 | .018133 | .51 | .95867 | .922 | .010998 |
| .02 | .74586 | .701 | .017953 | .52 | .96301 | 91.836 | .010889 |
| .03 | .75021 | 56.261 | .017774 | .53 | .96735 | 92.759 | .010781 |
| .04 | .75455 | .826 | .017597 | .54 | .97170 | 93.691 | .010673 |
| 4.05 | 1.75889 | 57.397 | 0.017422 | 4.55 | 1.97604 | 94.632 | 0.010567 |
| .06 | .76324 | .974 | .017249 | .56 | .98038 | 95.583 | .010462 |
| .07 | .76758 | 58.557 | .017077 | .57 | .98473 | 96.544 | .010358 |
| .08 | .77192 | 59.145 | .016907 | .58 | .98907 | 97.514 | .010255 |
| .09 | .77626 | .740 | .016739 | .59 | .99341 | 98.494 | .010153 |
| 4.10 | 1.78061 | 60.340 | 0.016573 | 4.60 | 1.99775 | 99.484 | 0.010052 |
| .11 | .78495 | .947 | .016408 | .61 | 2.00210 | 100.48 | .009952 |
| .12 | .78929 | 61.559 | .016245 | .62 | .00644 | 101.49 | .009853 |
| .13 | .79364 | 62.178 | .016083 | .63 | .01078 | 102.51 | .009755 |
| .14 | .79798 | .803 | .015923 | .64 | .01513 | 103.54 | .009658 |
| 4.15 | 1.80232 | 63.434 | 0.015764 | 4.65 | 2.01947 | 104.58 | 0.009562 |
| .16 | .80667 | 64.072 | .015608 | .66 | .02381 | 105.64 | .009466 |
| .17 | .81101 | .715 | .015452 | .67 | .02816 | 106.70 | .009372 |
| .18 | .81535 | 65.366 | .015299 | .68 | .03250 | 107.77 | .009279 |
| .19 | .81969 | 66.023 | .015146 | .69 | .03684 | 108.85 | .009187 |
| 4.20 | 1.82404 | 66.686 | 0.014996 | 4.70 | 2.04118 | 109.95 | 0.009095 |
| .21 | .82838 | 67.357 | .014846 | .71 | .04553 | 111.05 | .009005 |
| .22 | .83272 | 68.033 | .014699 | .72 | .04987 | 112.17 | .008915 |
| .23 | .83707 | .717 | .014552 | .73 | .05421 | 113.30 | .008826 |
| .24 | .84141 | 69.408 | .014408 | .74 | .05856 | 114.43 | .008739 |
| 4.25 | 1.84575 | 70.105 | 0.014264 | 4.75 | 2.06290 | 115.58 | 0.008652 |
| .26 | .85009 | .810 | .014122 | .76 | .06724 | 116.75 | .008566 |
| .27 | .85444 | 71.522 | .013982 | .77 | .07158 | 117.92 | .008480 |
| .28 | .85878 | 72.240 | .013843 | .78 | .07593 | 119.10 | .008396 |
| .29 | .86312 | .966 | .013705 | .79 | .08027 | 120.30 | .008312 |
| 4.30 | 1.86747 | 73.700 | 0.013569 | 4.80 | 2.08461 | 121.51 | 0.008230 |
| .31 | .87181 | 74.440 | .013434 | .81 | .08896 | 122.73 | .008148 |
| .32 | .87615 | 75.189 | .013300 | .82 | .09330 | 123.97 | .008067 |
| .33 | .88050 | .944 | .013168 | .83 | .09764 | 125.21 | .007987 |
| .34 | .88484 | 76.708 | .013037 | .84 | .10199 | 126.47 | .007907 |
| 4.35 | 1.88918 | 77.478 | 0.012907 | 4.85 | 2.10633 | 127.74 | 0.007828 |
| .36 | .89352 | 78.257 | .012778 | .86 | .11067 | 129.02 | .007750 |
| .37 | .89787 | 79.044 | .012651 | .87 | .11501 | 130.32 | .007673 |
| .38 | .90221 | 79.838 | .012525 | .88 | .11936 | 131.63 | .007597 |
| .39 | .90655 | 80.640 | .012401 | .89 | .12370 | 132.95 | .007521 |
| 4.40 | 1.91090 | 81.451 | 0.012277 | 4.90 | 2.12804 | 134.29 | 0.007447 |
| .41 | .91524 | 82.269 | .012155 | .91 | .13239 | 135.64 | .007372 |
| .42 | .91958 | 83.096 | .012034 | .92 | .13673 | 137.00 | .007299 |
| .43 | .92392 | .931 | .011914 | .93 | .14107 | 138.38 | .007227 |
| .44 | .92827 | 84.775 | .011796 | .94 | .14541 | 139.77 | .007155 |
| 4.45 | 1.93261 | 85.627 | 0.011679 | 4.95 | 2.14976 | 141.17 | 0.007083 |
| .46 | .93695 | 86.488 | .011562 | .96 | .15410 | 142.59 | .007013 |
| .47 | .94130 | 87.357 | .011447 | .97 | .15844 | 144.03 | .006943 |
| .48 | .94564 | 88.235 | .011333 | .98 | .16279 | 145.47 | .006874 |
| .49 | .94998 | 89.121 | .011221 | .99 | .16713 | 146.94 | .006806 |
| 4.50 | 1.95433 | 90.017 | 0.011109 | 5.00 | 2.17147 | 148.41 | 0.006738 |

TABLE 19 (concluded)
EXPONENTIAL FUNCTIONS

| x | $\log_{10}(e^x)$ | e^x | e^{-x} | x | $\log_{10}(e^x)$ | e^x | e^{-x} |
|------|------------------|--------|----------|------|------------------|--------|----------|
| 5.00 | 2.17147 | 148.41 | 0.006738 | 5.0 | 2.17147 | 148.41 | 0.006738 |
| .01 | .17582 | 149.90 | .006671 | .1 | .21490 | 164.02 | .006097 |
| .02 | .18016 | 151.41 | .006605 | .2 | .25833 | 181.27 | .005517 |
| .03 | .18450 | 152.93 | .006539 | .3 | .30176 | 200.34 | .004992 |
| .04 | .18884 | 154.47 | .006474 | .4 | .34519 | 221.41 | .004517 |
| 5.05 | 2.19319 | 156.02 | 0.006409 | 5.5 | 2.38862 | 244.69 | 0.004087 |
| .06 | .19753 | 157.59 | .006346 | .6 | .43205 | 270.43 | .003698 |
| .07 | .20187 | 159.17 | .006282 | .7 | .47548 | 298.87 | .003346 |
| .08 | .20622 | 160.77 | .006220 | .8 | .51891 | 330.30 | .003028 |
| .09 | .21056 | 162.39 | .006158 | .9 | .56234 | 365.04 | .002739 |
| 5.10 | 2.21490 | 164.02 | 0.006097 | 6.0 | 2.60577 | 403.43 | 0.002479 |
| .11 | .21924 | 165.67 | .006036 | .1 | .64920 | 445.86 | .002243 |
| .12 | .22359 | 167.34 | .005976 | .2 | .69263 | 492.75 | .002029 |
| .13 | .22793 | 169.02 | .005917 | .3 | .73606 | 544.57 | .001836 |
| .14 | .23227 | 170.72 | .005858 | .4 | .77948 | 601.85 | .001662 |
| 5.15 | 2.23662 | 172.43 | 0.005799 | 6.5 | 2.82291 | 665.14 | 0.001503 |
| .16 | .24096 | 174.16 | .005742 | .6 | .86634 | 735.10 | .001360 |
| .17 | .24530 | 175.91 | .005685 | .7 | .90977 | 812.41 | .001231 |
| .18 | .24965 | 177.68 | .005628 | .8 | .95320 | 897.85 | .001114 |
| .19 | .25399 | 179.47 | .005572 | .9 | .99663 | 992.27 | .001008 |
| 5.20 | 2.25833 | 181.27 | 0.005517 | 7.0 | 3.04006 | 1096.6 | 0.000912 |
| .21 | .26267 | 183.09 | .005462 | .1 | .08349 | 1212.0 | .000825 |
| .22 | .26702 | 184.93 | .005407 | .2 | .12692 | 1339.4 | .000747 |
| .23 | .27136 | 186.79 | .005354 | .3 | .17035 | 1480.3 | .000676 |
| .24 | .27570 | 188.67 | .005300 | .4 | .21378 | 1636.0 | .000611 |
| 5.25 | 2.28005 | 190.57 | 0.005248 | 7.5 | 3.25721 | 1808.0 | 0.000553 |
| .26 | .28439 | 192.48 | .005195 | .6 | .30064 | 1998.2 | .000500 |
| .27 | .28873 | 194.42 | .005144 | .7 | .34407 | 2208.3 | .000453 |
| .28 | .29307 | 196.37 | .005092 | .8 | .38750 | 2440.6 | .000410 |
| .29 | .29742 | 198.34 | .005042 | .9 | .43093 | 2697.3 | .000371 |
| 5.30 | 2.30176 | 200.34 | 0.004992 | 8.0 | 3.47436 | 2981.0 | 0.000335 |
| .31 | .30610 | 202.35 | .004942 | .1 | .51779 | 3294.5 | .000304 |
| .32 | .31045 | 204.38 | .004893 | .2 | .56121 | 3641.0 | .000275 |
| .33 | .31479 | 206.44 | .004844 | .3 | .60464 | 4023.9 | .000249 |
| .34 | .31913 | 208.51 | .004796 | .4 | .64807 | 4447.1 | .000225 |
| 5.35 | 2.32348 | 210.61 | 0.004748 | 8.5 | 3.69150 | 4914.8 | 0.000203 |
| .36 | .32782 | 212.72 | .004701 | .6 | .73493 | 5431.7 | .000184 |
| .37 | .33216 | 214.86 | .004654 | .7 | .77836 | 6002.9 | .000167 |
| .38 | .33650 | 217.02 | .004608 | .8 | .82179 | 6634.2 | .000151 |
| .39 | .34085 | 219.20 | .004562 | .9 | .86522 | 7332.0 | .000136 |
| 5.40 | 2.34519 | 221.41 | 0.004517 | 9.0 | 3.90865 | 8103.1 | 0.000123 |
| .41 | .34953 | 223.63 | .004472 | .1 | .95208 | 8955.3 | .000112 |
| .42 | .35388 | 225.88 | .004427 | .2 | .99551 | 9897.1 | .000101 |
| .43 | .35822 | 228.15 | .004383 | .3 | 4.03894 | 10938. | .000091 |
| .44 | .36256 | 230.44 | .004339 | .4 | .08237 | 12088. | .000083 |
| 5.45 | 2.36690 | 232.76 | 0.004296 | 9.5 | 4.12580 | 13360. | 0.000075 |
| .46 | .37125 | 235.10 | .004254 | .6 | .16923 | 14765. | .000068 |
| .47 | .37559 | 237.46 | .004211 | .7 | .21266 | 16318. | .000061 |
| .48 | .37993 | 239.85 | .004169 | .8 | .25609 | 18034. | .000055 |
| .49 | .38428 | 242.26 | .004128 | .9 | .29952 | 19930. | .000050 |
| 5.50 | 2.38862 | 244.69 | 0.004087 | 10.0 | 4.34294 | 22026. | 0.000045 |

EXPONENTIAL FUNCTIONS

Values of e^{x^2} and e^{-x^2} and their logarithms

| x | e^{x^2} | $\log e^{x^2}$ | e^{-x^2} | $\log e^{-x^2}$ |
|-----|-------------------------|----------------|--------------------------|------------------|
| 0.1 | 1.0101 | 0.00434 | 0.99005 | $\bar{1}.99566$ |
| 2 | 1.0408 | 01737 | 96079 | 98263 |
| 3 | 1.0942 | 03909 | 91393 | 96091 |
| 4 | 1.1735 | 06949 | 85214 | 93051 |
| 5 | 1.2840 | 10857 | 77880 | 89143 |
| 0.6 | 1.4333 | 0.15635 | 0.69768 | $\bar{1}.84365$ |
| 7 | 1.6323 | 21280 | 61263 | 78720 |
| 8 | 1.8965 | 27795 | 52729 | 72205 |
| 9 | 2.2479 | 35178 | 44486 | 64822 |
| 1.0 | 2.7183 | 43429 | 36788 | 56571 |
| 1.1 | 3.3535 | 0.52550 | 0.29820 | $\bar{1}.47450$ |
| 2 | 4.2207 | 62538 | 23693 | 37462 |
| 3 | 5.4195 | 73396 | 18452 | 26604 |
| 4 | 7.0993 | 85122 | 14086 | 14878 |
| 5 | 9.4877 | 97716 | 10540 | 02284 |
| 1.6 | 1.2936×10 | 1.11179 | 0.77305×10^{-1} | $\bar{2}.88821$ |
| 7 | 1.7993 " | 25511 | 55576 " | 74489 |
| 8 | 2.5534 " | 40711 | 39164 " | 59289 |
| 9 | 3.0966 " | 56780 | 27052 " | 43220 |
| 2.0 | 5.4598 " | 73718 | 18316 " | 26282 |
| 2.1 | 8.2269 " | 1.91524 | 0.12155 " | $\bar{2}.08476$ |
| 2 | 1.2647×10^2 | 2.10199 | 79071×10^{-2} | $\bar{3}.89801$ |
| 3 | 1.9834 " | 29742 | 50418 " | 70258 |
| 4 | 3.1735 " | 50154 | 31511 " | 49846 |
| 5 | 5.1801 " | 71434 | 19305 " | 28566 |
| 2.6 | 8.6264 " | 2.93583 | 0.11592 " | $\bar{3}.06417$ |
| 7 | 1.4656×10^3 | 3.16001 | 68233×10^{-3} | 4.83399 |
| 8 | 2.5402 " | 40487 | 39307 " | 59513 |
| 9 | 4.4918 " | 65242 | 22263 " | 34758 |
| 3.0 | 8.1031 " | 90865 | 12341 " | 09135 |
| 3.1 | 1.4913×10^4 | 4.17357 | 0.67055×10^{-4} | $\bar{5}.82643$ |
| 2 | 2.8001 " | 44718 | 35713 " | 55282 |
| 3 | 5.3637 " | 72947 | 18644 " | 27053 |
| 4 | 1.0482×10^5 | 5.02044 | 95402×10^{-5} | $\bar{6}.97956$ |
| 5 | 2.0898 " | 32011 | 47851 " | 67989 |
| 3.6 | 4.2507 " | 5.62846 | 0.23526 " | $\bar{6}.37154$ |
| 7 | 8.8205 " | 94549 | 11337 " | 05451 |
| 8 | 1.8673×10^6 | 6.27121 | 53553×10^{-6} | 7.72879 |
| 9 | 4.0329 " | 60562 | 24796 " | 39438 |
| 4.0 | 8.8861 " | 94871 | 11254 " | 05129 |
| 4.1 | 1.9975×10^7 | 7.30049 | 0.50062×10^{-7} | $\bar{8}.69951$ |
| 2 | 4.5809 " | 66095 | 21830 " | 33905 |
| 3 | 1.0718×10^8 | 8.03010 | 93303×10^{-8} | $\bar{9}.96990$ |
| 4 | 2.5582 " | 40794 | 39089 " | 59206 |
| 5 | 6.2296 " | 79446 | 16052 " | 20554 |
| 4.6 | 1.5476×10^9 | 9.18967 | 0.64614×10^{-9} | $\bar{10}.81033$ |
| 7 | 3.9225 " | 59357 | 25494 " | 40643 |
| 8 | 1.0142×10^{10} | 10.00614 | 98595×10^{-10} | $\bar{11}.99386$ |
| 9 | 2.6755 " | 42741 | 37376 " | 57259 |
| 5.0 | 7.2005 " | 85736 | 13888 " | 14264 |

TABLES 21 AND 22
EXPONENTIAL FUNCTIONS

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TABLE 21.—Values of $e^{\frac{\pi}{4}z}$ and $e^{-\frac{\pi}{4}z}$ and their logarithms

| x | $e^{\frac{\pi}{4}z}$ | $\log e^{\frac{\pi}{4}z}$ | $e^{-\frac{\pi}{4}z}$ | $\log e^{-\frac{\pi}{4}z}$ |
|-----|----------------------|---------------------------|--------------------------|----------------------------|
| 1 | 2.1933 | 0.34109 | 0.45594 | $\bar{1}.65891$ |
| 2 | 4.8105 | .68219 | .20788 | $\bar{.31781}$ |
| 3 | 1.0551×10 | 1.02328 | $.94780 \times 10^{-1}$ | $\bar{2}.97672$ |
| 4 | 2.3141 | .36438 | .43214 | $\bar{.63562}$ |
| 5 | 5.0754 | .70547 | .19703 | $\bar{.29453}$ |
| 6 | 1.1132×10^2 | 2.04656 | 0.89833×10^{-2} | $\bar{3}.95344$ |
| 7 | 2.4415 | .38766 | .40958 | $\bar{.61234}$ |
| 8 | 5.3549 | .72875 | .18674 | $\bar{.27125}$ |
| 9 | 1.1745×10^3 | 3.06985 | $.85144 \times 10^{-3}$ | $\bar{4}.93015$ |
| 10 | 2.5760 | .41094 | .38820 | $\bar{.58906}$ |
| 11 | 5.6498 | 3.75203 | 0.17700 | $\bar{4}.24797$ |
| 12 | 1.2392×10^4 | 4.09313 | $.80700 \times 10^{-4}$ | $\bar{5}.90687$ |
| 13 | 2.7178 | .43422 | .36794 | $\bar{.56578}$ |
| 14 | 5.9610 | .77532 | .16776 | $\bar{.22468}$ |
| 15 | 1.3074×10^5 | 5.11641 | $.76487 \times 10^{-5}$ | $\bar{6}.88359$ |
| 16 | 2.8675 | 5.45751 | 0.34873 | $\bar{6}.54249$ |
| 17 | 6.2893 | .79860 | .15900 | $\bar{.20140}$ |
| 18 | 1.3794×10^6 | 6.13969 | $.72495 \times 10^{-6}$ | $\bar{7}.86631$ |
| 19 | 3.0254 | .48079 | .33053 | $\bar{.51921}$ |
| 20 | 6.6356 | .82188 | .15070 | $\bar{.17812}$ |

TABLE 22.—Values of $e^{\frac{\sqrt{\pi}}{4}z}$ and $e^{-\frac{\sqrt{\pi}}{4}z}$ and their logarithms

| x | $e^{\frac{\sqrt{\pi}}{4}z}$ | $\log e^{\frac{\sqrt{\pi}}{4}z}$ | $e^{-\frac{\sqrt{\pi}}{4}z}$ | $\log e^{-\frac{\sqrt{\pi}}{4}z}$ |
|-----|-----------------------------|----------------------------------|------------------------------|-----------------------------------|
| 1 | 1.5576 | 0.19244 | 0.64203 | $\bar{1}.80756$ |
| 2 | 2.4260 | .38488 | .41221 | $\bar{.61512}$ |
| 3 | 3.7786 | .57733 | .26465 | $\bar{.42267}$ |
| 4 | 5.8853 | .76977 | .16992 | $\bar{.23023}$ |
| 5 | 9.1666 | .96221 | .10909 | $\bar{.03779}$ |
| 6 | 14.277 | 1.15465 | 0.070041 | $\bar{2}.84535$ |
| 7 | 22.238 | .34709 | .044968 | $\bar{.65291}$ |
| 8 | 34.636 | .53953 | .028871 | $\bar{.46047}$ |
| 9 | 53.948 | .73198 | .018536 | $\bar{.26802}$ |
| 10 | 84.027 | .92442 | .011901 | $\bar{.07558}$ |
| 11 | 130.88 | 2.11686 | 0.0076408 | $\bar{3}.88314$ |
| 12 | 203.85 | .30930 | .0049057 | $\bar{.69070}$ |
| 13 | 317.50 | .50174 | .0031496 | $\bar{.49826}$ |
| 14 | 494.52 | .69418 | .0020222 | $\bar{.30582}$ |
| 15 | 770.24 | .88663 | .0012983 | $\bar{.11337}$ |
| 16 | 1199.7 | 3.07907 | 0.00083355 | $\bar{4}.92093$ |
| 17 | 1868.6 | .27151 | .00053517 | $\bar{.72849}$ |
| 18 | 2910.4 | .46395 | .00034360 | $\bar{.53605}$ |
| 19 | 4533.1 | .65639 | .00022060 | $\bar{.34361}$ |
| 20 | 7060.5 | .84883 | .00014163 | $\bar{.15117}$ |

TABLES 23 AND 24
EXPONENTIAL FUNCTIONS AND LEAST SQUARES
EXPONENTIAL FUNCTIONS

TABLE 23.—Values of e^x and e^{-x} and their logarithms.

| x | e^x | $\log e^x$ | e^{-x} | x | e^x | $\log e^x$ | e^{-x} |
|------|--------|------------|----------|-----|---------|------------|----------|
| 1/64 | 1.0157 | 0.00679 | 0.98450 | 1/3 | 1.3956 | 0.14476 | 0.71653 |
| 1/32 | .0317 | .01357 | .96023 | 1/2 | .6487 | .21715 | .60653 |
| 1/16 | .0045 | .02714 | .93941 | 3/4 | 2.1170 | .32572 | .47237 |
| 1/10 | .1052 | .04343 | .90484 | 1 | .7183 | .43429 | .36788 |
| 1/9 | .1175 | .04825 | .89484 | 5/4 | 3.4903 | .54287 | .28650 |
| 1/8 | 1.1331 | 0.05429 | 0.88250 | 3/2 | 4.4817 | 0.65144 | 0.22313 |
| 1/7 | .1536 | .06204 | .86688 | 7/4 | 5.7546 | .76002 | .17377 |
| 1/6 | .1814 | .07238 | .84648 | 2 | 7.3891 | .86859 | .13534 |
| 1/5 | .2214 | .08686 | .81873 | 9/4 | 9.4877 | .97716 | .10540 |
| 1/4 | .2840 | .10857 | .77880 | 5/2 | 12.1825 | 1.08574 | .08208 |

LEAST SQUARES

TABLE 24.—Values of $P = \frac{2}{\sqrt{\pi}} \int_0^{hx} e^{-(hx)^2} d(hx)$.

P , the probability of an observational error having a value positive or negative equal to or less than x when h is the measure of precision, $P = \frac{2}{\sqrt{\pi}} \int_0^{hx} e^{-(hx)^2} d(hx)$. $h^2 = (\frac{1}{2} m \Delta x^2)$ where m = no. obs. of deviation Δx .

| hx | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|------|--------|--------|--------|---------|--------|--------|--------|--------|--------|--------|
| 0.0 | | .01128 | .02256 | .03384 | .04511 | .05637 | .06762 | .07886 | .09008 | .10128 |
| .1 | .11246 | .12362 | .13476 | .14587 | .15695 | .16800 | .17901 | .18999 | .20094 | .21184 |
| .2 | .22270 | .23352 | .24430 | .25502 | .26570 | .27633 | .28690 | .29742 | .30788 | .31828 |
| .3 | .32863 | .33891 | .34913 | .35928 | .36936 | .37938 | .38933 | .39921 | .40901 | .41874 |
| .4 | .42839 | .43797 | .44747 | .45689 | .46623 | .47548 | .48466 | .49375 | .50275 | .51167 |
| 0.5 | .52050 | .52924 | .53790 | .54646 | .55494 | .56332 | .57162 | .57982 | .58792 | .59594 |
| .6 | .60386 | .61168 | .61941 | .62705 | .63459 | .64203 | .64938 | .65663 | .66378 | .67084 |
| .7 | .67780 | .68467 | .69143 | .69810 | .70468 | .71116 | .71754 | .72382 | .73001 | .73610 |
| .8 | .74210 | .74800 | .75381 | .75952 | .76514 | .77067 | .77610 | .78144 | .78669 | .79184 |
| .9 | .79691 | .80188 | .80677 | .81156 | .81627 | .82089 | .82542 | .82987 | .83423 | .83851 |
| 1.0 | .84270 | .84681 | .85084 | .85478 | .85865 | .86244 | .86614 | .86977 | .87333 | .87680 |
| .1 | .88021 | .88353 | .88679 | .88997 | .89308 | .89612 | .89910 | .90200 | .90484 | .90761 |
| .2 | .91031 | .91296 | .91553 | .91805 | .92051 | .92290 | .92524 | .92751 | .92973 | .93190 |
| .3 | .93401 | .93606 | .93807 | .94002 | .94191 | .94376 | .94556 | .94731 | .94902 | .95067 |
| .4 | .95229 | .95385 | .95538 | .95686 | .95830 | .95970 | .96105 | .96237 | .96365 | .96490 |
| 1.5 | .96611 | .96728 | .96841 | .96952 | .97059 | .97162 | .97263 | .97360 | .97455 | .97546 |
| .6 | .97635 | .97721 | .97804 | .97884 | .97962 | .98038 | .98110 | .98181 | .98249 | .98315 |
| .7 | .98379 | .98441 | .98500 | .98558 | .98613 | .98667 | .98719 | .98769 | .98817 | .98864 |
| .8 | .98909 | .98952 | .98994 | .99035 | .99074 | .99111 | .99147 | .99182 | .99216 | .99248 |
| .9 | .99279 | .99309 | .99338 | .99366 | .99392 | .99418 | .99443 | .99466 | .99489 | .99511 |
| 2.0 | .99532 | .99552 | .99572 | .99591 | .99609 | .99626 | .99642 | .99658 | .99673 | .99688 |
| .1 | .99702 | .99715 | .99728 | .99741 | .99753 | .99764 | .99775 | .99785 | .99795 | .99805 |
| .2 | .99814 | .99822 | .99831 | .99839 | .99846 | .99854 | .99861 | .99867 | .99874 | .99880 |
| .3 | .99886 | .99891 | .99897 | .99902 | .99906 | .99911 | .99915 | .99920 | .99924 | .99928 |
| .4 | .99931 | .99935 | .99938 | .99941 | .99944 | .99947 | .99950 | .99952 | .99955 | .99957 |
| 2.5 | .99959 | .99961 | .99963 | .99965 | .99967 | .99969 | .99971 | .99972 | .99974 | .99975 |
| .6 | .99976 | .99978 | .99979 | .99980 | .99981 | .99982 | .99983 | .99984 | .99985 | .99986 |
| .7 | .99987 | .99987 | .99988 | .99989 | .99989 | .99990 | .99991 | .99991 | .99992 | .99992 |
| .8 | .99992 | .99993 | .99993 | .99994 | .99994 | .99994 | .99995 | .99995 | .99995 | .99996 |
| .9 | .99996 | .99996 | .99996 | .99997 | .99997 | .99997 | .99997 | .99997 | .99997 | .99998 |
| 3.0 | .99998 | .99999 | .99999 | 1.00000 | | | | | | |

Burgess, James. Trans. Roy. Soc. Edinburgh, 39, 257, 1900.

LEAST SQUARES

TABLE 25

This table gives the values of the probability P , as defined in last table, corresponding to different values of x/r where r is the "probable error." The probable error r is equal to $0.47694/h$.

| $\frac{x}{r}$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0.0 | .00000 | .00538 | .01076 | .01614 | .02152 | .02690 | .03228 | .03766 | .04303 | .04840 |
| 0.1 | .05378 | .05914 | .06451 | .06987 | .07523 | .08059 | .08594 | .09129 | .09663 | .10197 |
| 0.2 | .10731 | .11264 | .11796 | .12328 | .12860 | .13391 | .13921 | .14451 | .14980 | .15508 |
| 0.3 | .16035 | .16562 | .17088 | .17614 | .18138 | .18662 | .19185 | .19707 | .20229 | .20749 |
| 0.4 | .21268 | .21787 | .22304 | .22821 | .23336 | .23851 | .24364 | .24876 | .25388 | .25898 |
| 0.5 | .26407 | .26915 | .27421 | .27927 | .28431 | .28934 | .29436 | .29936 | .30435 | .30933 |
| 0.6 | .31430 | .31925 | .32419 | .32911 | .33402 | .33892 | .34380 | .34866 | .35352 | .35835 |
| 0.7 | .36317 | .36798 | .37277 | .37755 | .38231 | .38705 | .39178 | .39649 | .40118 | .40586 |
| 0.8 | .41052 | .41517 | .41979 | .42440 | .42899 | .43357 | .43813 | .44267 | .44719 | .45169 |
| 0.9 | .45618 | .46064 | .46509 | .46952 | .47393 | .47832 | .48270 | .48705 | .49139 | .49570 |
| 1.0 | .50000 | .50428 | .50853 | .51277 | .51699 | .52119 | .52537 | .52952 | .53366 | .53778 |
| 1.1 | .54188 | .54595 | .55001 | .55404 | .55806 | .56205 | .56602 | .56998 | .57391 | .57782 |
| 1.2 | .58171 | .58558 | .58942 | .59325 | .59705 | .60083 | .60460 | .60833 | .61205 | .61575 |
| 1.3 | .61942 | .62308 | .62671 | .63032 | .63391 | .63747 | .64102 | .64456 | .64804 | .65152 |
| 1.4 | .65498 | .65841 | .66182 | .66521 | .66858 | .67193 | .67526 | .67856 | .68184 | .68510 |
| 1.5 | .68833 | .69155 | .69474 | .69791 | .70106 | .70419 | .70729 | .71038 | .71344 | .71648 |
| 1.6 | .71949 | .72249 | .72546 | .72841 | .73134 | .73425 | .73714 | .74000 | .74285 | .74567 |
| 1.7 | .74847 | .75124 | .75400 | .75674 | .75945 | .76214 | .76481 | .76746 | .77009 | .77270 |
| 1.8 | .77528 | .77785 | .78039 | .78291 | .78542 | .78790 | .79036 | .79280 | .79522 | .79761 |
| 1.9 | .79999 | .80235 | .80469 | .80700 | .80930 | .81158 | .81383 | .81607 | .81828 | .82048 |
| 2.0 | .82266 | .82481 | .82695 | .82907 | .83117 | .83324 | .83530 | .83734 | .83936 | .84137 |
| 2.1 | .84335 | .84531 | .84726 | .84919 | .85109 | .85298 | .85486 | .85671 | .85854 | .86036 |
| 2.2 | .86216 | .86394 | .86570 | .86745 | .86917 | .87088 | .87258 | .87425 | .87591 | .87755 |
| 2.3 | .87918 | .88078 | .88237 | .88395 | .88550 | .88705 | .88857 | .89008 | .89157 | .89304 |
| 2.4 | .89450 | .89595 | .89738 | .89879 | .90019 | .90157 | .90293 | .90428 | .90562 | .90694 |
| 2.5 | .90825 | .90954 | .91082 | .91208 | .91332 | .91456 | .91578 | .91698 | .91817 | .91935 |
| 2.6 | .92051 | .92166 | .92280 | .92392 | .92503 | .92613 | .92721 | .92828 | .92934 | .93038 |
| 2.7 | .93141 | .93243 | .93344 | .93443 | .93541 | .93638 | .93734 | .93828 | .93922 | .94014 |
| 2.8 | .94105 | .94195 | .94284 | .94371 | .94458 | .94543 | .94627 | .94711 | .94793 | .94874 |
| 2.9 | .94954 | .95033 | .95111 | .95187 | .95263 | .95338 | .95412 | .95484 | .95557 | .95628 |
| 3 | .95698 | .95766 | .95833 | .95899 | .95964 | .96028 | .96091 | .96153 | .96215 | .96276 |
| 4 | .96337 | .96398 | .96458 | .96517 | .96575 | .96632 | .96688 | .96743 | .96798 | .96852 |
| 5 | .96906 | .96960 | .97013 | .97066 | .97118 | .97170 | .97221 | .97272 | .97323 | .97373 |

TABLE 26.—Values of the factor $0.6745\sqrt{\frac{1}{n-1}}$

This factor occurs in the equation $r_s = 0.6745\sqrt{\frac{\sum v^2}{n-1}}$ for the probable error of a single observation, and other similar equations.

| n | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|-----|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 00 | | | .06745 | .04769 | .03894 | .03372 | .03016 | .02754 | .02549 | .02385 |
| 10 | .02248 | .02133 | .2034 | .1947 | .1871 | .1803 | .1742 | .1686 | .1636 | .1590 |
| 20 | .1547 | .1508 | .1472 | .1438 | .1406 | .1377 | .1349 | .1323 | .1298 | .1275 |
| 30 | .1252 | .1231 | .1211 | .1192 | .1174 | .1157 | .1140 | .1124 | .1109 | .1094 |
| 40 | .1080 | .1066 | .1053 | .1041 | .1029 | .1017 | .1005 | .0994 | .0984 | .0974 |
| 50 | .0964 | .0954 | .0944 | .0935 | .0926 | .0918 | .0909 | .0901 | .0893 | .0886 |
| 60 | .0878 | .0871 | .0864 | .0857 | .0850 | .0843 | .0837 | .0830 | .0824 | .0818 |
| 70 | .0812 | .0806 | .0800 | .0795 | .0789 | .0784 | .0779 | .0774 | .0769 | .0764 |
| 80 | .0759 | .0754 | .0749 | .0745 | .0740 | .0736 | .0732 | .0727 | .0723 | .0719 |
| 90 | .0715 | .0711 | .0707 | .0703 | .0699 | .0696 | .0692 | .0688 | .0685 | .0681 |

TABLES 27-29
LEAST SQUARES

TABLE 27.—Values of the factor $0.6745\sqrt{\frac{1}{n(n-1)}}$

This factor occurs in the equation $r_0 = 0.6745\sqrt{\frac{\sum v^2}{n(n-1)}}$ for the probable error of the arithmetical mean.

| $n =$ | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 00 | | | 0.4769 | 0.2754 | 0.1947 | 0.1508 | 0.1231 | 0.1041 | 0.0901 | 0.0795 |
| 10 | 0.0711 | 0.0643 | .0587 | .0540 | .0500 | .0465 | .0435 | .0409 | .0386 | .0365 |
| 20 | .0346 | .0329 | .0314 | .0300 | .0287 | .0275 | .0265 | .0255 | .0245 | .0237 |
| 30 | .0229 | .0221 | .0214 | .0208 | .0201 | .0196 | .0190 | .0185 | .0180 | .0175 |
| 40 | .0171 | .0167 | .0163 | .0159 | .0155 | .0152 | .0148 | .0145 | .0142 | .0139 |
| 50 | 0.0136 | 0.0134 | 0.0131 | 0.0128 | 0.0126 | 0.0124 | 0.0122 | 0.0119 | 0.0117 | 0.0115 |
| 60 | .0113 | .0111 | .0110 | .0108 | .0106 | .0105 | .0103 | .0101 | .0100 | .0098 |
| 70 | .0097 | .0096 | .0094 | .0093 | .0092 | .0091 | .0089 | .0088 | .0087 | .0086 |
| 80 | .0085 | .0084 | .0083 | .0082 | .0081 | .0080 | .0079 | .0078 | .0077 | .0076 |
| 90 | .0075 | .0075 | .0074 | .0073 | .0072 | .0071 | .0071 | .0070 | .0069 | .0068 |

TABLE 28.—Values of the factor $0.8453\sqrt{\frac{1}{n(n-1)}}$

This factor occurs in the approximate equation $r = 0.8453\frac{\sum |v|}{\sqrt{n(n-1)}}$ for the probable error of a single observation.

| $n =$ | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 00 | | | 0.5978 | 0.3451 | 0.2440 | 0.1890 | 0.1543 | 0.1304 | 0.1130 | 0.0996 |
| 10 | 0.0891 | 0.0806 | .0736 | .0677 | .0627 | .0583 | .0546 | .0513 | .0483 | .0457 |
| 20 | .0434 | .0412 | .0393 | .0376 | .0360 | .0345 | .0332 | .0319 | .0307 | .0297 |
| 30 | .0287 | .0277 | .0268 | .0260 | .0252 | .0245 | .0238 | .0232 | .0225 | .0220 |
| 40 | .0214 | .0209 | .0204 | .0199 | .0194 | .0190 | .0186 | .0182 | .0178 | .0174 |
| 50 | 0.0171 | 0.0167 | 0.0164 | 0.0161 | 0.0158 | 0.0155 | 0.0152 | 0.0150 | 0.0147 | 0.0145 |
| 60 | .0142 | .0140 | .0137 | .0135 | .0133 | .0131 | .0129 | .0127 | .0125 | .0123 |
| 70 | .0122 | .0120 | .0118 | .0117 | .0115 | .0113 | .0112 | .0111 | .0109 | .0108 |
| 80 | .0106 | .0105 | .0104 | .0102 | .0101 | .0100 | .0099 | .0098 | .0097 | .0096 |
| 90 | .0094 | .0093 | .0092 | .0091 | .0090 | .0089 | .0089 | .0088 | .0087 | .0086 |

TABLE 29.—Values of $0.8453\frac{1}{n\sqrt{n-1}}$

This factor occurs in the approximate equation $r_0 = 0.8453\frac{\sum |v|}{n\sqrt{n-1}}$ for the probable error of the arithmetical mean.

| $n =$ | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 00 | | | 0.4227 | 0.1993 | 0.1220 | 0.0845 | 0.0630 | 0.0493 | 0.0399 | 0.0332 |
| 10 | 0.0282 | 0.0243 | .0212 | .0188 | .0167 | .0151 | .0136 | .0124 | .0114 | .0105 |
| 20 | .0097 | .0090 | .0084 | .0078 | .0073 | .0069 | .0065 | .0061 | .0058 | .0055 |
| 30 | .0052 | .0050 | .0047 | .0045 | .0043 | .0041 | .0040 | .0038 | .0037 | .0035 |
| 40 | .0034 | .0033 | .0031 | .0030 | .0029 | .0028 | .0027 | .0027 | .0026 | .0025 |
| 50 | 0.0024 | 0.0023 | 0.0023 | 0.0022 | 0.0022 | 0.0021 | 0.0020 | 0.0020 | 0.0019 | 0.0019 |
| 60 | .0018 | .0018 | .0017 | .0017 | .0017 | .0016 | .0016 | .0016 | .0015 | .0015 |
| 70 | .0015 | .0014 | .0014 | .0014 | .0013 | .0013 | .0013 | .0013 | .0012 | .0012 |
| 80 | .0012 | .0012 | .0011 | .0011 | .0011 | .0011 | .0011 | .0010 | .0010 | .0010 |
| 90 | .0010 | .0010 | .0010 | .0009 | .0009 | .0009 | .0009 | .0009 | .0009 | .0009 |

$$\begin{array}{lcl} a_1z_1 + b_1z_2 + \dots + l_1z_q & = & M_1, \text{ weight } p_1 \\ a_2z_1 + b_2z_2 + \dots + l_2z_q & = & M_2, \text{ weight } p_2 \\ \vdots & & \vdots \\ a_nz_1 + b_nz_2 + \dots + l_nz_q & = & M_n, \text{ weight } p_n. \end{array}$$
$$\begin{aligned} [\text{paa}] &= p_1 a_1^2 + p_2 a_2^2 + \dots + p_n a_n^2, \\ [\text{pab}] &= p_1 a_1 b_1 + p_2 a_2 b_2 + \dots + p_n a_n b_n, \\ [\text{paM}] &= p_1 a_1 M_1 + p_2 a_2 M_2 + \dots + p_n a_n M_n. \end{aligned}$$
$$\begin{aligned} & [\text{paa}]z_1 + [\text{pab}]z_2 + \dots [\text{pal}]z_q = [\text{paM}] \\ & [\text{pab}]z_1 + [\text{pbb}]z_2 + \dots [\text{pbl}]z_q = [\text{pbM}] \\ & \vdots \\ & [\text{pla}]z_1 + [\text{plb}]z_2 + \dots [\text{pll}]z_q = [\text{plM}]. \end{aligned}$$
$$\begin{aligned} z_1 &= A_1[\text{paM}] + B_1[\text{pbM}] + \dots L_1[\text{plM}] \\ z_2 &= A_2[\text{paM}] + B_2[\text{pbM}] + \dots L_2[\text{plM}] \\ &\vdots \\ z_n &= A_n[\text{paM}] + B_n[\text{pbM}] + \dots L_n[\text{plM}], \end{aligned}$$
[illegible]
$$r = \text{probable error of observation of weight unity} \\ = 0.6745 \sqrt{\frac{\sum p v^2}{n-q}}. \quad (q \text{ unknowns.})$$
$$r = 0.6745 \sqrt{\frac{\sum v^2}{n-1}} = \frac{0.8453 \sum v}{\sqrt{n(n-1)}} \quad (\text{approx.}) = \text{probable error of observation of weight unity.}$$

$$r_o = 0.6745 \sqrt{\frac{\sum v^2}{n(n-1)}} = \frac{0.8453 \sum v}{n\sqrt{n-1}} \quad (\text{approx.}) = \text{probable error of mean.}$$
$$r = 0.6745 \sqrt{\frac{\sum p v^2}{n-1}}; r_0 = \frac{r}{\sqrt{\sum p}} = 0.6745 \sqrt{\frac{\sum p v^2}{(n-1) \sum p}}$$
$$Z = f(z_1, z_2, \dots)$$

$$R^2 = \left(\frac{\partial Z}{\partial z_1} \right)^2 r_1^2 + \left(\frac{\partial Z}{\partial z_2} \right)^2 r_2^2 + \dots$$

$$R^2 = r_1^2 + r_2^2 + \dots$$

$$R^2 = A^2 r_1^2 + B^2 r_2^2 + \dots$$

$$R^2 = z_1^2 r_1^2 + z_2^2 r_2^2.$$

1932.

TABLE 31
DIFFUSION INTEGRAL

$$\text{Inverse * values of } v/c = 1 - \frac{2}{\sqrt{\pi}} \int_0^q e^{-q^2} dq$$

$\log x = \log (2q) + \log \sqrt{kt}$. t expressed in seconds.

$= \log \delta + \log \sqrt{kt}$. t expressed in days.

$= \log \gamma + \log \sqrt{kt}$. " " years.

k = coefficient of diffusion.†

c = initial concentration.

v = concentration at distance x , time t .

| v/c | $\log 2q$ | $2q$ | $\log \delta$ | δ | $\log \gamma$ | γ |
|-------------|-----------|-----------|---------------|-----------|---------------|----------|
| 0.00 | $+\infty$ | $+\infty$ | $+\infty$ | $+\infty$ | ∞ | ∞ |
| .01 | 0.56143 | 3.6428 | 3.02970 | 1070.78 | 4.31098 | 20463. |
| .02 | .51719 | 3.2900 | 2.98545 | 967.04 | .26674 | 18481. |
| .03 | .48699 | 3.0690 | .95525 | 902.90 | .23654 | 17240. |
| .04 | .46306 | 2.9044 | .93132 | 853.73 | .21261 | 16316. |
| 0.05 | 0.44276 | 2.7718 | 2.91102 | 814.74 | 4.19231 | 15571. |
| .06 | .42486 | 2.6598 | .89311 | 781.83 | .17440 | 14942. |
| .07 | .40865 | 2.5624 | .87691 | 753.20 | .15820 | 14395. |
| .08 | .39372 | 2.4758 | .86198 | 727.75 | .14327 | 13908. |
| .09 | .37979 | 2.3977 | .84804 | 704.76 | .12933 | 13469. |
| 0.10 | 0.36664 | 2.3262 | 2.83490 | 683.75 | 4.11619 | 13067. |
| .11 | .35414 | 2.2602 | .82240 | 664.36 | .10369 | 12697. |
| .12 | .34218 | 2.1988 | .81044 | 646.31 | .09173 | 12352. |
| .13 | .33067 | 2.1413 | .79893 | 629.40 | .08022 | 12029. |
| .14 | .31954 | 2.0871 | .78780 | 613.47 | .06909 | 11724. |
| 0.15 | 0.30874 | 2.0358 | 2.77699 | 598.40 | 4.05828 | 11436. |
| .16 | .29821 | 1.9871 | .76647 | 584.08 | .04776 | 11162. |
| .17 | .28793 | 1.9406 | .75619 | 570.41 | .03748 | 10901. |
| .18 | .27786 | 1.8961 | .74612 | 557.34 | .02741 | 10652. |
| .19 | .26798 | 1.8534 | .73624 | 544.80 | .01753 | 10412. |
| 0.20 | 0.25825 | 1.8124 | 2.72651 | 532.73 | 4.00780 | 10181. |
| .21 | .24866 | 1.7728 | .71692 | 521.10 | 3.99821 | 9958.9 |
| .22 | .23919 | 1.7346 | .70745 | 509.86 | .98874 | 9744.1 |
| .23 | .22983 | 1.6976 | .69808 | 498.98 | .97937 | 9536.2 |
| .24 | .22055 | 1.6617 | .68880 | 488.43 | .97010 | 9334.6 |
| 0.25 | 0.21134 | 1.6268 | 2.67960 | 478.19 | 3.96089 | 9138.9 |
| .26 | .20220 | 1.5930 | .67046 | 468.23 | .95175 | 8948.5 |
| .27 | .19312 | 1.5600 | .66137 | 458.53 | .94266 | 8763.2 |
| .28 | .18407 | 1.5278 | .65232 | 449.08 | .93361 | 8582.5 |
| .29 | .17505 | 1.4964 | .64331 | 439.85 | .92460 | 8406.2 |
| 0.30 | 0.16606 | 1.4657 | 2.63431 | 430.84 | 3.91560 | 8233.9 |
| .31 | .15708 | 1.4357 | .62533 | 422.02 | .90662 | 8065.4 |
| .32 | .14810 | 1.4064 | .61636 | 413.39 | .89765 | 7900.4 |
| .33 | .13912 | 1.3776 | .60738 | 404.93 | .88867 | 7738.8 |
| .34 | .13014 | 1.3494 | .59840 | 396.64 | .87969 | 7580.3 |
| 0.35 | 0.12114 | 1.3217 | 2.58939 | 388.50 | 3.87068 | 7424.8 |
| .36 | .11211 | 1.2945 | .58037 | 380.51 | .86166 | 7272.0 |
| .37 | .10305 | 1.2678 | .57131 | 372.66 | .85260 | 7122.0 |
| .38 | .09396 | 1.2415 | .56222 | 364.93 | .84351 | 6974.4 |
| .39 | .08482 | 1.2157 | .55308 | 357.34 | .83437 | 6829.2 |
| 0.40 | 0.07563 | 1.1902 | 2.54389 | 349.86 | 3.82518 | 6686.2 |
| .41 | .06639 | 1.1652 | .53464 | 342.49 | .81593 | 6545.4 |
| .42 | .05708 | 1.1405 | .52533 | 335.22 | .80662 | 6406.6 |
| .43 | .04770 | 1.1161 | .51595 | 328.06 | .79724 | 6269.7 |
| .44 | .03824 | 1.0920 | .50650 | 320.99 | .78779 | 6134.6 |
| 0.45 | 0.02870 | 1.0683 | 2.49696 | 314.02 | 3.77825 | 6001.3 |
| .46 | .01907 | 1.0449 | .48733 | 307.13 | .76862 | 5869.7 |
| .47 | .00934 | 1.0217 | .47760 | 300.33 | .75889 | 5739.7 |
| .48 | 9.99951 | 0.99886 | .46776 | 293.60 | .74905 | 5611.2 |
| .49 | .98956 | 0.97624 | .45782 | 286.96 | .73911 | 5484.1 |
| 0.50 | 9.97949 | 0.95387 | 2.44775 | 280.38 | 3.72904 | 5358.4 |

† Kelvin, Mathematical and Physical Papers, vol. III. p. 428 ; Becker, Am. Jour. of Sci. vol. III. 1897, p. 280. * For direct values see table 2a.

TABLE 31 (continued)
DIFFUSION INTEGRAL

| v/c | $\log zq$ | zq | $\log \delta$ | δ | $\log \gamma$ | γ |
|-------------|-----------|---------|---------------|----------|---------------|----------|
| 0.50 | 9.97949 | 0.95387 | 2.44775 | 280.38 | 3.72904 | 5358.4 |
| .51 | .96929 | .93174 | .43755 | 273.87 | .71884 | 5234.1 |
| .52 | .95896 | .90983 | .42722 | 267.43 | .70851 | 5111.0 |
| .53 | .94848 | .88813 | .41674 | 261.06 | .69803 | 4986.1 |
| .54 | .93784 | .86665 | .40610 | 254.74 | .68739 | 4868.4 |
| 0.55 | 9.92704 | 0.84536 | 2.39530 | 248.48 | 3.67659 | 4748.9 |
| .56 | .91607 | .82426 | .38432 | 242.28 | .66561 | 4630.3 |
| .57 | .90490 | .80335 | .37316 | 236.13 | .65445 | 4512.8 |
| .58 | .89354 | .78260 | .36180 | 230.04 | .64309 | 4396.3 |
| .59 | .88197 | .76203 | .35023 | 223.99 | .63152 | 4280.7 |
| 0.60 | 9.87018 | 0.74161 | 2.33843 | 217.99 | 3.61973 | 4166.1 |
| .61 | .85815 | .72135 | .32640 | 212.03 | .60770 | 4052.2 |
| .62 | .84587 | .70124 | .31412 | 206.12 | .59541 | 3939.2 |
| .63 | .83332 | .68126 | .30157 | 200.25 | .58286 | 3827.0 |
| .64 | .82048 | .66143 | .28874 | 194.42 | .57003 | 3715.6 |
| 0.65 | 9.80734 | 0.64172 | 2.27560 | 188.63 | 3.55689 | 3604.9 |
| .66 | .79388 | .62213 | .26214 | 182.87 | .54343 | 3494.9 |
| .67 | .78008 | .60266 | .24833 | 177.15 | .52962 | 3385.4 |
| .68 | .76590 | .58331 | .23416 | 171.46 | .51545 | 3276.8 |
| .69 | .75133 | .56407 | .21959 | 165.80 | .50088 | 3168.7 |
| 0.70 | 9.73634 | 0.54493 | 2.20459 | 160.17 | 3.48588 | 3061.1 |
| .71 | .72089 | .52588 | .18915 | 154.58 | .47044 | 2954.2 |
| .72 | .70495 | .50694 | .17321 | 149.01 | .45450 | 2847.7 |
| .73 | .68849 | .48808 | .15675 | 143.47 | .43804 | 2741.8 |
| .74 | .67146 | .46931 | .13972 | 137.95 | .42101 | 2636.4 |
| 0.75 | 9.65381 | 0.45062 | 2.12207 | 132.46 | 3.40336 | 2531.4 |
| .76 | .63550 | .43202 | .10376 | 126.99 | .38505 | 2426.9 |
| .77 | .61646 | .41348 | .08471 | 121.54 | .36600 | 2322.7 |
| .78 | .59662 | .39502 | .06487 | 116.11 | .34616 | 2219.0 |
| .79 | .57590 | .37662 | .04416 | 110.70 | .32545 | 2115.7 |
| 0.80 | 9.55423 | 0.35829 | 2.02249 | 105.31 | 3.30378 | 2012.7 |
| .81 | .53150 | .34001 | 1.99975 | 99.943 | .28104 | 1910.0 |
| .82 | .50758 | .32180 | .97584 | 94.589 | .25713 | 1807.7 |
| .83 | .48235 | .30363 | .95061 | 89.250 | .23190 | 1705.7 |
| .84 | .45564 | .28552 | .92389 | 83.926 | .20518 | 1603.9 |
| 0.85 | 9.42725 | 0.26745 | 1.89551 | 78.615 | 3.17680 | 1502.4 |
| .86 | .39695 | .24943 | .86521 | 73.317 | .14650 | 1401.2 |
| .87 | .36445 | .23145 | .83271 | 68.032 | .11400 | 1300.2 |
| .88 | .32940 | .21350 | .79766 | 62.757 | .07895 | 1199.4 |
| .89 | .29135 | .19559 | .75961 | 57.492 | 3.04090 | 1098.7 |
| 0.90 | 9.24972 | 0.17771 | 1.71797 | 52.236 | 2.99926 | 998.31 |
| .91 | .20374 | .15986 | .67200 | 46.889 | .95320 | 898.03 |
| .92 | .15239 | .14203 | .62065 | 41.750 | .90194 | 797.89 |
| .93 | .09423 | .12423 | .56249 | 36.516 | .84378 | 697.88 |
| .94 | .02714 | .10645 | .49539 | 31.289 | .77668 | 597.98 |
| 0.95 | 8.94783 | 0.08868 | 1.41609 | 26.067 | 2.69738 | 498.17 |
| .96 | .85082 | .07093 | .31907 | 20.848 | .60036 | 398.44 |
| .97 | .72580 | .05319 | .19406 | 15.633 | .47535 | 298.78 |
| .98 | .54965 | .03545 | .01791 | 10.421 | .29920 | 199.16 |
| .99 | .24859 | .01773 | 0.71684 | 5.21007 | 1.99813 | 99.571 |
| 1.00 | $-\infty$ | 0.00000 | $-\infty$ | 0.00000 | $-\infty$ | 0.000 |

VALUES OF THE EXPONENTIAL INTEGRAL

$$Ei(x) = \int_{-\infty}^{-x} (e^{-u}/u) du$$

| <i>x</i> | <i>Ei(x)</i> | <i>Ei(-x)</i> | <i>x</i> | <i>Ei(x)</i> | <i>Ei(-x)</i> |
|----------|--------------|---------------|----------|--------------|---------------|
| 0.00 | — ∞ | — ∞ | 0.50 | +0.454 220 | —0.559 774 |
| .01 | —4.017 929 | —4.037 930 | .51 | 0.487 032 | —0.547 822 |
| .02 | —3.314 707 | —3.354 708 | .52 | 0.519 531 | —0.536 220 |
| .03 | —2.899 116 | —2.959 119 | .53 | 0.551 730 | —0.524 952 |
| .04 | —2.601 257 | —2.681 264 | .54 | 0.583 646 | —0.514 004 |
| 0.05 | —2.367 885 | —2.467 898 | 0.55 | +0.615 291 | —0.503 364 |
| .06 | —2.175 283 | —2.295 307 | .56 | 0.646 677 | —0.493 020 |
| .07 | —2.010 800 | —2.150 838 | .57 | 0.677 819 | —0.482 960 |
| .08 | —1.866 884 | —2.026 941 | .58 | 0.708 726 | —0.473 173 |
| .09 | —1.738 664 | —1.918 745 | .59 | 0.739 410 | —0.463 650 |
| 0.10 | —1.622 813 | —1.822 924 | 0.60 | +0.769 881 | —0.454 380 |
| .11 | —1.516 959 | —1.737 107 | .61 | 0.800 150 | —0.445 353 |
| .12 | —1.419 350 | —1.659 542 | .62 | 0.830 226 | —0.436 562 |
| .13 | —1.328 655 | —1.588 899 | .63 | 0.860 119 | —0.427 997 |
| .14 | —1.243 841 | —1.524 146 | .64 | 0.889 836 | —0.419 652 |
| 0.15 | —1.164 086 | —1.464 462 | 0.65 | +0.919 386 | —0.411 517 |
| .16 | —1.088 731 | —1.409 187 | .66 | 0.948 778 | —0.403 586 |
| .17 | —1.017 234 | —1.357 781 | .67 | 0.978 019 | —0.395 853 |
| .18 | —0.949 148 | —1.309 796 | .68 | 1.007 116 | —0.388 309 |
| .19 | —0.884 095 | —1.264 858 | .69 | 1.036 077 | —0.380 950 |
| 0.20 | —0.821 761 | —1.222 651 | 0.70 | +1.064 907 | —0.373 769 |
| .21 | —0.761 872 | —1.182 902 | .71 | 1.093 615 | —0.366 760 |
| .22 | —0.704 195 | —1.145 380 | .72 | 1.122 205 | —0.359 918 |
| .23 | —0.648 529 | —1.109 883 | .73 | 1.150 684 | —0.353 237 |
| .24 | —0.594 697 | —1.076 235 | .74 | 1.179 058 | —0.346 713 |
| 0.25 | —0.542 543 | —1.044 283 | 0.75 | +1.207 333 | —0.340 341 |
| .26 | —0.491 932 | —1.013 889 | .76 | 1.235 513 | —0.334 115 |
| .27 | —0.442 741 | —0.984 933 | .77 | 1.263 605 | —0.328 032 |
| .28 | —0.394 863 | —0.957 308 | .78 | 1.291 613 | —0.322 088 |
| .29 | —0.348 202 | —0.930 918 | .79 | 1.319 542 | —0.316 277 |
| 0.30 | —0.302 669 | —0.905 677 | 0.80 | +1.347 397 | —0.310 597 |
| .31 | —0.258 186 | —0.881 506 | .81 | 1.375 182 | —0.305 043 |
| .32 | —0.214 683 | —0.858 335 | .82 | 1.402 902 | —0.299 611 |
| .33 | —0.172 095 | —0.836 101 | .83 | 1.430 561 | —0.294 299 |
| .34 | —0.130 363 | —0.814 746 | .84 | 1.458 164 | —0.289 103 |
| 0.35 | —0.089 434 | —0.794 215 | 0.85 | +1.485 714 | —0.284 019 |
| .36 | —0.049 258 | —0.774 462 | .86 | 1.513 216 | —0.279 045 |
| .37 | —0.009 790 | —0.755 441 | .87 | 1.540 673 | —0.274 177 |
| .38 | +0.029 011 | —0.737 112 | .88 | 1.568 089 | —0.269 413 |
| .39 | +0.067 185 | —0.719 437 | .89 | 1.595 467 | —0.264 749 |
| 0.40 | +0.104 765 | —0.702 380 | 0.90 | +1.622 812 | —0.260 184 |
| .41 | +0.141 786 | —0.685 910 | .91 | 1.650 126 | —0.255 714 |
| .42 | +0.178 278 | —0.669 997 | .92 | 1.677 413 | —0.251 336 |
| .43 | +0.214 270 | —0.654 613 | .93 | 1.704 677 | —0.247 050 |
| .44 | +0.249 787 | —0.639 733 | .94 | 1.731 920 | —0.242 851 |
| 0.45 | +0.284 855 | —0.625 331 | 0.95 | +1.759 146 | —0.238 738 |
| .46 | 0.319 497 | —0.611 387 | .96 | 1.786 357 | —0.234 708 |
| .47 | 0.353 735 | —0.597 877 | .97 | 1.813 557 | —0.230 760 |
| .48 | 0.387 589 | —0.584 784 | .98 | 1.840 749 | —0.226 891 |
| .49 | 0.421 078 | —0.572 089 | .99 | 1.867 935 | —0.223 100 |
| 0.50 | +0.454 220 | —0.559 774 | 1.00 | +1.895 118 | —0.219 384 |

(Taken from Glaisher, Philos. Trans., 160, 367, 1870)

VALUES OF EXPONENTIAL INTEGRAL

$$Ei(x) = \int_{-\infty}^{-x} (e^{-u}/u) du$$

| <i>x</i> | <i>Ei</i> (<i>x</i>) | <i>Ei</i> —(<i>x</i>) | <i>x</i> | <i>Ei</i> (<i>x</i>) | <i>Ei</i> —(<i>x</i>) |
|----------|------------------------|-------------------------|----------|------------------------|-------------------------|
| 1.0 | +1.895 118 | —0.219 384 | 3.0 | + 9.933 833 | —0.013 0484 |
| 1.1 | 2.167 378 | —0.185 991 | 3.1 | 10.626 300 | —0.011 4944 |
| 1.2 | 2.442 092 | —0.158 408 | 3.2 | 11.367 303 | —0.010 1330 |
| 1.3 | 2.721 399 | —0.135 451 | 3.3 | 12.161 041 | —0.008 9390 |
| 1.4 | 3.007 207 | —0.116 219 | 3.4 | 13.012 075 | —0.007 8910 |
| 1.5 | +3.301 285 | —0.100 020 | 3.5 | +13.925 354 | —0.006 9701 |
| 1.6 | 3.605 320 | —0.086 3083 | 3.6 | 14.906 254 | —0.006 1604 |
| 1.7 | 3.920 963 | —0.074 6546 | 3.7 | 15.960 619 | —0.005 4478 |
| 1.8 | 4.249 868 | —0.064 7131 | 3.8 | 17.094 802 | —0.004 8202 |
| 1.9 | 4.593 714 | —0.056 2044 | 3.9 | 18.315 714 | —0.004 2671 |
| 2.0 | +4.954 234 | —0.048 9005 | 4.0 | +19.630 874 | —0.003 7794 |
| 2.1 | 5.333 235 | —0.042 6143 | 4.1 | 21.048 467 | —0.003 3489 |
| 2.2 | 5.732 615 | —0.037 1911 | 4.2 | 22.577 401 | —0.002 9688 |
| 2.3 | 6.154 381 | —0.032 5023 | 4.3 | 24.227 380 | —0.002 6329 |
| 2.4 | 6.600 670 | —0.028 4403 | 4.4 | 26.008 973 | —0.002 3360 |
| 2.5 | +7.073 766 | —0.024 9149 | 4.5 | +27.933 697 | —0.002 0734 |
| 2.6 | 7.576 115 | —0.021 8502 | 4.6 | 30.014 099 | —0.001 8410 |
| 2.7 | 8.110 347 | —0.019 1819 | 4.7 | 32.263 860 | —0.001 6352 |
| 2.8 | 8.679 298 | —0.016 8553 | 4.8 | 34.697 890 | —0.001 4530 |
| 2.9 | 9.286 024 | —0.014 8240 | 4.9 | 37.332 451 | —0.001 2915 |
| 3.0 | +9.933 833 | —0.013 0484 | 5.0 | +40.185 275 | —0.001 1483 |
| <i>x</i> | <i>Ei</i> (<i>x</i>) | <i>Ei</i> (— <i>x</i>) | | | |
| 6 | + 85.989 762 | — 0.000 360 082 | | | |
| 7 | + 191.504 743 | — .000 115 482 | | | |
| 8 | + 440.379 900 | — .000 037 665 6 | | | |
| 9 | + 1037.878 291 | — .000 012 447 4 | | | |
| 10 | + 2492.228 976 | — .000 004 156 97 | | | |
| 11 | + 6071.406 374 | — .000 001 400 30 | | | |
| 12 | + 14959.532 666 | — .000 000 475 11 | | | |
| 13 | + 37197.688 491 | — .000 000 162 19 | | | |
| 14 | + 93192.513 634 | — .000 000 055 66 | | | |
| 15 | + 234955.852 491 | — .000 000 019 18 | | | |

(Taken from Glaisher, Philos. Trans., 160, 367, 1870)

GAMMA FUNCTION *

$$\text{Value of } \log \int_0^\infty e^{-x} x^{n-1} dx + 10$$

Values of the logarithms + 10 of the "Second Eulerian Integral" (Gamma function) $\int_0^\infty e^{-x} x^{n-1} dx = \log \Gamma(n) + 10$ for values of n between 1 and 2. When n has values not lying between 1 and 2 the value of the function can be readily calculated from the equation $\Gamma(n+1) = n\Gamma(n) = n(n-1) \dots (n-r)\Gamma(n-r)$.

| n | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|-------------|-----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1.00 | 9.99— | 97497 | 95001 | 92512 | 90030 | 87555 | 85087 | 82627 | 80173 | 77727 |
| 1.01 | 75287 | 72855 | 70430 | 68011 | 65600 | 63196 | 60798 | 58408 | 56025 | 53648 |
| 1.02 | 51279 | 48916 | 46561 | 44212 | 41870 | 39535 | 37207 | 34886 | 32572 | 30265 |
| 1.03 | 27964 | 25671 | 23384 | 21104 | 18831 | 16564 | 14305 | 12052 | 9806 | 7567 |
| 1.04 | 95334 | 93108 | 90889 | 88677 | 86471 | 84273 | 82080 | 79895 | 77716 | 75544 |
| 1.05 | 9.9883379 | 81220 | 79068 | 76922 | 74783 | 72651 | 70525 | 68406 | 66294 | 64188 |
| 1.06 | 62089 | 59996 | 57910 | 55830 | 53757 | 51690 | 49630 | 47577 | 45530 | 43489 |
| 1.07 | 41455 | 39428 | 37407 | 35392 | 33384 | 31382 | 29387 | 27398 | 25415 | 23430 |
| 1.08 | 21469 | 19506 | 17549 | 15599 | 13655 | 11717 | 9785 | 7860 | 5941 | 4029 |
| 1.09 | 02123 | 00223 | 98329 | 96442 | 94561 | 92686 | 90818 | 88956 | 87100 | 85250 |
| 1.10 | 9.9783407 | 81570 | 79738 | 77914 | 76095 | 74283 | 72476 | 70676 | 68882 | 67095 |
| 1.11 | 65313 | 63538 | 61768 | 60005 | 58248 | 56497 | 54753 | 53014 | 51281 | 49555 |
| 1.12 | 47834 | 46120 | 44411 | 42709 | 41013 | 39323 | 37638 | 35960 | 34288 | 32622 |
| 1.13 | 30962 | 29308 | 27659 | 26017 | 24381 | 22751 | 21126 | 19508 | 17896 | 16289 |
| 1.14 | 14689 | 13094 | 11505 | 9922 | 8345 | 6774 | 5209 | 3650 | 2096 | 0549 |
| 1.15 | 9.9699007 | 97471 | 95941 | 94417 | 92898 | 91386 | 89879 | 88378 | 86883 | 85393 |
| 1.16 | 83910 | 82432 | 80960 | 79493 | 78033 | 76578 | 75129 | 73686 | 72248 | 70816 |
| 1.17 | 69390 | 67969 | 66554 | 65145 | 63742 | 62344 | 60952 | 59566 | 58185 | 56810 |
| 1.18 | 55440 | 54076 | 52718 | 51366 | 50019 | 48677 | 47341 | 46011 | 44687 | 43368 |
| 1.19 | 42034 | 40746 | 39444 | 38147 | 36856 | 35570 | 34290 | 33016 | 31747 | 30483 |
| 1.20 | 9.9629225 | 27973 | 26725 | 25484 | 24248 | 23017 | 21792 | 20573 | 19358 | 18150 |
| 1.21 | 16946 | 15748 | 14556 | 13369 | 12188 | 11011 | 98341 | 86675 | 75015 | 63361 |
| 1.22 | 05212 | 04068 | 02930 | 01796 | 00669 | 99546 | 98430 | 97318 | 96212 | 95111 |
| 1.23 | 594015 | 52925 | 91840 | 90760 | 89685 | 88616 | 87553 | 86494 | 85441 | 84393 |
| 1.24 | 83350 | 82313 | 81280 | 80253 | 79232 | 78215 | 77204 | 76198 | 75197 | 74201 |
| 1.25 | 9.9573211 | 72226 | 71246 | 70271 | 69301 | 68337 | 67377 | 66423 | 65474 | 64530 |
| 1.26 | 63592 | 62658 | 61730 | 60806 | 59888 | 58975 | 58067 | 57165 | 56267 | 55374 |
| 1.27 | 54487 | 53604 | 52727 | 51855 | 50988 | 50126 | 49268 | 48416 | 47570 | 46728 |
| 1.28 | 45891 | 45059 | 44232 | 43410 | 42593 | 41782 | 40975 | 40173 | 39376 | 38585 |
| 1.29 | 37798 | 37016 | 36239 | 35467 | 34700 | 33938 | 33181 | 32429 | 31682 | 30940 |
| 1.30 | 9.9530203 | 29470 | 28743 | 28021 | 27303 | 26590 | 25883 | 25180 | 24482 | 23789 |
| 1.31 | 23100 | 22417 | 21739 | 21065 | 20396 | 19732 | 19073 | 18419 | 17770 | 17125 |
| 1.32 | 16485 | 15850 | 15220 | 14595 | 13975 | 13359 | 12748 | 12142 | 11541 | 10944 |
| 1.33 | 10353 | 99766 | 96184 | 92606 | 89034 | 85466 | 81903 | 78344 | 74791 | 71242 |
| 1.34 | 04698 | 04158 | 03624 | 03094 | 02568 | 02048 | 01532 | 01021 | 00514 | 00012 |
| 1.35 | 9.9499515 | 99023 | 98535 | 98052 | 97573 | 97100 | 96630 | 96166 | 95706 | 95251 |
| 1.36 | 94800 | 94355 | 93913 | 93477 | 93044 | 92617 | 92194 | 91776 | 91362 | 90953 |
| 1.37 | 90549 | 90149 | 89754 | 89363 | 88977 | 88595 | 88218 | 87846 | 87478 | 87115 |
| 1.38 | 86756 | 86402 | 86052 | 85707 | 85366 | 85030 | 84698 | 84371 | 84049 | 83731 |
| 1.39 | 83417 | 83108 | 82803 | 82503 | 82208 | 81916 | 81630 | 81348 | 81070 | 80797 |
| 1.40 | 9.9480528 | 80263 | 80003 | 79748 | 79497 | 79250 | 79008 | 78770 | 78537 | 78308 |
| 1.41 | 76084 | 77864 | 77648 | 77437 | 77230 | 77027 | 76829 | 76636 | 76446 | 76261 |
| 1.42 | 76081 | 75905 | 75733 | 75565 | 75402 | 75243 | 75089 | 74939 | 74793 | 74652 |
| 1.43 | 74515 | 74382 | 74254 | 74130 | 74010 | 73894 | 73783 | 73676 | 73574 | 73476 |
| 1.44 | 73382 | 73292 | 73207 | 73125 | 73049 | 72976 | 72908 | 72844 | 72784 | 72728 |

* Legendre's "Exercices de Calcul Intégral," tome ii.

GAMMA FUNCTION

| <i>n</i> | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|-------------|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 1.45 | 9.9472677 | 72630 | 72587 | 72549 | 72514 | 72484 | 72459 | 72437 | 72419 | 72406 |
| 1.46 | 72397 | 72393 | 72392 | 72396 | 72404 | 72416 | 72432 | 72452 | 72477 | 72506 |
| 1.47 | 72539 | 72576 | 72617 | 72662 | 72712 | 72766 | 72824 | 72886 | 72952 | 73022 |
| 1.48 | 73097 | 73175 | 73258 | 73345 | 73436 | 73531 | 73630 | 73734 | 73841 | 73953 |
| 1.49 | 74068 | 74188 | 74312 | 74440 | 74572 | 74708 | 74848 | 74992 | 75141 | 75293 |
| 1.50 | 9.9475449 | 75610 | 75774 | 75943 | 76116 | 76292 | 76473 | 76658 | 76847 | 77040 |
| 1.51 | 77237 | 77437 | 77642 | 77851 | 78064 | 78281 | 78502 | 78727 | 78956 | 79189 |
| 1.52 | 79426 | 79667 | 79912 | 80161 | 80414 | 80671 | 80932 | 81196 | 81465 | 81738 |
| 1.53 | 82015 | 82295 | 82580 | 82868 | 83161 | 83457 | 83758 | 84062 | 84370 | 84682 |
| 1.54 | 84998 | 85318 | 85642 | 85970 | 86302 | 86638 | 86977 | 87321 | 87668 | 88019 |
| 1.55 | 9.9488374 | 88733 | 89096 | 89463 | 89834 | 90208 | 90587 | 90969 | 91355 | 91745 |
| 1.56 | 92139 | 92537 | 92938 | 93344 | 93753 | 94166 | 94583 | 95004 | 95429 | 95857 |
| 1.57 | 96289 | 96725 | 97165 | 97609 | 98056 | 98508 | 98963 | 99422 | 99885 | 100351 |
| 1.58 | 500822 | 01296 | 01774 | 02255 | 02741 | 03230 | 03723 | 04220 | 04720 | 05225 |
| 1.59 | 05733 | 06245 | 06760 | 07280 | 07803 | 08330 | 08860 | 09395 | 09933 | 10475 |
| 1.60 | 9.9511020 | 11569 | 12122 | 12679 | 13240 | 13804 | 14372 | 14943 | 15519 | 16098 |
| 1.61 | 16680 | 17267 | 17857 | 18451 | 19048 | 19649 | 20254 | 20862 | 21475 | 22091 |
| 1.62 | 22710 | 23333 | 23960 | 24591 | 25225 | 25863 | 26504 | 27149 | 27798 | 28451 |
| 1.63 | 29107 | 29766 | 30430 | 31097 | 31767 | 32442 | 33120 | 33801 | 34486 | 35175 |
| 1.64 | 35867 | 36563 | 37263 | 37966 | 38673 | 39383 | 40097 | 40815 | 41536 | 42260 |
| 1.65 | 9.9542989 | 43721 | 44456 | 45195 | 45938 | 46684 | 47434 | 48187 | 48944 | 49704 |
| 1.66 | 50468 | 51236 | 52007 | 52782 | 53560 | 54342 | 55127 | 55916 | 56708 | 57504 |
| 1.67 | 58303 | 59106 | 59913 | 60723 | 61536 | 62353 | 63174 | 63998 | 64825 | 65656 |
| 1.68 | 66491 | 67329 | 68170 | 69015 | 69864 | 70716 | 71571 | 72430 | 73293 | 74159 |
| 1.69 | 75028 | 75901 | 76777 | 77657 | 78540 | 79427 | 80317 | 81211 | 82108 | 83008 |
| 1.70 | 9.9583912 | 84820 | 85731 | 86645 | 87563 | 88484 | 89409 | 90337 | 91268 | 92203 |
| 1.71 | 93141 | 94083 | 95028 | 95977 | 96929 | 97884 | 98843 | 99805 | 100771 | 101740 |
| 1.72 | 102712 | 103688 | 104667 | 105650 | 106636 | 107625 | 108618 | 109614 | 110613 | 111616 |
| 1.73 | 12622 | 13632 | 14645 | 15661 | 16681 | 17704 | 18730 | 19760 | 20793 | 21830 |
| 1.74 | 22869 | 23912 | 24959 | 26009 | 27062 | 28118 | 29178 | 30241 | 31308 | 32377 |
| 1.75 | 9.9633451 | 34527 | 35607 | 36690 | 37776 | 38866 | 39959 | 41055 | 42155 | 43258 |
| 1.76 | 44364 | 45473 | 46586 | 47702 | 48821 | 49944 | 51070 | 52199 | 53331 | 54467 |
| 1.77 | 55606 | 56749 | 57894 | 59043 | 60195 | 61350 | 62509 | 63671 | 64836 | 66004 |
| 1.78 | 67176 | 68351 | 69529 | 70710 | 71895 | 73082 | 74274 | 75468 | 76665 | 77866 |
| 1.79 | 79070 | 80277 | 81488 | 82701 | 83918 | 85138 | 86361 | 87588 | 88818 | 90051 |
| 1.80 | 9.9691287 | 92526 | 93768 | 95014 | 96263 | 97515 | 98770 | 100029 | 101291 | 102555 |
| 1.81 | 703823 | 05095 | 06369 | 07646 | 08927 | 10211 | 11498 | 12788 | 14082 | 15378 |
| 1.82 | 16678 | 17981 | 19287 | 20596 | 21908 | 23224 | 24542 | 25864 | 27189 | 28517 |
| 1.83 | 29848 | 31182 | 32520 | 33860 | 35204 | 36551 | 37900 | 39254 | 40610 | 41969 |
| 1.84 | 43331 | 44697 | 46065 | 47437 | 48812 | 50190 | 51571 | 52955 | 54342 | 55733 |
| 1.85 | 9.9757126 | 58522 | 59922 | 61325 | 62730 | 64139 | 65551 | 66966 | 68384 | 69805 |
| 1.86 | 71230 | 72657 | 74087 | 75521 | 76957 | 78397 | 79839 | 81285 | 82734 | 84186 |
| 1.87 | 85640 | 87098 | 88559 | 90023 | 91490 | 92960 | 94433 | 95909 | 97389 | 98871 |
| 1.88 | 800356 | 01844 | 03335 | 04830 | 06327 | 07827 | 09331 | 10837 | 12346 | 13859 |
| 1.89 | 15374 | 16893 | 18414 | 19939 | 21466 | 22996 | 24530 | 26066 | 27606 | 29148 |
| 1.90 | 9.9830693 | 32242 | 33793 | 35348 | 36905 | 38465 | 40028 | 41595 | 43164 | 44736 |
| 1.91 | 46311 | 47809 | 49471 | 51055 | 52642 | 54232 | 55825 | 57421 | 59020 | 60621 |
| 1.92 | 62226 | 63844 | 65445 | 67058 | 68675 | 70294 | 71917 | 73542 | 75170 | 76802 |
| 1.93 | 78436 | 80073 | 81713 | 83356 | 85002 | 86651 | 88302 | 89957 | 91614 | 93275 |
| 1.94 | 94938 | 96605 | 98274 | 99946 | 01621 | 03299 | 04980 | 06663 | 08350 | 10039 |
| 1.95 | 9.9911732 | 13427 | 15125 | 16826 | 18530 | 20237 | 21947 | 23659 | 25375 | 27093 |
| 1.96 | 28815 | 30539 | 32266 | 33995 | 35728 | 37464 | 39202 | 40943 | 42688 | 44435 |
| 1.97 | 46185 | 47937 | 49693 | 51451 | 53213 | 54977 | 56744 | 58513 | 60286 | 62062 |
| 1.98 | 63840 | 65621 | 67405 | 69192 | 70982 | 72774 | 74570 | 76368 | 78169 | 79972 |
| 1.99 | 81779 | 83588 | 85401 | 87216 | 89034 | 90854 | 92678 | 94504 | 96333 | 98165 |

TABLE 34
ZONAL SPHERICAL HARMONICS*

| Degrees | P ₁ | P ₂ | P ₃ | P ₄ | P ₅ | P ₆ | P ₇ |
|---------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|
| 0 | + 1.0000 | + 1.0000 | + 1.0000 | + 1.0000 | + 1.0000 | + 1.0000 | + 1.0000 |
| 1 | .9998 | .9995 | .9991 | .9985 | .9977 | .9968 | .9957 |
| 2 | .9994 | .9982 | .9963 | .9939 | .9909 | .9872 | .9830 |
| 3 | .9986 | .9959 | .9918 | .9863 | .9795 | .9714 | .9620 |
| 4 | .9976 | .9927 | .9854 | .9758 | .9638 | .9495 | .9329 |
| 5 | + 0.9962 | + 0.9886 | + 0.9773 | + 0.9623 | + 0.9437 | + 0.9216 | + 0.8962 |
| 6 | .9945 | .9836 | .9674 | .9459 | .9194 | .8881 | .8522 |
| 7 | .9925 | .9777 | .9557 | .9267 | .8911 | .8492 | .8016 |
| 8 | .9903 | .9709 | .9423 | .9048 | .8589 | .8054 | .7449 |
| 9 | .9877 | .9633 | .9273 | .8803 | .8232 | .7570 | .6830 |
| 10 | + 0.9848 | + 0.9548 | + 0.9106 | + 0.8532 | + 0.7840 | + 0.7045 | + 0.6164 |
| 11 | .9816 | .9454 | .8923 | .8238 | .7417 | .6483 | .5462 |
| 12 | .9781 | .9352 | .8724 | .7920 | .6966 | .5891 | .4731 |
| 13 | .9744 | .9241 | .8511 | .7582 | .6489 | .5273 | .3980 |
| 14 | .9703 | .9122 | .8283 | .7224 | .5990 | .4635 | .3218 |
| 15 | + 0.9659 | + 0.8995 | + 0.8042 | + 0.6847 | + 0.5471 | + 0.3983 | + 0.2455 |
| 16 | .9613 | .8860 | .7787 | .6454 | .4937 | .3323 | + .1700 |
| 17 | .9563 | .8718 | .7519 | .6046 | .4391 | .2661 | + .0961 |
| 18 | .9511 | .8568 | .7240 | .5624 | .3836 | .2002 | + .0248 |
| 19 | .9455 | .8410 | .6950 | .5192 | .3276 | .1353 | — .0433 |
| 20 | + 0.9397 | + 0.8245 | + 0.6649 | + 0.4750 | + 0.2715 | + 0.0719 | — 0.1972 |
| 21 | .9336 | .8074 | .6338 | .4300 | .2156 | + .0166 | .1664 |
| 22 | .9272 | .7895 | .6019 | .3845 | .1602 | — .0481 | .2202 |
| 23 | .9205 | .7710 | .5692 | .3386 | .1057 | — .1038 | .2680 |
| 24 | .9135 | .7518 | .5357 | .2926 | .0525 | — .1558 | .3094 |
| 25 | + 0.9063 | + 0.7321 | + 0.5016 | + 0.2465 | + 0.0009 | — 0.2040 | — 0.3441 |
| 26 | .8988 | .7117 | .4670 | .2007 | — .0489 | .2478 | .3717 |
| 27 | .8910 | .6908 | .4319 | .1553 | — .0964 | .2869 | .3922 |
| 28 | .8829 | .6694 | .3964 | .1105 | — .1415 | .3212 | .4053 |
| 29 | .8746 | .6474 | .3607 | .0665 | — .1839 | .3502 | .4113 |
| 30 | + 0.8660 | + 0.6250 | + 0.3248 | + 0.0234 | — 0.2233 | — 0.3740 | — 0.4102 |
| 31 | .8572 | .6021 | .2887 | — .0185 | .2595 | .3924 | .4022 |
| 32 | .8480 | .5788 | .2527 | — .0591 | .2923 | .4053 | .3877 |
| 33 | .8387 | .5551 | .2167 | — .0982 | .3216 | .4127 | .3671 |
| 34 | .8290 | .5310 | .1809 | — .1357 | .3473 | .4147 | .3409 |
| 35 | + 0.8192 | + 0.5065 | + 0.1454 | — 0.1714 | — 0.3691 | — 0.4114 | — 0.3096 |
| 36 | .8090 | .4818 | .1102 | .2052 | .3871 | .4031 | .2738 |
| 37 | .7986 | .4567 | .0755 | .2370 | .4011 | .3898 | .2343 |
| 38 | .7880 | .4314 | .0413 | .2666 | .4112 | .3719 | .1918 |
| 39 | .7771 | .4059 | .0077 | .2940 | .4174 | .3497 | .1470 |
| 40 | + 0.7660 | + 0.3802 | — 0.0252 | — 0.3190 | — 0.4197 | — 0.3236 | — 0.1006 |
| 41 | .7547 | .3544 | .0574 | .3416 | .4181 | .2939 | — .0535 |
| 42 | .7431 | .3284 | .0887 | .3616 | .4128 | .2610 | — .0064 |
| 43 | .7314 | .3023 | .1191 | .3791 | .4038 | .2255 | + .0398 |
| 44 | .7193 | .2762 | .1485 | .3940 | .3914 | .1878 | + .0846 |
| 45 | + 0.7071 | + 0.2500 | — 0.1768 | — 0.4063 | — 0.3757 | — 0.1484 | + 0.1271 |
| 46 | .6947 | .2238 | .2040 | .4158 | .3568 | — .1078 | .1667 |
| 47 | .6820 | .1977 | .2300 | .4227 | .3350 | — .0665 | .2028 |
| 48 | .6691 | .1716 | .2547 | .4270 | .3105 | — .0251 | .2350 |
| 49 | .6561 | .1456 | .2781 | .4286 | .2836 | + .0161 | .2626 |
| 50 | + 0.6428 | + 0.1198 | — 0.3002 | — 0.4275 | — 0.2545 | + 0.0564 | + 0.2854 |

* Calculated by Mr. C. E. Van Orstrand for this publication.

ZONAL SPHERICAL HARMONICS

| Degrees | P ₁ | P ₂ | P ₃ | P ₄ | P ₅ | P ₆ | P ₇ |
|---------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|
| 50 | + 0.6428 | + 0.1198 | — 0.3002 | — 0.4275 | — 0.2545 | + 0.0564 | + 0.2854 |
| 51 | .6293 | .0941 | .3209 | .4239 | .2235 | .0954 | .3031 |
| 52 | .6157 | .0686 | .3401 | .4178 | .1910 | .1326 | .3154 |
| 53 | .6018 | .0433 | .3578 | .4093 | .1571 | .1677 | .3221 |
| 54 | .5878 | .0182 | .3740 | .3984 | .1223 | .2002 | .3234 |
| 55 | + 0.5736 | — 0.0065 | — 0.3886 | — 0.3852 | — 0.0868 | + 0.2297 | + 0.3191 |
| 56 | .5592 | .0310 | .4016 | .3698 | — .0509 | .2560 | .3095 |
| 57 | .5446 | .0551 | .4131 | .3524 | — .0150 | .2787 | .2947 |
| 58 | .5299 | .0788 | .4229 | .3331 | + .0206 | .2976 | .2752 |
| 59 | .5150 | .1021 | .4310 | .3119 | + .0557 | .3125 | .2512 |
| 60 | + 0.5000 | — 0.1250 | — 0.4375 | — 0.2891 | + 0.0898 | + 0.3232 | + 0.2231 |
| 61 | .4848 | .1474 | .4423 | .2647 | .1229 | .3298 | .1916 |
| 62 | .4695 | .1694 | .4455 | .2390 | .1545 | .3321 | .1572 |
| 63 | .4540 | .1908 | .4471 | .2121 | .1844 | .3302 | .1203 |
| 64 | .4384 | .2117 | .4470 | .1841 | .2123 | .3240 | .0818 |
| 65 | + 0.4226 | — 0.2321 | — 0.4452 | — 0.1552 | + 0.2381 | + 0.3138 | + 0.0422 |
| 66 | .4067 | .2518 | .4419 | .1256 | .2615 | .2997 | + .0022 |
| 67 | .3907 | .2710 | .4370 | .0955 | .2824 | .2819 | — .0375 |
| 68 | .3746 | .2895 | .4305 | .0651 | .3005 | .2606 | — .0763 |
| 69 | .3584 | .3074 | .4225 | .0344 | .3158 | .2362 | — .1135 |
| 70 | + 0.3420 | — 0.3245 | — 0.4130 | — 0.0038 | + 0.3281 | + 0.2089 | — 0.1485 |
| 71 | .3256 | .3410 | .4021 | + .0267 | .3373 | .1791 | .1808 |
| 72 | .3090 | .3568 | .3898 | .0568 | .3434 | .1472 | .2099 |
| 73 | .2924 | .3718 | .3761 | .0864 | .3463 | .1136 | .2352 |
| 74 | .2756 | .3860 | .3611 | .1153 | .3461 | .0788 | .2563 |
| 75 | + 0.2588 | — 0.3995 | — 0.3449 | + 0.1434 | + 0.3427 | + 0.0431 | — 0.2730 |
| 76 | .2419 | .4122 | .3275 | .1705 | .3362 | + .0070 | .2850 |
| 77 | .2250 | .4241 | .3090 | .1964 | .3267 | — .0290 | .2921 |
| 78 | .2079 | .4352 | .2894 | .2211 | .3143 | — .0644 | .2942 |
| 79 | .1908 | .4454 | .2688 | .2443 | .2990 | — .0990 | .2913 |
| 80 | + 0.1736 | — 0.4548 | — 0.2474 | + 0.2659 | + 0.2810 | — 0.1321 | — 0.2835 |
| 81 | .1564 | .4633 | .2251 | .2859 | .2606 | .1635 | .2708 |
| 82 | .1392 | .4709 | .2020 | .3040 | .2378 | .1927 | .2536 |
| 83 | .1219 | .4777 | .1783 | .3203 | .2129 | .2193 | .2321 |
| 84 | .1045 | .4836 | .1539 | .3345 | .1861 | .2431 | .2067 |
| 85 | + 0.0872 | — 0.4886 | — 0.1291 | + 0.3468 | + 0.1577 | — 0.2638 | — 0.1778 |
| 86 | .0698 | .4927 | .1038 | .3569 | .1278 | .2810 | .1460 |
| 87 | .0523 | .4959 | .0781 | .3648 | .0969 | .2947 | .1117 |
| 88 | .0349 | .4982 | .0522 | .3704 | .0651 | .3045 | .0755 |
| 89 | .0175 | .4995 | .0262 | .3739 | .0327 | .3105 | .0381 |
| 90 | + 0.0000 | — 0.5000 | — 0.0000 | + 0.3750 | + 0.0000 | — 0.3125 | — 0.0000 |

TABLE 35
CYLINDRICAL HARMONICS OF THE 0TH AND 1ST ORDERS

$$J_n(x) = \frac{x^n}{2^n \Gamma(n+1)} \left\{ 1 - \frac{x^2}{2^2(n+1)} + \frac{x^4}{2^4 2!(n+1)(n+2)} - \dots \right\} \quad J_1(x) = -J'_0(x) = \frac{dJ_0(x)}{dx}$$

| x | $J_0(x)$ | $J_1(x)$ | x | $J_0(x)$ | $J_1(x)$ | x | $J_0(x)$ | $J_1(x)$ | x | $J_0(x)$ | $J_1(x)$ |
|------------|----------|----------|-------------|----------|----------|-------------|----------|----------|-------------|----------|----------|
| .00 | unity | zero | .50 | .938470 | .242268 | 1.00 | .765198 | .440051 | 1.50 | .511828 | .557937 |
| .01 | .999975 | .005000 | .51 | .936024 | .246799 | .01 | .760781 | .443286 | .51 | .506241 | .559315 |
| .02 | .999900 | .010000 | .52 | .933534 | .251310 | .02 | .756332 | .446488 | .52 | .500642 | .560503 |
| .03 | .999775 | .014998 | .53 | .930998 | .255803 | .03 | .751851 | .449658 | .53 | .495028 | .561951 |
| .04 | .999600 | .019996 | .54 | .928418 | .260277 | .04 | .747339 | .452794 | .54 | .489403 | .563208 |
| .05 | .999375 | .024992 | .55 | .925793 | .264732 | 1.05 | .742796 | .455897 | 1.55 | .483764 | .564424 |
| .06 | .999100 | .029987 | .56 | .923123 | .269166 | .06 | .738221 | .458966 | .56 | .478114 | .565600 |
| .07 | .998775 | .034979 | .57 | .920410 | .273581 | .07 | .733616 | .462001 | .57 | .472453 | .566735 |
| .08 | .998401 | .039968 | .58 | .917652 | .277975 | .08 | .728981 | .465003 | .58 | .466780 | .567830 |
| .09 | .997976 | .044954 | .59 | .914850 | .282349 | .09 | .724316 | .467970 | .59 | .461096 | .568883 |
| .10 | .997502 | .049938 | .60 | .912005 | .286701 | 1.10 | .719622 | .470902 | 1.60 | .455402 | .569896 |
| .11 | .996977 | .054917 | .61 | .909116 | .291032 | .11 | .714898 | .473800 | .61 | .449698 | .570868 |
| .12 | .996403 | .059892 | .62 | .905184 | .295341 | .12 | .710146 | .476663 | .62 | .443985 | .571798 |
| .13 | .995779 | .064863 | .63 | .903209 | .299628 | .13 | .705365 | .479491 | .63 | .438262 | .572688 |
| .14 | .995106 | .069820 | .64 | .900192 | .303893 | .14 | .700556 | .482284 | .64 | .432531 | .573537 |
| .15 | .994383 | .074789 | .65 | .897132 | .308135 | 1.15 | .695720 | .485041 | 1.65 | .426792 | .574344 |
| .16 | .993610 | .079744 | .66 | .894029 | .312355 | .16 | .690856 | .487763 | .66 | .421045 | .575111 |
| .17 | .992788 | .084693 | .67 | .890885 | .316551 | .17 | .685965 | .490449 | .67 | .415290 | .575836 |
| .18 | .991916 | .089636 | .68 | .887698 | .320723 | .18 | .681047 | .493098 | .68 | .409528 | .576520 |
| .19 | .990995 | .094572 | .69 | .884470 | .324871 | .19 | .676103 | .495712 | .69 | .403760 | .577163 |
| .20 | .990025 | .099501 | .70 | .881201 | .328996 | 1.20 | .671133 | .498289 | 1.70 | .397985 | .577765 |
| .21 | .989005 | .104422 | .71 | .877890 | .333096 | .21 | .666137 | .500830 | .71 | .392204 | .578326 |
| .22 | .987937 | .109336 | .72 | .874539 | .337170 | .22 | .661116 | .503334 | .72 | .386418 | .578845 |
| .23 | .986819 | .114241 | .73 | .871147 | .341220 | .23 | .656071 | .505801 | .73 | .380628 | .579323 |
| .24 | .985652 | .119138 | .74 | .867715 | .345245 | .24 | .651000 | .508231 | .74 | .374832 | .579760 |
| .25 | .984436 | .124026 | .75 | .864242 | .349244 | 1.25 | .645906 | .510623 | 1.75 | .369033 | .580156 |
| .26 | .983171 | .128905 | .76 | .860730 | .353216 | .26 | .640788 | .512979 | .76 | .363220 | .580511 |
| .27 | .981858 | .133774 | .77 | .857178 | .357163 | .27 | .635647 | .515296 | .77 | .357422 | .580824 |
| .28 | .980496 | .138632 | .78 | .853587 | .361083 | .28 | .630482 | .517577 | .78 | .351613 | .581096 |
| .29 | .979085 | .143481 | .79 | .849956 | .364976 | .29 | .625295 | .519819 | .79 | .345801 | .581327 |
| .30 | .977626 | .148319 | .80 | .846287 | .368842 | 1.30 | .620086 | .522023 | 1.80 | .339986 | .581517 |
| .31 | .976119 | .153146 | .81 | .842580 | .372681 | .31 | .614855 | .524189 | .81 | .334170 | .581666 |
| .32 | .974563 | .157991 | .82 | .838834 | .376492 | .32 | .609602 | .526317 | .82 | .328353 | .581773 |
| .33 | .972960 | .162764 | .83 | .835050 | .380275 | .33 | .604320 | .528407 | .83 | .322535 | .581840 |
| .34 | .971308 | .167555 | .84 | .831228 | .384029 | .34 | .599034 | .530458 | .84 | .316717 | .581865 |
| .35 | .969609 | .172334 | .85 | .827369 | .387755 | 1.35 | .593720 | .532470 | 1.85 | .310808 | .581849 |
| .36 | .967861 | .177100 | .86 | .823473 | .391453 | .36 | .588385 | .534444 | .86 | .305080 | .581793 |
| .37 | .966067 | .181852 | .87 | .819541 | .395121 | .37 | .583031 | .536379 | .87 | .299262 | .581695 |
| .38 | .964224 | .186501 | .88 | .815571 | .398760 | .38 | .577658 | .538274 | .88 | .293446 | .581557 |
| .39 | .962335 | .191316 | .89 | .811565 | .402370 | .39 | .572266 | .540131 | .89 | .287631 | .581377 |
| .40 | .960398 | .196027 | .90 | .807524 | .405950 | 1.40 | .566855 | .541948 | 1.90 | .281810 | .581157 |
| .41 | .958414 | .200723 | .91 | .803447 | .409499 | .41 | .561427 | .543726 | .91 | .276008 | .580896 |
| .42 | .956384 | .205403 | .92 | .799334 | .413018 | .42 | .555981 | .545404 | .92 | .270201 | .580595 |
| .43 | .954306 | .210069 | .93 | .795186 | .416507 | .43 | .550518 | .547162 | .93 | .264397 | .580252 |
| .44 | .952183 | .214719 | .94 | .791004 | .419965 | .44 | .545038 | .548821 | .94 | .258596 | .579870 |
| .45 | .950012 | .219353 | .95 | .786787 | .423392 | 1.45 | .539541 | .550441 | 1.95 | .252799 | .579446 |
| .46 | .947796 | .223970 | .96 | .782536 | .426787 | .46 | .534029 | .552020 | .96 | .247007 | .578983 |
| .47 | .945533 | .228571 | .97 | .778251 | .430151 | .47 | .528501 | .553559 | .97 | .241220 | .578478 |
| .48 | .943224 | .233154 | .98 | .773933 | .433483 | .48 | .522958 | .555050 | .98 | .235438 | .577934 |
| .49 | .940870 | .237720 | .99 | .769582 | .436783 | .49 | .517400 | .556518 | .99 | .229661 | .577349 |
| .50 | .938470 | .242268 | 1.00 | .765198 | .440051 | 1.50 | .511828 | .557937 | 2.00 | .223891 | .576725 |

CYLINDRICAL HARMONICS OF THE 0TH AND 1ST ORDERS

 $J_1(x) = -J_0'(x)$. Other orders may be obtained from the relation, $J_{n+1}(x) = \frac{2n}{x} J_n(x) - J_{n-1}(x)$.

$$J_{-n}(x) = (-1)^n J_n(x).$$

| x | $J_0(x)$ | $J_1(x)$ | x | $J_0(x)$ | $J_1(x)$ | x | $J_0(x)$ | $J_1(x)$ | x | $J_0(x)$ | $J_1(x)$ |
|-------------|----------|----------|-------------|----------|----------|-------------|----------|----------|-------------|----------|----------|
| 2.00 | .223891 | .576725 | 2.50 | -.048384 | .407094 | 3.00 | -.260052 | .339059 | 3.50 | -.380128 | .137378 |
| .01 | .218127 | .570060 | .51 | -.053342 | .404606 | .01 | -.263424 | .335319 | .51 | -.381481 | .133183 |
| .02 | .212370 | .575355 | .52 | -.058276 | .402086 | .02 | -.266758 | .331563 | .52 | -.382791 | .128989 |
| .03 | .206620 | .574611 | .53 | -.063184 | .409535 | .03 | -.270055 | .327780 | .53 | -.384060 | .124795 |
| .04 | .200878 | .573827 | .54 | -.068066 | .406953 | .04 | -.273314 | .323998 | .54 | -.385287 | .120601 |
| 2.05 | .195143 | .573003 | 2.55 | -.072923 | .404340 | 3.05 | -.276535 | .320191 | 3.55 | -.386472 | .116408 |
| .06 | .189418 | .572139 | .56 | -.077753 | .401666 | .06 | -.279718 | .316368 | .56 | -.387615 | .112216 |
| .07 | .183701 | .571236 | .57 | -.082557 | .479021 | .07 | -.282862 | .312529 | .57 | -.388717 | .108025 |
| .08 | .177993 | .570294 | .58 | -.087333 | .476317 | .08 | -.285968 | .308675 | .58 | -.389776 | .103836 |
| .09 | .172295 | .569313 | .59 | -.092083 | .473582 | .09 | -.289036 | .304805 | .59 | -.390793 | .099650 |
| 2.10 | .166607 | .568292 | 2.60 | -.096805 | .470818 | 3.10 | -.292064 | .300921 | 3.60 | -.391760 | .095466 |
| .11 | .160929 | .567233 | .61 | -.101499 | .468025 | .11 | -.295054 | .297023 | .61 | -.392703 | .091284 |
| .12 | .155262 | .566134 | .62 | -.106165 | .465202 | .12 | -.298005 | .293110 | .62 | -.393595 | .087106 |
| .13 | .149607 | .564997 | .63 | -.110803 | .462350 | .13 | -.300916 | .289184 | .63 | -.394445 | .082931 |
| .14 | .143963 | .563821 | .64 | -.115412 | .459470 | .14 | -.303788 | .285244 | .64 | -.395253 | .078760 |
| 2.15 | .138330 | .562607 | 2.65 | -.119992 | .456561 | 3.15 | -.306621 | .281291 | 3.65 | -.396020 | .074593 |
| .16 | .132711 | .561354 | .66 | -.124543 | .453625 | .16 | -.309414 | .277326 | .66 | -.396745 | .070431 |
| .17 | .127104 | .560063 | .67 | -.129065 | .450660 | .17 | -.312168 | .273348 | .67 | -.397429 | .066274 |
| .18 | .121509 | .558735 | .68 | -.133557 | .447668 | .18 | -.314881 | .269358 | .68 | -.398071 | .062122 |
| .19 | .115929 | .557368 | .69 | -.138018 | .444648 | .19 | -.317555 | .265356 | .69 | -.398671 | .057975 |
| 2.20 | .110362 | .555963 | 2.70 | -.142449 | .441601 | 3.20 | -.320188 | .261343 | 3.70 | -.399230 | .053834 |
| .21 | .104810 | .554521 | .71 | -.146850 | .438528 | .21 | -.322781 | .257319 | .71 | -.399748 | .049699 |
| .22 | .099272 | .553041 | .72 | -.151220 | .435428 | .22 | -.325355 | .253284 | .72 | -.400224 | .045571 |
| .23 | .093749 | .551524 | .73 | -.155559 | .432302 | .23 | -.327847 | .249239 | .73 | -.400659 | .041450 |
| .24 | .088242 | .549970 | .74 | -.159866 | .429150 | .24 | -.330319 | .245184 | .74 | -.401053 | .037336 |
| 2.25 | .082750 | .548378 | 2.75 | -.164141 | .425972 | 3.25 | -.332751 | .241120 | 3.75 | -.401406 | .033229 |
| .26 | .077274 | .546750 | .76 | -.168385 | .422769 | .26 | -.335142 | .237046 | .76 | -.401718 | .029131 |
| .27 | .071815 | .545085 | .77 | -.172597 | .419541 | .27 | -.337492 | .232963 | .77 | -.401989 | .025040 |
| .28 | .066373 | .543384 | .78 | -.176776 | .416288 | .28 | -.339801 | .228871 | .78 | -.402219 | .020958 |
| .29 | .060947 | .541646 | .79 | -.180922 | .413011 | .29 | -.342069 | .224771 | .79 | -.402408 | .016885 |
| 2.30 | .055540 | .539873 | 2.80 | -.185036 | .409709 | 3.30 | -.344296 | .220663 | 3.80 | -.402556 | .012821 |
| .31 | .050150 | .538063 | .81 | -.189117 | .406384 | .31 | -.346482 | .216548 | .81 | -.402664 | .008766 |
| .32 | .044779 | .536217 | .82 | -.193164 | .403035 | .32 | -.348627 | .212425 | .82 | -.402732 | .004722 |
| .33 | .039426 | .534336 | .83 | -.197177 | .399662 | .33 | -.350731 | .208296 | .83 | -.402759 | .000687 |
| .34 | .034092 | .532419 | .84 | -.201157 | .396267 | .34 | -.352793 | .204160 | .84 | -.402740 | -.003337 |
| 2.35 | .028778 | .530467 | 2.85 | -.205102 | .392840 | 3.35 | -.354814 | .200018 | 3.85 | -.402692 | -.007350 |
| .36 | .023383 | .528480 | .86 | -.209014 | .389408 | .36 | -.356793 | .195870 | .86 | -.402599 | -.011352 |
| .37 | .018208 | .526458 | .87 | -.212890 | .385945 | .37 | -.358731 | .191716 | .87 | -.402465 | -.015343 |
| .38 | .012954 | .524402 | .88 | -.216733 | .382461 | .38 | -.360628 | .187557 | .88 | -.402292 | -.019322 |
| .39 | .007720 | .522311 | .89 | -.220540 | .378955 | .39 | -.362482 | .183394 | .89 | -.402079 | -.023289 |
| 2.40 | .002508 | .520185 | 2.90 | -.224312 | .375427 | 3.40 | -.364296 | .179226 | 3.90 | -.401826 | -.027244 |
| .41 | -.002833 | .518026 | .91 | -.228048 | .371879 | .41 | -.366067 | .175054 | .91 | -.401534 | -.031186 |
| .42 | -.007853 | .515833 | .92 | -.231749 | .368311 | .42 | -.367797 | .170878 | .92 | -.401202 | -.035115 |
| .43 | -.013000 | .513606 | .93 | -.235414 | .364722 | .43 | -.369485 | .166690 | .93 | -.400832 | -.039031 |
| .44 | -.018125 | .511346 | .94 | -.239043 | .361113 | .44 | -.371131 | .162516 | .94 | -.400422 | -.042933 |
| 2.45 | -.023227 | .509052 | 2.95 | -.242636 | .357485 | 3.45 | -.372735 | .158331 | 3.95 | -.399973 | -.046821 |
| .46 | -.028306 | .506726 | .96 | -.246193 | .353837 | .46 | -.374297 | .154144 | .96 | -.399485 | -.050695 |
| .47 | -.033361 | .504366 | .97 | -.249713 | .350170 | .47 | -.375818 | .149954 | .97 | -.398959 | -.054555 |
| .48 | -.038393 | .501974 | .98 | -.253196 | .346484 | .48 | -.377296 | .145763 | .98 | -.398394 | -.058400 |
| .49 | -.043401 | .499550 | .99 | -.256643 | .342781 | .49 | -.378733 | .141571 | .99 | -.397791 | -.062229 |
| 2.50 | -.048384 | .497094 | 3.00 | -.260052 | .339059 | 3.50 | -.380128 | .137378 | 4.00 | -.397150 | .066043 |

CYLINDRICAL HARMONICS OF THE 0TH AND 1ST ORDERS

TABLE 36.—4-place Values for $x = 4$
to 15

| x | $J_0(x)$ | $J_1(x)$ | x | $J_0(x)$ | $J_1(x)$ |
|-----|----------|----------|------|----------|----------|
| 4.0 | -.3972 | -.0660 | 9.5 | -.1939 | +.1613 |
| .1 | -.3887 | -.1033 | .6 | -.2090 | .1395 |
| .2 | -.3766 | -.1386 | .7 | -.2218 | .1166 |
| .3 | -.3610 | -.1719 | .8 | -.2323 | .0928 |
| .4 | -.3423 | -.2028 | .9 | -.2403 | .0684 |
| 4.5 | -.3205 | -.2311 | 10.0 | -.2459 | .0435 |
| .6 | -.2961 | -.2566 | .1 | -.2490 | +.0184 |
| .7 | -.2693 | -.2791 | .2 | -.2496 | -.0066 |
| .8 | -.2404 | -.2985 | .3 | -.2477 | -.0313 |
| .9 | -.2097 | -.3147 | .4 | -.2434 | -.0555 |
| 5.0 | -.1776 | -.3276 | 10.5 | -.2366 | .0780 |
| .1 | -.1443 | -.3371 | .6 | -.2276 | -.1012 |
| .2 | -.1103 | -.3432 | .7 | -.2164 | -.1224 |
| .3 | -.0758 | -.3460 | .8 | -.2032 | -.1422 |
| .4 | -.0412 | -.3453 | .9 | -.1881 | -.1603 |
| 5.5 | -.0068 | -.3414 | 11.0 | -.1712 | -.1768 |
| .6 | +.0270 | -.3343 | .1 | -.1528 | -.1913 |
| .7 | .0599 | -.3241 | .2 | -.1330 | -.2039 |
| .8 | .0917 | -.3110 | .3 | -.1121 | -.2143 |
| .9 | .1220 | -.2951 | .4 | -.0902 | -.2225 |
| 6.0 | .1506 | -.2767 | 11.5 | -.0677 | -.2284 |
| .1 | .1773 | -.2559 | .6 | -.0446 | -.2320 |
| .2 | .2017 | -.2329 | .7 | -.0213 | -.2333 |
| .3 | .2238 | -.2081 | .8 | +.0020 | -.2323 |
| .4 | .2433 | -.1816 | .9 | .0250 | -.2290 |
| 6.5 | .2601 | -.1538 | 12.0 | .0477 | -.2234 |
| .6 | .2740 | -.1250 | .1 | .0697 | -.2157 |
| .7 | .2851 | -.0953 | .2 | .0908 | -.2060 |
| .8 | .2931 | -.0652 | .3 | .1108 | -.1943 |
| .9 | .2981 | -.0349 | .4 | .1296 | -.1807 |
| 7.0 | .3001 | -.0047 | 12.5 | .1469 | -.1655 |
| .1 | .2991 | +.0252 | .6 | .1626 | -.1487 |
| .2 | .2951 | .0543 | .7 | .1766 | -.1307 |
| .3 | .2882 | .0826 | .8 | .1887 | -.1114 |
| .4 | .2786 | .1096 | .9 | .1988 | -.0912 |
| 7.5 | .2663 | .1352 | 13.0 | .2069 | -.0703 |
| .6 | .2516 | .1592 | .1 | .2129 | -.0489 |
| .7 | .2346 | .1813 | .2 | .2167 | -.0271 |
| .8 | .2154 | .2014 | .3 | .2183 | -.0052 |
| .9 | .1944 | .2192 | .4 | .2177 | +.0166 |
| 8.0 | .1717 | .2346 | 13.5 | .2150 | .0380 |
| .1 | .1475 | .2476 | .6 | .2101 | .0590 |
| .2 | .1222 | .2580 | .7 | .2032 | .0791 |
| .3 | .0960 | .2657 | .8 | .1943 | .0984 |
| .4 | .0692 | .2708 | .9 | .1836 | .1165 |
| 8.5 | .0419 | .2731 | 14.0 | .1711 | .1334 |
| .6 | .0146 | .2728 | .1 | .1570 | .1488 |
| .7 | -.0125 | .2697 | .2 | .1414 | .1626 |
| .8 | -.0392 | .2641 | .3 | .1245 | .1747 |
| .9 | -.0653 | .2559 | .4 | .1065 | .1850 |
| 9.0 | -.0903 | .2453 | 14.5 | .0875 | .1934 |
| .1 | -.1142 | .2324 | .6 | .0679 | .1999 |
| .2 | -.1367 | .2174 | .7 | .0476 | .2043 |
| .3 | -.1577 | .2004 | .8 | .0271 | .2066 |
| .4 | -.1768 | .1816 | .9 | .0064 | .2069 |
| 9.5 | -.1939 | .1613 | 15.0 | -.0142 | .2051 |

TABLE 37.

(a) 1st 10 roots (R_m) of $J_0(x) = 0$; $J_1(R_m)$

Higher roots may be calculated to better than 1 part in 10,000 by the approximate formula $R_m = R_{m-1} + \pi$

| | |
|----------------------|-------------------------|
| $R_1 = 2.404826$ | $J_1(R_1) = +0.5191$ |
| $R_2 = 5.520078$ | $J_1(R_2) = -0.3403$ |
| $R_3 = 8.653728$ | $J_1(R_3) = +0.2715$ |
| $R_4 = 11.791534$ | $J_1(R_4) = -0.2325$ |
| $R_5 = 14.930918$ | $J_1(R_5) = +0.2065$ |
| $R_6 = 18.071064$ | $J_1(R_6) = -0.1877$ |
| $R_7 = 21.211637$ | $J_1(R_7) = +0.1733$ |
| $R_8 = 24.352472$ | $J_1(R_8) = -0.1617$ |
| $R_9 = 27.493479$ | $J_1(R_9) = +0.1522$ |
| $R_{10} = 30.634606$ | $J_1(R_{10}) = -0.1442$ |

(b) 1st 15 roots of $J_1(x) = \frac{dJ_0(x)}{dx} = 0$
with corresponding values of maximum or minimum values of $J_0(x)$.

| No. of root (n) | Root = x_n | $J_0(x_n)$ |
|---------------------|--------------|------------|
| 1 | 3.831706 | -.402759 |
| 2 | 7.015587 | +.300116 |
| 3 | 10.173468 | -.249705 |
| 4 | 13.323692 | +.218359 |
| 5 | 16.470630 | -.196465 |
| 6 | 19.615859 | +.180063 |
| 7 | 22.760084 | -.167185 |
| 8 | 25.903672 | +.156725 |
| 9 | 29.046829 | -.148011 |
| 10 | 32.189680 | +.140606 |
| 11 | 35.332308 | -.134211 |
| 12 | 38.474766 | +.128617 |
| 13 | 41.617904 | -.123668 |
| 14 | 44.759319 | +.119250 |
| 15 | 47.901401 | -.115274 |

Higher roots may be obtained as under (a).

NOTES. $y = J_n(x)$ is a particular solution of Bessel's equation,

$$x^2 \frac{d^2 y}{dx^2} + x \frac{dy}{dx} + (x^2 - n^2)y = 0.$$

The general formula for $J_n(x)$ is

$$J_n(x) = \sum_{s=0}^{\infty} \frac{(-1)^s x^{n+2s}}{2^{n+2s} \pi s! \Gamma(n+s+1)},$$

or

$$= \sum_{s=0}^{\infty} \frac{(-1)^s x^{n+2s}}{2^{n+2s} s! (n+s)!}$$

when n is an integer and

$$J_{n+1}(x) = \frac{2n}{x} J_n(x) - J_{n-1}(x),$$

and

$$J_1(x) = \frac{dJ_0(x)}{dx},$$

$$J_{-n}(x) = (-1)^n J_n(x).$$

Tables 36 to 37 are based upon Gray and Matthews' reprints from Dr. Meissel's tables. See also Reports of British Association, 1907-1916.

ELLIPTIC INTEGRALS

Values of $\int_0^{\pi/2} (1 - \sin^2 \theta \sin^2 \phi)^{\pm \frac{1}{2}} d\phi$

This table gives the values of the integrals between 0 and $\pi/2$ of the function $(1 - \sin^2 \theta \sin^2 \phi)^{\pm \frac{1}{2}} d\phi$ for different values of the modulus corresponding to each degree of θ between 0 and 90.

| θ | $\int_0^{\pi/2} \frac{d\phi}{(1 - \sin^2 \theta \sin^2 \phi)^{\frac{1}{2}}}$ | | $\int_0^{\pi/2} (1 - \sin^2 \theta \sin^2 \phi)^{\frac{1}{2}} d\phi$ | | θ | $\int_0^{\pi/2} \frac{d\phi}{(1 - \sin^2 \theta \sin^2 \phi)^{\frac{3}{2}}}$ | | $\int_0^{\pi/2} (1 - \sin^2 \theta \sin^2 \phi)^{\frac{3}{2}} d\phi$ | |
|----------|--|----------|--|----------|----------|--|----------|--|----------|
| | Number. | Log. | Number. | Log. | | Number. | Log. | Number. | Log. |
| 0° | 1.5708 | 0.196120 | 1.5708 | 0.196120 | 45° | 1.8541 | 0.268127 | 1.3506 | 0.130541 |
| 1 | 5709 | 196153 | 5707 | 196087 | 6 | 8691 | 271644 | 3418 | 127609 |
| 2 | 5713 | 196252 | 5703 | 195988 | 7 | 8848 | 275267 | 3329 | 124788 |
| 3 | 5719 | 196418 | 5697 | 195822 | 8 | 9011 | 279001 | 3238 | 121836 |
| 4 | 5727 | 196649 | 5689 | 195591 | 9 | 9180 | 282848 | 3147 | 118836 |
| 5° | 1.5738 | 0.196947 | 1.5678 | 0.195293 | 50° | 1.9356 | 0.286811 | 1.3055 | 0.115790 |
| 6 | 5751 | 197312 | 5665 | 194930 | 1 | 9539 | 290805 | 2963 | 112668 |
| 7 | 5767 | 197743 | 5649 | 194500 | 2 | 9729 | 295101 | 2870 | 109563 |
| 8 | 5785 | 198241 | 5632 | 194004 | 3 | 9927 | 299435 | 2776 | 106386 |
| 9 | 5805 | 198806 | 5611 | 193442 | 4 | 2.0133 | 303701 | 2681 | 103169 |
| 10° | 1.5828 | 0.199438 | 1.5589 | 0.192815 | 55° | 2.0347 | 0.308504 | 1.2587 | 0.099915 |
| 1 | 5854 | 200137 | 5564 | 192121 | 6 | 0571 | 313247 | 2492 | 096626 |
| 2 | 5882 | 200904 | 5537 | 191362 | 7 | 0804 | 318138 | 2397 | 093303 |
| 3 | 5913 | 201740 | 5507 | 190537 | 8 | 1047 | 323182 | 2301 | 089950 |
| 4 | 5946 | 202643 | 5476 | 189646 | 9 | 1300 | 328384 | 2206 | 086569 |
| 15° | 1.5981 | 0.203615 | 1.5442 | 0.188690 | 60° | 2.1565 | 0.333753 | 1.2111 | 0.083164 |
| 6 | 6020 | 204657 | 5405 | 187668 | 1 | 1842 | 339295 | 2015 | 079738 |
| 7 | 6061 | 205768 | 5367 | 186581 | 2 | 2132 | 345020 | 1920 | 076293 |
| 8 | 6105 | 206948 | 5326 | 185428 | 3 | 2435 | 350936 | 1826 | 072834 |
| 9 | 6151 | 208200 | 5283 | 184210 | 4 | 2754 | 357053 | 1732 | 069364 |
| 20° | 1.6200 | 0.209522 | 1.5238 | 0.182928 | 65° | 2.3088 | 0.363384 | 1.1638 | 0.065889 |
| 1 | 6252 | 210316 | 5191 | 181580 | 6 | 3439 | 369940 | 1545 | 062412 |
| 2 | 6307 | 212382 | 5141 | 180168 | 7 | 3809 | 376736 | 1453 | 058937 |
| 3 | 6365 | 213921 | 5090 | 178691 | 8 | 4198 | 383787 | 1362 | 055472 |
| 4 | 6426 | 215533 | 5037 | 177150 | 9 | 4610 | 391112 | 1272 | 052020 |
| 25° | 1.6490 | 0.217219 | 1.4981 | 0.175545 | 70° | 2.5046 | 0.398730 | 1.1184 | 0.048589 |
| 6 | 6557 | 218981 | 4924 | 173876 | 1 | 5507 | 406665 | 1096 | 045183 |
| 7 | 6627 | 220818 | 4864 | 172144 | 2 | 5998 | 414943 | 1011 | 041812 |
| 8 | 6701 | 222732 | 4803 | 170348 | 3 | 6521 | 423596 | 0927 | 038481 |
| 9 | 6777 | 224723 | 4740 | 168489 | 4 | 7081 | 432660 | 0844 | 035200 |
| 30° | 1.6858 | 0.226793 | 1.4675 | 0.166567 | 75° | 2.7681 | 0.442176 | 1.0764 | 0.031976 |
| 1 | 6941 | 228943 | 4608 | 164583 | 6 | 8327 | 452196 | 0686 | 028819 |
| 2 | 7028 | 231173 | 4539 | 162537 | 7 | 9026 | 462782 | 0611 | 025740 |
| 3 | 7119 | 233485 | 4469 | 160429 | 8 | 9786 | 474008 | 0538 | 022749 |
| 4 | 7214 | 235880 | 4397 | 158261 | 9 | 3.0617 | 485967 | 0468 | 019858 |
| 35° | 1.7312 | 0.238359 | 1.4323 | 0.156031 | 80° | 3.1534 | 0.498777 | 1.0401 | 0.017081 |
| 6 | 7415 | 240923 | 4248 | 153742 | 1 | 2553 | 512591 | 0338 | 014432 |
| 7 | 7522 | 243575 | 4171 | 151393 | 2 | 3699 | 527613 | 0278 | 011927 |
| 8 | 7633 | 246315 | 4092 | 148985 | 3 | 5004 | 544120 | 0223 | 009584 |
| 9 | 7748 | 249146 | 4013 | 146519 | 4 | 6519 | 562514 | 0172 | 007422 |
| 40° | 1.7868 | 0.252068 | 1.3931 | 0.143995 | 85° | 3.8317 | 0.583396 | 1.0127 | 0.005465 |
| 1 | 7992 | 255085 | 3849 | 141414 | 6 | 4.0528 | 607751 | 0086 | 003740 |
| 2 | 8122 | 258197 | 3765 | 138778 | 7 | 3387 | 637355 | 0053 | 002278 |
| 3 | 8256 | 261406 | 3680 | 136086 | 8 | 7427 | 676027 | 0026 | 001121 |
| 4 | 8396 | 264716 | 3594 | 133340 | 9 | 5.4349 | 735192 | 0008 | 000326 |
| 45° | 1.8541 | 0.268127 | 1.3506 | 0.130541 | 90° | ∞ | ∞ | 1.0000 | — |

MOMENTS OF INERTIA, RADII OF GYRATION, AND WEIGHTS

In each case the axis is supposed to traverse the centre of gravity of the body. The axis is one of symmetry. The mass of a unit of volume is w .

| Body. | Axis. | Weight. | Moment of Inertia I_0 . | Square of Radius of Gyration ρ_0^2 . |
|---|------------------------|------------------------------|---|---|
| Sphere of radius r | Diameter | $\frac{4\pi w r^3}{3}$ | $\frac{8\pi w r^5}{15}$ | $\frac{2r^2}{5}$ |
| Spheroid of revolution, polar axis $2a$, equatorial diameter $2r$ | Polar axis | $\frac{4\pi w a r^2}{3}$ | $\frac{8\pi w a r^4}{15}$ | $\frac{2r^2}{5}$ |
| Ellipsoid, axes $2a, 2b, 2c$ | Axis $2a$ | $\frac{4\pi w abc}{3}$ | $\frac{4\pi w abc(b^2+c^2)}{15}$ | $\frac{b^2+c^2}{5}$ |
| Spherical shell, external radius r , internal r' | Diameter | $\frac{4\pi w(r^3-r'^3)}{3}$ | $\frac{8\pi w(r^5-r'^5)}{15}$ | $\frac{2(r^5-r'^5)}{5(r^3-r'^3)}$ |
| Ditto, insensibly thin, radius r , thickness dr | Diameter | $4\pi w r^2 dr$ | $\frac{8\pi w r^4 dr}{3}$ | $\frac{2r^2}{3}$ |
| Circular cylinder, length $2a$, radius r | Longitudinal axis $2a$ | $2\pi w a r^2$ | $\pi w a r^4$ | $\frac{r^2}{2}$ |
| Elliptic cylinder, length $2a$, transverse axes $2b, 2c$ | Longitudinal axis $2a$ | $2\pi w abc$ | $\frac{\pi w abc(b^2+c^2)}{2}$ | $\frac{b^2+c^2}{4}$ |
| Hollow circular cylinder, length $2a$, external radius r , internal r' | Longitudinal axis $2a$ | $2\pi w a(r^2-r'^2)$ | $\pi w a(r^4-r'^4)$ | $\frac{r^2+r'^2}{2}$ |
| Ditto, insensibly thin, thickness dr | Longitudinal axis $2a$ | $4\pi w a r dr$ | $4\pi w a r^3 dr$ | r^2 |
| Circular cylinder, length $2a$, radius r | Transverse diameter | $2\pi w a r^2$ | $\frac{\pi w a r^2(3r^2+4a^2)}{6}$ | $\frac{r^2}{4} + \frac{a^2}{3}$ |
| Elliptic cylinder, length $2a$, transverse axes $2a, 2b$ | Transverse axis $2b$ | $2\pi w abc$ | $\frac{\pi w abc(3c^2+4a^2)}{6}$ | $\frac{c^2}{4} + \frac{a^2}{3}$ |
| Hollow circular cylinder, length $2a$, external radius r , internal r' | Transverse diameter | $2\pi w a(r^2-r'^2)$ | $\frac{\pi w a}{6} \left\{ 3(r^4-r'^4) + 4a^2(r^2-r'^2) \right\}$ | $\frac{r^2+r'^2}{4} + \frac{a^2}{3}$ |
| Ditto, insensibly thin, thickness dr | Transverse diameter | $4\pi w a r dr$ | $\pi w a \left(2r^3 + \frac{4}{3}a^2 r \right) dr$ | $\frac{r^2}{2} + \frac{a^2}{3}$ |
| Rectangular prism, dimensions $2a, 2b, 2c$ | Axis $2a$ | $8wabc$ | $\frac{8wabc(b^2+c^2)}{3}$ | $\frac{b^2+c^2}{3}$ |
| Rhombic prism, length $2a$, diagonals $2b, 2c$ | Axis $2a$ | $4wabc$ | $\frac{2wabc(b^2+c^2)}{3}$ | $\frac{b^2+c^2}{6}$ |
| Ditto | Diagonal $2b$ | $4wabc$ | $\frac{2wabc(c^2+2a^2)}{3}$ | $\frac{c^2}{6} + \frac{a^2}{3}$ |

(Taken from Rankine.)

For further mathematical data see Smithsonian Mathematical Tables, Becker and Van Orstrand (Hyperbolic, Circular and Exponential Functions); Smithsonian Mathematical Formulae and Tables of Elliptic Functions, Adams and Hippisley; Functionentafeln, Jahnke und Emde (xtgx , x^{-1}tgx , Roots of Transcendental Equations, $a+bi$ and $\text{re}^{i\theta}$, Exponentials, Hyperbolic Functions,

$\int_0^x \frac{\sin u}{u} du$, $\int_x^\infty \frac{\cos u}{u} du$, $\int_{-\infty}^x \frac{e^{-u}}{u} du$, Fresnel Integral, Gamma Function, Gauss Integral

$\frac{2}{\sqrt{\pi}} \int_0^x e^{-x^2} dx$, Pearson Function $e^{-\frac{1}{2}\pi v} \int_0^\pi \sin v x dx$, Elliptic Integrals and Functions, Spherical and Cylindrical Functions, etc.). For further references see under Tables, Mathematical, in the 11th ed. Encyclopædia Britannica. See also Carr's Synopsis of Pure Mathematics and Mellor's Higher Mathematics for Students of Chemistry and Physics.

PROBABLE VALUES OF THE GENERAL PHYSICAL CONSTANTS

(As of January 1, 1929)

(Considerably abbreviated from paper by Raymond T. Birge published in Phys. Rev. Suppl., vol. 1, no. 1, July, 1929, which see for further details)

Some of the most important results of physical science are embodied in the numerical magnitudes of various universal constants; the accurate determination of such constants has engaged the time and labor of many most eminent scientists. Some of these constants can be evaluated by various methods. Each has been investigated by various persons, at various times, and each investigation normally produces a result more or less different from that of any other investigation. Under such conditions there arises a general and continuous need for a searching examination of the *most probable* value of each important constant. An investigation of the values of general constants in current use reveals a surprising inconsistency, both in regard to the actually adopted values and to their origin, probably because of the fact that it is almost impossible to find a critical study of the best values, sufficiently up-to-date to be really reliable, and sufficiently detailed to explain the inconsistencies found among older tables.

(1) In what follows "each general constant has been determined from the available data, beginning with that constant whose value depends least on other constants. The value thus adopted has then been used *consistently* in the calculation of each succeeding constant for which it is an 'auxiliary constant'. No attempt has been made to compare the results of different investigators until these have been made properly comparable by the use of the same value of each auxiliary constant.

(2) "Each constant has been calculated from the available data by the use, as far as possible, of formulas which involve no approximations.

(3) "Each constant has been recalculated, whenever it seemed necessary, by analytic methods—usually by the method of least squares."

Attention should be directed to two important sources:

(1) The International Critical Tables (1926) publish a list of nine so-called "Accepted Basic Constants," each with its "Uncertainty." A list is given of 21 constants derived from these, and also certain other conventional and experimental constants. The I.C.T.¹ list was adopted in 1923; since then important work on nearly every constant has appeared. It was prepared with the aid of various scientific societies and individuals. The values are not claimed to be the best values then available, although obviously an attempt was made to obtain the best values. The chief weakness of this list is the lack of any statement as to their origins. By correspondence and in other ways Doctor Birge has obtained such information, and specific references to this are made in the various sections to follow.

¹ I.C.T. will be used for International Critical Tables, 1926.

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(2) The Geiger and Scheel "Handbuch der Physik"¹ contains an article by F. Henning and W. Jaeger on "The General Physical Constants." There is a list of 52 constants, basic and derived, and a statement as to the theoretical and numerical basis of each value. Many approximations and sources of inconsistency are pointed out, but with one or two exceptions no attempt is made to recalculate data to improve the published values. The Henning and Jaeger article, written in 1926, contains more recent information than the I.C.T.

Since 1926 much new material has appeared, so that practically every constant adopted in the present paper differs more or less in value from that given in either of these two preceding lists. In fact for the great majority of the constants considered the adopted value is based primarily on work which has appeared since 1926. In the case of most of the constants, the situation is now much more satisfactory than it was a few years ago.

The velocity of light in vacuum (c).—An accurate summary of all numerical results to 1927, in which many errors in the literature are corrected, has been given by de Bray.² A good recent account of the experimental methods for measuring c , as well as the numerical results, is that by Ladenburg.³

The latest and most accurate direct determination of the velocity of light is that by Michelson,⁴ in 1921-1926. When the various sets of results are collected under the five different mirrors used, the agreement is quite remarkable, all five results varying only from 299797 to 299795 with a mean of 299796 as before.

$$c = (2.99796 \pm 0.00004) \times 10^{10} \text{ cm} \cdot \text{sec}^{-1}$$

The velocity of electromagnetic waves may be obtained *indirectly* from the measured ratio of the electrostatic (es) to the electromagnetic (em) system of electrical units, according to the generally accepted electromagnetic theory of light. The best value of this ratio, which is here denoted by c' , is undoubtedly that found by Rosa and Dorsey.⁵ Their final result is the average of a very large number of individual results, taken at different times, under varying conditions, and of remarkable consistency. It seems to Doctor Birge that about one part in 30000 is a very conservative estimate for the *probable* error, giving $c' = 2.9971 \pm 0.0001$.

This result is in terms of international electrical units. Henning and Jaeger⁶ show that, to obtain the true ratio between the es and the em system, in absolute units, the result of Rosa and Dorsey must be multiplied by $p^{1/2}$, where one int. ohm = p abs. ohm. According to a subsequent discussion, $p = 1.00051 \pm 0.00002$. This gives a corrected value of $c' = (2.9979 \pm 0.0001) \times 10^{10} \text{ cm} \cdot \text{sec}^{-1}$. It is in beautiful agreement with Michelson's recent value of c .

¹ Henceforth denoted by H.P. ² Nature, 120, 602, 1927. ³ Handb. der Exp. Phys., 18, 1, 1928. ⁴ Astrophys. Journ. 65, 1, 1927. ⁵ Bur. Standards Bull., 3, 433, 1907. ⁶ H.P., 2, 507.

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The Newtonian constant of gravitation (G).—The H.P.¹ gives a table of seven determinations of G , ranging from 6.60 to 6.70×10^{-8} dyne \cdot cm² \cdot g⁻². Henning and Jaeger adopt 6.65. In their list they omit Poynting's value² of 6.66 ± 0.01 . The I.C.T. adopt as one of their basic constants $G = 6.66 \pm 0.01$.

Since the publication of these reviews, Heyl³ has made undoubtedly the most reliable determination of G . His final result is

$$G = (6.664 \pm 0.002) \times 10^{-8} \text{ dyne} \cdot \text{cm}^2 \cdot \text{g}^{-2}$$

This result is adopted here. It is based on five separate determinations varying from 6.661 to 6.667.

Mean density of the earth.—Assuming $R = 6.371 \times 10^8$ cm as the mean radius of the earth, as given in the H.P., and $g_{45} = 980.616$ cm \cdot sec⁻², $G \cdot \delta(\text{earth}) = 36.797 \times 10^{-8}$ sec⁻², where $\delta(\text{earth})$ is the *mean density* of the earth. From the H.P. result $G = 6.65$ $\delta(\text{earth}) = 5.53$ g \cdot cm⁻³. With the new result $G = 6.664$

$$\delta(\text{earth}) = 5.522 \pm 0.002 \text{ g} \cdot \text{cm}^{-3}$$

Relation of the liter to the cubic decimeter (1000 cm³).—The liter is defined as the volume of a kilogram of air-free water at its maximum density. In other words, the maximum density of water is, by definition, one kg \cdot l⁻¹. The kilogram is defined as the mass of the prototype kilogram preserved in Paris. This original prototype was intended to be the mass of a cubic decimeter (dm³) of water, at maximum density. Later determinations have shown a slight discrepancy. The various experimental results are discussed by Henning and Jaeger.⁴ The mean of the best determinations is 1 liter = 1000.027 cm³; this value has been accepted in all recent tables. Henning and Jaeger give no probable error for the result, but one unit in the last place seems a reasonable assumption. Hence

$$1 \text{ liter} = 1000.027 \pm 0.001 \text{ cm}^3 = 1.000027 \pm 0.000001 \text{ dm}^3$$

The maximum density of water $\delta_m(\text{H}_2\text{O})$ is accordingly

$$1/1.000027 = 0.999973 \pm 0.000001 \text{ kg} \cdot \text{dm}^{-3} \text{ or } \text{g} \cdot \text{cm}^{-3}$$

It should be noted in conclusion, that it is customary to define 1 cc as liter/1000, while 1 cm³ = liter/1000.027.

The normal mole volume of an ideal gas.—

$$(\nu_n \text{ cm}^3 \cdot \text{mole}^{-1}, \text{ or } R_n \text{ liter} \cdot \text{mole}^{-1})$$

The normal mole volume of an ideal gas is the volume occupied by one gram mole of an ideal gas, at 0° C, under one normal atmosphere pressure. This

¹ H.P., 2, 507. ² "Gravitation," Encyc. Brit., XI ed. ³ Proc. Nat. Acad. Sci., 13, 601, 1927. Heyl's more recent value is 6.670×10^{-8} cm³ \cdot g⁻¹ \cdot sec.⁻² Bur. Standards Journ. Res., 5, 1243, 1930. ⁴ H.P., 2, 491.

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quantity can theoretically be determined from any real gas, correcting to reduce to an ideal gas. Actually, only oxygen is used because its atomic weight is 16.000 by definition; there is no error in the resulting value due to error in the atomic weight. As a result of extensive investigations, the correction to change oxygen to an ideal gas is known with considerable accuracy.

The I.C.T. gives $v_n = 22.4115 \times 10^3 \text{ cm}^3$. The H.P. gives $22.4145 \times 10^3 \text{ cm}^3$ or $R_n = 22.4139$ liters. The discrepancy must be due to different values of $\delta_n(\text{O}_2)$, the normal density of oxygen, or of $(1-\alpha)$, the factor due to the deviation of oxygen from an ideal gas.¹ Thus

$$v_n = 32(1-\alpha)/\delta_n(\text{O}_2) = \{32(1-\alpha)/L_n(\text{O}_2)\} 1000.027 = R_n(1000.027)$$

where v_n is the normal mole volume in cm^3 , R_n the same in liters, $\delta_n(\text{O}_2)$ the normal density of O_2 , in grams per cm^3 , and $L_n(\text{O}_2)$ the normal density in grams per liter. All these values correspond to normal gravity ($g_n = 980.665$). It is, however, customary among chemists to express the experimental results in terms of g_{45} (980.616). Such values will be denoted by v , δ , L , and R . Thus

$$R = M(1-\alpha)/L$$

where M is the molecular weight.

¹ The most general definition of α is $(1/pv) d(pv)/d(p)$, (temp. = constant); it measures the change in pv , per unit change in pressure, and has the dimensions of pressure⁻¹. To make the numerical values more definite, it is customary to write $\alpha = [1/(pv)_1] d(pv)/d(p)$, where $(pv)_1$ refers to unit pressure. In investigations on normal density or normal mole volume, it is natural to choose one atmosphere as the unit of pressure. Henning and Heuse use one meter of mercury as the unit of p , and denote α by κ_t (see page 85). Since the numerical magnitude of α is proportional to the size of the unit of p , we have $\kappa_t = 100\alpha/76$. Henning (H.P. 9, 528) uses the symbol κ_t , but states that p is measured in atmospheres.

Within limits of error, the isothermal pv is a linear function of p , for the so-called permanent gases O_2 , N_2 , H_2 , etc., for such substances α is independent of p but is a function of temperature, and is more properly written α_t . The linear extrapolation of pv to $p = 0$ gives then $(pv)_0 = (1-\alpha)(pv)_1$. Now in the limit $p = 0$, any gas becomes, by definition, an ideal gas. Hence $(pv)_0$ is the constant pv of an ideal gas, and $(1-\alpha)$ is the factor which converts the real $(pv)_1$, (unit pressure) into the ideal $(pv)_0$, both at some definite temperature. $(1-\alpha)$ is often denoted by $(1+\lambda)$, and $(1-\alpha)$ or $(1+\lambda)$ may be defined as the ratio $(pv)_0/(pv)_1$. Frequently v is so chosen (in magnitude or unit) that $(pv)_1$ is unity. α (or κ_t) is then numerically (but not dimensionally) the slope of the pv isothermal (see H.P. 9, 528 and 538).

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Henning and Jaeger¹ give as a mean value, $L = 1.42892 \text{ g} \cdot \text{l}^{-1}$ and $(1-a) = 1.00092$. A more recent result by Baxter and Starkweather² ($L = 1.42901$) is omitted, but is included in the discussion by Henning and Jaeger, and raises the mean L to 1.42893. From this, and the value of $(1-a)$ just quoted, the H.P. gets its value of ν_n . The more recent values of $(1-a)$, average 1.00086, and this, taken with the Baxter and Starkweather value of L , gives $\nu_n = 22.4119 \times 10^3 \text{ cm}^3$, in close agreement with the I.C.T. value.

Baxter and Starkweather³ have recalculated their 1926 data in a more logical manner and obtain $L = 1.428965$ grams per liter, $(1-a) = 1.000927$.

$$L = (1.428965 \pm 0.000030) \text{ gram} \cdot \text{liter}^{-1} \quad (g = 980.616)$$

$$1-a = 1.000927 \pm 0.000030.$$

$$R = 22.4146 \pm 0.0008 \text{ liter} \cdot \text{mole}^{-1} \quad (g_{45} = 980.616)$$

$$R_n = 22.4135 \pm 0.0008 \text{ liter} \cdot \text{mole}^{-1} \quad (g_n = 980.665)$$

$$\nu_n = (22.4141 \pm 0.0008) \times 10^3 \text{ cm}^3 \cdot \text{mole}^{-1} \quad (g_n = 980.665).$$

Ratio of international (int.) to absolute (abs.) electrical units.—For practical convenience, the ohm, ampere, and volt have been defined, by international agreement,⁴ in terms of definite physical apparatus.⁵

These international units are to be compared with the corresponding absolute units, with which they were of course identical, within limits of experimental error, at the time of adoption in 1908. One abs. ohm $= 10^9 \text{ em}$ units of resistance, the em unit, under the assumption that permeability is dimensionless, being one $\text{cm} \cdot \text{sec}^{-1}$. Measurements of the abs. ohm have been made in a variety of ways, but all methods necessarily involve the measurement of length and time. The abs. ampere is 10^{-1} em units, the em unit being one $\text{dyne}^{1/2}$, again with the assumption of dimensionless permeability.

The definition of the int. amp. just given is the primary definition, and Doctor Birge follows the I.C.T. in designating the int. amp. so defined, and all quantities involving it, by the symbol "(a)." Now let

$$(1) \quad 1 \text{ int. ohm} = p \text{ abs. ohm} \qquad (2) \quad 1 \text{ int. amp. (a)} = q \text{ abs. amp.}$$

then

$$(3) \quad 1 \text{ int. coul. (a)} = q \text{ abs. coul.} \qquad (6) \quad 1 \text{ int. henry} = p \text{ abs. henry}$$

$$(4) \quad 1 \text{ int. volt (a)} = pq \text{ abs. volt} \qquad (7) \quad 1 \text{ int. gauss} = q \text{ abs. gauss}$$

$$(5) \quad 1 \text{ int. joule (a)} = pq^2 \text{ abs. joule}$$

¹ H.P., 2, 493. ² Proc. Nat. Acad. Sci., 10, 476, 1924. ³ Proc. Nat. Acad. Sci., 14, 57, 1928. ⁴ London, 1908. ⁵ This book, p. xlvi et seq.

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The int. ohm can be constructed as a definite laboratory standard. This is not true of the int. amp. (a). Hence the 1908 London conference appointed a committee to determine the e.m.f. of the Weston normal cell, in terms of the int. ohm and int. amp. The final value adopted by the committee (Jan. 1, 1911) was 1.0183 int. volts, at 20°C, which, to avoid ambiguity, is written 1.01830. This is effectively a new definition of the int. volt and to distinguish it, if necessary, from the primary definition, Doctor Birge again follows the I.C.T. in writing int. volt (v). Similarly all units involving the Weston normal cell will be designated by "(v)." Let

$$1 \text{ int. volt (v)} = r \text{ abs. volt} \quad (8)$$

as contrasted with eq. (4). It is now possible to use the int. volt (v) and the int. ohm to obtain a new (subsidiary) definition of the int. amp. Thus

$$1 \text{ int. amp. (v)} = r/p \text{ abs. amp.} \quad (9)$$

as compared to eq. (2). Finally, in many investigations, a so-called "semi-absolute" volt has been used. This is defined as the e.m.f. required to force one *abs.* amp. of current through one *int.* ohm resistance. Hence from eq. (1)

$$1 \text{ semiabs. volt} = p \text{ abs. volt.} \quad (10)$$

From eqs. (8) and (10) one obtains

$$1 \text{ int. volt (v)} = r/p \text{ semiabs. volt.} \quad (11)$$

We have now to consider the most probable value of p and of q , and the difference, if any, between r and pq (or between r/p and q). These questions are discussed by Henning and Jaeger in the H.P., and they conclude,

$$q = 1, \quad p = 1.00050, \quad r = pq = 1.00050.$$

On the other hand, the I.C.T. gives

$$q = 0.99993, \quad p = 1.00052, \quad r = 1.00042, \quad \text{while} \quad pq = 1.00045.$$

Hence $r/p = 0.99990 \neq q$. The correct determination of the best values of p and q is a very technical and extremely involved matter. Unfortunately, as just seen, there is no exact agreement on the subject. Part of the present disagreement in the values of p and q is due to the fact that there is no standard international unit of resistance or of voltage. Each national laboratory has its own standards which differ more or less among themselves, and also may change with time. The values of p and q finally adopted here represent, as well as possible, *mean* values both in respect to place and to time. Fortunately the accuracy of these quantities is so great that any possible error in the finally adopted values is entirely immaterial in its effect on the many constants derived later in this paper.

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The numerical relation of the int. and abs. ohm rests chiefly on two extensive investigations, one $p=1.00052 \pm 0.00004$, by Smith,¹ at the National Physical Laboratory (N.P.L.) of England, and the other, $p=1.00051$, by Grüneisen and Giebe,² at the German Reichsanstalt. The latter estimate their probable error, as well as that of Smith, as about 3 parts in 10^5 . In 1925 a committee at the N.P.L. began an investigation of the relation of the int. and abs. electrical units. This work is incomplete. It was stated in 1925³ that a comparison of various manganin with mercury resistances indicates that the former have all increased in resistance by about 2.5 parts per 10^5 since 1912, or that the mercury standards (defining the int. ohm) are really smaller by this amount. The latter assumption would give $p=1.000495$, in place of Smith's value of 1.00052. In a recent investigation at the Reichsanstalt, Steinwehr and Schulze⁴ evidently assume that the N.P.L. 1925 standards are 2 parts in 10^5 less than the older 1912 standards, giving a mean value of p in exact agreement with the 1920 Reichsanstalt value. Their own experiments in 1928 agree with this same mean value to ± 1 in 10^5 . Various intercomparisons at the N.P.L.⁵ show that the German and American standards lie between the 1912 and 1925 N.P.L. values. It seems certain that the best value of p , at the present time, is 1.00051 (p.e. seems to be not more than 2 parts in 10^5).

The most probable value of q is more uncertain. In the older work, the abs. amp., determined with either a current balance or a tangent galvanometer, was compared directly with the int. amp. as measured by a silver voltameter. There was measured by means of a silver voltameter, with certain specifications, the amount of silver, in grams, deposited per sec. by a current of one abs. amp. This mass of silver was then compared with 0.00111800 gram, the defined amount deposited, *under the same conditions*, by one int. amp. per sec.

Such a procedure determines q unambiguously, but does not necessarily evaluate the electrochemical equivalent of silver (E_{Ag}) per abs. coul. The electrochemical equivalent of a substance is the mass actually associated with unit charge, and is independent of experimental imperfections, while the mass deposited in an electrolytic cell per unit charge—the only quantity we can actually measure—is subject to experimental imperfections. This distinction has no bearing on the value of q , so long as one accepts the official definition of the int. ampere. It concerns only the value of electrochemical equivalents and the resulting value of the faraday. The various experimental values of q , determined as explained above, are listed by Henning and Jaeger.⁶

¹ Philos. Trans., 214, 27, 1914. ² Ann. Phys., 63, 179, 1920. ³ N.P.L. Reports, p. 94, 1925. ⁴ Ann. Phys., 87, 769, 1928. ⁵ N.P.L. Reports, p. 8, 1927. ⁶ H.P., 2, 499.

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In the later work (1906 to date) the current, measured in abs. amp., usually with a current balance, is sent through an int. ohm resistance, using a Weston normal cell. From the known current in abs. amp. and the known resistance in int. ohms, one obtains the e.m.f. of the Weston cell in semiabsolute volts. By eq. (11) the ratio of this result to the e.m.f. in int. volt (v), (1.01830 by definition), is r/p , evaluating only r/p , and not q .

The value of the e.m.f. of the Weston cell, in semiabs. volts, the assumed corresponding electrochemical equivalent of silver per abs. coul., and the true resulting value of r/p , are listed by Henning and Jaeger.¹ Omitting a probably less accurate value by Guthe, the remaining four values range from 1.00006 to 0.99989. Henning and Jaeger give correctly as 1.01822 semiabs. volts the Rosa, Dorsey and Miller² value of the e.m.f. of the Weston cell, but misquote and use in their averages the resulting E_{Ag} and r/p , giving 0.99995 for r/p in place of the true 0.99992 ($=1.01822/1.01830$). Using 0.99992, the unweighted average of the four investigations³ is $r/p=0.99995$. The Bureau of Standards⁴ considers only (a) (c) and (d) of reference 3 and gives 0.99991 as the best average value of r/p . The I.C.T. value (0.99990) is based on (a) and (d) only. Henning and Jaeger¹ take the unweighted average of all four values, and Doctor Birge has done the same, since there seem to be differences of opinion as to the relative weighting of these four values. It is very probable that (c) should be given a relatively lower weight; the final average is fortunately not changed.

The next question concerns the equality of r/p and q . Rosa, Vinal and McDaniel⁵ determined the e.m.f. of the Weston cell as 1.01827 int. volt (a), by using a silver voltameter and an int. ohm resistance. Hence by eqs. (4) and (8), knowing 1.01827 int. volt (a) $=$ 1.01830 int. volt (v), $pq/r=1.01830/1.01827=1.00003$. Hence $q=1.00003\ r/p$. These investigators naturally assumed $r/p=0.99992$, for reference 3 (d). Hence $q=0.99995$. This is the figure misquoted as r/p , by Henning and Jaeger.¹

The result indicates that q differs from r/p by 3 parts in 10^5 , and that, to agree with the primary int. units, the Weston cell should have been taken as 1.01827 int. volts. But at the Reichsanstalt,⁶ the corresponding quantity was found, in 1908, to be 1.01834 int. volts, and in 1922, 1.01831. The average of these three results indicates that the accepted value of 1.01830 int. volts is correct within limits of error. In other words, $q=r/p$, and one int. volt (a) $=$ one int. volt (v). This agrees with the view of Henning and Jaeger.⁷ The relative values of q and r/p adopted by the I.C.T. are based directly on the work of the Bureau of Standards.^{2, 6}

¹ H.P., 2, 500, Table 6. ² Bur. Standards Bull., 8, 269, 1912. ³ (a) Ayrton, Mather, Smith, (N.P.L.) 1908, $r/p=0.99989$, (b) Janet, Laporte, Jouaust, 1908, 1.00006, (c) Haga, Boerema, 1913, 0.99994, (d) Rosa, Dorsey, Miller (Bur. Standards), 1912, 0.99992. ⁴ Bur. Standards Circ. 60, 38, 1916. ⁵ Bur. Standards Bull., 10, 475, 1914. ⁶ Z. Instrument., 28, 327 and 353, 1908; *ibid.*, 42, 221, 1922. ⁷ H.P., 2, 501.

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Henning and Jaeger¹ consider that the variation from unity of either r/p or q is less than the experimental error, and think it more practical to assume $r/p=q=1.0000$. It seems best to accept the mean value of $r/p=0.99995$, determined in four different laboratories, with the probable error as ± 0.00005 . Assuming then no distinction between int. volt (v), and int. volt (a), we have

$$p=1.00051 \pm 0.00002$$

$$pq=1.00046 \pm 0.00005$$

$$q=0.99995 \pm 0.00005$$

$$pq^2=1.00041 \pm 0.00010$$

The atomic weights of certain elements.—In evaluating some of our constants, it is necessary to use the atomic weights of various elements. In the ultimate analysis, only ratios of atomic weights enter our formulas for the general constants. All atomic weights are determined from ratios, but in general not directly from the particular ratios we need. Hence it is necessary to consider individual atomic weights.

The present atomic weights are based on the arbitrary assumption that the weight of oxygen is 16 exactly. In choosing oxygen as a basis, it is assumed that it has always the same atomic weight; i. e., it has no isotopes. Giaque and Johnston² have very recently found an isotope of atomic weight 18, from an analysis of the atmospheric absorption bands of oxygen. H. D. Babcock states that experiments performed on absorption coefficients in these bands indicate that O_{18} has an abundance of only one part in 1250 (probable error some 25 per cent). Aston's atomic weights should be greater than the chemical values by about one part in 10,000. Babcock's determination of relative abundance, involves the *assumption* that the absorption coefficient is the same, per molecule, for each species of molecule ($O_{16}-O_{16}$ and $O_{16}-O_{18}$), and this may not be true. The atomic weights determined by Aston,³ from the mass spectrograph, need not be identical with those determined by chemical means, since Aston's atomic weights are based on the mass 16 isotope of oxygen considered as exactly 16, while the chemical atomic weights are based on the ordinary mixture of the two isotopes considered as exactly 16. We shall see that Aston's atomic weights of hydrogen, helium, nitrogen and iodine seem to agree with the chemical values within his *limit* of error (one part in ten thousand to one part in five thousand).

Hydrogen.—Moles⁴ lists nine results lying in the narrow range 1.00766 to 1.00783, with a mean value of 1.00777 ± 0.00002 , or a rounded figure of 1.0078. The final average represents the result of 223 different measurements by five different investigators, using four different methods, and seems to be the most reliable now available. Doctor Birge accordingly adopts

¹ H.P., 2, 501. ² Journ. Amer. Chem. Soc., 51, 1436, 1929. ³ Proc. Roy. Soc., 115 A, 487, 1927. ⁴ Berichte, 61 B, 1, 1928; 59, SII, (A) 1926.

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$$H = 1.00777 \pm 0.00002.$$

Aston, from positive ray analysis, obtains $H = 1.00778$ with a limit of error 0.00015. The recent discovery of an isotope of oxygen makes it permissible to use Aston's value only as an indication of the relative abundance of O_{18} and O_{16} , not as an atomic weight determination. It is in perfect agreement with the chemical value, which indicates a very low abundance of O_{18} .

Helium.—The true atomic weight of helium must be close to Aston's value. The chemical value is at present slightly less accurate than Aston's, and Doctor Birge accordingly adopts his value but his assumed error as the *probable* error, although he considers such a procedure may be open to criticism, in view of the situation regarding the oxygen isotopes. He accordingly writes

$$He = 4.0022 \pm 0.0004.$$

Nitrogen.—The error in the atomic weight of nitrogen produces practically the entire error in the atomic weight of silver. Since the great majority of the accepted atomic weights are derived more directly from silver than from oxygen, that of silver is of the highest importance.

The atomic weight of nitrogen can be obtained by direct comparison with oxygen, and also from density measurements, using the adopted value of R . According to Clarke,¹ the final average of these two methods gives $N = 14.0076$. The atomic weight can be obtained indirectly in many ways. The results of all methods, including the two just mentioned, are summarized by Clarke¹ and give $N = 14.0081$, presumably the best value in 1920. Now it is generally agreed that, as in the case of helium, the atomic weight of nitrogen can be determined most accurately from its density and deviation from a perfect gas, by the use of $R = M(1-a)/L$ where R is 22.4146 ± 0.0008 (see p. 77), $(1-a) = 1.00043 \pm 0.00002$,² and $L = 1.25046 \pm 0.000045$ ³ whence

$$N = 14.0083 \pm 0.008.$$

Aston⁴ obtains $N = 14.008$, but his assumed accuracy is only one part in 5000. Aston gives always the *limit* of error, and his *probable* error should be much smaller. His values all agree beautifully with the chemical values; the decision as to his actual probable error may be left open.

Silver.—The best atomic weight of silver is at present directly dependent on that of nitrogen. A summary is given by Moles and Clavera.² Of the many methods for obtaining the value of Ag , the most accurate is based on the reduc-

¹ Mem. Nat. Acad. Sci., 16, 1920. ² Z. anorg. Chem., 167, 49, 1927. ³ Ibid., 167, 40, 1927. ⁴ Proc. Roy. Soc., 115 A, 487, 1927.

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tion of AgNO_3 to Ag. Since $O = 16.000$, by definition, the sole error is due to that in N. The proportional error is due to that in NO_3 , only about one fourth the probable proportional error in N. The ratio AgNO_3/Ag can be determined with great precision. The most accurate ratio, by far, is that by Richards and Forbes,¹ yielding also 1.57479. A very elaborate investigation by Hönigschmid, Zintl and Thile,² gives again exactly the same ratio. With our adopted value of N and the above value of $\text{AgNO}_3/\text{Ag} = r$, one has $\text{NO}_3/(r-1) = (62.0083 \pm 0.0008)/(0.57479) = 107.8799 \pm 0.0014$.

The atomic weight of silver can be obtained in many ways. Clarke³ lists 43 methods, yielding a final weighted average of 107.8804. It seems reasonable that at the present time only the AgNO_3/Ag ratio results need be considered, with a final real error in Ag due merely to that in N. It seems reasonable to adopt

$$\text{Ag} = 107.880 \pm 0.001.$$

Iodine.—The atomic weight of iodine enters into the discussion of the value of the faraday. Clarke³ lists eight methods, with a mean of 126.926. This result will bear closer scrutiny. The most accurate is the direct determination of the I/Ag ratio, assuming the atomic weight of silver as known. Among the values of this ratio, 1.176603, obtained by Baxter,⁴ in 1910, is the most reliable. Clarke lists all determinations. Now the four earlier results are all approximately 1.1753, while the later results run much higher. These earlier results probably are vitiated by some systematic error. They are quite self consistent, and so by Clarke are given a high weighting. With the four earlier results eliminated, we have a new weighted average of 1.176549, in closer agreement with Baxter's 1910 result. This ratio, combined with $\text{Ag} = 107.880$, gives $\text{I} = 126.926$, while Baxter's result gives 126.932. Using the revised average value for the I/Ag ratio with Clarke's results for the other seven methods, we obtain a final weighted average of $\text{I} = 126.932$, in place of Clarke's value 126.926, and in exact agreement with Baxter's result. Doctor Birge adopts

$$\text{I} = 126.932 \pm 0.002.$$

In conclusion it is of interest to note that Aston gets $\text{I} = 126.932$, in exact agreement with our adopted value.

Carbon.—The atomic weight of carbon can be determined directly from oxygen. The result of all such determinations, as obtained by Clarke,³ is 12.0000 ± 0.00026 . This result (written 12.000) was accepted in 1925 by the International Committee on Atomic Weights,⁵ and has since been used by Baxter.⁶

¹ Journ. Amer. Chem. Soc., 29, 808, 1907. ² Z. anorg. Chem., 163, 65, 1927. ³ Mem. Nat. Acad. Sci., 16, 1920. ⁴ Journ. Amer. Chem. Soc., 32, 1591, 1910. ⁵ Journ. Amer. Chem. Soc., 47, 597, 1925. ⁶ Journ. Amer. Chem. Soc., 50, 603, 1928.

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Thirteen methods, including the above, listed by Clarke, give a weighted mean of 12.0025 ± 0.00019 . Aston¹ finds $C = 12.0036$, (limit of error 0.0012). The mean of the final Clarke value and Aston's value is 12.003, and is adopted here.

$$C = 12.003 \pm 0.001.$$

Calcium.—The atomic weight of calcium is needed for the grating space of calcite. The value of Ca, accepted since 1911, is 40.07. When readopted in 1925 by the International Committee, reference was made to the work of Richards and Hönigschmid.² These investigators precipitate CaCl_2 by a solution of Ag, and determine the amount of AgCl produced. They assume $\text{Ag} = 107.88$ and $\text{Cl} = 35.457$. The final result is $\text{Ca} = 40.075$, based on four determinations ranging from 40.085 to 40.070. It seems probable that the Richards and Hönigschmid value of 40.075 is the best. The probable error 0.005, is very uncertain.

$$\text{Ca} = 40.075 \pm 0.005.$$

The normal atmosphere (A_n).—The normal atmosphere is defined as the pressure due to a column of Hg 76 cm high, of normal density (0°C , A_n), under normal gravity.

The I.C.T. gives $A_n = 1.013250 \times 10^6$ dyne \cdot cm⁻², based on the definition of A_n as the pressure of a column of a liquid of density 13.5951 g per cm³, normal gravity. The H.P. gives $A_n = 1.013253 \times 10^6$, from the defining equation $A_n = H_n \cdot \rho_n(\text{Hg}) \cdot \delta_m(\text{H}_2\text{O}) \cdot g_n$, in which H_n = height of normal barometer = 76.000 cm, ρ_n = normal specific gravity of Hg (at 0°C , A_n), referred to air-free water of max. density, $\delta_m(\text{H}_2\text{O})$ = max. density of water, g_n = normal gravity⁴ = 980.665 cm \cdot sec.⁻². Henning and Jaeger,³ using the density of mercury in the definition, investigate the most probable value of ρ_n , then adopt $\rho_n = 13.5955$. The value of $\delta_m(\text{H}_2\text{O})$ is 0.999973 g \cdot cm⁻³. The product $\rho_n(\text{Hg}) \cdot \delta_m(\text{H}_2\text{O}) = D_n = 13.5955 \times 0.999973 = 13.595133$ g \cdot cm⁻³, agreeing with the I.C.T. value to the six significant figures given by the I.C.T., but, with the use of seven figures, leading to $A_n = 1,013,253$, as given by the H.P.

Doctor Birge adopts as the most probable value of ρ_n , the figure calculated by Scheel and Blankenstein,⁴ viz. 13.59546. $D_n = 13.59546 \times 0.999973 = 13.59509$ g \cdot cm⁻³, and $A_n = 13.59509 \times 76 \times 980.665 = 1.013249 \times 10^6$ dyne \cdot cm⁻². This should have a probable error of not more than two or three units in the last digit, ± 0.000003 .

The 45° atmosphere is obtained by the mere substitution of g_{45} (980.616) for g_n .

$$A_n = (1.013249 \pm 0.000003) \times 10^6 \text{ dyne} \cdot \text{cm}^{-2}.$$

$$A_{45} = (1.013199 \pm 0.000003) \times 10^6 \text{ dyne} \cdot \text{cm}^{-2}.$$

¹ Proc. Roy. Soc., 115 A, 487, 1927. ² Z. anorg. Chem., 163, 315, 1927. ³ H.P., 2, 490, 494. ⁴ Z. Phys., 31, 202, 1925.

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Note.—It is evident that the definition of the normal atmosphere given by Dorsey in the I.C.T. is technically quite different from Henning and Jaeger's in the H.P. The I.C.T. definition makes the normal atmosphere a conventional constant, with no probable error. Doctor Birge had some correspondence on this matter with Doctor Dorsey, leading to the conclusion that the H.P. definition is correct. The adopted value is therefore based on this H.P. definition.

Unfortunately, an article by Burgess¹ was overlooked in which the "standard atmosphere" is defined as "the pressure due to a column of mercury 760 mm high, having a mass of $13.5951 \text{ g} \cdot \text{cm}^{-3}$, gravitational acceleration of $980.665 \text{ cm} \cdot \text{sec}^{-2}$, and is equal to $1,013,250 \text{ dyne} \cdot \text{cm}^{-2}$." It is thus a conventional constant, with no error. This definition was adopted in 1927 by the International Commission of Weights and Measures. Fortunately, this definition makes no change in the magnitude or the error of any derived constant. It should be noted that no temperature is specified and that the word "mercury" is technically superfluous. This seems very objectionable, since there is thus technically no simple method for reducing to standard atmospheres an actual barometer reading at an actual observed temperature. The H.P. definition, as used by Doctor Birge, seems preferable, in spite of international agreement.

The absolute temperature of the ice-point (T_0).—The generally accepted value of T_0 was, for many years, 273.09°K. , based on Berthelot's analysis² of the data of Chappuis,³ and of Joule and Thomson for the porous plug experiment. The final average value was $\gamma = 36618 \times 10^{-7}$, or $T_0 = 273.09^\circ$. The I.C.T. gives $T_0 = 273.1$ as one of its basic constants.

Most extensive observations on the volume and pressure coefficients (α and β) of certain gases have recently been made by Henning and Heuse,⁴ at the Reichsanstalt. The value of γ was obtained by two different methods.⁵

The first method gave for the gases He, H_2 , and N_2 , $\gamma \times 10^7 = 36600, 36607$, and 36606 , or $T_0 = 273.224^\circ, 273.172^\circ$ and 273.179° . The mean is $\gamma \times 10^8 = 366043$ or $T_0 = 273.190^\circ \pm 0.015$.

The second method gave for He (two determinations at slightly different p_0), H_2 and N_2 , $\gamma \times 10^7 = 36598, 36597, 36617$, and 36604 . The mean is 36604.0 or $T_0 = 273.194^\circ$. They conclude that the best mean value of all the experiments is $\gamma \times 10^7 = 36604$. The reciprocal of this is $T_0 = 273.19^\circ$. They write it as 273.20° . In the later article⁴ by Heuse, neon is used, and the above value of γ is confirmed.

The only other determination of T_0 of comparable accuracy is that by Roebuck,⁶ using the Joule-Thomson effect in air.⁷ This method requires α , the volume coefficient, as well as the Joule-Thomson coefficient μ . Roebuck mea-

¹ Bur. Standards Journ. Res., 1, 635, 1928. ² Trav. et Mem. Bur. intern., 13, 12, 1907.

³ Ibid., vols. 6, 13. ⁴ Z. Phys., 5, 264, 1921; 5, 285, 1921; 37, 157, 1926. ⁵ H.P., 9, 527.

⁶ Proc. Amer. Acad. Arts and Sci., 60, 537, 1925. ⁷ H.P., 2, 496.

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sured μ , but for α used data, mainly by Chappuis. Henning and Jaeger¹ note this and adopt merely the Henning and Heuse value 273.20° (which as previously noted should be 273.19°). Roebuck obtained three results, 273.18° , 273.16° and 273.12° , average, 273.15° . He lists all previous determinations, and chooses 273.17° , lying midway between his own result and that of Henning and Heuse. He gives $\pm 0.02^\circ$ as the probable error. Doctor Birge feels that these two results (273.15° and 273.19°) are entitled to far more weight than any of the older work, but that the second result is probably the most accurate, being based on new determinations of α . Hence he adopts—with the probable error given by Henning and Jaeger—

$$T_0 = 273.18 \pm 0.03^\circ \text{K.}$$

(Roebuck's $\pm 0.02^\circ$ may well be more reasonable).

The mechanical equivalent of heat (J) and the electrical equivalent of heat (J').—A description of the methods for the evaluation of J , and a discussion of the results, is given by Jaeger in the H.P.² The value adopted by Henning and Jaeger in the H.P.³ is one cal.₁₅ = 4.184₂ int. joule = 4.186₃ abs. joule. The I.C.T. value is one cal.₁₅ = 4.185 abs. joule. The cal.₁₅ is defined as the amount of thermal energy required to heat one gram of pure water from 14.5° to 15.5°C .

Joule turned mechanical energy directly into thermal energy, and J was evaluated in abs. joules. In most modern work electrical energy is turned directly into thermal, thus evaluating the *electrical* equivalent of heat (J' , measured in int. joules). Since the relation between the int. joule and the abs. joule (10^7 ergs) is known with considerable precision, the mechanical equivalent may be obtained from the electrical equivalent.

The value of J adopted by the H.P. results from the work of Jaeger and Steinwehr.⁴ They determined J' , for many different mean temperatures lying between 4.75°C and 49.60°C . This is undoubtedly the most accurate work now available. They list 67 results. These results are represented as a parabolic function of t .

On examining their data, Doctor Birge finds that a parabola is not a sufficiently complex function. Their residuals show pronounced trends; unfortunately the largest trend is near 15°C . He accordingly made a separate investigation of the best curve for their data.

$$J' = 4.21040 - 2.78958 \times 10^{-3}t + 7.73723 \times 10^{-5}t^2 \\ - 8.52567 \times 10^{-7}t^3 + 3.7540 \times 10^{-9}t^4 \quad (1)$$

This gives $J'_{15} = 4.18327$ int. joules, and is the most probable value resulting from the work of Jaeger and Steinwehr. Jaeger gives two parts in 10000 (i.e., 8×10^{-4} joules) as the probable error. Doctor Birge therefore writes $J'_{15} = 4.1833 \pm 0.0008$ int. joules. We have one int. joule = pq^2 abs. joule, where $pq^2 = 1.00041 \pm 0.00010$. Hence there results

$$J_{15} = (4.1833 \pm 0.0008)(1.00041 \pm 0.00010) = 4.1850 \pm 0.0009 \text{ abs. joules.}$$

¹ H.P., 2, 496. ² H.P., 9, 476. ³ H.P., 2, 497. ⁴ Ann. Phys., 64, 305, 1921.

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The most accurate direct determination of the *mechanical* equivalent of heat J is the work of Laby and Hercus,¹ which appeared since the H.P. was compiled. They use a continuous flow calorimeter and make 23 determinations, grouped about six different temperatures, the temperature change in the calorimeter being always about 5°C . Their result is $J = 4.1841 \pm 0.0001$ abs. joules at 16.67°C .

A more precise method of reduction is first to adopt a curve for the temperature variation of the specific heat of water. Such a curve is given immediately by eq. (1). If it is desired that the specific heat at 15°C be unity, eq. (1) is to be divided by 4.18327. Doctor Birge finally adopts

$$\text{one } 15^{\circ} \text{ calorie } (J_{15}) = 4.1852 \pm 0.0006 \text{ abs. joules}$$

$$\text{one } 15^{\circ} \quad \quad (J'_{15}) = 4.1835 \pm 0.0007 \text{ int. joules}$$

and by eq. (1)

$$J_{20} = 4.1813 \pm 0.0006 \text{ abs. joules}$$

$$J'_{20} = 4.1796 \pm 0.0007 \text{ int. joules}$$

The faraday (F).—The faraday is defined as the quantity of electricity carried in electrolysis by one gram equivalent of any element. It is believed to be a general constant of nature. According to modern ideas, each univalent ion carries a charge numerically equal to the electronic charge e . The Avogadro number N_0 gives the number of atoms (or molecules) in one gram equivalent. Hence one may define the faraday more precisely as the product $N_0 \cdot e$. The fact that F can be most accurately evaluated from electrolysis, and N_0 is then obtained from F and e , does not affect the validity of the definition.

One electrochemical equivalent is the mass associated with unit electric charge. Like the faraday, its true value, independent of experimental conditions, depends only on the adopted unit of charge. On the other hand we can measure only the amount of a substance deposited or released in an electrolytic cell, per unit current per second. This is affected by experimental conditions, and may or may not equal the electrochemical equivalent. The faraday is then, by definition, the ratio of the gram equivalent of a substance to its electrochemical equivalent. Almost universally the distinction between mass deposited per unit charge, and electrochemical equivalent is ignored. Considerable confusion results regarding the best value of certain electrochemical equivalents, and the resulting best value of the faraday.

Nevertheless, it is convenient to *assume*, for the moment, that the silver deposited per unit charge in a silver voltameter, under the conditions defining the international ampere, is the electrochemical equivalent of silver (E_{Ag}). With this assumption, the value of faraday follows from constants already adopted. The gram equivalent of silver, or of any univalent substance, is numerically equal to its atomic weight in grams (Ag). The amount of silver deposited in electrolysis by one international coulomb is, by definition, 0.00111800 gram. Hence

¹ Phils. Trans., A 227, 63, 1927.

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$$\begin{aligned}
 F &= Ag/0.00111800 = (107.880 \pm 0.001)/0.00111800 \text{ int. coul.} \\
 &= 96494. \pm 1 \text{ int. coul.}, & (1) \\
 &= 96489. \pm 5 \text{ abs. coul.} & (2)
 \end{aligned}$$

If $q=1$, as adopted by the H.P., $F=96494$ int. coul. *or* abs. coul., the actual value adopted by Henning and Jaeger. If $q=0.99993$, as adopted by the I.C.T., there results $F=96487$ abs. coul. The I.C.T., however, adopts $F=96500 \pm 10$ abs. coul., which with its adopted value of q , leads to $F=96507$ int. coul. This last value requires $Ag=107.893$, in direct contradiction to facts. $F=96500 \pm 10$ abs. coul. is evidently taken from Vinal and Bates,¹ and to understand the seeming discrepancy, it would be necessary to examine in detail this last quoted work employing the distinction between mass carried in electrolysis and mass deposited (see Doctor Birge's discussion, Phys. Rev., Suppl. 1, 35, 1929). Henning and Jaeger² make no distinction between mass carried and mass deposited, writing $E_{Ag}=0.00111800$ g per int. coul. It seems evident from Vinal and Bouvard³ that there *are* inclusions in the silver deposit, tending to make E_{Ag} too large by 4×10^{-8} g, and F too small by 4 coulombs. There may be small parasitic chemical reactions in the silver voltameter, tending to decrease the value of E_{Ag} and hence to increase the value of F . It seemed best to *adopt* the value of F given in eqs. (1) and (2), but to assign to E_{Ag} a probable error of 5×10^{-8} g, i.e., an error slightly greater than the measured effect of the inclusions. Then

$$\begin{aligned}
 F &= \frac{107.880 \pm 0.001}{(1.11800 \pm 0.00005) \times 10^{-3}} = 96494 \pm 5 \text{ int. coul.} & (3) \\
 &= 96489 \pm 7 \text{ abs. coul.} \\
 &= 9648.9 \pm 0.7 \text{ abs. em units,} \\
 &= (2.89270 \pm 0.00021) \times 10^{14} \text{ abs. es units.}
 \end{aligned}$$

The electronic charge (e).—The values of a large number of important constants depend directly on the value of the electronic charge; in most cases the final probable error is due mainly to the error in e . It is desirable that it be determined in many different ways, and by many different persons. The situation has been the reverse. Only one precision method for the evaluation of e was known, and the work had been carried out by a single individual. It is very fortunate that the investigation referred to is a masterpiece. Millikan's⁴ investigations extend over more than a decade; the latest value of e was published in 1917. The great importance of e , and because higher values have recently been obtained, led Doctor Birge to investigate the matter in more than usual detail.

Millikan found that if the viscosity of air is taken as constant, in Stokes' law of fall, the apparent value of e is a function of the radius of the drop and of the pressure of the air. The true value of e can be found by assuming a modification of Stokes' law such that his observations could be plotted as a

¹ Bur. Standards Bull., 10, 425, 1914 (p. 447). ² H.P., 2, 502. ³ Bur. Standards Bull., 13, 147, 1916. ⁴ Phys. Rev., 29, 60, 1909; 32, 342, 1911; 2, 109, 1913; Philos. Mag., 34, 1, 1917; 19, 209, 1910.

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linear graph, its intercept on the y axis giving $e^{2/3}$, and leading to the desired quantity.

Millikan found that for values of $1/pa$ less than about 700 (p in cm Hg, a , radius of drop, in cm), the resulting graph was linear. Only that part of the curve corresponding to $1/pa$ less than 700 was used in precise determinations of e . The 1917 value of e was deduced from 25 oil drops, each giving one point on the graph. The 25 observations form a beautifully consistent set of data. The least squares solution, as calculated by Doctor Birge, gives for the intercept $(61.111 \pm 0.032) \times 10^{-8}$; but plotted data are based on the 1913 value (0.0001824) for the viscosity of air. The value of $a_0 (= e^{2/3})$ is proportional to the viscosity. With the improved 1917 value of the viscosity (0.00018227), $e = a_0^{3/2} = (4.7721 \pm 0.0038) \times 10^{-10}$ es units.

Millikan starts 18 of the points, with conditions of observation as perfect as possible. These 18 drops give $a_0 = 61.121 \pm 0.038$ ($e = 4.7733 \pm 0.0045$, 1917 viscosity). These 18 drops deviate from the best straight line more than do the other 7. The standard deviation of the 25 drops is 0.121×10^{-8} , while for the 18 drops it is 0.123×10^{-8} . The drops of smaller radius fall more slowly, and can be more accurately timed. Actually they are less reliable. Thus 13 smaller drops have a standard deviation of 0.134, considered as part of the 25 drops, definitely larger than the 0.121 average of the 25. A least squares solution of these 13 drops gives $a_0 = 61.143 \pm 0.050$, standard deviation of 0.132. This is so close to 0.134 that we can conclude that the 13 drops fit the graph of the entire 25 as well as a graph designed to fit them alone. On the other hand, the 12 larger drops give for the least square solution, $a_0 = 61.078 \pm 0.045$, standard deviation 0.117, thus definitely more reliable than the smaller drops. The resulting value of e , reduced to the 1917 viscosity, is 4.7759 ± 0.0058 for the 13 smaller drops, and 4.7683 ± 0.0053 for the larger drops. The weighted mean is 4.7718, in essential agreement with the value (4.7721) obtained from all 25 drops. This, of course, is what we should expect.

The average deviation from the average for small and large drops is 0.0038, much less than the probable error of either. This is an analytic proof that the true value of e is not a function of the radius of the drop. This also indicates that the larger drops are, if anything, more reliable than the smaller. If the larger are given a higher weight, the resulting value of e would lie between 4.772 and 4.768. The final conclusion is that there is no particular reason for giving different weights to the different drops, and that any such weighting, if made, would slightly lower e . We therefore take 4.772×10^{-10} es units as the best result of the 1917 work.

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In 1913 data on 58 drops were obtained. Millikan used, in evaluating e , the 23 drops (out of 58) of smallest $1/pa$. These are more consistent, having a standard deviation of only 0.092. They lead to $e=4.7665\pm0.0058$ (1917 viscosity), while the entire 58 give 4.7703 ± 0.0022 . This last figure might appear more reliable than that of 1917; such a conclusion ignores other errors. In 1913 Millikan estimated four factors, each with a maximum uncertainty of 0.1 per cent. In 1917 he estimated two such factors, each with a maximum uncertainty of 0.05 per cent. His final 1917 estimate for the maximum uncertainty in e is 0.1 per cent, based mainly on these two factors. The above calculations show, however, a *probable error* of 0.08 per cent (±0.0038) in the 1917 value, due to accidental errors. The final uncertainty is therefore several times as large. Doctor Birge estimates that the final *probable error* is about 0.1 per cent, and writes $e=(4.772\pm0.005)\times10^{-10}$ *es* units.

This value is now subject to two further corrections. In reducing the result to *es* units per cm, Millikan used $c=2.999\times10^{10}$ cm · sec.⁻¹, and made no distinction between international and absolute electrical units. It has been shown definitely that the int. volt differs from the abs. volt by an appreciable amount. We have also now the new value, $c=2.99796$. The change in c is obvious, it lowers e from 4.772 to 4.770. The other change seems to have been overlooked by everyone. Because the electrical potential forces the charged drops against the viscosity of air, instead of against *electrical* resistance, one has *only* electric voltage coming into the calculations. One int. volt = 1.00046 ± 0.00005 abs. volts. The true value of F , in abs. volts, is larger and the true value of e , in abs. *es* units is smaller by just this ratio. Hence, the value of e is reduced¹ from 4.770 to 4.768. Since the error in each of these corrections is negligible, the final result is $e=(4.768\pm0.005)\times10^{-10}$ abs. *es* units. This should be the most reliable value from Millikan's oil-drop work.

Recently an entirely different method has been devised for e . The two results which have already been published are apparently less reliable than the oil-drop value. This new method measures directly the Avogadro number N_0 , and from this and the value of the faraday, e immediately follows. It utilizes the absolute wave lengths of X-ray lines, determined with an ordinary ruled grating at grazing incidence, as compared with the wave lengths determined with a crystal grating.

$$\lambda = 2d \cdot \sin \theta \quad (1)$$

where d is the grating space. It has been pointed out by Siegbahn,² and by

¹ Professor Millikan agreed, 1928. ² Siegbahn, Spectroscopy of X-rays, p. 26.

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Compton, Beets and DeFoe,¹ that, to obtain the *true* X-ray wave length λ , it is necessary to use an *effective* grating space d , automatically correcting for the refraction of the X rays at the crystal surface. For first order spectra and the high frequencies of ordinary X rays, the *true* grating space d' is connected with the effective space d by the relation

$$d = d'(1 - 0.000135). \quad (2)$$

Siegbahn uses for calcite $d = 3.02904 \times 10^{-8}$ cm, at 18°C . This is a more or less arbitrary value, assuming that d for rock-salt, at 18°C , is 2.81400×10^{-8} cm. We shall denote by d''_{18} this 3.02904 value, and by λ'' the resulting wavelength. Hence

$$\lambda'' = 2d''_{18} \sin \theta \quad (2)$$

and

$$\lambda/\lambda'' = d_{18}/d''_{18} \quad (3)$$

where λ is the true wave length from a ruled grating, d_{18} the effective grating space of calcite at 18°C , λ'' the supposed true wave length from measures with a calcite crystal with d''_{18} as an assumed grating space at 18°C . d_{18} follows knowing d''_{18} and λ . From (2) we obtain d'_{18} , the true grating space of calcite. The temperature coefficient² is 1.04×10^{-5} ; d'_{20} is accordingly 2.08×10^{-5} larger. This 20° value is given theoretically by the formula

$$d'_{20} = \{nM/\rho N_0 \phi(\beta)\}^{1/3} \quad (4)$$

where n is $\frac{1}{2}$, M , the molecular weight of calcite (CaCO_3), ρ , its density at 20°C , $\phi(\beta)$, a geometrical constant depending on the crystal structure, and N_0 , F/e ; knowing d'_{20} we can obtain N_0 and then e .

We have $M = 100.078 \pm 0.005$; the best value of ρ is $2.7102 \pm 0.0004 \text{ g} \cdot \text{cm}^{-3}$ (DeFoe, Compton³), of $\phi(\beta)$, 1.09630 ± 0.00007 at 20°C (Beets⁴) whence

$$e = (1.7176 \pm 0.0003) \times 10^{13} (d'_{20})^3. \quad (5)$$

The two published determinations of d_{18} , based on absolute X-ray wave lengths, are by Bäcklin,⁵ and Wadlund.⁶ Using (3), Wadlund obtains $1.5373 \pm 0.0008\text{\AA}$ for the $\text{K}\alpha_1$ line of Cu, combined with Siegbahn's values of d''_{18} and λ'' , giving $d_{18} = (3.0290 \pm 0.0016) \times 10^{-8}$ cm. The corresponding value of d_{20} is 3.02906 ; the true grating space d'_{20} , $(3.0295 \pm 0.0016) \times 10^{-8}$ cm. This value is to be substituted in (5). It gives $e = (4.7757 \pm 0.0076) \times 10^{-10}$ abs. es units. This is not as accurate as the oil-drop value.

It is difficult to appraise the work of Bäcklin, as regards its accuracy. He gets $8.333 \pm 0.008\text{\AA}$ for the absolute wave length of the Al $\text{K}\alpha$ line. Comparing this with an unpublished result by A. Larsson ($8.3229 \pm 0.0008\text{\AA}$), obtained with a crystal, Bäcklin obtains $d_{18} = 3.033 \pm 0.003\text{\AA}$. This gives $d'_{20} = 3.03347\text{\AA}$, and $e = (4.794 \pm 0.015) \times 10^{-10}$ abs. es units. This value is 0.55 per cent higher than the oil-drop result.

¹ Phys. Rev., 25, 625, 1925. ² Siegbahn, Spectroscopy of X-rays, p. 85. ³ Phys. Rev., 25, 618, 1925. ⁴ Phys. Rev., 25, 621, 1925. ⁵ Upsala Dissertation, 1928. ⁶ Proc. Nat. Acad. Sci., 14, 588, 1928; Phys. Rev., 32, 841, 1928.

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Bäcklin's results lead to 4.794 ± 0.015 .

The investigation by Bäcklin is a pioneer piece of work, and it is quite likely, as such, to contain unsuspected systematic errors. If the three values of e (4.768 from Millikan's oil-drop work, 4.776 by Wadlund, and 4.794 by Bäcklin) are weighted according to the apparent probable error of each, the result is still suspiciously high. The thorough examination made of the actual value of e and its probable error, from the oil-drop work, was carried out because of this inconsistency. It seems best to reject the Bäcklin value, and to use the weighted mean of the remaining two values, viz. 4.768 ± 0.005 and 4.776 ± 0.008 , or 4.770; as usual adopt as its probable error the smaller of the two individual errors, rather than that given by least squares; the latter is meaningless when only two observations are concerned. The finally adopted value is then

$$e = (4.770 \pm 0.005) \times 10^{-10} \text{ abs. es units.}$$

The specific charge of the electron (e/m).—A very complete and critical account of all work on the measurement of e/m , up to 1919, has been given by Bestelmeyer.¹ His final conclusion is that $e/m = (1.76 \pm 0.02) \times 10^7 \text{ em units}$. A more recent discussion is that by Gerlach,² who concludes that $e/m = 1.766 \times 10^7 \text{ em units}$. The question is discussed very briefly by Henning and Jaeger,³ who however adopt Gerlach's value. The I.C.T. adopts 1.769 ± 0.003 .

The latest work greatly exceeds in accuracy all the preceding; it seems legitimate to confine the discussion to these new results. The value of e/m has been obtained with considerable accuracy by three distinct methods, (a) deflection of electrons in electric and magnetic fields, (b) Zeeman effect, (c) fine structure and relative wave lengths of H and He⁺ spectral lines. It may be obtained also from Bohr's theoretical expression for the Rydberg constant, R_∞ , provided one assumes the value of e and of h . This last method is not as accurate as the preceding. A fifth involves the Compton shift. This also is as yet a relatively inaccurate method.

The latest and most accurate work with method (a), that by Wolf,⁴ is carried out with every possible refinement. The essential point is the employment of a longitudinal magnetic field. The electron velocity is calculated from the potential fall. He concludes that $e/m = (1.7679 \pm 0.0018) \times 10^7 \text{ em units}$. 1.7679 should be corrected for the difference between the int. and abs. units. It then becomes $(1.7689 \pm 0.0018) \times 10^7 \text{ abs. em units}$.

¹ Marx, Handb. Radiologie, 5, 1, 1919. ² H.P., 22, 41. ³ H.P., 2, 504. ⁴ Ann. Phys., 83, 849, 1927.

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The most recent accurate work, using method (b), is by Babcock.¹ A large number of spectrum lines (116 in all) were employed. Nearly all showed a complex Zeeman pattern. For determining e/m it was necessary to assume the Runge denominator of each line. In cases where this is small, it was known with certainty. In some cases it was large and rather uncertain. His work has been criticized, and Gerlach, in his final table,² omits Babcock's result. It appears to Doctor Birge that the criticism is unjustified; at his suggestion, Babcock has recalculated his data, omitting all Zeeman patterns in any way doubtful. The new result,³ based on 48 lines for which the Zeeman pattern is definitely established, is 1.7606 ± 0.0012 ; the error is purely observational. The difference between the two values is just that produced by the change in the value of c . Doctor Birge therefore writes $e/m = (1.761 \pm 0.002) \times 10^7$ abs. cm units as the best result from Zeeman effect.

The latest, most accurate work using method (c), is by Houston,⁴ based on the Bohr-Sommerfeld model consisting of a positive nucleus and *one* encircling electron (moving in elliptic or circular orbits). Such atoms are H and He⁺. In order to determine e/m , we must evaluate the so-called Rydberg constant for hydrogen (R_H) and for ionized helium (R_{He}). Practically the entire error in e/m is merely the error in the *difference* $R_{He} - R_H$.

The pioneer work was performed by Paschen.⁵ He obtained $R_H = 109677.69 \pm 0.06 \text{ cm}^{-1}$, $R_{He} = 109722.14 \pm 0.04 \text{ cm}^{-1}$. Those give $e/m = 1.768 \pm 0.003$, using his values and assumed errors for R_H and R_{He} , but the present accepted values and errors for H , He , and F . The recent investigation by Houston,⁴ is so much more accurate than the work just mentioned that it alone will be considered. Houston's new experimental results are

$$R_{He} = 109722.403 \pm 0.004 \text{ cm}^{-1}, \quad R_H = 109677.759 \pm 0.008 \text{ cm}^{-1}.$$

The stated errors are purely least squares probable errors. He believes the *relative* values of R_{He} and R_H are correct to 0.02, although the *absolute* error in each may be about 0.05.

Houston used $m = 5.4 \times 10^{-4}$, $He = 4.0001$, $H = 1.0077$, $F = 96470$ abs. coulombs, and obtained $e/m = (1.7606 \pm 0.0010) \times 10^7 \text{ cm}$ units. Using his constants and the corrected formula the result is 1.7603. The error in his formula is therefore almost negligible. The entire probable error in e/m , due to errors in all factors, aside from $(R_{He} - R_H)$, is less than 0.01 per cent and so is entirely negligible compared to the error in $(R_{He} - R_H)$.

¹ Astrophys. Journ., 58, 149, 1923. ² H.P., 22, 81. ³ Phys. Rev., 33, 268 A, 1929; Astrophys. Journ., 69, 43, 1929. ⁴ Phys. Rev., 30, 608, 1927. ⁵ Ann. Phys., 50, 901, 1916.

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Using Houston's value of R_H , and of $R_{He} - R_H$, together with the values of H , He , etc., we obtain $e/m = (1.7608 \pm 0.0008) \times 10^7$ abs. em units. This value of e/m thus agrees with that obtained by Babcock. Summarizing the results we find $e/m = 1.769 \pm 0.002$ from deflection experiments, $= 1.761 \pm 0.002$ from Zeeman effect, $= 1.761 \pm 0.001$ from H and He spectra. The discrepancy between the first result and the last two is four times the probable error of the first. Theory gives only one chance in 143 of this occurring. The discrepancy seems to be real.

The last two results are measurements of e/m for electrons *inside of an atom*, based upon the quantum theory of atomic structure. The first is the measurement of e/m for electrons *in free space*. The figures point to the conclusion that the e/m of an electron is less when it is *inside* an atom than when it is *outside*. If this conclusion seems unacceptable, then it would appear that there is some general error in the equations of the quantum theory of atomic structure or there is some unknown general error in all the deflection experiments. Under the circumstances two values may be assumed of e/m —one for where atomic structure is involved, the other for free electrons. Hence

$$\begin{aligned} e/m \text{ (spectroscopic)} &= (1.761 \pm 0.001) \times 10^7 \text{ abs. } em \text{ units per g,} \\ &= (5.279 \pm 0.003) \times 10^{17} \text{ abs. es " " " ,} \\ e/m \text{ (free electrons)} &= (1.769 \pm 0.002) \times 10^7 \text{ abs. } em \text{ " " " ,} \\ &= (5.303 \pm 0.006) \times 10^{17} \text{ abs. es " " " .} \end{aligned}$$

The Planck constant (h).—The Planck constant has been evaluated in a number of ways. There is difference of opinion as to the relative accuracy of the results; some are more or less incompatible. A satisfactory determination of this constant is difficult.

The first attempt to obtain a value of h , from the results of all seven methods, was made by Doctor Birge in 1919. The value found was $(6.5543 \pm 0.0025) \times 10^{-27}$ erg · sec., the error being merely the least-squares probable error. This error has been criticized by Ladenburg as far too small. It is *not* the final error since, as clearly stated, one must add to it an error somewhat greater than the proportional error in e . This occurs with some positive power (unity to two) in every known method for obtaining h . This makes the total probable error more nearly ± 0.01 . Doctor Birge's 1919 evaluation of h has been adopted by the I.C.T., but the probable error should be ± 0.001 .

In 1920 Ladenburg¹ wrote an article on the evaluation of h , in which several of Doctor Birge's conclusions were criticized. His own result in that article was 6.54 ± 0.01 . In 1925 Ladenburg wrote another article on this subject, for the H.P.² He then concludes that $h = 6.547$, which value he rounds

¹ Jahrb. Radioakt. und Elektronik, 17, 93, 1920. ² H.P., 23, 279.

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off to 6.55 ± 0.01 . Henning and Jaeger¹ discuss the most probable value and adopt 6.55.

(a) *Bohr's formula for the Rydberg Constant.*—Bohr's theory of the Hydrogen atom leads to the equation

$$R_{\infty} = 2\pi^2 c^5 / h^3 c^2 e / m \quad (1)$$

in which R_{∞} is the Rydberg constant for infinite mass (cm^{-1} units), e , the electronic charge (abs. *es* units), and e/m is in *em* units. R_{∞} is derived from the observed R_H by the equation

$$R_{\infty} = R_H (1 + m/m_H) = R_H \{ 1 + F/(e/m)(H - m) \} = 109737.424 \text{ cm}^{-1}. \quad (2)$$

The probable error in R_{∞} is about 0.06 cm^{-1} . In absolute units $R_{\infty} \cdot c = (3.28988 \pm 0.00004) \times 10^{15} \text{ sec}^{-1}$. Substituting in (1) the spectroscopic value of e/m , since we are dealing with spectroscopic data,

$$h = (6.547 \pm 0.011) \times 10^{-27} \text{ erg} \cdot \text{sec}.$$

After adopting a weighted mean value of h , (1) becomes a method for calculating, indirectly, the value of R_{∞} . Or, using the directly determined value R_{∞} , (1) becomes a means for calculating e/m .

(b) *Ionization potentials.*—In 1919 Birge had available 13 values of ionization and resonance potentials. Many more such potentials have been obtained. The probable error in each is rather large. We have one really accurate determination obtained with electrons of carefully controlled velocity. This is Lawrence's value² of the ionization potential of Hg. His final value equals 10.40 ± 0.02 int. volts.

The equation for obtaining h is $h\nu = eV$; all quantities are in absolute units. The observed potential (V') is always in int. volts. The potential in abs. *es* units is then $V = pqV'10^8/c$. The spectral frequency ν (in sec^{-1}) is obtained always from the wave length λ , in cm. Hence $\nu'(\text{cm}^{-1}) = 1/\lambda$, and $\nu = c/\lambda$. The above equations lead to

$$h/e = (pqV'10^8)/(c^2\nu') = (pqV'\lambda10^8)/c^2 \quad (3)$$

It seems quite customary to assume that $V_{es} = V'$ volts/300 and to write this equation

$$h/e = V'\lambda/300c. \quad (4)$$

This is equivalent to assuming $c = 3 \times 10^{10} \text{ cm} \cdot \text{sec}^{-1}$, causing an error of 0.07 per cent. Scarcely anyone uses $c = 3 \times 10^{10} \text{ cm} \cdot \text{sec}^{-1}$ when reducing λ to ν , and thus in the same equation it is customary to use two different values of c . The "term" of Hg corresponding to the ordinary ionization potential is 84178.5 cm^{-1} , whence

$$h = (6.560 \pm 0.015) \times 10^{-27}.$$

The probable error in V' is 0.2 per cent and in e , 0.1 per cent. The errors of the other factors are negligibly small.

(c) *X-ray continuous spectrum.*—This method uses (3), λ being measured by means of a calcite crystal, i.e., $\lambda = 2d \sin \theta$ where d is the grating space, and θ the angle at which the given wave length shows constructive interference.

$$h/e = pq \ 2d (V' \sin \theta) 10^8 / c^2$$

Duane, Palmer, and Yeh³ have carried out an accurate investigation. The resulting value of h is $(6.556 \pm 0.009) \times 10^{-27}$. Another result for which equal accuracy is claimed, is by Wagner.⁴ Ladenburg⁵ gives a complete list of Wagner's experimental results. Ladenburg, using eq. (4), with $c = 2.9985 \times 10^{10}$, gets 6.529 ± 0.01 .

¹ H.P., 2, 510. ² Phys. Rev., 28, 947, 1926. ³ Proc. Nat. Acad. Sci., 7, 237, 1921. ⁴ Phys. Zeit., 21, 621, 1920. ⁵ H.P., 23, 296.

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Duane, Palmer, and Yeh used a known potential (int. volts) and measured the angle θ at which the ionization suddenly started (or stopped). This gives the critical ionization frequency corresponding to the given voltage. Wagner used known wave lengths varying the voltage for a given wave length, until ionization suddenly began (or ceased). Both methods involve the calcite grating space d . On page 91 the absolute wave lengths of rays were used to evaluate d' , the true grating space; d' was then used with other known constants to evaluate the electronic charge e . In this section we use the finally adopted value of e , $(4.770 \pm 0.005) \times 10^{-10}$ abs. *es* units, with these same constants, to evaluate d' .

$$d'_{20} = \{4.770 \times 10^{-10} / 1.7176 \times 10^{13}\} = (3.0283 \pm 0.0010) \times 10^{-8} \text{ cm}$$

This value of d'_{20} includes the result of the X-ray work, since the value of e just used is the weighted average from both oil-drop and X-ray work. We might have used $e = 4.768$ to get a value of d' based on oil-drop work. A second value of d' might then be obtained from absolute X-ray measurements. The weighted average of these two values would be the value given, provided we use the data and probable errors indicated on p. 91.

We obtain for the effective grating space of calcite at 20°C , for the first order spectrum,

$$d_{20} = (3.0279 \pm 0.0010) \times 10^{-8} \text{ cm.}$$

This value is to be substituted with the direct experimental value of $V' \sin \theta$. For the latter Duane, Palmer, and Yeh found 2039.9 ± 1 int. volts (mean temperature of about 20°C). Thus we have

$$h = (6.559 \pm 0.008) \times 10^{-27} \text{ erg} \cdot \text{sec.}$$

Similarly revising Wagner's result we obtain 6.532 ± 0.010 , in place of 6.526 ± 0.010 . It is difficult to judge what revision is required in the values of λ used by Wagner; the change is probably small. We thus have, as the two best values of h , from X-ray data, 6.559 ± 0.008 (or 0.009) and 6.532 ± 0.010 . The work of Wagner has not yet been published in sufficient detail. For this reason in adopting a weighted average only one-half as much weight is given to Wagner. Since the two results differ by much more than the probable error of either, the regular least squares probable error is used. Hence, from X-ray data,

$$h = (6.550 \pm 0.009) \times 10^{-27} \text{ erg} \cdot \text{sec.}$$

(d) *Photoelectric effect*.—The most accurate determination of h , from photoelectric work, is by Lukirsky and Prilezaev.¹ They use a somewhat different technique from that employed by Millikan,² and obtain a simple empirical relation for the ionization current as a function of voltage. The actual curve may be transposed into a linear graph, making the extrapolation to zero current more certain. They also carry the readings very close to this zero point.

¹ Zeit. Phys., 49, 236, 1928. ² Phys. Rev., 7, 355, 1916.

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The equation for evaluating h is that just used, except that now the energy (P) to pull an electron out of the metal is no longer negligible compared to $h\nu$. Hence we write

$$Ve = h\nu - P.$$

To eliminate P , light of varying frequencies is used, measuring for each the critical voltage V at which ionization starts. V is plotted against ν ; the resulting curves should be linear, with a slope

$$dV/d\nu = h/e.$$

With V measured as V' int. volts, and ν as ν' cm⁻¹, we have

$$dV'/d\nu = (pa10^8 dI'') / (c^2 d\nu') = h/e$$

Lukirsky and Prilezaev use the metals Al, Zn, Sn, Ni, Cd, Cu, and Pt. Six curves, three with Zn, two with Al, and one with Ni, were the best. Unfortunately these investigators give no detailed data, and no indication of the actual equation used. Their final value of h is 6.543×10^{-27} erg · sec., the individual results being 6.539, 6.542, 6.540, 6.556, 6.536, and 6.546. We take

$$h = (6.543 \pm 0.010) \times 10^{-27} \text{ erg} \cdot \text{sec.}$$

These investigators estimate their final error in h as 0.1 to 0.2 per cent.

(e) *Wien's displacement law; Planck equation.*— h may be had from radiation constants in two different ways. The first is by means of c_2 , in the Wien displacement law,

$$\lambda_{\max} T = c_2 / \beta = A.$$

where $\beta = 4.9651$ (root of $e^{-\beta} + \beta/5 - 1 = 0$). The radiation constant c_2 occurs also in Planck's black-body radiation law in the form

$$c_2 = hc/k.$$

c = velocity of light, k (Boltzmann constant) = R_0/N_0 , R_0 (gas constant per mole) = $\nu_n A_n / T_0$, and N_0 (Avogadro's number) = Fc/e . Substituting the values of ν_n , A_n , T_0 , F and e previously adopted,

$$N_0 = (6.0644 \pm 0.0061) \times 10^{23} \text{ mole}^{-1}.$$

$$R_0 = (8.3136 \pm 0.0010) \times 10^7 \text{ erg} \cdot \text{deg.}^{-1} \cdot \text{mole}^{-1}.$$

$$k = (1.3709 \pm 0.0014) \times 10^{-16} \text{ erg} \cdot \text{deg.}^{-1}.$$

In 1919 Doctor Birge asked Coblentz what in his opinion was then the best value of c_2 . He recommended 1.433 cm · deg.; this value was adopted. In a long critical review of the radiation constants, three years later, Coblentz¹ gives 1.432 as the most probable value. No probable error is given but the four results, obtained by four investigators, were 1.436, 1.430, 1.430 and 1.4318,

¹ Bur. Standards Bull., 17, 7, 1922.

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the last being Coblenz' own value. Ladenburg¹ gives 1.432 ± 0.006 . The separate results which he used are 1.425 to 1.441, 1.4295 ± 0.007 , 1.435, 1.4318, 1.430. The chief error arises from the various corrections applied to the observed values. Coblenz' original value² of 1.4456 has become 1.4318 in his latest article,³ Doctor Birge believes 0.003 is a much more reasonable estimate of error. Both Coblenz and Ladenburg agree on the absolute value. Hence he adopts

$$c_2 = 1.432 \pm 0.003 \text{ cm} \cdot \text{deg.}$$

$$h = (6.548 \pm 0.015) \times 10^{-27} \text{ erg} \cdot \text{sec.}$$

The radiation constant c_2 occurs in the Boltzmann factor $e^{-\epsilon/kT}$, (ϵ =energy, T =absolute temperature) in the form $e^{-c_2\nu/T} = e^{-c_2/\lambda T}$, where ν in cm^{-1} , or λ in cm , is the quantum equivalent of ϵ ergs.

(f) *The Stefan-Boltzmann law and the Planck equation.*—The second method for determining h by the radiation constants is through the Stefan-Boltzmann law, $E = \sigma T^4 = acT^4/4$. h is connected with σ , using Planck's law, by the relation

$$h = (2\pi^5 k^4 / 15c^2 \sigma)^{1/4}.$$

As in the case of c_2 , there is a difference of opinion concerning the accuracy with which σ may be measured. The best value, in 1919, was that obtained by Coblenz,³ namely $(5.722 \pm 0.012) \times 10^{-5} \text{ erg} \cdot \text{cm}^{-2} \cdot \text{deg.}^{-4} \cdot \text{sec.}^{-1}$. In his more recent discussion, Coblenz⁴ gives all available data, and concludes that the most probable value lies between 5.72 and 5.73.

Since this 1922 article by Coblenz, there have been two new determinations of σ , one by Hoffman⁵ (method of Westphal), giving $\sigma = 5.764 \pm 0.052$, and the other by Kussman,⁶ using the modified Ångström pyrhelioscope. This latter method was used also by Coblenz³ giving 5.722 as stated, by Gerlach⁷ giving 5.80, and by Kahanowicz⁸ giving 5.69 to 5.73 as corrected by Coblenz.⁴ Kussman obtained $\sigma = 5.795 \pm \text{one per cent}$. Ladenburg¹ quotes the four results by Gerlach, Hoffman, Coblenz, and Kussman. He adopts the *unweighted* mean. He agrees with Gerlach that Coblenz' true error is more nearly 0.06 than 0.012. The experimental results of Kussman⁶ and Coblenz³ are in almost perfect agreement. The discrepancy in their results is due to the correction for the lack of complete absorption of the receiver. Michel and Kussman⁹ claim to prove that the correction Coblenz applied is too small. The values of σ by Kussman and by Hoffman, as well as Gerlach's earlier value of 5.80, correspond to impossibly low values of h . Coblenz' result gives an h in good agreement with that obtained by more accurate methods. This tends to indicate the correctness of Coblenz' correction for incomplete absorption, as opposed to Kussman's.

¹ H.P., 23, 303. ² Bur. Standards Bull., 10, 1, 1914. ³ Proc. Nat. Acad. Sci., 3, 504, 1917. ⁴ Bur. Standards Bull., 17, 7, 1912. ⁵ Zeit. Phys., 14, 301, 1923. ⁶ Ibid., 25, 58, 1924. ⁷ Ann. Phys., 50, 259, 1916; Zeit. Phys., 2, 76, 1920. ⁸ Nuovo Cimento, 13, 142, 1917. ⁹ Zeit. Phys., 18, 263, 1923.

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It appears that Coblentz' estimated error for his own work (5.722 ± 0.012) is too small, but that his final average of the work of all investigators up to 1922 (5.72 to 5.73) should be more trustworthy than any single value. We will choose 5.725 and 0.02 for its probable error. This result is then to be averaged with the more recent work whence

$$\sigma = (5.735 \pm 0.011) \times 10^{-5} \text{ erg} \cdot \text{cm}^{-2} \cdot \text{deg.}^{-4} \cdot \text{sec.}^{-1}$$

and

$$a = 4\sigma/c = (7.652 \pm 0.015) \times 10^{-15} \text{ erg} \cdot \text{cm}^{-3} \cdot \text{deg.}^{-4}$$

There has appeared a further determination of this quantity, by Hoare.¹ He used a Callendar radio balance; the advantage of the method is that both source and receiver are essentially "black-bodies." Hoare obtains $\sigma = 5.735$, agreeing exactly with the value adopted. He lists 38 separate results, average deviation only 0.016. The inclusion of this new result leaves the average value unchanged, and Doctor Birge leaves the probable error unchanged. Objection might be made to this adopted error as too small; such an objection can hardly hold in the face of Hoare's work. This new work also speaks against Strum's assumption of an inadequacy of Planck's formula. We have then

$$h = (6.539 \pm 0.010) \times 10^{-27} \text{ erg} \cdot \text{sec.}$$

(g) *Summary*.—We have now six determinations of h :

| | | |
|-----------------------|-----------------------|------------------------------|
| Rydberg constant | $h = 6.547 \pm 0.011$ | Power of c involved, $5/3$ |
| Ionization potentials | 6.560 ± 0.015 | $3/3$ |
| X rays | 6.550 ± 0.009 | $4/3$ |
| Photoelectric | 6.543 ± 0.010 | $3/3$ |
| c_2 | 6.548 ± 0.015 | $3/3$ |
| σ | 6.539 ± 0.010 | $4/3$ |

Doctor Birge adopts

$$h = (6.547 \pm 0.008) \times 10^{-27} \text{ erg} \cdot \text{sec.}$$

This value of h is identical with Ladenburg's most recent estimate.² This identity is spurious, since Ladenburg assumes $c = 4.774 \times 10^{-10}$. If this older value of c had been used in the present work, we should have obtained $h = 6.5535$, in practically exact agreement with Doctor Birge's 1919 value (6.5543).

Another potentially accurate method is given by the Compton shift of X-ray lines. The theoretical equation for this is $\Delta\lambda = (h/mc)(1 - \cos \phi)$, where m is the mass of an electron, as deduced from the values of e and e/m . Since h varies in value with e , this equation can better be used to evaluate e/m . We can in fact write $\Delta\lambda = (h/e)(e/m)(1 - \cos \phi)$ in which e as usual is in es units, and e/m in em units. Then

$$e/m = (\Delta\lambda)/(h/e)(1 - \cos \phi)$$

The most accurate work on this subject has been done by Sharp,³ who obtains $\Delta\lambda = (0.04825 \pm 0.00017) \times 10^{-8} \text{ cm}$, for $(1 - \cos \phi) = (1.984 \pm 0.001)$. With the adopted values of h and e , we have $h/e = (1.3725 \pm 0.0005) \times 10^{-17}$

¹ Philos. Mag., 6, 828, 1928. ² H.P., 23, 279. ³ Phys. Rev., 26, 691, 1925.

PROBABLE VALUES OF THE GENERAL PHYSICAL CONSTANTS

$\text{erg} \cdot \text{sec} \cdot \text{es}^{-1}$. Substituting, one finds $e/m = (1.772 \pm 0.006) \times 10^7$ abs. em units, the final error being due almost entirely to the error in $\Delta\lambda$. It seems possibly significant that this value agrees better with the deflection than with the spectroscopic value of e/m , for the theory used in the derivation of the equation is essentially the collision theory of classical dynamics for free electrons.

e , e/m , and h appear in many important constants. h depends for its value on e , therefore the e appears implicitly, if not explicitly, in every quantum relation. The outstanding discrepancy was between the work of Wagner and of Duane and co-workers, on the value of h from the X-ray continuous spectrum. The recent work of Feder, using this method, gives h in exact agreement with the value adopted, and explains Wagner's low value. Doctor Birge now feels that the value of h/e listed in Table 43 can be assumed with some confidence. The real problem concerns the values of e and of e/m .

The need of two values of e/m is very annoying, and fundamentally unsatisfactory. The same situation seems to be arising in regard to e . Millikan's value has been accepted; it was the only one available. The new work on X rays opened another possibility. The value of Bäcklin is one-half per cent higher than Doctor Birge's adopted value. As a final result Doctor Bearden obtains for the absolute wave length of the (unresolved) Cu $K\alpha$ line, $1.5439 \pm 0.0002\text{\AA}$, and for the Cu $K\beta$ line, $1.3940 \pm 0.0002\text{\AA}$. These results are obtained under many varied conditions. The first is 0.345 per cent higher than Siegbahn's value, the second 0.336 per cent. The *relative* wave lengths are in agreement with Siegbahn, but the *absolute* wave lengths lead to a value for calcite of $d'_{20} = 3.0398\text{\AA}$, and $e = 4.825 \times 10^{-10}$ abs. es units, 1.15 per cent above Doctor Birge's adopted value of e . It is desirable to consider the various relations that have been suggested between these constants. The most famous connects e , e/m , h , and c in Bohr's formula for the Rydberg constant. This was used to evaluate h , and the value (6.54713) is identical to four digits with that adopted. Hence, the indirectly calculated value of e/m is also practically identical with that adopted. Thus the *adopted* values of e , e/m , h and c form a self-consistent system, as judged by the Bohr formula for R_∞ .

Lewis and Adams² (theory of ultimate rational units), have obtained, with the aid of Planck's radiation law, the relation: $hc/2\pi e^2 = 8\pi(8\pi^5/15)^{1/3}$. The right side equals 137.348; the left side, with the constants here adopted, equals 137.294 ± 0.11 . The left side equals the reciprocal of the fine structure constant α , and the value quoted is taken directly from Table 43. The numerical agreement is very striking. The present agreement shows that this method yields a value of h almost identical with that adopted.

α is a dimensionless constant involving fundamental general constants; it should be remembered that to make α dimensionless, we must include with the factor hc the unknown dimensions of specific inductive capacity.

¹ Note added by Birge April, 1929 (abbreviated). ² Phys. Rev., 3, 92, 1914.

PROBABLE VALUES OF THE GENERAL PHYSICAL CONSTANTS

Perles¹ has pointed out that the ratio of the mass of the proton to that of the electron (M_p/m_0) is another dimensionless constant which should have some significance, and has found that

$$(hc/e^2)(=2\pi/a) = (M_p/m_0)(\pi - 1)$$

the left side equals 862.64 ± 0.68 , the right 858.36 ± 0.49 or 862.26 ± 0.99 depending on whether one uses the spectroscopic or the deflection value of e/m . The agreement is good for the deflection value but poor for the spectroscopic.

Note.—In evaluating the constants, it has been necessary to calculate auxiliary constants, and also to use certain conventional quantities, such as g_{45} and g_n . All such quantities are listed in Table 42.

In addition to constants listed in Table 42 there are many other functions of constants given on page 103 of this table and in Table 42. A number of these derived constants are collected in Table 43. An attempt has been made to include the more important or more frequently used values. The process for obtaining the correct probable error for many of the constants of Tables 42 and 43 is sometimes involved. The various *derived* constants of Table 43 (and the occasional derived constant appearing on page 103 of this table and in Table 41) are given with one and often two more digits than required by the probable error. Such digits are printed below the line, and have been added that calculations made in different ways shall not introduce any appreciable error.

e/m always indicates merely the *ratio* of charge to mass for an electron, in em units; e indicates electronic charge in es units; m_0 , electronic mass; m , the atomic weight of an electron. A more logical but less convenient nomenclature would have been (e/m_0) es units, and possibly (e'/m_0) cm units.

In the quantum relation, $\epsilon = h\nu = eV$, each side represents energy in ergs, provided all quantities are in abs. c.g.s. units. $\nu/V' (= e/h)$ then measures the frequency in sec^{-1} associated with one abs. es unit of potential. It is usually convenient to substitute the wave number (ν') or the wave length (λ) in place of ν , and to substitute the number of abs. volts (V'') in place of V . ($V' = \text{int. volts}$, throughout this paper). The values of the various ratios, such as ν'/V'' etc., are given in Table 43.

An electron which has fallen through one abs. volt of potential is termed an abs. volt-electron; its energy in ergs and speed in $\text{cm} \cdot \text{sec}^{-1}$ are given in Table 43. Corresponding to any *ionization potential* of an atom or molecule in volts (V''), there is an *energy of ionization* (eV'') which can be measured in units equal to the energy of a volt-electron, and is so designated. An ionization potential of 10 volts corresponds to an energy of ionization of 10 volt-electrons. Similarly, in the case of molecules, we speak of a *dissociation potential* of, let us say, 10 volts, and a corresponding energy of dissociation (heat of dissociation) of 10 volt-electrons per molecule. The factor by which this last quantity must be multiplied to give the heat of dissociation in calories per mole is given in Table 43. Unfortunately there has arisen the practise, to which Doctor Birge pleads guilty, of designating the *heat* of dissociation as 10 volts, instead of stating, more correctly, that the equivalent dissociation *potential* is 10 volts, or that the heat of dissociation per molecule is 10 volt-electrons.

The name of the units conforms as far as possible with current practise. Difficulties arise with the unknown dimensions of magnetic permeability μ , and specific inductive capacity ϵ . It is customary to indicate these unknown dimensions by the symbols μ and ϵ . A given unit, such as the gauss, is applied only to quantities of a given set of dimensions, including μ and ϵ . In the present discussion we are concerned only with numerical magnitudes and no particular attention has accordingly been paid to this matter of dimensions.

¹ Naturwiss., 16, 1094, 1928.

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Thus the statement that the absolute cm unit of resistance is one $cm \cdot sec^{-1}$ involves the assumption not only of unit permeability, but also of dimensionless permeability. In a number of the equations given in Table 43 the two sides of the equation do *not* check dimensionally unless one assumes μ and e to be dimensionless. It follows from this that the name of the unit stated in the table applies strictly only to one side of such an equation. In such cases the unit applies to the left side of the equation, since this is the quantity being evaluated. The right side gives merely the most direct derivation of the numerical magnitude, in terms of quantities already evaluated. Since this ambiguity does not affect the numerical magnitude, it is inconsequential in the present discussion. As examples of this situation we cite the fine structure constant α , which is dimensionless. To satisfy this condition one should write $\alpha = 2\pi e^2 / \epsilon_0 h c$ where ϵ_0 is numerically unity, and represents merely the dimensions of ϵ . The ratio of the Bohr magneton μ_B to the Bohr unit of angular momentum ($h/2\pi$) is strictly $\mu_0^{1/2}(e/m)$, where μ_0 is numerically unity, and represents merely the dimensions of permeability.

The mole is a (variable) unit of mass, equal to the molecular weight in grams. The gram equivalent is a similar (variable) unit of mass, equal to the atomic or molecular weight in grams, divided by the valence.

The various quantities appearing on page 103 of this table and in Table 42 have been discussed. No general explanation will be given of the meaning or use of the quantities appearing in Table 43; any adequate explanation would constitute a textbook of modern physics and physical chemistry. For the more specialized constants, no explanation is needed by investigators working with such constants, and it is to such persons that the data will be most useful.

In conclusion, attention should be directed merely to two constants for which the formula used here differs from that normally given. It is customary to use for the speed of the electron in the normal orbit of hydrogen, as given by Bohr's original theory, a value which refers to the nucleus considered as the center of coordinates. This is called $v_0 (= \alpha c)$ in Table 43. It would seem more logical to give the speed referred to the center of mass, the quantity denoted v_0' in Table 43. There is a similar discrepancy in the case of the radius of this orbit. The electron, according to Bohr, moves about the center of mass in a circle of radius a_0' , as it is denoted in Table 43. This is not the same as the constant separation of the nucleus and electron, which is here denoted a_0 . In the literature these two quantities, a_0 and a_0' , are sometimes confused. The expressions for v_0 , v_0' , a_0 , and a_0' given in Table 43 include also the factor $(1 - \alpha^2)^{1/2}$, arising from the variation of mass with speed.

Birge. Probable values of e , h , e/m and α Phys. Rev. 40, 228, 1932.

$$\begin{aligned} e, & (4.7688 \pm 0.0040) \times 10^{-10} \text{ es units} \\ h, & (6.5443 \pm 0.0091) \times 10^{-27} \text{ erg} \cdot \text{sec.} \\ e/m, & (1.7611 \pm 0.0009) \times 10^7 \text{ cm units} \cdot \text{g}^{-1} \\ 1/\alpha, & 137.307 \pm 0.048 \end{aligned}$$

Fundamental constants, Birge.—The critical discussion of the determination by Dr. R. T. Birge of these values will be found in abbreviated form on pages 73 to 102 of this book; for full details see Phys. Rev. Suppl., 1, 1, 1929. These constants, for purposes of computation, are to be taken as exactly correct; that is, all additional digits in each constant are to be assumed as zero. The real probable error of each value is of course that indicated in the table, and each constant has an accepted value carried only to the number of significant figures required by the adopted probable error.

| | |
|---|---|
| Velocity of light..... | $c = (2.99796 \pm 0.00004) \times 10^{10} \text{ cm} \cdot \text{sec}^{-1}$ |
| Gravitation constant..... | $G = (6.664 \pm 0.002) \times 10^{-8} \text{ dyne} \cdot \text{cm}^2 \cdot \text{g}^{-2}$ |
| Liter..... | $l = 1000.027 \pm 0.001 \text{ cm}^3$ |
| Volume of perfect gas (0°C, A_n)... v_n | $= (22.4141 \pm 0.0008) \times 10^3 \text{ cm}^3 \cdot \text{mole}^{-1}$ |
| Volume of perfect gas (0°C, A_{45})... R | $= 22.4146 \pm 0.0008 \text{ liter} \cdot \text{mole}^{-1}$ |
| International ohm = p abs. ohm.... p | $= 1.00051 \pm 0.00002$ |
| International ampere = q abs. amp.... q | $= 0.99995 \pm 0.00005$ |
| Normal atmosphere..... A_n | $= (1.013249 \pm 0.000003) \times 10^8 \text{ dyne} \cdot \text{cm}^{-2}$ |
| 45° atmosphere..... A_{45} | $= (1.013199 \pm 0.000003) \times 10^8 \text{ dyne} \cdot \text{cm}^{-2}$ |
| Ice point (absolute scale)..... T_0 | $= 273.18 \pm 0.03^\circ \text{K}$. |
| Mechanical equivalent of heat.... J_{15} | $= 4.1852 \pm 0.0006 \text{ abs. joule} \cdot \text{cal}_{15}^{-1}$ |
| Electrical equivalent of heat.... J_{15} | $= 4.1835 \pm 0.0007 \text{ int. joule} \cdot \text{cal}_{15}^{-1}$ |
| Faraday constant..... F | $= 96494 \pm 5 \text{ int. coul.} \cdot \text{g-equiv.}^{-1}$ $= 96489 \pm 7 \text{ abs. coul.} \cdot \text{g-equiv.}^{-1}$ $= 9648.9 \pm 0.7 \text{ abs. cm-unit} \cdot \text{g-equiv.}^{-1}$ $Fc = (2.8927_0 \pm 0.0002) \times 10^{11} \text{ abs. es-unit} \cdot \text{g-equiv.}^{-1}$ |
| Electronic charge *..... e | $= (4.770 \pm 0.005) \times 10^{-10} \text{ abs. es-units}$ $e/c = (1.5910_8 \pm 0.0016) \times 10^{-20} \text{ abs. cm-units}$ |
| Specific electronic charge (spectroscopic)..... e/m | $= (1.761 \pm 0.001) \times 10^7 \text{ abs. cm-unit} \cdot \text{g}^{-1}$ $(e/m)c = (5.279_{11} \pm 0.003) \times 10^{17} \text{ abs. es-unit} \cdot \text{g}^{-1}$ |
| Specific electronic charge (deflection)..... e/m | $= (1.769 \pm 0.002) \times 10^7 \text{ abs. cm-unit} \cdot \text{g}^{-1}$ $(e/m)c = (5.303_{30} \pm 0.006) \times 10^{17} \text{ abs. es-unit} \cdot \text{g}^{-1}$ |
| Planck constant *..... h | $= (6.547 \pm 0.008) \times 10^{-27} \text{ erg} \cdot \text{sec}$. |
| Atomic weights | |
| O = 16.0000 | C = 12.003 ± 0.001 I = 126.932 ± 0.002 |
| He = 4.0022 ± 0.0004 | H = 1.00777 ± 0.00002 Ca = 40.075 ± 0.005 |
| Ag = 107.880 ± 0.001 | N = 14.0083 ± 0.0008 |

TABLE 41.—Powers of c , h , e , h/c

| | | | |
|--------------|--|--|---|
| c^{-2} ; | $(1.11262 \pm 0.00003) 10^{-21} \text{ cm}^{-2} \cdot \text{sec}^{-2}$ | h^{-3} ; | $(3.563_{17} \pm 0.012) 10^{78} \text{ erg}^{-3} \cdot \text{sec}^{-3}$ |
| c^{-1} ; | $(3.33560 \pm .00005) 10^{-11} \text{ cm}^{-1} \cdot \text{sec}^{-1}$ | h^{-2} ; | $(2.333_{00} \pm .005) 10^{52} \text{ erg}^{-2} \cdot \text{sec}^{-2}$ |
| $c^{-1/2}$; | $(5.77546 \pm .00006) 10^{-6} \text{ cm}^{-1/2} \cdot \text{sec}^{-1/2}$ | h^2 ; | $(4.286_{32} \pm .010) 10^{-54} \text{ erg}^2 \cdot \text{sec}^{-2}$ |
| $c^{1/2}$; | $(1.73146 \pm .00001) 10^5 \text{ cm}^{1/2} \cdot \text{sec}^{-1/2}$ | h^3 ; | $(2.806_{25} \pm .010) 10^{-79} \text{ erg}^3 \cdot \text{sec}^{-3}$ |
| c^2 ; | $(8.98782 \pm .00024) 10^{20} \text{ cm}^2 \cdot \text{sec}^{-2}$ | e^{-2} ; | $(4.395_{04} \pm .000) 10^{18} \text{ es-units}^{-2}$ |
| c^3 ; | $(2.69449 \pm .00011) 10^{31} \text{ cm}^3 \cdot \text{sec}^{-3}$ | $(2.275_{21} \pm .0045) 10^{-19} \text{ es-units}^2$ | |
| c^4 ; | $(8.07798 \pm .00043) 10^{41} \text{ cm}^4 \cdot \text{sec}^{-4}$ | e^3 ; | $(1.085_{31} \pm .0033) 10^{-28} \text{ es-units}^3$ |
| h/c ; | $(2.183_{11} \pm .003) 10^{-27} \text{ g} \cdot \text{cm}$ | e^4 ; | $(5.176_{91} \pm .021) 10^{-38} \text{ es-units}^4$ |
| | | e^5 ; | $(2.469_{10} \pm .012) 10^{-47} \text{ es-units}^5$ |

* Millikan, Phys. Rev., 35, 1930, takes $e = 4.774 \times 10^{-10}$, $h = 6.547 \times 10^{-27}$, $N = 6.062 \times 10^{23}$.

ADDITIONAL PHYSICAL CONSTANTS

Used or evaluated by Doctor Birge in Phys. Rev. Suppl., 1, 1, 1929, in connection with Table 40, p. 103.

Ratio of *es* to *cm* units (direct)..... $c' = (2.9979 \pm 0.0001) \times 10^{10} \text{ cm} \cdot \text{sec}^{-1}$

Acceleration of gravity (45°)..... $g_{45} = 980.616 \text{ cm} \cdot \text{sec}^{-2}$

Acceleration of gravity (normal).... $g_n = 980.665 \text{ cm} \cdot \text{sec}^{-2}$

Mean density of the earth..... $\delta = 5.522 \pm 0.002 \text{ g} \cdot \text{cm}^{-2}$

Maximum density of water... $\delta_m(\text{H}_2\text{O}) = 0.999973 \pm 0.000001 \text{ g} \cdot \text{cm}^{-3}$

Density of oxygen gas (0°C , A_{45})

$$L(\text{O}_2) = 1.428965 \pm 0.000030 \text{ g} \cdot \text{liter}^{-1}$$

Factor converting oxygen (0°C , A_{45}) to

ideal gas $1 - \alpha(\text{O}_2) = 1.000927 \pm 0.000030$

Density of nitrogen (0°C , A_{45})... $L(\text{N}_2) = 1.25046 \pm 0.000045 \text{ g} \cdot \text{liter}^{-1}$

Factor converting nitrogen (0°C , A_{45})

to ideal gas..... $1 - \alpha(\text{N}_2) = 1.00043 \pm 0.00002$

Density of Hg (0°C , A_n)..... $D_n = 13.59509 \pm 0.00003 \text{ g} \cdot \text{cm}^{-3}$

International volt (= pq abs. volts).. $pq = 1.00046 \pm 0.00005$

International joule (= pq^2 abs. joules)

$$pq^2 = 1.00041 \pm 0.00010$$

Electrochemical equivalent of Ag

$$E(\text{Ag}) = (1.11800 \pm 0.00005) \times 10^{-3} \text{ g} \cdot \text{int. coul.}^{-1}$$

$$= (1.11805 \pm 0.00007) \times 10^{-3} \text{ g} \cdot \text{abs. coul.}^{-1}$$

Density of calcite (20°C)..... $\rho = 2.7102 \pm 0.0004 \text{ g} \cdot \text{cm}^{-3}$

Structural constant of calcite (20°C)

$$\phi(\beta) = 1.09630 \pm 0.00007$$

True grating space of calcite (20°C)

$$d'_{20} = (3.0283 \pm 0.0010) \times 10^{-8} \text{ cm}$$

Effective grating space of calcite

$$(20^\circ\text{C}) \dots\dots\dots d_{20} = (3.0279 \pm 0.0010) \times 10^{-8} \text{ cm}$$

Rydberg constant for hydrogen..... $R_H = 109677.759 \pm 0.05 \text{ cm}^{-1}$

Rydberg constant for ionized helium

$$R_{He} = 109722.403 \pm 0.05 \text{ cm}^{-1}$$

Wave length of red Cd line (15°C , A_n)

$$\lambda_{Cd} = 6438.4696 \text{ I.A. (definition of I.A. unit)}$$

Rydberg constant for infinite mass.. $R_\infty = 109737.42 \pm 0.06 \text{ cm}^{-1}$

$$cR_\infty = (3.28988 \pm 0.00004) \times 10^{15} \text{ sec}^{-1}$$

Avogadro's number $N_0 = F/c = (6.064_{36} \pm 0.006) \times 10^{23} \text{ mole}^{-1}$

Gas constant per mole... $R_0 = \nu_n A_n / T_0 = (8.3136_0 \pm 0.0010) \times 10^7 \text{ erg} \cdot \text{degree}^{-1} \cdot \text{mole}^{-1}$

$$R'_0 = R_0 / (J_{15} \times 10^7) = 1.9864_3 \pm 0.0004 \text{ cal}_{15} \cdot \text{deg}^{-1} \cdot \text{mole}^{-1}$$

Boltzmann constant $k = R_0 / N_0 = (1.3708_0 \pm 0.0014) \times 10^{-16} \text{ erg} \cdot \text{deg}^{-1}$

Second radiation constant (exp. value)

$$c_2 = 1.432 \pm 0.003 \text{ cm} \cdot \text{deg.}$$

Second radiation constant (indirect)

$$c_2 = hc/k = 1.4317_4 \pm 0.0006 \text{ cm} \cdot \text{deg.}$$

Radiation density constant.... $a = 4\sigma/c = (7.651_8 \pm 0.015) \times 10^{-15} \text{ erg} \cdot \text{cm}^{-3} \cdot \text{deg.}^{-4}$

Stefan-Boltzmann constant (exp. value)

$$\sigma = (5.735 \pm 0.011) \times 10^{-5} \text{ erg} \cdot \text{cm}^{-2} \cdot \text{deg.}^{-4} \cdot \text{sec.}^{-1}$$

Stefan-Boltzmann constant (indirect)

$$\sigma = 2\pi^5 k^4 / 15c^2 h^3 = (5.713_9 \pm 0.006) \times 10^{-5} \text{ erg} \cdot \text{cm}^{-2} \cdot \text{deg.}^{-4} \cdot \text{sec.}^{-1}$$

MISCELLANEOUS DERIVED PHYSICAL CONSTANTS

Evaluated by Doctor Birge in Phys. Rev. Suppl., 1, 1, 1929.

(See notes on page 99.)

Mass of electron (spectroscopic)

$$m_0 = e / \left\{ c (e/m)_{sp} \right\} = (9.035_{50} \pm 0.010) \times 10^{-28} \text{ g}$$

Mass of electron (deflection)

$$m_0 = e / \left\{ c (e/m)_{defl} \right\} = (8.994_{25} \pm 0.014) \times 10^{-28} \text{ g}$$

Atomic weight of electron (spectroscopic)

$$m = F / (e/m)_{sp} = (5.479_{22} \pm 0.003) \times 10^{-4}$$

Atomic weight of electron (deflection)

$$m = F / (e/m)_{defl} = (5.454_{44} \pm 0.006) \times 10^{-4}$$

Mass of atom of unit atomic weight

$$M_0 = 1/N_0 = (1.6489_{90} \pm 0.0016) \times 10^{-24} \text{ g}$$

Mass of hydrogen atom..... $M_H = H/N_0 = (1.6617_{90} \pm 0.0017) \times 10^{-24} \text{ g}$

Number of atoms per gram of hydrogen

$$1/M_H = (6.017_{61} \pm 0.006) \times 10^{23} \text{ g}^{-1}$$

Mass of proton..... $M_P = (H - m)/N_0 = (1.6608_{90} \pm 0.0017) \times 10^{-24} \text{ g}$ Mass of α particle.... $M_\alpha = (Hc - 2m)/N_0 = (6.597_{71} \pm 0.007) \times 10^{-24} \text{ g}$

Charge (electrolysis) of 1 g hydrogen

$$e/M_H = F/H = (9574.5_{10} \pm 0.7) \text{ abs. cm-units} \cdot \text{g}^{-1}$$

Specific charge of proton

$$e/M_P = F/(H - m) = (9579.7_{30} \pm 0.7) \text{ abs. cm-units} \cdot \text{g}^{-1}$$

Specific charge of α particle

$$2e/M_\alpha = 2F/(Hc - 2m) = (4823.1_{10} \pm 0.6) \text{ abs. cm-units} \cdot \text{g}^{-1}$$

Ratio, mass H atom to mass electron (spec-

troscopic) $(e/m)_{sp}/(e/M_H) = 1839.26 \pm 1$

Ratio, mass H atom to mass electron (deflec-

tion) $(e/m)_{defl}/(e/M_H) = 1847.6_{10} \pm 2$

Ratio, mass proton to mass electron (spec-

troscopic) $M_P/m_{sp} = 1839.26 - 1 = 1838.26 \pm 1$

Ratio, mass proton to mass electron (deflec-

tion) $M_P/m_{defl} = 1847.6_{10} - 1 = 1846.6_{10} \pm 2$

Energy associated with unit wave number

$$\epsilon/\nu' = hc = (1.9627_{64} \pm 0.0025) \times 10^{-16} \text{ erg} \cdot \text{cm}$$

Potential ($e\mathcal{S}$) associated with unit frequency

$$V/\nu = h/e = (1.3725_{10} \pm 0.0005) \times 10^{-17} \text{ eS-units} \cdot \text{sec.}$$

Frequency associated with 1 abs. volt

$$\nu/I'' = 10^8 e/hc = (2.4302_{50} \pm 0.0009) \times 10^{14} \text{ sec.}^{-1} \cdot \text{abs. volt}^{-1}$$

Wave number associated with 1 abs. volt

$$\nu_0 = \nu'/I'' = 10^8 e/hc^2 = (8106.3_{10} \pm 3) \text{ cm}^{-1} \cdot \text{abs. volt}^{-1}$$

Wave length associated with 1 abs. volt

$$\lambda_0 = \lambda V'' = hc^2/e = (12336.1 \pm 5) \times 10^{-5} \text{ cm} \cdot \text{abs. volt}$$

MISCELLANEOUS DERIVED PHYSICAL CONSTANTS

Energy of one-abs.-volt-electron

$$h\nu/I'' = 10^5 c/c = (1.5910_8 \pm 0.0016) \times 10^{-12} \text{ ergs}$$

Speed of abs.-volt-electron (spectroscopic)

$$v_c = [2 \times 10^8 (e/m)_{sp}]^{1/2} = (5.9346_4 \pm 0.0017) \times 10^7 \text{ cm} \cdot \text{sec}^{-1}$$

Speed of abs.-volt-electron (deflection)

$$v_e = [2 \times 10^8 (e/m)_{defl}]^{1/2} = (5.9481_1 \pm 0.0034) \times 10^7 \text{ cm} \cdot \text{sec}^{-1}$$

Fine structure constant..... $\alpha = 2\pi e^2/hc = 7.283_64 \pm 0.006) \times 10^{-3}$ Reciprocal of fine structure constant..... $1/\alpha = 137.29_4 \pm 0.11$

Magnetic moment, Bohr magneton (spectro-

scopic)..... $\mu_1 = \{h(e/m)_{sp}\}/4\pi = (0.9174_{70} \pm 0.0013) \times 10^{-20} \text{ erg} \cdot \text{gauss}^{-1}$

Magnetic moment, Bohr magneton (deflection)

$$\mu_1 = \{h(e/m)_{defl}\}/4\pi = (0.9216_{38} \pm 0.0016) \times 10^{-20} \text{ erg} \cdot \text{gauss}^{-1}$$

Magnetic moment per mole (1 Bohr magneton

per molecule) (spectroscopic)..... $\mu_1 N_0 = 5563_{.87} \pm 10 \text{ erg} \cdot \text{gauss}^{-1} \cdot \text{mole}^{-1}$

Magnetic moment per mole (1 Bohr magneton

per molecule) (deflection)..... $\mu_1 N_0 = 5589_{.14} \pm 11 \text{ erg} \cdot \text{gauss}^{-1} \cdot \text{mole}^{-1}$

Zeeman displacement per gauss

$$\Delta\nu'/H = (e/m)_{sp}/4\pi c = (4.674_{38} \pm 0.003) \times 10^{-5} \text{ cm}^{-1} \cdot \text{gauss}^{-1}$$

Band spectrum constant connecting wave-number

$$(\text{cm}^{-1}) \text{ and moment of inertia} \dots h/8\pi^2 c = (27.65_{83} \pm 0.04) \times 10^{-40} \text{ g} \cdot \text{cm}$$

Atomic specific heat constant..... $c_2/c = h/k = (4.7757_3 \pm 0.0019) \times 10^{-11} \text{ sec} \cdot \text{deg}.$ Reduced mass of H atom..... $\mu_H = R_H(m_0)_{sp}/R_\infty = 9.030_{18} \pm 0.010) \times 10^{-28} \text{ g}$ Schroedinger constant for H atom..... $8\pi^2\mu_H/h^2 = (1.663_{12} \pm 0.003) \times 10^{27} \text{ g} \cdot \text{erg}^{-2} \cdot \text{sec}^{-2}$

Schroedinger constant for electron

$$8\pi^2(m_0)_{sp}/h^2 = (1.664_{32} \pm 0.003) \times 10^{27} \text{ g} \cdot \text{erg}^{-2} \cdot \text{sec}^{-2}$$

Ionization potential for H atom..... $R_H/\nu_0 = 13.529_6 \pm 0.005 \text{ abs. volt}$ Ionization potential for He⁺..... $4R_{He}/\nu_0 = 54.141_7 \pm 0.020 \text{ abs. volt}$

Radius of Bohr orbit in normal hydrogen, re-

ferred to center of mass, using experimental

$$\text{value of } R_\infty \dots a_0' = a(1 - \alpha^2)^{1/2}/4\pi R_\infty = (0.5281_{68} \pm 0.0004) \times 10^{-8} \text{ cm}$$

Speed of electron in normal H orbit, referred to

$$\text{center of mass} \dots v_0 = \alpha c R_H/R_\infty = (2.1824_2 \pm 0.0017) \times 10^8 \text{ cm} \cdot \text{sec}^{-1}$$

MISCELLANEOUS DERIVED PHYSICAL CONSTANTS

Hydrogen doublet constant

$$\Delta\nu_H = R_H\alpha^2/16 = 0.3636_{30} \pm 0.0006 \text{ cm}^{-1}$$

Compton shift at 90° (spectroscopic)

$$h/m_0c = (c/m)_{sph}/c = (0.024170_4 \pm 0.000016) \times 10^{-8} \text{ cm}$$

Compton shift at 90° (deflection)

$$h/m_0c = (c/m)_{def}/h/c = (0.02428_{02} \pm 0.00003) \times 10^{-8} \text{ cm}$$

Wave length of 1-abs.-volt-electron

$$h/[m_0(v_c)_{sp}] = (12.210_0 \pm 0.006) \times 10^{-8} \text{ cm}$$

Loschmidt number $n_0 = N_0/v_n = (2.705_{60} \pm 0.003) \times 10^{19} \text{ cm}^{-3} (0^\circ\text{C}, A_n)$

Wien's displacement constant (indirect)

$$A = c_2/4.9651 = 0.28836_1 \pm 0.00011 \text{ cm} \cdot \text{deg.}$$

First radiation constant *..... $c_1 = 8\pi hc = (4.932_{06} \pm 0.006) \times 10^{-15} \text{ erg} \cdot \text{cm}$

$$\text{or } hc^2 = (0.5884_{28} \pm 0.0008) \times 10^{-5} \text{ erg} \cdot \text{cm}^2 \cdot \text{sec.}^{-1}$$

$$\text{or } 2\pi hc^2 = (3.697_{20} \pm 0.005) \times 10^{-5} \text{ erg} \cdot \text{cm}^2 \cdot \text{sec.}^{-1}$$

Energy per mole, equivalent to 1-abs.

-volt-electron per molecule

$$F(\text{abs. coul.} \cdot \text{g-equiv.}^{-1})/$$

$$J_{15}(\text{abs. joule} \cdot \text{cal.}_{15}^{-1}) = 23054.8 \pm 4 \text{ cal.}_{15} \cdot \text{mole}^{-1}$$

Sackur-Tetrode constant ($\epsilon = \text{base of}$

log. = 2.71828)

$$S_0 = R_0' \ln [(2\pi k)^3/3 \epsilon^{5/2}/h^3 N_0^{5/2}] = -11.6533 \pm 0.0026 \text{ cal.}_{15} \cdot \text{deg.}^{-1} \cdot \text{mole}^{-1}$$

Chemical constant (unit at. wt., pressure

in atm.)

$$i_0' = \frac{3}{2} \log [2\pi k^5/3/N_0 h^2] - \log A_n = -1.5882_5 \pm 0.0004$$

Multiplier of (Curie constant) $^{1/2}$ to give

magnetic moment in Bohr magnetons

$$\text{per molecule} \dots\dots\dots (3k/N_0)^{1/2}/\mu_1 = 2.8384_5 \pm 0.0019 \text{ erg}^{-1/2} \cdot \text{gauss} \cdot \text{deg.}^{-1/2} \cdot \text{mole}^{1/2}$$

* $E_\lambda = c_1 \lambda^{-5} (e^{-c_2/\lambda T} - 1)^{-1}$; E_λ may be defined in various ways, and c_1 varies accordingly. If $E_\lambda d\lambda$ denotes the energy density of unpolarized radiation in range $d\lambda$, $c_1 = 8\pi hc$. If $E_\lambda d\lambda$ denotes the intensity of emission of linearly polarized radiation in range $d\lambda$, perpendicular to a surface, per unit of surface, per unit solid angle, $c_1 = hc^2$. If $E_\lambda d\lambda$ denotes the emission of unpolarized radiation in range $d\lambda$, per unit surface, in all directions (2π solid angle), $c_1 = 2\pi hc^2$.

VOLUME OF A GLASS VESSEL FROM THE WEIGHT OF ITS EQUIVALENT VOLUME OF MERCURY OR WATER

If a glass vessel contains at $t^{\circ}\text{C}$, P grammes of mercury, weighed with brass weights in air at 760 mm pressure, then its volume in ccm

$$\text{at the same temperature, } t, : V = PR = P \rho_d$$

$$\text{at another temperature, } t_1, : V = PR_1 = P \rho/d \{1 + \gamma (t_1 - t)\}$$

ρ = the weight, reduced to vacuum, of the mass of mercury or water which, weighed with brass weights, equals 1 gram :

d = the density of mercury or water at $t^{\circ}\text{C}$,

and $\gamma = 0.000025$, is the cubical expansion coefficient of glass.

| Temperature t | WATER. | | | MERCURY. | | |
|--------------------|----------|---------------------------|---------------------------|-----------|---------------------------|---------------------------|
| | R . | $R_1, t_1 = 10^{\circ}$. | $R_1, t_1 = 20^{\circ}$. | R . | $R_1, t_1 = 10^{\circ}$. | $R_1, t_1 = 20^{\circ}$. |
| 0° | 1.001192 | 1.001443 | 1.001693 | 0.0735499 | 0.0735683 | 0.0735867 |
| 1 | 1133 | 1358 | 1609 | 5633 | 5798 | 5982 |
| 2 | 1092 | 1292 | 1542 | 5766 | 5914 | 6098 |
| 3 | 1068 | 1243 | 1493 | 5900 | 6029 | 6213 |
| 4 | 1060 | 1210 | 1460 | 6033 | 6144 | 6328 |
| 5 | 1068 | 1193 | 1443 | 6167 | 6259 | 6443 |
| 6 | 1.001092 | 1.001192 | 1.001442 | 0.0736301 | 0.0736374 | 0.0736558 |
| 7 | 1131 | 1206 | 1456 | 6434 | 6490 | 6674 |
| 8 | 1184 | 1234 | 1485 | 6568 | 6605 | 6789 |
| 9 | 1252 | 1277 | 1527 | 6702 | 6720 | 6904 |
| 10 | 1333 | 1333 | 1584 | 6835 | 6835 | 7020 |
| 11 | 1.001428 | 1.001403 | 1.001653 | 0.0736969 | 0.0736951 | 0.0737135 |
| 12 | 1536 | 1486 | 1736 | 7103 | 7066 | 7250 |
| 13 | 1657 | 1552 | 1832 | 7236 | 7181 | 7365 |
| 14 | 1790 | 1690 | 1940 | 7370 | 7297 | 7481 |
| 15 | 1935 | 1810 | 2060 | 7504 | 7412 | 7596 |
| 16 | 1.002092 | 1.001942 | 1.002193 | 0.0737637 | 0.0737527 | 0.0737711 |
| 17 | 2261 | 2086 | 2337 | 7771 | 7642 | 7826 |
| 18 | 2441 | 2241 | 2491 | 7905 | 7757 | 7941 |
| 19 | 2633 | 2407 | 2658 | 8039 | 7872 | 8057 |
| 20 | 2835 | 2584 | 2835 | 8172 | 7988 | 8172 |
| 21 | 1.003048 | 1.002772 | 1.003023 | 0.0738306 | 0.0738103 | 0.0738288 |
| 22 | 3271 | 2970 | 3220 | 8440 | 8218 | 8403 |
| 23 | 3504 | 3178 | 3429 | 8573 | 8333 | 8518 |
| 24 | 3748 | 3396 | 3647 | 8707 | 8449 | 8633 |
| 25 | 4001 | 3624 | 3875 | 8841 | 8564 | 8748 |
| 26 | 1.004264 | 1.003862 | 1.004113 | 0.0738974 | 0.0738679 | 0.0738864 |
| 27 | 4537 | 4110 | 4361 | 9108 | 8794 | 8979 |
| 28 | 4818 | 4366 | 4616 | 9242 | 8910 | 9094 |
| 29 | 5110 | 4632 | 4884 | 9376 | 9025 | 9210 |
| 30 | 5410 | 4908 | 5159 | 9510 | 9140 | 9325 |

Taken from Landolt, Börnstein, and Meyerhoffer's Physikalisch-Chemische Tabellen.

SMITHSONIAN TABLES.

TABLE 45.—Reductions of Weighings in Air to Vacuo

When the weight M in grams of a body is determined in air, a correction is necessary for the buoyancy of the air equal to $M \delta (1/d - 1/d_1)$ where δ = the density (wt. of 1 ccm in grams = 0.0012) of the air during the weighing, d the density of the body, d_1 that of the weights. δ for various barometric values and humidities may be determined from Tables 128 to 130. The following table is computed for $\delta = 0.0012$. The corrected weight = $M + kM/1000$.

| Density of body weighed d . | Correction factor, k . | | | Density of body weighed d . | Correction factor, k . | | |
|-------------------------------|--------------------------------|--------------------|-----------------------------|-------------------------------|--------------------------------|--------------------|-----------------------------|
| | Pt. Ir. weights $d_1 = 21.5$. | Brass weights 8.4. | Quartz or Al. weights 2.65. | | Pt. Ir. weights $d_1 = 21.5$. | Brass weights 8.4. | Quartz or Al. weights 2.65. |
| .5 | + 2.34 | + 2.26 | + 1.95 | 1.6 | + 0.69 | + 0.61 | + 0.30 |
| .6 | + 1.91 | + 1.86 | + 1.55 | 1.7 | + .65 | + .56 | + .25 |
| .7 | + 1.66 | + 1.57 | + 1.26 | 1.8 | + .62 | + .52 | + .21 |
| .75 | + 1.55 | + 1.46 | + 1.15 | 1.9 | + .58 | + .49 | + .18 |
| .80 | + 1.44 | + 1.36 | + 1.05 | 2.0 | + .54 | + .46 | + .15 |
| .85 | + 1.36 | + 1.27 | + 0.96 | 2.5 | + .43 | + .34 | + .03 |
| .90 | + 1.28 | + 1.19 | + .88 | 3.0 | + .34 | + .26 | — .05 |
| .95 | + 1.21 | + 1.12 | + .81 | 4.0 | + .24 | + .16 | — .15 |
| 1.00 | + 1.14 | + 1.06 | + .75 | 6.0 | + .14 | + .06 | — .25 |
| 1.1 | + 1.04 | + 0.95 | + .64 | 8.0 | + .09 | + .01 | — .30 |
| 1.2 | + 0.94 | + .86 | + .55 | 10.0 | + .06 | — .02 | — .33 |
| 1.3 | + .87 | + .78 | + .47 | 15.0 | + .03 | — .06 | — .37 |
| 1.4 | + .80 | + .71 | + .40 | 20.0 | + .004 | — .08 | — .39 |
| 1.5 | + .75 | + .66 | + .35 | 22.0 | — .001 | — .09 | — .40 |

TABLE 46.—Reductions of Densities in Air to Vacuo

(This correction may be accomplished through the use of the above table for each separate weighing.)

If s is the density of the substance as calculated from the uncorrected weights, S its true density, and L the true density of the liquid used, then the vacuum correction to be applied to the uncorrected density, s , is $0.0012 (1 - s/L)$.

Let W_s = uncorrected weight of substance, W_l = uncorrected weight of the liquid displaced by the substance, then by definition, $s = W_s/W_l$. Assuming D to be the density of the balance of weights, $W_s \{1 + 0.0012 (1/S - 1/D)\}$ and $W_l \{1 + 0.0012 (1/L - 1/D)\}$ are the true weights of the substance and liquid respectively (assuming that the weighings are made under normal atmospheric corrections, so that the weight of 1 cc of air is 0.0012 gram).

$$\text{Then the true density } S = \frac{W_s \{1 + 0.0012 (1/S - 1/D)\}}{W_l \{1 + 0.0012 (1/L - 1/D)\}} L.$$

But from above $W_s/W_l = s/L$, and since L is always large compared with 0.0012, $S = s = 0.0012 (1 - s/L)$.

The values of $0.0012 (1 - s/L)$ for densities up to 20 and for liquids of density 1 (water), 0.852 (xylene) and 13.55 (mercury) follow:

(See reference below for discussion of density determinations).

| Density of substance s . | Corrections. | | | Density of substance s . | Corrections. | |
|----------------------------|-------------------|------------------------|-------------------------|----------------------------|-------------------|-------------------------|
| | $L = 1$ Water. | $L = 0.852$ Xylene. | $L = 13.55$ Mercury. | | $L = 1$ Water. | $L = 13.55$ Mercury. |
| 0.8 | + 0.00024 | — | — | 11. | — 0.0120 | + 0.0002 |
| 0.9 | + .00012 | — | — | 12. | — .0132 | + .0001 |
| 1. | 0.0000 | — 0.0002 | + 0.0011 | 13. | — .0144 | 0.0000 |
| 2. | — .0012 | — .0016 | + .0010 | 14. | — .0156 | 0.0000 |
| 3. | — .0024 | — .0030 | + .0009 | 15. | — .0168 | — .0001 |
| 4. | — .0036 | — .0044 | + .0008 | 16. | — .0180 | — .0002 |
| 5. | — .0048 | — .0058 | + .0008 | 17. | — .0192 | — .0003 |
| 6. | — .0060 | — .0073 | + .0007 | 18. | — .0204 | — .0004 |
| 7. | — .0072 | — .0087 | + .0006 | 19. | — .0216 | — .0005 |
| 8. | — .0084 | — .0101 | + .0005 | 20. | — .0228 | — .0006 |
| 9. | — .0096 | — .0115 | + .0004 | | | |
| 10. | — .0108 | — .0129 | + .0003 | | | |

Johnston and Adams, J. Am. Chem. Soc. 34, p. 563, 1912.

MECHANICAL PROPERTIES: INTRODUCTION AND DEFINITIONS

(Compiled from various sources by Harvey A. Anderson, C.E., Assistant Engineer Physicist, U. S. Bureau of Standards.)

The mechanical properties of most materials vary between wide limits; the following figures are given as being representative rather than what may be expected from an individual sample. Figures denoting such properties are commonly given either as specification or experimental values. Unless otherwise shown, the values below are experimental. Credit for information included is due the U. S. Bureau of Standards; the Am. Soc. for Testing Materials; the Soc. of Automotive Eng.; the Motor Transport Corps, U. S. War Dept.; the Inst. of Mech. Eng.; the Inst. of Metals; Forest Products Lab.; Dept. of Agriculture (Bull. 556); Moore's Materials of Engineering; Hatfield's Cast Iron; and various other American, English and French authorities.

The specified properties shown are indicated minimums as prescribed by the Am. Soc. for Testing Materials, U. S. Navy Dept., Panama Canal, Soc. of Automotive Eng., or Intern. Aircraft Standards Board. In the majority of cases, specifications show a range for chemical constituents and the average value only of this range is quoted. Corresponding average values are in general given for mechanical properties. In general, tensile test specimens were 12.8 mm (0.505 in.) diameter and 50.8 mm (2 in.) gage length. Sizes of compressive and transverse specimens are generally shown accompanying the data.

All data shown in these tables are as determined at ordinary room temperature, averaging 20° C (68° F.). The properties of most metals and alloys vary considerably from the values shown when the tests are conducted at higher or lower temperatures.

The following definitions govern the more commonly confused terms shown in the tables. In all cases the stress referred to in the definitions is equal to the total load at that stage of the test divided by the original cross-sectional area of the specimen (or the corresponding stress in the extreme fiber as computed from the flexure formula for transverse tests).

Proportional Limit (abbreviated P-limit). — Stress at which the deformation (or deflection) ceases to be proportional to the load (determined with extensometer for tension, compressometer for compression and deflectometer for transverse tests).

Elastic Limit. — Stress which produces a permanent elongation (or shortening) of 0.001 per cent of the gage length, as shown by an instrument capable of this degree of precision (determined from set readings with extensometer or compressometer). In transverse tests the extreme fiber stress at an appreciable permanent deflection.

Yield Point. — Stress at which marked increase in deformation (or deflection) of specimen occurs without increase in load (determined usually by drop of beam or with dividers for tension, compression or transverse tests).

Ultimate Strength in Tension or Compression. — Maximum stress developed in the material during test.

Modulus of Rupture. — Maximum stress in the extreme fiber of a beam tested to rupture, as computed by the empirical application of the flexure formula to stresses above the transverse proportional limit.

Modulus of Elasticity (Young's Modulus). — Ratio of stress within the proportional limit to the corresponding strain, — as determined with an extensometer. Note: All moduli shown are obtained from tensile tests of materials, unless otherwise stated.

Brinell Hardness Numeral (abbreviated B. h. n.). — Ratio of pressure on a sphere used to indent the material to be tested to the area of the spherical indentation produced. The standard sphere used is a 10-mm diameter hardened steel ball. The pressures used are 3000 kg for steel and 500 kg for softer metals, and the time of application of pressure is 30 seconds. Values shown in the tables are based on spherical areas computed in the main from measurements of the diameters of the spherical indentations, by the following formula:

$$B. h. n. = P \div \pi t D = P \div \pi D(D/2 - \sqrt{D^2/4 - d^2/4}).$$

P = pressure in kg, t = depth of indentation, D = diameter of ball, and d = diameter of indentation, — all lengths being expressed in mm. Brinell hardness values have a direct relation to tensile strength, and hardness determinations may be used to define tensile strengths by employing the proper conversion factor for the material under consideration.

Shore Scleroscope Hardness. — Height of rebound of diamond pointed hammer falling by its own weight on the object. The hardness is measured on an empirical scale on which the average hardness of martensitic high carbon steel equals 100. On very soft metals a "magnifier" hammer is used in place of the commonly used "universal" hammer and values may be converted to the corresponding "universal" value by multiplying the reading by $\frac{1}{2}$. The scleroscope hardness, when accurately determined, is an index of the tensile elastic limit of the metal tested.

Erichsen Value. — Index of forming quality of sheet metal. The test is conducted by supporting the sheet on a circular ring and deforming it at the center of the ring by a spherical pointed tool. The depth of impression (or cup) in mm required to obtain fracture is the Erichsen value for the metal. Erichsen standard values for trade qualities of soft metal sheets are furnished by the manufacturer of the machine corresponding to various sheet thicknesses. (See Proc. A. S. T. M. 17, part 2, p. 200, 1917.)

Alloy steels are commonly used in the heat treated condition, as strength increases are not commensurate with increases in production costs for annealed alloy steels. Corresponding strength values are accordingly shown for annealed alloy steels and for such steels after having been given certain recommended heat treatments of the Society of Automotive Engineers. The heat treatments followed in obtaining the properties shown are outlined on the pages immediately following the tables on steel. It will be noted that considerable latitude is allowed in the indicated drawing temperatures and corresponding wide variations in physical properties may be obtained with each heat treatment. The properties vary also with the size of the specimens heat treated. The drawing temperature is shown with the letter denoting the heat treatment, wherever the information is available.

MECHANICAL PROPERTIES

Iron and Iron Alloys

| Metal. | Grade. | Yield point. | Ultimate strength. | Yield point. | Ultimate strength. | Elong. in 50.8 mm (2 in.). | Reduct. in area. | Hardness. | |
|--------|--|-----------------------------|--------------------|----------------------------|--------------------|----------------------------|------------------|--------------------|---------------|
| | | Tension. kg/mm ² | | Tension lb/in ² | | Per cent. | | Brinell at 3000 kg | Sclero-scope. |
| Iron : | | | | | | | | | |
| | Electrolytic* (remelt): as forged... | 34.0 | 38.5 | 48,500 | 55,000 | 33.0 | 83.0 | 95 † | 18 |
| | annealed 900° C | 12.5 | 27.0 | 18,000 | 38,000 | 52.0 | 87.0 | 75 † | — |
| | Gray cast‡ (19 mm diam. bars) | indet. | { 17.5 20.5 | indet. | { 25,000 38,000 | negligible | — | { 100 150 | { 24 40 |
| | Malleable cast, American (after Hatfield) | { 14.0 31.5 | { 24.5 40.0 | { 20,000 45,000 | { 35,000 57,000 | { 15.0 4.5 | { 15.0 4.5 | — | — |
| | European (after Am. Malleable Castings Ass.) | { 19.0 28.0 | { 29.5 45.5 | { 27,000 40,000 | { 42,000 65,000 | { 6.0 2.0 | { 6.0 2.0 | — | — |
| | (see p. 653) | | | | | | | | |
| | Commercial wrought. | { 19.5 22.5 | { 34.0 37.0 | { 28,000 32,000 | { 48,000 53,000 | { 40.0 30.0 | { 45.0 35.0 | — | { 25 30 |
| | Silicon alloys Si 0.01: as forged... | 29.5 | 31.5 | 41,800 | 45,200 | 35.0 | 78.0 | — | — |
| | (Melted in vacuo) ann. 970° C | 11.0 | 24.5 | 16,000 | 34,900 | 53.0 | 81.5 | — | — |
| | (Note: C max. 0.01 per cent) | | | | | | | | |
| | Si 1.71 : as forged..... | 48.0 | 53.5 | 68,100 | 76,300 | 37.0 | 82.0 | — | — |
| | annealed 970° C..... | 25.0 | 38.0 | 35,800 | 54,200 | 50.0 | 90.6 | — | — |
| | Si 4.40 : as forged..... | 66.0 | 74.0 | 94,000 | 105,000 | 6.0 | 7.5 | — | — |
| | annealed 970° C | 51.0 | 64.5 | 72,900 | 91,600 | 24.0 | 25.1 | — | — |
| | Aluminum alloys¶ Al 0.00 : as forged | 35.5 | 38.5 | 50,700 | 54,700 | 26.0 | 84.3 | — | — |
| | (Melted in vacuo) ann. 1000° C | 12.5 | 24.5 | 17,600 | 34,900 | 60.0 | 93.5 | — | — |
| | (Note: C max. 0.01 per cent) | | | | | | | | |
| | Al 3.08 : as forged..... | 48.0 | 54.5 | 68,200 | 77,500 | 21.0 | 76.4 | — | — |
| | annealed 1000° C | 22.5 | 37.5 | 31,800 | 53,400 | 51.0 | 85.3 | — | — |
| | Al 6.24 : as forged..... | 54.5 | 60.5 | 77,700 | 86,000 | 28.0 | 74.7 | — | — |
| | annealed 1000° C | 37.5 | 49.0 | 53,400 | 69,800 | 27.0 | 55.5 | — | — |

Composition, approximate:

Electrolytic, C 0.0125 per cent; other impurities less than 0.05 per cent.

Cast, gray: Graphitic, C 3.0, Si 1.3 to 2.0, Mn 0.6 to 0.9, S max. 0.1, P max. 1.2.

A. S. T. M. Spec. A48 to 18 allows S max. 0.10, except S max. 0.12 for heavy castings.

Malleable: American "Black Heart," C 2.8 to 3.5, Si 0.6 to 0.8, Mn max. 0.4, S max. 0.07, P max. 0.2.

European "Steely Fracture," C 2.8 to 3.5, Si 0.6 to 0.8, Mn 0.15, S max. 0.35, P max. 0.2.

Compressive Strengths [Specimens tested: 25.4 mm (1 in.) diam. cylinders 76.2 mm (3 in.) long].

Electrolytic iron 56.5 kg/mm² or 80,000 lb/in².Gray and malleable cast iron 56.5 to 84.5 kg/mm² or 80,000 to 120,000 lb/in².

Wrought iron, approximately equal to tensile yield point (slightly above P-limit).

Density:

Electrolytic iron..... 7.8 g/cm³ or 487 lb/ft³ Malleable iron..... see page 653Cast iron..... 7.2 g/cm³ or 449 lb/ft³ Wrought iron..... 7.85 g/cm³ or 490 lb/ft³

Ductility: — Normal Erichsen values for good trade quality sheets, 0.4 mm (0.0156 in.)

Thickness, soft annealed.

Depth.

Sheet metal hoop iron, polished..... mm in.

Charcoal iron tinned sheet..... 9.5 0.374

Second quality tinned sheet..... 7.5 0.295

..... 6.7 0.264

Modulus of elasticity in tension and compression:

Electrolytic iron.... 17,500 kg/mm² or 25,000,000 lb/in² Malleable iron... see page 653Cast iron..... 10,500 kg/mm² or 15,000,000 lb/in² Wrought iron.... 17,500 kg/mm² or 25,000,000 lb/in²

Modulus of elasticity in shear:

Electrolytic iron..... 7030 kg/mm² or 10,000,000 lb/in² Cast iron 8450 kg/mm² or 12,000,000 lb/in²Wrought iron..... 7030 kg/mm² or 10,000,000 lb/in²

Scleroscope hardness values shown are as determined with the Shore Universal hammer.

Strength in Shear:

Electrolytic (remelt)

Commercial wrought

P-limit..... 8.4 kg/mm² or 12,000 lb/in²P-limit..... 21.1 kg/mm² or 30,000 lb/in²Ultimate strength..... 21.1 kg/mm² or 30,000 lb/in²Ultimate strength.. 35.0 kg/mm² or 50,000 lb/in²

Transverse strength, from flexure formula:

Gray cast iron

Modulus of rupture, 33.0 kg/mm² or 47,000 lb/in²

"Arbitration Bar," 31.8 mm (1¼ in.) diameter, or 304.8 mm (12 in.) span; minimum central load at rupture 1130 to 1500 kg (2500 to 3300 lb.); minimum central deflection at rupture 2.5 mm (0.1 in.), (A. S. T. M. Spec. A 48-18).

* Properties of Swedish iron (impurities less than 1 per cent) approximate those of electrolytic iron.

† These two values of B. h. n. only are as determined at 500 kg pressure.

‡ U. S. Navy specifies minimum tensile strength of 14.1 kg/mm² or 20,000 lb/in².

|| From T. D. Jensen, University of Illinois, Engr. Exp. Station, Bulletin No. 83, 1915 (shows Si 4.40 as alloy of maximum strength).

¶ From T. D. Jensen, University of Illinois, Engr. Exp. Station, Bulletin No. 95, 1917.

TABLES 49 AND 50 MECHANICAL PROPERTIES

TABLE 49. — Carbon Steels — Commercial Experimental Values

S. A. E. (Soc. of Automotive Eng., U. S. A.) classification scheme used as basis for steel groupings. First two digits S. A. E. Spec. No. show steel group number, and last two (or three in case of five figures) show carbon content in hundredths of one per cent.

The first lines of properties for each steel show values for the rolled or forged metal in the annealed or normalized condition. Comparative heat-treated values show properties after receiving modified S. A. E. heat treatment as shown below (Table 50). The P-limit and ductility of cast steel average slightly lower and the ultimate strength 10 to 15 per cent higher than the values shown for the same composition steel in the annealed condition. The properties of rolled steel (raw) are approximately equal to those shown for the annealed condition, which represents the normalized condition of the metal rather than the soft annealed state.

The data for heat-treated strengths are average values for specimens for heat treatment ranging in size from $\frac{1}{2}$ to $1\frac{1}{2}$ in. diameter. The final drawing or quenching temperature for the properties shown is indicated in degrees C with the heat treatment letter, wherever the information is available. In general, specimens were drawn near the lower limit of the indicated temperature range.

| Metal. | S. A. E. spec. no. | Nominal contents per cent. | S. A. E. heat treatment. | P-limit. | Ultimate strength. | P-limit. | Ultimate strength. | Elong. in 50.8 mm (2 in.). | Reduct. in area. | Hardness | | |
|--------------------|---|----------------------------|----------------------------|----------------------------|----------------------------------|----------------------------|--------------------|----------------------------|------------------|----------|----|--|
| | | | | Tension kg/mm ² | Tension lb/in ² | Tension lb/in ² | Per cent | Brinell @ 3000 kg. | Sclero-scope. | | | |
| Steel, carbon | 1010 } | See Spec. No. (Mn 0.45) | Ann. A | 24.0 | 32.0 | 34,500 | 46,000 | 37.0 | 72.0 | — | 18 | |
| | 1010 } | | A | 27.0 | 42.0 | 39,000 | 60,000 | 30.0 | 62.0 | 120 | 24 | |
| | 1020 } | | Ann. A | 28.0 | 38.0 | 39,500 | 54,100 | 32.0 | 68.0 | 100 | 17 | |
| | 1020 } | | H 230° C | 35.0 | 56.0 | 49,500 | 79,500 | 20.0 | 59.0 | 176 | 35 | |
| | 1045 } | (Mn 0.65) | Ann. A | 40.0 | 50.0 | 57,500 | 71,300 | 23.0 | 54.0 | 168 | 27 | |
| | 1045 } | | H 260° C | 62.0 | 86.0 | 88,000 | 123,000 | 13.5 | 36.0 | 290 | 45 | |
| | 1095 } | (Mn 0.35) | Ann. A | 42.0 | 56.0 | 59,500 | 79,000 | 21.0 | 51.0 | 187 | 20 | |
| | 1095 } | | F 510° C | 84.0 | 123.0 | 120,000 | 175,000 | 6.0 | 18.0 | 551 | 75 | |
| | Specification values: Steel, castings, Ann. A.S.T.M. A27-16, Class B; * P max. 0.06; S max. 0.05. | | | | | | | | | | | |
| | Grade. | Yield point. | Ultimate tensile strength. | | Per cent elong. 50.8 mm or 2 in. | Per cent reduct. area. | | | | | | |
| kg/mm ² | | | lb/in ² | | | | | | | | | |
| Hard..... | 0.45 ultimate | 56.2 | 80,000 | 15 | 20 | | | | | | | |
| Medium..... | 0.45 " | 49.2 | 70,000 | 18 | 25 | | | | | | | |
| Soft..... | 0.45 " | 42.2 | 60,000 | 22 | 30 | | | | | | | |

Structural Steel: Rolled; S max. 0.05; P-Bess. max. 0.10; —O-H. max. 0.06.

Tension: Yield Point min. = 0.5 ultimate; ultimate = 38.7 to 45.7 kg/mm² or 55,000 to 65,000 lb/in² with 22% min. elongation in 50.8 mm (2 in.).

* Average carbon contents: steel castings, C 0.30 to 0.40; structural steel, C 0.15 to 0.30 (mild carbon or medium hard steel).

TABLE 50. — Explanation of Heat Treatment Letters used in Table of Steel Data

Motor Transport Corps Modified S. A. E. Heat Treatments for Steels. (S. A. E. Handbook, Vol. 1, pp. 9d and 9e, 1915, q. v. for alternative treatments.)

Heat Treatment A. — After forging or machining (1) carbonize at a temperature between 870 and 930° C (1600 and 1700° F.); (2) cool slowly; (3) reheat to 760 to 820° C (1400 to 1500° F.) and quench in oil.

Heat Treatment D. — After forging or machining: (1) heat to 820 to 840° C (1500 to 1550° F.); (2) quench; (3) reheat to 700 to 820° C (1450 to 1500° F.); (4) quench; (5) reheat to 320 to 650° C (600 to 1200° F.) and cool slowly.

Heat Treatment F. — After shaping or coiling: (1) heat to 775 to 800° C (1425 to 1475° F.); (2) quench; (3) reheat to 200 to 480° C (400 to 900° F.) in accordance with degree of temper required and cool slowly.

Heat Treatment H. — After forging or machining: (1) heat to 820 to 840° C (1500 to 1550° F.); (2) quench; (3) reheat to 230 to 650° C (450 to 1200° F.) and cool slowly.

Heat Treatment L. — After forging or machining: (1) carbonize at a temperature between 870 and 950° C (1600 and 1750° F.), preferably between 900 and 930° C (1650 and 1700° F.); (2) cool slowly in carbonizing material; (3) reheat to 790 to 820° C (1450 to 1500° F.); (4) quench; (5) reheat to 700 to 760° C (1300 to 1400° F.); (6) quench; (7) reheat to 120 to 260° C (250 to 500° F.) and cool slowly.

Heat Treatment M. — After forging or machining: (1) heat to 790 to 820° C (1450 to 1500° F.); (2) quench; (3) reheat to between 260 and 680° C (500 and 1250° F.) and cool slowly.

Heat Treatment P. — After forging or machining: (1) heat to 790 to 820° C (1450 to 1500° F.); (2) quench; (3) reheat to 750 to 770° C (1375 to 1425° F.); (4) quench; (5) reheat to 260 to 650° C (500 to 1200° F.) and cool slowly.

Heat Treatment T. — After forging or machining: (1) heat to 900 to 950° C (1650 to 1750° F.); (2) quench; (3) reheat to 260 to 700° C (500 to 1300° F.) and cool slowly.

Heat Treatment U. — After forging: (1) heat to 830 to 870° C (1525 to 1600° F.), hold half an hour; (2) cool slowly; (3) reheat to 900 to 930° C (1650 to 1700° F.); (4) quench; (5) reheat to 180 to 290° C (350 to 550° F.) and cool slowly.

Heat Treatment V. — After forging or machining: (1) heat to 900 to 950° C (1650 to 1750° F.); (2) quench; (3) reheat to between 200 and 650° C (400 and 1200° F.) and cool slowly.

EDITOR'S NOTE: Oil quenching is recommended wherever the instructions specify "quench," inasmuch as the data in the table are taken from tests of automobile parts which must resist considerable vibration and which are usually small in section. The quenching medium must always be carefully considered.

MECHANICAL PROPERTIES

Alloy Steels — Commercial Experimental Values

| Metal. | S. A. E. spec. no. | Nominal contents, per cent. | S. A. E. heat treatment. | P-limit. | | Ultimate strength. | | Elong. in 50.8 mm (2 in.). | Reduct. in area. | Hardness. | |
|-------------------|--------------------|---|--------------------------|-----------------------------|-----------------------------|--------------------|-----------------------|----------------------------|------------------|---------------|----|
| | | | | Tension kg. mm ² | Tension lb./in ² | Per cent. | Brinell (w/ 3000 kg.) | | | Scler- scope. | |
| Steel, nickel. | 2315 | — | Ann. | 30.0 | 38.0 | 42,500 | 54,000 | 32.0 | 60.0 | 138 | — |
| | 2315 | — | H | 53.0 | 76.0 | 75,000 | 107,500 | 18.0 | 55.0 | 321 | 43 |
| | 2335 | Ni 3.50 (Mn 0.65) | Ann. | 39.0 | 48.0 | 55,000 | 68,000 | 24.0 | 53.0 | 165 | — |
| | 2335 | | H | 106.0 | 131.0 | 151,000 | 186,000 | 15.0 | 51.0 | 465 | 62 |
| | 2345 | | Ann. | 44.0 | 55.0 | 62,500 | 78,000 | 21.0 | 48.0 | 172 | — |
| | 2345 | | H | 136.0 | 149.0 | 193,000 | 212,000 | 12.0 | 45.0 | 570 | 76 |
| Invar | Ni 36.0 C 0.40 | Ann. | 50.0 | 77.5 | 71,000 | 110,000 | 30.0 | 50.0 | — | — | |
| nickel chrome.... | 3120 | { Ni 1.25 Cr 0.60 (Mn 0.65) | Ann. | 34.0 | 44.0 | 49,000 | 62,000 | 23.0 | 53.0 | 155 | 22 |
| | 3120 | | H 450° C | 60.0 | 82.0 | 85,000 | 116,000 | 23.0 | 48.0 | 270 | 36 |
| | 3135 | | Ann. | 40.0 | 50.0 | 57,000 | 71,300 | 20.0 | 46.0 | 182 | 30 |
| | 3135 | | H or D | 88.0 | 121.0 | 125,000 | 172,000 | 18.0 | 43.0 | 330 | 44 |
| | 3220 | { Ni 1.75 Cr 1.10 (Mn 0.45) | Ann. | 39.0 | 49.0 | 55,000 | 69,000 | 21.0 | 50.0 | 170 | — |
| | 3220 | | H or D | 77.0 | 106.0 | 110,000 | 151,000 | 23.0 | 48.0 | 375 | 50 |
| | 3250 | | Ann. | 44.0 | 55.0 | 62,000 | 78,000 | 19.0 | 42.0 | 180 | — |
| | 3250 | | M | 134.0 | 183.0 | 190,000 | 260,000 | 16.0 | 32.0 | 480 | 64 |
| | 3320 | { Ni 3.50 Cr 1.50 (Mn 0.45) | Ann. | 32.0 | 42.0 | 46,000 | 59,500 | 21.0 | 50.0 | — | — |
| | 3320 | | L | 77.0 | 105.0 | 110,000 | 150,000 | 23.0 | 48.0 | 375 | 50 |
| | 3340 | | Ann. | 39.0 | 52.0 | 56,000 | 74,000 | 18.0 | 45.0 | — | — |
| | 3340 | | P | 120.0 | 163.0 | 170,000 | 232,000 | 18.0 | 42.0 | 479 | 64 |
| chromium. | 51120 | Cr 1.00 | Ann. | 44.0 | 58.0 | 62,000 | 82,000 | 16.0 | 31.0 | — | — |
| | 51120 | (Mn 0.35) | M or P | 144.0 | 193.0 | 205,000 | 275,000 | 7.0 | 26.0 | 500 | 66 |
| | 52120 | Cr 1.20 | Ann. | 44.0 | 58.0 | 62,000 | 82,000 | 13.0 | 24.0 | — | — |
| | 52120 | (Mn 0.35) | M or P | 141.0 | 178.0 | 200,000 | 253,000 | 7.0 | 25.0 | 524 | 70 |
| chrome vanadium | 6130 | { (Mn 0.65) Cr 0.95 V 0.18 (Mn 0.35) | Ann. | 43.0 | 59.0 | 61,500 | 84,500 | 23.0 | 51.0 | 152 | — |
| | 6130 | | T | 84.0 | 115.0 | 120,000 | 163,000 | 16.0 | 43.0 | 432 | 59 |
| | 6195 | | Ann. | 48.0 | 63.0 | 68,200 | 90,000 | 16.0 | 38.0 | — | — |
| silico-manganese | 6195 | U | 176.0 | 232.0 | 250,000 | 330,000 | 8.0 | 24.0 | 562 | 75 | |
| | 9250 | { Si 1.95 Mn 0.70 Si 0.85 Mn 1.75 | Ann. | 42.0 | 54.0 | 60,000 | 77,000 | 16.0 | 28.0 | — | — |
| | 9250 | | V | 91.0 | 122.0 | 130,000 | 174,000 | 14.0 | 24.0 | 441 | 59 |
| | 9×30 | | Ann. | 48.0 | 61.0 | 68,000 | 87,000 | 13.0 | 22.0 | — | — |
| 9×30 | V | | 113.0 | 148.0 | 160,000 | 211,000 | 12.0 | 21.0 | 470 | 63 | |
| tungsten. | (C-73) | W 2.4 | Ann. | 34.0 | 59.0 | 48,100 | 84,200 | 20.5 | 31.5 | — | — |
| | (C-70) | W 9.7 | Ann. | 63.0 | 89.0 | 90,000 | 126,000 | 14.0 | 22.1 | — | — |
| | (C-47) | W 15.6 | Quench | | | | | | | | |
| | | 1065° Draw 205° C | 158.5 | 175.0 | 225,000 | 248,000 | 6.0 | 43.0 | 520 | 64 | |

GENERAL NOTE. — Table on steels after Motor Transport Corps, Metallurgical Branch of Engineering Division, Table No. 88.

Maximum allowable P 0.045 or less, maximum allowable S 0.05 or less.

Silicon contents were not determined by Motor Transport Corps in preparing table, except for silico-manganese steels.

Compressive strengths:

For all steels approx. equal to yield point in tension (slightly above P-limit).

Density:

Steel weighs about 7.85 g/cm³ or 490 lb/ft³

Ductility, Erichsen values:

0.75 mm (0.029 in.) thick, low carbon soft annealed sheet (B. S.), depth of indentation 12.0 mm or 0.472 in.

1.30 mm (0.050 in.) thick, low carbon soft annealed sheet (B. S.), depth of indentation 12.5 mm or 0.492 in.

Modulus of elasticity in tension and compression:

For all steels approx. 21,000 kg/mm² = 30,000,000 lb/in².

Modulus of elasticity in shear:

For all steels approx. 8,400 kg/mm² = 12,000,000 lb/in².

Scleroscope hardness values shown are as determined with the Shore Universal hammer.

Strength in shear:

P-limit and ultimate strength each about 70 per cent corresponding tensile values.

SMITHSONIAN TABLES.

TABLES 52-54

MECHANICAL PROPERTIES

TABLE 52. — Steel Wire — Specification Values

(After I. A. S. B. Specification 3S12, Sept., 1917, for High-strength Steel Wire.)

S. A. E. Carbon Steel, No. 1050 or higher number specified (see Carbon steels above). Steel used to be manufactured by acid open-hearth process, to be rolled, drawn, and then uniformly coated with pure tin to solder readily.

| American or B. and S. wire gage. | Diameter. | | Req'd twists in 203.2 mm or 8 in. | Weight. | | Req'd bends thru 90° | Spec. minimum tensile strength. | | | |
|----------------------------------|-----------|-------|-----------------------------------|----------|------------|----------------------|---------------------------------|------|--------------------|--------------------|
| | mm | in. | | kg/100 m | lb/100 ft. | | kg | lb. | kg/mm ² | lb/in ² |
| 6 | 4.115 | 0.162 | 16 | 10.44 | 7.01 | 5 | 2040 | 4500 | 154 | 219,000 |
| 7 | 3.605 | 0.144 | 19 | 8.28 | 5.56 | 6 | 1680 | 3700 | 161 | 229,000 |
| 8 | 3.264 | 0.129 | 21 | 6.55 | 4.40 | 8 | 1360 | 3000 | 164 | 235,000 |
| 9 | 2.906 | 0.114 | 23 | 5.21 | 3.50 | 9 | 1135 | 2500 | 172 | 244,000 |
| 10 | 2.588 | 0.102 | 26 | 4.12 | 2.77 | 11 | 910 | 2000 | 172 | 244,000 |
| 11 | 2.305 | 0.091 | 30 | 3.28 | 2.20 | 14 | 735 | 1620 | 179 | 254,000 |
| 12 | 2.053 | 0.081 | 33 | 2.60 | 1.74 | 17 | 590 | 1300 | 177 | 252,000 |
| 13 | 1.828 | 0.072 | 37 | 2.06 | 1.38 | 21 | 470 | 1040 | 179 | 255,000 |
| 14 | 1.628 | 0.064 | 42 | 1.64 | 1.10 | 25 | 375 | 830 | 181 | 258,000 |
| 15 | 1.450 | 0.057 | 47 | 1.30 | 0.87 | 29 | 300 | 660 | 182 | 259,000 |
| 16 | 1.291 | 0.051 | 53 | 1.03 | 0.69 | 34 | 245 | 540 | 186 | 264,000 |
| 17 | 1.150 | 0.045 | 60 | 0.81 | 0.55 | 42 | 195 | 425 | 188 | 267,000 |
| 18 | 1.024 | 0.040 | 67 | 0.65 | 0.43 | 52 | 155 | 340 | 190 | 270,000 |
| 19 | 0.912 | 0.036 | 75 | 0.51 | 0.34 | 70 | 125 | 280 | 193 | 275,000 |
| 20 | 0.812 | 0.032 | 85 | 0.41 | 0.27 | 85 | 100 | 225 | 197 | 280,000 |
| 21 | 0.723 | 0.028 | 96 | 0.32 | 0.22 | 105 | 80 | 175 | 200 | 284,000 |

NOTE. — Number of 90° bends specified above to be obtained by bending sample about 4.76 mm (0.188 in.) radius, alternately, in opposite directions.

(Above specification corresponds to U. S. Navy Department Specification 22W6, Nov. 1, 1916, for tinned, galvanized or bright aeroplane wire.)

TABLE 53. — Steel Wire — Experimental Values

(Data from tests at General Electric Company laboratories.) "Commercial Steel Music Wire (Hardened)."

| Diameter. | | Ultimate strength. | |
|-----------|-------|---|---------|
| mm | in. | kg/mm ² tension lb/in ² | |
| 12.95 | 0.051 | 226.0 | 321,500 |
| 11.70 | 0.46 | 249.0 | 354,000 |
| 9.15 | 0.36 | 253.0 | 360,000 |
| 7.60 | 0.30 | 260.0 | 370,000 |
| 6.35 | 0.25 | 262.0 | 372,500 |
| 4.55 | 0.18 | 265.5 | 378,000 |
| 2.55* | 0.10 | 386.5 | 550,000 |
| 1.65* | 0.065 | 527.0 | 750,000 |
| 4.55† | 0.18 | 49.2 | 70,000 |

* For 4.55 mm wire drawn cold to indicated sizes. † For 4.55 mm (0.018 in.) wire annealed in H₂ at 850° C.

TABLE 54. — Semi-steel

Test results at Bureau of Standards on 155-mm shell, Jan. 1919.

Microstructure — matrix resembling pearlitic steel, embedded in which are flakes of graphite.

Composition—Comb. C 0.60 to 0.76, Mn 0.88, P 0.12 to 0.43, S 0.077 to 0.088, Si 1.22 to 1.23, graphitic C 2.84 to 2.94.

| Metal. | P-limit. | Ultimate strength. | P-limit. | Ultimate strength. | P-limit. | Ultimate strength. | P-limit. | Ultimate strength. | Hardness. | |
|--|----------------------------|--------------------|----------------------------|--------------------|--------------------------------|--------------------|--------------------------------|--------------------|-------------------|---------------|
| | Tension kg/mm ² | | Tension lb/in ² | | Compression kg/mm ² | | Compression lb/in ² | | Brinell @ 3000 kg | Sclero-scope. |
| Semi-steel: Graph. C 2.85 Comb. C 0.76 | 7.9 | 19.8 | 11,200 | 28,200 | 24.3 | 72.6 | 34,500 | 103,000 | 176 | — |
| | 4.2 | 14.9 | 6,000 | 21,200 | 18.3 | 61.4 | 26,000 | 87,300 | 170 | — |

Tension specimens 12.7 mm (0.5 in.) diameter, 50.8 mm (2 in.) gage length; elongation and reduction of area negligible.

Compression specimens 20.3 mm (0.8 in.) diameter, 61.0 mm (2.4 in.) long; failure occurring in shear.

Tension set readings with extensometer showed elastic limit of 2.1 kg/mm² or 3000 lb/in².Modulus of elasticity in tension — 9560 kg/mm² or 13,600,000 lb/in².

TABLE 55. — Steel-wire Rope — Specification Values

Cast steel wire to be of hard crucible steel with minimum tensile strength of 155 kg/mm² or 220,000 lb/in² and minimum elongation of 2 per cent in 254 mm (10 in.).

Plow steel wire to be of hard crucible steel with minimum tensile strength of 183 kg/mm² or 260,000 lb/in² and minimum elongation of 2 per cent in 254 mm (10 in.).

Annealed steel wire to be of crucible cast steel, annealed, with minimum tensile strength of 77 kg/mm² or 110,000 lb/in² and minimum elongation of 7 per cent in 254 mm (10 in.).

Type A: 6 strands with hemp core and 19 wires to a strand (= 6 × 19), or 6 strands with hemp core and 18 wires to a strand with jute, cotton or hemp center.

Type B: 6 strands with hemp core, and 12 wires to a strand with hemp center.

Type C: 6 strands with hemp core, and 14 wires to a strand with hemp or jute center.

Type AA: 6 strands with hemp core, and 37 wires to a strand (= 6 × 37) or 6 strands with hemp core and 36 wires to a strand with jute, cotton or hemp center.

| Description. | Diameter. | | Approx. weight. | | Minimum strength. | |
|--------------------------------|-----------|-----------------|-----------------|-------|-------------------|---------|
| | mm | in. | kg/m | lb/ft | kg | lb. |
| Galv. cast steel, Type A..... | 9.5 | $\frac{3}{8}$ | 0.31 | 0.21 | 3,905 | 8,740 |
| " " " " "..... | 12.7 | $\frac{1}{2}$ | 0.55 | 0.37 | 6,910 | 15,230 |
| " " " " "..... | 25.4 | 1 | 2.23 | 1.50 | 27,650 | 60,960 |
| " " " " "..... | 38.1 | $1\frac{1}{2}$ | 5.06 | 3.40 | 63,485 | 139,960 |
| Galv. cast steel, Type AA..... | 9.5 | $\frac{3}{8}$ | 0.35 | 0.22 | 3,840 | 8,400 |
| " " " " "..... | 12.7 | $\frac{1}{2}$ | 0.58 | 0.39 | 7,410 | 16,330 |
| " " " " "..... | 25.4 | 1 | 2.23 | 1.50 | 27,650 | 60,960 |
| " " " " "..... | 38.1 | $1\frac{1}{2}$ | 5.28 | 3.55 | 59,735 | 131,690 |
| Galv. cast steel, Type B..... | 9.5 | $\frac{3}{8}$ | 0.25 | 0.17 | 2,995 | 6,600 |
| " " " " "..... | 12.7 | $\frac{1}{2}$ | 0.42 | 0.28 | 5,210 | 11,500 |
| " " " " "..... | 25.4 | 1 | 1.68 | 1.13 | 20,890 | 46,060 |
| " " " " "..... | 38.1 | $1\frac{1}{2}$ | 3.94 | 2.65 | 47,965 | 105,740 |
| Galv. cast steel, Type C..... | 25.4 | 1 | 1.59 | 1.07 | 18,825 | 41,500 |
| " " " " "..... | 41.3 | $1\frac{5}{8}$ | 4.35 | 2.92 | 51,575 | 113,700 |
| Galv. plow steel, Type A..... | 9.5 | $\frac{3}{8}$ | 0.31 | 0.21 | 4,690 | 10,340 |
| " " " " "..... | 12.7 | $\frac{1}{2}$ | 0.55 | 0.37 | 8,165 | 18,000 |
| " " " " "..... | 25.4 | 1 | 2.23 | 1.50 | 32,675 | 72,040 |
| " " " " "..... | 36.5 | $1\frac{7}{16}$ | 4.66 | 3.13 | 69,140 | 152,430 |
| Galv. plow steel, Type AA..... | 9.5 | $\frac{3}{8}$ | 0.33 | 0.22 | 4,540 | 10,000 |
| " " " " "..... | 12.7 | $\frac{1}{2}$ | 0.58 | 0.39 | 8,750 | 19,300 |
| " " " " "..... | 25.4 | 1 | 2.35 | 1.58 | 32,250 | 71,100 |
| " " " " "..... | 41.3 | $1\frac{5}{8}$ | 6.18 | 4.15 | 83,010 | 183,000 |

TABLE 56. — Steel-wire Rope — Experimental Values

(Wire rope purchased under Panama Canal Spec. 302 and tested by U. S. Bureau of Standards, Washington, D. C.)

| Description and analysis. | Diameter. | | Ultimate strength. | | Ultimate strength (net area). | |
|--|-----------|----------------|--------------------|---------|-------------------------------|--------------------|
| | mm | in. | kg | lb. | kg/mm ² | lb/in ² |
| Plow Steel, 6 strands × 19 wires C 0.90, S 0.034, P 0.024, Mn 0.48, Si 0.172..... | 50.8 | 2 | 137,900 | 304,000 | 129.5 | 184,200 |
| Plow Steel, 6 strands × 25 wires C 0.77, S 0.036, P 0.027, Mn 0.46, Si 0.152..... | 69.9 | $2\frac{3}{4}$ | 314,800 | 694,000 | 151.2 | 214,900 |
| Plow Steel, 6 × 37 plus 6 × 19 C 0.58, S 0.032, P 0.033, Mn 0.41, Si 0.160..... | 82.6 | $3\frac{1}{4}$ | 392,800 | 866,000 | 132.2 | 187,900 |
| Monitor Plow Steel, 6 × 61 plus 6 × 19, C 0.82, S 0.025, P 0.019, Mn 0.23, Si 0.169..... | 82.6 | $3\frac{1}{4}$ | 425,000 | 937,000 | 142.5 | 202,400 |

Recommended allowable load for wire rope running over sheave is one fifth of specified min. strength.

TABLE 57. — Plow-Steel Hoisting Rope (Bright)

(After Panama Canal Specification No. 302, 1912.)

Wire rope to be of best plow steel grade, and to be composed of 6 strands, 19 wires to the strand, with hemp center. Wires entering into construction of rope to have an elongation in 203.2 mm or 8 in. of about 2½ per cent.

| Diameter. | | Spec. minimum strength. | | Diameter. | | Spec. minimum strength. | |
|-----------|---------------|-------------------------|--------|-----------|----------------|-------------------------|---------|
| mm | in. | kg | lb. | mm | in. | kg | lb. |
| 9.5 | $\frac{3}{8}$ | 5,215 | 11,500 | 38.1 | $1\frac{1}{2}$ | 74,390 | 164,000 |
| 12.7 | $\frac{1}{2}$ | 9,070 | 20,000 | 50.8 | 2 | 127,000 | 280,000 |
| 19.0 | $\frac{3}{4}$ | 20,860 | 46,000 | 63.5 | $2\frac{1}{2}$ | 207,740 | 458,000 |
| 25.4 | 1 | 34,470 | 76,000 | 69.9 | $2\frac{3}{4}$ | 249,350 | 550,000 |

TABLES 58 AND 59
MECHANICAL PROPERTIES
TABLE 58. — Aluminum

| Metal, approx. composition, per cent. | Condition. | Density or weight. | | P-limit. | Ultimate strength. | P-limit. | Ultimate strength. | Elong. in 50.8 mm (2 in.). | Reduct. of area. | Hardness. | |
|--|---|------------------------------|----------------------------|--------------------------------|-----------------------|--------------------------------|-----------------------|----------------------------------|---------------------|---------------------|-------------------|
| | | gm per cm ³ | lb. per ft ³ | Tension, kg/mm ² | | Tension, lb/in ² | | Per cent. | | Brinell @ 500 kg | Sclero- scope. |
| ALUMINUM: Av. Al 99.3 Imp., Fe and Si. . . | Cast, sand at 700° C. | 2.57 | 160.5 | 6.0 to 7.0 | 8.0 to 9.8 | 8,500 to 10,000 | 12,000 to 14,000 | 20 to 15 | 36 to 22 | 25 to 26 | 4 to 5 |
| | Cast, sand and heat treated Ann. 500° C, air cooled. | — | — | — | 8.9 to | — | 12,600 to | 28 to | 30 to | 25 to | 4 to |
| | Cast, chill. | — | — | — | 9.6 | — | 13,600 | 18 | 22 | 27 | 5 |
| | Sheet, ann. | 2.57 | 160.5 | 6.0 | 9.0 | 9,000 | 13,000 | 20.0 | — | 26 | 5 |
| | Sheet, hard. | 2.60 | 168.0 | 6.0 | 9.0 | 8,500 | 13,500 | 23.0 | 25.0 | — | — |
| | Bars, hard. | 2.70 | 168.5 | 14.0 | 21.0 | 20,000 | 30,000 | 4.0 | 25.0 | — | 14 |
| | Wire, hard. | 2.70 | 168.5 | 15.0 | 23.0 | 22,000 | 33,000 | — | 35.0 | — | — |
| | Wire, hard. | 2.70 | 168.5 | 21.0 | 28.0 | 30,000 | 40,000 | 6.0 | 50.0 | — | — |

Compressive strength: cast, yield point 13.0 kg/mm² or 18,000 lb/in²; ultimate strength 47.0 kg/mm² or 67,000 lb/in².

Modulus of elasticity: cast, 6900 kg/mm² or 9,810,000 lb/in² at 17° C.

TABLE 59. — Aluminum Sheet

(a) *Grade A (Al min. 99.0) Experimental Erichsen and Scleroscope Hardness Values.*

[From tests on No. 18 B. & S. Gage sheet rolled from 6.3 mm (0.25 in.) slab. Iron Age v. 101, page 957].

| Heat treatment annealed. | Thickness, mm | Indentation, mm | Scleroscope hardness. |
|-----------------------------|------------------|--------------------|--------------------------|
| None (as rolled) | 1.08 | 6.83 | 14.0 |
| @ 200° C, 2 hours | 1.09 | 8.86 | 8.0 |
| @ 300° C, 2 hours | 1.07 | 10.17 | 4.5 |
| @ 400° C, 2 hours | 1.08 | 9.40 | 4.5 |
| @ 200° C, 30 min. | 1.07 | 7.97 | 11.8 |
| @ 400° C, 30 min. | 1.08 | 9.80 | 4.5 |

(b) *Specification Values.* — (1) Cast: U. S. Navy 49 Al, July 1, 1915; Al min. 94, Cu max. 6, Fe max. 0.5, Si max. 0.5, Mn max. 3.

Minimum tensile strength 12.5 kg/mm² or 18,000 lb/in² with minimum elongation of 8 per cent in 50.8 mm (2 in.).

(2) Sheet, Grade A: A. S. T. M. 25 to 18T; Al min. 99.0; minimum strengths and elongations.

| Gage, sheet thicknesses. | | | Temper, No. hardness. | Tensile strength. | | Elong. in 50.8 mm or 2 in. per cent. | |
|--------------------------|-------------------|--------------------|---------------------------------------|---------------------|----------------------------|--|---|
| (B. & S.) | mm | in. | | kg/mm ² | lb/in ² | | |
| 12 to 16 incl. | 2.052 to 1.293 | 0.0808 to .0509 | 1 Soft, Ann. 2 Half-hard 3 Hard | 8.8 12.5 15.5 | 12,500 18,000 22,000 | 30 7 4 | Sheets of temper No. 1 to withstand being bent double in any direction and hammered flat; temper No. 2 to bend 180° about radius equal to thickness without cracking. |
| 17 to 22 incl. | 1.152 to 0.643 | .0453 to .0253 | 1 Soft, Ann. 2 Half-hard 3 Hard | 8.8 12.5 17.5 | 12,500 18,000 25,000 | 5 20 2 | |
| 23 to 26 incl. | 0.574 to 0.404 | .0226 to .0159 | 1 Soft, Ann. 2 Half-hard 3 Hard | 8.8 12.5 21.0 | 12,500 18,000 30,000 | 10 5 2 | |

NOTE. — Tension test specimen to be taken parallel to the direction of cold rolling of the sheet.

TABLE 60
MECHANICAL PROPERTIES
Aluminum Alloys

| Alloy, approx. composition per cent. | Condition, per cent reduction. | Density or weight. | | P-limit. | Ultimate strength. | P-limit. | Ultimate strength. | Elong. in 50.8 mm (2 in.). | Reduct. of area. | Hardness. | |
|---|--------------------------------------|------------------------|------------------------|-------------|-----------------------|------------------|-----------------------|----------------------------------|---------------------|------------------------|-------------------|
| | | gm/ cm ³ | lb/ ft ³ | | | | | | | Brinell (at 500 kg) | Sclero- scope. |
| Aluminum — Copper. | | | | | | | | | | | |
| Al 98 Cu 1 Imp. max. 1 | Cast, chill. | — | — | 5.3 | 10.5 | 7,500 | 15,000 | 24.0 | 34.0 | — | — |
| | Rolled, 70% | — | — | 10.0 | 21.0 | 27,000 | 30,000 | 4.0 | — | — | — |
| Al 96 Cu 3 Imp. max. 1 | Cast, chill. | — | — | 8.1 | 13.7 | 11,500 | 19,500 | 12.0 | 21.0 | — | — |
| | Rolled, 70% | — | — | 25.0 | 28.8 | 35,000 | 41,000 | 5.5 | — | — | — |
| Al 94 Cu 5 Imp. max. 1 | Cast, chill. | — | — | 10.0 | 15.0 | 14,500 | 21,500 | 7.0 | 14.0 | — | — |
| | Rolled, 70% | — | — | 23.0 | 27.0 | 33,000 | 38,000 | 6.0 | — | — | — |
| Al 92 Cu 8; Alloy No. 12. | Cast, sand. | 2.88 | 180 | 7.7 to 10.5 | 10.5 to 16.2 | 11,000 to 15,000 | 15,000 to 23,000 | 4.0 to None | 3.5 to None | 50 to 65 | 13 to 18 |
| Al 90-92 Cu 7-8.5 Imp. max. 1.7. | Cast* | 2.9 | 181 | — | 12.7 | — | 18,000 | 1.0 | — | — | — |
| Copper, Magnesium. | Cast at 700° C. | — | — | 3.2 to 4.6 | 0.6 to 13.3 | 4,500 to 6,500 | 13,600 to 18,900 | 2.0 to 0 | 0.5 to 0 | 74 to 80 | 17 to 21 |
| Al 9.52 Cu 4.2 Mg 0.6 | Ann. 500° C. | — | — | 4.6 | 17.3 | 6,500 | 24,900 | 3.0 | 1.0 | — | — |
| Duralumin or 17S Alloy Al 94 Cu 4 Mg 0.5. | Rolled 70% | 2.8 | 174 | 25.0 | 42.0 | 35,100 | 50,500 | 21.1 | 29.5 | — | — |
| | Rolled heat treated† | — | — | 53.0 | 50.0 | 75,400 | 79,000 | 4.0 | 13.2 | — | — |
| Copper, Manganese. | Cast, chill. | — | — | 23.4 | 39.0 | 33,400 | 55,300 | 25.5 | 26.0 | — | — |
| Al 96 Cu 2 Mn 2 | Rolled, 20 mm | — | — | 10.0 | 14.0 | 14,300 | 20,300 | 5.0 | — | — | — |
| Al 96 Cu 3 Mn 1 | Cast, chill. | — | — | 19.0 | 27.0 | 27,100 | 38,200 | 10.0 | 28.0 | — | — |
| Naval Gun Factory. | Cast, sand. | 2.8 | 175 | 11.3 | 19.0 | 10,200 | 27,000 | 14.0 | — | — | — |
| Al 97 Cu 1.5 Mn 1. | Forged | — | — | — | 14.0 | — | 20,000 | 12.0 | — | — | — |
| Al 94 Cu max. 6 Mn max. 3 | Minimum ‡ | — | — | 14.0 | 19.0 | 19,500 | 27,800 | 12.0 | 47.0 | — | — |
| Copper, Nickel, Mg Mn. | Cast at 700° C. | — | — | — | 12.7 | — | 18,000 | 8.0 | — | — | — |
| Al 93.5 Cu 3.5 Ni 1.5 Mg 1 Mn 0.5. | — | — | — | 3.5 to 0.8 | 17.9 to 23.2 | 5,000 to 14,000 | 25,500 to 33,000 | 6.0 to 1.5 | 8.5 to 1.0 | 54 to 86 | 9 to 25 |
| Copper, Nickel Mn. | Cast at 700° C. | — | — | — | 14.5 to 21.4 | — | 20,600 to 30,500 | 6.0 to 1.0 | 11.0 to 2.0 | 50 to 91 | 9 to 27 |
| Al 94.2 Cu 3 Ni 2 Mn 0.8. | — | — | — | — | — | — | — | — | — | — | — |
| Magnesium: | | | | | | | | | | | |
| Magnalium Al 95 Mg 5 | Cast, sand | 2.5 | 156 | 5.6 | 15.5 | 8,000 | 22,000 | 7.0 | 8.5 | — | — |
| Al 77-98, Mg 23-2. | Cast, chill. | 2.4 to 2.57 | 150 to 160 | — | 20.5 to 45.0 | — | 42,000 to 64,000 | — | — | — | — |
| Nickel Al 97 Ni 2. | Cast, chill. | — | — | 4.0 | 11.0 | 5,800 | 14,900 | 21.0 | 36.0 | — | — |
| | Drawn, cold. | — | — | 14.0 | 16.0 | 19,700 | 22,700 | 13.0 | 37.0 | — | — |
| | Rolled, hot. | — | — | 8.0 | 13.0 | 11,900 | 18,200 | 28.0 | 52.0 | — | — |
| | Cast, chill. | — | — | 6.0 | 15.0 | 9,000 | 21,700 | 9.0 | 11.0 | — | — |
| Al 95 Ni 5. | Drawn, cold. | — | — | 16.0 | 20.0 | 22,900 | 27,900 | 8.0 | 24.0 | — | — |
| | Rolled, hot. | — | — | 9.0 | 16.0 | 13,500 | 22,300 | 22.0 | 36.0 | — | — |
| Nickel Copper: | | | | | | | | | | | |
| Al 93.5 Ni 5.5 Cu 1. | Cast, chill. | — | — | 7.0 | 17.0 | 10,700 | 24,800 | 6.0 | 8.0 | — | — |
| Al 91.5 Ni 4.5 Cu 4. | Cast, chill. | — | — | 7.0 | 18.0 | 9,900 | 25,200 | 4.0 | 5.0 | — | — |
| Al 92 Ni 5.5 Cu 2. | Drawn, cold. | — | — | 22.0 | 27.0 | 31,700 | 37,800 | 8.0 | 15.0 | — | — |
| | Rolled, hot. | — | — | 13.0 | 22.0 | 18,200 | 31,500 | 16.0 | 24.0 | — | — |
| Zinc, Copper: | | | | | | | | | | | |
| Al 88.6 Cu 3 Zn 8.4. | Cast at 700° C. | — | — | 4.7 | 18.5 | 6,700 | 26,300 | 8.0 | 7.5 | 50 | 10 |
| | Ann. 500° C. | — | — | 4.4 | 20.2 | 6,200 | 28,800 | 8.0 | 7.5 | 50 | 10 |
| Al 81.1 Cu 3 Zn 15.9. | Cast at 700° C. | 3.1 | 193 | 9.8 | 24.7 | 14,000 | 35,100 | 2.0 | 2.0 | 74 | 15 |
| | Ann. 500° C. | — | — | 9.8 | 20.0 | 14,000 | 41,200 | 4.0 | 4.0 | 70 | 15 |

* Specification Values: Alloy "No. 12": A. S. T. M. B26-18T, tentative specified minimums for aluminum, copper.
† Quenched in water from 475° C after heating in a salt bath. Modulus of elasticity for Duralumin averages 7000 kg/mm² or 10,000,000 lb/in².
‡ Specification values: Aluminum castings; U. S. Navy 49 Al, July 1, 1915 (Impurities: Fe max. 0.5, Si max. 0.5)

MECHANICAL PROPERTIES

TABLE 61. — Copper

| Metal and approx. composition. Per cent. | Condition. | Density or weight. | | P-limit. | | P-limit. | | Elong. in 50.8 mm (2 in.). | | Hardness. | |
|--|-------------------------------------|--------------------|--------------------|-----------------------------|--------------------|-----------------------------|--------------------|----------------------------|------------------|------------------|---------------|
| | | gm/cm ³ | lb/ft ³ | Tension, kg/mm ² | Ultimate strength. | Tension, lb/in ² | Ultimate strength. | Per cent. | Reduct. in area. | Brinell @ 500 kg | Sclero-scope. |
| | | | | | | | | | | | |
| Copper: | | | | | | | | | | | |
| 99.9: electrolytic | Ann. 200° C..... | 8.89 | 555 | 6.0 | 27.0 | 8,500 | 38,000 | 50.0 | 50.0 | 40 | 7 |
| Cu 99.0..... | Cast..... | 8.85 | 552 | 7.0 | 18.0 | 10,000 | 25,000 | 20.0 | 60.0 | 80 | 8 |
| | Hard, 40% reduct | 8.89 | 555 | 14.0 | 35.0 | 20,000 | 50,000 | 5.0 | 8.0 | 94 | — |
| Rolled..... | Ann. at 500° C..... | 8.90 | 556 | indet. | 25.0 | indet. | 35,000 | 50.0 | 60.0 | 42 | 6 |
| Cu 99.6..... | Drawn cold, 50% reduct..... | — | — | 26.0 | 35.0 | 37,000 | 50,000 | 9.0 | — | — | 18 |
| Cu 99.9*..... | No Ann. (96% reduction)..... | — | — | — | 47.3 | — | 67,400 | 0.8 | 64.5 | — | — |
| | Ann. 750° C after drawing cold..... | — | — | — | 21.9 | — | 31,200 | 24.5 | 76.0 | — | — |
| Cu 99.9†..... | Drawn hot (64% reduction)..... | — | — | — | 33.0 | — | 46,800 | 4.3 | 70.5 | — | — |

* Wire drawn cold from 3.18 mm (0.125 in.) to 0.64 mm (0.025 in.) Bull. Am. Inst. Min. Eng., Feb., 1919.

† Wire drawn at 150° C from 0.79 mm (0.031 in.) to 0.64 mm (0.025 in.) (Jeffries, *loc. cit.*).

Compression, cast copper, Ann. 15.0 mm (0.625 in.) diam. by 50.8 mm (2 in.) long cylinders.

Shortened 5 per cent at 22.0 kg/mm² or 31,300 lb/in² load.

" 10 " " 29.0 kg/mm² " 41,200 lb/in² " "

" 20 " " 39.0 kg/mm² " 55,400 lb/in² " "

Shearing strength, cast copper 21.0 kg/mm² or 30,000 lb/in²

Modulus of elasticity, electrolytic 12,200 kg/mm² or 17,400,000 lb/in²

" " " cast 7,700 kg/mm² or 11,000,000 lb/in²

" " " drawn, hard 12,400 kg/mm² or 17,600,000 lb/in²

TABLE 62. — Rolled Copper — Specification Values

Specification values: U. S. Navy Dept., 47C2, minimums for rolled copper, — Cu min. 99.5

| Description, temper and thickness. | Tensile strength. | | Elong. in 50.8 or 2 in. — per cent. |
|---------------------------------------|--------------------|--------------------|-------------------------------------|
| | kg/mm ² | lb/in ² | |
| Rods, bars, and shapes: | | | |
| Soft..... | 21.0 | 30,000 | 25 |
| Hard: to 9.5 mm (3/8 in.) incl..... | 35.0 | 50,000 | 10 |
| Hard: 9.5 mm to 25.4 mm (1 in.)..... | 31.5 | 45,000 | 12 |
| Hard: 25.4 mm to 50.8 mm (2 in.)..... | 28.0 | 40,000 | 15 |
| Hard: over 50.8 mm (2 in.)..... | 24.5 | 35,000 | 20 |
| Sheets and plates: | | | |
| Soft..... | 21.0 to 28.0 | 30,000 to 40,000 | 25 to 25 |
| Hard..... | 24.5 | 35,000 | 18 |

TABLE 63. — Copper Wire — Specification Values

Specific Gravity 8.89 at 20° C (68° F).

Copper wire: Hard Drawn (and Hard-rolled flat copper of thicknesses corresponding to diameters of wire) Specification values. (A. S. T. M. B1-15, and U. S. Navy Dept., 22W3, Mar. 1, 1915.)

| Diameter. | | Minimum tensile strength. | | Maximum elongation, per cent in 254 mm (10 in.). |
|-----------|------|---------------------------|--------------------|--|
| mm | in. | kg/mm ² | lb/in ² | |
| 11.68 | .460 | 34.5 | 49,000 | 2.75 |
| 10.41 | .410 | 35.9 | 51,000 | 3.25 |
| 9.27 | .365 | 37.1 | 52,800 | 2.80 |
| 8.25 | .325 | 38.3 | 54,500 | 2.40 |
| 7.34 | .289 | 39.4 | 56,100 | 2.17 |
| 6.35 | .253 | 40.5 | 57,600 | 1.98 |
| 5.82 | .229 | 41.5 | 59,000 | 1.79 |
| 5.18 | .204 | 42.2 | 60,100 | 1.24 |
| 4.62 | .182 | 43.0 | 61,200 | 1.18 |
| 4.12 | .162 | 43.7 | 62,100 | 1.14 |
| 3.66 | .144 | 44.3 | 63,000 | 1.09 |
| 3.25 | .128 | 44.8 | 63,700 | 1.06 |
| 2.90 | .114 | 45.2 | 64,300 | 1.02 |
| 2.59 | .102 | 45.7 | 64,900 | 1.00 |
| 2.31 | .091 | 46.0 | 65,400 | 0.97 |
| 2.06 | .081 | 46.2 | 65,700 | 0.95 |
| 1.83 | .072 | 46.3 | 65,900 | 0.92 |
| 1.63 | .064 | 46.5 | 66,200 | 0.90 |
| 1.45 | .057 | 46.7 | 66,400 | 0.89 |
| 1.30 | .051 | 46.8 | 66,600 | 0.87 |
| 1.14 | .045 | 47.0 | 66,800 | 0.86 |
| 1.02 | .040 | 47.1 | 67,000 | 0.85 |

P-limit of hard-drawn copper wire must average 55 per cent of ultimate tensile strength for four largest sized wires in table, and 60 per cent of tensile strength for smaller sizes.

MECHANICAL PROPERTIES

Table 64. — Copper Wire — Medium Hard-drawn

(A. S. T. M. B2-15) Minimum and Maximum Strengths.

| Diameter. | | Tensile strength. | | | | Elongation, minimum per cent in 254 mm (10 in.). |
|-----------|-------|--------------------|--------------------|--------------------|--------------------|--|
| | | Minimum. | | Maximum. | | |
| mm | in | kg/mm ² | lb/in ² | kg/mm ² | lb/in ² | |
| 11.70 | 0.460 | 29.5 | 42,000 | 34.5 | 49,000 | 3.75 |
| 6.55 | .258 | 33.0 | 47,000 | 38.0 | 54,000 | 2.50 |
| 4.12 | .162 | 34.5 | 49,000 | 39.5 | 56,000 | in 1524 mm (60 in.) |
| 2.59 | .102 | 35.5 | 50,330 | 40.5 | 57,330 | 1.15 |
| 1.02 | .040 | 37.0 | 53,000 | 42.0 | 60,000 | 1.04 |
| | | | | | | 0.88 |

Representative values only from table in specifications are shown above.
P-limit of medium hard-drawn copper averages 50 per cent of ultimate strength.

TABLE 65. — Copper Wire — Soft or Annealed

(A. S. T. M. B3-15) Minimum Values.

| Diameter. | | Minimum tensile strength. | | Elongation in 254 mm (10 in.), per cent. |
|---------------|----------------|---------------------------|--------------------|---|
| mm | in. | kg/mm ² | lb/in ² | |
| 11.70 to 7.37 | 0.460 to 0.290 | 25.5 | 36,000 | 35 |
| 7.34 to 2.62 | 0.289 to 0.103 | 26.0 | 37,000 | 30 |
| 2.59 to 0.53 | 0.102 to 0.021 | 27.0 | 38,500 | 25 |
| 0.51 to 0.08 | 0.020 to 0.003 | 28.0 | 40,000 | 20 |

NOTE. — Experimental results show tensile strength of concentric-lay copper cable to approximate 90 per cent of combined strengths of wires forming the cable.

TABLE 66. — Copper Plates

(A. S. T. M. B11-18) for Locomotive Fire Boxes. Specification Values.

| Minimum requirements. | Tensile strength. | | Elong. in 203.2 mm (8 in.), per cent. |
|---------------------------------|--------------------|--------------------|--|
| | kg/mm ² | lb/in ² | |
| Copper, Arsenical, As 0.25-0.50 | | | |
| Impurities, max. 0.12..... | 22.0 | 31,000 | 35 |
| Copper, Non-arsenical: | | | |
| Impurities, max. 0.12..... | 21.0 | 30,000 | 30 |

NOTE. — Copper to be fire-refined or electrolytic, hot-rolled from suitable cakes.

TABLE 67. — Copper Alloys

The general system of nomenclature employed has been to denominate all simple copper-zinc alloys as **brasses**, copper-tin alloys as **bronzes**, and three or more metals alloys composed primarily of either of these two combinations as alloy brasses or bronzes, e.g., "Zinc bronze" for U. S. Government composition "G" Cu 88 per cent, Sn 10 per cent, Zn 2 per cent. Alloys of the third type noted above, together with other alloys composed mainly of copper, have been called **copper alloys**, with the alloying elements other than minor impurities listed as modifying copper in the order of their relative percentages.

In some instances, the scientific name used to denote an alloy is based upon the deoxidizer used in its preparation, which may appear either as a minor element of its composition or not at all, e.g., phosphor bronze.

Commercial names are shown below the scientific names. Care should be taken to specify the chemical composition of a commercial alloy, as the same name frequently applies to widely varying compositions.

MECHANICAL PROPERTIES

Copper Alloys — Copper-Zinc or Brasses; Copper-Tin or Bronzes

| Metal and approx. composition, per cent. | Condition. | Density or weight. | | P-limit. | Ultimate strength. | P-limit. | Ultimate strength. | Elong. in 59.8 mm (2 in.). | Reduct. in area. | Hardness. | | | | |
|--|---------------------------------------|--------------------|--------------------|----------|--------------------|----------|--------------------|----------------------------|------------------|-----------------------------|-----------------------------|-----------|------------------|---------------|
| | | gm cm ³ | lb ft ³ | | | | | | | Tension. kg/mm ² | Tension. lb/in ² | Per cent. | Brinell @ 500 kg | Sclero-scope. |
| | | | | | | | | | | | | | | |
| Brass: | | | | | | | | | | | | | | |
| Cu 90 Zn 10†. | Sand cast..... | — | — | — | 20.0 | — | 29,000 | 22 | — | — | — | | | |
| | Cold rolled, hard | — | — | — | 39.0 | — | 55,000 * | 5 * | — | 60 | 20 | | | |
| | Cold rolled, soft. | 8.7 | 543 | — | 26.0 | — | 37,000 * | 40 * | 70 | 47 | 10 | | | |
| Cu 80, Zn 20 ‡. | Sand cast..... | — | — | — | 25.0 | — | 35,000 | 31 | 32 | — | — | | | |
| | Cold rolled, hard | — | — | — | 53.0 | — | 75,000 * | 5 * | — | 75 | 28 | | | |
| | Cold rolled, soft. | 8.6 | 537 | — | 29.0 | — | 42,000 * | 50 * | 85 | 46 | 12 | | | |
| Cu 70, Zn 30. | Sand cast..... | 8.4 | 524 | — | 28.0 | — | 40,000 | 35 | — | 37 | — | | | |
| Cu 66 Zn 34 Std. sheet | Cold rolled, hard | 8.5 | 530 | — | 42.0 | — | 60,000 | 5 * | — | 75§ | 26 | | | |
| | Cold rolled, soft. | 8.4 | 524 | — | 34.0 | — | 48,000 * | 50 * | 85 | 45 | 12 | | | |
| Cu 60, Zn 40... Muntz metal... | Sand cast..... | — | — | 15.5 | 32.2 | 21,800 | 45,800 | 15 | 22 | — | — | | | |
| | Cold rolled, hard | 8.4 | 522 | 31.5 | 49.0 | 45,000 | 70,000 | 30 | 50 | — | — | | | |
| Bronze: | | | | | | | | | | | | | | |
| Cu 97.7, Sn 2.3. | Cast..... | — | — | 6.0 | 19.5 | 8,500 | 28,000 | 20 | — | — | — | | | |
| | Rolled..... | — | — | 7.6 | 34.0 | 10,800 | 48,000 | 55 | 75 | — | — | | | |
| Cu 90, Sn 10... | Cast or gun bronze or bell metal..... | 8.78 | 548 | 7.2 | 23.0 | 10,300 | 33,000 | 10 | — | — | 23 | | | |
| Cu 80, Sn 20... | Cast..... | 8.81 | 550 | 7.1 | 22.5 | 10,100 | 32,000 | 1.5 | — | — | — | | | |
| Cu 70, Sn 30... | Cast..... | 8.84 | 552 | 1.4 | 5.0 | 2,000 | 7,000 | 0.5 | — | — | — | | | |

Compressive Strengths, Brasses:

Cu 90, Zn 10, cast 21.0 kg/mm² or 30,000 lb/in²
 Cu 80, Zn 20, cast 27.4 kg/mm² or 39,000 lb/in²
 Cu 70, Zn 30, cast 42.0 kg/mm² or 60,000 lb/in²
 Cu 60, Zn 40, cast 52.5 kg/mm² or 75,000 lb/in²
 Cu 50, Zn 50, cast 77.0 kg/mm² or 110,000 lb/in²

Modulus of elasticity, — cast brass, — average 9100 kg/mm² or 13,000,000 lb/in²

Erichsen values: Soft slab, 1.3 mm (0.05 in.) thick, no rolling, depth of impression 13.8 mm (0.55 in.).

Hard sheet, 1.3 mm, rolled 38% reduction, depth of impression 7.3 mm (0.29 in.).

Hard sheet, 0.5 mm, rolled 60% reduction, depth of impression 3.7 mm (0.15 in.).

Compressive Ultimate Strengths, Cast Bronzes:

Cu 97.7, Sn 2.3 to 24.0 kg/mm² or 34,000 lb/in²
 Cu 90, Sn 10 to 30.0 kg/mm² or 50,000 lb/in²
 Cu 80, Sn 20 to 83.0 kg/mm² or 118,000 lb/in²
 Cu 70, Sn 30 to 105.0 kg/mm² or 150,000 lb/in²

Specification value, A. S. T. M., B 22-18 T, for specimen = cylinder 645 sq. mm (1 sq. in.) area, 25.4 mm (1 in.) long.

Cu 80, Sn 20: minimum compressive elastic limit = 17.0 kg/mm² or 24,000 lb/in²

Modulus of elasticity for bronzes varies from 7000 kg/mm² or 10,000,000 lb/in² to 10,000 kg/mm² or 15,500,000 lb/in²

* Values marked thus are S. A. E. Spec. values. (See S. A. E. Handbook, Vol. I, p. 13a, rev. December, 1913.)
 † Red metal. ‡ Low brass or bell metal.

§ A. S. T. M. Spec. Br9-18T requires B.h.n. of 51-65 kg/mm² @ 5000 kg pressure for 70: 30 annealed sheet brass.

FOOT NOTES TO TABLE 69, PAGE 121

* Tensile, Cu 67, Zn 24, Al 4.4, Mn 3.8, P 0.01 compressive P-limit: 42.2 kg/mm² or 60,000 lb/in² and 1.33 per cent set for 70.3 kg/mm² or 100,000 lb/in² load.

† Compressive P-limit 20.0 to 28.2 kg/mm² or 28,500 to 40,000 lb/in²

‡ Compressive ultimate strength 54.5 kg/mm² or 77,500 lb/in²

§ Compressive P-limit 4.2 kg/mm² or 6000 lb/in² and 40 per cent set for 70.3 kg/mm² or 100,000 lb/in²

* Modulus of elasticity 9340 kg/mm² or 14,000,000 lb/in²

|| Values are for yield point. ** Minimum values for ingots.

†† Rolled manganese bronze (U. S. N.) Cu 57 to 60, Zn 40 to 37, Fe max. 2.0, Sn 0.5 to 1.5; 2.9 per cent increase for thickness 25.4 mm (1 in.) and under.

‡‡ Ni 9 per cent, B.h.n. = 130 as rolled; B.h.n. = 50 as annealed at 930° C.

U. S. Navy Dept. Spec. 46S 3a, June 1, 1917: German silver Cu 60 to 67, Zn 18 to 22, Ni min. 15, no mechanical requirements.

For list of 30 German silver alloys, see Braunt, "Metallic Alloys," p. 314, — "best" (Hiorns), "hard Sheffield," Cu 46, Zn 20, Ni 34.

§§ Platinum Cu 60, Zn 24, Ni 14, W 1 to 2; high electric resistance alloy with mechanical properties as nickel brass

||| Specification Values, Naval Brass Castings, U. S. Navy, 46B 10b, Dec. 1, 1917, for normal proportions Cu 62, Zn 37, Sn 1, min. tensile strength 17.5 kg/mm² or 25,000 lb/in² with 15 per cent elongation in 50.8 mm (2 in.).

MECHANICAL PROPERTIES

Copper Alloys — Three (or more) Components

| Alloy and approx. composition per cent. | Condition. | Density or weight. | | P-limit. | Ultimate strength. | P-limit. | Ultimate strength. | Elong. in 50.8 mm (2 in.). | Reduct. of area. | Hardness. | |
|---|-------------------------|------------------------------|--------------------------------|--------------|-----------------------|------------------|-----------------------|----------------------------------|---------------------|---------------------|-------------------|
| | | gm per cm ³ | lb. per in. ³ | | | | | | | Brinell @ 500 kg | Sclero- scope. |
| Brass, Aluminum. | Cast | — | — | — | 40.0 | — | 57,000 | 50.0 | — | — | — |
| Cu 57, Zn 42, Al 1... | | — | — | — | 00.0 | — | 85,400 | 16.5 | — | — | — |
| Cu 55, Zn 41, Al 4... | | — | — | — | 56.2 | — | 80,000 | — | — | — | — |
| Cu 62.9, Zn 33.3, Al 3.8 | | — | — | — | 33.0 | — | 47,000 | 50.0 | — | — | — |
| Cu 70.5, Zn 26.4, Al 3.1 | | — | — | 13.4 | 33.0 | 10,000 | 47,000 | 50.0 | — | — | — |
| Alum., Manganese. | Cast, tensile* | — | — | — | — | — | — | — | — | — | — |
| Cu 64, Zn 29, Al 3.1, Mn 2.5, Fe 1.2... | | — | — | 21.1 | 68.8 | 30,000 | 98,000 | 16.0 | 17.0 | 130 | — |
| Alum., Vanadium. | | — | — | — | — | — | — | — | — | — | — |
| Cu 58.5, Zn 38.5, Al 1.5, V 0.03... | | — | — | — | — | — | — | — | — | — | — |
| Iron: | | — | — | — | — | — | — | — | — | — | — |
| Cu 56, Zn 41.5, Fe 1. | Cast..... | — | — | — | 50.7 to 59.2 | — | 72,000 to 84,000 | 35.0 to 22.0 | 35.0 to 25.0 | 100 to 119 | — |
| Aich's Metal | | — | — | — | — | — | — | — | — | — | — |
| Cu 60, Zn 38.2, Fe 1.8 | Cast..... | 8.42 | 526 | — | 40.3 | — | 57,300 | — | — | — | — |
| Delta Metal | | — | — | — | — | — | — | — | — | — | — |
| Cu 57, Zn 42, Fe 1... | Cast, sand..... | — | — | — | 31.7 | — | 45,000 | 10.0 | — | — | — |
| Cu 65, Zn 30, Fe 5... | Rolled, hard..... | — | — | — | 42.2 | — | 60,000 | 17.0 | — | — | — |
| | Rolled hard..... | — | — | — | 45.5 | — | 65,000 | — | — | — | — |
| Iron, Tin: | | — | — | — | — | — | — | — | — | — | — |
| Cu 56.5, Zn 40, Fe 1.5, Sn 1.0... | Cast..... | — | — | 23.2 to 26.0 | 49.2 to 52.8 | 33,000 to 37,000 | 70,000 to 75,000 | 35.0 to 20.0 | 35.0 to 22.0 | 104 to 119 | — |
| Sterro metal: | | — | — | — | — | — | — | — | — | — | — |
| Cu 55, Zn 42.4 Fe 1.8, Sn 0.8... | Cast..... | 8.4 | 525 | — | 42.5 | — | 60,500 | — | — | — | — |
| | Forged..... | — | — | — | 53.6 | — | 76,200 | — | — | — | — |
| | Hard drawn..... | — | — | — | 58.5 | — | 83,100 | — | — | — | — |
| Lead or Yellow brass | Cast..... | 8.5 | 531 | — | 23.2 to 27.5 | — | 33,000 to 39,000 | 30.0 to 26.0 | 35.0 to 30.0 | — | — |
| Cu 60 to 63.5, Zn 35 to 33.5, Pb 5 to 3... | Sheet ann..... | — | — | — | 25.5 | — | 42,000 | 50.0 | — | — | — |
| | Sheet hard..... | — | — | — | 42.9 | — | 61,000 | 30.0 | — | — | — |
| Lead, Tin or | | — | — | — | — | — | — | — | — | — | — |
| Red brass: | | — | — | — | — | — | — | — | — | — | — |
| Cu 83, Zn 7, Pb 6, Sn 4 | Cast..... | 8.6 | 535 | 11.0 | 21.0 | 16,000 | 30,000 | 17.0 | 19.0 | — | 7.0 |
| Cu 78, Zn 9.5, Pb 10, Sn 2... | Cast..... | 8.87 | 554 | 8.4 | 18.6 | 12,000 | 26,500 | 22.0 | 24.9 | — | — |
| Yellow brass: | | — | — | — | — | — | — | — | — | — | — |
| Cu 70, Zn 27, Pb 2, Sn 1... | Cast §..... | 8.4 | 524 | 7.4 | 20.7 | 10,500 | 29,500 | 25.0 | 28.5 | 53.0 | — |
| Manganese or Manganese bronze | | — | — | — | — | — | — | — | — | — | — |
| Cu 58, Zn 39, Mn 0.05 | Cast, sand §..... | 8.3 | 520 | 21.1 to 24.6 | 49.2 to 52.7 | 30,000 to 35,000 | 70,000 to 75,000 | 30.0 to 22.0 | 32.0 to 25.0 | 109 to 119 | 18 to 19 |
| (Sn, Fe, Al, Pb.) | Cast, chill..... | — | — | 22.5 to 26.0 | 52.7 to 56.3 | 32,000 to 37,000 | 75,000 to 80,000 | 32.0 to 25.0 | 34.0 to 28.0 | 119 to 130 | 20 to 22 |
| Cu 60, Zn 39 Mn, tr | Rolled..... | 8.3 | 520 | 31.5 | 52.5 | 45,000 | 75,000 | 25.0 | 28.0 | — | 30 |
| Specification values: | | — | — | — | — | — | — | — | — | — | — |
| U. S. Navy, 46 B 16a ** | | — | — | — | 49.2 | — | 70,000 | 20.0 | — | — | — |
| U. S. N., 46 B 15a | Rolled††..... | — | — | 24.6 | 49.2 | 35,000 | 70,000 | 30.0 | — | — | — |
| Manganese Vanadium: | | — | — | — | — | — | — | — | — | — | — |
| Cu 58.6, Zn 38.5, Al 1.5 Mn 0.5, V 0.03 | Cold drawn..... | — | — | 35.6 | 57.0 | 50,600 | 81,400 | 12.0 | 14.0 | — | — |
| Nickel: Nickel silver, | | — | — | — | — | — | — | — | — | — | — |
| Cu 60.4, Zn 31.8, Ni 7.7... | Cast..... | 8.5 | 530 | 10.8 | 25.3 | 15,400 | 36,000 | 40.5 | 42.0 | 46 | — |
| German silver, | | — | — | — | — | — | — | — | — | — | — |
| Cu 61.6, Zn 17.2, Ni 21.1... | | 8.7 | 544 | 13.2 | 28.8 | 18,800 | 40,900 | 28.5 | 25.1 | 80 | — |
| Cu 60.6, Zn 11.8, Ni 27.3... | | 8.8 | 547 | 16.7 | 37.6 | 23,700 | 53,500 | 32.0 | 31.4 | 67 | — |
| Fine wire: | | — | — | — | — | — | — | — | — | — | — |
| Cu 58, Zn 24, Ni 18 | Drawn hard..... | 8.5 | 530 | — | 105.5 | — | 150,000 | — | — | — | — |
| Nickel Tungsten: §§ | | — | — | — | — | — | — | — | — | — | — |
| Tin: | | — | — | — | — | — | — | — | — | — | — |
| Cu 61, Zn 38, Sn 1... | Cast, sand..... | — | — | 11.0 | 30.0 | 15,700 | 42,600 | 20.6 | 32.0 | — | — |
| Naval brass, as above | | — | — | — | — | — | — | — | — | — | — |
| | Ann. after rolling..... | — | — | 26.0 | 43.5 | 37,000 | 62,000 | 25.0 | 37.0 | — | — |
| | Cast..... | 8.3 | 518 | 17.6 | 42.2 | 25,000 | 60,000 | — | — | — | — |
| Tobin bronze: as below | | — | — | — | — | — | — | — | — | — | — |
| Cu 58.2, Zn 39.5, Sn 2.3... | Rolled..... | 8.4 | 524 | 38.0 | 56.0 | 54,000 | 79,000 | 35.0 | 40.0 | — | — |
| Cu 55, Zn 43, Sn 2 | Cast | — | — | — | 48.4 | — | 68,900 | 48.0 | 70.0 | — | — |

For Footnotes see page 120.

MECHANICAL PROPERTIES

Copper Alloys — Three (or more) Components

| Alloy and approx. composition per cent. | Condition. | Density or weight. | | P-limit. | Ultimate strength. | P-limit. | Ultimate strength. | Elong. in 50.8 mm (2 in.). | Reduct. of area. | Hard- ness. | |
|---|---------------------------|------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|-----------------------|----------------------------------|---------------------|--|-----|
| | | gm per cm ³ | lb. per in. ³ | Tension, kg/mm ² | Tension, lb/in ² | Tension, lb/in ² | Per cent. | Brimell (@ 500 kg.) | Sclero- scope. | | |
| | | | | | | | | | | | |
| Brass, Tin — (continued): | | | | | | | | | | | |
| Rods: * 0 to 12.7 mm ($\frac{1}{2}$ in.) | | — | — | 19.0 | 42.2 | 27,000 | 60,000 | 35.0 | | To bend 120° cold about radius equal to diameter. | |
| 12.7 to 25.4 mm (1 in.) | | — | — | 18.3 | 40.8 | 26,000 | 58,000 | 40.0 | | | |
| over 25.4 mm (in.) diam. | | — | — | 17.6 | 38.0 | 25,000 | 54,000 | 40.0 | | | |
| Shapes, all | | — | — | 15.7 | 30.4 | 22,400 | 56,000 | 30.0 | | | |
| Plates to 12.7 mm ($\frac{1}{2}$ in.) | | — | — | 19.3 | 38.7 | 27,500 | 55,000 | 32.0 | | | |
| over 12.7 mm ($\frac{1}{2}$ in.) thick | | — | — | 17.6 | 39.4 | 25,000 | 56,000 | 35.0 | | | |
| Tubing (wall thickness) 0 to | | | | | | | | | | | |
| 3.2 mm ($\frac{1}{8}$ in.) | | — | — | 21.1 | 42.2 | 30,000 | 60,000 | 28.0 | — | | — |
| 3.2 to 6.4 mm ($\frac{1}{4}$ in.) | | — | — | 19.7 | 38.7 | 28,000 | 55,000 | 32.0 | — | | — |
| over 6.4 mm ($\frac{1}{4}$ in.) | | — | — | 18.3 | 35.1 | 26,000 | 50,000 | 35.0 | — | | — |
| Vanadium: | | | | | | | | | | | |
| Victor bronze, | | | | | | | | | | | |
| V 0.03, Cu 58.6, Zn 38.5, | Cold drawn | — | — | 56.5 | 64.5 | 80,000 | 92,000 | 11.5 | 29.0 | — | — |
| Al 1.5, Fe 1.0 | | | | | | | | | | | |
| U. S. Navy 49 B 1b. | | — | — | 15.8 | 38.7 | 22,500 | 55,000 | 25.0 | — | — | — |
| Bronze, Aluminum. | | | | | | | | | | | |
| Lead: | | | | | | | | | | | |
| Cu 89, Sn 10, Pb 1 | Cast † | — | — | — | 15.5 | — | 22,000 | — | — | — | — |
| Cu 88, Sn 10, Pb 2 | Cast ‡ | — | — | 13.4 to | 21.1 to | 19,000 to | 30,000 to | 20.0 to | 26.0 to | 65 to | — |
| | | | | 10.2 | 24.6 | 23,000 | 35,000 | 15.0 | 18.0 | 70 | — |
| Cu 80, Sn 10, Pb 10 | { Cast, sand. | 8.8 | 540 | 10.9 | 22.1 | 15,500 | 31,400 | 13.5 | 12.0 | 63 | — |
| | { Cast, chill. | — | — | 12.8 | 24.7 | 18,200 | 35,200 | 4.5 | 3.5 | 85 | — |
| Lead, Phosphor: | | | | | | | | | | | |
| Cu 80, Sn 10, Pb 10, P trace | Cast | 9.1 | 570 | 11.0 | 21.0 | 16,000 | 30,000 | 6.0 | 3.5 | 65 | 12 |
| Lead Zinc, Red brass: | | | | | | | | | | | |
| Cu 81, Sn 7, Pb 9, Zn 3 | Cast † | 8.9 | 555 | 13.4 to | 21.1 to | 19,000 to | 30,000 to | 18.0 to | 24.0 to | 50 to | 8.0 |
| | | | | 14.1 | 24.6 | 20,000 | 35,000 | 15.0 | 22.0 | 55 | — |
| Cu 88, Sn 8, Pb 2, Zn 2 | Cast | — | — | — | 21.8 to | — | 31,000 to | 20.0 to | — | 57 to | — |
| | | | | | 26.0 | — | 37,000 | 16.0 | — | 59 | — |
| Lead, Zinc Phosphor: | | | | | | | | | | | |
| Cu 73.2, Sn 11.3, Pb 12.0, | | | | | | | | | | | |
| Zn 2.5, P 1 | Cast ** | — | — | 10.5 | 21.4 | 15,000 | 30,400 | 4.0 | 3.3 | — | 11 |
| Manganese: | | | | | | | | | | | |
| Cu 88, Sn 10, Mn 2 | Cast | — | — | 9.0 | 19.1 | 12,800 | 27,200 | 25.0 | — | — | — |
| Nickel, Zinc: | | | | | | | | | | | |
| Cu 88, Sn 5, Ni 5, Zn 2 (1) | Cast †† | — | — | 9.2 | 28.6 | 13,100 | 40,700 | 32.0 | 28.0 | — | — |
| Cu 89, Sn 4, Ni 4, Zn 3 (2) | Cast †† | — | — | 8.1 | 27.9 | 11,500 | 30,700 | 31.0 | 31.0 | — | — |
| Phosphor: | | | | | | | | | | | |
| Cu 95, Sn 4.9, P 0.1 | Rollled | 8.6 | 535 | 28.0 | 46.0 | 40,000 | 65,000 | 30.0 | — | — | 37 |
| Cu 89, Sn 10.5, P 0.5 | Cast | — | — | 11.2 to | 21.8 to | 16,000 to | 31,000 to | 6.0 to | — | 72 to | — |
| Cu 80, Sn 20, P max. 1 | Cast †† | — | — | 14.1 | 24.6 | 20,000 | 35,000 | 10.0 | — | 77 | — |
| Rods and bars §§ up to 12.7 | | | | | | | | | | | |
| mm ($\frac{1}{2}$ in.) | | — | — | 42.2 | 56.2 | 60,000 | 80,000 | 12.0 | | Required to bend cold through 120° about radi- us equal to thickness. | |
| (minimum) over 12.7 mm | | — | — | 28.1 | 42.2 | 40,000 | 60,000 | 20.0 | | | |
| to 25.4 mm (1 in.) | | — | — | 21.1 | 38.7 | 30,000 | 55,000 | 25.0 | | | |
| over 25.4 mm (1 in.) | | — | — | | | | | | | | |
| Sheets and plates §§ spring | | | | | | | | | | | |
| temper. | | — | — | | | | | | | | |
| Medium temper. | | — | — | 17.6 | 35.1 | 25,000 | 50,000 | 25.0 | | | |
| Bronze, Phosphor: spring wire, hard-drawn or hard-rolled (U. S. Navy Spec. 22 W5, Dec. 1, 1915). Cu 94, | | | | | | | | | | | |
| Sn min. 4.5, Zn max 0.3, Fe max. 0.1, Pb max. 0.2, P 0.05 to 0.50; max. elong. in 203 mm (8 in.) = 4 per cent. | | | | | | | | | | | |
| Diameter (group limits). | Min. tensile strength. | | Diameter (group limits). | | Min. tensile strength. | | | | | | |
| | kg/mm ² | lb/in ² | mm | in. | kg/mm ² | lb/in ² | | | | | |
| Up to 1.59 mm or 0.0625 in. | 95.0 | 135,000 | to 6.35 | to 0.250 | 77.5 | 110,000 | | | | | |
| Over 1.59 mm to 3.17 mm (0.125 in.) | 88.0 | 125,000 | to 9.52 | to 0.375 | 74.0 | 105,000 | | | | | |

* Specification Values, Rolled Brass, Cu 62, Zn 37, Sn 1, min. properties after U. S. Navy Spec., 1918.

† Specification Values: Jan. 3, 1916, Vanadium Bronze Castings, Cu 61, Zn 38, Sn max. 1 (incl. V). Minima.

‡ Compressive P-limit 15.5 kg/mm² or 22,000 lb/in²

§ Compressive P-limit 10.5 kg/mm² or 15,000 lb/in² and 28 per cent set for 70 kg/mm² or 100,000 lb/in²

|| Ultimate compressive strength, 54.2 kg/mm² or 77,100 lb/in² (Cu 76, Sn 7, Pb 13, Zn 4).

* Compressive P-limit 8.8 to 9.1 kg/mm² or 12,500 to 13,000 lb/in², and 34 to 35 per cent set for 70 kg/mm²

** Compression: ultimate strength 49.5 kg/mm² or 70,500 lb/in²

†† Modulus of Elasticity: (1) 12,200 kg/mm² or 17,300,000 lb/in²; (2) 10,500 kg/mm² or 14,900,000 lb/in²

||| Compressive P-limit 17.6 to 28.1 kg/mm² or 25,000 to 40,000 lb/in² and 6 to 10 per cent set for 70 kg/mm² or 100,000 lb/in² load.

Specification Values: U. S. Navy 46 B 5c, Mar. 1, 1917, Cu 85 to 90, Sn 6 to 11, Zn max. 4: Cast, Grade 1. — Impurities max. 0.8; min. tensile strength 31.6 kg/mm² or 45,000 lb/in² with 20 per cent elong. in 50.8 mm (2 in.).

¶ Grade 2. — Impurities max. 1.6; min. tensile strength 21.1 kg/mm² or 30,000 lb/in² with 15 per cent elong. in 50.8 mm (2 in.).

§§ Specification Values: U. S. Navy 46 B 14b, Mar. 1, 1916, Cu min. 94, Sn min. 3.5, P 0.50, rolled or drawn.

||| Minimum yield points specified: for P-limits assume 66 per cent of values shown.

MECHANICAL PROPERTIES

Copper Alloys—Three (or more) Components

| Alloy and approx. composition, per cent. | Condition. | Density or weight. | | P-limit. | Ultimate strength. | P-limit. | Ultimate strength. | Elong. in 50.8 mm (2 in.). | Reduct. in area. | Hardness. | |
|---|-----------------------------------|------------------------|--------------------------|-----------------------------|--------------------|------------------------------|--------------------|----------------------------|---|------------------|---------------|
| | | gm per cm ³ | lb. per in. ³ | Tension, kg/mm ² | | Tension, lb/in. ² | | Per cent. | | Brimell @ 500 kg | Sclero-scope. |
| Bronze: | | | | | | | | | | | |
| Silicon..... | Cast..... | — | — | — | 46.0 | — | 65,000 | — | — | — | — |
| Cu 70, Zn 29.5, Si 0.5..... | Drawn, hard..... | — | — | — | 74.0 | — | 105,000 | — | — | — | — |
| Zinc * Comp. "G" | Cast..... | 8.6 | 535 | 8.6 | 27.4 | 12,200 | 38,900 | 25.0 | 21.0 | 64 | 13 |
| Admiralty gun metal..... | Cast†..... | — | — | 5.6 to | 22.5 to | 8,000 to | 32,000 to | 25.0 to | 25.0 to | 65 to | 10 to |
| Comm'l range..... | — | — | — | 8.4 | 26.7 | 12,000 | 38,000 | 10.0 | 12.0 | 75 | 20 |
| Spec. values..... | Cast (mins.)..... | — | — | — | 21.1 | — | 30,000 | 14.0 | — | — | — |
| Cu 88, Sn 8, Zn 4..... | Cast ‡..... | 8.5 | 530 | 7.7 | 27.5 | 11,000 | 39,200 | 30.5 | 24.0 | 58 | 11 |
| Cu 85, Sn 13, Zn 2..... | Cast..... | — | — | — | 26.7 | — | 38,000 | 2.5 | 2.5 | — | 25 |
| Zinc, Lead | | | | | | | | | | | |
| Cu 90, Sn 6.5, Zn 2, Pb 1.5 | Cast §..... | — | — | 8.4 to | 23.0 to | 12,000 to | 34,000 to | 33.0 to | 34.0 to | 50 to | — |
| Rods and bars up to 12.7 mm (½ in.)..... | — | — | — | 11.2 | 28.1 | 16,000 | 40,000 | 25.0 | 26.0 | 60 | — |
| over 12.7 mm to 25.4 mm (1 in.)..... | — | — | — | 28.1 | 56.2 | 40,000 | 80,000 | 30.0 | Required to bend cold through 120° about radius equal to thickness. | — | — |
| over 25.4 mm (1 in.)..... | — | — | — | — | 26.4 | 52.7 | 37,500 | 75,000 | 30.0 | — | — |
| Shapes, all thicknesses | — | — | — | — | 24.6 | 50.7 | 35,000 | 72,000 | 30.0 | — | — |
| Sheets and plates, 0 to 12.7 mm (½ in.)..... | — | — | — | — | 26.4 | 52.7 | 37,500 | 75,000 | 30.0 | — | — |
| over 12.7 mm (½ in.)..... | — | — | — | — | 27.4 | 54.8 | 39,000¶ | 78,000 | 30.0 | — | — |
| Aluminum Tin: | — | — | — | — | 26.4 | 52.7 | 37,500 | 75,000 | 30.0 | — | — |
| Cu 88.5, Al 10.4, Sn 1.2 | Cast, chill..... | — | — | 26.0 | 48.0 | 36,700 | 68,000 | 4.5 | 5.5 | 189 | 32 |
| Aluminum Titanium: | | | | | | | | | | | |
| Cu 90, Al 10..... | Cast **..... | — | — | 13.9 | 52.0 | 19,800 | 74,000 | 19.5 | 23.7 | 100 | 25 |
| Quench, 800° C..... | — | — | — | — | 29.0 | 74.0 | 40,500 | 105,200 | 1.0 | 0.8 | 262 |
| Cu 89, Al 10, Fe 1..... | Cast ††..... | 7.58 | 473 | 14.1 to | 45.7 to | 20,000 to | 65,000 to | 30.0 to | 30.0 to | 93 to | 25 to |
| | — | — | — | 17.6 | 56.2 | 25,000 | 80,000 | 20.0 | 20.0 | 100 | 26 |
| Lead: | | | | | | | | | | | |
| Cu 71.9, Pb 27.5, Sn 0.5 | Cast..... | — | — | — | 4.2 to | — | 6,000 to | 3.0 to | 4.2 to | — | — |
| | — | — | — | — | 4.6 | — | 6,600 | 3.2 | 6.7 | — | — |
| Nickel, Aluminum: | | | | | | | | | | | |
| Cu 82.1, Ni 14.6, Al 2.5, Zn 0.7 †..... | Forged..... | — | — | 44.5 | 90.0 | 63,300 | 128,000 | 10.0 | 12.0 | — | — |
| Cu 85, Sn 5, Zn 5, Pb 5..... | Cast §§..... | — | — | 10.5 to | 19.0 to | 15,000 to | 27,000 to | 20.0 to | 20.0 to | 50 to | — |
| | — | — | — | 13.4 | 23.2 | 19,000 | 33,000 | 16.0 | 15.0 | 62 | — |
| Cu 83, Sn 14, Zn 2, Pb 1..... | Cast..... | — | — | 10.5 to | 16.2 to | 15,000 to | 23,000 to | 4.0 to | 4.0 to | — | 20 |
| | — | — | — | 13.4 | 19.0 | 19,000 | 27,000 | 0.5 | 0.5 | — | 24 |
| Zinc, Phosphor ("Non Gran") | | | | | | | | | | | |
| Cu 86, Sn 11, Zn 3, Ptr. Vanadium. See Brass, Vanadium. | Cast..... | — | — | 13.0 | 25.0 | 19,000 | 35,000 | 9.0 | — | — | — |
| Copper, Aluminum or Aluminum Bronze: | | | | | | | | | | | |
| Cu 90, Al 10..... | Cast, sand | 7.5-7.45 | 468-405 | 13.9 to | 51.1 to | 19,800 to | 72,700 to | 28.8 to | 30.0 to | 102 to | 25 to |
| | — | — | — | 23.3 | 60.0 | 33,200 | 85,500 | 21.7 | 22.4 | 106 | 26 |
| Cu 92.5, Al 7.2..... | Rolled, and ann..... | — | — | 7.0 | 37.5 | 9,600 | 53,500 | 91.0 | 72.9 | 81 | 19 |
| Aluminum, Iron or Sill-man bronze. | Wrought..... | — | — | 9.8 | 59.3 | 14,000 | 84,400 | 11.5 | — | — | — |
| Cu 86.4, Al 9.7, Fe 3.9..... | Cast..... | — | — | 8.1 | 55.5 | 11,500 | 78,850 | 14.5 | — | — | — |
| | Cast, sand..... | — | — | 14.0 | 54.0 | 20,000 | 77,000 | 24.5 | 25.0 | 100 | — |
| | Quenched 850° C drawn 700° C..... | — | — | 28.0 | 65.0 | 40,000 | 92,000 | 14.0 | 18.5 | 140 | — |

* Gov't. Bronze: Cu 88, Sn 10, Zn 2 (values shown are averages for 30 specimens from five foundries tested at the Bureau of Standards).

† Compressive P-limit 10.5 kg/mm² or 15,000 lb/in² with 20 per cent set for 70 kg/mm² or 100,000 lb/in² load.

‡ Values from same series of tests as first values for "88-10-2," averages for 26 specimens from five foundries tested at Bureau of Standards.

§ Compressive P-limit 9.1 kg/mm² or 13,000 lb/in² with 34 per cent set for 70 kg/mm² or 100,000 lb/in² load.

|| Specification minimums: U. S. Navy 46B17, Dec. 2, 1918, for hot-rolled aluminum bronze, Cu 85 to 87, Al 7 to 9, Fe 2.5 to 4.5. Specification values under P-limit are for yield point.

¶ Two and six tenths per cent increase in strength up to 762 mm (30 in.) width.

** Compressive P-limit: cast, 14.1 kg/mm² or 20,000 lb/in² with 11.4 per cent set at 70 kg/mm² or 100,000 lb/in² load.

†† Compressive P-limit: cast, 12.7 to 14.1 kg/mm² or 18,000 to 20,000 lb/in² with 13 to 15 per cent set at 700 kg/mm² or 100,000 lb/in² load.

‡‡ Modulus of elasticity 14,800 kg/mm² or 21,150,000 lb/in²

§§ Compressive P-limit 8.4 kg/mm² or 12,000 lb/in² with 36 per cent set for 70.3 kg/mm² or 100,000 lb/in² load.

||| High values are after Jean Escard "L'Aluminum dans L'Industrie," Paris, 1918. Compressive P-limit 13.5 kg/mm² or 19,200 lb/in² with 13.5 per cent set for 70.3 kg/mm² or 100,000 lb/in² load.

TABLE 70
MECHANICAL PROPERTIES
Miscellaneous Metals and Alloys

| Metal or alloy. Approx. composition, per cent. | Condition. | Density or weight. | | P-limit. | Ultimate strength. | P-limit. | Ultimate strength. | Elong. in 50.8 mm (2 in.). | Reduct. of area. | Hardness. | |
|--|--|------------------------------|-------------------------------|----------|-----------------------|-----------|-----------------------|----------------------------------|---------------------|---------------------|-------------------|
| | | gm per cm ³ | lb. per ft ³ | | | | | | | Brinell @ 500 kg | Sclero- scope. |
| * Cobalt, Co 99.7 | Cast | 8.8 | 550 | — | 23.1 | — | 33,000 | — | — | 121 | — |
| | Ann. | 8.9 | 556 | — | 26.0 | — | 37,000 | — | — | 48 | — |
| Gold, Au 100 | Cast | 19.3 | 1203 | — | 18.0 | — | 25,000 | 25.0 | — | — | 20 |
| | Drawn hard | — | — | — | 26.0 | — | 37,000 | — | — | — | — |
| | Drawn hard | 17.2 | 1073 | — | 45.8 | — | 65,100 | — | — | — | — |
| Copper, Au 90, Cu 10 | Drawn hard | — | — | — | 102.0 | — | 145,000 | — | — | — | — |
| Copper, Silver, Au 58, Cu 30 Ag 12 | Cast | 11.38 | 710 | — | 1.3 | — | 1,780 | — | — | 8 | 3 |
| Lead, Pb | Rolled hard | 11.40 | 711 | — | 2.3 | — | 3,300 | — | — | — | — |
| (Comm'l.) | Drawn soft | — | — | — | 1.7 | — | 2,420 | — | — | — | — |
| | Drawn hard | — | — | — | 2.2 | — | 3,130 | — | — | — | — |
| Antimony † Pb 95.5, Sb 4.5 | Cast | 10.5 | 655 | 2.8 | 4.5 | 4,000 | 6,400 | — | — | — | — |
| Magnesium, Mg | Drawn hard | 1.7 | 106 | — | 21.0 | — | 30,000 | — | — | — | — |
| | Drawn hard | 1.74 | 109 | — | 23.2 | — | 33,000 | — | — | — | — |
| Nickel, Ni 98.5 | Cast | 8.3 | 518 | 16.7 ** | 26.7 | 23,800 ** | 38,000 | 5.7 | 6.1 | 76 | — |
| Ni 99.95 | Wrought, ann. | 8.7 | 543 | 12.6 | 20.9 | 17,900 | 42,500 | 11.0 | — | — | — |
| Ni 98.5 | Wrought, com. | — | — | — | 46.0 | — | 65,000 | — | — | 83 | 35 |
| Ni | Rolled hard | — | — | — | 64.7 | — | 92,000 | 11.0 | — | — | — |
| Ni | Rolled ann. | — | — | — | 53.4 | — | 76,000 | 35.0 | — | — | — |
| Ni | Drawn hard, D = 1.65 mm or 0.065 in. | — | — | — | 109.0 | — | 155,000 | — | — | — | — |
| Copper, iron, manganese or Monel metal: | | | | | | | | | | | |
| Ni 67, Cu 28, Fe 3, Mn 2 | Cast | 8.9 | 555 | 21.2 | 49.3 | 30,100 | 70,000 | 18.0 | 20.0 | — | 21 |
| | Rolled | — | — | 55.1 | 73.8 | 78,400 | 104,900 | 31.3 | 61.7 | — | 27 |
| Ni 66, Cu 28, Fe 3.5, Mn 2.5 | Wrought | — | — | 28.3 | 64.8 | 40,300 | 92,200 | 46.3 | 70.2 | — | — |
| Ni 71, Cu 27, Fe 2 § | Drawn hard | — | — | — | 112.5 | — | 160,000 | — | — | — | — |
| 46 M 1 a | Cast, minimums | — | — | 22.8 ** | 45.7 | 32,500 ** | 65,000 | 25.0 | — | — | — |
| 46 M 7 b | Rolled, min., rods and bars † | — | — | 28.1 ** | 56.2 | 40,000 ** | 80,000 | 32.0 | — | — | — |
| | Rolled, minimum, sheets and plates | — | — | 21.1 | 45.7 | 30,000 | 65,000 | 15.0 | — | — | — |
| Palladium, Pd | Drawn hard | 12.1 | 755 | — | 27.0 | — | 39,000 | — | — | — | — |
| Platinum, Pt | Drawn hard | 21.5 | 1342 | — | 37.3 | — | 53,000 | 18.0 | — | — | 24 |
| | Drawn ann. | — | — | — | 24.6 | — | 35,000 | 50.0 | — | — | 13 |
| Silver, Ag 100 | Cast | 10.5 | 655 | — | 28.1 | — | 40,000 | — | — | — | — |
| | Drawn hard | 10.57 | 660 | — | 36.0 | — | 51,200 | — | — | — | 39 |
| Copper, Ag 75, Cu 25 | Drawn hard | — | — | — | 77.0 † | — | 109,500 | — | — | — | 32 |
| Tantalum, Ta | Drawn hard | 16.6 | 1035 | — | 91.0 | — | 130,000 | — | — | — | — |
| | Cast | 7.3 | 456 | 1.1 | 2.8 | 1,600 | 4,000 | 35.0 | — | 14 | 8 |
| | Rolled | — | — | — | 3.7 | — | 5,300 | — | — | — | — |
| | Drawn hard | — | — | — | 7.0 | — | 10,000 | — | — | — | — |
| Tin, Sn 99.8 † | | | | | | | | | | | |
| Antimony, Copper, Zinc (Britannia Metal): | | | | | | | | | | | |
| Sn 81, Sb 16, Cu 2, Zn 1 | | | | | | | | | | | |
| Zinc, Aluminum, etc. (aluminum solder): | | | | | | | | | | | |
| Sn 63, Zn 18, Al 13, Cu 3, Sb 2, Pb 1 | Cast | — | — | — | 10.2 | — | 14,500 | 1.9 | 1.5 | — | — |
| Sn 62, Zn 15, Al 11, Pb 8, Cu 3, Sb 1 | Cast | — | — | — | 9.1 | — | 13,000 | 1.6 | 1.3 | — | — |
| Zinc, aluminum: | | | | | | | | | | | |
| Sn 86, Zn 9, Al 5 | Cast, chill | — | — | — | 8.6 | — | 12,200 | 41.0 | 81.0 | — | — |
| Aluminum, zinc, cadmium: | | | | | | | | | | | |
| Sn 78, Al 9, Zn 8, Cd 5 | Cast, chill | — | — | — | 10.1 | — | 14,300 | 18.0 | 41.0 | — | — |

Antimony: Modulus of Elasticity 7960 kg/mm² or 11,320,000 lb/in² (Bridgman).

* Compressive strength: cast and annealed, 86.0 kg/mm² or 122,000 lb/in²

Comm'l. comp., C 0.06, cast, tensile, ultimate, 42.8 kg/mm² or 61,000 lb/in², with 20 per cent elongation in 50.8 or 2 in.

Compression, ultimate 123.0 kg/mm² or 175,000 lb/in²

Stellite, Co 59.5, Mo 22.5, Cr 10.8, Fe 3.1, Mn 2.0, C 0.9, Si 0.8. Brinell hardness 512 at 3000 kg, density 8.3

† Modulus of elasticity, cast or rolled, 492 kg/mm² or 700,000 lb/in²; drawn hard 793 kg/mm² or 1,000,000 lb/in²

‡ For compressive test data on lead-base babbitt metal, see table following zinc.

§ Modulus of elasticity 15,800 kg/mm² or 22,500,000 lb/in²

|| Specification values, U. S. Navy, Monel metal, Ni min. 60, Cu min. 23, Fe max. 3.5, Mn max. 3.5, C + Si max. 0.8, Al max. 0.5.

* Values shown are subject to slight modifications dependent on shapes and thicknesses.

** Values are for yield point.

†† Compressive strength: cast, 4.5 kg/mm² or 6,400 lb/in²

Modulus of elasticity: cast av. 2,810 kg/mm² or 4,000,000 lb/in²; rolled av. 401.0 kg/mm² or 5,700,000 lb/in²

SMITHSONIAN TABLES.

MECHANICAL PROPERTIES

Miscellaneous Metals and Alloys

(a) TUNGSTEN AND ZINC

| Metal or alloy approx. comp. per cent. | Condition. | Density or weight. | | P-limit. | Ultimate strength. | P-limit. | Ultimate strength. | Elong. in 50.8 mm (2 in.). | Reduct. of area. | Hardness. | | | | |
|--|--|------------------------|-------------------------|----------------------------|--------------------|----------|--------------------|----------------------------|------------------|-----------------------------|-----------------------------|----------|------------------|---------------|
| | | gm per cm ³ | lb. per ft ³ | | | | | | | Tension, kg/mm ² | Tension, lb/in ² | Per cent | Brinell @ 500 kg | Sclero-scope. |
| | | | | | | | | | | | | | | |
| Tungsten, W 99.2 * | Ingot sintered, D = 5.7 mm or 0.22 in. | 18.0 | 1124 | — | 12.7 | — | 18,000 | 0.0 | 0.0 | — | — | | | |
| | Swaged rod, D = 0.7 mm or 0.03 in. | — | — | — | 151.0 | — | 215,000 | 4.0 | 28.0 | — | — | | | |
| | Drawn hard, D = 0.029 mm or 0.00114 in. | — | — | — | 415.0 | — | 590,000 | — | 65.0 | — | — | | | |
| | Swaged and drawn hot 97.5% reduction† | — | — | — | 164.0 | — | 233,500 | 3.2 | 14.0 | — | — | | | |
| | Same as above and equiaxed at 2000°C in H ₂ † | — | — | — | 118.0 | — | 168,000 | 0.0 | 0.0 | — | — | | | |
| | | | | | | | | | | | | | | |
| Zinc, 99.99 | Cast | 7.0 | 437 | (Impurities Pb, Fe and Cd) | | | | — | — | — | — | | | |
| | Coarse crystalline | — | — | — | 2.8 to 8.4 | — | 4,000 to 12,000 | — | — | 42 to 48 | 8 to 10 | | | |
| | Fine crystalline | — | — | — | — | — | — | — | — | — | — | | | |
| | Rolled (with grain or direction of rolling) | — | — | 2.0 | 19.0 | 2,900 | 27,000 | — | — | — | — | | | |
| | Rolled (across grain or direction of rolling) | — | — | 4.1 | 25.3 | 5,800 | 36,000 | — | — | — | — | | | |
| | Drawn hard | 7.1 | 443 | — | 7.0 | — | 10,000 | — | — | — | — | | | |

* Commercial composition for incandescent electric lamp filaments containing thorium (ThO₂) approx. 0.75 per cent after Z. Jeffries Am. Inst. Min. Eng. Bulletin 138, June, 1913.

† After Z. Jeffries Am. Inst. Min. Eng. Bulletin 149, May, 1910.

‡ Ordinary annealing treatment makes W brittle, and severe working, below recrystallization or equiaxing temperature, produces ductility. W rods which have been worked and recrystallized are stronger than sintered rods. The equiaxing temperature of worked tungsten, with a 5-min. exposure, varies from 2200°C for a work rod with 24 per cent reduction, to 1350°C for a fine wire with 100 per cent reduction. Tungsten wire, D = 0.635 mm or 0.025 in.

§ Compression on cylinder 25.4 mm (1 in.) by 65.1 mm (2.6 in.), at 20 per cent deformation:

For spelter (cast zinc) free from Cd, av. 17.2 kg/mm² or 24,500 lb/in²

For spelter with Cd 0.26, av. 27.4 kg/mm² or 39,000 lb/in² (See Proc. A. S. T. M., Vol. 13, pl. 19.)

Modulus of rupture averages twice the corresponding tensile strength.

Shearing strength: rolled, averages 13.6 kg/mm² or 194,000 lb/in²

Modulus of elasticity: cast, 7,750 kg/mm² or 11,025,000 lb/in²

Modulus of elasticity: rolled, 8,450 kg/mm² or 12,000,000 lb/in² (Moore, Bulletin 52, Eng. Exp. Sta. Univ. of Ill.)

(b) WHITE METAL BEARING ALLOYS (BABBITT METAL)

A. S. T. M. vol. xviii, I, p. 491.

Experimental permanent deformation values from compression tests on cylinders 31.8 mm (1½ in.) diam. by 63.5 mm (2½ in.) long, tested at 21°C (70°F.) (Set readings after removing loads.)

| Alloy No. | Formula, per cent. | | | | Pouring temp. | | Weight. | | Permanent deformation @ 21° C | | | | | | Hardness. | |
|------------|--------------------|------|-----|------|---------------|-----|---------|---------|-------------------------------|--------|----------------------|--------|------------------------|--------|-----------------|-------------------|
| | | | | | | | | | @ 454 kg = 1000 lb. | | @ 2268 kg = 5000 lb. | | @ 4536 kg = 10,000 lb. | | Brinell @ 21° C | @ 500 kg @ 100° C |
| | Sn | Sb | Cu | Pb | C | F. | g/cm³ | lb./ft³ | mm | in. | mm | in. | mm | in. | | |
| | Tin Base. | | | | | | | | | | | | | | | |
| 1 | 91.0 | 4.5 | 4.5 | — | 440 | 824 | 7.34 | 458 | 0.000 | 0.0000 | 0.025 | 0.0010 | 0.380 | 0.0150 | 28.6 | 12.8 |
| 2 * | 89.0 | 7.5 | 3.5 | — | 432 | 808 | 7.39 | 401 | .0000 | .0000 | .038 | .0015 | .305 | .0120 | 28.3 | 12.7 |
| 3 | 83.3 | 8.3 | 8.3 | — | 401 | 916 | 7.46 | 465 | .025 | .0010 | .114 | .0045 | .180 | .0070 | 34.4 | 15.7 |
| 4 | 75.0 | 12.0 | 3.0 | 10.0 | 360 | 680 | 7.52 | 469 | .013 | .0005 | .064 | .0025 | .230 | .0090 | 29.6 | 12.8 |
| 5 | 65.0 | 15.0 | 2.0 | 18.0 | 350 | 661 | 7.75 | 484 | .025 | .0010 | .076 | .0030 | .230 | .0090 | 29.6 | 11.8 |
| Lead Base. | | | | | | | | | | | | | | | | |
| 6 | 20.0 | 15.0 | 1.5 | 63.5 | 337 | 638 | 9.33 | 582 | .038 | .0015 | .127 | .0050 | .457 | .0180 | 24.3 | 11.1 |
| 7 | 10.0 | 15.0 | — | 75.0 | 329 | 625 | 9.73 | 607 | .025 | .0010 | .127 | .0050 | .583 | .0230 | 24.1 | 11.7 |
| 8 | 5.0 | 15.0 | — | 80.0 | 329 | 625 | 10.04 | 627 | .051 | .0020 | .229 | .0090 | 1.575 | .0620 | 20.9 | 10.3 |
| 9 | 5.0 | 10.0 | — | 85.0 | 319 | 616 | 10.24 | 640 | .102 | .0040 | .305 | .0120 | 2.130 | .0840 | 19.5 | 8.6 |
| 10 | 2.0 | 15.0 | — | 83.0 | 325 | 625 | 10.07 | 629 | .025 | .0010 | .254 | .0100 | 3.910 | .1540 | 17.0 | 8.9 |
| 11 | — | 15.0 | — | 85.0 | 325 | 625 | 10.28 | 642 | .025 | .0010 | .254 | .0100 | 3.020 | .1190 | 17.0 | 9.9 |
| 12 | — | 10.0 | — | 90.0 | 334 | 634 | 10.67 | 666 | 0.064 | 0.0025 | 0.432 | 0.0170 | 7.240 | 0.2850 | 14.3 | 6.4 |

* U. S. Navy Spec. 46M2b (Cu 3 to 4.5, Sn 88 to 89.5, Sb 7.0 to 8.0) covers manufacture of anti-friction-metal castings. (Composition W.)

NOTE. — See also Brass, Lead (yellow brass), Brass, Lead-Tin (Red Brass); Bronze, Phosphor, etc., under Copper alloys.

SMITHSONIAN TABLES.

TABLE 72
MECHANICAL PROPERTIES
Cement and Concrete

(a) CEMENT

CEMENT: Specification Values (A. S. T. M. C₉ to 17, C₁₀ to 09, and C₉ to 16T).

Minimum strengths based on tests of 645 mm² (1 in²) cross section briquettes for tension, and cylinders 50.8 mm (2 in.) diameter by 101.6 mm (4 in.) length for compression. Mortar composed of 1 part cement to 3 parts Ottawa sand by volume; specimens kept in damp closet for first 24 hours and in water from then on until tested.

| Cement (1: 3 mortar tested). | Specific gravity. | Age, days. | Tension. | | Compression. | |
|---------------------------------|----------------------|---------------|--------------------|--------------------|--------------------|--------------------|
| | | | kg/mm ² | lb/in ² | kg/mm ² | lb/in ² |
| Std. Portland..... | 3.10 | 7 | 0.16 | 200 | 0.85 | 1,200 |
| White Portland.... | 3.07 | 28 | .24 | 300 | 1.60 | 2,000 |
| Natural Av..... | 2.85 | 7 | .03 | 50 | — | — |
| Natural..... | — | 28 | 0.09 | 125 | — | — |

(b) CEMENT AND CEMENT MORTARS

CEMENT AND CEMENT MORTARS. — Bureau of Standards Experimental Values. Compressive Strengths of Portland cement mortars of uniform plastic consistency. Data from tests on 50.8 mm (2 in.) cubes stored in water. Sand: Potomac River, representative concrete sand.

| Cement. | Sand. | Water, per cent. | Age, days. | Compressive strength. | |
|------------------------|-------|---------------------|---------------|-----------------------|--------------------|
| Proportions by volume. | | | | kg/mm ² | lb/in ² |
| I | 0 | 30.0 | 7 28 | 4.20 6.40 | 5,970 9,120 |
| I | 1 | 16.0 | 7 28 | 3.10 4.75 | 4,440 6,750 |
| I | 2 | 13.6 | 7 28 | 2.05 3.10 | 2,900 4,440 |
| I | 3 | 13.9 | 7 28 | 1.25 2.05 | 1,780 2,890 |
| I | 9 | 15.1 | 7 28 | 0.10 0.15 | 120 200 |

NOTE. — (From Bureau of Standards Tech. Paper 58.) Neat cement briquettes mixed at plastic consistency (water 21 per cent) show 0.52 kg/mm² or 740 lb/in² tensile strength at 28 days' age;

1 Cement: 3 Ottawa sand-mortar briquettes, mixed at plastic consistency (water 9 per cent) show 0.28 kg/mm² or 400 lb/in² tensile strength at 28 days' age.

SMITHSONIAN TABLES.

TABLE 72 (continued)
MECHANICAL PROPERTIES

(c) CONCRETE

CONCRETE: Compressive strengths. Experimental values for various mixtures. Results compiled by Joint Committee on Concrete and Reinforced Concrete. Final Report adopted by the Committee July 1, 1916. Data are based on tests of cylinders 203.2 mm (8 in.) diameter and 406.4 mm (16 in.) long at 28 days age.

American Standard Concrete Compressive Strengths.

| Aggregate. | Units. | Mix. | | | | |
|--|--------------------|------|------|------|------|------|
| | | 1:3 | 1:4½ | 1:6 | 1:7½ | 1:9 |
| Granite, trap rock | kg/mm ² | 2.3 | 2.0 | 1.5 | 1.3 | 1.0 |
| | lb/in ² | 3300 | 2800 | 2200 | 1800 | 1400 |
| Gravel, hard limestone and hard sandstone | kg/mm ² | 2.1 | 1.8 | 1.4 | 1.1 | 0.9 |
| | lb/in ² | 3000 | 2500 | 2000 | 1600 | 1300 |
| Soft limestone and soft sandstone | kg/mm ² | 1.5 | 1.3 | 1.1 | 0.8 | 0.7 |
| | lb/in ² | 2200 | 1800 | 1500 | 1200 | 1000 |
| Cinders | kg/mm ² | 0.6 | 0.5 | 0.4 | 0.4 | 0.3 |
| | lb/in ² | 800 | 700 | 600 | 500 | 400 |

NOTE. — Mix shows ratio of cement (Portland) to combined volume of fine and coarse aggregate (latter as shown).

Committee recommends certain fractions of tabular values as safe working stresses in reinforced concrete design, which may be summarized as follows:

Bearing, 35 per cent of compressive strength;

Compression, extreme fiber, 32.5 per cent of compressive strength;

Vertical shearing stress 2 to 6 per cent of compressive strength, depending on reinforcing;

Bond stress, 4 and 5 per cent of compressive strength, for plain and deformed bars, respectively.

Modulus of Elasticity to be assumed as follows:

| For concrete with strength. | | Assume modulus of elasticity. | |
|-----------------------------|--------------------|-------------------------------|--------------------|
| kg/mm ² | lb/in ² | kg/mm ² | lb/in ² |
| up to 0.6 | up to 800 | 530 | 750,000 |
| 0.6 to 1.5 | 800 to 2200 | 1400 | 2,000,000 |
| 1.5 to 2.0 | 2200 to 2900 | 1750 | 2,500,000 |
| over 2.0 | over 2900 | 2100 | 3,000,000 |

(See Joint Committee Report, Proc. A. S. T. M. v. XVII, 1917, p. 201.)

EDITOR'S NOTE. — The values shown in the table above are probably fair values for the compressive strengths of concretes made with average commercial material, although higher results are usually obtained in laboratory tests of specimens with high grade aggregates. Observed values on 1:2:4 gravel concrete show moduli of elasticity up to 3160 kg/mm² or 4,500,000 lb/in² and compressive strengths to 4.2 kg/mm² or 6000 lb/in².

Tensile strengths average 10 per cent of values shown from compressive strengths.

Shearing strengths average from 75 to 125 per cent of the compressive strengths; the larger percentage representing the shear of the leaner mixtures (for direct shear, Hatt gives 60 to 80 per cent of crushing strength).

Compressive strengths of natural cement concrete average from 30 to 40 per cent of that of Portland cement concrete of the same proportioned mix.

Transverse strength: modulus of rupture of 1:2½:5 concrete at 1 and 2 months equal to one sixth crushing strength at same age (Hatt).

Weight of granite, gravel and limestone, 1:2:4 concretes averages about 2.33 g/cm³ or 145 lb/ft³; that of cinder concrete of same mix is about 1.85 g/cm³ or 115 lb/ft³.

Concrete, 1:2:4 Mix, Compressive Strengths at Various Ages.

Experimental Values: one part cement, two parts Ohio River sand and four parts of coarse aggregate as shown. Compressive tests made on 203.2 mm (8 in.) diameter cylinders, 406.4 mm (16 in.) long. (After Pittsburgh Testing Laboratory Results. See *Rwy Age*, vol. 64, Jan. 18, 1918, pp. 165-166.)

| Coarse aggregate. | Unit. | Age. | | | |
|----------------------|--------------------|----------|----------|----------|-----------|
| | | 14 days. | 30 days. | 60 days. | 180 days. |
| Gravel | kg/mm ² | 1.35 | 1.61 | 2.06 | 2.67 |
| | lb/in ² | 1921 | 2294 | 2925 | 3798 |
| Limestone | kg/mm ² | 1.24 | 1.53 | 2.35 | 3.11 |
| | lb/in ² | 1758 | 2174 | 3343 | 4426 |
| Trap rock | kg/mm ² | 1.45 | 1.67 | 2.36 | 3.39 |
| | lb/in ² | 2063 | 2386 | 3360 | 4819 |
| Granite | kg/mm ² | 1.49 | 1.61 | 2.14 | 2.92 |
| | lb/in ² | 2122 | 2292 | 3043 | 4151 |
| Slag No. 1 | kg/mm ² | 1.75 | 2.16 | 2.37 | 3.38 |
| | lb/in ² | 2484 | 3075 | 3365 | 4803 |
| Slag No. 2 | kg/mm ² | 1.37 | 1.78 | 2.06 | 2.64 |
| | lb/in ² | 1941 | 2525 | 2930 | 3753 |

NOTE. — Maximum and minimum test results varied about 5 per cent above or below average values shown above.

TABLE 73
MECHANICAL PROPERTIES
Stone and Clay Products

(a) STRENGTH AND STIFFNESS OF AMERICAN BUILDING STONES *

| Stone. | Weight, average. | | Compression. Ultimate strength. | | | Flexure. Modulus of rupture. | | | Shear. Ultimate strength. | | | Flexure. Modulus of elasticity. | | |
|------------|---------------------|--------------------|------------------------------------|--------------------|--------------------|------------------------------------|--------------------|--------------------|---------------------------------|--------------------|--------------------|------------------------------------|--------------------|--------------------|
| | | | Average. | | Range per cent. | Average. | | Range per cent. | Average. | | Range per cent. | Average. | | Range per cent. |
| | g/cm ³ | lb/ft ³ | kg/mm ² | lb/in ² | | kg/mm ² | lb/in ² | | kg/mm ² | lb/in ² | | kg/mm ² | lb/in ² | |
| Granite... | 2.6 | 165 | 14.20 | 20,200 | 25 | 1.15 | 1600 | 30 | 1.60 | 2300 | 20 | 5300 | 7,500,000 | 25 |
| Marble... | 2.7 | 170 | 8.85 | 12,600 | 25 | 1.05 | 1500 | 50 | 0.90 | 1300 | 25 | 5750 | 8,200,000 | 50 |
| Limestone | 2.6 | 160 | 6.30 | 9,000 | 95 | 0.85 | 1200 | 100 | 1.00 | 1400 | 45 | 5900 | 8,400,000 | 65 |
| Sandstone. | 2.2 | 135 | 8.80 | 12,500 | 50 | 1.05 | 1500 | 55 | 1.20 | 1700 | 45 | 2300 | 3,300,000 | 100 |

* Values based on tests of American building stones from upwards of twenty-five localities, made at Watertown (Mass.) Arsenal (Moore, p. 184). Each value shown under "Range" is one half the difference between maximum and minimum locality averages expressed as a percentage of the average for the stone.

(b) STRENGTH AND STIFFNESS OF BAVARIAN BUILDING STONES *

| Stone. | Weight, average. | | Compression. Ultimate strength. | | | Flexure. Modulus of rupture. | | | Shear. Ultimate Strength.† | | | Flexure. Modulus of elasticity. | | |
|-----------|---------------------|--------------------|------------------------------------|--------------------|--------------------|------------------------------------|--------------------|--------------------|----------------------------------|--------------------|--------------------|---------------------------------------|--------------------|--------------------|
| | | | Average. | | Range per cent. | Average. | | Range per cent. | Average. | | Range per cent. | Average. | | Range per cent. |
| | g/cm ³ | lb/ft ³ | kg/mm ² | lb/in ² | | kg/mm ² | lb/in ² | | kg/mm ² | lb/in ² | | kg/mm ² | lb/in ² | |
| Granite. | 2.66 | 165 | 13.70 | 19,500 | 5 | 0.90 | 1300 | 5 | 1.00 | 1420 | 0 | 1600 | 2,300,000 | 30 |
| Marble ‡. | 2.16 | 135 | 5.60 | 8,000 | 15 | 0.30 | 450 | — | 0.45 | 620 | 50 | 3450 | 4,900,000 | — |
| Limestone | 2.48 | 155 | 8.10 | 11,500 | 5 | 1.10 | 1550 | 45 | 0.60 | 870 | 20 | 2350 | 3,350,000 | 90 |
| Sandstone | 2.30 | 145 | 8.10 | 11,500 | 75 | 0.45 | 650 | 55 | 0.50 | 680 | 35 | 2500 | 3,550,000 | 35 |

* Values based on careful tests by Bauschinger, "Communications," Vol. 10.

† Shearing strength determined perpendicular to bed of stone.

‡ Values are for Jurassic limestone.

GENERAL NOTES.—1. Later transverse strength (flexure) tests on Wisconsin building stones (Johnson's "Materials of Construction," 1918 ed., p. 255) show moduli of rupture as follows: Granite, 1.90 to 2.75 kg/mm² or 2710 to 3910 lb/in²; limestone, 0.80 to 3.30 kg/mm² or 1160 to 4660 lb/in²; sandstone, 0.25 to 0.95 kg/mm² or 360 to 1320 lb/in².

2. Good slate has a modulus of rupture of 4.90 kg/mm² or 7000 lb/in² (*loc. cit.*, p. 257).

MECHANICAL PROPERTIES

Stone and Clay Products

(c) STRENGTH OF AMERICAN BUILDING BRICKS *

| Brick — description. | Absorption average per cent. | Compression. Min. ult. strength. | | Flexure. Min. modulus rupture. | |
|------------------------------|------------------------------------|-------------------------------------|--------------------|-----------------------------------|---------------------|
| | | kg/mm ² | lb/in ² | kg/mm ² | lb. in ² |
| Class A (Vitrified)..... | 5 | 3.50 | 5000 | 0.65 | 900 |
| Class B (Hard burned)..... | 12 | 2.45 | 3500 | 0.40 | 600 |
| Class C (Common firsts)..... | 18 | 1.40 | 2000 | 0.30 | 400 |
| Class D (Common)..... | — | 1.05 | 1500 | 0.20 | 300 |

* After A. S. T. M. Committee C-3, Report 1913, and University laboratories' tests for Committee C-3 (Johnson, p. 281).

(d) STRENGTH IN COMPRESSION OF BRICK PIERS AND OF TERRA-COTTA BLOCK PIERS

Tabular values are based on test data from Watertown Arsenal, Cornell University, U. S. Bureau of Standards, and University of Ill. (Moore, p. 185).

| Brick or block used. | Mortar. | Compression.* Av. ult. strength. | |
|---------------------------|--------------------------------------|-------------------------------------|--------------------|
| | | kg/mm ² | lb in ² |
| Vitrified brick..... | 1 part P.† cement : 3 parts sand.... | 1.95 | 2800 |
| Pressed (face) brick..... | 1 part P. cement : 3 parts sand.... | 1.40 | 2000 |
| Pressed (face) brick..... | 1 part lime : 3 parts sand..... | 1.00 | 1400 |
| Common brick..... | 1 part P. cement : 3 parts sand.... | 0.70 | 1000 |
| Common brick..... | 1 part lime : 3 parts sand..... | 0.50 | 700 |
| Terra-cotta brick..... | 1 part P. cement : 3 parts sand.... | 2.10 | 3000 |

* Building ordinances of American cities specify allowable working stresses in compression over bearing area of 12.5 per cent (vitrified brick) to 17.5 per cent (common brick) of corresponding ultimate compressive strength shown in table.

† P. denotes Portland.

(e) STRENGTH OF COMPRESSION OF VARIOUS BRICKS

Reasonable minimum average compressive strengths for other types of brick than building brick are noted by Johnson, "Materials of Construction," pp. 289 ff., as follows:

| Brick. | kg/mm ² | lb. in ² |
|--------------------------|--------------------|----------------------|
| sand-lime | 2.10 | 3000 |
| sand-lime (German) | 1.53 | 2180 (av. 255 tests) |
| paving | 5.00 | 8000 |
| acid-refractory | 0.70 | 1000 |
| silica-refractory | 1.40 | 2000 |

The specific gravity of brick ranges from 1.9 to 2.6 (corresponding to 120 to 160 lb ft³).

Building tile: hollow clay blocks of good quality, — minimum compressive strength: 0.70 kg/mm² or 1000 lb in². Tests made for A. S. T. M. Committee C-10 (A. S. T. M. Proc. XVII, I, p. 334) show compressive strengths ranging from 0.45 to 8.70 kg/mm² or 640 to 12,360 lb/in² of net section, corresponding to 0.05 to 4.20 kg/mm² or 95 to 6000 lb/in² of gross section. Recommended safe loads (Marks, "Mechanical Engineers' Handbook," p. 625) for effective bearing parts of hollow tile: hard fire-clay tiles 0.06 kg/mm² or 80 lb/in²; ordinary clay tiles 0.04 kg/mm² or 60 lb/in²; porous terra-cotta tiles 0.03 kg/mm² or 40 lb/in². The specific gravity of tile ranges from 1.9 to 2.5 corresponding to a weight of 120 to 155 lb/ft³.

TABLE 74
MECHANICAL PROPERTIES
Rubber and Leather

(a) RUBBER, SHEET *

| Grade. | Ultimate strength. | | | | Ult. elongation. | | Set.† | |
|--------|--------------------|--------------------|--------------------|--------------------|------------------|---------|-----------|---------|
| | Longitudinal.† | | Transverse. | | Longit. | Transv. | Longit. | Transv. |
| | kg/mm ² | lb/in ² | kg/mm ² | lb/in ² | Per cent. | | Per cent. | |
| 1 | 1.92 | 2730 | 1.81 | 2575 | 630 | 640 | 11.2 | 7.3 |
| 2 | 1.45 | 2070 | 1.43 | 2030 | 640 | 670 | 6.0 | 5.0 |
| 3 | 0.84 | 1200 | 0.89 | 1260 | 480 | 555 | 22.1 | 16.3 |
| 4 | 1.30 | 1850 | 1.20 | 1700 | 410 | 460 | 34.0 | 24.0 |
| 5 | 0.48 | 690 | 0.36 | 510 | 320 | 280 | 27.5 | 25.0 |
| 6 | 0.62 | 880 | 0.48 | 690 | 315 | 315 | 34.3 | 25.9 |

* Data from Bureau of Standards Circular 38.
† Longitudinal indicates direction of rolling through the calendar.
‡ Set measured after 300 per cent elongation for 1 minute with 1 minute rest.

The specific gravity of rubber averages from 0.95 to 1.25, corresponding to an average weight of 60 to 80 lb/ft³.

Four-ply rubber belts show an average ultimate tensile strength of 0.63 to 0.65 kg/mm² or 890 to 930 lb/in² (Benjamin), and a working tensile stress of 0.07 to 0.11 kg/mm² or 100 to 150 lb/in² is recommended (Bach).

(b) LEATHER, BELTING

Oak tanned leather from the center or back of the hide:

Minimum tensile strengths of belts { single 2.8 kg/mm² or 4000 lb/in²
(Marks, p. 622) { double 2.5 kg/mm² or 3600 lb/in²

Maximum elongation for one hour application of { single 13.5 per cent
1.6 kg/mm² or 2250 lb/in² stress { double 12.5 per cent

Modulus of elasticity of leather varies from an average value of 12.5 kg/mm² or 17,800 lb/in² (new) to 22.5 kg/mm² or 32,000 lb/in² (old).

Chrome leather has a tensile strength of 6.0 to 9.1 kg/mm² or 8500 to 12,900 lb/in².

The specific gravity of leather varies from 0.86 to 1.02, corresponding to a weight of 53.6 to 63.6 lb./ft³.

TABLE 75
MECHANICAL PROPERTIES
Manila Rope

Manila Rope, Weight and Strength — Specification Values. From U. S. Government Standard Specifications adopted April 4, 1918.

Rope to be made of manila or Abaca fiber with no fiber of grade lower than U. S. Government Grade I, to be three-strand,* medium-laid, with maximum weights and minimum strengths shown in the table below, lubricant content to be not less than 8 nor more than 12 per cent of the weight of the rope as sold.

| Approximate diameter. | | Circumference. | | Maximum net weight. | | Minimum breaking strength. | |
|-----------------------|-----------------|----------------|----------------|---------------------|---------|----------------------------|--------|
| mm | in. | mm | in. | kg./m | lb./ft. | kg | lb. |
| 6.3 | $\frac{1}{4}$ | 19.1 | $\frac{3}{4}$ | 0.029 | 0.0196 | 320 | 700 |
| 7.9 | $\frac{5}{16}$ | 25.4 | 1 | 0.044 | 0.0286 | 540 | 1,200 |
| 9.5 | $\frac{3}{8}$ | 28.6 | $1\frac{1}{8}$ | 0.061 | 0.0408 | 660 | 1,450 |
| 11.1 | $\frac{7}{16}$ | 31.8 | $1\frac{1}{4}$ | 0.080 | 0.0539 | 790 | 1,750 |
| 11.9 | $\frac{1}{2}$ | 34.9 | $1\frac{3}{8}$ | 0.095 | 0.0637 | 950 | 2,100 |
| 12.7 | $\frac{1}{2}$ | 38.1 | $1\frac{1}{2}$ | 0.109 | 0.0735 | 1,110 | 2,450 |
| 14.3 | $\frac{9}{16}$ | 44.5 | $1\frac{3}{4}$ | 0.153 | 0.1029 | 1,430 | 3,150 |
| 15.9 | $\frac{5}{8}$ | 50.8 | 2 | 0.195 | 0.1307 | 1,810 | 4,000 |
| 19.1 | $\frac{3}{4}$ | 57.2 | $2\frac{1}{4}$ | 0.241 | 0.1617 | 2,220 | 4,900 |
| 20.6 | $1\frac{1}{16}$ | 63.5 | $2\frac{1}{2}$ | 0.284 | 0.1911 | 2,680 | 5,900 |
| 22.2 | $\frac{7}{8}$ | 69.9 | $2\frac{3}{4}$ | 0.328 | 0.2205 | 3,170 | 7,000 |
| 25.4 | 1 | 76.2 | 3 | 0.394 | 0.2645 | 3,720 | 8,200 |
| 27.0 | $1\frac{1}{16}$ | 82.6 | $3\frac{1}{4}$ | 0.459 | 0.3087 | 4,310 | 9,500 |
| 28.6 | $1\frac{1}{8}$ | 88.9 | $3\frac{1}{2}$ | 0.525 | 0.3528 | 4,990 | 11,000 |
| 31.8 | $1\frac{1}{4}$ | 95.2 | $3\frac{3}{4}$ | 0.612 | 0.4115 | 5,670 | 12,500 |
| 33.3 | $1\frac{5}{16}$ | 101.6 | 4 | 0.700 | 0.4703 | 6,440 | 14,200 |
| 34.9 | $1\frac{3}{8}$ | 108.0 | $4\frac{1}{4}$ | 0.787 | 0.5290 | 7,260 | 16,000 |
| 38.1 | $1\frac{1}{2}$ | 114.3 | $4\frac{1}{2}$ | 0.875 | 0.5879 | 7,940 | 17,500 |
| 39.4 | $1\frac{9}{16}$ | 120.7 | $4\frac{3}{4}$ | 0.984 | 0.6615 | 8,840 | 19,500 |
| 41.2 | $1\frac{5}{8}$ | 127.0 | 5 | 1.094 | 0.7348 | 9,750 | 21,500 |
| 44.5 | $1\frac{3}{4}$ | 140.0 | $5\frac{1}{2}$ | 1.312 | 0.8818 | 11,550 | 25,500 |
| 50.8 | 2 | 152.4 | 6 | 1.576 | 1.059 | 13,610 | 30,000 |
| 52.4 | $2\frac{1}{16}$ | 165.1 | $6\frac{1}{2}$ | 1.823 | 1.225 | 15,420 | 34,000 |
| 57.2 | $2\frac{1}{4}$ | 177.8 | 7 | 2.144 | 1.441 | 17,460 | 38,500 |
| 63.5 | $2\frac{1}{2}$ | 190.5 | $7\frac{1}{2}$ | 2.450 | 1.646 | 19,730 | 43,500 |
| 66.7 | $2\frac{3}{8}$ | 203.2 | 8 | 2.799 | 1.881 | 22,220 | 49,000 |
| 73.0 | $2\frac{7}{8}$ | 215.9 | $8\frac{1}{2}$ | 3.136 | 2.107 | 24,940 | 55,000 |
| 76.2 | 3 | 228.6 | 9 | 3.543 | 2.381 | 27,670 | 61,000 |
| 79.4 | $3\frac{1}{8}$ | 241.3 | $9\frac{1}{4}$ | 3.936 | 2.645 | 30,390 | 67,000 |
| 82.5 | $3\frac{1}{4}$ | 254.0 | 10 | 4.375 | 2.940 | 33,110 | 73,000 |

* Four-strand, medium-laid rope when ordered may run up to 7% heavier than three-strand rope of the same size, and must show 95% of the strength required for three-strand rope of the same size.

132 TABLE 76.—Mechanical Properties of Hardwoods Grown in U. S. (Metric Units)

| Common and botanical name. | Specific gravity, oven-dry, based on | | Static bending. | | | Impact bend- ing. | | Compression. | | | Shear. | Ten- sion. | Hard- ness |
|---|--------------------------------------|----------------|-----------------------------|--|---|-----------------------------|------------------------------------|--------------------|-----------|--|---|--|--------------------------|
| | vol. when green. | vol. oven-dry. | P-limit, kg/mm ² | Modulus of rupture, kg/mm ² | Modulus of elasticity, kg/mm ² | P-limit, kg/mm ² | 22.7 kg hammer fall for failure—m. | Parallel to grain. | | Perpendicular to grain P-limit, kg/mm ² | Parallel to grain ult. st. kg/mm ² | Perpendicular to grain ult. st. kg/mm ² | Load 1/4 in. 3 m. d. bar |
| | | | | | | | | P-limit | Ultimate. | | | | end kg |
| 1 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
| Alder, red. (<i>Alnus oregona</i>) | 0.37 | 0.43 | 2.65 | 4.55 | 830 | 5.60 | 0.56 | 1.85 | 2.10 | 0.22 | 0.54 | 0.27 | 250 |
| Ash, black. (<i>Fraxinus nigra</i>) | 0.46 | 0.53 | 1.85 | 4.20 | 720 | 5.10 | 0.81 | 1.15 | 1.60 | 0.31 | 0.61 | 0.35 | 270 |
| Ash, white (forest grown) (<i>Fraxinus americana</i>) | 0.52 | 0.60 | 3.45 | 6.40 | 950 | 8.25 | 0.91 | 2.30 | 2.70 | 0.57 | 0.89 | 0.44 | 455 |
| Ash, white (second growth) (<i>Fraxinus americana</i>) | 0.58 | 0.71 | 4.30 | 7.60 | 1150 | 9.70 | 1.19 | 2.70 | 2.90 | 0.56 | 1.13 | 0.56 | 515 |
| Aspen. (<i>Populus tremuloides</i>) | 0.36 | 0.42 | 2.05 | 3.75 | 590 | 4.85 | 0.71 | 1.10 | 1.50 | 0.14 | 0.44 | 0.13 | 120 |
| Basswood. (<i>Tilia americana</i>) | 0.33 | 0.40 | 1.90 | 3.50 | 725 | 4.35 | 0.43 | 1.20 | 1.55 | 0.15 | 0.43 | 0.20 | 125 |
| Beech. (<i>Fagus alropinicea</i>) | 0.54 | 0.66 | 3.15 | 5.80 | 875 | 7.30 | 1.02 | 1.80 | 2.30 | 0.43 | 0.85 | 0.56 | 430 |
| Birch, paper. (<i>Betula papyrifera</i>) | 0.47 | 0.60 | 2.05 | 4.10 | 710 | 5.50 | 1.14 | 1.20 | 1.55 | 0.21 | 0.56 | 0.27 | 180 |
| Birch, yellow. (<i>Betula lutea</i>) | 0.54 | 0.66 | 3.25 | 6.05 | 1080 | 8.25 | 1.02 | 1.90 | 2.40 | 0.32 | 0.78 | 0.34 | 370 |
| Butternut. (<i>Juglans cinerea</i>) | 0.36 | 0.42 | 2.05 | 3.80 | 680 | 5.15 | 0.61 | 1.40 | 1.70 | 0.19 | 0.53 | 0.30 | 185 |
| Cherry, black. (<i>Prunus serotina</i>) | 0.47 | 0.53 | 2.95 | 5.65 | 920 | 7.20 | 0.84 | 2.10 | 2.50 | 0.31 | 0.80 | 0.40 | 340 |
| Chestnut. (<i>Castanea dentata</i>) | 0.40 | 0.46 | 2.20 | 3.95 | 655 | 5.55 | 0.61 | 1.45 | 1.75 | 0.27 | 0.56 | 0.30 | 240 |
| Cottonwood. (<i>Populus deltoides</i>) | 0.37 | 0.43 | 2.05 | 3.75 | 710 | 5.05 | 0.53 | 1.25 | 1.60 | 0.17 | 0.48 | 0.20 | 175 |
| Cucumber tree. (<i>Magnolia acuminata</i>) | 0.44 | 0.52 | 2.95 | 5.20 | 1100 | 6.55 | 0.76 | 1.95 | 2.20 | 0.29 | 0.70 | 0.31 | 270 |
| Dogwood (flowering). (<i>Cornus florida</i>) | 0.61 | 0.80 | 3.40 | 6.20 | 830 | 5.00 | 1.47 | — | 2.55 | 0.73 | 1.07 | — | 640 |
| Elm, cork. (<i>Ulmus racemosa</i>) | 0.58 | 0.66 | 3.25 | 6.70 | 840 | 7.75 | 1.27 | 2.00 | 2.70 | 0.53 | 0.89 | 0.47 | 445 |
| Elm, white. (<i>Ulmus americana</i>) | 0.44 | 0.54 | 2.55 | 4.85 | 725 | 5.70 | 0.80 | 1.60 | 2.00 | 0.28 | 0.65 | 0.39 | 275 |
| Gum, blue. (<i>Eucalyptus globulus</i>) | 0.62 | 0.80 | 5.35 | 7.85 | 1430 | 10.00 | 1.02 | 3.40 | 3.70 | 0.72 | 1.09 | 0.45 | 595 |
| Gum, cotton. (<i>Nyssa aquatica</i>) | 0.46 | 0.52 | 2.95 | 5.15 | 740 | 6.30 | 0.76 | 1.95 | 2.40 | 0.42 | 0.84 | 0.42 | 365 |
| Gum, red. (<i>Liquidambar styraciflua</i>) | 0.44 | 0.53 | 2.60 | 4.80 | 810 | 7.05 | 0.84 | 1.70 | 1.95 | 0.32 | 0.75 | 0.36 | 285 |
| Hickory pecan. (<i>Ilicoria pecan</i>) | 0.60 | 0.69 | 3.65 | 6.90 | 960 | 8.65 | 1.35 | 2.15 | 2.80 | 0.63 | 1.04 | 0.48 | 575 |
| Hickory, shagbark. (<i>Ilicoria ovala</i>) | 0.64 | — | 4.15 | 7.75 | 1105 | 10.10 | 1.88 | 2.40 | 3.20 | 0.70 | 0.93 | — | — |
| Holly, American. (<i>Ilex opaca</i>) | 0.50 | 0.61 | 2.40 | 4.55 | 630 | 6.25 | 1.30 | 1.40 | 1.85 | 0.43 | 0.80 | 0.43 | 390 |
| Laurel, mountain. (<i>Kalmia latifolia</i>) | 0.62 | 0.74 | 4.10 | 5.90 | 650 | 7.20 | 0.81 | — | 3.00 | 0.78 | 1.18 | — | 635 |
| Locust, black. (<i>Robinia pseudacacia</i>) | 0.65 | 0.71 | 6.20 | 9.70 | 1300 | 12.90 | 1.12 | 4.40 | 4.80 | 1.01 | 1.24 | 0.54 | 740 |
| Locust, honey. (<i>Gleditsia triacanthos</i>) | 0.60 | 0.67 | 3.95 | 7.20 | 910 | 8.30 | 1.20 | 2.35 | 3.10 | 1.00 | 1.17 | 0.66 | 655 |
| Magnolia (evergreen). (<i>Magnolia foetida</i>) | 0.46 | 0.53 | 2.55 | 4.80 | 780 | 6.20 | 1.37 | 1.55 | 1.90 | 0.40 | 0.73 | 0.43 | 355 |
| Maple, silver. (<i>Acer saccharinum</i>) | 0.44 | 0.51 | 2.20 | 4.10 | 660 | 4.80 | 0.74 | 1.35 | 1.75 | 0.32 | 0.74 | 0.39 | 305 |
| Maple, sugar. (<i>Acer saccharum</i>) | 0.56 | 0.66 | 3.50 | 6.40 | 1040 | 8.50 | 0.91 | 2.20 | 2.80 | 0.53 | 0.97 | 0.54 | 455 |
| Oak, canyon live. (<i>Quercus chrysolepis</i>) | 0.70 | 0.84 | 4.45 | 7.45 | 945 | 7.90 | 1.20 | 2.85 | 3.30 | 1.04 | 1.20 | 0.68 | 720 |
| Oak, red. (<i>Quercus rubra</i>) | 0.56 | 0.65 | 2.60 | 5.40 | 910 | 7.30 | 1.04 | 1.65 | 2.25 | 0.51 | 0.79 | 0.52 | 465 |
| Oak, white. (<i>Quercus alba</i>) | 0.60 | 0.71 | 3.30 | 5.85 | 880 | 7.55 | 1.07 | 2.10 | 2.50 | 0.59 | 0.88 | 0.54 | 510 |
| Persimmon. (<i>Diospyros virginiana</i>) | 0.64 | 0.78 | 3.95 | 7.05 | 965 | 8.50 | 1.04 | 2.15 | 2.95 | 0.78 | 1.03 | 0.54 | 565 |
| Poplar, yellow. (<i>Liriodendron tulipifera</i>) | 0.37 | 0.42 | 2.25 | 3.95 | 830 | 5.65 | 0.43 | 1.40 | 1.80 | 0.22 | 0.56 | 0.32 | 190 |
| Sycamore. (<i>Platanus occidentalis</i>) | 0.46 | 0.54 | 2.30 | 4.60 | 745 | 6.20 | 0.84 | 1.70 | 2.00 | 0.32 | 0.71 | 0.44 | 320 |
| Walnut, black. (<i>Juglans nigra</i>) | 0.51 | 0.56 | 3.80 | 6.70 | 1000 | 8.40 | 0.94 | 2.55 | 3.05 | 0.42 | 0.86 | 0.43 | 435 |
| Willow, black. (<i>Salix nigra</i>) | 0.34 | 0.41 | 1.25 | 2.75 | 395 | 3.60 | 0.91 | 0.70 | 1.05 | 0.15 | 0.44 | 0.30 | 160 |

NOTE.—Results of tests on sixty-eight species; test specimens, small clear pieces, 50.8 by 50.8 mm in section, 762 mm for bending; others, shorter. Data taken from Bulletin 556, Forest Service, U. S. Dept. of Agriculture, containing data on 13 tests. See pages 133 and 135 for explanation of columns.

TABLE 77.—Mechanical Properties of Conifers Grown in U. S. (Metric Units)

| Common and botanical name. | Specific gravity, oven-dry, based on | | Static bending. | | | Impact bending. | | Compression. | | | Shear. | Tension. | Hardness. | |
|--|--------------------------------------|-----------|-----------------------------|--|---|-----------------------------|-------------------------------------|--------------------|---------|--|---|--|-----------------------------------|-----|
| | | | P-limit, kg/mm ² | Modulus of rupture, kg/mm ² | Modulus of elasticity, kg/mm ² | P-limit, kg/mm ² | 22.7 kg hammer fall for failure — m | Parallel to grain. | | Perpendicular to grain P-limit, kg/mm ² | Parallel to grain ult. st. kg/mm ² | Perpendicular to grain ult. st. kg/mm ² | Load to 1/2 imbed 11.3 mm d. ball | |
| | P-limit. | Ultimate. | | | | | | end kg | side kg | | | | | |
| | | | | | | | | | | | | | kg/mm ² | |
| 1 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 |
| incense..... | 0.35 | 0.36 | 2.75 | 4.35 | 590 | 5.15 | 0.43 | 2.00 | 2.20 | 0.32 | 0.53 | 0.20 | 260 | 175 |
| <i>cedrus deccarens</i>) Port Orford..... | 0.41 | 0.47 | 2.75 | 4.80 | 1055 | 6.55 | 0.64 | 2.10 | 2.30 | 0.27 | 0.62 | 0.17 | 255 | 220 |
| <i>aeconyphus laesoniana</i>) western red..... | 0.31 | 0.34 | 2.30 | 3.05 | 670 | 5.05 | 0.43 | 1.75 | 2.00 | 0.22 | 0.51 | 0.15 | 195 | 118 |
| <i>ya plicata</i>) white..... | 0.29 | 0.32 | 1.85 | 2.95 | 450 | 3.75 | 0.38 | 1.00 | 1.40 | 0.20 | 0.44 | 0.17 | 145 | 104 |
| <i>ya occidentalis</i>) s, bald..... | 0.41 | 0.47 | 2.80 | 4.80 | 835 | 5.60 | 0.61 | 2.20 | 2.45 | 0.33 | 0.58 | 0.20 | 215 | 175 |
| <i>cedrium distichum</i>) tabilis..... | 0.37 | 0.42 | 2.75 | 4.45 | 915 | 5.50 | 0.53 | 1.70 | 2.00 | 0.22 | 0.47 | 0.17 | 165 | 140 |
| <i>es amabilis</i>) lsam..... | 0.34 | 0.41 | 2.10 | 3.45 | 675 | 4.85 | 0.41 | 1.55 | 1.70 | 0.15 | 0.43 | 0.23 | 135 | 135 |
| <i>es balsamea</i>) Douglas (1)..... | 0.45 | 0.52 | 3.50 | 5.50 | 1110 | 6.60 | 0.63 | 2.40 | 2.80 | 0.37 | 0.64 | 0.14 | 230 | 215 |
| <i>udotsuga taxifolia</i>) Douglas (2)..... | 0.40 | 0.44 | 2.55 | 4.50 | 830 | 6.40 | 0.51 | 1.80 | 2.10 | 0.32 | 0.62 | 0.25 | 205 | 180 |
| <i>udotsuga taxifolia</i>) ind..... | 0.37 | 0.42 | 2.55 | 4.30 | 915 | 5.70 | 0.56 | 1.90 | 2.10 | 0.24 | 0.53 | 0.16 | 190 | 165 |
| <i>es grandis</i>) ble..... | 0.35 | 0.41 | 2.40 | 4.00 | 900 | 5.55 | 0.51 | 1.70 | 1.90 | 0.22 | 0.49 | 0.13 | 135 | 115 |
| <i>es nobilis</i>) ute..... | 0.35 | 0.44 | 2.75 | 4.20 | 795 | 5.05 | 0.46 | 1.85 | 1.95 | 0.31 | 0.51 | 0.18 | 175 | 150 |
| <i>es concolor</i>) ck, eastern..... | 0.38 | 0.44 | 2.95 | 4.70 | 790 | 5.55 | 0.51 | 1.90 | 2.30 | 0.35 | 0.62 | 0.18 | 230 | 185 |
| <i>ga canadensis</i>) ck, western..... | 0.38 | 0.43 | 2.40 | 4.30 | 835 | 5.50 | 0.51 | 1.60 | 2.05 | 0.25 | 0.57 | 0.18 | 245 | 195 |
| <i>ga heterophylla</i>) western..... | 0.48 | 0.59 | 3.25 | 5.25 | 950 | 6.60 | 0.61 | 2.30 | 2.70 | 0.39 | 0.65 | 0.16 | 215 | 205 |
| <i>ix occidentalis</i>) uban..... | 0.58 | 0.68 | 3.95 | 6.20 | 1150 | 7.95 | 0.94 | 2.80 | 3.15 | 0.41 | 0.72 | 0.20 | 260 | 285 |
| <i>us heterophylla</i>) obollos..... | 0.50 | 0.59 | 3.10 | 5.30 | 970 | 6.70 | 0.81 | 2.00 | 2.50 | 0.39 | 0.63 | 0.20 | 185 | 205 |
| <i>ustada</i>) odgepole..... | 0.38 | 0.44 | 2.10 | 3.85 | 760 | 5.05 | 0.51 | 1.50 | 1.85 | 0.22 | 0.49 | 0.15 | 145 | 150 |
| <i>us contorta</i>) ngleaf..... | 0.55 | 0.64 | 3.80 | 6.10 | 1150 | 7.60 | 0.86 | 2.70 | 3.10 | 0.42 | 0.75 | 0.20 | 250 | 270 |
| <i>us palustris</i>) Norway..... | 0.44 | 0.51 | 2.60 | 4.50 | 970 | 5.35 | 0.71 | 1.75 | 2.20 | 0.25 | 0.55 | 0.13 | 165 | 155 |
| <i>us resinosa</i>) itch..... | 0.47 | 0.54 | 2.60 | 4.70 | 790 | 6.40 | 0.74 | 1.50 | 2.15 | 0.36 | 0.67 | 0.25 | 210 | 220 |
| <i>us rigida</i>) hortleaf..... | 0.50 | 0.58 | 3.15 | 5.65 | 1020 | 7.90 | 0.99 | 2.50 | 2.70 | 0.34 | 0.63 | 0.23 | 220 | 255 |
| <i>us echinata</i>) ugar..... | 0.36 | 0.39 | 2.30 | 3.75 | 685 | 4.70 | 0.43 | 1.65 | 1.85 | 0.25 | 0.50 | 0.19 | 150 | 145 |
| <i>us lambertiana</i>) western white..... | 0.39 | 0.45 | 2.45 | 4.00 | 935 | 5.35 | 0.58 | 1.95 | 2.15 | 0.21 | 0.50 | 0.18 | 150 | 150 |
| <i>us monticola</i>) western yellow..... | 0.38 | 0.42 | 3.20 | 3.65 | 710 | 4.70 | 0.48 | 1.45 | 1.75 | 0.24 | 0.48 | 0.20 | 140 | 145 |
| <i>us ponderosa</i>) white..... | 0.36 | 0.39 | 2.40 | 3.75 | 750 | 4.55 | 0.46 | 1.65 | 1.90 | 0.22 | 0.45 | 0.18 | 135 | 135 |
| <i>us strobus</i>) red..... | 0.48 | 0.41 | 2.40 | 4.00 | 830 | 5.05 | 0.46 | 1.65 | 1.95 | 0.25 | 0.54 | 0.15 | 190 | 160 |
| <i>ga rubens</i>) a, Sitka..... | 0.34 | 0.37 | 2.10 | 3.85 | 830 | 5.05 | 0.74 | 1.60 | 1.85 | 0.23 | 0.55 | 0.16 | 195 | 170 |
| <i>ea sitchensis</i>) ack..... | 0.49 | 0.56 | 2.95 | 5.05 | 875 | 5.50 | 0.71 | 2.20 | 2.45 | 0.34 | 0.66 | 0.18 | 180 | 170 |
| <i>ix laricina</i>) western..... | 0.60 | 0.67 | 4.55 | 7.10 | 695 | 9.20 | 0.97 | 2.40 | 3.25 | 0.73 | 1.14 | 0.32 | 610 | 520 |
| <i>cus brevifolia</i>) | | | | | | | | | | | | | | |

NOTE. — The data above are extracted from tests on one hundred and twenty-six species of wood made at the Forest Products Laboratory, Madison, Wisconsin. Bulletin 556 records results of tests on air-dry timber also, but only data on green timber are shown. The data are based on a larger number of tests and on tests which are not influenced by variations in moisture content. The data of dry material usually exceeds that of green material, but allowable working stresses in design should be based on strengths of timber, inasmuch as the increase of strength due to drying is a variable, uncertain factor and likely to be offset by defects. Specimens were two inches square, by lengths as shown.

COLUMN NOTES. — 2, Locality where grown, — see Tables 78 and 79; 3, Moisture includes all matter volatile at 100°C expressed as per cent of ordinary weight; 5, Weight, air-dry is for wood with 12 per cent moisture; 6, See metric unit tables 76 and 77; 6-10, 762 mm (30 in.) long specimen on 711.2 mm (28 in.) span, with center.

UNIT TABLES.

| Common and botanical name. | Locality where grown. | Moisture content, green, per cent. | Weight. | | Static bending. | | | Impact bending. | Compression. | | Shear. | Tension. |
|---|---------------------------|------------------------------------|--------------------|----------|-----------------------------|--|---|-----------------------------|--------------------|--|--|---|
| | | | Green. | Air-dry. | P-limit, lb/in ² | Modulus of rupture, lb/in ² | Modulus of elasticity 1000 X lb/in ² | P-limit, lb/in ² | Parallel to grain. | Perpendicular to grain, P-limit lb/in ² | Parallel to grain, ult. st. lb/in ² | Perpendicular to grain, ult. st. lb/in ² |
| | | | | | | | | | P-limit. | | | |
| | | | lb/ft ³ | | | | | | lb/in ² | | | |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 11 | 13 | 14 | 15 |
| Alder, red. (<i>Alnus oregona</i>) | Wash. | 98 | 46 | 28 | 3800 | 6500 | 1170 | 8000 | 2650 | 310 | 770 | 390 |
| Ash, black. (<i>Fraxinus nigra</i>) | Mich. and Wis. | 83 | 53 | 34 | 2600 | 6000 | 1020 | 7200 | 1620 | 430 | 870 | 490 |
| Ash, white (forest grown). (<i>Fraxinus americana</i>) | Ark. and W. Va. | 43 | 46 | 40 | 4900 | 9100 | 1350 | 11700 | 3230 | 800 | 1260 | 620 |
| Ash, white (2d growth). (<i>Fraxinus americana</i>) | N. Y. | 40 | 51 | 46 | 6100 | 10800 | 1640 | 13800 | 3820 | 790 | 1600 | 790 |
| Aspen (<i>Populus tremuloides</i>) | Wis. | 107 | 47 | 27 | 2900 | 5300 | 840 | 6900 | 1620 | 200 | 620 | 180 |
| Basswood (<i>Tilia americana</i>) | Wis. and Pa. | 103 | 41 | 26 | 2700 | 5000 | 1030 | 6200 | 1710 | 210 | 610 | 280 |
| Beech (<i>Fagus atropunica</i>) | Ind. and Pa. | 62 | 55 | 44 | 4500 | 8200 | 1240 | 10400 | 2550 | 610 | 1210 | 760 |
| Birch, paper. (<i>Betula papyrifera</i>) | Wis. and Pa. | 72 | 51 | 38 | 2900 | 5800 | 1010 | 7800 | 1650 | 300 | 790 | 380 |
| Birch, yellow. (<i>Betula lutea</i>) | Wis. | 68 | 58 | 45 | 4600 | 8600 | 1540 | 11700 | 2760 | 450 | 1110 | 480 |
| Butternut. (<i>Juglans cinerea</i>) | Tenn. and Wis. | 104 | 46 | 27 | 2900 | 5400 | 970 | 7300 | 1960 | 270 | 760 | 430 |
| Cherry, black. (<i>Prunus serotina</i>) | Pa. | 55 | 46 | 36 | 4200 | 8000 | 1310 | 10200 | 2940 | 440 | 1130 | 570 |
| Chestnut. (<i>Castanea dentata</i>) | Md. and Tenn. | 122 | 55 | 30 | 3100 | 5600 | 930 | 7900 | 2040 | 380 | 800 | 430 |
| Cottonwood. (<i>Populus deltoides</i>) | Mo. | 111 | 49 | 29 | 2900 | 5300 | 1010 | 7200 | 1770 | 240 | 680 | 410 |
| Cucumber tree (<i>Magnolia acuminata</i>) | Tenn. | 80 | 50 | 33 | 4200 | 7400 | 1560 | 9300 | 2760 | 410 | 990 | 440 |
| Dogwood (flowering). (<i>Cornus florida</i>) | Tenn. | 62 | 65 | 54 | 4800 | 8800 | 1180 | 7100 | — | 1030 | 1520 | — |
| Elm, cork. (<i>Ulmus racemosa</i>) | Wis. | 50 | 54 | 45 | 4600 | 9500 | 1190 | 11000 | 2870 | 750 | 1270 | 660 |
| Elm, white. (<i>Ulmus americana</i>) | Wis. and Pa. | 88 | 52 | 35 | 3600 | 6900 | 1030 | 8100 | 2290 | 390 | 920 | 560 |
| Gum, blue. (<i>Eucalyptus globulus</i>) | Cal. | 79 | 70 | 54 | 7600 | 11200 | 2010 | 14200 | 4870 | 1020 | 1550 | 640 |
| Gum, cotton. (<i>Nyssa aquatica</i>) | La. | 97 | 56 | 34 | 4200 | 7300 | 1050 | 9000 | 2760 | 590 | 1190 | 600 |
| Gum, red. (<i>Liquidambar styraciflua</i>) | Mo. | 81 | 50 | 36 | 3700 | 6800 | 1150 | 10000 | 2360 | 460 | 1070 | 510 |
| Hickory, pecan. (<i>Hicoria pecan</i>) | Mo. | 63 | 61 | 46 | 5200 | 9800 | 1370 | 12300 | 3040 | 960 | 1480 | 680 |
| Hickory, shagbark. (<i>Hicoria ovata</i>) | O., Miss., Pa. and W. Va. | 60 | 64 | 51 | 5900 | 11000 | 1570 | 14400 | 3430 | 1000 | 1320 | — |
| Holly, American. (<i>Ilex opaca</i>) | Tenn. | 82 | 57 | 40 | 3400 | 6500 | 900 | 8900 | 1970 | 610 | 1130 | 610 |
| Laurel, mountain. (<i>Kalmia latifolia</i>) | Tenn. | 62 | 62 | 49 | 5800 | 8400 | 920 | 10200 | — | 1110 | 1670 | — |
| Locust, black. (<i>Robinia pseudacacia</i>) | Tenn. | 40 | 58 | 49 | 8300 | 13800 | 1850 | 18300 | 6280 | 1430 | 1760 | 770 |
| Locust, honey. (<i>Gleditsia triacanthos</i>) | Mo. and Ind. | 63 | 61 | 47 | 5600 | 10200 | 1290 | 11800 | 3320 | 1420 | 1660 | 930 |
| Magnolia (evergreen). (<i>Magnolia foetida</i>) | La. | 117 | 62 | 35 | 3600 | 6800 | 1110 | 8800 | 2200 | 570 | 1040 | 610 |
| Maple, silver. (<i>Acer saccharinum</i>) | Wis. | 66 | 46 | 34 | 3100 | 5800 | 940 | 6800 | 1950 | 460 | 1050 | 560 |
| Maple, sugar. (<i>Acer saccharum</i>) | Ind., Pa. and Wis. | 60 | 56 | 44 | 5000 | 9100 | 1480 | 12100 | 3120 | 750 | 1380 | 770 |
| Oak, canyon live. (<i>Quercus chrysolepsis</i>) | Cal. | 62 | 71 | 56 | 6300 | 10600 | 1340 | 11200 | 4050 | 1480 | 1700 | 970 |
| Oak, red. (<i>Quercus rubra</i>) | Ark., La., Ind. and Tenn. | 84 | 64 | 45 | 3700 | 7700 | 1290 | 10400 | 2330 | 730 | 1120 | 740 |
| Oak, white. (<i>Quercus alba</i>) | Ark., La. and Ind. | 68 | 62 | 47 | 4700 | 8300 | 1250 | 10700 | 2990 | 830 | 1250 | 770 |
| Persimmon. (<i>Diospyros virginiana</i>) | Mo. | 58 | 63 | 53 | 5600 | 10000 | 1370 | 12100 | 3030 | 1110 | 1470 | 770 |
| Poplar, yellow. (<i>Liriodendron tulipifera</i>) | Tenn. | 64 | 38 | 28 | 3200 | 5600 | 1210 | 8000 | 2000 | 310 | 790 | 460 |
| Sycamore. (<i>Platanus occidentalis</i>) | Ind. and Tenn. | 83 | 52 | 35 | 3300 | 6500 | 1060 | 8800 | 2390 | 450 | 1000 | 630 |
| Walnut, black. (<i>Juglans nigra</i>) | Ky. | 81 | 58 | 39 | 5400 | 9500 | 1420 | 11900 | 3600 | 600 | 1220 | 570 |

NOTE.—Results of tests on sixty-eight species; test specimens, small clear pieces, 2 by 2 inches in section, 30 inches long for bending; others, shorter. Tested in a green condition. Data taken from Bulletin 556, Forest Service, U. S. Dept. of Agriculture, containing data on 130,000 tests. See pages 133 and 135 for explanation of columns.

TABLE 79.—Mechanical Properties of Conifers Grown in U. S. (English Units)

| Common and botanical name. | Locality where grown. | Moisture content, green, per cent. | Weight. | | Static bending. | | | Impact bending. | Compression. | | Shear. | Tension. |
|--|------------------------------------|------------------------------------|---------|----------|------------------------------|---|--|------------------------------|-------------------|---|---|--|
| | | | Green. | Air-dry. | P-limit, lb./in ² | Modulus of rupture, lb./in ² | Modulus of elasticity 1000 × lb./in ² | P-limit, lb./in ² | Parallel to grain | Perpendicular to grain, P-limit lb./in ² | Parallel to grain, ult. st. lb./in ² | Perpendicular to grain, ult. st. lb./in ² |
| | | | | | | | | | P-limit. | | | |
| | | | | | | | | | | | | |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 11 | 13 | 14 | 15 |
| Cedar, incense..... (<i>Libocedrus decurrens</i>) | Cal. and Ore. | 108 | 45 | 24 | 3900 | 6200 | 840 | 7300 | 2870 | 460 | 830 | 280 |
| Cedar, Port Orford..... (<i>Chamaecyparis lawsoniana</i>) | Ore. | 52 | 39 | 31 | 3900 | 6800 | 1500 | 9300 | 3970 | 380 | 880 | 240 |
| Cedar, western red..... (<i>Thuja plicata</i>) | Wash. and Mont. | 39 | 27 | 23 | 3300 | 5200 | 950 | 7100 | 2500 | 310 | 720 | 210 |
| Cedar, white..... (<i>Thuja occidentalis</i>) | Wis. | 55 | 28 | 21 | 2600 | 4200 | 640 | 5300 | 1420 | 290 | 620 | 240 |
| Cypress, bald..... (<i>Taxodium distichum</i>) | La. and Mo. | 87 | 48 | 30 | 4000 | 6800 | 1190 | 8000 | 3100 | 470 | 820 | 280 |
| Fir, amabilis..... (<i>Abies amabilis</i>) | Ore. and Wash. | 102 | 47 | 27 | 3900 | 6300 | 1300 | 7800 | 2380 | 320 | 670 | 240 |
| Fir, balsam..... (<i>Abies balsamea</i>) | Wis. | 117 | 45 | 25 | 3000 | 4900 | 960 | 6900 | 2220 | 210 | 610 | 180 |
| Fir, Douglas (1)..... (<i>Pseudotsuga taxifolia</i>) | Wash. and Ore. | 36 | 38 | 34 | 5000 | 7800 | 1580 | 9400 | 3400 | 530 | 910 | 200 |
| Fir, Douglas (2)..... (<i>Pseudotsuga taxifolia</i>) | Mont. and Wyo. | 38 | 34 | 32 | 3600 | 6400 | 1180 | 9100 | 2520 | 450 | 880 | 350 |
| Fir, grand..... (<i>Abies grandis</i>) | Mont. and Ore. | 94 | 44 | 27 | 3600 | 6100 | 1300 | 8100 | 2680 | 340 | 700 | 230 |
| Fir, noble..... (<i>Abies nobilis</i>) | Ore. | 41 | 31 | 26 | 3400 | 5700 | 1280 | 7900 | 2370 | 310 | 700 | 180 |
| Fir, white..... (<i>Abies concolor</i>) | Cal. | 156 | 56 | 26 | 3900 | 6000 | 1130 | 7200 | 2610 | 440 | 730 | 260 |
| Hemlock (eastern)..... (<i>Tsuga canadensis</i>) | Tenn. and Wis. | 105 | 48 | 29 | 4200 | 6700 | 1120 | 7900 | 2710 | 500 | 880 | 260 |
| Hemlock (western)..... (<i>Tsuga heterophylla</i>) | Wash. | 71 | 41 | 29 | 3400 | 6100 | 1190 | 7800 | 2290 | 350 | 810 | 260 |
| Larch, western..... (<i>Larix occidentalis</i>) | Mont. and Wash. | 58 | 48 | 37 | 4600 | 7500 | 1350 | 9400 | 3250 | 560 | 920 | 230 |
| Pine, Cuban..... (<i>Pinus heterophylla</i>) | Fla. | 47 | 53 | 45 | 5600 | 8800 | 1630 | 11300 | 3950 | 590 | 1030 | 290 |
| Pine, loblolly..... (<i>Pinus taeda</i>) | Fla., N. and S. Car. | 70 | 54 | 39 | 4400 | 7500 | 1380 | 9500 | 2870 | 550 | 900 | 280 |
| Pine, lodgepole..... (<i>Pinus contorta</i>) | Col., Mont. and Wyo. | 65 | 39 | 28 | 3000 | 5500 | 1080 | 7200 | 2100 | 310 | 690 | 220 |
| Pine, longleaf..... (<i>Pinus palustris</i>) | Fla., La. and Miss. | 47 | 50 | 43 | 5400 | 8700 | 1630 | 10800 | 3840 | 600 | 1070 | 290 |
| Pine, Norway..... (<i>Pinus resinosa</i>) | Wis. | 54 | 42 | 34 | 3700 | 6400 | 1380 | 7500 | 2470 | 360 | 780 | 190 |
| Pine, pitch..... (<i>Pinus rigida</i>) | Tenn. | 85 | 54 | 35 | 3700 | 6700 | 1120 | 9100 | 2100 | 510 | 950 | 350 |
| Pine, shortleaf..... (<i>Pinus echinata</i>) | Ark. and La. | 64 | 50 | 37 | 4500 | 8000 | 1450 | 11200 | 3650 | 480 | 890 | 330 |
| Pine, sugar..... (<i>Pinus lambertiana</i>) | Cal. | 123 | 50 | 26 | 3300 | 5300 | 970 | 6700 | 2340 | 350 | 710 | 270 |
| Pine, western white..... (<i>Pinus monticola</i>) | Mont. | 58 | 39 | 30 | 3500 | 5700 | 1330 | 7600 | 2770 | 300 | 710 | 250 |
| Pine, western yellow..... (<i>Pinus ponderosa</i>) | Col., Mont., Ariz., Wash. and Cal. | 95 | 46 | 28 | 3100 | 5200 | 1010 | 6700 | 2080 | 340 | 680 | 280 |
| Pine, white..... (<i>Pinus strobus</i>) | Wis. | 74 | 39 | 27 | 3400 | 5300 | 1070 | 6500 | 2370 | 310 | 640 | 260 |
| Spruce, red..... (<i>Picea rubens</i>) | N. H. and Tenn. | 43 | 34 | 28 | 3400 | 5700 | 1180 | 7200 | 2360 | 350 | 770 | 220 |
| Spruce, Sitka..... (<i>Picea sitchensis</i>) | Wash. | 53 | 33 | 26 | 3000 | 5500 | 1180 | 7900 | 2280 | 330 | 780 | 230 |
| Tamarack..... (<i>Larix laricina</i>) | Wis. | 52 | 47 | 38 | 4200 | 7200 | 1240 | 7800 | 3010 | 480 | 860 | 260 |
| Yew, western..... (<i>Taxus brevifolia</i>) | Wash. | 44 | 54 | 45 | 6500 | 10100 | 990 | 13100 | 3400 | 1040 | 1620 | 450 |

COLUMN NOTES (continued).—(7) recommended allowable working stress (interior construction): $\frac{1}{2}$ tabular value; experimental results on tests of air-dry timber in small clear pieces average 50 per cent higher; kiln-dry, double tabular values; (10) repeated falls of 50-lb. hammer from increasing heights; 11-12, 293.2-mm (8 in.) long specimen loaded on ends with deformations measured in a 152.4-mm (6 in.) gage length; (12) allowable working stress $\frac{1}{2}$ tabular crushing strength; (13) 152.4-mm (6 in.) long block loaded on its side with a central bearing area of 2580.6-mm² (4 in.²) allowable working stress, $\frac{1}{2}$ tabular value. (14) 50.8-mm by 50.8-mm (2 in.) projecting lip sheared from block; allowable working stress, $\frac{1}{2}$ tabular value; (15) 63.5-mm (2½ in.) specimen with 25.4-mm (1 in.) free loaded length; allowable working stress, $\frac{1}{2}$ tabular value. (16-17) for values in lbs. multiply values of metric tables by 2.2.

ELASTIC MODULI

TABLE 80.—Rigidity Modulus

If to the four consecutive faces of a cube a tangential stress is applied, opposite in direction on adjacent sides, the modulus of rigidity is obtained by dividing the numerical value of the tangential stress per unit area (kg per sq. mm) by the number representing the change of angles on the non-stressed faces, measured in radians.

| Substance. | Rigidity Modulus. | Reference. | Substance. | Rigidity Modulus. | Reference. |
|---------------------------------------|-------------------|------------|----------------------------|-------------------|------------|
| Aluminum | 3350 | 14 | Quartz fibre | 2888 | 20 |
| “ cast | 2580 | 5 | “ “ | 2380 | 21 |
| Brass | 3550 | 10 | Silver | 2960 | 5 |
| “ | 3715 | 11 | “ | 2650 | 10 |
| “ cast, 60 Cu + 12 Sn | 3700 | 5 | “ | 2566 | 16 |
| Bismuth, slowly cooled | 1240 | 5 | “ hard-drawn | 2816 | 11 |
| Bronze, cast, 88 Cu + 12 Sn | 4060 | 5 | Steel | 8290 | 16 |
| Cadmium, cast | 2450 | 5 | “ cast | 7458 | 15 |
| Copper, cast | 4780 | 5 | “ cast, coarse gr. | 8070 | 5 |
| “ | 4213 | 18 | “ silver- | 7872 | 11 |
| “ | 4450 | 10 | Tin, cast | 1730 | 5 |
| “ | 4664 | 19 | “ | 1543 | 19 |
| Gold | 2850 | 5 | Zinc | 3880 | 5 |
| “ | 3950 | 14 | “ | 3820 | 19 |
| Iron, cast | 5210 | 5 | Platinum | 6630 | 16 |
| “ | 6706 | 15 | “ | 6220 | 22 |
| “ | 7975 | 10 | Glass | 2350 | — |
| “ | 6940 | 7 | “ | 2730 | — |
| “ | 8108 | 16 | Clay rock | 1770 | 23 |
| “ | 7505 | 14 | Granite | 1280 | 23 |
| Magnesium, cast | 1710 | 5 | Marble | 1190 | 23 |
| Nickel | 7820 | 5 | Slate | 2290 | 23 |
| Phosphor bronze | 4359 | 11 | | | |

References 1-16, see Table 48.
 17 Gratz, Wied. Ann. 28, 1886.
 18 Savart, Pogg. Ann. 16, 1829.
 19 Kiewiet, Diss. Göttingen, 1886.
 20 Threlfall, Philos. Mag. (5) 30, 1890.
 21 Boys, Philos. Mag. (5) 30, 1890.
 22 Thomson, Lord Kelvin.
 23 Gray and Milne.
 24 Adams-Coker, Carnegie Publ. No. 46, 1906.

TABLE 81.—Variation of the Rigidity Modulus with the Temperature

$n_t = n_0 (1 - \alpha t - \beta t^2 - \gamma t^3)$, where t = temperature Centigrade.

| Substance. | n_0 | $\alpha 10^6$ | $\beta 10^8$ | $\gamma 10^{10}$ | Authority. |
|--------------------|-------|---------------|--------------|------------------|-------------------------------------|
| Brass | 2652 | 2158 | 48 | 32 | Pisati, Nuovo Cimento, 5, 34, 1879. |
| “ | 3200 | 455 | 36 | — | Kohlrausch-Loomis, Pogg. Ann. 141. |
| Copper | 3972 | 2716 | —23 | 47 | Pisati, loc. cit. |
| “ | 3900 | 572 | 28 | — | K and L, loc. cit. |
| Iron | 8108 | 206 | 19 | —11 | Pisati, loc. cit. |
| “ | 6940 | 483 | 12 | — | K and L, loc. cit. |
| Platinum | 6632 | 111 | 50 | —8 | Pisati, loc. cit. |
| Silver | 2566 | 387 | 38 | 11 | “ “ “ |
| Steel | 8290 | 187 | 59 | —9 | “ “ “ |

$n_t^* = n_{15} [1 - \alpha (t - 15)]$; Horton, Philos. Trans. 204 A, 1905.

| | | | | | | | | |
|--------------------------|-------|-------------------|----------|-------|-------------------|---------|-------|-------------------|
| Copper | 4.37* | $\alpha = .00039$ | Platinum | 6.46* | $\alpha = .00012$ | Tin | 1.50* | $\alpha = .00416$ |
| Copper (com- mercial) | 3.80 | .00038 | Gold | 2.45 | .00031 | Lead | 0.80 | .00164 |
| Iron | 8.26 | .00029 | Silver | 2.67 | .00048 | Cadmium | 2.31 | .0058 |
| Steel | 8.45 | .00026 | Aluminum | 2.55 | .00148 | Quartz | 3.00 | .00012 |

* Modulus of rigidity in 10^{11} dynes per sq. cm

TABLE 82.—Interior Friction at Low Temperatures

C is the damping coefficient for infinitely small oscillations; T, the period of oscillation in seconds; N, the second modulus of elasticity. Guye and Schapper, C. R. 150, p. 963, 1910.

| Substance | | Cu | Ni | Au | Pd | Pt | Ag | Quartz |
|-----------------------|---------------------|------|--------|--------|--------|--------|--------|--------|
| Length of wire in cm. | | 22.5 | 22.2 | 22.3 | 22.2 | 23.0 | 17.2 | 17.3 |
| Diameter in mm..... | | .643 | .411 | .609 | .553 | .812 | .601 | .612 |
| 100° C | C | | 24.1 | 1.34 | 27.5 | 1.67 | 2.98 | 55.8 |
| | T | | 2.381s | 3.831s | 3.010s | 2.579 | 1.143s | 1.808s |
| | N×10 ⁻¹¹ | | 3.32 | 7.54 | 2.55 | 5.08 | 5.77 | 2.71 |
| 0° C | C | | 5.88 | .417 | 4.82 | 1.25 | 4.60 | 7.19 |
| | T | | 2.336s | 3.754s | 2.969s | 2.571s | 1.133s | 1.759s |
| | N×10 ⁻¹¹ | | 3.45 | 7.85 | 2.62 | 5.12 | — | 2.87 |
| -195° C | C | | 3.64 | .556 | 6.36 | .744 | 3.02 | 1.64 |
| | T | | 2.274s | 3.577s | 2.902s | 2.552s | 1.111s | 1.694s |
| | N×10 ⁻¹¹ | | 3.64 | 8.65 | 2.74 | 5.19 | 6.10 | 3.18 |
| | | | | | | | | 2.20 |

TABLE 83.—Hardness

| | | | | | | | |
|------------|-------|------------|---------|-----------------|---------|--------------|---------|
| Agate | 7. | Brass | 3-4. | Iridosmium | 7. | Sulphur | 1.5-2.5 |
| Alabaster | 1.7 | Calamine | 5. | Iron | 4-5. | Stibnite | 2. |
| Alum | 2-2.5 | Calcite | 3. | Kaolin | 1. | Serpentine | 3-4. |
| Aluminum | 2. | Copper | 2.5-3. | Loess (o°) | 0.3 | Silver | 2.5-3. |
| Amber | 2-2.5 | Corundum | 9. | Magnetite | 6. | Steel | 5-8.5 |
| Andalusite | 7.5 | Diamond | 10. | Marble | 3-4. | Talc | 1. |
| Anthracite | 2.2 | Dolomite | 3.5-4. | Meerschaum | 2-3. | Tin | 1.5 |
| Antimony | 3-3 | Feldspar | 6. | Mica | 2.8 | Topaz | 8. |
| Apatite | 5. | Flint | 7. | Opal | 4-6. | Tourmaline | 7-3 |
| Aragonite | 3.5 | Fluorite | 4. | Orthoclase | 6. | Wax (o°) | 0.2 |
| Arsenic | 3.5 | Galena | 2.5 | Palladium | 4.8 | Wood's metal | 3. |
| Asbestos | 5. | Garnet | 7. | Phosphorbronze | 4. | | |
| Asphalt | 1-2. | Glass | 4.5-6.5 | Platinum | 4.3 | | |
| Augite | 6. | Gold | 2.5-3. | Platin-iridium | 6.5 | | |
| Barite | 3.3 | Graphite | 0.5-1. | Pyrite | 6.3 | | |
| Beryl | 7.8 | Gypsum | 1.6-2. | Quartz | 7. | | |
| Bell-metal | 4. | Hematite | 6. | Rock-salt | 2. | | |
| Bismuth | 2.5 | Hornblende | 5.5 | Ross' metal | 2.5-3.0 | | |
| Boric acid | 3. | Iridium | 6. | Silver chloride | 1.3 | | |

From Landolt-Börnstein-Meyerhoffer Tables: Auerbachs, Winklemann, Handb. der Phys. 1891.

TABLE 84.—Relative Hardness of the Elements (Means)

| | | | | | | | | | | | |
|----|-----|----|-----|----|-----|----|-----|----|-----|----|-----|
| C | 10. | Ir | 6.5 | Pt | 4.3 | Al | 2.9 | Se | 2.0 | In | 1.2 |
| B | 9.5 | Ge | 6.2 | Ti | 4.0 | Ag | 2.7 | Cd | 2.0 | Tl | 1.2 |
| Cr | 9. | Rh | 6. | Pd | 4.0 | Zn | 2.5 | Sr | 1.8 | Li | 0.6 |
| Ru | 7.5 | Mo | 6? | Fe | 4. | Te | 2.3 | Bi | 1.8 | K | 0.5 |
| Ta | 7. | Mn | 6. | As | 3.5 | Mg | 2.6 | Sn | 1.8 | Na | 0.4 |
| Os | 7. | Co | 5. | Sb | 3. | Au | 2.5 | Pb | 1.5 | Rb | 0.3 |
| W | 7. | Ni | 5. | Be | 3. | Ce | 2.5 | Ga | 1.5 | Cs | 0.2 |
| Si | 6.5 | Zr | 4.5 | Cu | 3.0 | S | 2.0 | Hg | 1.5 | | |

TABLE 85.—Ratio, ρ , of Transverse Contraction to Longitudinal Extension under Tensile Stress (Poisson's Ratio)

| Metal | Pb | Au | Pd | Pt | Ag | Cu | Al | Bi | Sn | Ni | Cd | Fe |
|--------|------|------|------|------|------|------|------|------|------|------|------|------|
| ρ | 0.45 | 0.42 | 0.39 | 0.39 | 0.38 | 0.35 | 0.34 | 0.33 | 0.33 | 0.31 | 0.30 | 0.28 |

From data from Physikalisch-Technischen Reichsanstalt, 1907.

ρ for: marbles, 0.27; granites, 0.24; basic-intrusives, 0.26; glass, 0.23. Adams-Coker, 1906.

ELASTICITY OF CRYSTALS *

The formulæ were deduced from experiments made on rectangular prismatic bars cut from the crystal. These bars were subjected to cross bending and twisting and the corresponding Elastic Moduli deduced. The symbols $\alpha, \beta, \gamma, \alpha_1, \beta_1, \gamma_1$ and $\alpha_2, \beta_2, \gamma_2$ represent the direction cosines of the length, the greater and the less transverse dimensions of the prism with reference to the principal axis of the crystal. E is the modulus for extension or compression, and T is the modulus for torsional rigidity. The moduli are in grams per square centimeter.

Barite.

$$\frac{10^{10}}{E} = 16.13\alpha^4 + 18.51\beta^4 + 10.42\gamma^4 + 2(38.79\beta^2\gamma^2 + 15.21\gamma^2\alpha^2 + 8.88\alpha^2\beta^2)$$

$$\frac{10^{10}}{T} = 69.52\alpha^4 + 117.66\beta^4 + 116.46\gamma^4 + 2(20.16\beta^2\gamma^2 + 85.29\gamma^2\alpha^2 + 127.35\alpha^2\beta^2)$$

Beryl (Emerald).

$$\frac{10^{10}}{E} = 4.325 \sin^4 \phi + 4.619 \cos^4 \phi + 13.328 \sin^2 \phi \cos^2 \phi \quad \left\{ \begin{array}{l} \text{where } \phi, \phi_1, \phi_2 \text{ are the angles which} \\ \text{the length, breadth, and thickness} \\ \text{of the specimen make with the} \\ \text{principal axis of the crystal.} \end{array} \right.$$

$$\frac{10^{10}}{T} = 15.00 - 3.675 \cos^4 \phi_2 - 17.536 \cos^2 \phi \cos^2 \phi_1$$

Fluorite.

$$\frac{10^{10}}{E} = 13.05 - 6.26 (\alpha^4 + \beta^4 + \gamma^4)$$

$$\frac{10^{10}}{T} = 58.04 - 50.08 (\beta^2\gamma^2 + \gamma^2\alpha^2 + \alpha^2\beta^2)$$

Pyrite.

$$\frac{10^{10}}{E} = 5.08 - 2.24 (\alpha^4 + \beta^4 + \gamma^4)$$

$$\frac{10^{10}}{T} = 18.60 - 17.95 (\beta^2\gamma^2 + \gamma^2\alpha^2 + \alpha^2\beta^2)$$

Rock salt.

$$\frac{10^{10}}{E} = 33.48 - 9.66 (\alpha^4 + \beta^4 + \gamma^4)$$

$$\frac{10^{10}}{T} = 154.58 - 77.28 (\beta^2\gamma^2 + \gamma^2\alpha^2 + \alpha^2\beta^2)$$

Sylvite.

$$\frac{10^{10}}{E} = 75.1 - 48.2 (\alpha^4 + \beta^4 + \gamma^4)$$

$$\frac{10^{10}}{T} = 306.0 - 192.8 (\beta^2\gamma^2 + \gamma^2\alpha^2 + \alpha^2\beta^2)$$

Topaz.

$$\frac{10^{10}}{E} = 4.341\alpha^4 + 3.460\beta^4 + 3.771\gamma^4 + 2(3.879\beta^2\gamma^2 + 2.856\gamma^2\alpha^2 + 2.39\alpha^2\beta^2)$$

$$\frac{10^{10}}{T} = 14.88\alpha^4 + 16.54\beta^4 + 16.45\gamma^4 + 30.89\beta^2\gamma^2 + 40.89\gamma^2\alpha^2 + 43.51\alpha^2\beta^2$$

Quartz.

$$\frac{10^{10}}{E} = 12.734 (1 - \gamma^2)^2 + 16.693 (1 - \gamma^2)\gamma^2 + 9.705\gamma^4 - 8.46\beta\gamma (3\alpha^2 - \beta^2)$$

$$\frac{10^{10}}{T} = 19.665 + 9.060\gamma_2^2 + 22.984\gamma^2\gamma_1^2 - 16.920 [(\gamma\beta_1 + \beta\gamma_1) (3\alpha\alpha_1 - \beta\beta_1) - \beta_2\gamma_2]$$

* These formulæ are taken from Voigt's papers (Wied. Ann. vols. 31, 34, and 35).

MECHANICAL PROPERTIES OF SOME SINGLE METAL CRYSTALS (BRIDGMAN)

All the following metals have an axis of rotational symmetry: Zn and Cd have a 6-fold axis (hexagonal system); Bi, Sb, Te, 3-fold, trigonal; Sn, 4-fold, tetragonal. The rotational axis is taken as the datum line. The notation of Voigt is used (Lehrbuch der Kristallphysik, Berlin, 1910). Bridgman, Proc. Amer. Acad. Arts and Sci., 60, 305, 1925.

TABLE 88.—Elastic Constants, Abs. c.g.s. units

| Constant | Zn | Cd | Bi | Sb | Te | Sn | W |
|---------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|-------------------------|
| s_{11} | 8.23×10^{-13} | 12.9×10^{-13} | 26.9×10^{-13} | 17.7×10^{-13} | 48.7×10^{-13} | 18.5×10^{-13} | 2.534×10^{-13} |
| s_{12} | +0.34 | -1.5 | -14.0 | -3.8 | -6.9 | -9.9 | -0.726 |
| s_{13} | -6.64 | -9.3 | -6.2 | -8.5 | -13.8 | -2.5 | s_{12} |
| s_{33} | 26.38 | 36.9 | 28.7 | 33.8 | 23.4 | 11.8 | s_{11} |
| s_{44} | 25.0 | 64.0 | 104.8 | 41.0 | 58.1 | 57.0 | 6.55 |
| $\frac{1}{2}s_{66}$ | $s_{11}-s_{12}$ | $s_{11}-s_{12}$ | $s_{11}-s_{12}$ | $s_{11}-s_{12}$ | $s_{11}-s_{12}$ | 67.5 | $s_{11}-s_{12}$ |
| s_{14} | 0 | 0 | +16 | -8.0 | - | 0 | 0 |

TABLE 89.—Linear Compressibility, $1/\alpha$ Pressure in kg/cm² Range 12,000 kg/cm²

| Metal | at 30° C | | at 75° C | |
|-------|-------------------------|----------------------------|-------------------------|----------------------------|
| Zn | $12.98 \times 10^{-7}p$ | $-5.32 \times 10^{-12}p^2$ | $13.55 \times 10^{-7}p$ | $-7.82 \times 10^{-12}p^2$ |
| | 1.946 | -1.11 | 2.025 | -1.47 |
| Bi | 15.92 | -11.1 | 15.80 | -11.6 |
| | 6.450 | -4.60 | 6.423 | -4.57 |
| Sb | 16.48 | -20.5 | 16.37 | -18.0 |
| | 5.256 | -4.56 | 5.091 | -3.04 |
| Te | -4.137 | +9.6 | -5.132 | +13.2 |
| | 27.48 | -52.7 | 27.77 | -53.6 |
| Sn | 6.719 | -4.07 | 6.956 | -3.91 |
| | 6.022 | -4.20 | 6.144 | -4.26 |

TABLE 90.—Cubic Compressibility

 (V/V_0) ; Pressure kg/cm² Range, 12,000 kg/cm² (calculated)

| Metal | at 30° C | | at 75° C | |
|-------|-------------------------|----------------------------|-------------------------|-----------------------------|
| Zn | $16.87 \times 10^{-7}p$ | $-8.08 \times 10^{-12}p^2$ | $17.60 \times 10^{-7}p$ | $-11.35 \times 10^{-12}p^2$ |
| Bi | 29.17 | -22.43 | 29.89 | -31.13 |
| Sb | 26.99 | -31.6 | 26.55 | -25.3 |
| Te | 50.82 | -101.1 | 50.41 | -85.6 |
| Sn | 18.76 | -13.6 | 19.24 | -13.7 |
| W | 3.18 | -1.4 | 3.18 | -1.5 |

CALCULATIONS INVOLVING THE RELATIONS BETWEEN THE TEMPERATURES, PRESSURES, VOLUMES, AND WEIGHTS OF GASES

(Abridged from S. F. Pickering, Bur. Standards Circ. 279, which see for further details.)

Simple laws.—Any amount of gas completely fills the space in which it is confined. The pressure it exerts upon the confining walls depends upon the temperature. A quantity of gas can not be specified by volume only; all three factors—volume, temperature, and pressure—must be stated. The relations between these three factors are expressed by means of the following equation,

$$pv = KT \quad (1)$$

in which p , v , and T represent simultaneous values of the pressure, volume, and absolute temperature of any definite quantity of gas, while K is a constant, the numerical value of which depends upon the quantity of gas considered and the units in which pressure, volume, and temperature are measured.

While the behavior of gases at atmospheric pressure closely approximates the equation (1), the relation is not exact. The expansion of air is nearer one 272nd of its volume at 273.1° K. per degree. For most practical purposes such errors may be neglected.

If we take weights of gases proportional to their molecular weights, a new relation of the greatest importance develops: *The value of the constant in equation (1) is the same for each gas.* It is customary to use as the unit of quantity, the mol, the number of grams of gas equal to the molecular weight. When 1 mol is the quantity considered, the resulting value of K is designated R .

| Absolute temperature | Pressure | Volume | R |
|----------------------|-----------------------------|------------|---------|
| °C + 273.1 | Atmosphere | Liter | 0.08206 |
| °C + 273.1 | mm of mercury | do | 62.37 |
| °C + 273.1 | Gram per cm ² | do | 84.79 |
| °C + 273.1 | Megabar | do | .08315 |
| °C + 273.1 | Atmosphere | Cubic feet | .002898 |
| °C + 273.1 | mm of mercury | do | 2.2024 |
| °C + 273.1 | Inches of mercury | do | .08671 |
| °C + 273.1 | Pounds per in. ² | do | .04259 |

With the mol the unit of quantity, N the number of mols of gas, equation (1) becomes

$$pv = NRT \quad (2)$$

By the use of equation (2), the above table, and a table of molecular weights, the solution of any problem involving volumes, temperatures, pressures, and weights of gases is very simple.

Mixtures of gases.—Any quantity of gas fills the space in which it is confined and exerts a pressure upon the confining walls. If an additional quantity is added, the pressure is increased in direct proportion to the quantity added. One can regard the pressure exerted by each portion of the total quantity of gas as independent of the presence of the rest. This is true if the second portion of gas is different chemically from the first (Dalton's law), provided the gases do not react chemically.

Vapor pressure and the effect of vapor pressure upon the measurement of gas.—If a volatile liquid is introduced, a portion evaporates and exerts a pressure on the confining walls. The amount evaporated and the pressure exerted are independent of the presence of any other gas. If there is enough so that not all evaporates and if time is allowed for equilibrium, the pressure is independent of the volume of space and of the amount of liquid left unevaporated; but it does depend upon the temperature. For each volatile liquid there is therefore a definite saturation pressure or vapor pressure corresponding to every temperature (see pages 223 to 232).

When any gas is in contact with a volatile substance, the measured pressure is the pressure exerted by the gas plus the vapor pressure of the volatile material. With no change of temperature, this vapor pressure remains constant no matter how we change the total pressure. Hence for the purposes of volume conversion the saturated gas may be considered as a dry gas, the pressure of which is the partial pressure of the gas, or its equivalent, the difference between the total pressure and the saturated vapor pressure of the volatile material.

Volume conversions involving high pressures.—In the measurement of gases at high pressures, pressure 2,000 lbs./in.², the quantity pv is no longer constant at constant temperature, but varies with the pressure by amounts which differ for each gas. Consequently the relation $p_1v_1/T_1 = p_2v_2/T_2$ is no longer true.

In Table 92 $\{273.1/T\}pv$ is given as a function of the pressure. This quantity $\{273.1/T\}pv$ is called the factor (F). Consider the 0°C isothermals. They are taken on the basis of pv at 0°C and 1 atm. as unity. The factor for any pressure given by the table will represent the ratio of the value of pv at this pressure to the value of pv at 1 atmosphere; that is,

$$(pv)_n / (pv)_1 = F_n$$

where F_n is the factor for n atmospheres. This relation, of course, holds for all pressures, therefore, $v_m = v_n \{P_n F_m / P_m F_n\}$. The corrections are made as though the substance behaved as a perfect gas, and the result multiplied by the ratio of the factor at the desired pressure to the factor at the measured pressure.

TABLES 92 AND 93

TABLE 92.—Values of Factor

$$F = (273.1/T)_{pv}. \quad (\text{See p. 141})$$

$$v = 1 \text{ at } 1 \text{ atm. pressure, } 0^\circ \text{C}$$

| Atm. | Air: Holborn, Schultze, 1915 | | | | Argon: Holborn, Schultze, 1915 | | | | Neon* |
|------|------------------------------|--------|--------|--------|--------------------------------|-------|-------|--------|----------|
| | 0°C | 50°C | 100°C | 200°C | 0°C | 50°C | 100°C | 200°C | 0°C |
| 10 | .9950 | .9995 | 1.0019 | 1.0059 | .9919 | .9971 | .9998 | 1.0021 | 1.0043 |
| 25 | .9875 | .9985 | 1.0042 | 1.0082 | .9782 | .9916 | .9982 | 1.0042 | 1.0117 |
| 50 | .9780 | .9994 | 1.0098 | 1.0175 | .9575 | .9840 | .9969 | 1.0082 | 1.0233 |
| 75 | .9720 | 1.002 | 1.0189 | 1.0275 | .9401 | .9781 | .9969 | 1.0136 | 1.0356 |
| 100 | .9710 | 1.0075 | 1.0251 | 1.0380 | .9260 | .9744 | .9988 | 1.0195 | (1.0490) |

| Atm. | Helium: Holborn, Otto, 1922 | | | Hydrogen: Holborn, 1920 | | | Oxygen: Holborn, Otto, 1922 | | | |
|------|-----------------------------|--------|--------|-------------------------|--------|--------|-----------------------------|-------|-------|--------|
| | 0°C | 50°C | 100°C | 0°C | 50°C | | 0°C | 20°C | 50°C | 100°C |
| 10 | 1.0048 | 1.0040 | 1.0033 | 1.0055 | 1.0055 | 1.0045 | .9915 | .9940 | .9972 | 1.0000 |
| 25 | 1.0127 | 1.0106 | 1.0090 | 1.0150 | 1.0136 | 1.0122 | .9778 | .9842 | .9915 | .9987 |
| 50 | 1.0258 | 1.0216 | 1.0183 | 1.0311 | 1.0280 | 1.0248 | .9569 | .9692 | .9838 | .9975 |
| 75 | 1.0390 | 1.0327 | 1.0277 | 1.0475 | 1.0422 | 1.0375 | .9385 | | .9778 | .9978 |
| 100 | 1.0522 | 1.0438 | 1.0370 | 1.0640 | 1.0565 | 1.0500 | .9238 | | .9740 | .9990 |

| Atm. | Nitrogen Mean † | | | Methane: Keyes, Smith, Joubert | | | | | | |
|------|-----------------|-------|-------|--------------------------------|------|-------|-------|--|--|--|
| | 0°C | 50°C | 100°C | 0°C | 50°C | 100°C | 200°C | | | |
| 10 | .996 | 1.000 | 1.002 | .978 | .989 | .993 | .999 | *Onnes, Crommelin, 1915. † Holborn, Otto, 1922, Smith, Taylor, 1923. | | |
| 50 | .982 | 1.002 | 1.011 | .883 | .941 | .971 | .997 | | | |
| 100 | .982 | 1.013 | 1.028 | .781 | .896 | .951 | .998 | | | |
| 150 | 1.000 | 1.037 | 1.053 | (.730) | .873 | .943 | 1.004 | | | |
| 200 | | 1.067 | 1.082 | ... | .873 | .950 | 1.020 | | | |

TABLE 93.—Relative Gas Volumes at Various Pressures

(Deduced by Cochrane, from the pv curves of Amagat and other observers)

Relative volumes when the pressure is reduced from the value given at the head of the column to 1 atmosphere; see also Bur. Standards Circ. 279:

| Gas (Temp. = 16°C) | Relative volume which the gas will occupy when the pressure is reduced to atmospheric from | | | | | |
|-----------------------|--|---------|----------|----------|----------|----------|
| | 1 atm. | 50 atm. | 100 atm. | 120 atm. | 150 atm. | 200 atm. |
| "Perfect" gas..... | 1 | 50 | 100 | 120 | 150 | 200 |
| Helium..... | 1 | ... | 94.6 | 112.5 | 141 | ... |
| Hydrogen..... | 1 | 48.5 | 93.6 | 111.3 | 136.3 | 176.4 |
| Nitrogen..... | 1 | 50.5 | 100.6 | 120.0 | 147.6 | 190.8 |
| Air..... | 1 | 50.9 | 101.8 | 121.9 | 150.3 | 194.8 |
| Argon..... | .. | ... | 106.3 | 127.6 | 161 | ... |
| Oxygen..... | 1 | ... | 105.2 | ... | ... | 212.6 |
| Oxygen (at 0°C)..... | 1 | 52.3 | 107.9 | 128.6 | 161.9 | 218.8 |
| Carbon dioxide..... | 1 | 69 | 477* | 485* | 498* | 515* |

* Carbon dioxide is liquid at pressures greater than 90 atmospheres.

CORRECTING FACTORS: SATURATED GAS VOLUME TO VOLUME AT 760 MM HG AND 0°C

[Multiply observed volumes of saturated gas by factor to correct to volume of dry gas at 760 mm of mercury pressure (0°C) and 0°C]

(Abridged from Bur. Standards Circ. 279)

| Tem- pera- ture (°C) | 715 | 720 | 725 | 730 | Pressure mm of Hg. | | | 750 | 755 | 760 | 765 | 770 |
|-------------------------------|-------|-------|-------|-------|--------------------|-------|-------|-------|-------|-------|-------|-------|
| | | | | | 735 | 740 | 745 | | | | | |
| 5° | 0.916 | 0.922 | 0.928 | 0.935 | 0.942 | 0.948 | 0.954 | 0.961 | 0.967 | 0.974 | 0.980 | 0.986 |
| 6 | .912 | .918 | .924 | .931 | .937 | .944 | .950 | .957 | .963 | .970 | .976 | .982 |
| 7 | .908 | .914 | .920 | .927 | .933 | .940 | .946 | .952 | .959 | .965 | .972 | .978 |
| 8 | .904 | .910 | .916 | .923 | .929 | .936 | .942 | .948 | .955 | .961 | .967 | .974 |
| 9 | .900 | .906 | .912 | .919 | .925 | .932 | .938 | .944 | .951 | .957 | .963 | .970 |
| 10 | .896 | .902 | .908 | .915 | .921 | .928 | .934 | .940 | .946 | .953 | .959 | .966 |
| 11 | .892 | .898 | .904 | .911 | .917 | .924 | .930 | .936 | .942 | .949 | .955 | .962 |
| 12 | .888 | .894 | .900 | .907 | .913 | .919 | .925 | .932 | .939 | .945 | .951 | .957 |
| 13 | .884 | .890 | .896 | .903 | .909 | .915 | .921 | .928 | .934 | .940 | .947 | .953 |
| 14 | .880 | .886 | .892 | .899 | .905 | .911 | .917 | .924 | .930 | .936 | .942 | .949 |
| 15 | .876 | .882 | .888 | .895 | .901 | .907 | .913 | .920 | .925 | .932 | .938 | .944 |
| 16 | .872 | .878 | .884 | .890 | .896 | .903 | .909 | .915 | .921 | .928 | .934 | .940 |
| 17 | .868 | .874 | .880 | .886 | .892 | .898 | .905 | .911 | .917 | .923 | .929 | .936 |
| 18 | .864 | .870 | .875 | .882 | .888 | .894 | .900 | .907 | .913 | .919 | .925 | .931 |
| 19 | .859 | .865 | .871 | .878 | .884 | .890 | .896 | .902 | .908 | .915 | .920 | .927 |
| 20 | .855 | .861 | .867 | .874 | .879 | .886 | .892 | .898 | .904 | .910 | .916 | .922 |
| 21 | .851 | .857 | .863 | .869 | .875 | .881 | .887 | .893 | .899 | .906 | .912 | .918 |
| 22 | .847 | .853 | .858 | .865 | .871 | .877 | .883 | .888 | .894 | .901 | .907 | .913 |
| 23 | .842 | .848 | .854 | .860 | .866 | .872 | .878 | .884 | .890 | .897 | .903 | .909 |
| 24 | .838 | .844 | .849 | .856 | .862 | .868 | .874 | .880 | .886 | .892 | .898 | .904 |
| 25 | .833 | .839 | .845 | .851 | .857 | .863 | .869 | .875 | .881 | .888 | .893 | .899 |
| 26 | .829 | .835 | .841 | .847 | .853 | .859 | .865 | .871 | .877 | .883 | .889 | .895 |
| 27 | .824 | .830 | .836 | .842 | .848 | .854 | .860 | .866 | .872 | .878 | .884 | .890 |
| 28 | .820 | .825 | .831 | .837 | .843 | .849 | .855 | .861 | .867 | .873 | .879 | .885 |
| 29 | .815 | .821 | .826 | .832 | .838 | .844 | .850 | .856 | .862 | .868 | .874 | .880 |
| 30 | .810 | .816 | .822 | .828 | .833 | .840 | .845 | .851 | .857 | .863 | .869 | .875 |
| 31 | .805 | .811 | .817 | .823 | .829 | .835 | .840 | .846 | .852 | .858 | .864 | .870 |
| 32 | .800 | .806 | .812 | .818 | .823 | .830 | .835 | .841 | .847 | .853 | .859 | .865 |
| 33 | .795 | .801 | .807 | .813 | .818 | .824 | .830 | .836 | .842 | .848 | .853 | .860 |
| 34 | .790 | .796 | .801 | .807 | .813 | .819 | .825 | .831 | .837 | .842 | .848 | .854 |
| 35 | .785 | .790 | .796 | .802 | .808 | .814 | .819 | .825 | .831 | .837 | .843 | .849 |
| 36 | .780 | .785 | .791 | .797 | .802 | .808 | .814 | .820 | .826 | .832 | .836 | .843 |
| 37 | .774 | .780 | .785 | .791 | .797 | .803 | .809 | .814 | .820 | .826 | .832 | .838 |
| 38 | .769 | .774 | .780 | .786 | .791 | .796 | .803 | .809 | .814 | .820 | .826 | .832 |
| 39 | .763 | .768 | .774 | .780 | .785 | .790 | .797 | .803 | .809 | .814 | .820 | .826 |
| 40 | .756 | .763 | .768 | .774 | .780 | .786 | .792 | .797 | .803 | .809 | .814 | .820 |
| 41 | .751 | .757 | .762 | .768 | .774 | .780 | .786 | .791 | .797 | .803 | .808 | .814 |
| 42 | .745 | .751 | .756 | .762 | .768 | .774 | .779 | .785 | .791 | .796 | .802 | .808 |
| 43 | .739 | .745 | .750 | .756 | .762 | .767 | .773 | .779 | .784 | .790 | .796 | .802 |
| 44 | .733 | .738 | .744 | .750 | .755 | .761 | .766 | .772 | .778 | .784 | .789 | .795 |
| 45 | .726 | .732 | .737 | .743 | .749 | .754 | .760 | .766 | .771 | .777 | .783 | .788 |
| 46 | .720 | .725 | .731 | .737 | .742 | .748 | .754 | .759 | .765 | .770 | .776 | .782 |
| 47 | .713 | .719 | .724 | .730 | .735 | .741 | .746 | .752 | .758 | .764 | .769 | .775 |
| 48 | .706 | .712 | .717 | .723 | .728 | .734 | .739 | .745 | .751 | .756 | .762 | .768 |
| 49 | .700 | .705 | .710 | .716 | .721 | .727 | .732 | .738 | .744 | .750 | .755 | .761 |

COMPRESSIBILITY OF GASES

TABLE 95.—Compressibility at Ordinary Temperatures

As a measure of the compressibility, it is customary to use a coefficient, $1 + \lambda = p_0 v_0 / p_1 v_1$, p_0, v_0 being at 0°C

| | | | |
|----------------------------------|-------------------------------------|---|-------------------------|
| H ₂ | $1 + \lambda = 0.99939 \pm 0.00001$ | CO | $1 + \lambda = 1.00081$ |
| N ₂ | 1.00044 0.00001 | CO ₂ | 1.00668 |
| O ₂ | 1.00094 0.000013 | N ₂ O | 1.00747 |
| He | 0.99948 0.000005 | | |
| Ne | 0.99951 0.000025 | | |
| A | 1.00099 0.000026 | | |
| Wild, Philos. Mag., 12, 49, 1911 | | Rayleigh, Z. Phys. Chem., 52, 705, 1905 | |

TABLE 96.—Compressibility at Low Temperatures

$p_0 v_0 = 1$ for 0° , 1 atmosphere

| Table 96a.—Helium | | | | Table 96b.—Hydrogen | | | |
|----------------------------|-------------|-----------|---------|--|-------------|-----------|---------|
| $t^\circ\text{C}$ | p atm. | $p_0 v_0$ | Density | $t^\circ\text{C}$ | p atm. | $p_0 v_0$ | Density |
| 0.00 | 26.66 | 1.0146 | 26.28 | 0.00 | 32.313 | 1.0188 | 31.715 |
| " | 38.95 | 1.0196 | 38.20 | " | 44.119 | 1.0266 | 43.284 |
| " | 58.58 | 1.0294 | 56.91 | -103.57 | 38.41 | .6376 | 38.41 |
| -103.64 | 24.13 | .6337 | 38.07 | " | 51.49 | .6433 | 80.04 |
| " | 49.96 | .6479 | 77.08 | -204.70 | 16.75 | .2404 | 69.68 |
| -269.69 | .232 | .01126 | 20.63 | " | 37.00 | .2316 | 159.7 |
| " | .353 | .01041 | 33.92 | " | 44.63 | .2300 | 194.0 |
| -270.52 | .0308 | .00911 | 3.381 | -257.26 | .06698 | .05783 | 1.1582 |
| " | .0649 | .00858 | 7.535 | " | .13153 | .057104 | 2.3031 |
| Bocke, Onnes, 1924 | | | | Nighoff, Keesom, 1928; Onnes, Penning, 1903; Onnes, Braak, 1907 | | | |
| Table 96c.—Neon | | | | Table 96d.—Argon | | | |
| $t^\circ\text{C}$ | p atm. | $p_0 v_0$ | Density | $t^\circ\text{C}$ | p atm. | $p_0 v_0$ | Density |
| 0.0 | 23.06 | 1.0089 | 21.87 | 0.0 | 20.58 | .9856 | 20.88 |
| " | 30.79 | 1.0147 | 30.34 | " | 31.57 | .9774 | 32.30 |
| " | 84.66 | 1.0408 | 81.35 | -102.51 | 14.86 | .5813 | 25.57 |
| -200.1 | 61.66 | .2337 | 763.8 | " | 45.09 | .4706 | 95.80 |
| " | 79.92 | .2293 | 348.6 | " | 62.24 | .3939 | 158.01 |
| -217.5 | 49.93 | .1393 | 358.5 | -130.38 | 12.77 | .4663 | 27.39 |
| " | 64.97 | .1269 | 511.8 | -159.62 | 11.99 | .4262 | 28.12 |
| " | 79.42 | .1256 | 632.2 | -149.60 | 11.15 | .3821 | 29.18 |
| Onnes, Crommelin, 1915 | | | | Onnes, Crommelin, 1910 | | | |
| Table 96e.—Oxygen | | | | Table 96f.—Nitrogen | | | |
| $t^\circ\text{C}$ | p atm. | $p_0 v_0$ | Density | $t^\circ\text{C}$ | p atm. | $p_0 v_0$ | Density |
| 0 | 20.92 | .9813 | 21.32 | 0 | 33.14 | .9886 | 33.52 |
| " | 49.79 | .9573 | 52.01 | " | 43.08 | .9860 | 43.70 |
| -80.03 | 21.01 | .6550 | 32.09 | " | 58.63 | .9834 | 59.62 |
| " | 34.18 | .6213 | 55.02 | -81.10 | 30.17 | .6516 | 46.13 |
| " | 61.88 | .5464 | 13.23 | " | 45.47 | .6270 | 72.52 |
| -116.01 | 22.30 | .4835 | 46.12 | " | 56.71 | .6109 | 92.84 |
| " | 43.95 | .3541 | 124.1 | -146.32 | 22.92 | .3340 | 68.62 |
| " | 55.05 | .1667 | 330.2 | " | 30.14 | .2656 | 113.48 |
| Onnes, Kuypers, 1923, 1924 | | | | " | 36.49 | .1058 | 344.5 |
| | | | | Onnes, Van Urk, 1924 | | | |

COMPRESSIBILITY OF GASES

TABLE 97.—O, Air, N, and H. Relative Volumes at Various Pressures and Temperatures, the volumes at 0°C and at 1 atmosphere being taken as 1 000 000

| Atm. | Oxygen. | | | Air. | | | Nitrogen. | | | Hydrogen. | | |
|------|---------|-------|--------|------|-------|--------|-----------|-------|--------|-----------|-------|--------|
| | 0° | 99°·5 | 199°·5 | 0° | 99°·4 | 200°·4 | 0° | 99°·5 | 199°·6 | 0° | 99°·3 | 200°·5 |
| 100 | 9265 | — | — | 9730 | — | — | 9910 | — | — | — | — | — |
| 200 | 4570 | 7000 | 9095 | 5050 | 7360 | 9430 | 5195 | 7445 | 9532 | 5690 | 7567 | 9420 |
| 300 | 3208 | 4843 | 6283 | 3658 | 5170 | 6622 | 3786 | 5301 | 6715 | 4030 | 5286 | 6520 |
| 400 | 2629 | 3830 | 4900 | 3036 | 4170 | 5240 | 3142 | 4265 | 5331 | 3207 | 4147 | 5075 |
| 500 | 2312 | 3244 | 4100 | 2680 | 3565 | 4422 | 2780 | 3655 | 4515 | 2713 | 3462 | 4210 |
| 600 | 2115 | 2867 | 3570 | 2450 | 3180 | 3883 | 2543 | 3258 | 3973 | 2387 | 3006 | 3627 |
| 700 | 1979 | 2610 | 3202 | 2288 | 2904 | 3502 | 2374 | 2980 | 3589 | 2149 | 2680 | 3212 |
| 800 | 1879 | 2417 | 2929 | 2168 | 2699 | 3219 | 2240 | 2775 | 3300 | 1972 | 2444 | 2900 |
| 900 | 1800 | 2268 | 2718 | 2070 | 2544 | 3000 | 2149 | 2616 | 3085 | 1832 | 2244 | 2657 |
| 1000 | 1735 | 2151 | — | 1992 | 2415 | 2828 | 2068 | — | — | 1720 | 2093 | — |

Amagat, C. R. 111, p. 871, 1890; Ann. chim. phys. (6) 29, pp. 68 and 505, 1893.

TABLE 98.—Ethylene

 $p\theta$ at 0°C and 1 atm. = 1

| Atm. | 0° | 10° | 20° | 30° | 40° | 60° | 80° | 100° | 137°·5 | 198°·5 |
|------|-------|-------|-------|-------|-------|-------|-------|-------|--------|--------|
| 46 | — | 0.562 | 0.684 | — | — | — | — | — | — | — |
| 48 | — | 0.508 | — | — | — | — | — | — | — | — |
| 50 | 0.176 | 0.420 | 0.629 | 0.731 | 0.814 | 0.954 | 1.077 | 1.192 | 1.374 | 1.652 |
| 52 | — | 0.240 | 0.598 | — | — | — | — | — | — | — |
| 54 | — | 0.229 | 0.561 | — | — | — | — | — | — | — |
| 56 | — | 0.227 | 0.524 | — | — | — | — | — | — | — |
| 100 | 0.310 | 0.331 | 0.360 | 0.403 | 0.471 | 0.668 | 0.847 | 1.005 | 1.247 | 1.580 |
| 150 | 0.441 | 0.459 | 0.485 | 0.515 | 0.551 | 0.649 | 0.776 | 0.924 | 1.178 | 1.540 |
| 200 | 0.565 | 0.585 | 0.610 | 0.638 | 0.669 | 0.744 | 0.838 | 0.946 | 1.174 | 1.537 |
| 300 | 0.806 | 0.827 | 0.852 | 0.878 | 0.908 | 0.972 | 1.048 | 1.133 | 1.310 | 1.628 |
| 500 | 1.256 | 1.280 | 1.308 | 1.337 | 1.367 | 1.431 | 1.500 | 1.578 | 1.721 | 1.985 |
| 1000 | 2.289 | 2.321 | 2.354 | 2.387 | 2.422 | 2.493 | 2.566 | 2.643 | 2.798 | — |

Amagat, C. R. 111, p. 871, 1890; 116, p. 946, 1893.

TABLE 99.—Carbon Dioxide

| Pressure in meters of mercury | Relative values of $p\theta$ at— | | | | | | | | |
|-------------------------------------|----------------------------------|-------|-------|-------|-------|-------|-------|-------|--------|
| | 18°.2 | 35°.1 | 40°.2 | 50°.0 | 60°.0 | 70°.0 | 80°.0 | 90°.0 | 100°.0 |
| 30 | liquid | 2360 | 2460 | 2590 | 2730 | 2870 | 2995 | 3120 | 3225 |
| 50 | — | 1725 | 1900 | 2145 | 2330 | 2525 | 2685 | 2845 | 2980 |
| 80 | 625 | 750 | 825 | 1200 | 1650 | 1975 | 2225 | 2440 | 2635 |
| 110 | 825 | 930 | 980 | 1090 | 1275 | 1550 | 1845 | 2105 | 2325 |
| 140 | 1020 | 1120 | 1175 | 1250 | 1360 | 1525 | 1715 | 1950 | 2160 |
| 170 | 1210 | 1310 | 1360 | 1430 | 1520 | 1645 | 1780 | 1975 | 2135 |
| 200 | 1405 | 1500 | 1550 | 1615 | 1705 | 1810 | 1930 | 2075 | 2215 |
| 230 | 1590 | 1690 | 1730 | 1800 | 1890 | 1990 | 2090 | 2210 | 2340 |
| 260 | 1770 | 1870 | 1920 | 1985 | 2070 | 2166 | 2265 | 2375 | 2490 |
| 290 | 1950 | 2060 | 2100 | 2170 | 2260 | 2340 | 2440 | 2550 | 2655 |
| 320 | 2135 | 2240 | 2280 | 2360 | 2440 | 2525 | 2620 | 2725 | 2830 |

| Atm. | Relative values of $p\theta$; $p\theta$ at 0°C and 1 atm. = 1 | | | | | | | | | | |
|------|--|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | 0° | 10° | 20° | 30° | 40° | 60° | 80° | 100° | 137° | 198° | 258° |
| 50 | 0.105 | 0.114 | 0.680 | 0.775 | 0.750 | 0.984 | 1.096 | 1.206 | 1.380 | — | — |
| 100 | 0.202 | 0.213 | 0.229 | 0.255 | 0.309 | 0.661 | 0.873 | 1.030 | 1.259 | 1.582 | 1.847 |
| 150 | 0.295 | 0.309 | 0.326 | 0.346 | 0.377 | 0.485 | 0.681 | 0.878 | 1.159 | 1.530 | 1.818 |
| 300 | 0.559 | 0.578 | 0.599 | 0.623 | 0.649 | 0.710 | 0.790 | 0.890 | 1.108 | 1.493 | 1.820 |
| 500 | 0.891 | 0.913 | 0.938 | 0.963 | 0.990 | 1.054 | 1.124 | 1.201 | 1.362 | 1.678 | — |
| 1000 | 1.656 | 1.685 | 1.716 | 1.748 | 1.780 | 1.848 | 1.921 | 1.999 | — | — | — |

Amagat, C. R. 111, p. 871, 1890; Ann. chim. phys. (5) 22, p. 353, 1881; (6) 29, pp. 68 and 405, 1893.

COMPRESSIBILITY OF GASES

TABLE 100.—Some Physical Properties of Compressed Nitrogen

(Abridged from Deming, Shupe, Phys. Rev., 37, 639, 1931; based on data by Bartlett and collaborators, Journ. Amer. Chem. Soc., 1927-31.)

Tables published by Bartlett *et al* show compressibility factors $pv/(p_0v_0)$ at the different pressures and temperatures. The denominator (p_0v_0) is the value of p_0v_0 at S.T.P. In order to find the specific volume of the gas it is required to know the volume of 1 g at S.T.P. Birge gives 22414.1 cc as the volume of a mole of an ideal gas at S.T.P.

$p_0/(pv)$ at 1 atm. is close to $1/1.00046$. The gas used by Bartlett contained 0.9993 nitrogen and 0.0007 inert gas, presumably argon; the apparent molecular weight is therefore taken as 28.025. The volume adopted for 1 g at S.T.P. is $22414.1/1.00046 \times 28.025 = 799.42$ cc, and the value of RT at 0° is $22414.1/28.025 = 799.79$ cc atm./g. When one of Bartlett's compressibility factors is divided by the pressure and multiplied by 799.42 the result is the volume in cc of 1 g of the gas at the given temperature and pressure.

For fugacities, see Lewis and Randall, Thermodynamics, 1923.

| t $^\circ\text{C}$ | p atm. | Sp. vol. cc/g | Density ρ g/cc | f fugacity atm. | $\left(\frac{-p}{v} \cdot \frac{dv}{dp}\right)_T$ | $\left(\frac{T}{v} \cdot \frac{dv}{dT}\right)_p$ | ΔC_p cal./mole $^\circ$ | Joule- Thomson coefficient $^\circ\text{C}/\text{atm.}$ |
|-------------------------|-------------|------------------|---------------------------|-------------------------|---|--|------------------------------------|--|
| -70 | 20 | 28.50 | .03508 | 19.22 | 1.053 | 1.162 | .50 | .627 |
| | 60 | 8.840 | .1131 | 53.31 | 1.075 | 1.530 | 1.79 | .538 |
| | 100 | 5.082 | .1908 | 83.18 | 1.004 | 1.806 | 3.13 | .408 |
| | 200 | 2.725 | .3609 | 152.1 | .717 | 1.504 | 5.17 | .128 |
| | 400 | 1.896 | .5273 | 319.2 | .403 | .918 | 5.10 | -.013 |
| | 800 | 1.508 | .6630 | 976.2 | .280 | .551 | 4.97 | -.057 |
| | 1200 | 1.358 | .7305 | 2545 | .250 | .356 | 4.81 | -.074 |
| -50 | 20 | 31.75 | .03149 | 19.48 | 1.031 | 1.129 | .45 | .559 |
| | 60 | 10.13 | .09872 | 55.49 | 1.048 | 1.381 | 1.43 | .463 |
| | 100 | 5.952 | .1680 | 88.75 | 1.000 | 1.560 | 2.41 | .355 |
| | 200 | 3.139 | .3186 | 168.4 | .775 | 1.462 | 3.76 | .136 |
| | 400 | 2.068 | .4836 | 357.8 | .472 | .937 | 3.84 | -.012 |
| | 800 | 1.591 | .6284 | 1063 | .313 | .578 | 3.66 | -.064 |
| | 1200 | 1.408 | .7103 | 2645 | .286 | .404 | 3.48 | -.081 |
| -25 | 20 | 35.75 | .02798 | 19.70 | 1.018 | 1.094 | .36 | .479 |
| | 60 | 11.66 | .08578 | 57.43 | 1.025 | 1.266 | 1.14 | .383 |
| | 100 | 6.950 | .1439 | 93.70 | .900 | 1.377 | 1.90 | .298 |
| | 200 | 3.645 | .2744 | 183.6 | .830 | 1.363 | 2.95 | .134 |
| | 400 | 2.287 | .4372 | 395.5 | .540 | .961 | 3.02 | -.008 |
| | 800 | 1.605 | .5901 | 1121 | .353 | .608 | 2.72 | -.069 |
| | 1200 | 1.473 | .6789 | 2703 | .320 | .457 | 2.53 | -.085 |
| 0 | 20 | 39.67 | .02521 | 10.84 | 1.010 | 1.068 | .29 | .387 |
| | 60 | 13.11 | .07627 | 58.72 | 1.005 | 1.183 | .92 | .308 |
| | 100 | 7.886 | .1268 | 97.05 | .978 | 1.265 | 1.53 | .247 |
| | 200 | 4.139 | .2416 | 194.6 | .850 | 1.281 | 2.34 | .125 |
| | 400 | 2.510 | .3984 | 424.2 | .590 | .983 | 2.48 | -.005 |
| | 800 | 1.798 | .5560 | 1194 | .390 | .639 | 2.20 | -.071 |
| | 1200 | 1.543 | .6481 | 2732 | .350 | .503 | 2.01 | -.084 |
| 20 | 20 | 42.74 | .02340 | 19.02 | 1.003 | 1.055 | .25 | .325 |
| | 60 | 14.23 | .07027 | 59.41 | .995 | 1.140 | .75 | .263 |
| | 100 | 8.604 | .1162 | 99.06 | .970 | 1.199 | 1.22 | .211 |
| | 200 | 4.524 | .2210 | 201.0 | .860 | 1.223 | 2.05 | .114 |
| | 400 | 2.693 | .3713 | 441.5 | .628 | .994 | 2.33 | -.002 |
| | 800 | 1.880 | .5318 | 1226 | .417 | .660 | 2.13 | -.071 |
| | 1200 | 1.601 | .6248 | 2737 | .373 | .534 | 1.98 | -.083 |
| 50 | 20 | 47.33 | .02113 | 20.01 | .998 | 1.037 | .19 | .248 |
| | 60 | 15.87 | .06301 | 60.18 | .984 | 1.099 | .54 | .208 |
| | 100 | 9.639 | .1038 | 100.9 | .961 | 1.138 | .86 | .169 |
| | 200 | 5.078 | .1969 | 207.5 | .845 | 1.151 | 1.46 | .094 |
| | 400 | 2.967 | .3371 | 459.7 | .670 | .995 | 1.88 | -.001 |
| | 800 | 2.010 | .4974 | 1254 | .456 | .688 | 1.83 | -.071 |
| | 1200 | 1.688 | .5925 | 2719 | .402 | .566 | 1.74 | -.083 |
| 100 | 20 | 54.87 | .01822 | 20.08 | .995 | 1.023 | .12 | .162 |
| | 60 | 18.52 | .05400 | 60.87 | .975 | 1.052 | .35 | .138 |
| | 100 | 11.29 | .08856 | 102.1 | .953 | 1.078 | .56 | .114 |
| | 200 | 5.955 | .1679 | 213.7 | .881 | 1.078 | 1.01 | .058 |
| | 400 | 3.421 | .2924 | 470.8 | .716 | .974 | 1.53 | -.010 |
| | 800 | 2.225 | .4494 | 1271 | .515 | .720 | 1.70 | -.072 |
| | 1200 | 1.830 | .5447 | 2649 | .445 | .597 | 1.98 | -.085 |
| 300 | 20 | 84.64 | .01181 | 20.18 | .990 | 1.003 | .05 | .010 |
| | 60 | 28.73 | .03480 | 61.62 | .970 | .997 | .14 | -.006 |
| | 100 | 17.57 | .05692 | 104.6 | .951 | .992 | .22 | -.018 |
| | 200 | 9.230 | .1083 | 219.6 | .907 | .969 | .39 | -.042 |
| | 400 | 5.098 | .1962 | 487.4 | .808 | .894 | .64 | -.071 |
| | 800 | 3.060 | .3268 | 1218 | .658 | .751 | .91 | -.066 |
| | 1200 | 2.387 | .4190 | 2306 | .570 | .642 | 1.02 | -.107 |
| 600 | 20 | 128.8 | .007766 | 20.15 | .992 | .995 | .01 | -.083 |
| | 60 | 43.57 | .02295 | 61.36 | .976 | .987 | .04 | -.090 |
| | 100 | 26.54 | .03768 | 103.9 | .961 | .978 | .06 | -.095 |
| | 200 | 13.77 | .07264 | 215.8 | .926 | .943 | .11 | -.101 |
| | 400 | 7.409 | .1350 | 466.9 | .860 | .891 | .19 | -.110 |
| | 800 | 4.234 | .2362 | 1097 | .746 | .792 | .31 | -.117 |
| | 1200 | 3.177 | .3148 | 1938 | .670 | .720 | .35 | -.119 |

TABLE 101.—Compressibility of Gases Under High Pressures

(Bridgman, Proc. Amer. Acad., 59, 173, 1924.)

Actual vols. rest upon Amagat's doubtful values at 3000 kg/cm.² Vol. of gas = 1 cm³ at 0°C, 1 kg/cm.² pressure. Densities at highest pressures indicate that the molecules or atoms are very nearly in contact in the sense of the kinetic theory.

| (a).—Results for Hydrogen | | | | | | | (b).—Results for Nitrogen | | | | | | |
|---------------------------|---|------|--|-------|---------------------------|---------------------------------------|---------------------------|--|-------|--|-------|---------------------------|--|
| kg/cm ² | Vol. change c ³ /g from 3000 kg 30°C 65°C | | Volume c ³ /g 30°C 65°C | | p ^v at 65°C | Vol. c ³ /mol 30°C 65°C | | Vol. change 68°C c ³ /g c ² /mol | | Volume at 68°C c ³ /g c ³ /mol | | p ^v at 68°C | |
| | | | | | | | | | | | | | |
| 3000 | 0.00 | 0.00 | 11.64 | 12.17 | 3.18 | 23.47 | 24.53 | .000 | 0.00 | 1.290 | 36.13 | 4.68 | |
| 4000 | 1.12 | 1.14 | 10.52 | 11.03 | 3.83 | 21.21 | 22.24 | .089 | 2.49 | 1.201 | 33.64 | 5.82 | |
| 5000 | 1.84 | 1.88 | 9.80 | 10.29 | 4.50 | 19.76 | 20.74 | .152 | 4.25 | 1.138 | 31.88 | 6.89 | |
| 7000 | 2.77 | 2.88 | 8.87 | 9.29 | 5.65 | 17.88 | 18.73 | .234 | 6.56 | 1.056 | 29.57 | 8.95 | |
| 10000 | 3.63 | 3.68 | 8.01 | 8.49 | 7.29 | 16.15 | 17.12 | .308 | 8.61 | .982 | 27.52 | 11.01 | |
| 13000 | 4.32 | 4.21 | 7.32 | 7.96 | 8.66 | 14.76 | 16.05 | .357 | 10.00 | .933 | 26.13 | 14.70 | |
| 15000 | ... | ... | ... | ... | ... | ... | ... | .382 | 10.70 | .908 | 25.43 | 16.50 | |

| (c).—Results for Helium | | | | | | (d).—Results for Argon | | (e).—Results for Ammonia | | |
|-------------------------|---|--|-------------------|---------------------|---------------------------|---------------------------|------------------------|--------------------------|------------------------|---------------------|
| kg/cm ² | Vol. change c ³ /g 65°C | Total vol. change 30-95° c ³ /g | Volume at 65°C | | p ^v at 65°C | Vol. change at 55° | | kg/cm ² | Vol. change at 30°C | |
| | | | c ³ /g | c ³ /mol | | c ³ /g | c ³ /g atom | | c ³ /g | c ² /mol |
| 3000 | 0.00 | 0.613 | 5.54 | 22.16 | 2.31 | 0.000 | 0.00 | 1000 | -0.827 | -14.1 |
| 4000 | 0.77 | .598 | 4.77 | 19.08 | 2.64 | .049 | 1.96 | 2000 | - .217 | - 3.70 |
| 5000 | 1.23 | .589 | 4.31 | 17.24 | 2.99 | .085 | 3.39 | 3000 | .000 | 0.00 |
| 7000 | 1.77 | .581 | 3.77 | 15.08 | 3.66 | .134 | 5.34 | 5000 | + .200 | + 3.41 |
| 10000 | 2.22 | .576 | 3.32 | 13.27 | 4.60 | .180 | 7.18 | 7000 | .120 | 5.28 |
| 13000 | 2.48 | .572 | 3.06 | 12.24 | 5.52 | .209 | 8.34 | 10000 | .409 | 6.97 |
| 15000 | 2.60 | .570 | 2.94 | 11.76 | 6.11 | .224 | 8.94 | 12000 | .461 | 7.85 |

TABLE 102.—Gage Pressure (lb./in.²) to Atmospheres (absolute)

(Taken from Bur. Standards Circ., 279, 1926.)

| lb./in. ² | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0 | 1.00 | 1.68 | 2.36 | 3.04 | 3.72 | 4.40 | 5.08 | 5.76 | 6.44 | 7.12 |
| 100 | 7.80 | 8.48 | 9.17 | 9.85 | 10.53 | 11.21 | 11.89 | 12.57 | 13.25 | 13.93 |
| 200 | 14.61 | 15.29 | 15.97 | 16.65 | 17.33 | 18.01 | 18.69 | 19.37 | 20.05 | 20.73 |
| 300 | 21.41 | 22.09 | 22.77 | 23.45 | 24.14 | 24.82 | 25.50 | 26.18 | 26.86 | 27.54 |
| 400 | 28.22 | 28.90 | 29.58 | 30.26 | 30.94 | 31.62 | 32.30 | 32.98 | 33.66 | 34.34 |
| 500 | 35.02 | 35.70 | 36.38 | 37.06 | 37.74 | 38.42 | 39.11 | 39.79 | 40.47 | 41.15 |
| 600 | 41.83 | 42.51 | 43.19 | 43.87 | 44.55 | 45.23 | 45.91 | 46.59 | 47.27 | 47.95 |
| 700 | 48.63 | 49.31 | 49.99 | 50.67 | 51.35 | 52.03 | 52.71 | 53.39 | 54.08 | 54.76 |
| 800 | 55.44 | 56.12 | 56.80 | 57.48 | 58.16 | 58.84 | 59.52 | 60.20 | 60.88 | 61.56 |
| 900 | 62.24 | 62.92 | 63.60 | 64.28 | 64.96 | 65.64 | 66.32 | 67.00 | 67.68 | 68.36 |
| 1,000 | 69.04 | 69.73 | 70.41 | 71.09 | 71.77 | 72.45 | 73.13 | 73.81 | 74.49 | 75.17 |
| 1,100 | 75.85 | 76.53 | 77.21 | 77.89 | 78.57 | 79.25 | 79.93 | 80.61 | 81.29 | 81.97 |
| 1,200 | 82.65 | 83.34 | 84.01 | 84.70 | 85.38 | 86.06 | 86.74 | 87.42 | 88.10 | 88.78 |
| 1,300 | 89.46 | 90.14 | 90.82 | 91.50 | 92.18 | 92.86 | 93.54 | 94.22 | 94.90 | 95.58 |
| 1,400 | 96.27 | 96.95 | 97.63 | 98.31 | 98.98 | 99.67 | 100.3 | 101.0 | 101.7 | 102.4 |
| 1,500 | 103.1 | 103.8 | 104.4 | 105.1 | 105.8 | 106.5 | 107.1 | 107.8 | 108.5 | 109.2 |
| 1,600 | 109.9 | 110.6 | 111.3 | 111.9 | 112.6 | 113.3 | 114.0 | 114.6 | 115.3 | 116.0 |
| 1,700 | 116.7 | 117.4 | 118.0 | 118.7 | 119.4 | 120.1 | 120.8 | 121.4 | 122.1 | 122.8 |
| 1,800 | 123.5 | 124.2 | 124.8 | 125.5 | 126.2 | 126.9 | 127.6 | 128.2 | 128.9 | 129.6 |
| 1,900 | 130.3 | 131.0 | 131.6 | 132.3 | 133.0 | 133.7 | 134.4 | 135.0 | 135.7 | 136.4 |
| 2,000 | 137.1 | 137.8 | 138.4 | 139.1 | 139.8 | 140.5 | 141.2 | 141.9 | 142.5 | 143.2 |
| 2,100 | 143.9 | 144.6 | 145.2 | 145.9 | 146.6 | 147.3 | 148.0 | 148.7 | 149.3 | 150.0 |
| 2,200 | 150.7 | 151.4 | 152.1 | 152.7 | 153.4 | 154.1 | 154.8 | 155.5 | 156.1 | 156.8 |
| 2,300 | 157.5 | 158.2 | 158.9 | 159.5 | 160.2 | 160.9 | 161.6 | 162.3 | 162.9 | 163.6 |
| 2,400 | 164.3 | 165.0 | 165.7 | 166.3 | 167.0 | 167.7 | 168.4 | 169.1 | 169.8 | 170.4 |
| 2,500 | 171.1 | 171.8 | 172.5 | 173.2 | 173.8 | 174.5 | 175.2 | 175.9 | 176.6 | 177.2 |
| 2,600 | 177.9 | 178.6 | 179.3 | 180.0 | 180.6 | 181.3 | 182.0 | 182.7 | 183.4 | 184.0 |
| 2,700 | 184.7 | 185.4 | 186.1 | 186.8 | 187.4 | 188.1 | 188.8 | 189.5 | 190.2 | 190.8 |
| 2,800 | 191.5 | 192.2 | 192.9 | 193.6 | 194.2 | 194.9 | 195.6 | 196.3 | 197.0 | 197.7 |
| 2,900 | 198.3 | 199.0 | 199.7 | 200.4 | 201.1 | 201.7 | 202.4 | 203.1 | 203.8 | 204.4 |

RELATION BETWEEN PRESSURE, TEMPERATURE, AND VOLUME OF SULPHUR DIOXIDE AND AMMONIA*

TABLE 103.—Sulphur Dioxide

Original volume 100000 under one atmosphere of pressure and the temperature of the experiments as indicated at the top of the different columns.

| Pressure in Atmos. | Corresponding Volume for Experiments at Temperature — | | | Volume. | Pressure in Atmospheres for Experiments at Temperature — | | |
|--------------------|---|-------------------|--------------------|---------|--|-------------------|--------------------|
| | 58°. ₀ | 99°. ₆ | 183°. ₂ | | 58°. ₀ | 99°. ₆ | 183°. ₂ |
| 10 | 8560 | 9440 | — | 10000 | — | 9.60 | — |
| 12 | 6360 | 7800 | — | | — | — | — |
| 14 | 4040 | 6420 | — | 9000 | 9.60 | 10.35 | — |
| 16 | — | 5310 | — | 8000 | 10.40 | 11.85 | — |
| 18 | — | 4405 | — | 7000 | 11.55 | 13.05 | — |
| 20 | — | 4030 | — | 6000 | 12.30 | 14.70 | — |
| 24 | — | 3345 | — | 5000 | 13.15 | 16.70 | — |
| 28 | — | 2780 | 3180 | 4000 | 14.00 | 20.15 | — |
| 32 | — | 2305 | 2640 | 3500 | 14.40 | 23.00 | — |
| 36 | — | 1935 | 2260 | 3000 | — | 26.40 | 29.10 |
| 40 | — | 1450 | 2040 | 2500 | — | 30.15 | 33.25 |
| 50 | — | — | 1640 | 2000 | — | 35.20 | 40.95 |
| 60 | — | — | 1375 | 1500 | — | 39.60 | 55.20 |
| 70 | — | — | 1130 | 1000 | — | — | 76.00 |
| 80 | — | — | 930 | 500 | — | — | 117.20 |
| 90 | — | — | 790 | | | | |
| 100 | — | — | 680 | | | | |
| 120 | — | — | 545 | | | | |
| 140 | — | — | 430 | | | | |
| 160 | — | — | 325 | | | | |

TABLE 104.—Ammonia

Original volume 100000 under one atmosphere of pressure and the temperature of the experiments as indicated at the top of the different columns.

| Pressure in Atmos. | Corresponding Volume for Experiments at Temperature — | | | Volume. | Pressure in Atmospheres for Experiments at Temperature — | | | |
|--------------------|---|-------------------|--------------------|---------|--|-------------------|-------------------|--------------------|
| | 46°. ₆ | 99°. ₆ | 183°. ₆ | | 30°. ₂ | 46°. ₆ | 99°. ₆ | 183°. ₀ |
| 10 | 9500 | — | — | 10000 | 8.85 | 9.50 | — | — |
| 12.5 | 7245 | 7635 | — | 9000 | 9.60 | 10.45 | — | — |
| 15 | 5880 | 6305 | — | 8000 | 10.40 | 11.50 | 12.00 | — |
| 20 | — | 4645 | 4875 | 7000 | 11.05 | 13.00 | 13.60 | — |
| 25 | — | 3560 | 3835 | 6000 | 11.80 | 14.75 | 15.55 | — |
| 30 | — | 2875 | 3185 | 5000 | 12.00 | 16.60 | 18.60 | 19.50 |
| 35 | — | 2440 | 2680 | 4000 | — | 18.35 | 22.70 | 24.00 |
| 40 | — | 2080 | 2345 | 3500 | — | 18.30 | 25.40 | 27.20 |
| 45 | — | 1795 | 2035 | 3000 | — | — | 29.20 | 31.50 |
| 50 | — | 1490 | 1775 | 2500 | — | — | 34.25 | 37.35 |
| 55 | — | 1250 | 1590 | 2000 | — | — | 41.45 | 45.50 |
| 60 | — | 975 | 1450 | 1500 | — | — | 49.70 | 58.00 |
| 70 | — | — | 1245 | 1000 | — | — | 59.65 | 93.60 |
| 80 | — | — | 1125 | | | | | |
| 90 | — | — | 1035 | | | | | |
| 100 | — | — | 950 | | | | | |

* From the experiments of Roth, "Wied. Ann." vol. 11, 1880

TABLE 105

VOLUME OF CASES

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Values of $1 + .00367 t$

The quantity $1 + .00367 t$ gives for a gas the volume at t° when the pressure is kept constant, or the pressure at t° when the volume is kept constant, in terms of the volume or the pressure at 0° .

- This part of the table gives the values of $1 + .00367 t$ for values of t between 0° and 10° C by tenths of a degree.
- This part gives the values of $1 + .00367 t$ for values of t between -90° and $+1990^\circ$ C by 10° steps.

These two parts serve to give any intermediate value to one tenth of a degree by a simple computation as follows:— In the (b) table find the number corresponding to the nearest lower temperature, and to this number add the decimal part of the number in the (a) table which corresponds to the difference between the nearest temperature in the (b) table and the actual temperature. For example, let the temperature be 682.2° :

We have for 680 in table (b) the number 3.49560

And for 2.2 in table (a) the decimal00807

Hence the number for 682.2° is 3.50367

- This part gives the logarithms of $1 + .00367 t$ for values of t between -49° and $+399^\circ$ C by degrees.
- This part gives the logarithms of $1 + .00367 t$ for values of t between 400° and 1990° C by 10° steps.

(a) Values of $1 + .00367 t$ for Values of t between 0 and 10° C by 0.1° Steps

| t | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 |
|-----|---------|---------|---------|---------|---------|
| 0 | 1.00000 | 1.00037 | 1.00073 | 1.00110 | 1.00147 |
| 1 | .00367 | .00404 | .00440 | .00477 | .00514 |
| 2 | .00734 | .00771 | .00807 | .00844 | .00881 |
| 3 | .01101 | .01138 | .01174 | .01211 | .01248 |
| 4 | .01468 | .01505 | .01541 | .01578 | .01615 |
| 5 | 1.01835 | 1.01872 | 1.01908 | 1.01945 | 1.01982 |
| 6 | .02202 | .02239 | .02275 | .02312 | .02349 |
| 7 | .02569 | .02606 | .02642 | .02679 | .02716 |
| 8 | .02936 | .02973 | .03009 | .03046 | .03083 |
| 9 | .03303 | .03340 | .03376 | .03413 | .03450 |
| t | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| 0 | 1.00184 | 1.00220 | 1.00257 | 1.00294 | 1.00330 |
| 1 | .00550 | .00587 | .00624 | .00661 | .00697 |
| 2 | .00918 | .00954 | .00991 | .01028 | .01064 |
| 3 | .01284 | .01321 | .01358 | .01395 | .01431 |
| 4 | .01652 | .01688 | .01725 | .01762 | .01798 |
| 5 | 1.02018 | 1.02055 | 1.02092 | 1.02129 | 1.02165 |
| 6 | .02386 | .02422 | .02459 | .02496 | .02532 |
| 7 | .02752 | .02789 | .02826 | .02863 | .02899 |
| 8 | .03120 | .03156 | .03193 | .03229 | .03266 |
| 9 | .03486 | .03523 | .03560 | .03597 | .03633 |

(b) Logarithms of $1 + .00367 t$ for Values

| t | 0 | 1 | 2 | 3 | 4 | Mean diff. per degree. |
|------------|------------------|------------------|------------------|------------------|------------------|---------------------------|
| -40 | $\bar{1}.931051$ | $\bar{1}.929179$ | $\bar{1}.927299$ | $\bar{1}.925410$ | $\bar{1}.923513$ | 1884 |
| -30 | .949341 | .947546 | .945744 | .943934 | .942117 | 1805 |
| -20 | .966892 | .965160 | .963438 | .961701 | .959957 | 1733 |
| -10 | .983762 | .982104 | .980440 | .978769 | .977092 | 1667 |
| -0 | 0.000000 | .998403 | .996801 | .995192 | .993577 | 1605 |
| +0 | 0.000000 | 0.001591 | 0.003176 | 0.004755 | 0.006329 | 1582 |
| 10 | .015653 | .017188 | .018717 | .020241 | .021760 | 1526 |
| 20 | .030762 | .032244 | .033721 | .035193 | .036661 | 1474 |
| 30 | .045362 | .046796 | .048224 | .049648 | .051068 | 1426 |
| 40 | .059488 | .060875 | .062259 | .063637 | .065012 | 1381 |
| 50 | 0.073168 | 0.074513 | 0.075853 | 0.077190 | 0.078522 | 1335 |
| 60 | .086431 | .087735 | .089036 | .090332 | .091624 | 1299 |
| 70 | .099301 | .100597 | .101829 | .103088 | .104344 | 1259 |
| 80 | .111800 | .113030 | .114257 | .115481 | .116701 | 1226 |
| 90 | .123950 | .125146 | .126339 | .127529 | .128716 | 1191 |
| 100 | 0.135768 | 0.136933 | 0.138094 | 0.139252 | 0.140408 | 1158 |
| 110 | .147274 | .148408 | .149539 | .150667 | .151793 | 1129 |
| 120 | .158483 | .159588 | .160691 | .161790 | .162887 | 1101 |
| 130 | .169410 | .170488 | .171563 | .172635 | .173705 | 1074 |
| 140 | .180068 | .181120 | .182169 | .183216 | .184260 | 1048 |
| 150 | 0.190472 | 0.191498 | 0.192523 | 0.193545 | 0.194564 | 1023 |
| 160 | .200632 | .201635 | .202635 | .203634 | .204630 | 1000 |
| 170 | .210559 | .211540 | .212518 | .213494 | .214468 | 976 |
| 180 | .220265 | .221224 | .222180 | .223135 | .224087 | 956 |
| 190 | .229759 | .230697 | .231633 | .232567 | .233499 | 935 |
| 200 | 0.239049 | 0.239967 | 0.240884 | 0.241798 | 0.242710 | 916 |
| 210 | .248145 | .249044 | .249942 | .250837 | .251731 | 897 |
| 220 | .257054 | .257935 | .258814 | .259692 | .260567 | 878 |
| 230 | .265784 | .266648 | .267510 | .268370 | .269228 | 861 |
| 240 | .274343 | .275189 | .276034 | .276877 | .277719 | 844 |
| 250 | 0.282735 | 0.283566 | 0.284395 | 0.285222 | 0.286048 | 828 |
| 260 | .290969 | .291784 | .292597 | .293409 | .294219 | 813 |
| 270 | .299049 | .299849 | .300648 | .301445 | .302240 | 798 |
| 280 | .306982 | .307768 | .308552 | .309334 | .310115 | 784 |
| 290 | .314773 | .315544 | .316314 | .317083 | .317850 | 769 |
| 300 | 0.322426 | 0.323184 | 0.323941 | 0.324696 | 0.325450 | 756 |
| 310 | .329947 | .330692 | .331435 | .332178 | .332919 | 743 |
| 320 | .337339 | .338072 | .338803 | .339533 | .340262 | 730 |
| 330 | .344608 | .345329 | .346048 | .346766 | .347482 | 719 |
| 340 | .351758 | .352466 | .353174 | .353880 | .354585 | 707 |
| 350 | 0.358791 | 0.359488 | 0.360184 | 0.360879 | 0.361573 | 696 |
| 360 | .365713 | .366399 | .367084 | .367768 | .368451 | 684 |
| 370 | .372525 | .373201 | .373875 | .374549 | .375221 | 674 |
| 380 | .379233 | .379898 | .380562 | .381225 | .381887 | 664 |
| 390 | .385439 | .386094 | .386748 | .387401 | .388053 | 654 |

CASES.

of t between -49° and $+399^{\circ}$ G by 1° Steps

| t | 5 | 6 | 7 | 8 | 9 | Mean diff. per degree. |
|------------|------------------|------------------|------------------|------------------|------------------|---------------------------|
| -40 | $\bar{1}.921608$ | $\bar{1}.919695$ | $\bar{1}.917773$ | $\bar{1}.915843$ | $\bar{1}.913904$ | 1926 |
| -30 | .940292 | .938400 | .936619 | .934771 | .932915 | 1845 |
| -20 | .958205 | .956447 | .954681 | .952909 | .951129 | 1771 |
| -10 | .975409 | .973719 | .972022 | .970319 | .968609 | 1699 |
| -0 | .991957 | .990330 | .988697 | .987058 | .985413 | 1636 |
| +0 | 0.007897 | 0.009459 | 0.011016 | 0.012567 | 0.014113 | 1554 |
| 10 | .023273 | .024781 | .026284 | .027782 | .029274 | 1500 |
| 20 | .038123 | .039581 | .041034 | .042481 | .043924 | 1450 |
| 30 | .052482 | .053893 | .055298 | .056699 | .058096 | 1402 |
| 40 | .066382 | .067748 | .069109 | .070466 | .071819 | 1359 |
| 50 | 0.079847 | 0.081174 | 0.082495 | 0.083811 | 0.085123 | 1315 |
| 60 | .092914 | .094198 | .095486 | .096765 | .098031 | 1281 |
| 70 | .105595 | .106843 | .108088 | .109329 | .110566 | 1243 |
| 80 | .117917 | .119130 | .120340 | .121547 | .122750 | 1210 |
| 90 | .129899 | .131079 | .132256 | .133430 | .134601 | 1175 |
| 100 | 0.141559 | 0.142708 | 0.143854 | 0.144997 | 0.146137 | 1144 |
| 110 | .152915 | .154034 | .155151 | .156264 | .157375 | 1115 |
| 120 | .163981 | .164972 | .166161 | .167246 | .168330 | 1087 |
| 130 | .174772 | .175836 | .176898 | .177958 | .179014 | 1060 |
| 140 | .185301 | .186340 | .187377 | .188411 | .189443 | 1035 |
| 150 | 0.195581 | 0.196596 | 0.197608 | 0.198619 | 0.199626 | 1011 |
| 160 | .205624 | .206615 | .207605 | .208592 | .209577 | 988 |
| 170 | .215439 | .216409 | .217376 | .218341 | .219304 | 966 |
| 180 | .225038 | .225986 | .226932 | .227876 | .228819 | 946 |
| 190 | .234429 | .235357 | .236283 | .237207 | .238129 | 925 |
| 200 | 0.243621 | 0.244529 | 0.245436 | 0.246341 | 0.247244 | 906 |
| 210 | .252623 | .253512 | .254400 | .255287 | .256172 | 887 |
| 220 | .261441 | .262313 | .263184 | .264052 | .264919 | 870 |
| 230 | .270085 | .270940 | .271793 | .272644 | .273494 | 853 |
| 240 | .278559 | .279398 | .280234 | .281070 | .281903 | 836 |
| 250 | 0.286872 | 0.287694 | 0.288515 | 0.289326 | 0.290133 | 820 |
| 260 | .295028 | .295835 | .296640 | .297445 | .298248 | 805 |
| 270 | .303034 | .303827 | .304618 | .305407 | .306196 | 790 |
| 280 | .310895 | .311673 | .312450 | .313226 | .314000 | 776 |
| 290 | .318616 | .319381 | .320144 | .320906 | .321667 | 763 |
| 300 | 0.326203 | 0.326954 | 0.327704 | 0.328453 | 0.329201 | 750 |
| 310 | .333659 | .334397 | .335135 | .335871 | .336606 | 737 |
| 320 | .340989 | .341715 | .342441 | .343164 | .343887 | 724 |
| 330 | .348198 | .348912 | .349624 | .350337 | .351048 | 713 |
| 340 | .355289 | .355991 | .356693 | .357394 | .358093 | 701 |
| 350 | 0.362266 | 0.362957 | 0.363648 | 0.364337 | 0.365025 | 690 |
| 360 | .369132 | .369813 | .370493 | .371171 | .371849 | 678 |
| 370 | .375892 | .376562 | .377232 | .377900 | .378567 | 668 |
| 380 | .382548 | .383208 | .383868 | .384525 | .385183 | 658 |
| 390 | .389104 | .389754 | .390403 | .391052 | .391699 | 648 |

TABLE 105 (*continued*)
VOLUME OF GASES

(c) Values of $1 + .00367t$ for Values of t between -90° and $+2090^{\circ}$ C by
 10° Steps

| t | 00 | 10 | 20 | 30 | 40 |
|-------------|---------|---------|---------|---------|---------|
| -000 | 1.00000 | 0.96330 | 0.92660 | 0.88990 | 0.85320 |
| +000 | 1.00000 | 1.03670 | 1.07340 | 1.11010 | 1.14680 |
| 100 | 1.36700 | 1.40370 | 1.44040 | 1.47710 | 1.51380 |
| 200 | 1.73400 | 1.77070 | 1.80740 | 1.84410 | 1.88080 |
| 300 | 2.10100 | 2.13770 | 2.17440 | 2.21110 | 2.24780 |
| 400 | 2.46800 | 2.50470 | 2.54140 | 2.57810 | 2.61480 |
| 500 | 2.83500 | 2.87170 | 2.90840 | 2.94510 | 2.98180 |
| 600 | 3.20200 | 3.23870 | 3.27540 | 3.31210 | 3.34880 |
| 700 | 3.56900 | 3.60570 | 3.64240 | 3.67910 | 3.71580 |
| 800 | 3.93600 | 3.97270 | 4.00940 | 4.04610 | 4.08280 |
| 900 | 4.30300 | 4.33970 | 4.37640 | 4.41310 | 4.44980 |
| 1000 | 4.67000 | 4.70670 | 4.74340 | 4.78010 | 4.81680 |
| 1100 | 5.03700 | 5.07370 | 5.11040 | 5.14710 | 5.18380 |
| 1200 | 5.40400 | 5.44070 | 5.47740 | 5.51410 | 5.55080 |
| 1300 | 5.77100 | 5.80770 | 5.84440 | 5.88110 | 5.91780 |
| 1400 | 6.13800 | 6.17470 | 6.21140 | 6.24810 | 6.28480 |
| 1500 | 6.50500 | 6.54170 | 6.57840 | 6.61510 | 6.65180 |
| 1600 | 6.87200 | 6.90870 | 6.94540 | 6.98210 | 7.01880 |
| 1700 | 7.23900 | 7.27570 | 7.31240 | 7.34910 | 7.38580 |
| 1800 | 7.60600 | 7.64270 | 7.67940 | 7.71610 | 7.75280 |
| 1900 | 7.97300 | 8.00970 | 8.04640 | 8.08310 | 8.11980 |
| 2000 | 8.34000 | 8.37670 | 8.41340 | 8.45010 | 8.48680 |

| t | 50 | 60 | 70 | 80 | 90 |
|-------------|---------|---------|---------|---------|---------|
| -000 | 0.81650 | 0.77980 | 0.74310 | 0.70640 | 0.66970 |
| +000 | 1.18350 | 1.22020 | 1.25690 | 1.29360 | 1.33030 |
| 100 | 1.55050 | 1.58720 | 1.62390 | 1.66060 | 1.69730 |
| 200 | 1.91750 | 1.95420 | 1.99090 | 2.02760 | 2.06430 |
| 300 | 2.28450 | 2.32120 | 2.35790 | 2.39460 | 2.43130 |
| 400 | 2.65150 | 2.68820 | 2.72490 | 2.76160 | 2.79830 |
| 500 | 3.01850 | 3.05520 | 3.09190 | 3.12860 | 3.16530 |
| 600 | 3.38550 | 3.42220 | 3.45890 | 3.49560 | 3.53230 |
| 700 | 3.75250 | 3.78920 | 3.82590 | 3.86260 | 3.89930 |
| 800 | 4.11950 | 4.15620 | 4.19290 | 4.22960 | 4.26630 |
| 900 | 4.48650 | 4.52320 | 4.55990 | 4.59660 | 4.63330 |
| 1000 | 4.85350 | 4.89020 | 4.92690 | 4.96360 | 5.00030 |
| 1100 | 5.22050 | 5.25720 | 5.29390 | 5.33060 | 5.36730 |
| 1200 | 5.58750 | 5.62420 | 5.66090 | 5.69760 | 5.73430 |
| 1300 | 5.95450 | 5.99120 | 6.02790 | 6.06460 | 6.10130 |
| 1400 | 6.32150 | 6.35820 | 6.39490 | 6.43160 | 6.46830 |
| 1500 | 6.68850 | 6.72520 | 6.76190 | 6.79860 | 6.83530 |
| 1600 | 7.05550 | 7.09220 | 7.12890 | 7.16560 | 7.20230 |
| 1700 | 7.42250 | 7.45920 | 7.49590 | 7.53260 | 7.56930 |
| 1800 | 7.78950 | 7.82620 | 7.86290 | 7.89960 | 7.93630 |
| 1900 | 8.15650 | 8.19320 | 8.22990 | 8.26660 | 8.30330 |
| 2000 | 8.52350 | 8.56020 | 8.59690 | 8.63360 | 8.67030 |

VOLUME OF GASES

(d) Logarithms of $1 + .00367 t$ for Values of t between 400° and 1990° C by 10° Steps

| t | 00 | 10 | 20 | 30 | 40 |
|-------------|----------|----------|----------|----------|----------|
| 400 | 0.392345 | 0.398756 | 0.405073 | 0.411300 | 0.417439 |
| 500 | 0.452553 | 0.458139 | 0.463654 | 0.469100 | 0.474479 |
| 600 | .505421 | .510371 | .515264 | .520103 | .524889 |
| 700 | .552547 | .556990 | .561388 | .565742 | .570052 |
| 800 | .595955 | .599086 | .603079 | .607037 | .610958 |
| 900 | .633771 | .637460 | .641117 | .644744 | .648341 |
| 1000 | 0.669317 | 0.672717 | 0.676090 | 0.679437 | 0.682759 |
| 1100 | .702172 | .705325 | .708455 | .711563 | .714648 |
| 1200 | .732715 | .735655 | .738575 | .741475 | .744356 |
| 1300 | .761251 | .764004 | .766740 | .769459 | .772160 |
| 1400 | .788027 | .790616 | .793190 | .795748 | .798292 |
| 1500 | 0.813247 | 0.815691 | 0.818120 | 0.820536 | 0.822939 |
| 1600 | .837083 | .839396 | .841697 | .843986 | .846263 |
| 1700 | .859679 | .861875 | .864060 | .866234 | .868398 |
| 1800 | .881156 | .883247 | .885327 | .887398 | .889459 |
| 1900 | .901622 | .903616 | .905602 | .907578 | .909545 |

| t | 50 | 60 | 70 | 80 | 90 |
|-------------|----------|----------|----------|----------|----------|
| 400 | 0.423492 | 0.429462 | 0.435351 | 0.441161 | 0.446804 |
| 500 | 0.479791 | 0.485040 | 0.490225 | 0.495350 | 0.500415 |
| 600 | .529623 | .534305 | .538938 | .543522 | .548058 |
| 700 | .574321 | .578548 | .582734 | .586880 | .590987 |
| 800 | .614845 | .618696 | .622515 | .626299 | .630051 |
| 900 | .651908 | .655446 | .658955 | .662437 | .665890 |
| 1000 | 0.686055 | 0.689327 | 0.692574 | 0.695797 | 0.698996 |
| 1100 | .717712 | .720755 | .723776 | .726776 | .729756 |
| 1200 | .747218 | .750061 | .752886 | .755692 | .758480 |
| 1300 | .774845 | .777514 | .780166 | .782802 | .785422 |
| 1400 | .800820 | .803334 | .805834 | .808319 | .810790 |
| 1500 | 0.825329 | 0.827705 | 0.830069 | 0.832420 | 0.834758 |
| 1600 | .848528 | .850781 | .853023 | .855253 | .857471 |
| 1700 | .870550 | .872692 | .874824 | .876945 | .879056 |
| 1800 | .891510 | .893551 | .895583 | .897605 | .899618 |
| 1900 | .911504 | .913451 | .915395 | .917327 | .919251 |

COMPRESSIBILITY OF LIQUIDS

At the constant temperature t , the compressibility $\beta = (1/V)(dV/dP)$. In general as P increases, β decreases rapidly at first and then slowly; the change of β with t is large at low pressures but very small at pressures above 1000 to 2000 megabaryes. 1 megabarye $= 10^6$ dynes/cm² $= 1.020$ kg/cm² $= 0.987$ atmospheres.

| Substance. | Temp. °C | Pressure, megabaryes. | Compressibility per megabaryes, $\beta \times 10^6$. | Reference. | Substance. | Temp. °C | Pressure, megabaryes. | Compressibility per megabaryes, $\beta \times 10^6$. | Reference. |
|----------------------|----------|-----------------------|---|------------|----------------------|----------|-----------------------|---|------------|
| Acetone. | 14 | 23 | 111 | 9 | Ethyl ether, ct'd... | 20 | 1,000 | 61 | 1 |
| " " " " " " | 20 | 500 | 61 | 1 | " " " " " " | 20 | 12,000 | 10 | 1 |
| " " " " " " | 20 | 1,000 | 52 | 1 | Ethyl iodide. | 20 | 200 | 81 | 16 |
| " " " " " " | 40 | 12,000 | 9 | 1 | " " " " " " | 20 | 400 | 60 | 16 |
| Amyl alcohol. | 14 | 23 | 88 | 10 | " " " " " " | 20 | 500 | 64 | 1 |
| " " " iso. | 20 | 200 | 84 | 16 | " " " " " " | 20 | 1,000 | 50 | 1 |
| " " " iso. | 20 | 400 | 70 | 16 | " " " " " " | 20 | 12,000 | 8 | 1 |
| " " " " " " | 20 | 500 | 61 | 1 | Gallium. | 30 | 300 | 3.97 | 6 |
| " " " " " " | 20 | 1,000 | 46 | 1 | Glycerine. | 15 | 5 | 22 | 12 |
| " " " " " " | 20 | 12,000 | 8 | 1 | Hexane. | 20 | 200 | 117 | 16 |
| " " " " " " | 40 | 12,000 | 8 | 1 | " " " " " " | 20 | 400 | 91 | 16 |
| Benzene. | 17 | 5 | 89 | 2, 3 | Kerosene. | 20 | 500 | 55 | 1 |
| " " " " " " | 20 | 200 | 77 | 16 | " " " " " " | 20 | 1,000 | 45 | 1 |
| " " " " " " | 20 | 400 | 67 | 16 | " " " " " " | 20 | 12,000 | 8 | 1 |
| Bromine. | 20 | 200 | 56 | 16 | " " " " " " | 20 | 12,000 | 8 | 13 |
| " " " " " " | 20 | 400 | 51 | 16 | Mercury. | 20 | 300 | 3.95 | 7 |
| Butyl alcohol, iso.. | 18 | 8 | 97 | 2 | " " " " " " | 22 | 500 | 3.97 | 8 |
| " " " iso. | 20 | 200 | 81 | 16 | " " " " " " | 22 | 1,000 | 3.91 | 8 |
| " " " iso. | 20 | 400 | 64 | 16 | " " " " " " | 22 | 12,000 | 2.37 | 8 |
| " " " iso. | 20 | 500 | 56 | 1 | Methyl alcohol. | 15 | 23 | 103 | 10 |
| " " " iso. | 20 | 1,000 | 46 | 1 | " " " " " " | 20 | 200 | 95 | 16 |
| " " " iso. | 20 | 12,000 | 8 | 1 | " " " " " " | 20 | 400 | 80 | 16 |
| Carbon bisulphide.. | 16 | 21 | 86 | 10 | " " " " " " | 20 | 500 | 65 | 1 |
| " " " " " " | 20 | 500 | 57 | 1 | " " " " " " | 20 | 1,000 | 54 | 1 |
| " " " " " " | 20 | 1,000 | 48 | 1 | " " " " " " | 20 | 12,000 | 8 | 1 |
| " " " " " " | 20 | 12,000 | 6 | 1 | Nitric acid. | 0 | 17 | 32 | 14 |
| Carb. tetrachloride. | 20 | 200 | 86 | 16 | Oils: Almond. | 15 | 5 | 53 | 12 |
| " " " " " " | 20 | 400 | 73 | 16 | Castor. | 15 | 5 | 46 | 12 |
| Chloroform. | 20 | 200 | 83 | 16 | Linseed. | 15 | 5 | 51 | 12 |
| " " " " " " | 20 | 400 | 70 | 16 | Olive. | 15 | 5 | 55 | 12 |
| Dichlorethylsulfide. | 32 | 1,000 | 34 | 5 | Rape-seed. | 20 | — | 59 | 15 |
| " " " " " " | 32 | 2,000 | 24 | 5 | Phosph. trichloride. | 10 | 250 | 71 | 11 |
| Ethyl acetate. | 13 | 23 | 103 | 10 | " " " " " " | 20 | 500 | 63 | 1 |
| " " " " " " | 20 | 200 | 90 | 16 | " " " " " " | 20 | 1,000 | 47 | 1 |
| " " " " " " | 20 | 400 | 75 | 16 | " " " " " " | 20 | 12,000 | 8 | 1 |
| Ethyl alcohol. | 14 | 23 | 100 | 10 | Propyl alcohol, n... | 20 | 200 | 77 | 16 |
| " " " " " " | 20 | 500 | 63 | 1 | " " " " (n?) | 20 | 400 | 67 | 16 |
| " " " " " " | 20 | 1,000 | 54 | 1 | " " " " (n?) | 20 | 500 | 65 | 1 |
| " " " " " " | 20 | 12,000 | 8 | 1 | " " " " (n?) | 20 | 1,000 | 47 | 1 |
| Ethyl bromide. | 20 | 200 | 100 | 16 | " " " " (n?) | 20 | 12,000 | 7 | 1 |
| " " " " " " | 20 | 400 | 82 | 16 | Toluene. | 20 | 200 | 74 | 16 |
| " " " " " " | 20 | 500 | 70 | 1 | " " " " " " | 20 | 400 | 64 | 16 |
| " " " " " " | 20 | 1,000 | 54 | 1 | Turpentine. | 20 | — | 74 | 15 |
| " " " " " " | 20 | 12,000 | 8 | 1 | Water. | 20 | 13 | 49 | 11 |
| Ethyl chloride. | 15 | 23 | 151 | 10 | " " " " " " | 20 | 200 | 43 | 16 |
| " " " " " " | 20 | 500 | 102 | 1 | " " " " " " | 20 | 400 | 41 | 16 |
| " " " " " " | 20 | 1,000 | 66 | 1 | " " " " " " | 20 | 500 | 39 | 4 |
| " " " " " " | 20 | 12,000 | 8 | 1 | " " " " " " | 40 | 500 | 38 | 4 |
| Ethyl ether. | 25 | 23 | 188 | 10 | " " " " " " | 40 | 1000 | 33 | 4 |
| " " " " " " | 20 | 500 | 84 | 1 | " " " " " " | 40 | 12,000 | 9 | 4 |
| | | | | | Xylene, meta. | 20 | 200 | 60 | 16 |
| | | | | | " " " " " " | 20 | 400 | 60 | 16 |

For references, see page 156.

COMPRESSIBILITY AND THERMAL EXPANSION OF PETROLEUM OILS,

0.50 kg/cm², 0-400°C

(R. S. Jessup, Bur. Standards Journ. Res., 5, 985, 1930.)

It was found that the compressibility and thermal expansion of two samples of the same specific gravity, but from different sources, differed more than 30 per cent at the higher temperatures, whereas oils of the same specific gravity and the same viscosity had the same compressibility and thermal expansion within rather narrow limits. In other words, with a knowledge of the specific gravity and viscosity of the oils, it was possible to represent all the measured volumes within less than 0.5 per cent over the entire range of temperature and pressure covered by the measurements.

| Kinematic viscosity 100°F., c.g.s. | Specific gravity 60°/60°F. | Pressure kg/cm ² | Relative volumes | | | | | | |
|--|----------------------------------|--------------------------------|------------------|-------|-------|-------|-------|-------|--------|
| | | | 0° | 20° | 50° | 100° | 200° | 300° | 400° |
| .020 | .80 | 0 | 1.000 | 1.018 | 1.045 | 1.096 | 1.222 | 1.422 | |
| " | " | 50 | 0.996 | 1.014 | 1.041 | 1.089 | 1.205 | 1.370 | (1.63) |
| " | .85 | 0 | 1.000 | 1.017 | 1.044 | 1.093 | 1.213 | 1.396 | (1.71) |
| " | " | 50 | 0.997 | 1.014 | 1.040 | 1.086 | 1.197 | 1.352 | (1.58) |
| " | .90 | 0 | 1.000 | 1.017 | 1.043 | 1.090 | 1.204 | 1.375 | (1.67) |
| " | " | 50 | 0.997 | 1.013 | 1.038 | 1.084 | 1.191 | 1.337 | (1.55) |
| .050 | .80 | 0 | 1.000 | 1.017 | 1.043 | 1.089 | 1.202 | 1.369 | (1.71) |
| " | " | 50 | 0.997 | 1.013 | 1.038 | 1.083 | 1.189 | 1.333 | (1.56) |
| " | .85 | 0 | 1.000 | 1.016 | 1.041 | 1.087 | 1.194 | 1.349 | (1.63) |
| " | " | 50 | 0.997 | 1.013 | 1.037 | 1.081 | 1.182 | 1.318 | (1.51) |
| " | .90 | 0 | 1.000 | 1.016 | 1.040 | 1.084 | 1.188 | 1.331 | (1.56) |
| " | " | 50 | 0.997 | 1.012 | 1.036 | 1.078 | 1.176 | 1.304 | (1.48) |
| .100 | .85 | 0 | 1.000 | 1.016 | 1.040 | 1.083 | 1.185 | 1.325 | (1.54) |
| " | " | 50 | 0.997 | 1.012 | 1.036 | 1.078 | 1.174 | 1.299 | (1.47) |
| " | .95 | 0 | 1.000 | 1.015 | 1.038 | 1.079 | 1.174 | 1.297 | (1.47) |
| " | " | 50 | 0.997 | 1.012 | 1.034 | 1.074 | 1.164 | 1.276 | (1.43) |
| .500 | .85 | 0 | 1.000 | 1.015 | 1.038 | 1.078 | 1.170 | 1.280 | (1.45) |
| " | " | 50 | 0.997 | 1.012 | 1.034 | 1.073 | 1.161 | 1.260 | (1.41) |
| " | .95 | 0 | 1.000 | 1.014 | 1.036 | 1.074 | 1.161 | 1.260 | (1.40) |
| " | " | 50 | 0.998 | 1.012 | 1.033 | 1.070 | 1.152 | 1.252 | (1.37) |
| 1.000 | .85 | 0 | 1.000 | 1.015 | 1.037 | 1.076 | 1.165 | 1.279 | (1.43) |
| " | " | 50 | 0.997 | 1.012 | 1.034 | 1.071 | 1.157 | 1.260 | (1.39) |
| " | .95 | 0 | 1.000 | 1.014 | 1.035 | 1.073 | 1.157 | 1.261 | (1.39) |
| " | " | 50 | 0.998 | 1.011 | 1.032 | 1.068 | 1.149 | 1.244 | (1.36) |
| 2.000 | .85 | 0 | 1.000 | 1.014 | 1.036 | 1.075 | 1.162 | 1.270 | (1.41) |
| " | " | 50 | 0.998 | 1.011 | 1.033 | 1.070 | 1.153 | 1.253 | (1.37) |
| " | .95 | 0 | 1.000 | 1.014 | 1.035 | 1.071 | 1.153 | 1.254 | (1.37) |
| " | " | 50 | 0.998 | 1.011 | 1.032 | 1.067 | 1.145 | 1.239 | (1.35) |
| 5.000 | .85 | 0 | 1.000 | 1.014 | 1.035 | 1.073 | 1.157 | 1.261 | (1.39) |
| " | " | 50 | 0.998 | 1.011 | 1.032 | 1.068 | 1.149 | 1.245 | (1.36) |
| " | .95 | ● | 1.000 | 1.013 | 1.034 | 1.069 | 1.148 | 1.244 | (1.36) |
| " | " | 50 | 0.998 | 1.011 | 1.031 | 1.065 | 1.141 | 1.229 | (1.33) |
| 210°F., c.g.s. | 60°/60°F. | kg/cm ² | 0° | 20° | 50° | 100° | 200° | 300° | 400° |
| .100 | .90 | 0 | 1.000 | 1.014 | 1.036 | 1.074 | 1.161 | 1.260 | (1.41) |
| " | " | 50 | 0.998 | 1.011 | 1.032 | 1.070 | 1.152 | 1.252 | (1.37) |
| " | .95 | 0 | 1.000 | 1.014 | 1.035 | 1.071 | 1.154 | 1.256 | (1.38) |
| " | " | 50 | 0.998 | 1.011 | 1.032 | 1.067 | 1.147 | 1.241 | (1.35) |
| " | 1.00 | 0 | 1.000 | 1.014 | 1.034 | 1.070 | 1.149 | 1.247 | (1.37) |
| " | " | 50 | 0.998 | 1.011 | 1.031 | 1.066 | 1.142 | 1.232 | (1.34) |
| .200 | .90 | 0 | 1.000 | 1.014 | 1.035 | 1.072 | 1.155 | 1.258 | (1.39) |
| " | " | 50 | 0.998 | 1.011 | 1.031 | 1.067 | 1.147 | 1.241 | (1.35) |
| " | 1.00 | 0 | 1.000 | 1.013 | 1.033 | 1.067 | 1.144 | 1.237 | (1.35) |
| " | " | 50 | 0.998 | 1.011 | 1.030 | 1.064 | 1.137 | 1.223 | (1.32) |
| .440 | .90 | 0 | 1.000 | 1.013 | 1.034 | 1.070 | 1.151 | 1.248 | (1.36) |
| " | " | 50 | 0.998 | 1.011 | 1.031 | 1.066 | 1.143 | 1.234 | (1.34) |
| " | 1.00 | 0 | 1.000 | 1.012 | 1.032 | 1.066 | 1.140 | 1.228 | (1.33) |
| " | " | 50 | 0.998 | 1.010 | 1.029 | 1.063 | 1.134 | 1.214 | (1.31) |
| 1.100 | .90 | 0 | 1.000 | 1.013 | 1.033 | 1.068 | 1.146 | 1.241 | (1.35) |
| " | " | 50 | 0.998 | 1.010 | 1.030 | 1.065 | 1.139 | 1.225 | (1.33) |
| " | 1.00 | 0 | 1.000 | 1.012 | 1.031 | 1.063 | 1.134 | 1.218 | (1.32) |
| " | " | 50 | 0.998 | 1.010 | 1.028 | 1.060 | 1.128 | 1.205 | (1.29) |

COMPRESSIBILITY OF SOLIDS

If V is the volume of the material under a pressure P megabaryes and V_0 is the volume at atmospheric pressure, then the compressibility $\beta = -(1/V_0)(dV/dP)$. Its unit is $\text{cm}^2/\text{megadynes}$ (reciprocal megabaryes). $10^6/\beta$ is the bulk modulus in absolute units (dynes/ cm^2). The following values of β , arranged in order of increasing compressibility, are for $P = 0$ and room temperature. 1 megabarye = 10^6 dynes/ cm^2 = 1.020 kg/ cm^2 = 0.987 atmosphere.

| Substance | Compression per unit vol. per megabarye $\times 10^6$ | Bulk modulus, dynes/ cm^2 $\times 10^{12}$ | Reference | Substance | Compression per unit vol. per megabarye $\times 10^6$ | Bulk modulus, dynes/ cm^2 $\times 10^{12}$ | Reference |
|-------------------------|---|---|-----------|-------------------------|---|---|-----------|
| Tungsten..... | 0.27 | 3.7 | 2 | Plate glass..... | 2.23 | 0.45 | 4 |
| Boron..... | 0.3 | 3.0 | 2 | Lead..... | 2.27 | 0.44 | 1, 2 |
| Silicon..... | 0.32 | 3.1 | 2 | Thallium..... | 2.3 | 0.43 | 2 |
| Platinum..... | 0.38 | 2.6 | 2 | Antimony..... | 2.4 | 0.42 | 2 |
| Nickel..... | 0.43 | 2.3 | 2 | Quartz..... | 2.7 | 0.37 | 1 |
| Molybdenum..... | 0.46 | 2.2 | 2 | Magnesium..... | 2.9 | 0.34 | 2 |
| Tantalum..... | 0.53 | 1.9 | 2 | Bismuth..... | 3.0 | 0.33 | 1 |
| Palladium..... | 0.54 | 1.9 | 2 | Graphite..... | 3.0 | 0.33 | 2 |
| Cobalt..... | 0.55 | 1.82 | 9 | Silica glass..... | 3.1 | 0.32 | 1 |
| Nichrome..... | 0.56 | 1.79 | 9 | Cerium..... | 3.6 | 0.27 | 9 |
| Iron..... | 0.60 | 1.67 | 3 | Sodium chloride..... | 4.12 | 0.24 | 1 |
| Gold..... | 0.60 | 1.67 | 1, 2 | Arsenic..... | 4.5 | 0.22 | 2 |
| Pyrite..... | 0.7 | 1.4 | 4 | Calcium..... | 5.7 | 0.175 | 2 |
| Copper..... | 0.75 | 1.33 | 1 | Potassium chloride..... | 7.4 | 0.135 | 6 |
| Manganese..... | 0.84 | 1.19 | 2 | Strontium..... | 8.4 | 0.120 | 9 |
| Brass..... | 0.89 | 1.12 | 1 | Lithium..... | 9.0 | 0.111 | 2 |
| Chromium..... | 0.9 | 1.12 | 1 | Phosphorus (red)..... | 9.2 | 0.109 | 2 |
| Silver..... | 0.99 | 1.01 | 1, 2 | Selenium..... | 12.0 | 0.083 | 2 |
| Mg. silicate, crys..... | 1.03 | 0.97 | 4 | Ice..... | 12.0 | 0.083 | 8 |
| Mg. silicate..... | 1.21 | 0.82 | 7 | Sulphur..... | 12.9 | 0.078 | 2 |
| Aluminum..... | 1.33 | 0.75 | 1-3 | Iodine..... | 13.0 | 0.077 | 2 |
| Calcite..... | 1.39 | 0.72 | 1 | Sodium..... | 15.6 | 0.064 | 2 |
| Germanium..... | 1.40 | 0.71 | 9 | Hard rubber..... | 19.4 | | 7 |
| Zinc..... | 1.74 | 0.57 | 1 | Phosphorus (white)..... | 20.5 | 0.049 | 2 |
| Tin..... | 1.89 | 0.53 | 1 | Potassium..... | 31.7 | 0.032 | 2 |
| Gallium..... | 2.09 | 0.48 | 5 | Rubidium..... | 40.0 | 0.025 | 2 |
| Cadmium..... | 2.17 | 0.46 | 1, 2 | Caesium..... | 61.0 | 0.016 | 2 |

Winklemann, Schott, and Straule (Wied Ann., 1897, 1899) give the following (among others) for Jena glasses in terms of the volume decrease divided by the increase of pressure expressed in kg/mm².

| No. | Glass | Bulk moduli | No. | Glass | Bulk moduli |
|------|----------------------------|-------------|------|-----------------------------------|-------------|
| 665 | | 7520 | 2154 | Kaliblisilicat..... | 3660 |
| 1299 | Barytborosilicat..... | 5800 | S208 | Heaviest Bleisilicat..... | 3550 |
| 16 | Natronkalkzinksilicat..... | 4530 | S196 | Tonerdborat with sodium, baryte.. | 3470 |

These values are in $\text{cm}^2/\text{kg} \times 10^6 \times$ Compressibility, Grüneisen, Ann. der Phys. 33, p. 65, 1910.

Al — 191° , 1.32; 17° , 1.46; 125° , 1.70
 Cu — 191° , 0.72; 17° , 0.77; 165° , 0.83
 Pt — 189° , 0.37; 17° , 0.39; 164° , 0.40

Fe — 190° , 0.61; 18° , 0.63; 165° , 0.67
 Ag — 191° , 0.71; 16° , 0.76; 166° , 0.86
 Pb — 191° , (2.5); 14° , (3.2)

References to Table 106, p. 154:

- (1) Bridgman, Pr. Am. Acad. 49, 1, 1913;
- (2) Roentgen, Ann. Phys. 44, 1, 1891;
- (3) Pagliani-Palazzo, Mem. Acad. Lin. 3, 18, 1883;
- (4) Bridgman, Pr. Am. Acad. 48, 341, 1912;
- (5) Adams, Williamson, J. Wash. Acad. Sc. 9, Jan. 19, 1919;
- (6) Richards, Boyer, Pr. Nat. Acad. Sc. 4, 389, 1918;
- (7) Richards, J. Am. Ch. Soc. 37, 1646, 1915;
- (8) Bridgman, Pr. Am. Acad. 47, 381, 1911;
- (9) Amagat, C. R. 73, 143, 1872;
- (10) Amagat, C. R. 68, 1170, 1869;
- (11) Amagat, Ann. chim. phys. 29, 68, 505, 1893;
- (12) de Metz, Ann. Phys. 41, 663, 1890;
- (13) Adams, Williamson, Johnston, J. Am. Chem. Soc. 41, 27, 1919;
- (14) Colladon, Sturm, Ann. Phys. 12, 39, 1828;
- (15) Quincke, Ann. Phys. 19, 401, 1883;
- (16) Richards *et al.* J. Am. Ch. Soc. 34, 988, 1912.

References to Table 108, p. 156:

- (1) Adams, Williamson, Johnston, J. Am. Ch. Soc. 41, 39, 1919;
- (2) Richards, *ibid.* 37, 1646, 1915;
- (3) Bridgman, Pr. Am. Acad. 44, 279, 1909; 47, 366, 1911;
- (4) Adams, Williamson, unpublished;
- (5) Richards, Boyer, Pr. Nat. Acad. Sc. 4, 388, 1918;
- (6) Voigt, Ann. Phys. 31, 1887; 36, 1888;
- (7) R. E. Gibson, L. H. Adams, unpublished;
- (8) Bridgman, Pr. Am. Acad., 48, 310, 1912;
- (9) Bridgman, Pr. Am. Acad., 58, 166, 1923.

TABLE 109
COMPRESSIBILITY OF CRYSTALS

| Crystal | System | Linear, $L/L_0 =$ $a/p - b/p^2 =$ | | Volume, $V/V_0 =$ $a/p - b/p^2 =$ | | | |
|--------------------|------------------------|--------------------------------------|--------------------|--------------------------------------|--------------------|-----------------|--------------------|
| | | 30°C | | 30°C | | 75°C | |
| | | $a \times 10^6$ | $b \times 10^{12}$ | $a \times 10^6$ | $b \times 10^{12}$ | $a \times 10^6$ | $b \times 10^{12}$ |
| Quartz | Trigonal \parallel * | 0.7052 | 6.44 | 2.658 | 24.4 | 2.705 | 25.0 |
| | \perp * | .9764 | 7.79 | | | | |
| Hanksite | Hexagonal \parallel | 1.1651 | 12.34 | 2.413 | 24.8 | 2.509 | 26.9 |
| | \perp | .624 | 5.31 | | | | |
| Orthoclase | Monoclinic A | .9944 | 5.09 | 2.085 | 15.3 | 2.078 | 14.8 |
| | B | .5490 | 5.15 | | | | |
| | C | .4599 | 1.68 | | | | |
| | Y | 1.0765 | 7.14 | | | | |
| Galena | Cubic | .6122 | 2.48 | 1.837 | 6.33 | 1.893 | 7.14 |
| Barite | Orthorhom A | .4940 | 3.57 | 1.729 | 12.70 | 1.760 | 13.44 |
| | B | .6695 | 4.34 | | | | |
| | C | .5660 | 3.81 | | | | |
| Celestite | Orthorhom A | .6268 | 3.67 | 1.528 | 7.20 | 1.545 | 8.67 |
| | B | .4476 | 2.59 | | | | |
| | C | .4537 | 1.70 | | | | |
| Calcite | Trigonal \parallel | .8071 | 3.26 | 1.345 | 4.16 | 1.370 | 4.38 |
| | \perp | .2688 | .70 | | | | |
| Sphalerite | Cubic† | .427 | .70 | 1.281 | 1.56 | 1.257 | 1.56 |
| Fluorite | Cubic | .4019 | 2.39 | 1.206 | 6.69 | 1.238 | 6.75 |
| Apatite | Hexagonal \parallel | .2410 | .35 | 1.0730 | 5.34 | 1.0910 | 5.07 |
| | \perp | .4160 | 2.31 | | | | |
| Jeffersonite | Monoclinic A | .3093 | 2.02 | .8947 | 5.21 | .9400 | 6.79 |
| | B | .3924 | 1.74 | | | | |
| | C | .3078 | 2.51 | | | | |
| | Y | .1945 | .70 | | | | |
| Tourmaline (black) | Trigonal \parallel | .478 | 1.59 | .804 | 3.18 | .849 | 3.37 |
| | \perp | .163 | .70 | | | | |
| Cobaltite | Cubic | .2519 | 1.01 | .756 | 2.85 | .768 | 2.82 |
| Spodumene | Monoclinic A | .1801 | .70 | .6930 | 2.84 | .6969 | 3.50 |
| | B | .2459 | .70 | | | | |
| | C | .1997 | .70 | | | | |
| | Y | .2474 | 1.28 | | | | |
| Pyrite | Cubic | .2243 | .70 | .673 | 1.95 | .671 | 1.95 |
| Andradite | Cubic | .2210 | .70 | .6630 | 2.25 | .6606 | 2.25 |
| Topaz | Orthorhom A | .2145 | .70 | .6024 | 2.32 | .5991 | 2.32 |
| | B | .1486 | .70 | | | | |
| | C | .2393 | .70 | | | | |
| Magnetite | Cubic | .1799 | .70 | .5397 | 2.01 | .5376 | 2.01 |
| Garnet | Cubic | .1793 | .73 | .5379 | 2.19 | .5439 | 2.19 |

* These symbols relate to the corresponding trigonal, tetragonal, hexagonal, axes respectively. † Transition above 9000°. Data from Bridgman, Amer. Journ. Sci., 10, Dec., 1925; 15, Apr., 1928. Unit of pressure kg/cm². The following additional crystal volume compressibilities have been taken from Madelung, Fuchs, Ann. Phys., 65, 305, 1921. Their unit of pressure is dynes $\times 10^6$ per cm² at 0°C. 1 dyne/cm² equals 1.020×10^{-6} kg/cm².

| | | | | | |
|---|--------|---|------|--|------|
| Sylvite, KCl | 5.62 | Anhydrite, CaSO ₄ | 1.76 | Zincite, ZnO | 0.77 |
| Halite, NaCl | 4.14 | Strontianite, SrCO ₃ | 1.74 | Periclase, MgO | 0.71 |
| AgNO ₃ | 3.67 | Aragonite, CaCO ₃ | 1.53 | Hematite (specular) | 0.59 |
| Bismuthinite, Bi ₂ S ₃ | 3.31 | Rhodocrosite, MnFeS ₂ | 1.3 | Rutile, TiO ₂ | 0.58 |
| Argentite, Ag ₂ S | 3.06 | Chalcocryite, CuFeS ₂ | 1.28 | Ilmenite, (FeTi)O ₃ | 0.55 |
| Gypsum | 2.52 | Dolomite, CaCO ₃ MgCO ₃ | 1.21 | Cassiterite, SnO ₂ | 0.48 |
| Witherite, BaCO ₃ | 2.02 | Hematite, Fe ₂ O ₃ | 1.08 | Sapphire | 0.43 |
| Anglesite, PbSO ₄ | (1.93) | Siderite, FeCO ₃ | 0.99 | Corundum, Al ₂ O ₃ | 0.38 |
| Cerussite, PbCO ₃ | 1.90 | Zircon, SiO ₂ ZnO ₂ | 0.85 | | |
| Andularia, K ₂ Al ₂ Si ₆ O ₁₆ | 1.79 | Marcasite, FeS ₂ | 0.81 | | |

SMITHSONIAN TABLES

TABLE 110. — Specific Gravities Corresponding to the Baumé Scale

The specific gravities are for 15.56°C (60°F.) referred to water at the same temperature as unity. For specific gravities less than unity the values are calculated from the formula:

$$\text{Degrees Baumé} = \frac{140}{\text{Specific Gravity}} - 130.$$

For specific gravities greater than unity from:

$$\text{Degrees Baumé} = 145 - \frac{145}{\text{Specific Gravity}}.$$

| Specific Gravities less than 1. | | | | | | | | | | |
|------------------------------------|----------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Specific Gravity. | 0.00 | 0.01 | 0.02 | 0.03 | 0.04 | 0.05 | 0.06 | 0.07 | 0.08 | 0.09 |
| | Degrees Baumé. | | | | | | | | | |
| 0.60 | 103.33 | 99.51 | 95.81 | 92.22 | 88.75 | 85.38 | 82.12 | 78.95 | 75.88 | 72.90 |
| .70 | 70.00 | 67.18 | 64.44 | 61.78 | 59.19 | 56.67 | 54.21 | 51.82 | 49.49 | 47.22 |
| .80 | 45.00 | 42.84 | 40.73 | 38.68 | 36.67 | 34.71 | 32.79 | 30.92 | 29.09 | 27.30 |
| .90 | 25.56 | 23.85 | 22.17 | 20.54 | 18.94 | 17.37 | 15.83 | 14.33 | 12.86 | 11.41 |
| 1.00 | 10.00 | | | | | | | | | |
| Specific Gravities greater than 1. | | | | | | | | | | |
| Specific Gravity. | 0.00 | 0.01 | 0.02 | 0.03 | 0.04 | 0.05 | 0.06 | 0.07 | 0.08 | 0.09 |
| | Degrees Baumé. | | | | | | | | | |
| 1.00 | 0.00 | 1.44 | 2.84 | 4.22 | 5.58 | 6.91 | 8.21 | 9.49 | 10.74 | 11.97 |
| 1.10 | 13.18 | 14.37 | 15.54 | 16.68 | 17.81 | 18.91 | 20.00 | 21.07 | 22.12 | 23.15 |
| 1.20 | 24.17 | 25.16 | 26.15 | 27.11 | 28.06 | 29.00 | 29.92 | 30.83 | 31.72 | 32.60 |
| 1.30 | 33.46 | 34.31 | 35.15 | 35.98 | 36.79 | 37.59 | 38.38 | 39.16 | 39.93 | 40.68 |
| 1.40 | 41.43 | 42.16 | 42.89 | 43.60 | 44.31 | 45.00 | 45.68 | 46.36 | 47.03 | 47.68 |
| 1.50 | 48.33 | 48.97 | 49.60 | 50.23 | 50.84 | 51.45 | 52.05 | 52.64 | 53.23 | 53.80 |
| 1.60 | 54.33 | 54.94 | 55.49 | 56.04 | 56.58 | 57.12 | 57.65 | 58.17 | 58.69 | 59.20 |
| 1.70 | 59.71 | 60.20 | 60.70 | 61.18 | 61.67 | 62.14 | 62.61 | 63.08 | 63.54 | 63.99 |
| 1.80 | 64.44 | 64.89 | 65.33 | 65.76 | 66.20 | 66.62 | | | | |

TABLE 111. Degrees A. P. I. Corresponding to Specific Gravities at 60°/60° F.

(15.56°/15.56° C) for petroleum oils.

In order to avoid confusion and misunderstanding the American Petroleum Institute, the Bureau of Mines, and the Bureau of Standards have agreed that a scale based on the modulus 141.5 shall be used in the United States Petroleum Industry and shall be known as the A. P. I. scale. The United States Baumé scale based on the modulus 140 will continue to be used for other liquids lighter than water.

$$\text{Calculated from the formula, degrees A. P. I.} = \frac{141.5}{\text{Sp. Gr. } 60^\circ/60^\circ \text{ F}} - 131.5$$

| Degrees A. P. I. 60°/60° F. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|-----------------------------|--------|--------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0.6 | 104.33 | 100.47 | 96.73 | 93.10 | 89.59 | 86.19 | 82.89 | 79.69 | 76.59 | 73.57 |
| .7 | 70.64 | 67.80 | 65.03 | 62.34 | 59.72 | 57.17 | 54.68 | 52.27 | 49.91 | 47.61 |
| .8 | 45.38 | 43.19 | 41.06 | 38.98 | 36.95 | 34.97 | 33.03 | 31.14 | 29.30 | 27.49 |
| .9 | 25.72 | 23.99 | 22.30 | 20.65 | 19.03 | 17.45 | 15.90 | 14.38 | 12.89 | 11.43 |
| 1.0 | 10.00 | | | | | | | | | |

DENSITY OF THE ELEMENTS, LIQUID OR SOLID

The density may depend considerably on previous treatment.
To reduce to lbs./cu. ft. multiply by 62.4.

| Element | Physical State | g/cm ³ | °C* | Authority |
|-----------|--------------------|-------------------|-------|--------------------------|
| Aluminum | commercial h'd d'n | 2.70 | 20° | Wolf, Dellinger, 1910 |
| " | liquid | 2.43 | 740 | |
| " | " | 2.29 | 1000 | Edwards, Taylor |
| Antimony | vacuo-distilled | 6.618 | 20 | Kahlbaum, 1902 |
| " | ditto-compressed | 6.691 | 20 | " |
| " | amorphous | 6.22 | | Hérard |
| " | liquid | 6.55 | 631 | Pascal, Jauniaux |
| Argon | " | 1.40 | -186 | Baly-Donnan |
| " | solid | 1.65 | -233 | Simon, 1924 |
| Arsenic | crystallized | 5.73 | 14 | |
| " | amorph. br.-black | 3.70 | | Geuther |
| " | yellow | 3.88 | | Linck |
| Barium | solid | 3.78 | | Guntz |
| Bismuth | electrolytic | 9.747 | | Classen, 1890 |
| " | vacuo-distilled | 9.781 | 20 | Kahlbaum, 1902 |
| " | liquid | 10.00 | 271 | Vincentini-Omodei |
| " | solid | 9.67 | 271 | " |
| Boron | crystal | 2.535 | | Wigand |
| " | amorph. pure | 2.45 | | Moissan |
| Bromine | liquid | 3.12 | | Richards-Stull |
| " | solid | 4.2 | -273 | Computed† |
| Cadmium | wrought | 8.67 | | |
| " | vacuo-distilled | 8.648 | 20 | Kahlbaum, 1902 |
| " | solid | 8.37 | 318 | Vincentini-Omodei |
| " | liquid | 7.99 | 318 | " |
| Cæsium | solid | 1.873 | 20 | Richards-Brink |
| " | liquid | 1.836 | 27 | Eckardt, Graefe, 1900 |
| Calcium | " | 1.54 | | Brink |
| Carbon | diamond | 3.52 | | Wigand |
| " | graphite | 2.25 | | |
| Cerium | electrolytic | 6.79 | | Muthmann-Weiss |
| " | pure | 7.02 | | " |
| Chlorine | liquid | 1.507 | -33.6 | Drugman-Ramsay |
| " | solid | 2.2 | -273 | Computed† |
| Chromium | " | 6.52-6.73 | | |
| " | pure | 6.93 | 25 | Peffer, 1931 |
| Cobalt | " | 8.71 | 21 | Tilden, Ch. C., 1898 |
| Columbium | " | 8.4 | 15 | Muthmann-Weiss |
| Copper | cast | 8.30-8.95 | | |
| " | annealed | 8.89 | 20 | Dellinger, 1911 |
| " | hard drawn | 8.89 | 20 | " |
| " | vacuo-distilled | 8.9326 | 20 | Kahlbaum, 1902 |
| " | ditto-compressed | 8.9376 | 20 | " |
| " | liquid | 8.217 | | Roberts-Wrightson |
| Erbium | " | 4.77 | | St. Meyer, Z. Ph. Ch. 37 |
| Fluorine | liquid | 1.14 | -200 | Moissan-Dewar |
| " | solid | 1.5 | -273 | Computed† |
| Gallium | " | 5.93 | 23 | de Boisbaudran |
| Germanium | " | 5.46 | 20 | Winkler |
| Glucinum | " | 1.85 | | Humpidge |
| Gold | cast | 19.3 | | |
| " | vacuo-distilled | 18.88 | 20 | Kahlbaum, 1902 |
| " | ditto-compressed | 19.27 | 20 | " |
| Hafnium | solid | 13.3 | | |
| Helium | liquid | 0.15 | -269 | de Boer, 1930 |
| " | solid | 0.19 | -273 | Onnes, 1908 |
| " | " | 0.19 | -273 | Computed† |
| Hydrogen | liquid | 0.070 | -252 | Dewar, Ch. News, 1904 |
| " | solid | 0.763 | -260 | Dewar |
| Indium | " | 7.28 | | Richards |

* Where the temperature is not given, ordinary temperature is understood. † Herz, 1919.

DENSITY OF THE ELEMENTS, LIQUID OR SOLID

| Element | Physical State | g/cm ³ | °C* | Authority |
|--------------|------------------|-------------------|--------|-------------------------|
| Iridium | | 22.42 | 17 | Deville-Debray |
| Iodine | | 4.940 | 20 | Richards-Stull |
| " | liquid | 3.71 | 184 | Drugman, Ramsey |
| Iron | pure | 7.86 | | Bureau of Standards |
| " | gray cast | 7.03-7.13 | | |
| " | white cast | 7.58-7.73 | | |
| " | wrought | 7.80-7.90 | | |
| " | liquid | 6.88 | | Roberts-Austen |
| " | " | 6.91 | 1200 | Honda |
| Krypton | " | 2.16 | -146 | Ramsay-Travers |
| " | solid | 3.4 | -273 | Computed† |
| Lanthanum | | 6.15 | | Muthmann-Weiss |
| Lead | vacuo-distilled | 11.342 | 20 | Kahlbaum, 1902 |
| " | ditto-compressed | 11.347 | 20 | " |
| " | solid | 11.005 | 325 | Vincentini-Omodei |
| " | liquid | 10.597 | 400 | Day, Sosman, Hostetter, |
| " | " | 10.078 | 850 | 1914 |
| Lithium | | 0.534 | 20 | Richards-Brink, 1907 |
| Magnesium | | 1.741 | | Voigt |
| Manganese | | 7.3 | | Mean |
| Mercury | liquid | 13.596 | 0 | Thiesen, Scheel, Sell, |
| " | " | 13.546 | 20 | Heuse, 1912 |
| " | " | 13.690 | -38.8 | Vincentini-Omodei |
| " | solid | 14.193 | -38.8 | Mallet |
| " | " | 14.383 | -188 | Dewar, 1902 |
| Molybdenum | | 10.2 | | Davy, 1925 |
| Neodymium | | 7.00 | | Kremers, 1925 |
| Neon | | 1.204 | -245 | Onnes, Alii |
| Nickel | | 8.8 | | |
| Nitrogen | liquid | 0.810 | -195 | Baly-Donnan, 1902 |
| " | " | 0.854 | -205 | " |
| " | solid | 1.0265 | -252.5 | Dewar |
| " | " | 1.14 | -273 | Computed† |
| Osmium | | 22.5 | | Dewille-Debray |
| Oxygen | liquid | 1.132 | -183.6 | Drugman, Ramsey |
| " | solid | 1.426 | -252.5 | Dewar |
| " | " | 1.568 | -273 | Computed† |
| Palladium | | 11.5 | | |
| Phosphorus | white | 1.83 | | |
| " | red | 2.20 | | |
| " | metallic | 2.34 | 15 | Hittorf |
| " | black | 2.69 | | Bridgman, 1918 |
| Platinum | | 21.37 | 20 | Richards-Stull |
| " | black | 2.70 | | |
| Potassium | | 0.870 | 20 | Richards-Brink, 1907 |
| " | solid | 0.851 | 62.1 | Vincentini-Omodei |
| " | liquid | 0.830 | 62.1 | " |
| Praseodymium | | 6.6 | 25 | Wierda, Kremers, 1925 |
| Rhodium | | 12.44 | | Holborn Henning |
| Rubidium | | 1.532 | 20 | Richards-Brink, 1907 |
| Ruthenium | | 12.30 | 19 | Ruff, Vidic, 1925 |
| Samarium | | 7.7-7.8 | | Muthmann-Weiss |
| Selenium | | 4.82 | | Bradley, 1924 |
| Silicon | cryst. | 2.42 | 20 | Richards-Stull-Brink |
| " | amorph. | 2.35 | 15 | Vigorous |
| Silver | cast | 10.42-10.53 | | |
| " | vacuo-distilled | 10.492 | 20 | Kahlbaum, 1902 |
| " | "-compressed | 10.503 | 20 | " |
| " | liquid | 9.51 | | Wrightson |
| Sodium | | 0.9712 | 20 | Richards-Brink, 1907 |
| " | solid | 0.9519 | 97.6 | Vincentini-Omodei |
| " | liquid | 0.9287 | 97.6 | " |
| " | " | 1.0066 | -188 | Dewar |

* Where the temperature is not given, ordinary temperature is understood. † Herz, 1919.

TABLE 112 (concluded).—Density of the elements, liquid or solid

| Element | Physical state | g/cm ³ | °C* | Authority |
|-----------|------------------|-------------------|------|-------------------|
| Strontium | solid | 2.60 | | |
| Sulphur | " | 2.0-2.1 | | |
| " | liquid | 1.811 | 113 | Vincentini-Omodei |
| Tantalum | | 16.6 | | |
| Tellurium | crystallized | 6.25 | | |
| " | amorphous | 6.02 | 20 | Bjeljankin |
| Thallium | | 11.86 | | Stull |
| Thorium | | 11.00 | 17 | Nilson |
| Tin | white, cast | 7.29 | | Matthiessen |
| " | " wrought | 7.30 | | |
| " | " solid | 7.184 | | Vincentini-Omodei |
| " | liquid | 6.99 | 226 | " |
| " | gray | 5.8 | 226 | " |
| Titanium | | 4.5 | 18 | Mixer |
| Tungsten | | 18.6-19.1 | | |
| Uranium | | 18.7 | 13 | Zimmermann |
| Vanadium | | 5.6 | | |
| Xenon | liquid | 3.52 | 109 | Ramsay-Travers |
| Yttrium | | 4.57 | | Kremers, 1926 |
| Zinc | cast | 7.04-7.16 | | |
| " | solid | 4.32 | -273 | Herz, computed |
| " | vacuo-distilled | 6.92 | 20 | Kahlbaum, 1902 |
| " | ditto-compressed | 7.13 | 20 | " |
| " | liquid | 6.48 | | Roberts-Wrightson |
| Zirconium | | 6.53 | | De Boer, 1930 |

TABLE 113.—Density in grams per cubic centimeter and in pounds per cubic foot of different kinds of wood

Wood is to be seasoned and of average dryness. See also pages 132 to 135 and 163

| Wood | Grams per cubic centimeter | Pounds per cubic foot | Wood | Grams per cubic centimeter | Pounds per cubic foot |
|-----------------------|----------------------------|-----------------------|-----------------------|----------------------------|-----------------------|
| Alder..... | 0.42-0.68 | 26-42 | Greenheart..... | 0.93-1.04 | 58-65 |
| Apple..... | 0.66-0.84 | 41-52 | Hazel..... | 0.60-0.80 | 37-49 |
| Ash..... | 0.65-0.85 | 40-53 | Hickory..... | 0.60-0.93 | 37-58 |
| Balsa..... | < Cork | | Holly..... | 0.76 | 47 |
| Bamboo..... | 0.31-0.40 | 19-25 | Iron-bark..... | 1.03 | 64 |
| Basswood..... | | | Juniper..... | 0.56 | 35 |
| See Linden..... | | | Laburnum..... | 0.92 | 57 |
| Beech..... | 0.70-0.90 | 43-56 | Lancewood..... | 0.68-1.00 | 42-62 |
| Blue gum..... | 1.00 | 62 | Lignum vite..... | 1.17-1.33 | 73-83 |
| Birch..... | 0.51-0.77 | 32-48 | Linden or Lime-tree.. | 0.32-0.59 | 20-37 |
| Box..... | 0.95-1.16 | 59-72 | Locust..... | 0.67-0.71 | 42-44 |
| Bullet-tree..... | 1.05 | 65 | Logwood..... | 0.91 | 57 |
| Butternut..... | 0.38 | 24 | Mahogany, Honduras.. | 0.66 | 41 |
| Cedar..... | 0.49-0.57 | 30-35 | " Spanish..... | 0.85 | 53 |
| Cherry..... | 0.70-0.90 | 43-56 | Maple..... | 0.62-0.75 | 39-47 |
| Cork..... | 0.22-0.26 | 14-16 | Oak..... | 0.60-0.90 | 37-56 |
| Dogwood..... | 0.76 | 47 | Pear-tree..... | 0.61-0.73 | 38-45 |
| Ebony..... | 1.11-1.33 | 69-83 | Plum-tree..... | 0.66-0.78 | 41-49 |
| Elm..... | 0.54-0.60 | 34-37 | Poplar..... | 0.35-0.5 | 22-31 |
| Pine, Eastern White.. | 0.35-0.50 | 22-31 | Satinwood..... | 0.95 | 59 |
| " Larch..... | 0.50-0.56 | 31-35 | Sycamore..... | 0.40-0.60 | 24-37 |
| " Pitch..... | 0.83-0.85 | 52-53 | Teak, Indian..... | 0.66-0.88 | 41-55 |
| " Red..... | 0.48-0.70 | 30-44 | " African..... | 0.98 | 61 |
| " Scotch..... | 0.43-0.53 | 27-33 | Walnut..... | 0.64-0.70 | 40-43 |
| " Spruce..... | 0.48-0.70 | 30-44 | Water gum..... | 1.00 | 62 |
| " Yellow..... | 0.37-0.60 | 23-37 | Willow..... | 0.40-0.60 | 24-37 |

* Where the temperature is not given, ordinary atmospheric temperature is understood.

DENSITY IN GRAMS PER CUBIC CENTIMETER AND POUNDS PER CUBIC FOOT OF VARIOUS SOLIDS

N. B. The density of a specimen depends considerably on its state and previous treatment; especially is this the case with porous materials.

| Material. | Grams per cu. cm. | Pounds per cu. foot. | Material. | Grams per cu. cm. | Pounds per cu. foot. |
|----------------|-------------------|----------------------|-----------------|-------------------|----------------------|
| Agate | 2.5-2.7 | 156-168 | Gum arabic | 1.3-1.4 | 80-85 |
| Alabaster : | | | Gypsum | 2.31-2.33 | 144-145 |
| Carbonate | 2.69-2.78 | 168-173 | Hematite | 4.9-5.3 | 306-330 |
| Sulphate | 2.26-2.32 | 141-145 | Hornblende | 3.0 | 187 |
| Albite | 2.62-2.65 | 163-165 | Ice | 0.917 | 57.2 |
| Amber | 1.06-1.11 | 66-69 | Ilmenite | 4.5-5. | 280-310 |
| Amphiboles | 2.9-3.2 | 180-200 | Ivory | 1.83-1.92 | 114-120 |
| Anorthite | 2.74-2.76 | 171-172 | Labradorite | 2.7-2.72 | 168-170 |
| Anthracite | 1.4-1.8 | 87-112 | Lava : basaltic | 2.8-3.0 | 175-185 |
| Asbestos | 2.0-2.8 | 125-175 | trachytic | 2.0-2.7 | 125-168 |
| Asphalt | 1.1-1.5 | 69-94 | Leather : dry | 0.86 | 54 |
| Basalt | 2.4-3.1 | 150-190 | greased | 1.02 | 64 |
| Beeswax | 0.96-0.97 | 60-61 | Lime : mortar | 1.65-1.78 | 103-111 |
| Beryl | 2.69-2.7 | 168-168 | slaked | 1.3-1.4 | 81-87 |
| Biotite | 2.7-3.1 | 170-190 | Limestone | 2.68-2.76 | 167-171 |
| Bone | 1.7-2.0 | 106-125 | Litharge : | | |
| Brick | 1.4-2.2 | 87-137 | Artificial | 9.3-9.4 | 580-585 |
| Butter | 0.86-0.87 | 53-54 | Natural | 7.8-8.0 | 490-500 |
| Calamine | 4.1-4.5 | 255-280 | Magnetite | 4.9-5.2 | 306-324 |
| Caoutchouc | 0.92-0.99 | 57-62 | Malachite | 3.7-4.1 | 231-256 |
| Celluloid | 1.4 | 87 | Marble | 2.6-2.84 | 160-177 |
| Cement, set | 2.7-3.0 | 170-190 | Meerschäum | 0.99-1.28 | 62-80 |
| Chalk | 1.9-2.8 | 118-175 | Mica | 2.6-3.2 | 165-200 |
| Charcoal : oak | 0.57 | 35 | Muscovite | 2.76-3.00 | 172-225 |
| pine | 0.28-0.44 | 18-28 | Ochre | 3.5 | 218 |
| Chrome yellow | 6.00 | 374 | Oligoclase | 2.65-2.67 | 165-167 |
| Chromite | 4.32-4.57 | 270-285 | Olivine | 3.27-3.37 | 204-210 |
| Cinnabar | 8.12 | 507 | Opal | 2.2 | 137 |
| Clay | 1.8-2.6 | 122-162 | Orthoclase | 2.58-2.61 | 161-163 |
| Coal, soft | 1.2-1.5 | 75-94 | Paper | 0.7-1.15 | 44-72 |
| Cocoa butter | 0.89-0.91 | 56-57 | Paraffin | 0.87-0.91 | 54-57 |
| Coke | 1.0-1.7 | 62-105 | Peat | 0.84 | 52 |
| Copal | 1.04-1.14 | 65-71 | Pitch | 1.07 | 67 |
| Corundum | 3.9-4.0 | 245-250 | Porcelain | 2.3-2.5 | 143-156 |
| Diamond : | | | Porphyry | 2.6-2.9 | 162-181 |
| Anthracitic | 1.66 | 104 | Pyrite | 4.95-5.1 | 309-318 |
| Carbonado | 3.01-3.25 | 188-203 | Quartz | 2.65 | 165 |
| Diorite | 2.52 | 157 | Quartzite | 2.73 | 170 |
| Dolomite | 2.84 | 177 | Resin | 1.07 | 67 |
| Ebonite | 1.15 | 72 | Rock salt | 2.18 | 136 |
| Emery | 4.0 | 250 | Rutile | 4.2 | 260 |
| Epidote | 3.25-3.5 | 203-218 | Sandstone | 2.14-2.36 | 134-147 |
| Feldspar | 2.55-2.75 | 159-172 | Serpentine | 2.50-2.65 | 156-165 |
| Flint | 2.63 | 164 | Slag, furnace | 2.0-3.9 | 125-240 |
| Fluorite | 3.18 | 198 | Slate | 2.6-3.3 | 162-205 |
| Gamboge | 1.2 | 75 | Soapstone | 2.6-2.8 | 162-175 |
| Garnet | 3.15-4.3 | 197-268 | Starch | 1.53 | 95 |
| Gas carbon | 1.88 | 117 | Sugar | 1.61 | 100 |
| Gelatine | 1.27 | 180 | Talc | 2.7-2.8 | 168-174 |
| Glass : common | 2.4-2.8 | 150-175 | Tallow | 0.91-0.97 | 57-60 |
| flint | 2.9-5.9 | 180-370 | Topaz | 3.5-3.6 | 219-223 |
| Glue | 1.27 | 80 | Tourmaline | 3.0-3.2 | 190-200 |
| Granite | 2.64-2.76 | 165-172 | Zircon | 4.68-4.70 | 292-293 |
| Graphite | 2.30-2.72 | 144-170 | | | |

TABLE 115.—Density in Grams per Cubic Centimeter and Pounds per Cubic Foot of Various Alloys

| Alloy | Grams per cubic centimeter | Pounds per cubic foot |
|--|----------------------------------|-----------------------------|
| Brasses: Yellow, 70Cu + 30Zn, cast | 8.44 | 527 |
| “ “ “ rolled | 8.56 | 534 |
| “ “ “ drawn | 8.70 | 542 |
| “ Red, 90Cu + 10Zn | 8.60 | 536 |
| “ White, 50Cu + 50Zn | 8.20 | 511 |
| Bronzes: 90Cu + 10Sn | 8.78 | 548 |
| “ 85Cu + 15Sn | 8.89 | 555 |
| “ 80Cu + 20Sn | 8.74 | 545 |
| “ 75Cu + 25Sn | 8.83 | 551 |
| German Silver: Chinese, 26.3Cu + 36.6Zn + 36.8Ni | 8.30 | 518 |
| “ “ Berlin (1) 52Cu + 26Zn + 22Ni | 8.45 | 527 |
| “ “ (2) 59Cu + 30Zn + 11Ni | 8.34 | 520 |
| “ “ (3) 63Cu + 30Zn + 6Ni | 8.30 | 518 |
| “ “ Nickel | 8.77 | 547 |
| Lead and Tin: 87.5Pb + 12.5Sn | 10.60 | 661 |
| “ “ 84Pb + 16Sn | 10.33 | 644 |
| “ “ 77.8Pb + 22.2Sn | 10.05 | 627 |
| “ “ 63.7Pb + 36.3Sn | 9.43 | 588 |
| “ “ 46.7Pb + 53.3Sn | 8.73 | 545 |
| “ “ 30.5Pb + 69.5Sn | 8.24 | 514 |
| Bismuth, Lead, and Cadmium: 53Bi + 40Pb + 7Cd | 10.56 | 659 |
| Wood's Metal: 50Bi + 25Pb + 12.5Cd + 12.5Sn | 9.70 | 605 |
| Cadmium and Tin: 32Cd + 68Sn | 7.70 | 480 |
| Gold and Copper: 98Au + 2Cu | 18.84 | 1176 |
| “ “ 96Au + 4Cu | 18.36 | 1145 |
| “ “ 94Au + 6Cu | 17.95 | 1120 |
| “ “ 90Au + 10Cu | 17.16 | 1071 |
| “ “ 86Au + 14Cu | 16.47 | 1027 |
| Aluminum and Copper: 10Al + 90Cu | 7.69 | 480 |
| “ “ 5Al + 95Cu | 8.37 | 522 |
| “ “ 3Al + 97Cu | 8.69 | 542 |
| Aluminum and Zinc: 91Al + 9Zn | 2.80 | 175 |
| Platinum and Iridium: 90Pt + 10Ir | 21.62 | 1348 |
| “ “ 85Pt + 15Ir | 21.62 | 1348 |
| “ “ 66.67Pt + 33.33Ir | 21.87 | 1364 |
| Carboloy | 14.3 | 895 |
| Constantan: 60Cu + 40Ni | 8.88 | 554 |
| Magnalium: 70Al + 30Mg | 2.0 | 125 |
| Manganin: 84Cu + 12Mn + 4Ni | 8.5 | 530 |
| Monel metal | 8.87 | 554 |
| Platinoid: German silver + little Tungsten | 9.0 | 560 |
| Stellite: Co 59.5; Mo 22.5; Cr 10.8; Fe 3.1; Mn 2.0; C 0.9; Si 0.8 | 8.3 | 518 |

TABLE 116.—Density (g/cm³) of some foreign woods on the American market
(See also pages 132-135 and 161.)

| | | | | | |
|----------------------|-----------|------------|--------------------|-----------|---------|
| Almon | 0.464 | Gardner | Olive | 0.94 | Boulger |
| Bullet-wood, Guiana | 1.03-1.23 | Boulger | Orange Wood | .70 | “ |
| Boxwood, West Indian | .83-.88 | “ | Padouk | .89-1.29 | “ |
| Balsa | .11 | Carpenter | Prima Vera | .58 | Howard |
| Carreto | .84 | U.S.F.P.L. | Purple-heart | .72-.97 | Boulger |
| Cedar, Spanish | .38 | “ | Quebracho | 1.25 | “ |
| Cocobola | 1.20 | Boulger | Rosewood, Brazil | .77-.84 | “ |
| Cocus | 1.25 | Stone | Rosewood, Honduras | 1.09-1.23 | “ |
| Fustic | .68 | Boulger | Sabicu | .90-.96 | “ |
| Koa | .83 | Howard | Snakewood | 1.05-1.33 | “ |
| Lauan, Red | .41 | Gardner | Tamarind | 1.32 | “ |
| Mahogany, African | .55 | Boulger | Tanguile | .47-.51 | Gardner |
| Mahogany, E. Indian | .38 | “ | Wallaba | .93-.94 | Boulger |
| Mora | 1.07-1.09 | “ | Zebra Wood | 1.03 | “ |
| Oak, English | .60-.78 | “ | | | |

Table prepared by W. M. N. Watkins, U. S. National Museum

DENSITY OF VARIOUS NATURAL AND ARTIFICIAL MINERALS

| Name and formula | | Density in grams per cm ³ | Sp. vol. in cm ³ per gram | Reference |
|---|-------|--|--|---------------------|
| <i>Oxides</i> | | C | | |
| Corundum Al ₂ O ₃ art. | (0°) | 3.980 | .2513 | 11, 14 ^a |
| Lime CaO art. | (25°) | 3.306 | .3025 | 2 |
| Magnesia MgO art. | (25°) | 3.003 | .2775 | 5, 13 ^a |
| Ferrous oxide FeO art. | (20°) | 5.99 | .1669 | 15 ^a |
| Hematite Fe ₂ O ₃ | (20°) | 5.25 | .1905 | 14 ^a |
| Magnetite Fe ₃ O ₄ | (0°) | 5.172 | .1933 | 11 |
| Quartz SiO ₂ nat. | (20°) | 2.649 | .3775 | 22 |
| " art. | (25°) | 2.648 | .3770 | 22 |
| Cristobalite SiO ₂ art. | (25°) | 2.325 | .4301 | 22 |
| Vitreous silica | (0°) | 2.203 | .4539 | 22 |
| Rutile TiO ₂ | (0°) | 4.250 | .2353 | 11 |
| Ilmenite (FeTi)O ₃ | (0°) | 5.088 | .1905 | 11 |
| <i>Silicates</i> | | | | |
| Sillimanite Al ₂ O ₃ .SiO ₂ | (25°) | 3.247 | .3080 | 16 |
| Mullite 3Al ₂ O ₃ .2SiO ₂ art. | (25°) | 3.156 | .3160 | 16 |
| Albite NaAlSi ₃ O ₈ art. | (25°) | 2.597 | .3851 | 1 |
| Apothite CaAl ₂ Si ₂ O ₇ art. | (25°) | 2.757 | .3627 | 1 |
| Nephelite NaAlSi ₃ O ₈ art. | (21°) | 2.619 | .3818 | 6 |
| Labradorite Ab ₅₄ An ₄₆ | (26°) | 2.695 | .3711 | 12 |
| Oligoclase Ab ₇₅ An ₂₅ | (25°) | 2.638 | .3791 | 12 |
| Orthoclase KAlSi ₃ O ₈ ^b | (15°) | 2.554 | .3915 | 20 |
| adularia | (15°) | 2.566 | .3897 | 20 |
| Microcline | (25°) | 2.557 | .3911 | 12 |
| <i>Calcium Orthosilicates</i> | | | | |
| α - Ca ₂ SiO ₄ art. | (25°) | 3.26 | .307 | 2 |
| β - Ca ₂ SiO ₄ art. | (25°) | 3.27 | .306 | 2 |
| γ - Ca ₂ SiO ₄ art. | (25°) | 2.905 | .3373 | 2 |
| <i>Calcium Metasilicates</i> | | | | |
| α - CaSiO ₃ (ψ - Wollastonite) art. | (25°) | 2.904 | .3444 | 2 |
| β - CaSiO ₃ (Wollastonite) art. | (25°) | 2.906 | .3441 | 2 |
| Diopside CaSiO ₃ .MgSiO ₃ | (28°) | 3.257 | .3070 | 12 |
| art. | (25°) | 3.265 | .3063 | 4 |
| Enstatite MgSiO ₃ art. | (25°) | 3.166 | .3159 | 3 |
| (MgSiO ₃) ₈₈ (FeSiO ₃) ₁₂ | (25°) | 3.254 | .3073 | 12 |
| Hypersthene (MgSiO ₃) ₇₀ (FeSiO ₃) ₃₀ | (20°) | 3.415 | .2928 | 12 |
| Forsterite Mg ₂ SiO ₄ | (20°) | 3.223 | .3103 | 17 |
| Fayalite Fe ₂ SiO ₄ art. | (15°) | 4.28 | .234 | 10 |
| Garnet—grossularite | (31°) | 3.544 | .2822 | 18 |
| " almandite | (31°) | 4.160 | .2404 | 18 |
| Jadeite | (31°) | 3.328 | .3005 | 18 |
| <i>Miscellaneous Substances</i> | | | | |
| Borax, Anhydrous, Na ₂ B ₄ O ₇ art. | | 2.27 | .440 | 1 |
| CaCO ₃ ; aragonite | (0°) | 2.932 | .3411 | 11 |
| CaCO ₃ ; calcite | (20°) | 2.7102 | .3688 | 21 |
| CaF ₂ ; fluorite | (10°) | 3.180 | .3145 | 8 |
| Diamond | (25°) | 3.516 | .2844 | 12 |
| NaCl; rock salt | (20°) | 2.1632 | .4623 | 21 |
| Na ₂ SO ₄ V; thenardite art. | (25°) | 2.664 | .3754 | 19 |
| Na ₂ SO ₄ III art. | (25°) | 2.697 | .3708 | 19 |
| KCl; fine powder art. | (30°) | 1.984 | .5040 | 7 |
| Pyrite FeS ₂ | (25°) | 5.012 | .1995 | 9 |
| Marcasite FeS ₂ | (25°) | 4.873 | .2052 | 9 |

(1) Day and Allen, 1905. (2) Day and Shepherd, 1906. (3) Allen, Wright and Clement, 1906. (4) Allen and White, 1909. (5) Larsen, 1909. (6) Bowen, 1912. (7) Johnston and Adams, 1911. (8) Merwin, 1911. (9) Allen and Crenshaw, 1911. (10) Busz and Rüsberg, 1913. (11) Madelung and Fuchs, 1921. (12) Adams and Williamson, 1923. (13) Rinne, 1923. (14) Pauling and Hendricks, 1925. (15) Wyckoff and Crittenden, 1925. (16) Greig (unpublished). (17) Auroisseau and Merwin, 1928. (18) Adams and Gibson, 1929. (19) Kracek and Gibson, 1929. (20) Bjeljankin, 1927. (21) DeFoe and Compton, 1925. (22) Sosman, 1927.

^a X-ray diffraction data.

^b Calculated from density and composition of adularia.

DENSITY OF LIQUIDS

Density or mass in grams per cubic centimeter and in pounds per cubic foot of various liquids.

| Liquid. | Grams per cubic centimeter. | Pounds per cubic foot. | Temp. C. |
|-------------------------------------|--------------------------------|---------------------------|----------|
| Acetone | 0.792 | 49.4 | 20° |
| Alcohol, ethyl | 0.807 | 50.4 | 0 |
| " methyl | 0.810 | 50.5 | 0 |
| Aniline | 1.035 | 64.5 | 0 |
| Benzene | 0.899 | 56.1 | 0 |
| Bromine | 3.187 | 199.0 | 0 |
| Carbolic acid (crude) | 0.950-0.965 | 59.2-60.2 | 15 |
| Carbon disulphide | 1.293 | 80.6 | 0 |
| Chloroform | 1.489 | 93.0 | 20 |
| Cocoa-butter | 0.857 | 53.5 | 100 |
| Ether | 0.736 | 45.9 | 0 |
| Gasoline | 0.66-0.69 | 41.0-43.0 | - |
| Glycerine | 1.260 | 78.6 | 0 |
| Japan wax | 0.875 | 54.6 | 100 |
| Milk | 1.028-1.035 | 64.2-64.6 | - |
| Naphtha (wood) | 0.848-0.810 | 52.9-50.5 | 0 |
| Naphtha (petroleum ether) | 0.665 | 41.5 | 15 |
| Oils: Amber | 0.800 | 49.9 | 15 |
| Anise-seed | 0.996 | 62.1 | 16 |
| Camphor | 0.910 | 56.8 | - |
| Castor | 0.969 | 60.5 | 15 |
| Clove | 1.04-1.06 | 65.-66. | 25 |
| Cocoanut | 0.925 | 57.7 | 15 |
| Cotton Seed | 0.926 | 57.8 | 16 |
| Creosote | 1.040-1.100 | 64.9-68.6 | 15 |
| Lard | 0.920 | 57.4 | 15 |
| Lavender | 0.877 | 54.7 | 16 |
| Lemon | 0.844 | 52.7 | 16 |
| Linseed (boiled) | 0.942 | 58.8 | 15 |
| Neat's foot | 0.913-0.917 | 57.0-57.2 | - |
| Olive | 0.918 | 57.3 | 15 |
| Palm | 0.905 | 56.5 | 15 |
| Pentane | 0.650 | 40.6 | 0 |
| " | 0.623 | 38.9 | 25 |
| Peppermint | 0.90-0.92 | 56-57 | 25 |
| Petroleum | 0.878 | 54.8 | 0 |
| " (light) | 0.795-0.805 | 49.6-50.2 | 15 |
| Pine | 0.850-0.860 | 53.0-54.0 | 15 |
| Poppy | 0.924 | 57.7 | - |
| Rapeseed (crude) | 0.915 | 57.1 | 15 |
| " (refined) | 0.913 | 57.0 | 15 |
| Resin | 0.955 | 59.6 | 15 |
| Sperm | 0.88 | 55. | 25 |
| Soya-bean | 0.919 | 57.3 | 30 |
| " | 0.906 | 56.5 | 90 |
| Train or Whale | 0.918-0.925 | 57.3-57.7 | 15 |
| Turpentine | 0.873 | 54.2 | 16 |
| Valerian | 0.965 | 60.2 | 16 |
| Wintergreen | 1.18 | 74. | 25 |
| Pyroligneous acid | 0.800 | 49.9 | 0 |
| Water | 1.000 | 62.4 | 4 |

DENSITY OF PURE WATER FREE FROM AIR. 0° TO 41° C

[Under standard pressure (76 cm), at every tenth part of a degree of the international hydrogen scale from 0° to 41° C, in grams per milliliter ¹]

| De- grees Cen- ti- grade. | Tenths of Degrees. | | | | | | | | | | Mean Differ- ences. |
|---------------------------------------|--------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------------------------|
| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | |
| 0 | 0.999 8681 | 8747 | 8812 | 8875 | 8936 | 8996 | 9053 | 9109 | 9163 | 9216 | + 59 |
| 1 | 9267 | 9315 | 9363 | 9408 | 9452 | 9494 | 9534 | 9573 | 9610 | 9645 | + 41 |
| 2 | 9679 | 9711 | 9741 | 9769 | 9796 | 9821 | 9844 | 9866 | 9887 | 9905 | + 24 |
| 3 | 9922 | 9937 | 9951 | 9962 | 9973 | 9981 | 9988 | 9994 | 9998 | *0000 | + 8 |
| 4 | 1.000 0000 | *9999 | *9996 | *9992 | *9986 | *9979 | *9970 | *9960 | *9947 | *9934 | — 8 |
| 5 | 0.999 9919 | 9902 | 9884 | 9864 | 9842 | 9819 | 9795 | 9769 | 9742 | 9713 | — 24 |
| 6 | 9682 | 9650 | 9617 | 9582 | 9545 | 9507 | 9468 | 9427 | 9385 | 9341 | — 39 |
| 7 | 9296 | 9249 | 9201 | 9151 | 9100 | 9048 | 8994 | 8938 | 8881 | 8823 | — 53 |
| 8 | 8764 | 8703 | 8641 | 8577 | 8512 | 8445 | 8377 | 8308 | 8237 | 8165 | — 67 |
| 9 | 8091 | 8017 | 7940 | 7863 | 7784 | 7704 | 7622 | 7539 | 7455 | 7369 | — 81 |
| 10 | 7282 | 7194 | 7105 | 7014 | 6921 | 6826 | 6729 | 6632 | 6533 | 6432 | — 95 |
| 11 | 6331 | 6228 | 6124 | 6020 | 5913 | 5805 | 5696 | 5586 | 5474 | 5362 | —108 |
| 12 | 5248 | 5132 | 5016 | 4898 | 4780 | 4660 | 4538 | 4415 | 4291 | 4166 | —121 |
| 13 | 4040 | 3912 | 3784 | 3654 | 3523 | 3391 | 3257 | 3122 | 2986 | 2850 | —133 |
| 14 | 2712 | 2572 | 2431 | 2289 | 2147 | 2003 | 1858 | 1711 | 1564 | 1416 | —145 |
| 15 | 1266 | 1114 | 0962 | 0809 | 0655 | 0499 | 0343 | 0185 | 0026 | *9865 | —156 |
| 16 | 0.998 9705 | 9542 | 9378 | 9214 | 9048 | 8881 | 8713 | 8544 | 8373 | 8202 | —168 |
| 17 | 8029 | 7856 | 7681 | 7505 | 7328 | 7150 | 6971 | 6791 | 6610 | 6427 | —178 |
| 18 | 6244 | 6058 | 5873 | 5686 | 5498 | 5309 | 5119 | 4927 | 4735 | 4541 | —190 |
| 19 | 4347 | 4152 | 3955 | 3757 | 3558 | 3358 | 3158 | 2955 | 2752 | 2549 | —200 |
| 20 | 3343 | 2137 | 1930 | 1722 | 1511 | 1301 | 1090 | 0878 | 0663 | 0449 | —211 |
| 21 | 0233 | 0016 | *9799 | *9580 | *9359 | *9139 | *8917 | *8694 | *8470 | *8245 | —221 |
| 22 | 0.997 8019 | 7792 | 7564 | 7335 | 7104 | 6873 | 6641 | 6408 | 6173 | 5938 | —232 |
| 23 | 5702 | 5466 | 5227 | 4988 | 4747 | 4506 | 4264 | 4021 | 3777 | 3531 | —242 |
| 24 | 3286 | 3039 | 2790 | 2541 | 2291 | 2040 | 1788 | 1535 | 1280 | 1026 | —252 |
| 25 | 0770 | 0513 | 0255 | *9997 | *9736 | *9476 | *9214 | *8951 | *8688 | *8423 | —261 |
| 26 | 0.996 8158 | 7892 | 7624 | 7356 | 7087 | 6817 | 6545 | 6273 | 6000 | 5726 | —271 |
| 27 | 5451 | 5176 | 4898 | 4620 | 4342 | 4062 | 3782 | 3500 | 3218 | 2935 | —280 |
| 28 | 2652 | 2366 | 2080 | 1793 | 1505 | 1217 | 0928 | 0637 | 0346 | 0053 | —289 |
| 29 | 0.995 9761 | 9466 | 9171 | 8876 | 8579 | 8282 | 7983 | 7684 | 7383 | 7083 | —298 |
| 30 | 6780 | 6478 | 6174 | 5869 | 5564 | 5258 | 4950 | 4642 | 4334 | 4024 | —307 |
| 31 | 3714 | 3401 | 3089 | 2776 | 2462 | 2147 | 1832 | 1515 | 1198 | 0880 | —315 |
| 32 | 0561 | 0241 | *9920 | *9599 | *9276 | *8954 | *8630 | *8304 | *7979 | *7653 | —324 |
| 33 | 0.994 7325 | 6997 | 6668 | 6338 | 6007 | 5676 | 5345 | 5011 | 4678 | 4343 | —332 |
| 34 | 4007 | 3671 | 3335 | 2997 | 2659 | 2318 | 1978 | 1638 | 1296 | 0953 | —340 |
| 35 | 0610 | 0267 | *9922 | *9576 | *9230 | *8883 | *8534 | *8186 | *7837 | *7486 | —347 |
| 36 | 0.993 7136 | 6784 | 6432 | 6078 | 5725 | 5369 | 5014 | 4658 | 4301 | 3943 | —355 |
| 37 | 3585 | 3226 | 2866 | 2505 | 2144 | 1782 | 1419 | 1055 | 0691 | 0326 | —362 |
| 38 | 0.992 9960 | 9593 | 9227 | 8859 | 8490 | 8120 | 7751 | 7380 | 7008 | 6636 | —370 |
| 39 | 6263 | 5890 | 5516 | 5140 | 4765 | 4389 | 4011 | 3634 | 3255 | 2876 | —377 |
| 40 | 2497 | 2116 | 1734 | 1352 | 0971 | 0587 | 0203 | *9818 | *9433 | *9047 | —384 |
| 41 | 0.991 8661 | | | | | | | | | | |

¹ According to P. Chappuis, Bureau international des Poids et Mesures, Travaux et Mémoires, 13; 1907.

**VOLUME IN CUBIC CENTIMETERS AT VARIOUS TEMPERATURES OF A
CUBIC CENTIMETER OF WATER FREE FROM AIR AT THE
TEMPERATURE OF MAXIMUM DENSITY. 0° TO 36° C**

Hydrogen Thermometer Scale

| Temp. C. | .0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 |
|-------------|----------|------|------|------|------|------|------|------|------|------|
| 0 | 1.000132 | 125 | 118 | 112 | 106 | 100 | 095 | 089 | 084 | 079 |
| 1 | 073 | 069 | 064 | 059 | 055 | 051 | 047 | 043 | 039 | 035 |
| 2 | 032 | 029 | 026 | 023 | 020 | 018 | 016 | 013 | 011 | 009 |
| 3 | 008 | 006 | 005 | 004 | 003 | 002 | 001 | 001 | 000 | 000 |
| 4 | 000 | 000 | 000 | 001 | 001 | 002 | 003 | 004 | 005 | 007 |
| 5 | 008 | 010 | 012 | 014 | 016 | 018 | 021 | 023 | 026 | 029 |
| 6 | 032 | 035 | 039 | 042 | 046 | 050 | 054 | 058 | 062 | 066 |
| 7 | 070 | 075 | 080 | 085 | 090 | 095 | 101 | 106 | 112 | 118 |
| 8 | 124 | 130 | 137 | 142 | 149 | 156 | 162 | 169 | 176 | 184 |
| 9 | 191 | 198 | 206 | 214 | 222 | 230 | 238 | 246 | 254 | 263 |
| 10 | 272 | 281 | 290 | 299 | 308 | 317 | 327 | 337 | 347 | 357 |
| 11 | 367 | 377 | 388 | 398 | 409 | 420 | 430 | 441 | 453 | 464 |
| 12 | 476 | 487 | 499 | 511 | 522 | 534 | 547 | 559 | 571 | 584 |
| 13 | 596 | 609 | 623 | 636 | 649 | 661 | 675 | 688 | 702 | 715 |
| 14 | 729 | 743 | 757 | 772 | 786 | 800 | 815 | 830 | 844 | 859 |
| 15 | 873 | 890 | 905 | 920 | 935 | 951 | 967 | 983 | 998 | 015* |
| 16 | 1.001031 | 047 | 063 | 080 | 097 | 113 | 130 | 147 | 164 | 182 |
| 17 | 198 | 216 | 233 | 252 | 269 | 287 | 305 | 323 | 341 | 358 |
| 18 | 378 | 396 | 415 | 433 | 452 | 471 | 490 | 510 | 529 | 548 |
| 19 | 568 | 588 | 606 | 626 | 646 | 667 | 687 | 707 | 728 | 748 |
| 20 | 769 | 790 | 811 | 832 | 853 | 874 | 895 | 916 | 938 | 960 |
| 21 | 981 | 002* | 024* | 046* | 068* | 091* | 113* | 135* | 158* | 181* |
| 22 | 1.002203 | 226 | 249 | 271 | 295 | 319 | 342 | 364 | 389 | 412 |
| 23 | 436 | 459 | 483 | 507 | 532 | 556 | 581 | 605 | 629 | 654 |
| 24 | 679 | 704 | 729 | 754 | 779 | 804 | 829 | 854 | 879 | 905 |
| 25 | 932 | 958 | 983 | 010* | 036* | 061* | 088* | 115* | 141* | 168* |
| 26 | 1.003195 | 221 | 248 | 275 | 302 | 330 | 357 | 384 | 412 | 439 |
| 27 | 467 | 495 | 523 | 550 | 579 | 607 | 635 | 663 | 692 | 720 |
| 28 | 749 | 776 | 806 | 836 | 865 | 893 | 922 | 951 | 981 | 011* |
| 29 | 1.004041 | 069 | 100 | 129 | 160 | 189 | 220 | 250 | 280 | 310 |
| 30 | 341 | 371 | 403 | 432 | 464 | 494 | 526 | 557 | 588 | 619 |
| 31 | 651 | 682 | 713 | 744 | 777 | 808 | 840 | 872 | 904 | 936 |
| 32 | 968 | 001* | 033* | 066* | 098* | 132* | 163* | 197* | 229* | 263* |
| 33 | 1.005296 | 328 | 361 | 395 | 427 | 461 | 496 | 530 | 562 | 597 |
| 34 | 631 | 665 | 698 | 732 | 768 | 802 | 836 | 871 | 904 | 940 |
| 35 | 975 | 009* | 044* | 078* | 115* | 150* | 185* | 219* | 255* | 290* |

Reciprocals of the preceding table.

Influence of Pressure *

| kg/cm ² | 0° C | 20° C | 40° C | kg/cm ² | 20° C | 40° C |
|--------------------|--------|--------|--------|--------------------|--------|--------|
| 1 | 1.0000 | 1.0016 | 1.0076 | 7,000 | 0.8404 | 0.8485 |
| 500 | .9771 | .9808 | .9873 | 8,000 | .8275 | .8360 |
| 1,000 | .9578 | .9630 | .9700 | 9,000 | .8160 | .8240 |
| 2,000 | .9260 | .9327 | .9403 | 10,000 | — | .8140 |
| 3,000 | .9015 | .9087 | .9164 | 11,000 | — | .8050 |
| 5,000 | .8632 | .8702 | .8778 | 12,000 | — | .7966 |
| 6,000 | .8480 | .8545 | .8623 | 12,500 | — | .7922 |

* Williamson, Change of Physical Properties with Pressure, J. Frank. Inst. 193, p. 491, 1922.

DENSITY AND VOLUME OF WATER
-10° TO +250° C

The mass of one cubic centimeter at 4° C is taken as unity.

| Temp. C. | Density. | Volume. | Temp. C. | Density. | Volume. |
|-------------|----------|---------|-------------|----------|---------|
| -10° | 0.99815 | 1.00186 | +35° | 0.99406 | 1.00598 |
| -9 | 843 | 157 | 36 | 371 | 633 |
| -8 | 869 | 131 | 37 | 336 | 669 |
| -7 | 892 | 108 | 38 | 300 | 706 |
| -6 | 912 | 088 | 39 | 263 | 743 |
| 5 | 0.99930 | 1.00070 | 40 | 0.99225 | 1.00782 |
| -4 | 945 | 055 | 41 | 187 | 821 |
| -3 | 958 | 042 | 42 | 147 | 861 |
| -2 | 970 | 031 | 43 | 107 | 901 |
| -1 | 979 | 021 | 44 | 066 | 943 |
| +0 | 0.99987 | 1.00013 | 45 | 0.99025 | 1.00985 |
| 1 | 993 | 007 | 46 | 0.98982 | 1.01028 |
| 2 | 997 | 003 | 47 | 940 | 072 |
| 3 | 999 | 001 | 48 | 896 | 116 |
| 4 | 1.00000 | 1.00000 | 49 | 852 | 162 |
| 5 | 0.99999 | 1.00001 | 50 | 0.98807 | 1.01207 |
| 6 | 997 | 003 | 51 | 762 | 254 |
| 7 | 993 | 007 | 52 | 715 | 301 |
| 8 | 988 | 012 | 53 | 669 | 349 |
| 9 | 981 | 019 | 54 | 621 | 398 |
| 10 | 0.99973 | 1.00027 | 55 | 0.98573 | 1.01448 |
| 11 | 963 | 037 | 60 | 324 | 795 |
| 12 | 952 | 048 | 65 | 059 | 979 |
| 13 | 940 | 060 | 70 | 0.97781 | 1.02270 |
| 14 | 927 | 073 | 75 | 489 | 576 |
| 15 | 0.99913 | 1.00087 | 80 | 0.97183 | 1.02899 |
| 16 | 897 | 103 | 85 | 0.96865 | 1.03237 |
| 17 | 880 | 120 | 90 | 534 | 590 |
| 18 | 862 | 138 | 95 | 192 | 959 |
| 19 | 843 | 157 | 100 | 0.95838 | 1.04343 |
| 20 | 0.99823 | 1.00177 | 110 | 0.9510 | 1.0515 |
| 21 | 802 | 198 | 120 | .9434 | 1.0601 |
| 22 | 780 | 220 | 130 | .9352 | 1.0693 |
| 23 | 757 | 244 | 140 | .9264 | 1.0794 |
| 24 | 733 | 268 | 150 | .9173 | 1.0902 |
| 25 | 0.99708 | 1.00293 | 160 | 0.9075 | 1.1019 |
| 26 | 682 | 320 | 170 | .8973 | 1.1145 |
| 27 | 655 | 347 | 180 | .8866 | 1.1279 |
| 28 | 627 | 375 | 190 | .8750 | 1.1429 |
| 29 | 598 | 404 | 200 | .8628 | 1.1590 |
| 30 | 0.99568 | 1.00434 | 210 | 0.850 | 1.177 |
| 31 | 537 | 465 | 220 | .837 | 1.195 |
| 32 | 506 | 497 | 230 | .823 | 1.215 |
| 33 | 473 | 530 | 240 | .809 | 1.236 |
| 34 | 440 | 563 | 250 | .794 | 1.259 |

From -10° to 0° the values are due to means from Pierre, Weidner, and Rosetti; from 0° to 41°, to Chappuis, 42° to 100°, to Thiesen; 110° to 250°, to means from the works of Ramsey, Young, Waterston, and Hirn.

SMITHSONIAN TABLES.

DENSITY AND VOLUME OF MERCURY

- 10° to + 360°C

Density or mass in grams per cubic centimeter, and the volume in cubic centimeters of one gram of mercury.

| Temp. C. | Mass in grams per cu. cm. | Volume of 1 gram in cu. cms. | Temp. C. | Mass in grams per cu. cm. | Volume of 1 gram in cu. cms. |
|----------|---------------------------------|------------------------------------|----------|---------------------------------|------------------------------------|
| -10° | 13.6198 | 0.0734225 | 30° | 13.5213 | 0.0739572 |
| -9 | 6173 | 4358 | 31 | 5189 | 9705 |
| -8 | 6148 | 4402 | 32 | 5164 | 9839 |
| -7 | 6124 | 4626 | 33 | 5140 | 9973 |
| -6 | 6099 | 4759 | 34 | 5116 | 40107 |
| -5 | 13.6074 | 0.0734893 | 35 | 13.5091 | 0.0740241 |
| -4 | 6050 | 5026 | 36 | 5066 | 0374 |
| -3 | 6025 | 5160 | 37 | 5042 | 0508 |
| -2 | 6000 | 5293 | 38 | 5018 | 0642 |
| -1 | 5976 | 5427 | 39 | 4994 | 0776 |
| -0 | 13.5951 | 0.0735560 | 40 | 13.4969 | 0.0740910 |
| 1 | 5926 | 5694 | 50 | 4725 | 2250 |
| 2 | 5901 | 5828 | 60 | 4482 | 3592 |
| 3 | 5877 | 5961 | 70 | 4240 | 4936 |
| 4 | 5852 | 6095 | 80 | 3998 | 6282 |
| 5 | 13.5827 | 0.0736228 | 90 | 13.3723 | 0.0747631 |
| 6 | 5803 | 6362 | 100 | 3515 | 8981 |
| 7 | 5778 | 6496 | 110 | 3279 | 50305 |
| 8 | 5754 | 6629 | 120 | 3040 | 1653 |
| 9 | 5729 | 6763 | 130 | 2801 | 3002 |
| 10 | 13.5704 | 0.0736893 | 140 | 13.2563 | 0.075454 |
| 11 | 5680 | 7030 | 150 | 2326 | 5708 |
| 12 | 5655 | 7164 | 160 | 2090 | 7064 |
| 13 | 5630 | 7298 | 170 | 1853 | 8422 |
| 14 | 5606 | 7431 | 180 | 1617 | 9784 |
| 15 | 13.5581 | 0.0737565 | 190 | 13.1381 | 0.0761149 |
| 16 | 5557 | 7699 | 200 | 1145 | 2516 |
| 17 | 5532 | 7832 | 210 | 0910 | 3886 |
| 18 | 5507 | 7966 | 220 | 0677 | 5260 |
| 19 | 5483 | 8100 | 230 | 0440 | 6637 |
| 20 | 13.5458 | 0.0738233 | 240 | 13.0206 | 0.0768017 |
| 21 | 5434 | 8367 | 250 | 12.9972 | 9402 |
| 22 | 5409 | 8501 | 260 | 9738 | 7090 |
| 23 | 5385 | 8635 | 270 | 9504 | 2182 |
| 24 | 5360 | 8768 | 280 | 9270 | 3579 |
| 25 | 13.5336 | 0.0738902 | 290 | 12.9036 | 0.0774979 |
| 26 | 5311 | 9036 | 300 | 8803 | 6385 |
| 27 | 5287 | 9170 | 310 | 8569 | 7795 |
| 28 | 5262 | 9304 | 320 | 8336 | 9210 |
| 29 | 5238 | 9437 | 330 | 8102 | 80630 |
| 30 | 13.5213 | 0.0739571 | 340 | 12.7869 | 0.0782054 |
| | | | 350 | 7635 | 3485 |
| | | | 360 | 7402 | 4921 |

Based upon Thiesen und Scheel, Tätigkeitber. Phys.-Techn. Reichsanstalt, 1897-1898; Chappuis, Trav. Bur. Int. 13, 1903. Thiesen, Scheel, Sell: Wiss. Abh. Phys.-Techn. Reichsanstalt 2, p. 184, 1895, and 1 liter = 1.000027 cu. dm.

SMITHSONIAN TABLES.

DENSITY OF AQUEOUS SOLUTIONS *

The following table gives the density of solutions of various salts in water. The numbers give the weight in grams per cubic centimeter. For brevity the substance is indicated by formula only.

| Substance. | Weight of the dissolved substance in 100 parts by weight of the solution. | | | | | | | | | Temp. C. | Authority. |
|---------------------------------------|---|-------|-------|-------|-------|-------|-------|-------|-------|----------|--------------|
| | 5 | 10 | 15 | 20 | 25 | 30 | 40 | 50 | 60 | | |
| K ₂ O . . . | 1.047 | 1.098 | 1.153 | 1.214 | 1.284 | 1.354 | 1.503 | 1.659 | 1.809 | 15. | Schiff. |
| KOH . . . | 1.040 | 1.082 | 1.127 | 1.176 | 1.229 | 1.286 | 1.410 | 1.538 | 1.666 | 15. | " |
| Na ₂ O . . . | 1.073 | 1.144 | 1.218 | 1.284 | 1.354 | 1.421 | 1.557 | 1.689 | 1.829 | 15. | " |
| NaOH . . . | 1.058 | 1.114 | 1.169 | 1.224 | 1.279 | 1.331 | 1.436 | 1.539 | 1.642 | 15. | " |
| NH ₃ . . . | 0.978 | 0.959 | 0.940 | 0.924 | 0.909 | 0.896 | — | — | — | 16. | Carius. |
| NH ₄ Cl . . . | 1.015 | 1.030 | 1.044 | 1.058 | 1.072 | — | — | — | — | 15. | Gerlach. |
| KCl . . . | 1.031 | 1.065 | 1.099 | 1.135 | — | — | — | — | — | 15. | " |
| NaCl . . . | 1.035 | 1.072 | 1.110 | 1.150 | 1.191 | — | — | — | — | 15. | " |
| LiCl . . . | 1.029 | 1.057 | 1.085 | 1.116 | 1.147 | 1.181 | 1.255 | — | — | 15. | " |
| CaCl ₂ . . . | 1.041 | 1.086 | 1.132 | 1.181 | 1.232 | 1.286 | 1.402 | — | — | 15. | " |
| CaCl ₂ + 6H ₂ O | 1.019 | 1.040 | 1.061 | 1.083 | 1.105 | 1.128 | 1.176 | 1.225 | 1.276 | 18. | Schiff. |
| AlCl ₃ . . . | 1.030 | 1.072 | 1.111 | 1.153 | 1.196 | 1.241 | 1.340 | — | — | 15. | Gerlach. |
| MgCl ₂ . . . | 1.041 | 1.085 | 1.130 | 1.177 | 1.226 | 1.278 | — | — | — | 15. | " |
| MgCl ₂ + 6H ₂ O | 1.014 | 1.032 | 1.049 | 1.067 | 1.085 | 1.103 | 1.141 | 1.183 | 1.222 | 24. | Schiff. |
| ZnCl ₂ . . . | 1.043 | 1.089 | 1.135 | 1.184 | 1.236 | 1.289 | 1.417 | 1.563 | 1.737 | 19.5 | Kremers. |
| CdCl ₂ . . . | 1.043 | 1.087 | 1.138 | 1.193 | 1.254 | 1.319 | 1.469 | 1.653 | 1.887 | 19.5 | " |
| SrCl ₂ . . . | 1.044 | 1.092 | 1.143 | 1.198 | 1.257 | 1.321 | — | — | — | 15. | Gerlach. |
| SrCl ₂ + 6H ₂ O | 1.027 | 1.053 | 1.082 | 1.111 | 1.042 | 1.174 | 1.242 | 1.317 | — | 15. | " |
| BaCl ₂ . . . | 1.045 | 1.094 | 1.147 | 1.205 | 1.269 | — | — | — | — | 15. | " |
| BaCl ₂ + 2H ₂ O | 1.035 | 1.075 | 1.119 | 1.166 | 1.217 | 1.273 | — | — | — | 21. | Schiff. |
| CuCl ₂ . . . | 1.044 | 1.091 | 1.155 | 1.221 | 1.291 | 1.360 | 1.527 | — | — | 17.5 | Franz. |
| NiCl ₂ . . . | 1.048 | 1.098 | 1.157 | 1.223 | 1.299 | — | — | — | — | 17.5 | " |
| HgCl ₂ . . . | 1.041 | 1.092 | — | — | — | — | — | — | — | 20. | Mendelejeff. |
| Fe ₂ Cl ₆ . . . | 1.041 | 1.086 | 1.130 | 1.179 | 1.232 | 1.290 | 1.413 | 1.545 | 1.668 | 17.5 | Hager. |
| PtCl ₄ . . . | 1.046 | 1.097 | 1.153 | 1.214 | 1.285 | 1.362 | 1.546 | 1.785 | — | — | Precht. |
| SnCl ₂ + 2H ₂ O | 1.032 | 1.067 | 1.104 | 1.143 | 1.185 | 1.229 | 1.329 | 1.444 | 1.580 | 15. | Gerlach. |
| SnCl ₄ + 5H ₂ O | 1.029 | 1.058 | 1.089 | 1.122 | 1.157 | 1.193 | 1.274 | 1.365 | 1.467 | 15. | " |
| LiBr . . . | 1.033 | 1.070 | 1.111 | 1.154 | 1.202 | 1.252 | 1.366 | 1.498 | — | 19.5 | Kremers. |
| KBr . . . | 1.035 | 1.073 | 1.114 | 1.157 | 1.205 | 1.254 | 1.364 | — | — | 19.5 | " |
| NaBr . . . | 1.038 | 1.078 | 1.123 | 1.172 | 1.224 | 1.279 | 1.408 | 1.563 | — | 19.5 | " |
| MgBr ₂ . . . | 1.041 | 1.085 | 1.135 | 1.189 | 1.245 | 1.308 | 1.449 | 1.623 | — | 19.5 | " |
| ZnBr ₂ . . . | 1.043 | 1.091 | 1.144 | 1.202 | 1.263 | 1.328 | 1.473 | 1.648 | 1.873 | 19.5 | " |
| CdBr ₂ . . . | 1.041 | 1.088 | 1.139 | 1.197 | 1.258 | 1.324 | 1.479 | 1.678 | — | 19.5 | " |
| CaBr ₂ . . . | 1.042 | 1.087 | 1.137 | 1.192 | 1.250 | 1.313 | 1.459 | 1.639 | — | 19.5 | " |
| BaBr ₂ . . . | 1.043 | 1.090 | 1.142 | 1.199 | 1.260 | 1.327 | 1.483 | 1.683 | — | 19.5 | " |
| SrBr ₂ . . . | 1.043 | 1.089 | 1.140 | 1.198 | 1.260 | 1.328 | 1.489 | 1.693 | 1.953 | 19.5 | " |
| KI . . . | 1.036 | 1.076 | 1.118 | 1.164 | 1.216 | 1.269 | 1.394 | 1.544 | 1.732 | 19.5 | " |
| LiI . . . | 1.036 | 1.077 | 1.122 | 1.170 | 1.222 | 1.278 | 1.412 | 1.573 | 1.775 | 19.5 | " |
| NaI . . . | 1.038 | 1.080 | 1.126 | 1.177 | 1.232 | 1.292 | 1.430 | 1.598 | 1.808 | 19.5 | " |
| ZnI ₂ . . . | 1.043 | 1.089 | 1.138 | 1.194 | 1.253 | 1.316 | 1.467 | 1.648 | 1.873 | 19.5 | " |
| CdI ₂ . . . | 1.042 | 1.086 | 1.136 | 1.192 | 1.251 | 1.317 | 1.474 | 1.678 | — | 19.5 | " |
| MgI ₂ . . . | 1.041 | 1.086 | 1.137 | 1.192 | 1.252 | 1.318 | 1.472 | 1.666 | 1.913 | 19.5 | " |
| CaI ₂ . . . | 1.042 | 1.088 | 1.138 | 1.196 | 1.258 | 1.319 | 1.475 | 1.663 | 1.908 | 19.5 | " |
| SrI ₂ . . . | 1.043 | 1.089 | 1.140 | 1.198 | 1.260 | 1.328 | 1.489 | 1.693 | 1.953 | 19.5 | " |
| BaI ₂ . . . | 1.043 | 1.089 | 1.141 | 1.199 | 1.263 | 1.331 | 1.493 | 1.702 | 1.968 | 19.5 | " |
| NaClO ₃ . . . | 1.035 | 1.068 | 1.106 | 1.145 | 1.188 | 1.233 | 1.329 | — | — | 19.5 | " |
| NaBrO ₃ . . . | 1.039 | 1.081 | 1.127 | 1.176 | 1.229 | 1.287 | — | — | — | 19.5 | " |
| KNO ₃ . . . | 1.031 | 1.064 | 1.099 | 1.135 | — | — | — | — | — | 15. | Gerlach. |
| NaNO ₃ . . . | 1.031 | 1.065 | 1.101 | 1.140 | 1.180 | 1.222 | 1.313 | 1.416 | — | 20.2 | Schiff. |
| AgNO ₃ . . . | 1.044 | 1.090 | 1.140 | 1.195 | 1.255 | 1.322 | 1.479 | 1.675 | 1.918 | 15. | Kohlrausch. |

* Compiled from two papers on the subject by Gerlach in the "Zeit. für Anal. Chim.," vols. 8 and 27.

DENSITY OF AQUEOUS SOLUTIONS

| Substance. | Weight of the dissolved substance in 100 parts by weight of the solution. | | | | | | | | | Temp. C. | Authority. |
|--|---|-------|-------|-------|-------|-------|-------|-------|-------|----------|------------|
| | 5 | 10 | 15 | 20 | 25 | 30 | 40 | 50 | 60 | | |
| NH ₄ NO ₃ . . . | 1.020 | 1.041 | 1.063 | 1.085 | 1.107 | 1.131 | 1.178 | 1.229 | 1.282 | 17.5 | Gerlach. |
| Zn(NO ₃) ₂ . . . | 1.048 | 1.095 | 1.146 | 1.201 | 1.263 | 1.325 | 1.456 | 1.597 | — | 17.5 | Franz. |
| Zn(NO ₃) ₂ + 6H ₂ O . . . | — | 1.054 | — | 1.113 | — | 1.178 | 1.250 | 1.329 | — | 14. | Oudemans. |
| Ca(NO ₃) ₂ . . . | 1.037 | 1.075 | 1.118 | 1.162 | 1.211 | 1.260 | 1.367 | 1.482 | 1.604 | 17.5 | Gerlach. |
| Cu(NO ₃) ₂ . . . | 1.044 | 1.093 | 1.143 | 1.203 | 1.263 | 1.328 | 1.471 | — | — | 17.5 | Franz. |
| Sr(NO ₃) ₂ . . . | 1.039 | 1.083 | 1.129 | 1.179 | — | — | — | — | — | 19.5 | Kremers. |
| Pb(NO ₃) ₂ . . . | 1.043 | 1.091 | 1.143 | 1.199 | 1.262 | 1.332 | — | — | — | 17.5 | Gerlach. |
| Cd(NO ₃) ₂ . . . | 1.052 | 1.097 | 1.150 | 1.212 | 1.283 | 1.355 | 1.536 | 1.759 | — | 17.5 | Franz. |
| Co(NO ₃) ₂ . . . | 1.045 | 1.090 | 1.137 | 1.192 | 1.252 | 1.318 | 1.465 | — | — | 17.5 | " |
| Ni(NO ₃) ₂ . . . | 1.045 | 1.090 | 1.137 | 1.192 | 1.252 | 1.318 | 1.465 | — | — | 17.5 | " |
| Fe ₂ (NO ₃) ₆ . . . | 1.039 | 1.076 | 1.117 | 1.160 | 1.210 | 1.261 | 1.373 | 1.496 | 1.657 | 17.5 | " |
| Mg(NO ₃) ₂ + 6H ₂ O . . . | 1.018 | 1.038 | 1.060 | 1.082 | 1.105 | 1.129 | 1.179 | 1.232 | — | 21 | Schiff. |
| Mn(NO ₃) ₂ + 6H ₂ O . . . | 1.025 | 1.052 | 1.079 | 1.108 | 1.138 | 1.169 | 1.235 | 1.307 | 1.386 | 8 | Oudemans. |
| K ₂ CO ₃ . . . | 1.044 | 1.092 | 1.141 | 1.192 | 1.245 | 1.300 | 1.417 | 1.543 | — | 15 | Gerlach. |
| K ₂ CO ₃ + 2H ₂ O . . . | 1.037 | 1.072 | 1.110 | 1.150 | 1.191 | 1.233 | 1.320 | 1.415 | 1.511 | 15. | " |
| Na ₂ CO ₃ 10H ₂ O . . . | 1.019 | 1.038 | 1.057 | 1.077 | 1.098 | 1.118 | — | — | — | 15. | " |
| (NH ₄) ₂ SO ₄ . . . | 1.027 | 1.055 | 1.084 | 1.113 | 1.142 | 1.170 | 1.226 | 1.287 | — | 19. | Schiff. |
| Fe ₂ (SO ₄) ₃ . . . | 1.045 | 1.096 | 1.150 | 1.207 | 1.270 | 1.336 | 1.489 | — | — | 18. | Hager. |
| FeSO ₄ + 7H ₂ O . . . | 1.025 | 1.053 | 1.081 | 1.111 | 1.141 | 1.173 | 1.238 | — | — | 17.2 | Schiff. |
| MgSO ₄ . . . | 1.051 | 1.104 | 1.161 | 1.221 | 1.284 | — | — | — | — | 15 | Gerlach. |
| MgSO ₄ + 7H ₂ O . . . | 1.025 | 1.050 | 1.075 | 1.101 | 1.129 | 1.155 | 1.215 | 1.278 | — | 15. | " |
| Na ₂ SO ₄ + 10H ₂ O . . . | 1.019 | 1.039 | 1.059 | 1.081 | 1.102 | 1.124 | — | — | — | 15. | " |
| CuSO ₄ + 5H ₂ O . . . | 1.031 | 1.064 | 1.098 | 1.134 | 1.173 | 1.213 | — | — | — | 18. | Schiff. |
| MnSO ₄ + 4H ₂ O . . . | 1.031 | 1.064 | 1.099 | 1.135 | 1.174 | 1.214 | 1.303 | 1.398 | — | 15. | Gerlach. |
| ZnSO ₄ + 7H ₂ O . . . | 1.027 | 1.057 | 1.089 | 1.122 | 1.156 | 1.191 | 1.269 | 1.351 | 1.443 | 20.5 | Schiff. |
| Fe ₂ (SO ₄) ₃ · K ₂ SO ₄ + 24H ₂ O . . . | 1.026 | 1.045 | 1.066 | 1.088 | 1.112 | 1.141 | — | — | — | 17.5 | Franz. |
| Cr ₂ (SO ₄) ₃ · K ₂ SO ₄ + 24H ₂ O . . . | 1.016 | 1.033 | 1.051 | 1.073 | 1.099 | 1.126 | 1.188 | 1.287 | 1.454 | 17.5 | " |
| MgSO ₄ + K ₂ SO ₄ + 6H ₂ O . . . | 1.032 | 1.066 | 1.101 | 1.138 | — | — | — | — | — | 15. | Schiff. |
| (NH ₄) ₂ SO ₄ + FeSO ₄ + 6H ₂ O . . . | 1.028 | 1.058 | 1.090 | 1.122 | 1.154 | 1.191 | — | — | — | 19. | " |
| K ₂ CrO ₄ . . . | 1.039 | 1.082 | 1.127 | 1.174 | 1.225 | 1.279 | 1.397 | — | — | 19.5 | " |
| K ₂ Cr ₂ O ₇ . . . | 1.035 | 1.071 | 1.108 | — | — | — | — | — | — | 19.5 | Kremers. |
| Fe(Cy) ₆ K ₄ . . . | 1.028 | 1.059 | 1.092 | 1.126 | — | — | — | — | — | 15. | Schiff. |
| Fe(Cy) ₆ K ₃ . . . | 1.025 | 1.053 | 1.070 | 1.113 | — | — | — | — | — | 13 | " |
| Pb(C ₂ H ₃ O ₂) ₂ + 3H ₂ O . . . | 1.031 | 1.064 | 1.100 | 1.137 | 1.177 | 1.220 | 1.315 | 1.426 | — | 15. | Gerlach. |
| 2NaOH + As ₂ O ₅ + 24H ₂ O . . . | 1.020 | 1.042 | 1.066 | 1.089 | 1.114 | 1.140 | 1.194 | — | — | 14. | Schiff. |
| | 5 | 10 | 15 | 20 | 30 | 40 | 60 | 80 | 100 | | |
| SO ₃ . . . | 1.040 | 1.084 | 1.132 | 1.179 | 1.227 | 1.389 | 1.564 | 1.840 | — | 15. | Brineau. |
| SO ₂ . . . | 1.013 | 1.028 | 1.045 | 1.063 | — | — | — | — | — | 4. | Schiff. |
| N ₂ O ₅ . . . | 1.033 | 1.069 | 1.104 | 1.141 | 1.217 | 1.294 | 1.422 | 1.506 | — | 15. | Kolb. |
| C ₄ H ₆ O ₆ . . . | 1.021 | 1.047 | 1.070 | 1.096 | 1.150 | 1.207 | — | — | — | 15. | Gerlach. |
| C ₆ H ₈ O ₇ . . . | 1.018 | 1.038 | 1.058 | 1.079 | 1.123 | 1.170 | 1.273 | — | — | 15. | " |
| Cane sugar . . . | 1.019 | 1.039 | 1.060 | 1.082 | 1.129 | 1.178 | 1.289 | — | — | 17.5 | " |
| HCl . . . | 1.025 | 1.050 | 1.075 | 1.101 | 1.151 | 1.200 | — | — | — | 15. | Kolb. |
| HBr . . . | 1.035 | 1.073 | 1.114 | 1.158 | 1.257 | 1.376 | — | — | — | 14. | Topsöe. |
| HI . . . | 1.037 | 1.077 | 1.118 | 1.165 | 1.271 | 1.400 | — | — | — | 13. | " |
| H ₂ SO ₄ . . . | 1.032 | 1.069 | 1.106 | 1.145 | 1.223 | 1.307 | 1.501 | 1.732 | 1.838 | 15. | Kolb. |
| H ₂ SiF ₆ . . . | 1.040 | 1.082 | 1.127 | 1.174 | 1.273 | — | — | — | — | 17.5 | Stolba. |
| P ₂ O ₅ . . . | 1.035 | 1.077 | 1.119 | 1.167 | 1.271 | 1.385 | 1.676 | — | — | 17.5 | Hager. |
| P ₂ O ₅ + 3H ₂ O . . . | 1.027 | 1.057 | 1.086 | 1.119 | 1.188 | 1.264 | 1.438 | — | — | 15. | Schiff. |
| HNO ₃ . . . | 1.028 | 1.056 | 1.088 | 1.119 | 1.184 | 1.250 | 1.373 | 1.459 | 1.528 | 15. | Kolb. |
| C ₂ H ₄ O ₂ . . . | 1.007 | 1.014 | 1.021 | 1.028 | 1.041 | 1.052 | 1.068 | 1.075 | 1.055 | 15. | Oudemans. |

DENSITY OF MIXTURES OF ETHYL ALCOHOL AND WATER IN GRAMS PER MILLILITER

The densities in this table are numerically the same as specific gravities at the various temperatures in terms of water at 4° C. as unity. Based upon work done at U. S. Bureau of Standards. See Bulletin Bur. Sids. vol. 9, no. 3; contains extensive bibliography; also Circular 19, 1913.

| Per cent C ₂ H ₅ OH by weight | Temperatures. | | | | | | |
|---|---------------|---------|---------|---------|---------|---------|---------|
| | 10° C. | 15° C. | 20° C. | 25° C. | 30° C. | 35° C. | 40° C. |
| 0 | 0.99973 | 0.99913 | 0.99823 | 0.99708 | 0.99568 | 0.99406 | 0.99225 |
| 1 | 785 | 725 | 636 | 520 | 379 | 217 | 034 |
| 2 | 602 | 542 | 453 | 336 | 194 | 031 | .98846 |
| 3 | 426 | 365 | 275 | 157 | 014 | .98849 | 663 |
| 4 | 258 | 195 | 103 | .98984 | .98839 | 672 | 485 |
| 5 | 098 | 032 | .98938 | 817 | 670 | 501 | 311 |
| 6 | .98946 | .98877 | 780 | 656 | 507 | 335 | 142 |
| 7 | 801 | 729 | 627 | 500 | 347 | 172 | .97975 |
| 8 | 660 | 584 | 478 | 346 | 189 | 009 | 808 |
| 9 | 524 | 442 | 331 | 193 | 031 | .97846 | 641 |
| 10 | 393 | 304 | 187 | 043 | .97875 | 685 | 475 |
| 11 | 267 | 171 | 047 | .97897 | 723 | 527 | 312 |
| 12 | 145 | 041 | .97910 | 753 | 573 | 371 | 150 |
| 13 | 026 | .97914 | 775 | 611 | 424 | 216 | .96989 |
| 14 | .97911 | 790 | 643 | 472 | 278 | 063 | 829 |
| 15 | 800 | 669 | 514 | 334 | 133 | .96911 | 670 |
| 16 | 692 | 552 | 387 | 199 | .96990 | 760 | 512 |
| 17 | 583 | 433 | 259 | 062 | 844 | 607 | 352 |
| 18 | 473 | 313 | 129 | .96923 | 697 | 452 | 189 |
| 19 | 363 | 191 | .96997 | 782 | 547 | 294 | 023 |
| 20 | 252 | 068 | 864 | 639 | 395 | 134 | .95856 |
| 21 | 139 | .96944 | 729 | 495 | 242 | .95973 | 687 |
| 22 | 024 | 818 | 592 | 348 | 087 | 809 | 516 |
| 23 | .96907 | 689 | 453 | 199 | .95929 | 643 | 343 |
| 24 | 787 | 558 | 312 | 048 | 769 | 476 | 168 |
| 25 | 665 | 424 | 168 | .95895 | 607 | 306 | .94991 |
| 26 | 539 | 287 | 020 | 738 | 442 | 133 | 810 |
| 27 | 406 | 144 | .95867 | 576 | 272 | .94955 | 625 |
| 28 | 268 | .95996 | 710 | 410 | 098 | 774 | 438 |
| 29 | 125 | 844 | 548 | 241 | .94922 | 590 | 248 |
| 30 | .95977 | 686 | 382 | 067 | 741 | 403 | 055 |
| 31 | 823 | 524 | 212 | .94890 | 557 | 214 | .93860 |
| 32 | 665 | 357 | 038 | 709 | 370 | 021 | 662 |
| 33 | 502 | 186 | .94860 | 525 | 180 | .93825 | 461 |
| 34 | 334 | 011 | 679 | 337 | .93986 | 626 | 257 |
| 35 | 162 | .94832 | 494 | 146 | 790 | 425 | 051 |
| 36 | .94986 | 650 | 306 | .93952 | 591 | 221 | .92843 |
| 37 | 805 | 464 | 114 | 756 | 390 | 016 | 634 |
| 38 | 620 | 273 | .93919 | 556 | 186 | .92808 | 422 |
| 39 | 431 | 079 | 720 | 353 | .92979 | 597 | 268 |
| 40 | 238 | .93882 | 518 | 148 | 770 | 385 | .91992 |
| 41 | 042 | 682 | 314 | .92940 | 558 | 170 | 774 |
| 42 | .93842 | 478 | 107 | 729 | 344 | .91952 | 554 |
| 43 | 639 | 271 | .92897 | 516 | 128 | 733 | 332 |
| 44 | 433 | 062 | 685 | 301 | .91910 | 513 | 168 |
| 45 | 226 | .92852 | 472 | 085 | 692 | 291 | .90884 |
| 46 | 017 | 640 | 257 | .91868 | 472 | 069 | 660 |
| 47 | .92806 | 426 | 041 | 649 | 250 | .90845 | 434 |
| 48 | 593 | 211 | .91823 | 429 | 028 | 621 | 207 |
| 49 | 379 | .91995 | 604 | 208 | .90805 | 396 | .89979 |
| 50 | 162 | 776 | 384 | .90985 | 580 | 168 | 750 |

DENSITY OF MIXTURES OF ETHYL ALCOHOL AND WATER IN GRAMS PER MILLILITER

| Per cent C_2H_5OH by weight | Temperature. | | | | | | |
|-------------------------------------|--------------|---------|---------|---------|---------|---------|---------|
| | 10° C. | 15° C. | 20° C. | 25° C. | 30° C. | 35° C. | 40° C. |
| 50 | 0.92162 | 0.91776 | 0.91384 | 0.90985 | 0.90580 | 0.90168 | 0.89750 |
| 51 | .91943 | 555 | 160 | 760 | 353 | .89940 | 519 |
| 52 | 723 | 333 | .90936 | 534 | 125 | 710 | 288 |
| 53 | 502 | 110 | 711 | 307 | .89896 | 479 | 056 |
| 54 | 279 | .90885 | 485 | 079 | 667 | 248 | .88823 |
| 55 | 055 | 659 | 258 | .89850 | 437 | 016 | 589 |
| 56 | .90831 | 433 | 031 | 621 | 206 | .88784 | 356 |
| 57 | 607 | 207 | .89803 | 392 | .88975 | 552 | 122 |
| 58 | 381 | .89980 | 574 | 162 | 744 | 319 | .87888 |
| 59 | 154 | 752 | 344 | .88931 | 512 | 085 | 653 |
| 60 | .89927 | 523 | 113 | 699 | 278 | .87851 | 417 |
| 61 | 698 | 293 | .88882 | 466 | 044 | 615 | 180 |
| 62 | 468 | 062 | 650 | 233 | .87809 | 379 | .86943 |
| 63 | 237 | .88830 | 417 | .87998 | 574 | 142 | 705 |
| 64 | 006 | 597 | 183 | 763 | 337 | .86905 | 466 |
| 65 | .88774 | 364 | .87948 | 527 | 100 | 667 | 227 |
| 66 | 541 | 130 | 713 | 291 | .86863 | 429 | .85987 |
| 67 | 308 | .87895 | 477 | 054 | 625 | 190 | 747 |
| 68 | 074 | 660 | 241 | .86817 | 387 | .85950 | 507 |
| 69 | .87839 | 424 | 004 | 579 | 148 | 710 | 266 |
| 70 | 602 | 187 | .86766 | 340 | .85908 | 470 | 025 |
| 71 | 365 | .86949 | 527 | 100 | 667 | 228 | .84783 |
| 72 | 127 | 710 | 287 | .85859 | 426 | .84986 | 540 |
| 73 | .86888 | 470 | 047 | 618 | 184 | 743 | 297 |
| 74 | 648 | 229 | .85806 | 376 | .84941 | 500 | 053 |
| 75 | 408 | .85988 | 564 | 134 | 698 | 257 | .83809 |
| 76 | 168 | 747 | 322 | .84891 | 455 | 013 | 564 |
| 77 | .85927 | 505 | 079 | 647 | 211 | .83768 | 319 |
| 78 | 685 | 262 | .84835 | 403 | .83966 | 523 | 074 |
| 79 | 442 | 018 | 590 | 158 | 720 | 277 | .82827 |
| 80 | 197 | .84772 | 344 | .83911 | 473 | 029 | 578 |
| 81 | .84950 | 525 | 096 | 664 | 224 | .82780 | 329 |
| 82 | 702 | 277 | .83848 | 415 | .82974 | 530 | 079 |
| 83 | 453 | 028 | 599 | 164 | 724 | 279 | .81828 |
| 84 | 203 | .83777 | 348 | .82913 | 473 | 027 | 576 |
| 85 | .83951 | 525 | 095 | 660 | 220 | .81774 | 322 |
| 86 | 697 | 271 | .82840 | 405 | .81965 | 519 | 067 |
| 87 | 441 | 014 | 583 | 148 | 708 | 262 | .80811 |
| 88 | 181 | .82754 | 323 | .81888 | 448 | 003 | 552 |
| 89 | .82919 | 492 | 062 | 626 | 186 | .80742 | 291 |
| 90 | 654 | 227 | .81797 | 362 | .80922 | 478 | 028 |
| 91 | 386 | .81959 | 529 | 094 | 655 | 211 | .79761 |
| 92 | 114 | 688 | 257 | .80823 | 384 | .79941 | 491 |
| 93 | .81839 | 413 | .80983 | 549 | 111 | 669 | 220 |
| 94 | 561 | 134 | 705 | 272 | .79835 | 393 | .78947 |
| 95 | 278 | .80852 | 424 | .79991 | 555 | 114 | 670 |
| 96 | .80991 | 566 | 138 | 706 | 271 | .78831 | 388 |
| 97 | 698 | 274 | .79846 | 415 | .78981 | 542 | 100 |
| 98 | 399 | .79975 | 547 | 117 | 684 | 247 | .77806 |
| 99 | 094 | 670 | 243 | .78814 | 382 | .77946 | 507 |
| 100 | .79784 | 360 | .78934 | 506 | 075 | 641 | 203 |

**DENSITY OF AQUEOUS MIXTURES OF METHYL ALCOHOL, CANE SUGAR,
OR SULFURIC ACID**

| Per cent by weight of substance. | Methyl Alcohol. D $\frac{15^\circ}{4^\circ}$ C. | Cane Sugar. 20° See p. 175 | Sulphuric Acid. 20° D $\frac{4^\circ}{4^\circ}$ C. | Per cent by weight of substance. | Methyl Alcohol. D $\frac{15^\circ}{4^\circ}$ C. | Cane Sugar. 20° See p. 175 | Sulphuric Acid. 20° D $\frac{4^\circ}{4^\circ}$ C. |
|---|---|-------------------------------------|---|---|---|-------------------------------------|---|
| 0 | 0.99913 | 0.998234 | 0.99823 | 50 | 0.91852 | 1.229567 | 1.39505 |
| 1 | .99727 | 1.002120 | 1.00506 | 51 | .91653 | 1.235085 | 1.40487 |
| 2 | .99543 | 1.006015 | 1.01178 | 52 | .91451 | 1.240641 | 1.41481 |
| 3 | .99370 | 1.009934 | 1.01839 | 53 | .91248 | 1.246234 | 1.42487 |
| 4 | .99198 | 1.013881 | 1.02500 | 54 | .91044 | 1.251866 | 1.43503 |
| 5 | .99029 | 1.017854 | 1.03168 | 55 | .90839 | 1.257535 | 1.44530 |
| 6 | .98864 | 1.021855 | 1.03843 | 56 | .90631 | 1.263243 | 1.45568 |
| 7 | .98701 | 1.025885 | 1.04527 | 57 | .90421 | 1.268989 | 1.46615 |
| 8 | .98547 | 1.029942 | 1.05216 | 58 | .90210 | 1.274774 | 1.47673 |
| 9 | .98394 | 1.034029 | 1.05909 | 59 | .89996 | 1.280595 | 1.48740 |
| 10 | .98241 | 1.038143 | 1.06609 | 60 | .89781 | 1.286456 | 1.49818 |
| 11 | .98093 | 1.042288 | 1.07314 | 61 | .89563 | 1.292354 | 1.50904 |
| 12 | .97945 | 1.046462 | 1.08026 | 62 | .89341 | 1.298291 | 1.51999 |
| 13 | .97802 | 1.050665 | 1.08744 | 63 | .89117 | 1.304267 | 1.53102 |
| 14 | .97660 | 1.054900 | 1.09468 | 64 | .88890 | 1.310282 | 1.54213 |
| 15 | .97518 | 1.059165 | 1.10199 | 65 | .88662 | 1.316334 | 1.55333 |
| 16 | .97377 | 1.063460 | 1.10936 | 66 | .88433 | 1.322425 | 1.56460 |
| 17 | .97237 | 1.067789 | 1.11679 | 67 | .88203 | 1.328554 | 1.57595 |
| 18 | .97096 | 1.072147 | 1.12428 | 68 | .87971 | 1.334722 | 1.58739 |
| 19 | .96955 | 1.076537 | 1.13183 | 69 | .87739 | 1.340928 | 1.59890 |
| 20 | .96814 | 1.080959 | 1.13943 | 70 | .87507 | 1.347174 | 1.61048 |
| 21 | .96673 | 1.085414 | 1.14709 | 71 | .87271 | 1.353456 | 1.62213 |
| 22 | .96533 | 1.089900 | 1.15480 | 72 | .87033 | 1.359778 | 1.63384 |
| 23 | .96392 | 1.094420 | 1.16258 | 73 | .86792 | 1.366139 | 1.64560 |
| 24 | .96251 | 1.098971 | 1.17041 | 74 | .86546 | 1.372536 | 1.65738 |
| 25 | .96108 | 1.103557 | 1.17830 | 75 | .86300 | 1.378971 | 1.66917 |
| 26 | .95963 | 1.108175 | 1.18624 | 76 | .86051 | 1.385446 | 1.68095 |
| 27 | .95817 | 1.112828 | 1.19423 | 77 | .85801 | 1.391956 | 1.69268 |
| 28 | .95668 | 1.117512 | 1.20227 | 78 | .85551 | 1.398505 | 1.70433 |
| 29 | .95518 | 1.122231 | 1.21036 | 79 | .85300 | 1.405091 | 1.71585 |
| 30 | .95366 | 1.126984 | 1.21850 | 80 | .85048 | 1.411715 | 1.72717 |
| 31 | .95213 | 1.131773 | 1.22669 | 81 | .84794 | 1.418374 | 1.73827 |
| 32 | .95056 | 1.136596 | 1.23492 | 82 | .84536 | 1.425072 | 1.74904 |
| 33 | .94896 | 1.141453 | 1.24320 | 83 | .84274 | 1.431807 | 1.75943 |
| 34 | .94734 | 1.146345 | 1.25154 | 84 | .84009 | 1.438579 | 1.76932 |
| 35 | .94570 | 1.151275 | 1.25992 | 85 | .83742 | 1.445388 | 1.77860 |
| 36 | .94404 | 1.156238 | 1.26836 | 86 | .83475 | 1.452232 | 1.78721 |
| 37 | .94237 | 1.161236 | 1.27685 | 87 | .83207 | 1.459114 | 1.79509 |
| 38 | .94067 | 1.166269 | 1.28543 | 88 | .82937 | 1.466032 | 1.80223 |
| 39 | .93894 | 1.171340 | 1.29407 | 89 | .82667 | 1.472986 | 1.80864 |
| 40 | .93720 | 1.176447 | 1.30278 | 90 | .82396 | 1.479976 | 1.81438 |
| 41 | .93543 | 1.181592 | 1.31157 | 91 | .82124 | 1.487002 | 1.81950 |
| 42 | .93365 | 1.186773 | 1.32043 | 92 | .81849 | 1.494063 | 1.82401 |
| 43 | .93185 | 1.191993 | 1.32938 | 93 | .81568 | 1.501158 | 1.82790 |
| 44 | .93001 | 1.197247 | 1.33843 | 94 | .81285 | 1.508289 | 1.83115 |
| 45 | .92815 | 1.202540 | 1.34759 | 95 | .80999 | 1.515455 | 1.83368 |
| 46 | .92627 | 1.207870 | 1.35686 | 96 | .80713 | 1.522656 | 1.83548 |
| 47 | .92436 | 1.213238 | 1.36625 | 97 | .80428 | 1.529891 | 1.83637 |
| 48 | .92242 | 1.218643 | 1.37574 | 98 | .80143 | 1.537161 | 1.83605 |
| 49 | .92048 | 1.224086 | 1.38533 | 99 | .79859 | 1.544462 | |
| 50 | .91852 | 1.229567 | 1.39505 | 100 | .79577 | 1.551800 | |

- (1) Calculated from the specific gravity determinations of Doroschewski and Rozhdstvenski at 15°/15°C; J. Russ., Phys. Chem. Soc., 41, p. 977, 1909.
 (2) According to Dr. F. Plato; Wiss. Abh. der K. Normal-Eichungs-Kommission, 2, p. 153, 1900.
 (3) Calculated from Dr. Domke's table; Wiss. Abh. der K. Normal-Eichungs-Kommission, 5, p. 131, 1900.

All reprinted from Circular 19, U.S. Bureau of Standards, 1913.

DENSITY, BRIX, AND BAUMÉ DEGREES, OF CANE SUGAR SOLUTIONS

Degrees Brix, Specific Gravity, and Degrees Baumé of Sugar Solutions.

Degrees Brix = Per cent Sucrose by Weight.

Specific Gravities and Degrees Baumé corresponding to the Degrees Brix are for $\frac{20^{\circ}}{20^{\circ}}$ C.The relation between the specific gravity and Degrees Baumé is given by Degrees Baumé = $145 - \frac{145}{\text{specific gravity}}$

| Degrees Brix or per cent sucrose by weight | Specific gravity at 20°/20°C | Degrees Baumé (modulus 145) | Degrees Brix or per cent sucrose by weight | Specific gravity at 20°/20°C | Degrees Baumé (modulus 145) | Degrees Brix or per cent sucrose by weight | Specific gravity at 20°/20°C | Degrees Baumé (modulus 145) |
|--|------------------------------|-----------------------------|--|------------------------------|-----------------------------|--|------------------------------|-----------------------------|
| 0.0 | 1.00000 | 0.00 | 40.0 | 1.17853 | 21.97 | 80.0 | 1.41421 | 42.47 |
| 1.0 | 1.00389 | 0.56 | 41.0 | 1.18368 | 22.50 | 81.0 | 1.42088 | 42.95 |
| 2.0 | 1.00779 | 1.12 | 42.0 | 1.18887 | 23.04 | 82.0 | 1.42759 | 43.43 |
| 3.0 | 1.01172 | 1.68 | 43.0 | 1.19410 | 23.57 | 83.0 | 1.43434 | 43.91 |
| 4.0 | 1.01567 | 2.24 | 44.0 | 1.19936 | 24.10 | 84.0 | 1.44112 | 44.38 |
| 5.0 | 1.01965 | 2.79 | 45.0 | 1.20467 | 24.63 | 85.0 | 1.44794 | 44.86 |
| 6.0 | 1.02366 | 3.35 | 46.0 | 1.21001 | 25.17 | 86.0 | 1.45480 | 45.33 |
| 7.0 | 1.02770 | 3.91 | 47.0 | 1.21538 | 25.70 | 87.0 | 1.46170 | 45.80 |
| 8.0 | 1.03176 | 4.46 | 48.0 | 1.22080 | 26.23 | 88.0 | 1.46862 | 46.27 |
| 9.0 | 1.03586 | 5.02 | 49.0 | 1.22625 | 26.75 | 89.0 | 1.47559 | 46.73 |
| 10.0 | 1.03998 | 5.57 | 50.0 | 1.23174 | 27.28 | 90.0 | 1.48259 | 47.20 |
| 11.0 | 1.04413 | 6.13 | 51.0 | 1.23727 | 27.81 | 91.0 | 1.48963 | 47.66 |
| 12.0 | 1.04831 | 6.68 | 52.0 | 1.24284 | 28.33 | 92.0 | 1.49671 | 48.12 |
| 13.0 | 1.05252 | 7.24 | 53.0 | 1.24844 | 28.86 | 93.0 | 1.50381 | 48.58 |
| 14.0 | 1.05677 | 7.79 | 54.0 | 1.25408 | 29.38 | 94.0 | 1.51096 | 49.03 |
| 15.0 | 1.06104 | 8.34 | 55.0 | 1.25976 | 29.90 | 95.0 | 1.51814 | 49.49 |
| 16.0 | 1.06534 | 8.89 | 56.0 | 1.26548 | 30.42 | 96.0 | 1.52535 | 49.94 |
| 17.0 | 1.06968 | 9.45 | 57.0 | 1.27123 | 30.94 | 97.0 | 1.53260 | 50.39 |
| 18.0 | 1.07404 | 10.00 | 58.0 | 1.27703 | 31.46 | 98.0 | 1.53988 | 50.84 |
| 19.0 | 1.07844 | 10.55 | 59.0 | 1.28286 | 31.97 | 99.0 | 1.54719 | 51.28 |
| 20.0 | 1.08287 | 11.10 | 60.0 | 1.28873 | 32.49 | 100.0 | 1.55454 | 51.73 |
| 21.0 | 1.08733 | 11.65 | 61.0 | 1.29464 | 33.00 | | | |
| 22.0 | 1.09183 | 12.20 | 62.0 | 1.30059 | 33.51 | | | |
| 23.0 | 1.09636 | 12.74 | 63.0 | 1.30657 | 34.02 | | | |
| 24.0 | 1.10092 | 13.29 | 64.0 | 1.31260 | 34.53 | | | |
| 25.0 | 1.10551 | 13.84 | 65.0 | 1.31866 | 35.04 | | | |
| 26.0 | 1.11014 | 14.39 | 66.0 | 1.32476 | 35.55 | | | |
| 27.0 | 1.11480 | 14.93 | 67.0 | 1.33090 | 36.05 | | | |
| 28.0 | 1.11949 | 15.48 | 68.0 | 1.33708 | 36.55 | | | |
| 29.0 | 1.12422 | 16.02 | 69.0 | 1.34330 | 37.06 | | | |
| 30.0 | 1.12898 | 16.57 | 70.0 | 1.34956 | 37.56 | | | |
| 31.0 | 1.13378 | 17.11 | 71.0 | 1.35585 | 38.06 | | | |
| 32.0 | 1.13861 | 17.65 | 72.0 | 1.36218 | 38.55 | | | |
| 33.0 | 1.14347 | 18.19 | 73.0 | 1.36856 | 39.05 | | | |
| 34.0 | 1.14837 | 18.73 | 74.0 | 1.37496 | 39.54 | | | |
| 35.0 | 1.15331 | 19.28 | 75.0 | 1.38141 | 40.03 | | | |
| 36.0 | 1.15828 | 19.81 | 76.0 | 1.38790 | 40.53 | | | |
| 37.0 | 1.16329 | 20.35 | 77.0 | 1.39442 | 41.01 | | | |
| 38.0 | 1.16833 | 20.89 | 78.0 | 1.40098 | 41.50 | | | |
| 39.0 | 1.17341 | 21.43 | 79.0 | 1.40758 | 41.99 | | | |

The above table is abridged from Bureau of Standards Technologic Paper No. 115. The original table is given in steps of 0.1 Degrees Brix.

SMITHSONIAN TABLES.

TABLE 127
DENSITY OF GASES

The following table gives the density as the weight in grams of a liter (normal liter) of the gas at 0°C, 76 cm pressure, and standard gravity, 980.665 cm/sec.², (sea-level, 45° latitude), the specific gravity referred to dry, carbon-dioxide-free air, and to pure oxygen, and the weight in pounds per cubic foot. Dry, carbon-dioxide-free air is of remarkably uniform density; Guye, Kovacs and Wourzel found maximum variations in the density of only 7 to 8 parts in 10,000. For highest accuracy pure oxygen should be used as the standard gas for specific gravities. Observed densities are closely proportional to the molecular weights. The following table was prepared by the Gas Chemistry Section, Bur. Standards, 1929.

| Gas | Formula | Weight of normal liter in grams | Air = 1 | O ₂ = 1 | Pounds per cubic foot | Reference |
|----------------------------|-----------------------------------|--|--------------------|----------------------|--------------------------------|-----------|
| Air..... | | 1.2929 | 1.0000 | .9047 | .08071 | 1 |
| Acetylene..... | C ₂ H ₂ | 1.173 | .907 | .8208 | .07323 | 1 |
| Ammonia..... | NH ₃ | .7710 | .5963 | .5395 | .04813 | 1 |
| Argon..... | A | 1.7837 | 1.3796 | 1.2482 | .11135 | 2 |
| Arsine..... | AsH ₃ | 3.48 | 2.69 | 2.44 | .217 | 1 |
| Butane-iso..... | C ₄ H ₁₀ | 2.673 | 2.067 | 1.870 | .1669 | 1 |
| Butane-n..... | C ₄ H ₁₀ | 2.519 ₀ { at 710 mm } | 2.0854* | 1.886 ₈ * | .1572 ₈ * | 5, 6 |
| Carbon dioxide..... | CO ₂ | 1.9769 | 1.5290 | 1.3834 | .12341 | 1 |
| Carbon monoxide..... | CO | 1.2504 | .9671 | .8750 | .07806 | 1 |
| Carbon oxysulphide..... | COS | 2.72 | 2.10 | 1.90 | .170 | 1 |
| Chlorine..... | Cl ₂ | 3.214 | 2.486 | 2.249 | .2006 | 1 |
| Chlorine monoxide..... | Cl ₂ O | 3.89 | 3.01 | 2.72 | .243 | 1 |
| Ethane..... | C ₂ H ₆ | 1.3566 | 1.0493 | .9493 | .08469 | 1 |
| Ethylene..... | C ₂ H ₄ | 1.2604 | .9749 | .8820 | .07868 | 1 |
| Fluorine..... | F ₂ | 1.696 | 1.312 | 1.187 | .1059 | 1 |
| Helium..... | He | .1784 ₇ | .1380 ₄ | .1248 ₉ | .01114 ₂ | 1 |
| Hydrogen..... | H ₂ | .08988 | .0695 ₂ | .06290 | .005611 | 1 |
| Hydrogen bromide..... | HBr | 3.6445 | 2.8189 | 2.5503 | .22752 | 1 |
| Hydrogen chloride..... | HCl | 1.6392 | 1.2678 | 1.1471 | .10233 | 1 |
| Hydrogen iodide..... | HI | 5.7891 | 4.477 ₆ | 4.051 ₀ | .3614 ₀ | 1 |
| Hydrogen selenide..... | H ₂ Se | 3.670 | 2.839 | 2.568 | .229 | 1 |
| Hydrogen sulphide..... | H ₂ S | 1.539 | 1.190 | 1.077 | .09608 | 1 |
| Krypton..... | Kr | 3.70 ₈ | 2.86 ₈ | 2.59 ₈ | .231 ₆ | 1 |
| Methane..... | CH ₄ | .716 ₈ | .554 ₄ | .501 ₆ | .0447 ₈ | 1 |
| Monomethylamine..... | CH ₃ NH ₂ | 1.396 | 1.080 | .9769 | .08715 | 1 |
| Methyl chloride..... | CH ₃ Cl | 2.3076 | 1.7848 | 1.6148 | .14406 | 1 |
| Methyl ether..... | (CH ₃) ₂ O | 2.1098 | 1.6318 | 1.4764 | .13171 | 1 |
| Methyl fluoride..... | CH ₃ F | 1.5452 | 1.1951 | 1.0813 | .09646 | 1 |
| Neon..... | Ne | .9003 ₅ | .6963 ₃ | .6300 ₄ | .05620 ₇ | 3 |
| Nitric oxide..... | NO | 1.3402 | 1.0366 | .9378 | .08367 | 1 |
| Nitrogen (chem)..... | N ₂ | 1.2505 ₆ | .9672 ₄ | .8751 ₀ | .07806 ₉ | 1, 4 |
| Nitrogen (atm)..... | | 1.2568 | .9721 | .8795 | .07846 | 1 |
| Nitrosyl chloride..... | NOCl | 2.992 | 2.314 | 2.094 | .1868 | 1 |
| Nitrous oxide..... | N ₂ O | 1.977 ₈ | 1.529 ₇ | 1.384 ₀ | .1234 ₇ | 1 |
| Oxygen..... | O ₂ | 1.42904 | 1.10527 | 1.0000 | .089212 | 1 |
| Phosphine..... | PH ₃ | 1.5294 | 1.182 ₉ | 1.070 ₂ | .0954 ₈ | 1 |
| Propane..... | C ₃ H ₈ | 2.020 | 1.562 | 1.414 | .1261 | 1 |
| Silicon tetrafluoride..... | SiF ₄ | 4.684 | 3.62 ₃ | 3.27 ₈ | .2924 | 1 |
| Sulphur dioxide..... | SO ₂ | 2.9269 | 2.2638 | 2.0482 | .18272 | 1 |
| Xenon..... | X | 5.851 | 4.52 ₆ | 4.09 ₄ | .365 ₃ | 1 |

* Both butane and air at 710 mm.

1. Based on densities in I. C. T., 3, 3, 1928.

2. Baxter and Starkweather, Proc. Nat. Acad. Sci., 14, 57, 1928.

3. Baxter and Starkweather, Proc. Nat. Acad. Sci., 14, 50, 1928.

4. Moles and Clavera, Z. Anorg. Allgem. Chem., 167, 49, 1927.

5. Bogaert, Bull. Soc. Chim. Belg., 36, 384, 1927.

6. Beckers, Bull. Soc. Chim. Belg., 36, 559, 1927.

RELATIVE DENSITY OF MOIST AIR FOR DIFFERENT PRESSURES AND HUMIDITIES

TABLE 128.—Values of $\frac{h}{760}$, from $h = 1$ to $h = 9$, for the Computation of Different Values of the Ratio of Actual to Normal Barometric Pressure

This gives the density of moist air at pressure h in terms of the same air at normal atmosphere pressure. When air contains moisture, as is usually the case with the atmosphere, we have the following equation for pressure term: $h = B - 0.378e$, where e is the vapor pressure, and B the corrected barometric pressure. When the necessary psychrometric observations are made the value of e may be taken from Table 212 and then $0.378e$ from Table 130, or the dew point may be found and the value of $0.378e$ taken from Table 130.

| h | $\frac{h}{760}$ |
|-----|-----------------|
| 1 | 0.0013158 |
| 2 | .0026316 |
| 3 | .0039474 |
| 4 | 0.0052632 |
| 5 | .0065789 |
| 6 | .0078947 |
| 7 | 0.0092105 |
| 8 | .0105263 |
| 9 | .0118421 |

EXAMPLES OF USE OF THE TABLE.

To find the value of $\frac{h}{760}$ when $h = 754.3$

| | |
|-----------------|---------|
| $h = 700$ gives | .92105 |
| 50 " | .065789 |
| 4 " | .005263 |
| .3 " | .000395 |
| 754.3 | .992497 |

To find the value of $\frac{h}{760}$ when $h = 5.73$

| | |
|---------------|----------|
| $h = 5$ gives | .0065789 |
| .7 " | .000210 |
| .03 " | .0000395 |
| 5.73 | .0075394 |

TABLE 129.—Values of the logarithms of $\frac{h}{760}$ for values of h between 80 and 800

Values from 8 to 80 may be got by subtracting 1 from the characteristic, and from 0.8 to 8 by subtracting 2 from the characteristic, and so on.

| h | Values of $\log \frac{h}{760}$ | | | | | | | | | |
|-----|--------------------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 80 | .102228 | .102767 | .103300 | .103826 | .104347 | .104861 | .105368 | .105871 | .106367 | .106858 |
| 90 | .07343 | .07823 | .08297 | .08767 | .09231 | .09691 | .10146 | .10596 | .11041 | .11482 |
| 100 | .111919 | .112351 | .112779 | .113202 | .113622 | .114038 | .114449 | .114857 | .115261 | .115661 |
| 110 | .16058 | .16451 | .16840 | .17226 | .17609 | .17988 | .18364 | .18737 | .19107 | .19473 |
| 120 | .19837 | .20197 | .20555 | .20909 | .21261 | .21611 | .21956 | .22299 | .22640 | .22978 |
| 130 | .23313 | .23646 | .23976 | .24304 | .24629 | .24952 | .25273 | .25591 | .25907 | .26220 |
| 140 | .26531 | .26841 | .27147 | .27452 | .27755 | .28055 | .28354 | .28650 | .28945 | .29237 |
| 150 | .29528 | .29816 | .30103 | .30388 | .30671 | .30952 | .31231 | .31509 | .31784 | .32058 |
| 160 | .32331 | .32601 | .32870 | .33137 | .33403 | .33667 | .33929 | .34190 | .34450 | .34707 |
| 170 | .34964 | .35218 | .35471 | .35723 | .35974 | .36222 | .36470 | .36716 | .36961 | .37204 |
| 180 | .37446 | .37686 | .37926 | .38164 | .38400 | .38636 | .38870 | .39128 | .39334 | .39565 |
| 190 | .39794 | .40022 | .40249 | .40474 | .40699 | .40922 | .41144 | .41365 | .41585 | .41804 |
| 200 | .42022 | .42238 | .42454 | .42668 | .42882 | .43094 | .43305 | .43516 | .43725 | .43933 |
| 210 | .44141 | .44347 | .44552 | .44757 | .44960 | .45162 | .45364 | .45565 | .45764 | .45963 |
| 220 | .46161 | .46358 | .46554 | .46749 | .46943 | .47137 | .47329 | .47521 | .47712 | .47902 |
| 230 | .48091 | .48280 | .48467 | .48654 | .48840 | .49025 | .49210 | .49393 | .49576 | .49758 |
| 240 | .49940 | .50120 | .50300 | .50479 | .50658 | .50835 | .51012 | .51188 | .51364 | .51539 |
| 250 | .51713 | .51886 | .52059 | .52231 | .52402 | .52573 | .52743 | .52912 | .53081 | .53249 |
| 260 | .53416 | .53583 | .53749 | .53914 | .54079 | .54243 | .54407 | .54570 | .54732 | .54894 |
| 270 | .55055 | .55216 | .55376 | .55535 | .55694 | .55852 | .56010 | .56167 | .56323 | .56479 |
| 280 | .56634 | .56789 | .56944 | .57097 | .57250 | .57403 | .57555 | .57707 | .57858 | .58008 |
| 290 | .58158 | .58308 | .58457 | .58605 | .58753 | .58901 | .59048 | .59194 | .59340 | .59486 |
| 300 | .59631 | .59775 | .59919 | .60063 | .60206 | .60349 | .60491 | .60632 | .60774 | .60914 |
| 310 | .61055 | .61195 | .61334 | .61473 | .61611 | .61750 | .61887 | .62025 | .62161 | .62298 |
| 320 | .62434 | .62569 | .62704 | .62839 | .62973 | .63107 | .63240 | .63373 | .63506 | .63638 |
| 330 | .63770 | .63901 | .64032 | .64163 | .64293 | .64423 | .64553 | .64682 | .64810 | .64939 |
| 340 | .65067 | .65194 | .65321 | .65448 | .65574 | .65701 | .65826 | .65952 | .66077 | .66201 |

TABLE 129 (*continued*)
DENSITY OF MOIST AIR

Values of logarithms of $\frac{h}{760}$ for values of h between 80 and 800

| h | Values of $\log \frac{h}{760}$ | | | | | | | | | |
|------------|--------------------------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 350 | $\bar{1}.66325$ | $\bar{1}.66449$ | $\bar{1}.66573$ | $\bar{1}.66696$ | $\bar{1}.66819$ | $\bar{1}.66941$ | $\bar{1}.67064$ | $\bar{1}.67185$ | $\bar{1}.67307$ | $\bar{1}.67428$ |
| 360 | .67549 | .67669 | .67790 | .67909 | .68029 | .68148 | .68267 | .68385 | .68503 | .68621 |
| 370 | .68739 | .68856 | .68973 | .69090 | .69206 | .69322 | .69437 | .69553 | .69668 | .69783 |
| 380 | .69897 | .70011 | .70125 | .70239 | .70352 | .70465 | .70577 | .70690 | .70802 | .70914 |
| 390 | .71025 | .71136 | .71247 | .71358 | .71468 | .71578 | .71688 | .71798 | .71907 | .72016 |
| 400 | $\bar{1}.72125$ | $\bar{1}.72233$ | $\bar{1}.72341$ | $\bar{1}.72449$ | $\bar{1}.72557$ | $\bar{1}.72664$ | $\bar{1}.72771$ | $\bar{1}.72878$ | $\bar{1}.72985$ | $\bar{1}.73091$ |
| 410 | .73197 | .73303 | .73408 | .73514 | .73619 | .73723 | .73828 | .73932 | .74036 | .74140 |
| 420 | .74244 | .74347 | .74450 | .74553 | .74655 | .74758 | .74860 | .74961 | .75063 | .75164 |
| 430 | .75265 | .75366 | .75467 | .75567 | .75668 | .75768 | .75867 | .75967 | .76066 | .76165 |
| 440 | .76264 | .76362 | .76461 | .76559 | .76657 | .76755 | .76852 | .76949 | .77046 | .77143 |
| 450 | $\bar{1}.77240$ | $\bar{1}.77336$ | $\bar{1}.77432$ | $\bar{1}.77528$ | $\bar{1}.77624$ | $\bar{1}.77720$ | $\bar{1}.77815$ | $\bar{1}.77910$ | $\bar{1}.78005$ | $\bar{1}.78100$ |
| 460 | .78194 | .78289 | .78383 | .78477 | .78570 | .78664 | .78757 | .78850 | .78943 | .79036 |
| 470 | .79128 | .79221 | .79313 | .79405 | .79496 | .79588 | .79679 | .79770 | .79861 | .79952 |
| 480 | .80043 | .80133 | .80223 | .80313 | .80403 | .80493 | .80582 | .80672 | .80761 | .80850 |
| 490 | .80938 | .81027 | .81115 | .81203 | .81291 | .81379 | .81467 | .81554 | .81642 | .81729 |
| 500 | $\bar{1}.81816$ | $\bar{1}.81902$ | $\bar{1}.81989$ | $\bar{1}.82075$ | $\bar{1}.82162$ | $\bar{1}.82248$ | $\bar{1}.82334$ | $\bar{1}.82419$ | $\bar{1}.82505$ | $\bar{1}.82590$ |
| 510 | .82676 | .82761 | .82846 | .82930 | .83015 | .83099 | .83184 | .83268 | .83352 | .83435 |
| 520 | .83519 | .83602 | .83686 | .83769 | .83852 | .83935 | .84017 | .84100 | .84182 | .84264 |
| 530 | .84346 | .84428 | .84510 | .84591 | .84673 | .84754 | .84835 | .84916 | .84997 | .85076 |
| 540 | .85158 | .85238 | .85319 | .85399 | .85479 | .85558 | .85638 | .85717 | .85797 | .85876 |
| 550 | $\bar{1}.85955$ | $\bar{1}.86034$ | $\bar{1}.86113$ | $\bar{1}.86191$ | $\bar{1}.86270$ | $\bar{1}.86348$ | $\bar{1}.86426$ | $\bar{1}.86504$ | $\bar{1}.86582$ | $\bar{1}.86660$ |
| 560 | .86737 | .86815 | .86892 | .86969 | .87047 | .87123 | .87200 | .87277 | .87353 | .87430 |
| 570 | .87506 | .87582 | .87658 | .87734 | .87810 | .87885 | .87961 | .88036 | .88111 | .88186 |
| 580 | .88261 | .88336 | .88411 | .88486 | .88560 | .88634 | .88708 | .88782 | .88856 | .88930 |
| 590 | .89004 | .89077 | .89151 | .89224 | .89297 | .89370 | .89443 | .89516 | .89589 | .89661 |
| 600 | $\bar{1}.89734$ | $\bar{1}.89806$ | $\bar{1}.89878$ | $\bar{1}.89950$ | $\bar{1}.90022$ | $\bar{1}.90094$ | $\bar{1}.90166$ | $\bar{1}.90238$ | $\bar{1}.90309$ | $\bar{1}.90380$ |
| 610 | .90452 | .90523 | .90594 | .90665 | .90735 | .90806 | .90877 | .90947 | .91017 | .91088 |
| 620 | .91158 | .91228 | .91298 | .91367 | .91437 | .91507 | .91576 | .91645 | .91715 | .91784 |
| 630 | .91853 | .91922 | .91990 | .92059 | .92128 | .92196 | .92264 | .92333 | .92401 | .92469 |
| 640 | .92537 | .92604 | .92672 | .92740 | .92807 | .92875 | .92942 | .93009 | .93076 | .93143 |
| 650 | $\bar{1}.93210$ | $\bar{1}.93277$ | $\bar{1}.93343$ | $\bar{1}.93410$ | $\bar{1}.93476$ | $\bar{1}.93543$ | $\bar{1}.93609$ | $\bar{1}.93675$ | $\bar{1}.93741$ | $\bar{1}.93807$ |
| 660 | .93873 | .93939 | .94004 | .94070 | .94135 | .94201 | .94266 | .94331 | .94396 | .94461 |
| 670 | .94526 | .94591 | .94656 | .94720 | .94785 | .94849 | .94913 | .94978 | .95042 | .95106 |
| 680 | .95170 | .95233 | .95297 | .95361 | .95424 | .95488 | .95551 | .95614 | .95677 | .95741 |
| 690 | .95804 | .95866 | .95929 | .95992 | .96055 | .96117 | .96180 | .96242 | .96304 | .96366 |
| 700 | $\bar{1}.96428$ | $\bar{1}.96490$ | $\bar{1}.96552$ | $\bar{1}.96614$ | $\bar{1}.96676$ | $\bar{1}.96738$ | $\bar{1}.96799$ | $\bar{1}.96861$ | $\bar{1}.96922$ | $\bar{1}.96983$ |
| 710 | .97044 | .97106 | .97167 | .97228 | .97288 | .97349 | .97410 | .97471 | .97531 | .97592 |
| 720 | .97652 | .97712 | .97772 | .97832 | .97892 | .97951 | .98012 | .98072 | .98132 | .98191 |
| 730 | .98251 | .98310 | .98370 | .98429 | .98488 | .98547 | .98606 | .98665 | .98724 | .98783 |
| 740 | .98842 | .98900 | .98959 | .99018 | .99076 | .99134 | .99193 | .99251 | .99309 | .99367 |
| 750 | $\bar{1}.99425$ | $\bar{1}.99483$ | $\bar{1}.99540$ | $\bar{1}.99598$ | $\bar{1}.99656$ | $\bar{1}.99713$ | $\bar{1}.99771$ | $\bar{1}.99828$ | $\bar{1}.99886$ | $\bar{1}.99942$ |
| 760 | 0.00000 | 0.00057 | 0.00114 | 0.00171 | 0.00228 | 0.00285 | 0.00342 | 0.00398 | 0.00455 | 0.00511 |
| 770 | .00568 | .00624 | .00680 | .00737 | .00793 | .00849 | .00905 | .00961 | .01017 | .01072 |
| 780 | .01128 | .01184 | .01239 | .01295 | .01350 | .01406 | .01461 | .01516 | .01571 | .01626 |
| 790 | .01681 | .01736 | .01791 | .01846 | .01901 | .01955 | .02010 | .02064 | .02119 | .02173 |

DENSITY OF MOIST AIR

TABLE 130. — Values of $0.378e^*$

This table gives the humidity term $0.378e$, which occurs in the equation $\delta = \delta_0 \frac{h}{760}$
 $= \delta_0 \frac{B - 0.378e}{760}$ for the calculation of the density of air containing aqueous vapor at pressure e ; δ_0 is the density of dry air at normal temperature and barometric pressure, B the observed barometric pressure, and $h = B - 0.378e$, the pressure corrected for humidity. For values of $\frac{h}{760}$, see Table 128. Temperatures are in degrees Centigrade, and pressures in millimeters of mercury.

| Dew point. | $\frac{e}{\text{Vapor pressure (ice)}}$ | $0.378e$ | Dew point. | $\frac{e}{\text{Vapor pressure (water)}}$ | $0.378e$ | Dew point. | $\frac{e}{\text{Vapor pressure (water)}}$ | $0.378e$ |
|------------|---|----------|------------|---|----------|------------|---|----------|
| C | mm | mm | C | mm | mm | C | mm | mm |
| -50° | 0.029 | 0.01 | 0° | 4.58 | 1.73 | 30° | 31.86 | 12.0 |
| -45 | 0.054 | 0.02 | 1 | 4.92 | 1.86 | 31 | 33.74 | 12.8 |
| -40 | 0.096 | 0.04 | 2 | 5.29 | 2.00 | 32 | 35.70 | 13.5 |
| -35 | 0.169 | 0.06 | 3 | 5.68 | 2.15 | 33 | 37.78 | 14.3 |
| -30 | 0.288 | 0.11 | 4 | 6.10 | 2.31 | 34 | 39.95 | 15.1 |
| -25 | 0.480 | 0.18 | 5 | 6.54 | 2.47 | 35 | 42.23 | 16.0 |
| 24 | 0.530 | 0.20 | 6 | 7.01 | 2.66 | 36 | 44.62 | 16.9 |
| 23 | 0.585 | 0.22 | 7 | 7.51 | 2.84 | 37 | 47.13 | 17.8 |
| 22 | 0.646 | 0.24 | 8 | 8.04 | 3.04 | 38 | 49.76 | 18.8 |
| 21 | 0.712 | 0.27 | 9 | 8.61 | 3.25 | 39 | 52.51 | 19.8 |
| -20 | 0.783 | 0.30 | 10 | 9.21 | 3.48 | 40 | 55.40 | 20.9 |
| 19 | 0.862 | 0.33 | 11 | 9.85 | 3.72 | 41 | 58.42 | 22.1 |
| 18 | 0.947 | 0.36 | 12 | 10.52 | 3.98 | 42 | 61.58 | 23.3 |
| 17 | 1.041 | 0.39 | 13 | 11.24 | 4.25 | 43 | 64.89 | 24.5 |
| 16 | 1.142 | 0.43 | 14 | 11.99 | 4.53 | 44 | 68.35 | 25.8 |
| -15 | 1.252 | 0.47 | 15 | 12.79 | 4.84 | 45 | 71.97 | 27.2 |
| 14 | 1.373 | 0.52 | 16 | 13.64 | 5.16 | 46 | 75.75 | 28.6 |
| 13 | 1.503 | 0.57 | 17 | 14.54 | 5.50 | 47 | 79.70 | 30.1 |
| 12 | 1.644 | 0.62 | 18 | 15.49 | 5.85 | 48 | 83.83 | 31.7 |
| 11 | 1.798 | 0.68 | 19 | 16.49 | 6.23 | 49 | 88.14 | 33.3 |
| -10 | 1.964 | 0.74 | 20 | 17.55 | 6.63 | 50 | 92.6 | 35.0 |
| 9 | 2.144 | 0.81 | 21 | 18.66 | 7.06 | 51 | 97.3 | 36.8 |
| 8 | 2.340 | 0.88 | 22 | 19.84 | 7.50 | 52 | 102.2 | 38.6 |
| 7 | 2.550 | 0.96 | 23 | 21.09 | 7.97 | 53 | 107.3 | 40.6 |
| 6 | 2.778 | 1.05 | 24 | 22.40 | 8.47 | 54 | 112.7 | 42.6 |
| -5 | 3.025 | 1.14 | 25 | 23.78 | 8.99 | 55 | 118.2 | 44.7 |
| 4 | 3.291 | 1.24 | 26 | 25.24 | 9.54 | 56 | 124.0 | 46.9 |
| 3 | 3.578 | 1.35 | 27 | 26.77 | 10.12 | 57 | 130.0 | 49.1 |
| 2 | 3.887 | 1.47 | 28 | 28.38 | 10.73 | 58 | 136.3 | 51.5 |
| 1 | 4.220 | 1.60 | 29 | 30.08 | 11.37 | 59 | 142.8 | 54.0 |
| 0 | 4.580 | 1.73 | 30 | 31.86 | 12.04 | 60 | 149.6 | 56.5 |

* Table quoted from Smithsonian Meteorological Tables.

TABLE 131. — Maintenance of Air at Definite Humidities

Taken from Stevens, *Phytopathology*, 6, 428, 1916; see also Curtis, *Bul. Bur. Standards*, 11, 359, 1914; Dieterici, *Ann. d. Phys. u. Chem.*, 50, 47, 1893. The relative humidity and vapor pressure of aqueous vapor of moist air in equilibrium conditions above aqueous solutions of sulphuric acid are given below.

| Density of acid sol. | Relative humidity. | Vapor pressure. | | Density of acid sol. | Relative humidity. | Vapor pressure. | |
|----------------------|--------------------|-----------------|-------|----------------------|--------------------|-----------------|-------|
| | | 20° C | 30° C | | | 20° C | 30° C |
| | | mm | mm | | | mm | mm |
| 1.00 | 100.0 | 17.4 | 31.0 | 1.30 | 58.3 | 10.1 | 18.4 |
| 1.05 | 97.5 | 17.0 | 30.7 | 1.35 | 47.2 | 8.3 | 15.0 |
| 1.10 | 93.9 | 16.3 | 29.6 | 1.40 | 37.1 | 6.5 | 11.9 |
| 1.15 | 88.8 | 15.4 | 28.0 | 1.50 | 18.8 | 3.3 | 6.0 |
| 1.20 | 80.5 | 14.0 | 25.4 | 1.60 | 8.5 | 1.5 | 2.7 |
| 1.25 | 70.4 | 12.2 | 22.2 | 1.70 | 3.2 | 0.6 | 1.0 |

PRESSURE OF COLUMNS OF MERCURY AND WATER

British and metric measures. Correct at 0° C. for mercury and at 4° C. for water.

| METRIC MEASURE. | | | BRITISH MEASURE. | | |
|-----------------|-------------------------------|----------------------------------|------------------|-------------------------------|----------------------------------|
| Cms. of Hg. | Pressure in grams per sq. cm. | Pressure in pounds per sq. inch. | Inches of Hg. | Pressure in grams per sq. cm. | Pressure in pounds per sq. inch. |
| 1 | 13.5956 | 0.193376 | 1 | 34.533 | 0.491174 |
| 2 | 27.1912 | 0.386752 | 2 | 69.066 | 0.982348 |
| 3 | 40.7868 | 0.580128 | 3 | 103.598 | 1.473522 |
| 4 | 54.3824 | 0.773504 | 4 | 138.131 | 1.964696 |
| 5 | 67.9780 | 0.966880 | 5 | 172.664 | 2.455870 |
| 6 | 81.5736 | 1.160256 | 6 | 207.197 | 2.947044 |
| 7 | 95.1692 | 1.353632 | 7 | 241.730 | 3.438218 |
| 8 | 108.7648 | 1.547008 | 8 | 276.262 | 3.929392 |
| 9 | 122.3604 | 1.740384 | 9 | 310.795 | 4.420566 |
| 10 | 135.9560 | 1.933760 | 10 | 345.328 | 4.911740 |

| Cms. of H ₂ O. | Pressure in grams per sq. cm. | Pressure in pounds per sq. inch. | Inches of H ₂ O. | Pressure in grams per sq. cm. | Pressure in pounds per sq. inch. |
|---------------------------|-------------------------------|----------------------------------|-----------------------------|-------------------------------|----------------------------------|
| 1 | 1 | 0.0142234 | 1 | 2.54 | 0.036127 |
| 2 | 2 | 0.0284468 | 2 | 5.08 | 0.072255 |
| 3 | 3 | 0.0426702 | 3 | 7.62 | 0.108382 |
| 4 | 4 | 0.0568936 | 4 | 10.16 | 0.144510 |
| 5 | 5 | 0.0711170 | 5 | 12.70 | 0.180637 |
| 6 | 6 | 0.0853404 | 6 | 15.24 | 0.216764 |
| 7 | 7 | 0.0995638 | 7 | 17.78 | 0.252892 |
| 8 | 8 | 0.1137872 | 8 | 20.32 | 0.289019 |
| 9 | 9 | 0.1280106 | 9 | 22.86 | 0.325147 |
| 10 | 10 | 0.1422340 | 10 | 25.40 | 0.361274 |

SMITHSONIAN TABLES.

REDUCTION OF BAROMETRIC HEIGHT TO STANDARD TEMPERATURE *

| Corrections for brass scale and English measure. | | Corrections for brass scale and metric measure. | | Corrections for glass scale and metric measure. | |
|--|---------------------------------|---|-----------------------------|---|-----------------------------|
| Height of barometer in inches. | α in inches for temp. F. | Height of barometer in mm. | α in mm for temp. C. | Height of barometer in mm. | α in mm for temp. C. |
| 15.0 | .00135 | 400 | .0651 | 50 | .0086 |
| 16.0 | .00145 | 410 | .0668 | 100 | .0172 |
| 17.0 | .00154 | 420 | .0684 | 150 | .0258 |
| 17.5 | .00158 | 430 | .0700 | 200 | .0345 |
| 18.0 | .00163 | 440 | .0716 | 250 | .0431 |
| 18.5 | .00167 | 450 | .0732 | 300 | .0517 |
| 19.0 | .00172 | 460 | .0749 | 350 | .0603 |
| 19.5 | .00176 | 470 | .0765 | | |
| | | 480 | .0781 | 400 | .0689 |
| 20.0 | .00181 | 490 | .0797 | 450 | .0775 |
| 20.5 | .00185 | | | 500 | .0861 |
| 21.0 | .00190 | 500 | .0813 | 520 | .0895 |
| 21.5 | .00194 | 510 | .0830 | 540 | .0930 |
| 22.0 | .00199 | 520 | .0846 | 560 | .0965 |
| 22.5 | .00203 | 530 | .0862 | 580 | .0999 |
| 23.0 | .00208 | 540 | .0878 | | |
| 23.5 | .00212 | 550 | .0894 | 600 | .1034 |
| | | 560 | .0911 | 610 | .1051 |
| 24.0 | .00217 | 570 | .0927 | 620 | .1068 |
| 24.5 | .00221 | 580 | .0943 | 630 | .1085 |
| 25.0 | .00226 | 590 | .0959 | 640 | .1103 |
| 25.5 | .00231 | | | 650 | .1120 |
| 26.0 | .00236 | 600 | .0975 | 660 | .1137 |
| 26.5 | .00240 | 610 | .0992 | | |
| 27.0 | .00245 | 620 | .1008 | 670 | .1154 |
| 27.5 | .00249 | 630 | .1024 | 680 | .1172 |
| | | 640 | .1040 | 690 | .1189 |
| 28.0 | .00254 | 650 | .1056 | 700 | .1206 |
| 28.5 | .00258 | 660 | .1073 | 710 | .1223 |
| 29.0 | .00263 | 670 | .1089 | 720 | .1240 |
| 29.2 | .00265 | 680 | .1105 | 730 | .1258 |
| 29.4 | .00267 | 690 | .1121 | | |
| 29.6 | .00268 | | | 740 | .1275 |
| 29.8 | .00270 | 700 | .1137 | 750 | .1292 |
| 30.0 | .00272 | 710 | .1154 | 760 | .1309 |
| | | 720 | .1170 | 770 | .1327 |
| 30.2 | .00274 | 730 | .1186 | 780 | .1344 |
| 30.4 | .00276 | 740 | .1202 | 790 | .1361 |
| 30.6 | .00277 | 750 | .1218 | 800 | .1378 |
| 30.8 | .00279 | 760 | .1235 | | |
| 31.0 | .00281 | 770 | .1251 | 850 | .1464 |
| 31.2 | .00283 | 780 | .1267 | 900 | .1551 |
| 31.4 | .00285 | 790 | .1283 | 950 | .1639 |
| 31.6 | .00287 | 800 | .1299 | 1000 | .1725 |

*The height of the barometer is affected by the relative thermal expansion of the mercury and the glass, in the case of instruments graduated on the glass tube, and by the relative expansion of the mercury and the metallic inclosing case, usually of brass, in the case of instruments graduated on the brass case. This relative expansion is practically proportional to the first power of the temperature. The above tables of values of the coefficient of relative expansion will be found to give corrections almost identical with those given in the International Meteorological Tables. The numbers tabulated under α are the values of α in the equation $H_t = H'_t - \alpha(t' - t)$ where H_t is the height at the standard temperature, H'_t the observed height at the temperature t' , and $\alpha(t' - t)$ the correction for temperature. The standard temperature is 0°C for the metric system and 28°F . for the English system. The English barometer is correct for the temperature of melting ice at a temperature of approximately 28°F , because of the fact that the brass scale is graduated so as to be standard at 62°F , while mercury has the standard density at 32°F .

EXAMPLE.—A barometer having a brass scale gave $H = 765$ mm at 25°C ; required, the corresponding reading at 0°C . Here the value of α is the mean of .1235 and .1251, or .1243; $\therefore \alpha(t' - t) = .1243 \times 25 = 3.11$. Hence $H_0 = 765 - 3.11 = 761.89$.

N. B.—Although α is here given to three and sometimes to four significant figures, it is seldom worth while to use more than the nearest two-figure number. In fact, all barometers have not the same values for α , and when great accuracy is wanted the proper coefficients have to be determined by experiment.

SMITHSONIAN TABLES.

REDUCTION OF BAROMETER TO STANDARD GRAVITY

Free-air Altitude Term. Correction to be subtracted.

The correction to reduce the barometer to sea-level is $(g_1 - g)/g \times B$ where B is the barometer reading and g and g_1 the value of gravity at sea-level and the place of observation respectively. The following values were computed for free-air values of gravity g_1 (Table 706). It has been customary to assume for mountain stations that the value of g_1 = say about $\frac{1}{2}$ the free-air value, but a comparison of modern determinations of g_1 in this country shows that little reliance can be placed on such an assumption. Where g_1 is known its value should be used in the above correction term. (See Tables 707 to 709. Similarly for the latitude term, see succeeding tables, the true value of g should be used if known; the succeeding tables are based on the theoretical values, Table 706.)

| Height above sea-level. | $g_1 - g$ | Observed height of barometer in millimeters. | | | | | | | | | | |
|---|-----------|---|------|------|------|------|---|------|------|------|-----------|-------------------------------|
| | | 400 | 450 | 500 | 550 | 600 | 650 | 700 | 750 | 800 | | |
| meters. | | | | | | | | | | | | |
| 100 | 0.031 | Correction in mm to be subtracted for height above sea-level in first column and barometer reading in the top line. | | | | | | .02 | .02 | .02 | — | |
| 200 | 0.062 | | | | | | .04 | .05 | .05 | — | | |
| 300 | 0.093 | | | | | | .07 | .07 | .07 | — | | |
| 400 | 0.123 | | | | | | .09 | .10 | .10 | — | | |
| 500 | 0.154 | — | — | — | — | — | .11 | .12 | .13 | — | | |
| 600 | 0.185 | — | — | — | — | .12 | .13 | .14 | — | — | | |
| 700 | 0.216 | — | — | — | — | .14 | .15 | .16 | — | — | | |
| 800 | 0.247 | — | — | — | — | .16 | .18 | .19 | — | — | | |
| 900 | 0.278 | — | — | — | — | .18 | .20 | .22 | — | — | | |
| 1000 | 0.309 | — | — | — | .18 | .19 | .20 | .22 | .24 | — | | |
| 1100 | 0.339 | — | — | — | .19 | .21 | .22 | .24 | — | — | | |
| 1200 | 0.370 | — | — | — | .21 | .23 | .24 | .26 | — | — | | |
| 1300 | 0.401 | — | — | — | .22 | .24 | .26 | .29 | — | — | | |
| 1400 | 0.432 | — | — | — | .24 | .26 | .28 | .31 | — | — | | |
| 1500 | 0.463 | — | — | .24 | .26 | .28 | .30 | .33 | — | — | | |
| 1600 | 0.494 | — | — | .25 | .28 | .30 | .32 | — | — | — | | |
| 1700 | 0.525 | — | — | .27 | .30 | .32 | .34 | — | — | — | | |
| 1800 | 0.555 | — | — | .28 | .31 | .34 | .36 | — | — | .020 | | |
| 1900 | 0.586 | — | — | .30 | .33 | .36 | .39 | — | — | .019 | | |
| 2000 | 0.617 | — | .28 | .31 | .34 | .38 | .41 | — | .021 | .019 | | |
| 2100 | 0.648 | — | .30 | .33 | .36 | .40 | — | — | .021 | .018 | | |
| 2200 | 0.679 | — | .31 | .35 | .38 | .41 | — | — | .020 | .017 | | |
| 2300 | 0.710 | — | .32 | .36 | .40 | .43 | — | .021 | .019 | .017 | | |
| 2400 | 0.740 | — | .34 | .38 | .42 | .45 | — | .021 | .018 | .016 | | |
| 2500 | 0.771 | .31 | .35 | .39 | .43 | .47 | — | .020 | .018 | .015 | | |
| 2600 | 0.802 | .33 | .37 | .41 | — | — | .021 | .019 | .017 | .015 | | |
| 2700 | 0.833 | .34 | .38 | .42 | — | — | .020 | .018 | .016 | .014 | | |
| 2800 | 0.864 | .35 | .40 | .44 | — | — | .019 | .017 | .015 | .013 | | |
| 2900 | 0.895 | .36 | .41 | .46 | — | .020 | .018 | .016 | .015 | .013 | | |
| 3000 | 0.926 | .38 | .42 | .47 | — | .019 | .017 | .016 | .014 | .012 | | |
| 3100 | 0.957 | .39 | .44 | — | — | .018 | .016 | .015 | .013 | — | | |
| 3200 | 0.988 | .40 | .46 | — | — | .017 | .015 | .014 | .012 | — | | |
| 3300 | 1.019 | .42 | .47 | — | .017 | .016 | .014 | .013 | — | — | | |
| 3400 | 1.049 | .43 | .48 | — | .016 | .015 | .013 | .012 | — | — | | |
| 3500 | 1.080 | .44 | .49 | — | .015 | .014 | .012 | .011 | — | — | | |
| 3600 | 1.111 | .45 | — | — | .014 | .013 | .011 | — | — | — | | |
| 3700 | 1.142 | .46 | — | — | .013 | .012 | .011 | — | — | — | | |
| 3800 | 1.173 | .48 | — | .012 | .011 | .011 | .010 | — | — | — | | |
| 3900 | 1.204 | .49 | — | .011 | .010 | .010 | — | — | — | — | | |
| 4000 | 1.235 | .50 | — | .010 | .009 | .009 | — | — | — | — | | |
| — | — | — | .008 | .008 | .007 | — | Corrections in in. to be subtracted for height above sea-level in last column and barometer reading in bot- tom line. | | | | .0092 | |
| — | — | .006 | .005 | .005 | .004 | — | | | | | .0062 | |
| — | — | .003 | .003 | .003 | — | — | | | | | .0031 | |
| | | | | | | | | | | | | feet. |
| | | 30 | 28 | 26 | 24 | 22 | 20 | 18 | 16 | 14 | $g_1 - g$ | |
| Observed height of barometer in inches. | | | | | | | | | | | | Height above sea-level. |

REDUCTION OF BAROMETER TO STANDARD GRAVITY *

METRIC MEASURES

From Latitude 0° to 45°, the Correction is to be Subtracted.

| Latitude | 520 | 540 | 560 | 580 | 600 | 620 | 640 | 660 | 680 | 700 | 720 | 740 | 760 | 780 |
|----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| 0 | -1.39 | -1.45 | -1.50 | -1.55 | -1.61 | -1.66 | -1.71 | -1.77 | -1.82 | -1.87 | -1.93 | -1.98 | -2.04 | -2.09 |
| 5 | -1.37 | -1.42 | -1.48 | -1.53 | -1.58 | -1.64 | -1.69 | -1.74 | -1.79 | -1.85 | -1.90 | -1.95 | -2.00 | -2.06 |
| 6 | 1.36 | 1.42 | 1.47 | 1.52 | 1.57 | 1.63 | 1.68 | 1.73 | 1.78 | 1.83 | 1.89 | 1.94 | 1.99 | 2.04 |
| 7 | 1.35 | 1.40 | 1.46 | 1.51 | 1.56 | 1.61 | 1.66 | 1.72 | 1.77 | 1.82 | 1.87 | 1.92 | 1.98 | 2.03 |
| 8 | 1.34 | 1.39 | 1.44 | 1.49 | 1.55 | 1.60 | 1.65 | 1.70 | 1.75 | 1.80 | 1.85 | 1.91 | 1.96 | 2.01 |
| 9 | 1.33 | 1.38 | 1.43 | 1.48 | 1.53 | 1.58 | 1.63 | 1.68 | 1.73 | 1.78 | 1.84 | 1.89 | 1.94 | 1.99 |
| 10 | -1.31 | -1.36 | -1.41 | -1.46 | -1.51 | -1.56 | -1.61 | -1.66 | -1.71 | -1.76 | -1.81 | -1.86 | -1.92 | -1.97 |
| 11 | 1.29 | 1.34 | 1.39 | 1.44 | 1.49 | 1.54 | 1.59 | 1.64 | 1.69 | 1.74 | 1.79 | 1.84 | 1.89 | 1.94 |
| 12 | 1.27 | 1.32 | 1.37 | 1.42 | 1.47 | 1.52 | 1.57 | 1.62 | 1.67 | 1.72 | 1.76 | 1.81 | 1.86 | 1.91 |
| 13 | 1.25 | 1.30 | 1.35 | 1.40 | 1.45 | 1.50 | 1.54 | 1.59 | 1.64 | 1.69 | 1.74 | 1.78 | 1.83 | 1.88 |
| 14 | 1.23 | 1.28 | 1.33 | 1.38 | 1.42 | 1.47 | 1.52 | 1.56 | 1.61 | 1.66 | 1.71 | 1.75 | 1.80 | 1.85 |
| 15 | -1.21 | -1.26 | -1.30 | -1.35 | -1.40 | -1.44 | -1.49 | -1.54 | -1.58 | -1.63 | -1.67 | -1.72 | -1.77 | -1.81 |
| 16 | 1.19 | 1.23 | 1.28 | 1.32 | 1.37 | 1.41 | 1.46 | 1.50 | 1.55 | 1.60 | 1.64 | 1.69 | 1.73 | 1.78 |
| 17 | 1.16 | 1.20 | 1.25 | 1.29 | 1.34 | 1.38 | 1.43 | 1.47 | 1.52 | 1.56 | 1.60 | 1.65 | 1.69 | 1.74 |
| 18 | 1.13 | 1.18 | 1.22 | 1.26 | 1.31 | 1.35 | 1.39 | 1.44 | 1.48 | 1.52 | 1.57 | 1.61 | 1.65 | 1.70 |
| 19 | 1.10 | 1.15 | 1.19 | 1.23 | 1.27 | 1.32 | 1.36 | 1.40 | 1.44 | 1.48 | 1.53 | 1.57 | 1.61 | 1.65 |
| 20 | -1.07 | -1.11 | -1.16 | -1.20 | -1.24 | -1.28 | -1.32 | -1.36 | -1.40 | -1.44 | -1.49 | -1.53 | -1.57 | -1.61 |
| 21 | 1.04 | 1.08 | 1.12 | 1.16 | 1.20 | 1.24 | 1.28 | 1.32 | 1.36 | 1.40 | 1.44 | 1.48 | 1.52 | 1.56 |
| 22 | 1.01 | 1.05 | 1.09 | 1.13 | 1.16 | 1.20 | 1.24 | 1.28 | 1.32 | 1.36 | 1.40 | 1.44 | 1.48 | 1.51 |
| 23 | 0.98 | 1.01 | 1.05 | 1.09 | 1.13 | 1.16 | 1.20 | 1.24 | 1.28 | 1.31 | 1.35 | 1.39 | 1.43 | 1.46 |
| 24 | 0.94 | 0.98 | 1.01 | 1.05 | 1.08 | 1.12 | 1.16 | 1.19 | 1.23 | 1.27 | 1.30 | 1.34 | 1.37 | 1.41 |
| 25 | -0.90 | -0.94 | -0.97 | -1.01 | -1.04 | -1.08 | -1.11 | -1.15 | -1.18 | -1.22 | -1.25 | -1.29 | -1.32 | -1.36 |
| 26 | 0.87 | 0.90 | 0.93 | 0.97 | 1.00 | 1.03 | 1.07 | 1.10 | 1.13 | 1.17 | 1.20 | 1.23 | 1.27 | 1.30 |
| 27 | 0.83 | 0.86 | 0.89 | 0.92 | 0.96 | 0.99 | 1.02 | 1.05 | 1.08 | 1.12 | 1.15 | 1.18 | 1.21 | 1.24 |
| 28 | 0.79 | 0.82 | 0.85 | 0.88 | 0.91 | 0.94 | 0.97 | 1.00 | 1.03 | 1.06 | 1.09 | 1.12 | 1.15 | 1.18 |
| 29 | 0.75 | 0.78 | 0.81 | 0.84 | 0.86 | 0.89 | 0.92 | 0.95 | 0.98 | 1.01 | 1.04 | 1.07 | 1.10 | 1.12 |
| 30 | -0.71 | -0.74 | -0.76 | -0.79 | -0.82 | -0.85 | -0.87 | -0.90 | -0.93 | -0.95 | -0.98 | -1.01 | -1.04 | -1.06 |
| 31 | 0.67 | 0.69 | 0.72 | 0.74 | 0.77 | 0.80 | 0.82 | 0.85 | 0.87 | 0.90 | 0.92 | 0.95 | 0.98 | 1.00 |
| 32 | 0.62 | 0.65 | 0.67 | 0.70 | 0.72 | 0.74 | 0.77 | 0.79 | 0.82 | 0.84 | 0.86 | 0.89 | 0.91 | 0.94 |
| 33 | 0.58 | 0.60 | 0.63 | 0.65 | 0.67 | 0.69 | 0.72 | 0.74 | 0.76 | 0.78 | 0.80 | 0.83 | 0.85 | 0.87 |
| 34 | 0.54 | 0.56 | 0.58 | 0.60 | 0.62 | 0.64 | 0.66 | 0.68 | 0.70 | 0.72 | 0.74 | 0.76 | 0.79 | 0.81 |
| 35 | -0.49 | -0.51 | -0.53 | -0.55 | -0.57 | -0.59 | -0.61 | -0.63 | -0.64 | -0.66 | -0.68 | -0.70 | -0.72 | -0.74 |
| 36 | 0.45 | 0.46 | 0.48 | 0.50 | 0.52 | 0.53 | 0.55 | 0.57 | 0.58 | 0.60 | 0.62 | 0.64 | 0.65 | 0.67 |
| 37 | 0.40 | 0.42 | 0.43 | 0.45 | 0.46 | 0.48 | 0.49 | 0.51 | 0.52 | 0.54 | 0.56 | 0.57 | 0.59 | 0.60 |
| 38 | 0.36 | 0.37 | 0.38 | 0.40 | 0.41 | 0.42 | 0.44 | 0.45 | 0.46 | 0.48 | 0.49 | 0.51 | 0.52 | 0.53 |
| 39 | 0.31 | 0.32 | 0.33 | 0.34 | 0.36 | 0.37 | 0.38 | 0.39 | 0.40 | 0.42 | 0.43 | 0.44 | 0.45 | 0.46 |
| 40 | -0.26 | -0.27 | -0.28 | -0.29 | -0.30 | -0.31 | -0.32 | -0.33 | -0.34 | -0.35 | -0.36 | -0.37 | -0.38 | -0.39 |
| 41 | 0.21 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 | 0.30 | 0.31 | 0.32 |
| 42 | 0.17 | 0.17 | 0.18 | 0.19 | 0.19 | 0.20 | 0.21 | 0.21 | 0.22 | 0.22 | 0.23 | 0.24 | 0.24 | 0.25 |
| 43 | 0.12 | 0.12 | 0.13 | 0.13 | 0.14 | 0.14 | 0.15 | 0.15 | 0.16 | 0.16 | 0.16 | 0.17 | 0.17 | 0.18 |
| 44 | 0.07 | 0.07 | 0.08 | 0.08 | 0.08 | 0.08 | 0.09 | 0.09 | 0.09 | 0.10 | 0.10 | 0.10 | 0.10 | 0.11 |
| 45 | -0.02 | -0.02 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.04 |

* "Smithsonian Meteorological Tables."

REDUCTION OF BAROMETER TO STANDARD GRAVITY *

METRIC MEASURES

From Latitude 46° to 90°, the Correction is to be Added.

| Latitude | 520 | 540 | 560 | 580 | 600 | 620 | 640 | 660 | 680 | 700 | 720 | 740 | 760 | 780 |
|----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| 45 | -0.02 | -0.02 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.04 |
| 46 | +0.02 | +0.03 | +0.03 | +0.03 | +0.03 | +0.03 | +0.03 | +0.03 | +0.03 | +0.03 | +0.03 | +0.03 | +0.04 | +0.04 |
| 47 | 0.07 | 0.08 | 0.08 | 0.08 | 0.08 | 0.09 | 0.09 | 0.09 | 0.09 | 0.10 | 0.10 | 0.10 | 0.10 | 0.11 |
| 48 | 0.12 | 0.12 | 0.13 | 0.13 | 0.14 | 0.14 | 0.15 | 0.15 | 0.16 | 0.16 | 0.17 | 0.17 | 0.18 | 0.18 |
| 49 | 0.17 | 0.17 | 0.18 | 0.19 | 0.19 | 0.20 | 0.21 | 0.21 | 0.22 | 0.23 | 0.23 | 0.24 | 0.25 | 0.25 |
| 50 | 0.22 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 | 0.31 | 0.31 | 0.32 |
| 51 | +0.26 | +0.27 | +0.28 | +0.29 | +0.30 | +0.31 | +0.32 | +0.33 | +0.34 | +0.35 | +0.36 | +0.37 | +0.38 | +0.39 |
| 52 | 0.31 | 0.32 | 0.33 | 0.34 | 0.36 | 0.37 | 0.38 | 0.39 | 0.40 | 0.42 | 0.43 | 0.44 | 0.45 | 0.46 |
| 53 | 0.36 | 0.37 | 0.38 | 0.40 | 0.41 | 0.42 | 0.44 | 0.45 | 0.46 | 0.48 | 0.49 | 0.51 | 0.52 | 0.53 |
| 54 | 0.40 | 0.42 | 0.43 | 0.45 | 0.46 | 0.48 | 0.49 | 0.51 | 0.52 | 0.54 | 0.56 | 0.57 | 0.59 | 0.60 |
| 55 | 0.45 | 0.46 | 0.48 | 0.50 | 0.52 | 0.53 | 0.55 | 0.57 | 0.58 | 0.60 | 0.62 | 0.64 | 0.65 | 0.67 |
| 56 | +0.49 | +0.51 | +0.53 | +0.55 | +0.57 | +0.59 | +0.60 | +0.62 | +0.64 | +0.66 | +0.68 | +0.70 | +0.72 | +0.74 |
| 57 | 0.54 | 0.56 | 0.58 | 0.60 | 0.62 | 0.64 | 0.66 | 0.68 | 0.70 | 0.72 | 0.74 | 0.76 | 0.78 | 0.80 |
| 58 | 0.58 | 0.60 | 0.62 | 0.65 | 0.67 | 0.69 | 0.71 | 0.74 | 0.76 | 0.78 | 0.80 | 0.82 | 0.85 | 0.87 |
| 59 | 0.62 | 0.65 | 0.67 | 0.69 | 0.72 | 0.74 | 0.77 | 0.79 | 0.81 | 0.84 | 0.86 | 0.89 | 0.91 | 0.93 |
| 60 | 0.66 | 0.69 | 0.72 | 0.74 | 0.77 | 0.79 | 0.82 | 0.84 | 0.87 | 0.89 | 0.92 | 0.94 | 0.97 | 1.00 |
| 61 | +0.71 | +0.73 | +0.76 | +0.79 | +0.81 | +0.84 | +0.87 | +0.89 | +0.92 | +0.95 | +0.98 | +1.00 | +1.03 | +1.06 |
| 62 | 0.74 | 0.77 | 0.80 | 0.83 | 0.85 | 0.88 | 0.91 | 0.94 | 0.97 | 1.00 | 1.02 | 1.05 | 1.08 | 1.11 |
| 63 | 0.78 | 0.81 | 0.85 | 0.88 | 0.91 | 0.94 | 0.97 | 1.00 | 1.03 | 1.06 | 1.09 | 1.12 | 1.15 | 1.18 |
| 64 | 0.82 | 0.85 | 0.89 | 0.92 | 0.95 | 0.98 | 1.01 | 1.04 | 1.08 | 1.11 | 1.14 | 1.17 | 1.20 | 1.23 |
| 65 | 0.86 | 0.89 | 0.93 | 0.96 | 0.99 | 1.03 | 1.06 | 1.09 | 1.13 | 1.16 | 1.19 | 1.22 | 1.26 | 1.29 |
| 66 | +0.90 | +0.93 | +0.97 | +1.00 | +1.04 | +1.07 | +1.10 | +1.14 | +1.17 | +1.21 | +1.24 | +1.28 | +1.31 | +1.35 |
| 67 | 0.93 | 0.97 | 1.00 | 1.04 | 1.08 | 1.11 | 1.15 | 1.18 | 1.22 | 1.25 | 1.29 | 1.33 | 1.36 | 1.40 |
| 68 | 0.97 | 1.00 | 1.04 | 1.08 | 1.11 | 1.15 | 1.19 | 1.23 | 1.26 | 1.30 | 1.34 | 1.37 | 1.41 | 1.45 |
| 69 | 1.00 | 1.04 | 1.08 | 1.11 | 1.15 | 1.19 | 1.23 | 1.27 | 1.31 | 1.34 | 1.38 | 1.42 | 1.46 | 1.50 |
| 70 | 1.03 | 1.07 | 1.11 | 1.15 | 1.19 | 1.23 | 1.27 | 1.31 | 1.35 | 1.39 | 1.43 | 1.47 | 1.51 | 1.55 |
| 71 | +1.06 | +1.10 | +1.14 | +1.18 | +1.22 | +1.26 | +1.31 | +1.35 | +1.39 | +1.43 | +1.47 | +1.51 | +1.55 | +1.59 |
| 72 | 1.09 | 1.13 | 1.17 | 1.22 | 1.26 | 1.30 | 1.34 | 1.38 | 1.42 | 1.47 | 1.51 | 1.55 | 1.59 | 1.63 |
| 73 | 1.12 | 1.16 | 1.20 | 1.25 | 1.29 | 1.33 | 1.37 | 1.42 | 1.46 | 1.50 | 1.55 | 1.59 | 1.63 | 1.67 |
| 74 | 1.14 | 1.19 | 1.23 | 1.28 | 1.32 | 1.36 | 1.41 | 1.45 | 1.50 | 1.54 | 1.58 | 1.63 | 1.67 | 1.72 |
| 75 | 1.17 | 1.21 | 1.26 | 1.30 | 1.35 | 1.39 | 1.44 | 1.48 | 1.53 | 1.57 | 1.62 | 1.66 | 1.71 | 1.75 |
| 76 | +1.19 | +1.24 | +1.28 | +1.33 | +1.37 | +1.42 | +1.47 | +1.51 | +1.56 | +1.60 | +1.65 | +1.70 | +1.74 | +1.79 |
| 77 | 1.21 | 1.26 | 1.31 | 1.35 | 1.40 | 1.45 | 1.49 | 1.54 | 1.59 | 1.63 | 1.68 | 1.73 | 1.77 | 1.82 |
| 78 | 1.23 | 1.28 | 1.33 | 1.38 | 1.42 | 1.47 | 1.52 | 1.57 | 1.61 | 1.66 | 1.71 | 1.76 | 1.80 | 1.85 |
| 79 | 1.25 | 1.30 | 1.35 | 1.40 | 1.45 | 1.49 | 1.54 | 1.59 | 1.64 | 1.69 | 1.73 | 1.78 | 1.83 | 1.88 |
| 80 | 1.27 | 1.32 | 1.37 | 1.42 | 1.47 | 1.51 | 1.56 | 1.61 | 1.66 | 1.71 | 1.76 | 1.81 | 1.86 | 1.90 |
| 81 | +1.29 | +1.33 | +1.38 | +1.43 | +1.48 | +1.53 | +1.58 | +1.63 | +1.68 | +1.73 | +1.78 | +1.83 | +1.88 | +1.93 |
| 82 | 1.30 | 1.35 | 1.40 | 1.45 | 1.50 | 1.55 | 1.60 | 1.65 | 1.70 | 1.75 | 1.80 | 1.85 | 1.90 | 1.95 |
| 83 | 1.31 | 1.36 | 1.41 | 1.46 | 1.51 | 1.56 | 1.61 | 1.67 | 1.72 | 1.77 | 1.82 | 1.87 | 1.92 | 1.97 |
| 84 | 1.32 | 1.37 | 1.42 | 1.48 | 1.53 | 1.58 | 1.63 | 1.68 | 1.73 | 1.78 | 1.83 | 1.88 | 1.93 | 1.98 |
| 85 | 1.33 | 1.38 | 1.43 | 1.49 | 1.54 | 1.59 | 1.64 | 1.69 | 1.74 | 1.79 | 1.84 | 1.90 | 1.95 | 2.00 |
| 90 | +1.35 | +1.41 | +1.46 | +1.51 | +1.56 | +1.61 | +1.67 | +1.72 | +1.77 | +1.82 | +1.87 | +1.93 | +1.98 | +2.03 |

* "Smithsonian Meteorological Tables."

REDUCTION OF BAROMETER TO STANDARD GRAVITY *

ENGLISH MEASURES

From Latitude 0° to 45°, the Correction is to be Subtracted.

| Latitude | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 |
|----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. |
| 0 | 0.051 | 0.054 | 0.056 | 0.059 | 0.062 | 0.064 | 0.067 | 0.070 | 0.072 | 0.075 | 0.078 | 0.080 |
| 5 | 0.050 | 0.053 | 0.055 | 0.058 | 0.061 | 0.063 | 0.066 | 0.069 | 0.071 | 0.074 | 0.077 | 0.079 |
| 6 | 0.050 | 0.052 | 0.055 | 0.058 | 0.060 | 0.063 | 0.066 | 0.068 | 0.071 | 0.073 | 0.076 | 0.079 |
| 7 | 0.049 | 0.052 | 0.055 | 0.057 | 0.060 | 0.062 | 0.065 | 0.068 | 0.070 | 0.073 | 0.075 | 0.078 |
| 8 | 0.049 | 0.052 | 0.054 | 0.057 | 0.059 | 0.062 | 0.064 | 0.067 | 0.070 | 0.072 | 0.075 | 0.077 |
| 9 | 0.048 | 0.051 | 0.054 | 0.056 | 0.059 | 0.061 | 0.064 | 0.066 | 0.069 | 0.071 | 0.074 | 0.076 |
| 10 | 0.048 | 0.050 | 0.053 | 0.055 | 0.058 | 0.060 | 0.063 | 0.066 | 0.068 | 0.071 | 0.073 | 0.076 |
| 11 | 0.047 | 0.050 | 0.052 | 0.055 | 0.057 | 0.060 | 0.062 | 0.065 | 0.067 | 0.070 | 0.072 | 0.075 |
| 12 | 0.047 | 0.049 | 0.051 | 0.054 | 0.056 | 0.059 | 0.061 | 0.064 | 0.066 | 0.069 | 0.071 | 0.074 |
| 13 | 0.046 | 0.048 | 0.051 | 0.053 | 0.055 | 0.058 | 0.060 | 0.063 | 0.065 | 0.068 | 0.070 | 0.072 |
| 14 | 0.045 | 0.047 | 0.050 | 0.052 | 0.055 | 0.057 | 0.059 | 0.062 | 0.064 | 0.066 | 0.069 | 0.071 |
| 15 | 0.044 | 0.047 | 0.049 | 0.051 | 0.053 | 0.056 | 0.058 | 0.060 | 0.063 | 0.065 | 0.067 | 0.070 |
| 16 | 0.043 | 0.046 | 0.048 | 0.050 | 0.052 | 0.055 | 0.057 | 0.059 | 0.062 | 0.064 | 0.066 | 0.068 |
| 17 | 0.042 | 0.045 | 0.047 | 0.049 | 0.051 | 0.053 | 0.056 | 0.058 | 0.060 | 0.062 | 0.065 | 0.067 |
| 18 | 0.041 | 0.044 | 0.046 | 0.048 | 0.050 | 0.052 | 0.054 | 0.057 | 0.059 | 0.061 | 0.063 | 0.065 |
| 19 | 0.040 | 0.042 | 0.045 | 0.047 | 0.049 | 0.051 | 0.053 | 0.055 | 0.057 | 0.059 | 0.062 | 0.064 |
| 20 | 0.039 | 0.041 | 0.043 | 0.045 | 0.047 | 0.050 | 0.052 | 0.054 | 0.056 | 0.058 | 0.060 | 0.062 |
| 21 | 0.038 | 0.040 | 0.042 | 0.044 | 0.046 | 0.048 | 0.050 | 0.052 | 0.054 | 0.056 | 0.058 | 0.060 |
| 22 | 0.037 | 0.039 | 0.041 | 0.043 | 0.045 | 0.047 | 0.049 | 0.050 | 0.052 | 0.054 | 0.056 | 0.058 |
| 23 | 0.036 | 0.038 | 0.039 | 0.041 | 0.043 | 0.045 | 0.047 | 0.049 | 0.051 | 0.053 | 0.054 | 0.056 |
| 24 | 0.034 | 0.036 | 0.038 | 0.040 | 0.042 | 0.043 | 0.045 | 0.047 | 0.049 | 0.051 | 0.052 | 0.054 |
| 25 | 0.033 | 0.035 | 0.037 | 0.038 | 0.040 | 0.042 | 0.043 | 0.045 | 0.047 | 0.049 | 0.050 | 0.052 |
| 26 | 0.032 | 0.033 | 0.035 | 0.037 | 0.038 | 0.040 | 0.042 | 0.043 | 0.045 | 0.047 | 0.048 | 0.050 |
| 27 | 0.030 | 0.032 | 0.033 | 0.035 | 0.037 | 0.038 | 0.040 | 0.041 | 0.043 | 0.045 | 0.046 | 0.048 |
| 28 | 0.029 | 0.030 | 0.032 | 0.033 | 0.035 | 0.036 | 0.038 | 0.039 | 0.041 | 0.043 | 0.044 | 0.046 |
| 29 | 0.027 | 0.029 | 0.030 | 0.032 | 0.033 | 0.035 | 0.036 | 0.037 | 0.039 | 0.040 | 0.042 | 0.043 |
| 30 | 0.026 | 0.027 | 0.029 | 0.030 | 0.031 | 0.033 | 0.034 | 0.035 | 0.037 | 0.038 | 0.040 | 0.041 |
| 31 | 0.024 | 0.026 | 0.027 | 0.028 | 0.030 | 0.031 | 0.032 | 0.033 | 0.035 | 0.036 | 0.037 | 0.038 |
| 32 | 0.023 | 0.024 | 0.025 | 0.026 | 0.028 | 0.029 | 0.030 | 0.031 | 0.032 | 0.034 | 0.035 | 0.036 |
| 33 | 0.021 | 0.022 | 0.023 | 0.025 | 0.026 | 0.027 | 0.028 | 0.029 | 0.030 | 0.031 | 0.032 | 0.034 |
| 34 | 0.020 | 0.021 | 0.022 | 0.023 | 0.024 | 0.025 | 0.026 | 0.027 | 0.028 | 0.029 | 0.030 | 0.031 |
| 35 | 0.018 | 0.019 | 0.020 | 0.021 | 0.022 | 0.023 | 0.024 | 0.025 | 0.026 | 0.027 | 0.027 | 0.028 |
| 36 | 0.016 | 0.017 | 0.018 | 0.019 | 0.020 | 0.021 | 0.022 | 0.022 | 0.023 | 0.024 | 0.025 | 0.026 |
| 37 | 0.015 | 0.015 | 0.016 | 0.017 | 0.018 | 0.019 | 0.019 | 0.020 | 0.021 | 0.022 | 0.022 | 0.023 |
| 38 | 0.013 | 0.014 | 0.014 | 0.015 | 0.016 | 0.016 | 0.017 | 0.018 | 0.018 | 0.019 | 0.020 | 0.020 |
| 39 | 0.011 | 0.012 | 0.012 | 0.013 | 0.014 | 0.014 | 0.015 | 0.015 | 0.016 | 0.017 | 0.017 | 0.018 |
| 40 | 0.010 | 0.010 | 0.011 | 0.011 | 0.012 | 0.012 | 0.013 | 0.013 | 0.014 | 0.014 | 0.015 | 0.015 |
| 41 | 0.008 | 0.008 | 0.009 | 0.009 | 0.009 | 0.010 | 0.010 | 0.011 | 0.011 | 0.012 | 0.012 | 0.012 |
| 42 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.008 | 0.008 | 0.008 | 0.009 | 0.009 | 0.009 | 0.010 |
| 43 | 0.004 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 |
| 44 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 |
| 45 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |

* "Smithsonian Meteorological Tables."

REDUCTION OF BAROMETER TO STANDARD GRAVITY *

ENGLISH MEASURES

From Latitude 46° to 90° the Correction is to be Added.

| Latitude | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 |
|----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. |
| 45 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 |
| 46 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 |
| 47 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 |
| 48 | 0.004 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 |
| 49 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.008 | 0.008 | 0.008 | 0.009 | 0.009 | 0.009 | 0.010 |
| 50 | 0.008 | 0.008 | 0.009 | 0.009 | 0.010 | 0.010 | 0.010 | 0.011 | 0.011 | 0.012 | 0.012 | 0.012 |
| 51 | +0.010 | +0.010 | +0.011 | +0.011 | +0.012 | +0.012 | +0.013 | +0.013 | +0.014 | +0.014 | +0.015 | +0.015 |
| 52 | 0.011 | 0.012 | 0.012 | 0.013 | 0.014 | 0.014 | 0.015 | 0.015 | 0.016 | 0.016 | 0.017 | 0.018 |
| 53 | 0.013 | 0.014 | 0.014 | 0.015 | 0.016 | 0.016 | 0.017 | 0.018 | 0.018 | 0.019 | 0.020 | 0.020 |
| 54 | 0.015 | 0.015 | 0.016 | 0.017 | 0.018 | 0.019 | 0.019 | 0.020 | 0.021 | 0.022 | 0.022 | 0.023 |
| 55 | 0.016 | 0.017 | 0.018 | 0.019 | 0.020 | 0.021 | 0.021 | 0.022 | 0.023 | 0.024 | 0.025 | 0.026 |
| 56 | +0.018 | +0.019 | +0.020 | +0.021 | +0.022 | +0.023 | +0.024 | +0.024 | +0.026 | +0.026 | +0.027 | +0.028 |
| 57 | 0.020 | 0.021 | 0.022 | 0.023 | 0.024 | 0.025 | 0.026 | 0.027 | 0.028 | 0.029 | 0.030 | 0.031 |
| 58 | 0.021 | 0.022 | 0.023 | 0.025 | 0.026 | 0.027 | 0.028 | 0.029 | 0.030 | 0.031 | 0.032 | 0.033 |
| 59 | 0.023 | 0.024 | 0.025 | 0.026 | 0.028 | 0.029 | 0.030 | 0.031 | 0.032 | 0.033 | 0.035 | 0.036 |
| 60 | 0.024 | 0.026 | 0.027 | 0.028 | 0.029 | 0.031 | 0.032 | 0.033 | 0.034 | 0.036 | 0.037 | 0.038 |
| 61 | +0.026 | +0.027 | +0.028 | +0.030 | +0.031 | +0.033 | +0.034 | +0.035 | +0.037 | +0.038 | +0.039 | +0.041 |
| 62 | 0.027 | 0.029 | 0.030 | 0.032 | 0.033 | 0.034 | 0.036 | 0.037 | 0.039 | 0.040 | 0.042 | 0.043 |
| 63 | 0.029 | 0.030 | 0.032 | 0.033 | 0.035 | 0.036 | 0.038 | 0.039 | 0.041 | 0.042 | 0.044 | 0.045 |
| 64 | 0.030 | 0.032 | 0.033 | 0.035 | 0.036 | 0.038 | 0.040 | 0.041 | 0.043 | 0.044 | 0.046 | 0.047 |
| 65 | 0.031 | 0.033 | 0.035 | 0.036 | 0.038 | 0.040 | 0.041 | 0.043 | 0.045 | 0.046 | 0.048 | 0.050 |
| 66 | +0.033 | +0.034 | +0.036 | +0.038 | +0.040 | +0.041 | +0.043 | +0.045 | +0.047 | +0.048 | +0.050 | +0.052 |
| 67 | 0.034 | 0.036 | 0.038 | 0.039 | 0.041 | 0.043 | 0.045 | 0.047 | 0.048 | 0.050 | 0.052 | 0.054 |
| 68 | 0.035 | 0.037 | 0.039 | 0.041 | 0.043 | 0.045 | 0.046 | 0.048 | 0.050 | 0.052 | 0.054 | 0.056 |
| 69 | 0.036 | 0.038 | 0.040 | 0.042 | 0.044 | 0.046 | 0.048 | 0.050 | 0.052 | 0.054 | 0.056 | 0.058 |
| 70 | 0.038 | 0.040 | 0.042 | 0.044 | 0.046 | 0.048 | 0.050 | 0.052 | 0.053 | 0.055 | 0.057 | 0.059 |
| 71 | +0.039 | +0.041 | +0.043 | +0.045 | +0.047 | +0.049 | +0.051 | +0.053 | +0.055 | +0.057 | +0.059 | +0.061 |
| 72 | 0.040 | 0.042 | 0.044 | 0.046 | 0.048 | 0.050 | 0.052 | 0.054 | 0.057 | 0.059 | 0.061 | 0.063 |
| 73 | 0.041 | 0.043 | 0.045 | 0.047 | 0.049 | 0.052 | 0.054 | 0.056 | 0.058 | 0.060 | 0.062 | 0.064 |
| 74 | 0.042 | 0.044 | 0.046 | 0.048 | 0.051 | 0.053 | 0.055 | 0.057 | 0.059 | 0.062 | 0.064 | 0.066 |
| 75 | 0.043 | 0.045 | 0.047 | 0.049 | 0.052 | 0.054 | 0.056 | 0.058 | 0.061 | 0.063 | 0.065 | 0.067 |
| 76 | +0.044 | +0.046 | +0.048 | +0.050 | +0.053 | +0.055 | +0.057 | +0.060 | +0.062 | +0.064 | 0.066 | 0.069 |
| 77 | 0.044 | 0.047 | 0.049 | 0.051 | 0.054 | 0.056 | 0.058 | 0.061 | 0.063 | 0.065 | 0.068 | 0.070 |
| 78 | 0.045 | 0.047 | 0.050 | 0.052 | 0.055 | 0.057 | 0.059 | 0.062 | 0.064 | 0.066 | 0.069 | 0.071 |
| 79 | 0.046 | 0.048 | 0.051 | 0.053 | 0.055 | 0.058 | 0.060 | 0.063 | 0.065 | 0.067 | 0.070 | 0.072 |
| 80 | 0.046 | 0.049 | 0.051 | 0.054 | 0.056 | 0.059 | 0.061 | 0.063 | 0.066 | 0.068 | 0.071 | 0.073 |
| 81 | +0.047 | +0.049 | +0.052 | +0.054 | +0.057 | +0.059 | +0.062 | +0.064 | +0.067 | +0.069 | +0.072 | +0.074 |
| 82 | 0.047 | 0.050 | 0.052 | 0.055 | 0.057 | 0.060 | 0.062 | 0.065 | 0.067 | 0.070 | 0.072 | 0.075 |
| 83 | 0.048 | 0.050 | 0.053 | 0.056 | 0.058 | 0.061 | 0.063 | 0.066 | 0.068 | 0.071 | 0.073 | 0.076 |
| 84 | 0.048 | 0.051 | 0.053 | 0.056 | 0.059 | 0.061 | 0.064 | 0.066 | 0.069 | 0.071 | 0.074 | 0.076 |
| 85 | 0.049 | 0.051 | 0.054 | 0.056 | 0.059 | 0.061 | 0.064 | 0.067 | 0.069 | 0.072 | 0.074 | 0.077 |
| 90 | +0.049 | +0.052 | +0.055 | +0.057 | +0.060 | +0.062 | +0.065 | +0.068 | +0.070 | +0.073 | +0.075 | +0.078 |

* "Smithsonian Meteorological Tables."

TABLE 137.—Correction of the Barometer for Capillarity *

| 1. METRIC MEASURE. | | | | | | | | |
|-------------------------------|--|------|------|------|------|------|------|------|
| Diameter of tube in mm. | HEIGHT OF MENISCUS IN MILLIMETERS. | | | | | | | |
| | 0.4 | 0.6 | 0.8 | 1.0 | 1.2 | 1.4 | 1.6 | 1.8 |
| | Correction to be added in millimeters. | | | | | | | |
| 4 | 0.83 | 1.22 | 1.54 | 1.98 | 2.37 | — | — | — |
| 5 | .47 | 0.65 | 0.86 | 1.19 | 1.45 | 1.80 | — | — |
| 6 | .27 | .41 | .56 | 0.78 | 0.98 | 1.21 | 1.43 | — |
| 7 | .18 | .28 | .40 | .53 | .67 | 0.82 | 0.97 | 1.13 |
| 8 | — | .20 | .29 | .38 | .46 | .56 | .65 | 0.77 |
| 9 | — | .15 | .21 | .28 | .33 | .40 | .46 | .52 |
| 10 | — | — | .15 | .20 | .25 | .29 | .33 | .37 |
| 11 | — | — | .10 | .14 | .18 | .21 | .24 | .27 |
| 12 | — | — | .07 | .10 | .13 | .15 | .18 | .19 |
| 13 | — | — | .04 | .07 | .10 | .12 | .13 | .14 |

| 2. BRITISH MEASURE. | | | | | | | | |
|-----------------------------------|-----------------------------------|-------|-------|-------|-------|-------|-------|-------|
| Diameter of tube in inches. | HEIGHT OF MENISCUS IN INCHES. | | | | | | | |
| | .01 | .02 | .03 | .04 | .05 | .06 | .07 | .08 |
| | Correction to be added in inches. | | | | | | | |
| .15 | 0.024 | 0.047 | 0.069 | 0.092 | 0.116 | — | — | — |
| .20 | .011 | .022 | .033 | .045 | .059 | 0.078 | — | — |
| .25 | .006 | .012 | .019 | .028 | .037 | .047 | 0.059 | — |
| .30 | .004 | .008 | .013 | .018 | .023 | .029 | .035 | 0.042 |
| .35 | — | .005 | .008 | .012 | .015 | .018 | .022 | .026 |
| .40 | — | .004 | .006 | .008 | .010 | .012 | .014 | .016 |
| .45 | — | — | .003 | .005 | .007 | .008 | .010 | .012 |
| .50 | — | — | .002 | .004 | .005 | .006 | .006 | .007 |
| .55 | — | — | .001 | .002 | .003 | .004 | .005 | .005 |

* The first table is from Kohlrausch (Experimental Physics), and is based on the experiments of Mendeleff and Gutkowski (Jour. de Phys. Chem. Geo. Petersburg, 1877, or Wied. Beib. 1877). The second table has been calculated from the same data by conversion into inches and graphic interpolation.

TABLE 138.—Volume of Mercury Meniscus in Cu. Mm

| Height of meniscus. | Diameter of tube in mm | | | | | | | | | | |
|------------------------|------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| mm | | | | | | | | | | | |
| 1.6 | 157 | 185 | 214 | 245 | 280 | 318 | 356 | 398 | 444 | 492 | 541 |
| 1.8 | 181 | 211 | 244 | 281 | 320 | 362 | 407 | 455 | 507 | 560 | 616 |
| 2.0 | 206 | 240 | 278 | 319 | 362 | 409 | 460 | 513 | 571 | 631 | 694 |
| 2.2 | 233 | 271 | 313 | 358 | 406 | 459 | 515 | 574 | 637 | 704 | 776 |
| 2.4 | 262 | 303 | 350 | 400 | 454 | 511 | 573 | 639 | 708 | 781 | 859 |
| 2.6 | 291 | 338 | 388 | 444 | 503 | 565 | 633 | 706 | 782 | 862 | 948 |

Scheel und Heuse, Annalen der Physik, 33, p. 291, 1910.

PRESSURES AND THE BOILING POINT OF WATER

Useful when a boiling-point apparatus is used in the determination of heights.

(A) METRIC UNITS.

| Temperature. | .0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 |
|--------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| C | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| 80° | 355.40 | 356.84 | 358.28 | 359.73 | 361.19 | 362.65 | 364.11 | 365.58 | 367.06 | 368.54 |
| 81 | 370.03 | 371.52 | 373.01 | 374.51 | 376.02 | 377.53 | 379.05 | 380.57 | 382.09 | 383.62 |
| 82 | 385.16 | 386.70 | 388.25 | 389.80 | 391.36 | 392.92 | 394.49 | 396.06 | 397.64 | 399.22 |
| 83 | 400.81 | 402.40 | 404.00 | 405.61 | 407.22 | 408.83 | 410.45 | 412.08 | 413.71 | 415.35 |
| 84 | 416.99 | 418.64 | 420.29 | 421.95 | 423.61 | 425.28 | 426.95 | 428.64 | 430.32 | 432.01 |
| 85 | 433.71 | 435.41 | 437.12 | 438.83 | 440.55 | 442.28 | 444.01 | 445.75 | 447.49 | 449.24 |
| 86 | 450.99 | 452.75 | 454.51 | 456.28 | 458.06 | 459.84 | 461.63 | 463.42 | 465.22 | 467.03 |
| 87 | 468.84 | 470.66 | 472.48 | 474.31 | 476.14 | 477.99 | 479.83 | 481.68 | 483.54 | 485.41 |
| 88 | 487.28 | 489.16 | 491.04 | 492.93 | 494.82 | 496.72 | 498.63 | 500.54 | 502.46 | 504.39 |
| 89 | 506.32 | 508.26 | 510.20 | 512.15 | 514.11 | 516.07 | 518.04 | 520.01 | 521.99 | 523.98 |
| 90 | 525.97 | 527.97 | 529.98 | 531.99 | 534.01 | 536.04 | 538.07 | 540.11 | 542.15 | 544.21 |
| 91 | 546.26 | 548.33 | 550.40 | 552.48 | 554.56 | 556.65 | 558.75 | 560.85 | 562.96 | 565.08 |
| 92 | 567.20 | 569.33 | 571.47 | 573.61 | 575.76 | 577.92 | 580.08 | 582.25 | 584.43 | 586.61 |
| 93 | 588.80 | 591.00 | 593.20 | 595.41 | 597.63 | 599.86 | 602.09 | 604.33 | 606.57 | 608.82 |
| 94 | 611.08 | 613.35 | 615.62 | 617.90 | 620.19 | 622.48 | 624.79 | 627.09 | 629.41 | 631.73 |
| 95 | 634.06 | 636.40 | 638.74 | 641.09 | 643.45 | 645.82 | 648.19 | 650.57 | 652.96 | 655.35 |
| 96 | 657.75 | 660.16 | 662.58 | 665.00 | 667.43 | 669.87 | 672.32 | 674.77 | 677.23 | 679.70 |
| 97 | 682.18 | 684.66 | 687.15 | 689.65 | 692.15 | 694.67 | 697.19 | 699.71 | 702.25 | 704.79 |
| 98 | 707.35 | 709.90 | 712.47 | 715.04 | 717.63 | 720.22 | 722.81 | 725.42 | 728.03 | 730.65 |
| 99 | 733.28 | 735.92 | 738.56 | 741.21 | 743.87 | 746.54 | 749.22 | 751.90 | 754.59 | 757.29 |
| 100 | 760.00 | 762.72 | 765.44 | 768.17 | 770.91 | 773.66 | 776.42 | 779.18 | 781.95 | 784.73 |

(B) ENGLISH UNITS.

| Temperature. | .0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 |
|--------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| F. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 185° | 17.075 | 17.112 | 17.150 | 17.187 | 17.224 | 17.262 | 17.300 | 17.337 | 17.375 | 17.413 |
| 186 | 17.450 | 17.488 | 17.526 | 17.564 | 17.602 | 17.641 | 17.679 | 17.717 | 17.756 | 17.794 |
| 187 | 17.832 | 17.871 | 17.910 | 17.948 | 17.987 | 18.026 | 18.065 | 18.104 | 18.143 | 18.182 |
| 188 | 18.221 | 18.261 | 18.300 | 18.340 | 18.379 | 18.419 | 18.458 | 18.498 | 18.538 | 18.578 |
| 189 | 18.618 | 18.658 | 18.698 | 18.738 | 18.778 | 18.818 | 18.859 | 18.899 | 18.940 | 18.980 |
| 190 | 19.021 | 19.062 | 19.102 | 19.143 | 19.184 | 19.225 | 19.266 | 19.308 | 19.349 | 19.390 |
| 191 | 19.431 | 19.473 | 19.514 | 19.556 | 19.598 | 19.639 | 19.681 | 19.723 | 19.765 | 19.807 |
| 192 | 19.849 | 19.892 | 19.934 | 19.976 | 20.019 | 20.061 | 20.104 | 20.146 | 20.189 | 20.232 |
| 193 | 20.275 | 20.318 | 20.361 | 20.404 | 20.447 | 20.490 | 20.533 | 20.577 | 20.620 | 20.664 |
| 194 | 20.707 | 20.751 | 20.795 | 20.839 | 20.883 | 20.927 | 20.971 | 21.015 | 21.059 | 21.103 |
| 195 | 21.148 | 21.192 | 21.237 | 21.282 | 21.326 | 21.371 | 21.416 | 21.461 | 21.506 | 21.551 |
| 196 | 21.597 | 21.642 | 21.687 | 21.733 | 21.778 | 21.824 | 21.870 | 21.915 | 21.961 | 22.007 |
| 197 | 22.053 | 22.099 | 22.145 | 22.192 | 22.238 | 22.284 | 22.331 | 22.377 | 22.424 | 22.471 |
| 198 | 22.517 | 22.564 | 22.611 | 22.658 | 22.706 | 22.752 | 22.800 | 22.847 | 22.895 | 22.942 |
| 199 | 22.990 | 23.038 | 23.085 | 23.133 | 23.181 | 23.229 | 23.277 | 23.325 | 23.374 | 23.422 |
| 200 | 23.470 | 23.519 | 23.568 | 23.616 | 23.665 | 23.714 | 23.763 | 23.812 | 23.861 | 23.910 |
| 201 | 23.959 | 24.009 | 24.058 | 24.108 | 24.157 | 24.207 | 24.257 | 24.307 | 24.357 | 24.407 |
| 202 | 24.457 | 24.507 | 24.557 | 24.608 | 24.658 | 24.709 | 24.759 | 24.810 | 24.861 | 24.912 |
| 203 | 24.963 | 25.014 | 25.065 | 25.116 | 25.168 | 25.219 | 25.271 | 25.322 | 25.374 | 25.426 |
| 204 | 25.478 | 25.530 | 25.582 | 25.634 | 25.686 | 25.738 | 25.791 | 25.843 | 25.896 | 25.948 |
| 205 | 26.001 | 26.054 | 26.107 | 26.160 | 26.213 | 26.266 | 26.319 | 26.373 | 26.426 | 26.480 |
| 206 | 26.534 | 26.587 | 26.641 | 26.695 | 26.749 | 26.803 | 26.857 | 26.912 | 26.966 | 27.021 |
| 207 | 27.075 | 27.130 | 27.184 | 27.239 | 27.294 | 27.349 | 27.404 | 27.460 | 27.515 | 27.570 |
| 208 | 27.626 | 27.681 | 27.737 | 27.793 | 27.848 | 27.904 | 27.960 | 28.016 | 28.073 | 28.129 |
| 209 | 28.185 | 28.242 | 28.298 | 28.355 | 28.412 | 28.469 | 28.526 | 28.583 | 28.640 | 28.697 |
| 210 | 28.754 | 28.812 | 28.869 | 28.927 | 28.985 | 29.042 | 29.100 | 29.158 | 29.216 | 29.275 |
| 211 | 29.333 | 29.391 | 29.450 | 29.508 | 29.567 | 29.626 | 29.685 | 29.744 | 29.803 | 29.862 |
| 212 | 29.921 | 29.981 | 30.040 | 30.100 | 30.159 | 30.219 | 30.279 | 30.339 | 30.399 | 30.459 |
| 213 | 30.519 | 30.580 | 30.640 | 30.701 | 30.761 | 30.822 | 30.883 | 30.944 | 31.005 | 31.066 |
| 214 | 31.127 | 31.199 | 31.250 | 31.311 | 31.373 | 31.435 | 31.497 | 31.559 | 31.621 | 31.683 |

DETERMINATION OF HEIGHTS BY THE BAROMETER

$$\text{Formula of Babinet: } Z = C \frac{B_0 - B}{B_0 + B}$$

$$C \text{ (in feet)} = 52494 \left[1 + \frac{t_0 + t - t_1}{900} \right] \text{ English measures.}$$

$$C \text{ (in meters)} = 16000 \left[1 + \frac{2(t_0 + t)}{1000} \right] \text{ metric measures.}$$

In which Z = difference of height of two stations in feet or meters.

B_0, B = barometric readings at the lower and upper stations respectively, corrected for all sources of instrumental error.

t_0, t = air temperatures at the lower and upper stations respectively.

Values of C

| ENGLISH MEASURES. | | | METRIC MEASURES. | | |
|------------------------|-------|---------|------------------------|---------|---------|
| $\frac{1}{2}(t_0 + t)$ | C | Log C | $\frac{1}{2}(t_0 + t)$ | C | Log C |
| Fahr. | Feet. | | Cent. | Meters. | |
| 10° | 49928 | 4.69834 | -10° | 15360 | 4.18639 |
| 15 | 50511 | .70339 | -8 | 15488 | .19000 |
| | | | -6 | 15616 | .19357 |
| 20 | 51094 | 4.70837 | -4 | 15744 | .19712 |
| 25 | 51677 | .71330 | -2 | 15872 | .20063 |
| 30 | 52261 | 4.71818 | 0 | 16000 | 4.20412 |
| 35 | 52844 | .72300 | + 2 | 16128 | .20758 |
| | | | 4 | 16256 | .21101 |
| 40 | 53428 | 4.72777 | 6 | 16384 | .21442 |
| 45 | 54011 | .73248 | 8 | 16512 | .21780 |
| 50 | 54595 | 4.73715 | 10 | 16640 | 4.22115 |
| 55 | 55178 | .74177 | 12 | 16768 | .22448 |
| | | | 14 | 16896 | .22778 |
| 60 | 55761 | 4.74633 | 16 | 17024 | .23106 |
| 65 | 56344 | .75085 | 18 | 17152 | .23431 |
| 70 | 56927 | 4.75532 | 20 | 17280 | 4.23754 |
| 75 | 57511 | .75975 | 22 | 17408 | .24075 |
| | | | 24 | 17536 | .24393 |
| 80 | 58094 | 4.76413 | 26 | 17664 | .24709 |
| 85 | 58677 | .76847 | 28 | 17792 | .25022 |
| 90 | 59260 | 4.77276 | 30 | 17920 | 4.25334 |
| 95 | 59844 | .77702 | 32 | 18048 | .25643 |
| | | | 34 | 18176 | .25950 |
| 100 | 60427 | 4.78123 | 36 | 18304 | .26255 |

Values only approximate. Not good for great altitudes. A more accurate formula with corresponding tables may be found in Smithsonian Meteorological Tables.

SMITHSONIAN TABLES.

TABLES 141 AND 142
VELOCITY OF SOUND

TABLE 141.—Velocity of Sound in Solids

The velocity of sounds in solids varies as $\sqrt{E/\rho}$, where E is Young's modulus of elasticity and ρ the density. These constants for most materials vary through a somewhat wide range. The numbers can be taken only as rough approximations to the velocity in any particular case. When temperatures are not marked, between 10° and 20° is to be understood.

| Substance | t°C | m/sec. | Ref. | Substance | t°C | m/sec. | Ref. |
|-----------------------------|-----|--------|------|---------------------------|-----|--------|------|
| Ag hard | 20 | 2678 | 2 | Fe | 200 | 4720 | 2 |
| " " | 100 | 2640 | 2 | " " | 20 | 4990 | 3 |
| " " | 200 | 2480 | 2 | " " | 100 | 4920 | 3 |
| Al | | 5104 | 1 | " " | 200 | 4790 | 3 |
| Au hard | 20 | 1743 | 2 | Mg | | 4602 | 4 |
| " " | 100 | 1720 | 2 | Ni | | 4973 | 1 |
| Cd | | 2307 | 1 | Pb | | 1322 | 1 |
| Co | | 4724 | 1 | Pd | | 3150 | |
| Cu | 20 | 3560 | 2 | Pt | 20 | 2690 | 2 |
| " " | 100 | 3290 | 2 | " " | 100 | 2570 | 2 |
| " " | 200 | 2950 | 2 | " " | 200 | 2460 | 2 |
| Fe | 20 | 5130 | 2 | Sn | | 2500 | |
| " " | 100 | 5300 | 2 | Zn | | 3700 | |
| Ash, along the fiber . . . | | 4670 | 2 | Brick | | 3652 | 5 |
| " across the rings . . . | | 1390 | 2 | Clay rock | | 3480 | 6 |
| " along the rings . . . | | 1260 | 2 | Cork | | 500 | 7 |
| Beech, along the fiber . . | | 3340 | 2 | Granite | | 3950 | 6 |
| " across the rings . . . | | 1840 | 2 | Marble | | 3810 | 6 |
| " along the rings . . . | | 1415 | 2 | Paraffin | 15 | 1304 | 8 |
| Elm, along the fiber . . . | | 4120 | 2 | Slate | | 4510 | 6 |
| " across the rings . . . | | 1420 | 2 | Tallow | 16 | 390 | 8 |
| " along the rings . . . | | 1013 | 2 | Tuff | | 2850 | 6 |
| Fir, along the fiber . . . | | 4640 | 2 | Glass {from | | 5000 | |
| Mahogany, along the fiber . | | 4135 | 3 | " " " " {to | | 6000 | |
| Maple, along the fiber . . | | 4110 | 2 | Ivory | | 3013 | 9 |
| Oak, along the fiber . . . | | 3850 | 2 | Vul. rubber (black) . . . | 0 | 54 | 10 |
| Pine, along the fiber . . . | | 3320 | 2 | " " " " (red) | 50 | 31 | 10 |
| Poplar, along the fiber . . | | 4280 | 2 | " " " " " " | 0 | 69 | 10 |
| Sycamore, along the fiber . | | | | " " " " " " | 70 | 34 | 10 |
| | | | | Wax | 17 | 880 | 7 |
| | | | | " " " " " " | 28 | 441 | 7 |
| | | 4460 | 2 | | | | |

(1) Masson. (2) Wertheim. (3) Cast steel, Wertheim. (4) Melde. (5) Chladni. (6) Gray & Milne. (7) Stefan. (8) Warburg. (9) Ciccone & Campanile. (10) Exner.

TABLE 142.—Velocity of Sound in Water

| Substance | t°C | m/sec. | Ref. | Substance | t°C | m/sec. | Ref. |
|---------------------------|-----|--------|------|-------------------------|-----|--------|------|
| Water, air-free | 13 | 1441 | 1 | Water, sea: (continued) | | | |
| " dust-free | 19 | 1461 | 1 | Seine River | 60 | 1724 | 5 |
| " " | 31 | 1505 | 1 | N. Atlantic, | | | |
| " distilled | 20 | 1470 | 2 | 1228m deep | | 1520 | 6 |
| " 10% Na Cl sol. | 15 | 1470 | 1 | Carib. Sea, | | | |
| " 15% Na Cl sol. | 15 | 1530 | 1 | 338m deep | | 1478 | 6 |
| " 20% Na Cl sol. | 15 | 1650 | 1 | Carib. Sea, | | | |
| Water, sea: | | | | 1771m deep | | 1486 | 6 |
| 35.1% salt | 6 | 1474 | 3 | Pacific, 2962m deep . . | | 1493 | 6 |
| 35.2% " | 7 | 1477.4 | 3 | Explosive Waves: | | | |
| 35% " | 17 | 1510.4 | 3 | Gun Cotton, 9 oz. . . . | | 1732 | 7 |
| Lake Geneva | 9 | 1435 | 4 | " " " " 10 " | | 1775 | 7 |
| Seine River | 15 | 1437 | 5 | " " " " 18 " | | 1942 | 7 |
| " " | 30 | 1528 | 5 | " " " " 64 " | | 2013 | 7 |

(1) Dörsing, 1908. (2) Ionescu, 1924. (3) Wood, Browne, Cochran, 1923. (4) Colladon-Sturm. (5) Wertheim. (6) Heck & Service, 1924. (7) Threlfall, Adair, 1889, see Barstow's Sound, p. 518.

VELOCITY OF SOUND IN LIQUIDS AND GASES

For gases, the velocity of sound = $\sqrt{\gamma P/\rho}$, where P is the pressure, ρ the density, and γ the ratio of specific heat at constant pressure to that at constant volume. For moderate temperature changes $V_t = V_0(1 + \alpha t)$ where $\alpha = 0.00367$. The velocity of sound in tubes increases with the diameter up to the free-air value as a limit. The values from ammonia to methane inclusive, except for argon and helium, are for closed tubes.

| Substance | Temp. C | m/sec. | ft./sec. | Authority |
|-----------------------------------|---------|--------|----------|---|
| Liquids: Alcohol, 93% Ethyl..... | 18° | 1150 | 3772 | Cisman, 1926 |
| " Methyl..... | 19 | 1143 | 3750 | Busse, 1924 |
| Ammonia, .880..... | 16 | 1663 | 5456 | Dörsing, 1908 |
| Benzol..... | 17 | 1166 | 3826 | " |
| Carbon bisulphide..... | 18 | 1060 | 3477 | Cisman, 1926 |
| Chloroform..... | 15 | 983 | 3225 | Dörsing, 1908 |
| Ether..... | 0 | | 3386 | Mean |
| Mercury..... | 20 | 1407 | 4614 | Bungetziam |
| Turpentine oil..... | 15 | 1326 | 4351 | Dörsing, 1908 |
| Gases: Air, dry, 1 atmosphere.... | 0 | 331.7 | 1088 | Mean |
| " " 25 "..... | 0 | 332.0 | 1089 | " (Witkowski) |
| " " 50 "..... | 0 | 334.7 | 1098 | " |
| " " 100 "..... | 0 | 350.6 | 1150 | " |
| " "..... | 100 | 386 | 1266 | Stevens |
| " "..... | 500 | 553 | 1814 | " |
| " "..... | 1000 | 700 | 2297 | " |
| Ammonia..... | 0 | 415 | 1361 | Masson |
| Argon..... | 0 | 308 | 1010 | Mean |
| "..... | 1000 | 666 | 2184 | D, C, P, 1921 |
| Carbon monoxide..... | 0 | 337.1 | 1106 | Wullner |
| " "..... | 0 | 337.4 | 1107 | Dulong |
| " dioxide..... | 0 | 258.0 | 846 | Brockendahl, 1906 |
| " disulphide..... | 0 | 189 | 620 | Masson |
| Chlorine..... | 0 | 206.4 | 677 | Martini |
| "..... | 0 | 205.3 | 674 | Strecker |
| Ethylene..... | 0 | 314 | 1030 | Dulong |
| Helium..... | 0 | 971 | 3185 | Scheel, Heuse, 1919 |
| Hydrogen..... | 0 | 1269.5 | 4165 | Dulong |
| "..... | 0 | 1286.4 | 4221 | Zoch |
| Illuminating gas..... | 0 | 490.4 | 1609 | " |
| Methane..... | 0 | 432 | 1417 | Masson |
| Nitric oxide..... | 0 | 325 | 1066 | " |
| Nitrogen..... | 0 | 337.8 | 1108 | Mean |
| Nitrous oxide..... | 0 | 261.8 | 859 | Dulong |
| Oxygen..... | 0 | 317.2 | 1041 | " |
| Explosive waves in air: | | | | |
| Charge of powder, 0.24 gms.... | | 336 | 1102 | } Violle, Cong. Intern. Phys. I, 243, 1900 |
| " " 3.80 "..... | | 500 | 1640 | |
| " " 17.40 "..... | | 931 | 3060 | |
| " " 45.60 "..... | | 1268 | 4160 | |
| Vapors: Alcohol..... | 0 | 230.6 | 756 | Masson |
| Ether..... | 0 | 179.2 | 588 | " |
| Water..... | 0 | 401 | 1315 | " |
| "..... | 100 | 404.8 | 1328 | Treitz, 1903 |

Supersonics: Reid, 1930:—Air, 0°C, no CO₂, 42 Kc/sec., 331.75 m/sec.; 20°C, sat. H₂O, 333.1 m/sec.; 140 Kc/sec, 331.60, 332.92, respectively; Thompson, 1930:—109 c/sec. sat. H₂O vapor, 27°C, 432 m/sec.; Poole, 1930:—Water, distilled, audio-frequency, 25°C, 1485 m/sec.

MUSICAL SCALES

The pitch relations between two notes may be expressed precisely (1) by the ratio of their vibration frequencies; (2) by the number of equally-tempered semitones between them (E. S.); also, less conveniently, (3) by the common logarithm of the ratio in (1); (4) by the lengths of the two portions of the tense string which will furnish the notes; and (5) in terms of the octave as unity. The ratio in (4) is the reciprocal of that in (1); the number for (5) is 1/12 of that for (2); the number for (2) is nearly 40 times that for (3).

Table 144 gives data for the middle octave, including vibration frequencies for three standards of pitch; $A_4=435$ double vibrations per second, is the international standard, and was adopted by the American Piano Manufacturers' Association. The "just-diatonic scale" of C-major is usually deduced, following Chladni, from the ratios of the three perfect major triads reduced to one octave, thus:

| | | | | | | | | | | | | |
|----|---|----|---|----|---|----|---|----|---|----|---|----|
| 4 | : | 5 | : | 4 | : | 5 | : | 6 | : | 5 | : | 6 |
| F | : | A | : | C | : | E | : | G | : | B | : | 1 |
| 16 | | 20 | | 24 | | 30 | | 36 | | 45 | | 54 |
| | | | | 24 | | 27 | | 30 | | 32 | | 36 |
| | | | | | | | | 40 | | 45 | | 48 |

Other equivalent ratios and their values in E. S. are given in Table 145. By transferring D to the left and using the ratio 10:12:15 the scale of A-minor is obtained, which agrees with that of C-major except that D=26 2/3. Nearly the same ratios are obtained from a series of harmonics beginning with the eighth; also by taking 12 successive perfect or Pythagorean fifths or fourths and reducing to one octave. Such calculations are most easily made by adding and subtracting intervals expressed in E. S. The notes needed to furnish a just major scale in other keys may be found by successive transpositions by fifths or fourths as shown in Table 145. Disregarding the usually negligible difference of 0.02 E. S., the table gives the 24 notes to the octave required in the simplest enharmonic organ; the notes fall into pairs that differ by a comma, 0.22 E. S. The line "mean tone" is based on Dom Bedos' rule for tuning the organ (1746). The tables have been checked by the data in Ellis' Helmholtz's "Sensations of Tone."

TABLE 144.—Data for Middle Octave

| Note. | Interval. | | Ratios. | | Logarithms. | | Number of double Vibrations per second. | | | | | |
|----------------|-----------|-----------|---------|-----------|-------------|-----------|---|-------|-------|-----------|-----------|-----------|
| | Just. | Tempered. | Just. | Tempered. | Just. | Tempered. | Just. | Just. | Just. | Tempered. | Tempered. | Tempered. |
| C ₈ | E. S. | E. S. | | | | | | | | | | |
| | 0. | 0 | 1.00 | 1.00000 | .0000 | .00000 | 256 | 264 | 258.7 | 258.7 | 261.6 | 271.1 |
| | | 1 | | 1.05926 | | .02509 | | | | 274.0 | 277.2 | 287.3 |
| D ₈ | 2.04 | 2 | 1.125 | 1.12246 | .05115 | .05017 | 288 | 297 | 291.0 | 290.3 | 293.7 | 304.3 |
| | | 3 | | 1.18921 | | .07526 | | | | 307.6 | 311.1 | 322.4 |
| E ₈ | 3.86 | 4 | 1.25 | 1.25992 | .09691 | .10034 | 320 | 330 | 323.4 | 325.9 | 329.6 | 341.6 |
| F ₈ | 4.98 | 5 | 1.33 | 1.33484 | .12494 | .12543 | 341.3 | 352 | 344.9 | 345.3 | 349.2 | 361.9 |
| | | 6 | | 1.41421 | | .15051 | | | | 365.8 | 370.0 | 383.4 |
| G ₈ | 7.02 | 7 | 1.50 | 1.49831 | .17609 | .17560 | 384 | 396 | 388 | 387.5 | 392.0 | 406.2 |
| | | 8 | | 1.58740 | | .20069 | | | | 410.6 | 415.3 | 430.4 |
| A ₈ | 8.84 | 9 | 1.67 | 1.68179 | .22185 | .22577 | 426.7 | 440 | 431.1 | 435.0 | 440.0 | 456.0 |
| | | 10 | | 1.78180 | | .25086 | | | | 460.9 | 466.2 | 483.1 |
| B ₈ | 10.88 | 11 | 1.875 | 1.88775 | .27300 | .27594 | 480 | 495 | 485.0 | 488.3 | 493.9 | 511.8 |
| C ₉ | 12.00 | 12 | 2.00 | 2.00000 | .30103 | .30103 | 512 | 528 | 517.3 | 517.3 | 523.2 | 542.3 |

TABLE 145.—Notes Needed to Transpose to Other Scales

| Key of | | C | D | E | F | G | A | B | C |
|------------------|----------------|-------|------|------|------|------|------|-------|-------|
| 7 #s | C [♯] | | 1.14 | 3.18 | 5.00 | 6.12 | 8.16 | 9.98 | 12.02 |
| | | | 0.92 | 2.96 | 4.78 | 5.90 | 7.94 | 9.76 | 11.80 |
| 6 " | F [♯] | | 1.14 | 2.96 | 5.00 | 6.12 | 8.16 | 9.98 | |
| | | | 0.92 | 2.74 | 4.78 | 5.90 | 7.94 | 9.76 | 10.88 |
| 5 " | B | | 1.14 | 2.96 | 4.08 | 6.12 | 7.94 | 9.98 | 11.10 |
| | | | 0.92 | 2.74 | 3.86 | 5.90 | 7.72 | 9.76 | 10.88 |
| 4 " | E | | 0.92 | 2.96 | 4.08 | 6.12 | 7.94 | 9.06 | 10.88 |
| | | | 0.70 | 2.74 | 3.86 | 5.90 | 7.72 | 8.84 | 10.88 |
| 3 " | A | | 0.92 | 2.04 | 4.08 | 5.90 | 7.94 | 9.06 | 11.10 |
| | | | 0.70 | 1.82 | 3.86 | 5.68 | 7.72 | 8.84 | 10.88 |
| 2 " | D | | 0.92 | 2.04 | 4.08 | 5.90 | 7.02 | 9.06 | 10.88 |
| 1 # | G | 0.00 | 2.04 | 3.86 | 5.90 | 7.02 | 9.06 | 10.88 | 12.00 |
| | C | 0.00 | 2.04 | 3.86 | 4.98 | 7.02 | 8.84 | 10.88 | 12.00 |
| 1 b | F | 0.00 | 1.82 | 3.86 | 4.98 | 7.02 | 8.84 | 9.96 | 12.00 |
| 2 bs | B [♭] | 0.00 | 1.82 | 2.94 | 4.98 | 6.80 | 8.84 | 9.96 | 12.00 |
| 3 " | E [♭] | -2.22 | 1.82 | 2.94 | 4.98 | 6.80 | 7.92 | 9.96 | 11.78 |
| 4 " | A [♭] | -2.22 | 0.90 | 2.94 | 4.76 | 6.80 | 7.92 | 9.96 | 11.78 |
| 5 " | D [♭] | -2.22 | 0.90 | 2.94 | 4.76 | 5.88 | 7.92 | 9.74 | 11.78 |
| 6 " | G [♭] | | 0.90 | 2.72 | 4.76 | 5.88 | 7.92 | 9.74 | 10.86 |
| 7 " | C [♭] | | 0.90 | 2.72 | 3.84 | 5.88 | 7.70 | 9.74 | 10.86 |
| Harmonic Series | | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| | | 0.0 | 1.05 | 2.04 | 3.86 | 5.51 | 7.73 | 8.41 | 9.69 |
| Cycle of fifths | | 0.0 | 1.14 | 2.04 | 3.18 | 4.08 | 5.22 | 6.12 | 7.02 |
| Cycle of fourths | | 0.0 | 0.90 | 1.80 | 2.94 | 3.84 | 4.98 | 5.88 | 6.78 |
| Mean tone | | 0.0 | 0.76 | 1.93 | 3.11 | 3.86 | 5.03 | 5.79 | 6.97 |
| Equal 7 step | | 0.0 | | 1.71 | 3.43 | | 5.14 | | 6.86 |

TABLE 146.—A Fundamental Tone, its Harmonics (Overtones) and the Nearest Tone of the Equal-tempered Scale

| No. of partial..... | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|------------------------------|-----|-----|-----|-----|-----|-----|-----|------|------|------|
| Frequency..... | 129 | 259 | 388 | 517 | 647 | 776 | 905 | 1035 | 1164 | 1293 |
| Nearest tempered note..... | C | C | G | C | E | G | Bb | C | D | E |
| Corresponding frequency..... | 129 | 259 | 388 | 517 | 652 | 775 | 922 | 1035 | 1164 | 1293 |

| No. of partial..... | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 |
|------------------------------|------|------|------|------|------|------|------|------|------|------|
| Frequency..... | 1423 | 1552 | 1681 | 1811 | 1940 | 2069 | 2199 | 2328 | 2457 | 2586 |
| Nearest tempered note..... | Gb | G | G# | Bb | B | C | C# | D | D# | E |
| Corresponding frequency..... | 1463 | 1550 | 1642 | 1843 | 1953 | 2069 | 2192 | 2323 | 2461 | 2607 |

CHARACTERISTICS OF SPEECH, MUSIC, AND NOISE

(See Kaye, *Nature* 128, 253, 1931; Fletcher, *Rev. Mod. Phys.*, 3, 258, 1931.)

Average ear perceives frequencies 20–20,000 cycles/sec. Upper limit less with increasing age. Ordinarily attention largely restricted to 50–5,000 for speech, 35–7,000 in music.

Matching of sounds.—Average ear detects 10 per cent difference of energy when two notes of medium loudness sound alternately without break; doubled if interval of silence; ordinarily 25 per cent holds.

Weber-Fechner law.—When sound sensation advances arithmetically, physical intensity advances geometrically (Kingsbury). Frequencies, 700–4,000 c/sec., relation between loudness and intensity independent of frequency. Lower frequencies, loudness increases proportionally more rapidly than intensity.

TABLE 147.—The Bel and the Decibel

Bel, Decibel.—One bel is 10-fold increase in power or energy.

Intensities differing as r to 1 differ by $\log r$ bels.

| | | | | | | |
|------------------------------------|---|----|-----|-------|--------|------------------|
| Ratio intensities..... | 1 | 10 | 100 | 1,000 | 10,000 | 10 ¹³ |
| Number decibels, 10 $\log r$ | 0 | 10 | 20 | 30 | 40 | 130 db |

Least perceptible change in loudness of a sound of medium loudness under various conditions = 1 db (0.2 to 9 db according to frequency and loudness). Threshold of audibility taken as zero (see Table 148). Pure sounds of medium frequency: range of audibility between threshold and sensation of "feeling" of the sound about 130 db.

If intensity levels of two pure sounds is the same, then if each is increased by the same amount of energy they no longer give an equal sensation of tone. Standard for mixed sounds may be taken as a pure note. Frequency about 1000 cycles/sec. Threshold value (zero) = about 1 millidyne/cm².

TABLE 148.—Loudness Levels of Various Noises

| Source | Distance ft. | Average decibels above threshold | Note | Source | Distance ft. | Average decibels above threshold | Note |
|----------------------|--------------|----------------------------------|------|----------------------|--------------|----------------------------------|------|
| Quiet whisper..... | 5 | 10 | 6 | Lindbergh applause.. | Street | 90 | 5 |
| Quiet garden..... | .. | 30 | 1 | Pneumatic drill..... | 20 | 90 | 1 |
| Ordinary talk..... | 3 | 50 | 6 | Elevated R.R., N.Y. | 20 | 90 | 3 |
| Express train..... | Pullman | 60 | 4 | N. Y. subway..... | Int. | 95 | 4 |
| Steamship siren..... | 1,500 | 60 | 3 | Riveting..... | 35 | 95 | 3 |
| Busy traffic, N. Y. | .. | 72 | 2 | Steamship siren..... | 115 | 95 | 3 |
| Police whistle..... | 15 | 80 | 3 | Airplane cabin..... | Int. | 80–110 | .. |
| Lion roaring, Zoo.. | 18 | 85 | 3 | Airplane engine..... | 18 | 115 | 4 |

(1) Davis, *Journ. Roy. Aeron. Soc.*, 1931. (2) Free. (3) Galt. (4) Parkinson, *Journ. Acoust. Soc. Amer.*, 1930. (5) Fletcher. (6) Kaye.

TABLE 149.—Peak Power in Watts of Musical Instruments (Fortissimo)

(Sivian, Dunn, White, *Journ. Acoust. Soc. Amer.*, Jan. 1931.)

| | | | | | |
|-------------------------|----|----------------|------|------------------|------|
| 75-piece orchestra..... | 70 | Trombone..... | 6 | Piccolo..... | 0.08 |
| Large bass drum..... | 25 | Piano..... | 0.4 | Flute..... | 0.06 |
| Pipe organ..... | 13 | Trumpet..... | 0.3 | Clarinet..... | 0.03 |
| Snare drum..... | 12 | Bass tuba..... | 0.2 | French horn..... | 0.05 |
| Cymbals..... | 10 | Base viol..... | 0.16 | Triangle..... | 0.05 |

Peak powers, fortissimo playing. Orchestra of 75 pieces. Both peak and average powers of orchestra are about 10,000 times such for conversational speech. Violin played as softly as possible, 4 microwatts. Threshold peak power 20,000,000 times this.

TABLE 150.—Relative Strength of the Partial in Various Musical Instruments

The values given are for tones of medium loudness. Individual tones vary greatly in quality and, therefore, in loudness.

| Instrument. | Strength of partials in per cent of total tone strength. | | | | | | | | | | | |
|-----------------------|--|----|----|----|----|----|---|----|----|----|----|----|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| Tuning fork on box... | 100 | — | — | — | — | — | — | — | — | — | — | — |
| Flute..... | 66 | 24 | 4 | 6 | — | — | — | — | — | — | — | — |
| Violin, A string..... | 26 | 25 | 9 | 10 | 27 | 1 | 0 | 2 | — | — | — | — |
| Oboe..... | 2 | 2 | 4 | 29 | 35 | 14 | 4 | 2 | 3 | 4 | 1 | 0 |
| Clarinet..... | 12 | 0 | 10 | 3 | 5 | 0 | 8 | 18 | 15 | 18 | 5 | 6 |
| Horn..... | 36 | 26 | 17 | 7 | 4 | 3 | 2 | 1 | 1 | 1 | 1 | 1 |
| Trombone..... | 6 | 11 | 35 | 12 | 8 | 11 | 6 | 4 | 3 | 2 | 1 | 1 |

TABLE 151.—Miscellaneous Sound Data

Koenig's temperature coefficient for the frequency (n) of forks is nearly the same for all pitches. $n_t = n_0(1 - 0.0011t^\circ \text{C})$, Ann. d. Phys. 9, p. 408, 1880.

Vibration frequencies for continuous sound sensations are practically the same as for continuous light sensation, 10 or more per second. Helmholtz' value of 32 per sec. may be taken as the flicker value for the ear. Moving pictures use 16 or more per sec. For light the number varies with the intensity.

The quality of a musical tone depends solely on the number and relative strength of its partials (simple tones) and probably not at all on their phases.

The wave lengths of sound issuing from a closed pipe of length L are $4L$, $4L/3$, $4L/5$, etc., and from an open pipe, $2L$, $2L/2$, $2L/3$, etc. The end correction for a pipe with a flange is such that the antinode is $0.82 \times$ radius of pipe beyond the end; with no flange the correction is $0.57 \times$ radius of pipe.

The energy of a pure sine wave is proportional to $n^2 A^2$; the energy per cm^3 is on the average $2\pi^2 U^2 A^2 / \lambda^2$; the energy passing per sec. through 1 cm^2 perpendicular to direction of propagation is $2\pi^2 U^3 A^2 / \lambda^2$; the pressure is $\frac{1}{2}(\gamma + 1)$ (average energy per cm^3); where n is the vibration number per sec., λ the wave length, A the amplitude, V the velocity of sound, ρ the density of the medium, γ the specific heat ratio. Altberg (Ann. d. Phys. 11, p. 405, 1903) measured sound-wave pressures of the order of $0.24 \text{ dynes/cm}^2 = 0.00018 \text{ mm Hg}$.

TABLE 152.—Audibility as Dependent on Sound Pressure and Frequency

The ear detects sounds over a pressure range about 0.001 to 1000 dynes/cm^2 ; over much of this range it differentiates between complex sounds so nearly alike that no existing physical device can distinguish them. Plot shows minimum audibility pressures from 72 normal ears from 60 to 4000 cycles (both scales logarithmic); standard deviation indicated by dotted curves. The maximum audibility curve was obtained from 48 normal ears. A louder sound becomes painful. The intensity of pressure necessary is about that required to excite the tactile nerves in the finger tips. (Wegel, Pr. Nat. Acad. Sci., 8, p. 155, 1922.)

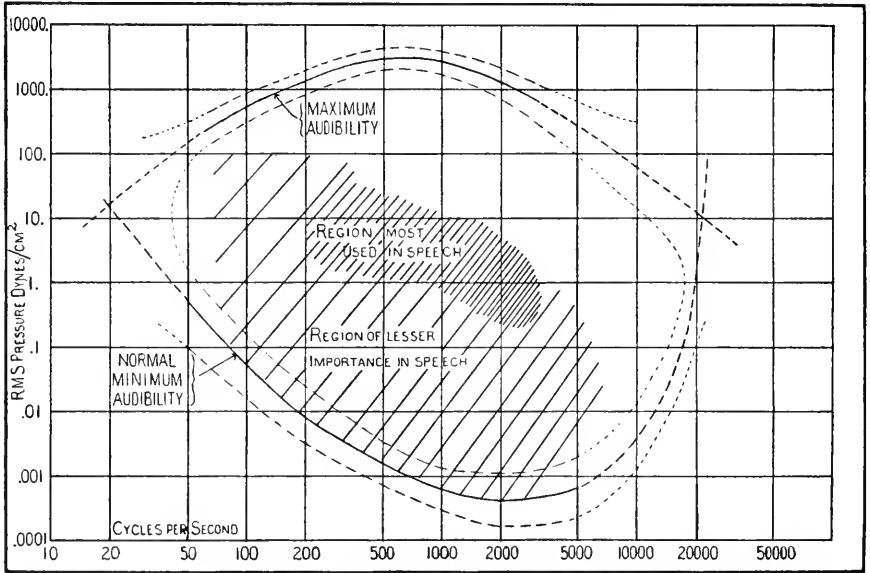


TABLE 153.—Speech

(Fletcher, Rev. Mod. Phys., 3, 258, 1931.)

Speech is composed of vowels and consonants. Most are continued in steady tones (continuants), long vowels, a, short, i, diphthongs, ou, semivowels, l, fricative consonants, s; others are interrupted (stops). The pure stops are p, t, ch, k; voiced, b, d, j, g.

When frequencies, f , are measured in kilocycles, then the pitch $P = \log_2 F$. J is the intensity of the sound passing through a cm^2 of the wave-front. The intensity level $I = \log_{10} J$ and is expressed in bells.

TABLE 154.—Characteristic Resonance Values for Spoken Vowels

The larynx generates a fundamental tone of a *chosen* pitch with some 20 partials, usually of low intensity. The particular partial, or partials, most nearly in unison with the mouth cavity is greatly strengthened by resonance. Each vowel, for a given mouth, is characterized by a particular *fixed* pitch, or pitches, of resonance corresponding to that vowel's definite form of mouth cavity. These pitches may be judged by whispering the vowels. It is difficult to sing vowels true above the corresponding pitches. The greater part of the energy or loudness of a vowel of a *chosen* pitch is in those partials reinforced by resonance. The vowels may be divided into two classes,—the first having one characteristic resonance region, the second, two. The representative pitches of maximum resonance of a mouth cavity for selected vowels in each group are given in the following table.

| Vowel indicated by italics in the words. | Pitch of maximum resonance. | Vowel indicated by italics in the words. | Pitch of maximum resonance. |
|---|-----------------------------|--|-----------------------------|
| <i>father</i> , <i>far</i> , <i>guard</i> | 910 | <i>mat</i> , <i>add</i> , <i>cat</i> | 800 and 1840 |
| <i>raw</i> , <i>fall</i> , <i>haul</i> | 732 | <i>pet</i> , <i>feather</i> , <i>bless</i> | 691 and 1953 |
| <i>no</i> , <i>rode</i> , <i>goal</i> | 461 | <i>they</i> , <i>bait</i> , <i>hate</i> | 488 and 2461 |
| <i>gloom</i> , <i>move</i> , <i>group</i> | 326 | <i>bee</i> , <i>pique</i> , <i>machine</i> | 308 and 3100 |

Pitch in octaves from one kilocycle. For the first 6 vowels high pitch region less intense (Fletcher).

| | | | | | | | |
|------|-------------|--------|-------------|------|--------------|------|-------------|
| pool | — 0.3 — 1.3 | talk | — 0.1 — 0.7 | tap | — 0.45 + 0.8 | tip | — 1.2 + 1.2 |
| put | 0.0 — 1.1 | ton | + 0.2 — 0.5 | ten | — 0.7 + 0.9 | team | — 1.4 + 1.3 |
| tone | — 0.2 — 1.0 | father | + 0.3 — 0.3 | tape | — 0.9 + 1.1 | | |

TABLE 155.—Speech Power (Fletcher)

Average conversational speech power, 10 microwatts or 100 ergs per second. About 1/3 of time no sound is flowing (pauses), so if silent intervals are excluded these values may be taken as 15 and 150. Shouting as loud as possible increases 100-fold, whispering intelligibly 1/10,000. The *mean speech power* may be defined as average over 1/100 sec. period; *phonetic speech power*, max. value of mean speech power of a fundamental vowel or consonant; *peak speech power*, max. value of instantaneous power over interval considered.

TABLE 156.—Phonetic Powers, Average Conversation

| | | | | | | | | | | | | | | | |
|---|-----|---|-----|---|-----|----|-----|----|----|---|----|---|----|----|---|
| ó | 680 | ō | 470 | ū | 310 | l | 100 | ch | 42 | s | 16 | v | 12 | f | 5 |
| a | 600 | u | 460 | i | 260 | sh | 80 | n | 36 | t | 15 | b | 7 | th | 1 |
| o | 510 | ā | 370 | ē | 220 | ng | 73 | j | 23 | g | 15 | d | 7 | | |
| ā | 490 | e | 350 | r | 210 | m | 52 | z | 16 | k | 13 | p | 6 | | |

The most powerful sound is "*awl*,"—900 times the power of *th* in *thigh*. Intoned without emphasis it is about 50 microvolts. Peak powers are 10-20 times the phonetic power. In ordinary conversation 2% of time > 20 db over average level; 42%, 6 to 16 db.

NOTE.—For Bibliography of Acoustics of Buildings (Watson) see Nat. Res. Council, Reprint, and Circulars, No. 98, 1931, or Journ. Acoust. Soc. Amer., 2, 14, 1931.

VELOCITY PRESSURE AT DIFFERENT AIR SPEEDS

The resistance F of a body of fixed shape and presentation moving through a fluid may be written

$$F = \rho L^2 V^2 \left(\frac{VL\rho}{\mu} \right) \quad (1)$$

in which ρ denotes the fluid density, μ the viscosity, L a linear dimension of the body fixing the scale, and V is the speed of the body relative to the fluid. The dimensionless ratio $\frac{VL\rho}{\mu}$ is termed the Reynolds Number R . Values of R are comparable only for geometrically similar bodies. The quantity $(1/2)\rho V^2$ is termed the velocity pressure q ; it is the increase in pressure above the static pressure set up in a tube whose open end is pointed into the relative wind. The relation (1) is usually written $F = CAq$, A being some specifically defined area as, for example, the area of the projection of the body on a plane normal to the wind. C is usually termed the absolute resistance coefficient. It has the same value in any self-consistent system of units and is a function of the Reynolds Number R . The method of defining A and L must in every case be explicitly stated.

For speeds near the speed of sound, C is also a function of the ratio of the air speed to the speed of sound. Values given in these Tables can not then be used.

The table gives values of the velocity pressure q at different air speeds. In conjunction with the values of C in subsequent tables, this table can be used for computation of the resistance under specified conditions. It is computed for standard air density: dry air, normal CO_2 content, 15°C , one atmosphere, standard gravity,

$$0.12497 \frac{\text{metric slugs}}{\text{m}^3} \left(\frac{\text{Kg (mass)}}{9.807 \text{ m}^3} \right) = 0.002378 \frac{\text{slugs}}{\text{ft}^3} \left(\frac{\text{lbs. (mass)}}{32.156 \text{ ft}^3} \right)$$

For other densities the values must be multiplied by the ratio of the actual density to the standard density.

| Air speed m/sec. | Pressure, q kg/m ² | Air speed m/sec. | Pressure, q kg/m ² | Air speed m/sec. | Pressure, q kg/m ² | Air speed m/sec. | Pressure, q kg/m ² | Air speed m/sec. | Pressure, q kg/m ² |
|-----------------------|---------------------------------------|-----------------------|---------------------------------------|-----------------------|---------------------------------------|-----------------------|---------------------------------------|-----------------------|---------------------------------------|
| 1 | 0.063 | 11 | 7.56 | 21 | 27.56 | 31 | 60.06 | 41 | 105.1 |
| 2 | .250 | 12 | 9.00 | 22 | 30.25 | 32 | 64.00 | 42 | 110.3 |
| 3 | .562 | 13 | 10.56 | 23 | 33.06 | 33 | 68.06 | 43 | 115.6 |
| 4 | 1.00 | 14 | 12.25 | 24 | 36.00 | 34 | 72.25 | 44 | 121.0 |
| 5 | 1.56 | 15 | 14.06 | 25 | 39.06 | 35 | 76.56 | 45 | 126.6 |
| 6 | 2.25 | 16 | 16.00 | 26 | 42.25 | 36 | 81.00 | 46 | 132.2 |
| 7 | 3.06 | 17 | 18.06 | 27 | 45.56 | 37 | 85.56 | 47 | 138.1 |
| 8 | 4.00 | 18 | 20.25 | 28 | 49.00 | 38 | 90.25 | 48 | 144.0 |
| 9 | 5.06 | 19 | 22.56 | 29 | 52.56 | 39 | 95.06 | 49 | 150.1 |
| 10 | 6.25 | 20 | 25.00 | 30 | 56.25 | 40 | 100.0 | 50 | 156.3 |
| Air speed ft./sec. | Pressure, q lb./ft. ² | Air speed ft./sec. | Pressure, q lb./ft. ² | Air speed ft./sec. | Pressure, q lb./ft. ² | Air speed ft./sec. | Pressure, q lb./ft. ² | Air speed ft./sec. | Pressure, q lb./ft. ² |
| 1 | 0.00119 | 11 | .1438 | 21 | .5243 | 55 | 3.597 | 105 | 13.11 |
| 2 | .00476 | 12 | .1712 | 22 | .5755 | 60 | 4.280 | 110 | 14.39 |
| 3 | .01070 | 13 | .2009 | 23 | .6290 | 65 | 5.024 | 115 | 15.72 |
| 4 | .0190 | 14 | .2330 | 24 | .6849 | 70 | 5.826 | 120 | 17.12 |
| 5 | .0297 | 15 | .2675 | 25 | .7431 | 75 | 6.688 | 125 | 18.58 |
| 6 | .0428 | 16 | .3044 | 30 | 1.070 | 80 | 7.610 | 130 | 20.09 |
| 7 | .0583 | 17 | .3436 | 35 | 1.457 | 85 | 8.591 | 135 | 21.67 |
| 8 | .0761 | 18 | .3852 | 40 | 1.902 | 90 | 9.631 | 140 | 23.30 |
| 9 | .0963 | 19 | .4292 | 45 | 2.408 | 95 | 10.73 | 145 | 25.00 |
| 10 | .1189 | 20 | .4756 | 50 | 2.973 | 100 | 11.89 | 150 | 26.75 |

CORRECTIONS TO ROBINSON CUP ANEMOMETERS

The official Weather Bureau instrument used for measuring speed of natural winds is a Robinson type cup anemometer. Before January 1, 1928, a four-cup driving unit was used; after that date a three-cup unit, because of the large errors of the older type at high speeds. The table gives the speeds indicated by the old and new instruments at various true speeds.

| True speed, miles per hour | Indicated speed, four-cup standard, miles per hour | Indicated speed, three-cup standard, miles per hour | True speed, miles per hour | Indicated speed, four-cup standard, miles per hour | Indicated speed, three-cup standard, miles per hour | True speed, miles per hour | Indicated speed, four-cup standard, miles per hour | Indicated speed, three-cup standard, miles per hour |
|----------------------------|--|---|----------------------------|--|---|----------------------------|--|---|
| 5 | 5 | 5 | 40 | 50 | 41 | 75 | 98 | 79 |
| 10 | 11 | 10 | 45 | 57 | 47 | 80 | 105 | 84 |
| 15 | 17 | 15 | 50 | 64 | 52 | 85 | 112 | 89 |
| 20 | 23 | 20 | 55 | 71 | 57 | 90 | 118 | 95 |
| 25 | 30 | 25 | 60 | 78 | 63 | 95 | 125 | 100 |
| 30 | 37 | 31 | 65 | 85 | 68 | 100 | 132 | 105 |
| 35 | 44 | 36 | 70 | 91 | 73 | 110 | 145 | 116 |

NOTE.—Values above a true speed of 75 miles per hour are extrapolated.

It must be borne in mind that problems in aerodynamics can not be idealized as easily as many problems in mechanics. The side of a building may not be regarded as a thin flat plate in computing the force of the wind, and data for a cylinder of a given length can not be directly applied for the wind force on a cylinder of some other length. Further, objects nearby exert an appreciable influence.

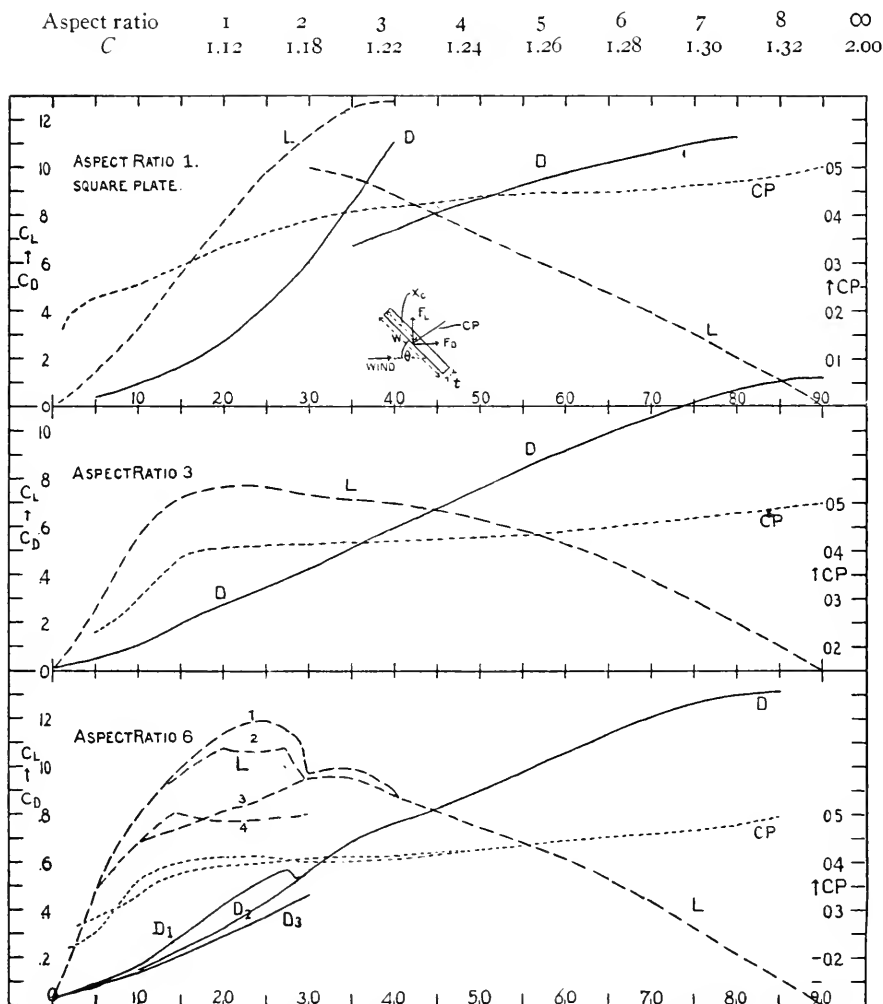
These complications limit the strict application of a test on a particular object to geometrically similar objects in similar surroundings. They also cause apparent discrepancies among the results of different experimenters which are to be attributed to departure from geometrical similarity of the models, to the effects of the relative size of the body and the air stream, of the supports or other nearby objects, and to differences in the fine structure (turbulence) of the approximately steady air streams rather than to errors of measuring.

The data here given are intended to apply to the ideal condition of an isolated body of exactly the shape specified in a uniform, steady air stream of infinite extent.

Example of tables: Take the problem of the resistance of a sphere 1.5 cm. diam. moving at a speed 35 m/sec. (3500 cm/sec.) through still air of density 0.0010 g/cm³ and viscosity 0.000173 g/cm sec. The Reynolds number is $3500 \times 1.5 \times 0.0010 / 0.000173$ or 30,347; $\log_{10} R$ is 4.482; whence from Table 162 C is 0.50. From Table 157 the value of q for std. density is 76.56 kg(force)/m². The ratio of the actual to std. density is 0.0010/0.0012253 or 0.816. The resistance is therefore $\{ 0.50 \} \{ \pi/4 \} \{ 1.5/100 \}^2 \{ 76.56 \} \{ 0.816 \} = 0.00552$ kg(force) = 5413 dynes.

RESISTANCE COEFFICIENT FOR THIN FLAT PLATES NORMAL TO THE WIND

The pressure on a thin rectangular plate varies with the "aspect ratio," a term introduced by Langley for the ratio of the length of the leading edge (span) to the chord length. The resistance coefficient is nearly independent of the Reynolds Number if the Reynolds Number (L taken as the chord length) is greater than 100. In the following table the values of C are given as a function of the aspect ratio. A is taken as the area of the plane, viz., product of chord and span. Values of C for circular disks are practically the same as for a square plate.



COEFFICIENTS OF RECTANGULAR PLATES, SEE P. 199.

FORCES ON THIN FLAT PLATES AT ANGLES TO THE WIND

For plates at angles, the force is usually resolved into components at right angles and parallel to the direction of the relative wind. The components, termed the lift and drag respectively, are expressed in the form of absolute coefficients, the forces being divided by the product of the velocity pressure and the area of the plate (N. B.—*not* the projected area on a plane normal to the wind). The line of action of the force is given by the intersection of the resultant force with the plate expressed as the ratio of the distance of the intersection from the leading edge to the chord length, a quantity called the center of pressure coefficient. The lift coefficient $L = \text{lift}/Aq$, the drag coefficient $D = \text{drag}/Aq$, and the center of pressure coefficient for various angles are given for plates of aspect ratios 1, 3, and 6 in the form of graphs. (See page 198.)

The following formulae indicate the use of the coefficients from the plots for the determination of the forces:

F_d = component of resulting wind force parallel to wind = drag = DAq ;

F_l = that normal to wind and width = lift = LAq ;

x_c (see small figure in upper set of curves) = $\overline{CP} \cdot W$; W is that dimension of the plane of reference which makes the least angle with wind.

A = area of one surface of plate. D , L , \overline{CP} are independent of Reynold's No. and temperature.

Authorities and the conditions of their experiments: (1) Eiffel. (2) Dines, 1890. (3) Föppl, 1910. (4) Riabouchinski, 1912. (5) Stanton, 1903. (6) Bureau of Standards. In lower figure of previous page: L_1 , Föppl; L_2 , L_3 , B. of S.; L_4 , Eiffel; D_1 , Föppl, B. of S.; D_2 , B. of S.; D_3 , Eiffel. For more detailed information as to references and data see I.C.T. 1, 406, 1926.

| Authority | Aspect ratio 1 | | | | Aspect ratio 3 | | | Aspect ratio 6 | | | |
|-----------------------|----------------|----------|------|------|----------------|------|------|----------------|------|------|------|
| | (1) | (2) | (3) | (4) | (1) | (3) | (5) | (1) | (3) | (6) | (6) |
| Span | 25 | 30.5 | 12 | 12 | 45 | 7.6 | 36 | 90 | 30.5 | 72 | 30.5 |
| Chord | 25 | 30.5 | 12 | 12 | 15 | 2.5 | 12 | 15 | 5.08 | 12 | 5.08 |
| Thickness | .33 | .32 | .17 | | .3 | .025 | .17 | .3 | .117 | .17 | .129 |
| Tunnel diam. | 1500 | ∞ | 2000 | 1200 | 1500 | 600 | 2000 | 1500 | 1370 | 2000 | 1370 |
| Reynold's No. | 210 | 382 | 55 | 42 | 126 | 10 | 55 | 126 | 64 | 55 | 64 |

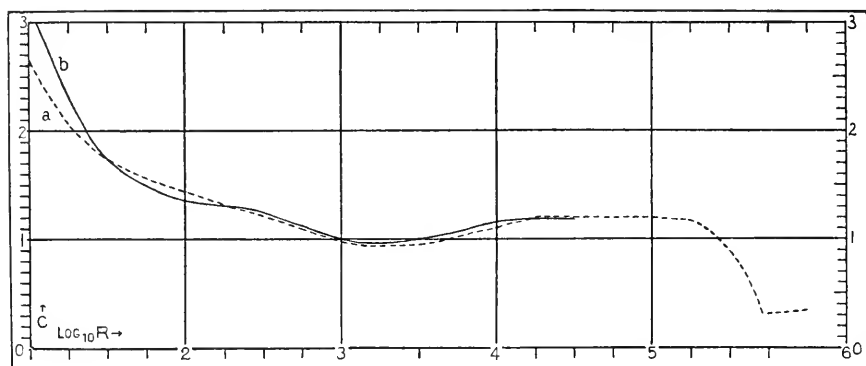
FORCES ON NON-ROTATING CIRCULAR CYLINDERS

The coefficient for cylinders normal to the wind, the area A being taken as the product of length and diameter and the linear dimension L as the diameter, depends to a marked degree on the ratio of length to diameter and on the Reynolds Number, R . The graph shows the variation of C with R for cylinders of infinite length.

The variation of C with the length-diameter ratio for a Reynolds Number of 80,000 is as follows:

| | | | | | | | | |
|-----------------------------|------|-----|-----|-----|-----|-----|------|------|
| Ratio of length to diameter | 1 | 2 | 3 | 5 | 10 | 20 | 40 | |
| C | 0.63 | .69 | .75 | .74 | .83 | .92 | 1.00 | 1.20 |

If the axis of the cylinder is inclined to the wind direction, the force remains approximately at right angles to the axis of the cylinder, its magnitude falling off approximately as the square of the sine of the angle of the axis to the wind.



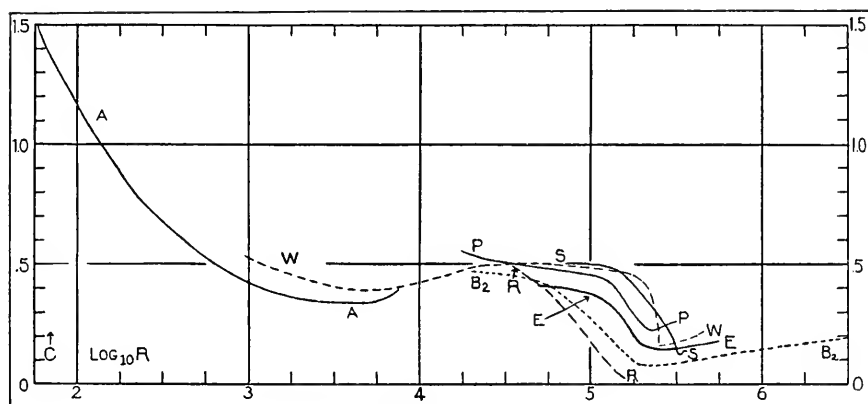
AIR FORCES, CIRCULAR CYLINDERS.

Force = $C A q$. Reynold's number = $R = V D \rho / \mu$.

C is taken from above plot; for q see Table 157; A = Area axial section of cylinder = L (length) $\times D$ (diameter); the plane of reference contains the axis and is perpendicular to the plane defined by the axis and the wind direction; V = air speed; ρ , the density of the medium and μ , its viscosity. Curve (a) is due to Wieselsberger, 1922; curve (b) to Relf.

TABLE 162.—Forces on Spheres

For spheres the linear dimension L is taken as the diameter of the sphere D and the area as $\frac{\pi D^2}{4}$. For values of the Reynolds Number between 80,000 and 300,000 the value of C depends in large measure on the turbulence of the air stream (*cf.* Technical Report 342 of the National Advisory Committee for Aeronautics). The curves marked S and W most clearly approximate the condition of zero turbulence.



AIR FORCES ON SPHERES.

$$\text{Force} = F = CAq. \quad A = \pi D^2/4. \quad R = VD\rho/\mu.$$

For meaning of letters see previous table.

Authorities: A, Allen, 1900; B₂, Bacon and Reid; E, Eiffel; P, Pannell; R, Riabouchinski, 1914; S, Bureau of Standards; W, Wieselsberger, 1914, 1922. For more detailed references see I.C.T., I, 411, 1926.

TABLE 163.—Forces on Miscellaneous Bodies

The values of the shape coefficients in the following table are to be used with the area of the projection of the body on a plane normal to the wind direction. Where this projection is a circle, the diameter is used as the quantity L in the Reynolds Number. Where the projection is rectangular, the shortest side of the rectangle is taken as L .

TABLE 163 (continued).—Forces on Miscellaneous Bodies

| Body | C | Reynolds Number |
|---|-----------|-----------------|
| Struts (bodies streamlined in two dimensions)..... | 0.06–0.08 | above 40,000 |
| Streamline bodies of revolution..... | 0.03–0.04 | above 100,000 |
| Rectangular prism, 1 x 1 x 3, normal to 1 x 3 face..... | 1.60 * | 400,000 |
| Model of automobile..... | .78 * | about 300,000 |
| Cone, angle 60°, diam. base 40 cm, point to wind, solid.. | .51 | about 270,000 |
| Cone, angle 30°, diam. base 40 cm, point to wind, solid.. | .34 | 270,000 |
| Hemisphere, convex to wind..... | .34 | 170,000 |
| Hemisphere, concave to wind..... | .13 | 170,000 |
| Concave cup | 1.39 | 170,000 |
| Convex cup | .35 | 170,000 |
| Sphero-conic body, diam. 20 cm, cone 20° point forward. | .16 | 135,000 |
| Sphero-conic body, diam. 20 cm, cone 20° point to rear.. | .088 | 135,000 |
| Cylinder 120 cm long, spherical ends..... | .19 | 100,000 |

* C varies very little with Reynolds Number.

TABLE 164.—Forces on Cylinders

| Cylinder, base perpendicular to wind, $\frac{\text{length}}{\text{diameter}}$ | 0 | C * | 100,000 to 200,000 |
|--|----|------|--------------------|
| " | 1 | 1.07 | " |
| " | 2 | .88 | " |
| " | 4 | .81 | " |
| " | 6 | .82 | " |
| " | 8 | .82 | " |
| " | 14 | .94 | " |

* Eiffel's values: See Table 159 for best value, 1.12.

SKIN FRICTION

The surface friction on well-varnished surfaces of thin flat plates may be expressed in the following form:

$$R_F = 0.0375 A q R^{-0.15}$$

where R_F is the frictional force on the area A exposed to the stream, q is the velocity pressure, and R the Reynolds Number based on the length of the plate parallel to the wind direction. The values in the table apply when the flow is fully turbulent as in most practical applications. (Cf. Technical Report 342 of the National Advisory Committee for Aeronautics.)

| Speed m/sec. | Skin friction kg per sq. m plane | | Speed ft./sec. | Skin friction lbs. per sq. ft. plane | |
|-----------------|--|-----------|-------------------|--|-------------|
| | 1 m long | 30 m long | | 1 ft. long | 30 ft. long |
| 10 | 0.0311 | 0.0187 | 10 | 0.00083 | 0.00050 |
| 20 | .112 | .0673 | 20 | .00303 | .00182 |
| 30 | .237 | .142 | 30 | .00641 | .00385 |
| 40 | .404 | .243 | 40 | .0109 | .00655 |
| 50 | .611 | .366 | 50 | .0164 | .00987 |
| 60 | .856 | .514 | 60 | .0231 | .0139 |
| 70 | 1.138 | .683 | 70 | .0307 | .0184 |
| 80 | 1.457 | .874 | 80 | .0393 | .0236 |
| 90 | 1.812 | 1.087 | 90 | .0488 | .0293 |
| 100 | 2.202 | 1.321 | 100 | .0594 | .0356 |
| 110 | 2.626 | 1.576 | 110 | .0708 | .0425 |
| 120 | 3.085 | 1.851 | 120 | .0831 | .0499 |
| 130 | 3.577 | 2.146 | 130 | .0964 | .0579 |
| 140 | 4.102 | 2.461 | 140 | .1106 | .0664 |
| 150 | 4.662 | 2.797 | 150 | .1256 | .0754 |
| 160 | 5.253 | 3.152 | 160 | .1416 | .0850 |
| 170 | 5.875 | 3.525 | 170 | .1584 | .0951 |
| 180 | 6.531 | 3.919 | 180 | .1761 | .1057 |
| 190 | 7.218 | 4.331 | 190 | .1946 | .1168 |
| 200 | 7.937 | 4.762 | 200 | .2140 | .1284 |

TABLE 166.—Friction

The required force F necessary to just move an object along a horizontal plane $= fN$ where N is the normal pressure on the plane and f the "coefficient of friction." The angle of repose Φ ($\tan \Phi = F/N$) is the angle at which the plane must be tilted before the object will move from its own weight. The following table of coefficients was compiled by Rankine from the results of General Morin and other authorities and is sufficient for ordinary purposes.

| Material. | f | $1/f$ | ϕ |
|---|-----------|------------|-----------|
| Wood on wood, dry | .25-.50 | 4.00-2.00 | 14.0-26.5 |
| " " soapy | .20 | 5.00 | 11.5 |
| Metals on oak, dry | .50-.60 | 2.00-1.67 | 26.5-31.0 |
| " " wet | .24-.26 | 4.17-3.85 | 13.5-14.5 |
| " " soapy | .20 | 5.00 | 11.5 |
| " " elm, dry | .20-.25 | 5.00-4.00 | 11.5-14.0 |
| Hemp on oak, dry | .53 | 1.89 | 28.0 |
| " " wet | .33 | 3.00 | 18.5 |
| Leather on oak | .27-.38 | 3.70-2.86 | 15.0-19.5 |
| " " metals, dry | .56 | 1.79 | 29.5 |
| " " wet | .36 | 2.78 | 20.0 |
| " " greasy | .23 | 4.35 | 13.0 |
| " " oily | .15 | 6.67 | 8.5 |
| Metals on metals, dry | .15-.20 | 6.67-5.00 | 8.5-11.5 |
| " " wet | .3 | 3.33 | 16.5 |
| Smooth surfaces, occasionally greased | .07-.08 | 14.3-12.50 | 4.0-4.5 |
| " " continually greased | .05 | 20.00 | 3.0 |
| " " best results | .03-.036 | 33.3-27.6 | 1.75-2.0 |
| Steel on agate, dry * | .20 | 5.00 | 11.5 |
| " " oiled * | .107 | 9.35 | 6.1 |
| Iron on stone | .30-.70 | 3.33-1.43 | 16.7-35.0 |
| Wood on stone | About .40 | 2.50 | 22.0 |
| Masonry and brick work, dry | .60-.70 | 1.67-1.43 | 33.0-35.0 |
| " " " damp mortar | .74 | 1.35 | 36.5 |
| " " on dry clay | .51 | 1.96 | 27.0 |
| " " moist clay | .33 | 3.00 | 18.25 |
| Earth on earth | .25-1.00 | 4.00-1.00 | 14.0-45.0 |
| " " dry sand, clay, and mixed earth | .38-.75 | 2.63-1.33 | 21.0-37.0 |
| " " damp clay | 1.00 | 1.00 | 45.0 |
| " " wet clay | .31 | 3.23 | 17.0 |
| " " shingle and gravel | .81-1.11 | 1.23-0.9 | 39.0-48.0 |

* Quoted from a paper by Jenkin and Ewing, "Phil. Trans. R. S." vol. 167. In this paper it is shown that in cases where "static friction" exceeds "kinetic friction" there is a gradual increase of the coefficient of friction as the speed is reduced towards zero.

TABLE 167.—Lubricants

The best lubricants are in general the following: Low temperatures, light mineral lubricating oils. Very great pressures, slow speeds, graphite, soapstone and other solid lubricants. Heavy pressures, slow speeds, ditto and lard, tallow and other greases. Heavy pressures and high speeds, sperm oil, castor oil, heavy mineral oils. Light pressures, high speeds, sperm, refined petroleum olive, rape, cottonseed. Ordinary machinery, lard oil, tallow oil, heavy mineral oils and the heavier vegetable oils. Steam cylinders, heavy mineral oils, lard, tallow. Watches and delicate mechanisms, clarified sperm, neat's-foot, porpoise, olive and light mineral lubricating oils.

TABLE 168.—Lubricants For Cutting Tools

| Material. | Turning. | Chucking. | Drilling. | Tapping Milling. | Reaming. |
|------------------|------------------------|--------------|--------------|---------------------|----------|
| Tool Steel, | dry or oil | oil or s. w. | oil | oil | lard oil |
| Soft Steel, | dry or soda water | soda water | oil or s. w. | oil | lard oil |
| Wrought iron | dry or soda water | soda water | oil or s. w. | oil | lard oil |
| Cast iron, brass | dry | dry | dry | dry | dry |
| Copper | dry | dry | dry | dry | dry |
| Glass | turpentine or kerosene | | | | mixture |

Mixture = $\frac{1}{3}$ crude petroleum, $\frac{2}{3}$ lard oil. Oil = sperm or lard.

Tables 167 and 168 quoted from "Friction and Lost Work in Machinery and Mill Work," Thurston, Wiley and Sons.

TABLE 169.—Viscosity of Fluids and Solids

The coefficient of viscosity of a substance is the tangential force required to move a unit area of a plane surface with unit speed relative to another parallel plane surface from which it is separated by a layer a unit thick of the substance. Viscosity measures the temporary rigidity it gives to the substance. The viscosity of fluids is generally measured by the rate of flow of the fluid through a capillary tube the length of which is great in comparison with its diameter. The equation generally used is

$$\mu, \text{ the viscosity, } = \frac{\gamma \pi g d^4}{128 Q (l + \lambda)} \left(h - \frac{mv^2}{g} \right),$$

where γ is the density (g/cm^3), d and l are the diameter and length in cm of the tube, Q the volume in cm^3 discharged in t sec., λ the Couette correction which corrects the measured to the effective length of the tube, h the average head in cm, m the coefficient of kinetic energy correction, mv^2/g , necessary for the loss of energy due to turbulent in distinction from viscous flow, g being the acceleration of gravity (cm/sec^2), v the mean velocity in cm per sec. (See Technologic Paper of the Bureau of Standards, 100 and 112, Herschel, 1917-1918, for discussion of this correction and λ .)

The fluidity is the reciprocal of the absolute viscosity. The kinetic viscosity is the absolute viscosity divided by the density. Specific viscosity is the viscosity relative to that of some standard substance, generally water, at some definite temperature. The dimensions of viscosity are $ML^{-1}T^{-1}$. It is generally expressed in cgs units as dyne-seconds per cm^2 or poises.

The viscosity of solids may be measured in relative terms by the damping of the oscillations of suspended wires (see Table 82). Ladenburg (1906) gives the viscosity of Venice turpentine at 18.3° as 1300 poises; Trouton and Andrews (1904) of pitch at 0° , 51×10^{10} , at 15° , 1.3×10^{10} ; of shoemakers' wax at 8° , 4.7×10^6 ; of soda glass at 575° , 11×10^{12} ; Deeley (1908) of glacier ice as 12×10^{18} .

TABLE 170.—Viscosity of Water in Centipoises (Temperature Variation)

Bingham and Jackson, Bulletin Bureau of Standards, 14, 75, 1917. Pressure effect, see p. 652.

| $^\circ\text{C.}$ | Vis- cosity. cp | $^\circ\text{C.}$ | Vis- cosity. cp | $^\circ\text{C.}$ | Vis- cosity. cp | $^\circ\text{C.}$ | Vis- cosity. cp | $^\circ\text{C.}$ | Vis- cosity. cp | $^\circ\text{C.}$ | Vis- cosity. cp | $^\circ\text{C.}$ | Vis- cosity. cp |
|-------------------|-----------------------|-------------------|-----------------------|-------------------|-----------------------|-------------------|-----------------------|-------------------|-----------------------|-------------------|-----------------------|-------------------|-----------------------|
| 0 | 1.7921 | 10 | 1.3077 | 20 | 1.0050 | 30 | 0.8007 | 40 | 0.6560 | 50 | 0.5494 | 60 | 0.4683 |
| 1 | 1.7313 | 11 | 1.2713 | 21 | 0.9810 | 31 | 0.7840 | 41 | 0.6439 | 51 | 0.5404 | 61 | 0.4355 |
| 2 | 1.6728 | 12 | 1.2373 | 22 | 0.9579 | 32 | 0.7679 | 42 | 0.6321 | 52 | 0.5315 | 70 | 0.4061 |
| 3 | 1.6101 | 13 | 1.2023 | 23 | 0.9353 | 33 | 0.7523 | 43 | 0.6207 | 53 | 0.5229 | 75 | 0.3799 |
| 4 | 1.5674 | 14 | 1.1709 | 24 | 0.9142 | 34 | 0.7371 | 44 | 0.6097 | 54 | 0.5146 | 80 | 0.3595 |
| 5 | 1.5188 | 15 | 1.1404 | 25 | 0.8937 | 35 | 0.7225 | 45 | 0.5983 | 55 | 0.5064 | 85 | 0.3355 |
| 6 | 1.4728 | 16 | 1.1111 | 26 | 0.8737 | 36 | 0.7085 | 46 | 0.5883 | 56 | 0.4985 | 90 | 0.3165 |
| 7 | 1.4284 | 17 | 1.0828 | 27 | 0.8545 | 37 | 0.6947 | 47 | 0.5782 | 57 | 0.4907 | 95 | 0.2994 |
| 8 | 1.3800 | 18 | 1.0550 | 28 | 0.8360 | 38 | 0.6814 | 48 | 0.5683 | 58 | 0.4832 | 100 | 0.2838 |
| 9 | 1.3402 | 19 | 1.0290 | 29 | 0.8180 | 39 | 0.6685 | 49 | 0.5583 | 59 | 0.4759 | 153 | 0.181* |

* de Haas, 1894. Undercooled water: -2.10° , 1.33 cp; -4.70° , 2.12 cp; -6.20° , 2.25 cp; -8.48° , 2.46 cp; -9.30° , 2.55 cp; White, Twining, J. Amer. Ch. Soc., 50, 380, 1913.

TABLE 171.—Viscosity of Alcohol-water Mixtures in Centipoises (Temperature Variation)

| ° C. | Percentage by weight of ethyl alcohol. | | | | | | | | | | | | |
|------|--|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | 0 | 10 | 20 | 30 | 39 | 40 | 45 | 50 | 60 | 70 | 80 | 90 | 100 |
| 0 | 1.792 | 3.311 | 5.319 | 6.94 | 7.25 | 7.14 | 6.94 | 6.58 | 5.75 | 4.762 | 3.690 | 2.732 | 1.773 |
| 5 | 1.519 | 2.577 | 4.005 | 5.29 | 5.62 | 5.59 | 5.50 | 5.26 | 4.63 | 3.906 | 3.125 | 2.309 | 1.623 |
| 10 | 1.308 | 2.179 | 3.165 | 4.05 | 4.39 | 4.39 | 4.35 | 4.18 | 3.77 | 3.268 | 2.710 | 2.101 | 1.460 |
| 15 | 1.140 | 1.792 | 2.618 | 3.26 | 3.52 | 3.53 | 3.51 | 3.44 | 3.14 | 2.770 | 2.309 | 1.802 | 1.332 |
| 20 | 1.005 | 1.538 | 2.183 | 2.71 | 2.88 | 2.91 | 2.88 | 2.87 | 2.67 | 2.370 | 2.008 | 1.610 | 1.200 |
| 25 | 0.894 | 1.323 | 1.815 | 2.18 | 2.35 | 2.35 | 2.39 | 2.40 | 2.24 | 2.037 | 1.748 | 1.424 | 1.096 |
| 30 | 0.801 | 1.160 | 1.553 | 1.87 | 2.00 | 2.02 | 2.02 | 2.02 | 1.93 | 1.707 | 1.531 | 1.279 | 1.003 |
| 35 | 0.722 | 1.006 | 1.332 | 1.58 | 1.71 | 1.72 | 1.73 | 1.72 | 1.60 | 1.529 | 1.355 | 1.147 | 0.914 |
| 40 | 0.656 | 0.907 | 1.100 | 1.368 | 1.473 | 1.482 | 1.495 | 1.499 | 1.447 | 1.344 | 1.203 | 1.035 | 0.834 |
| 45 | 0.599 | 0.812 | 1.015 | 1.180 | 1.284 | 1.289 | 1.307 | 1.294 | 1.271 | 1.189 | 1.081 | 0.939 | 0.794 |
| 50 | 0.549 | 0.734 | 0.907 | 1.050 | 1.124 | 1.132 | 1.148 | 1.155 | 1.127 | 1.062 | 0.968 | 0.848 | 0.702 |
| 60 | 0.469 | 0.609 | 0.736 | 0.834 | 0.885 | 0.893 | 0.907 | 0.913 | 0.902 | 0.856 | 0.780 | 0.704 | 0.592 |
| 70 | 0.406 | 0.514 | 0.608 | 0.683 | 0.725 | 0.727 | 0.740 | 0.740 | 0.729 | 0.695 | 0.650 | 0.580 | 0.504 |
| 80 | 0.356 | 0.430 | 0.505 | 0.567 | 0.598 | 0.601 | 0.600 | 0.612 | 0.604 | — | — | — | — |

Same authority as preceding table.

TABLE 172.—Viscosity and Density of Sucrose in Aqueous Solution

See Scientific Paper 208, Bingham and Jackson, Bureau of Standards, 1917, and Technologic Paper 100, Herschel, Bureau of Standards, 1917.

| Temperature. | Viscosity in centipoises. | | | | Density d_4^{25} . | | | |
|-------------------------|-----------------------------|-------|-------|-------|-----------------------------|---------|---------|---------|
| | Per cent sucrose by weight. | | | | Per cent sucrose by weight. | | | |
| | 0 | 20 | 40 | 60 | 0 | 20 | 40 | 60 |
| 0° C | 1.7921 | 3.804 | 14.77 | 238. | 0.99987 | 1.08540 | 1.18349 | 1.29560 |
| 5 | 1.5188 | 3.154 | 11.56 | 156. | 0.99999 | 1.08400 | 1.18192 | 1.29341 |
| 10 | 1.3077 | 2.652 | 9.794 | 109.8 | 0.99973 | 1.08353 | 1.18020 | 1.29117 |
| 15 | 1.1404 | 2.267 | 7.468 | 74.6 | 0.99913 | 1.08233 | 1.17837 | 1.28884 |
| 20 | 1.0050 | 1.960 | 6.200 | 56.5 | 0.99823 | 1.08094 | 1.17648 | 1.28644 |
| 30 | 0.8007 | 1.504 | 4.382 | 33.78 | 0.99568 | 1.07767 | 1.17214 | 1.28144 |
| 40 | 0.6560 | 1.193 | 3.249 | 21.28 | 0.99225 | 1.07366 | 1.16759 | 1.27615 |
| 50 | 0.5494 | 0.970 | 2.497 | 14.01 | 0.98807 | 1.06898 | 1.16248 | 1.27058 |
| 60 | 0.4688 | 0.808 | 1.982 | 9.83 | 0.98330 | 1.06358 | 1.15693 | 1.26468 |
| 70 | 0.4061 | 0.685 | 1.608 | 7.15 | | | | |
| 80 | 0.3565 | 0.590 | 1.334 | 5.40 | | | | |
| Densities due to Plato. | | | | | | | | |

TABLE 173.—Viscosity and Density of Glycerol in Aqueous Solution (20° C)

| % Glycerol. | Density, g/cm ³ | Viscosity in centipoises. | 100 × Kinematic viscosity. | % Glycerol. | Density, g/cm ³ | Viscosity in centipoises. | 100 × Kinematic viscosity. | % Glycerol. | Density, g/cm ³ | Viscosity in centipoises. | 100 × Kinematic viscosity. |
|-------------|----------------------------|---------------------------|----------------------------|-------------|----------------------------|---------------------------|----------------------------|-------------|----------------------------|---------------------------|----------------------------|
| 5 | 1.0098 | 1.181 | 1.170 | 35 | 1.0855 | 3.115 | 2.870 | 65 | 1.1662 | 14.51 | 12.44 |
| 10 | 1.0217 | 1.364 | 1.335 | 40 | 1.0989 | 3.791 | 3.450 | 70 | 1.1797 | 21.49 | 18.22 |
| 15 | 1.0337 | 1.580 | 1.529 | 45 | 1.1124 | 4.692 | 4.218 | 75 | 1.1932 | 33.71 | 28.25 |
| 20 | 1.0461 | 1.846 | 1.765 | 50 | 1.1258 | 5.908 | 5.248 | 80 | 1.2066 | 55.34 | 45.80 |
| 25 | 1.0590 | 2.176 | 2.055 | 55 | 1.1393 | 7.664 | 6.727 | 85 | 1.2201 | 102.5 | 84.01 |
| 30 | 1.0720 | 2.585 | 2.411 | 60 | 1.1528 | 10.31 | 8.943 | 90 | 1.2335 | 207.6 | 168.3 |

The kinematic viscosity is the ordinary viscosity in cgs units (poises) divided by the density.

TABLE 174.—Viscosity and Density of Castor Oil (Temperature Variation)

| ° C | Density, g/cm ³ | Viscosity in poises. | Kinematic viscosity. | ° C | Density, g/cm ³ | Viscosity in poises. | Kinematic viscosity. | ° C | Density, g/cm ³ | Viscosity in poises. | Kinematic viscosity. | ° C | Density, g/cm ³ | Viscosity in poises. | Kinematic viscosity. |
|-----|----------------------------|----------------------|----------------------|-----|----------------------------|----------------------|----------------------|-----|----------------------------|----------------------|----------------------|-----|----------------------------|----------------------|----------------------|
| 5 | .9707 | 37.6 | 38.7 | 14 | .9645 | 16.61 | 17.22 | 23 | .9583 | 7.67 | 8.00 | 32 | .9520 | 3.94 | 4.14 |
| 6 | .9700 | 34.5 | 35.5 | 15 | .9638 | 15.14 | 15.71 | 24 | .9576 | 7.06 | 7.37 | 33 | .9513 | 3.65 | 3.84 |
| 7 | .9693 | 31.6 | 32.6 | 16 | .9631 | 13.80 | 14.33 | 25 | .9569 | 6.51 | 6.80 | 34 | .9506 | 3.40 | 3.58 |
| 8 | .9686 | 28.9 | 29.8 | 17 | .9624 | 12.65 | 13.14 | 26 | .9562 | 6.04 | 6.32 | 35 | .9499 | 3.16 | 3.33 |
| 9 | .9679 | 26.4 | 27.3 | 18 | .9617 | 11.62 | 12.09 | 27 | .9555 | 5.61 | 5.87 | 36 | .9492 | 2.94 | 3.10 |
| 10 | .9672 | 24.2 | 25.0 | 19 | .9610 | 10.71 | 11.15 | 28 | .9548 | 5.21 | 5.46 | 37 | .9485 | 2.74 | 2.89 |
| 11 | .9665 | 22.1 | 22.8 | 20 | .9603 | 9.86 | 10.27 | 29 | .9541 | 4.85 | 5.08 | 38 | .9478 | 2.58 | 2.72 |
| 12 | .9659 | 20.1 | 20.8 | 21 | .9596 | 9.06 | 9.44 | 30 | .9534 | 4.51 | 4.73 | 39 | .9471 | 2.44 | 2.58 |
| 13 | .9652 | 18.2 | 18.9 | 22 | .9589 | 8.34 | 8.70 | 31 | .9527 | 4.21 | 4.42 | 40 | .9464 | 2.31 | 2.44 |

Tables 173 and 174, taken from Technologic Paper 112, Bureau of Standards, 1918. Glycerol data due to Archbutt, Deeley and Gerlach; Castor Oil to Kahlbaum and Räber. See preceding table for definition of kinematic viscosity. Archbutt and Deeley give for the density and viscosity of castor oil at 65.6° C, 0.9284 and 0.605, respectively; at 100° C, 0.9050 and 0.169.

TABLE 175.—Viscosity of Organic Liquids

Compiled from Landolt and Börnstein, 1912. Based principally on work of Thorpe and Rogers, 1894-97. Viscosity given in centipoises. One centipoise = 0.01 dyne-second per cm².

| Liquid | Viscosity in centipoises | | | | | | | | |
|----------------------------|--|-------|-------|-------|-------|-------|-------|-------|-------|
| | Formula | 0°C | 10°C | 20°C | 30°C | 40°C | 50°C | 70°C | 100°C |
| Acids: Formic..... | CH ₃ O ₂ | solid | 2.247 | 1.784 | 1.460 | 1.219 | 1.036 | .780 | .549 |
| Acetic..... | C ₂ H ₄ O ₂ | solid | solid | 1.222 | 1.040 | .905 | .796 | .631 | .465 |
| Propionic..... | C ₃ H ₆ O ₂ | 1.521 | 1.289 | 1.102 | .960 | .845 | .752 | .607 | .459 |
| Butyric..... | C ₄ H ₈ O ₂ | 2.286 | 1.851 | 1.540 | 1.304 | 1.120 | .975 | .760 | .551 |
| Alcohols: Methyl..... | CH ₃ O | .817 | .690 | .596 | .520 | .456 | .403 | | |
| Allyl..... | C ₃ H ₆ O | 2.145 | 1.705 | 1.363 | 1.168 | .914 | .763 | .553 | |
| Propyl..... | C ₃ H ₈ O | 3.883 | 2.918 | 2.256 | 1.779 | 1.405 | 1.130 | .760 | |
| i-Propyl..... | C ₃ H ₈ O | 4.565 | 3.246 | 2.370 | 1.757 | 1.331 | 1.029 | .646 | |
| Butyric..... | C ₄ H ₁₀ O | 5.186 | 3.873 | 2.948 | 2.267 | 1.782 | 1.411 | .930 | .540 |
| Aromatics: Benzol..... | C ₆ H ₆ | .906 | .763 | .654 | .567 | .498 | .444 | .359 | |
| Toluene..... | C ₇ H ₈ | .772 | .671 | .590 | .525 | .471 | .426 | .354 | .278 |
| Orthoxylene..... | C ₈ H ₁₀ | 1.105 | .937 | .810 | .709 | .627 | .560 | .458 | .352 |
| Metaxylene..... | C ₈ H ₁₀ | .806 | .702 | .620 | .552 | .497 | .451 | .375 | .296 |
| Paraxylene..... | C ₈ H ₁₀ | solid | .738 | .648 | .574 | .513 | .463 | .383 | .300 |
| Bromides: Ethyl..... | C ₂ H ₅ Br | .487 | .441 | .402 | .368 | | | | |
| Propyl..... | C ₃ H ₇ Br | .651 | .582 | .524 | .475 | .433 | .397 | .338 | |
| Ethylene..... | C ₂ H ₄ Br | 2.438 | 2.039 | 1.721 | 1.475 | 1.286 | 1.131 | .903 | .678 |
| Bromine..... | Br | 1.267 | 1.120 | 1.005 | .911 | .830 | .761 | | |
| Chlorides: Ethylene..... | C ₂ H ₄ Cl | 1.132 | .966 | .838 | .736 | .652 | .584 | .479 | |
| Chloroform..... | CHCl ₃ | .706 | .633 | .571 | .519 | .474 | .435 | | |
| Carbon-tetra..... | CCl ₄ | 1.351 | 1.138 | .975 | .848 | .746 | .662 | .534 | |
| Ethers: Diethyl..... | C ₄ H ₁₀ O | .294 | .268 | .245 | .223 | | | | |
| Methyl-propyl..... | C ₄ H ₁₀ O | .314 | .285 | .260 | .237 | | | | |
| Ethyl-propyl..... | C ₅ H ₁₂ O | .402 | .360 | .324 | .294 | .268 | .245 | | |
| Esters: Methylformate..... | C ₂ H ₄ O ₂ | .436 | .391 | .355 | .325 | | | | |
| Ethylformate..... | C ₃ H ₆ O | .510 | .454 | .408 | .369 | .336 | .308 | | |
| Methylacetate..... | C ₃ H ₆ O ₂ | .484 | .431 | .388 | .352 | .320 | .293 | | |
| Ethylacetate..... | C ₄ H ₈ O ₂ | .582 | .512 | .455 | .407 | .367 | .333 | .279 | |
| Iodides: Methyl..... | CH ₃ I | .606 | .548 | .500 | .460 | .424 | | | |
| Ethyl..... | C ₂ H ₅ I | .727 | .654 | .592 | .540 | .495 | .456 | .391 | |
| Propyl..... | C ₃ H ₇ I | .944 | .833 | .744 | .669 | .607 | .552 | .466 | .371 |
| Allyl..... | C ₃ H ₅ I | .936 | .826 | .734 | .660 | .597 | .544 | .458 | .365 |
| Paraffines: Pentane..... | C ₅ H ₁₂ | .289 | .262 | .240 | .220 | | | | |
| Hexane..... | C ₆ H ₁₄ | .401 | .360 | .326 | .296 | .271 | .248 | | |
| i-Hexane..... | C ₆ H ₁₄ | .376 | .338 | .306 | .279 | .254 | .233 | | |
| Heptane..... | C ₇ H ₁₆ | .524 | .465 | .416 | .375 | .341 | .310 | .262 | |
| i-Heptane..... | C ₇ H ₁₆ | .481 | .428 | .384 | .347 | .315 | .288 | .243 | |
| Octane..... | C ₈ H ₁₈ | .706 | .616 | .542 | .483 | .433 | .391 | .324 | .252 |
| Sulphides: Carbon di..... | CS ₂ | .438 | .405 | .376 | .352 | .330 | | | |
| Turpentine..... | | 2.248 | 1.783 | 1.487 | 1.272 | 1.071 | .926 | .728 | |

Table 176.—Fluidities of Gasolines and Kerosene (Temperature Variation)

(Henschel, Bur. Standards, Techn. Paper, 125, 1919.)

| Sp. gr. 15°/6/15°/6 | Temperature | | | | | | Sp. gr. 15°/6/15°/6 | Temperature | | | | | |
|------------------------|-------------|------|------|------|------|------|------------------------|-------------|------|------|------|------|------|
| | 5°C | 15°C | 25°C | 35°C | 45°C | 55°C | | 5°C | 15°C | 25°C | 35°C | 45°C | 55°C |
| 0.757 | 145 | 166 | 193 | 212 | 235 | 262 | 0.702 | 233 | 261 | 296 | 321 | 358 | 400 |
| .748 | 130 | 151 | 170 | 194 | 214 | 243 | .701 | 230 | 262 | 287 | 333 | 373 | 398 |
| .743 | 129 | 156 | 185 | 203 | 227 | ... | .699 | 233 | 269 | 306 | 335 | 372 | 423 |
| .726 | 202 | 233 | 264 | 293 | 324 | 360 | .694 | 251 | 286 | 316 | 354 | 387 | 427 |
| .722 | 189 | 219 | 244 | 278 | 308 | 342 | .680 | 288 | 323 | 365 | 413 | 441 | 475 |
| .716 | 197 | 217 | 256 | 289 | 321 | 341 | .813 | } 39 | 47 | 61 | 71 | 84 | ... |
| .708 | 203 | 230 | 257 | 292 | 332 | 260 | Kerosene | | | | | | |

PRESSURE EFFECT ON VISCOSITY OF PURE LIQUIDS

This table gives \log_{10} of the relative viscosity as a function of pressure and density, the viscosity at 30°C and atmospheric pressure taken as unity. Bridgman, Proc. Amer. Acad., 61, 59, 1926, which see for further liquids. For each compound first line $\log \eta/\eta_0$ at 30°C, second line at 75°C, third line η_{30}/η_{75} .

| Substance | Pressure kg/cm ² | | | | | | | | | | η_{30} |
|----------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|-------------------------------|--------------------------------|--------------------------------|--------------------------------|--------|-------------|
| | 1 | 500 | 1000 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | | |
| Methyl alcohol... | .000 9.769 1.702 .000 | .094 9.862 1.706 .107 | .167 9.933 1.714 .200 | .286 9.933 1.750 .363 | .471 1.208 1.832 .617 | .616 .334 1.914 .829 | .750 .448 2.004 1.023 | .874 .555 2.084 1.211 | .998 .655 2.203 1.390 | .00520 | |
| Ethyl alcohol... | 9.657 2.203 .000 | 9.772 2.163 .151 | 9.873 2.123 .283 | .045 2.080 .494 | .289 2.128 .836 | .473 2.270 1.131 | .634 2.449 1.402 | .778 2.710 1.667 | .919 2.958 1.915 | | |
| n-propyl alcohol... | 9.598 2.523 .000 | 9.754 2.495 .175 | 9.880 2.529 .321 | .074 2.630 .554 | .368 2.938 .934 | .610 3.319 1.289 | .827 3.758 1.609 | 1.033 4.305 1.912 | 1.223 4.920 2.208 | | .01779 |
| n-butyl alcohol... | 2.845 2.884 .000 | 2.838 2.917 .188 | 2.858 2.951 .341 | 2.932 3.177 .607 | 3.343 3.926 1.060 | 3.991 4.742 1.448 | 4.679 5.781 1.811 | 5.521 7.096 2.164 | 6.518 8.570 2.495 | .02237 | |
| n-amyl alcohol... | 9.540 2.884 .000 | 9.723 2.917 .181 | 9.871 2.951 .315 | .105 3.177 .524 | .466 3.926 .847 | .772 4.742 1.112 | 1.049 5.781 1.360 | 1.313 7.096 1.615 | 1.562 8.570 1.846 | | |
| n-pentane... | 9.811 1.545 .000 | .014 1.469 .184 | .163 1.419 .332 | .380 1.393 .561 | .676 1.483 .914 | .908 1.600 1.224 | 1.119 1.742 1.514 | 1.313 2.004 1.803 | 1.493 2.254 1.803 | | .00296 |
| n-hexane... | 9.803 1.574 .000 | .028 1.432 .134 | .171 1.449 .242 | .379 1.521 .405 | .701 1.633 .649 | .961 1.832 .837 | 1.198 2.070 1.008 | 1.426 2.382 1.172 | 1.646 2.782 1.323 | .00368 | |
| Ethyl chloride... | 9.850 1.413 .000 | .017 1.309 .121 | .131 1.291 .222 | .285 1.318 .387 | .514 1.365 .631 | .683 1.426 .854 | .834 1.493 1.043 | .977 1.567 1.223 | 1.111 1.633 1.400 | | |
| Ethyl bromide... | 9.806 1.567 .000 | 9.959 1.452 .115 | .072 1.413 .218 | .235 1.419 .385 | .472 1.442 .656 | .653 1.589 .888 | .816 1.687 1.108 | .978 1.758 1.330 | 1.123 1.892 1.549 | | .00285 |
| Ethyl iodide... | 9.837 1.455 .000 | 9.954 1.449 .135 | .057 1.445 .226 | .227 1.439 .373 | .467 1.545 .605 | .672 1.644 .804 | .854 1.795 .987 | 1.030 1.995 1.160 | 1.200 2.234 1.160 | .00285 | |
| Acetone... | 9.895 1.274 .000 | .017 1.312 .134 | .113 1.297 .260 | .245 1.343 .497 | .445 1.445 .936 | .610 1.563 1.346 | .762 1.679 1.741 | .898 1.828 2.133 | 1.031 1.828 2.133 | | |
| Glycerine... | 8.810 15.49 .000 | 8.920 16.37 .190 | 9.023 17.26 .351 | 9.204 19.63 .493 | 9.529 25.53 (1500) | 9.818 33.73 (1500) | .094 44.36 (1500) | .369 58.08 (1500) | .628 (1500) | | .00845 |
| CCl ₄ ... | 9.760 1.738 .000 | 9.949 1.742 .110 | .100 1.782 .211 | .349 .386 .493 | .542 .660 .884 | | | | | .00519 | |
| Chloroform... | 9.858 1.387 .000 | 9.985 1.334 .090 | .094 1.309 .160 | .251 1.365 .307 | .480 1.514 .509 | .691 1.560 .674 | .914 1.560 .840 | 1.141 1.560 1.010 | 1.189 1.560 1.189 | | |
| CS ₂ ... | 9.875 1.334 .000 | 9.972 1.312 .189 | .051 1.285 .324 | .180 1.340 .514 | .372 1.371 .792 | .527 1.403 1.042 | .671 1.476 1.261 | .808 1.592 1.469 | .946 1.750 1.670 | | .00212 |
| Ether... | 9.878 1.324 .000 | .024 1.462 .173 | .149 1.496 .347 | .344 1.479 .308 | .601 1.552 .498 | .806 1.722 (3000) | .986 1.884 (3000) | 1.155 2.061 (3000) | 1.311 2.286 (3000) | .00566 | |
| Benzene... | 9.765 1.718 .000 | 9.938 1.718 .145 | .081 1.845 .274 | .308 .497 .597 | .498 .897 1.285 | | | | | | |
| Toluene... | 9.796 1.600 .000 | 9.939 1.607 .288 | .065 1.618 .541 | .267 1.698 1.652 | .597 1.995 (3000) | .896 2.449 (5000) | 1.186 3.258 (5000) | 1.504 4.710 (5000) | 1.832 (5000) | | .00523 |
| Eugenol... | 9.429 3.724 | 9.616 4.699 | 9.810 5.383 | .143 8.670 | .805 29.38 | 1.520 | 2.343 | | | | |

VISCOSITY OF MISCELLANEOUS LIQUIDS

Viscosities are given in cgs units, dyne-seconds per cm², or poises.

| Liquid. | ° C | Viscosity. | Refer- ence. | Liquid. | ° C | Viscosity. | Refer- ence. |
|-----------------------------|------------------------------|----------------------|-----------------|-----------------------|-------|------------|-----------------|
| Acetaldehyde..... | 0. | 0.00275 | 1 | * Dark cylinder..... | 37.8 | 7.324 | 10 |
| "..... | 10. | 0.00252 | 1 | " " Extra L. L."..... | 100.0 | 0.341 | 10 |
| "..... | 20. | 0.00231 | 1 | "..... | 37.8 | 11.156 | 10 |
| Air..... | -102.3 | 0.00172 | 2 | "..... | 100.0 | 0.451 | 10 |
| Aniline..... | 20. | 0.04407 | 3 | Linseed .925 †..... | 30. | 0.331 | 9 |
| "..... | 60. | 0.0150 | 3 | "..... | 50. | 0.176 | 9 |
| Bismuth..... | 285. | 0.0161 | 4 | "..... | 90. | 0.071 | 9 |
| "..... | 305. | 0.0146 | 4 | Olive .9195..... | 10. | 1.38 | 11 |
| Copal lac..... | 22. | 4.80 | 5 | "..... | 15. | 1.075 | 11 |
| Glycerine..... | 2.8 | 42.2 | 6 | "..... | 20. | 0.840 | 11 |
| "..... | 14.3 | 13.87 | 6 | "..... | 30. | 0.540 | 11 |
| "..... | 20.3 | 8.30 | 6 | "..... | 40. | 0.363 | 11 |
| "..... | 26.5 | 4.94 | 6 | "..... | 50. | 0.258 | 11 |
| "..... | 80.31° H ₂ O..... | 8.5 | 1.021 | "..... | 70. | 0.124 | 11 |
| "..... | 64.05° H ₂ O..... | 8.5 | 0.222 | † Rape..... | 15.6 | 1.118 | 10 |
| "..... | 49.79° H ₂ O..... | 8.5 | 0.002 | "..... | 37.8 | 0.422 | 10 |
| Hydrogen, liquid..... | — | 0.00011 | 2 | "..... | 100.0 | 0.080 | 10 |
| Menthol, solid..... | 14.9 | 2 × 10 ¹² | 7 | " (another)..... | 15.6 | 1.176 | 10 |
| " liquid..... | 56.0 | 0.060 | 7 | " (another)..... | 100.0 | 0.085 | 10 |
| Mercury..... | -20. | 0.0184 | 8 | Soya bean .919 †..... | 30.0 | 0.406 | 9 |
| "..... | 0. | 0.01601 | 4 | "..... | 50.0 | 0.206 | 9 |
| "..... | 20. | 0.01547 | 4 | "..... | 90.0 | 0.078 | 9 |
| "..... | 34. | 0.01476 | 4 | † Sperm..... | 15.6 | 0.420 | 10 |
| "..... | 08. | 0.01263 | 4 | "..... | 37.8 | 0.185 | 10 |
| "..... | 103. | 0.01079 | 4 | "..... | 100.0 | 0.046 | 10 |
| "..... | 299. | 0.00075 | 4 | Paraffins: | | | |
| Oils: | | | | Pentane..... | 21.0 | 0.0026 | 12 |
| Dogfish-liver .923 †..... | 30. | 0.414 | 9 | Hexane..... | 23.7 | 0.0033 | 12 |
| "..... | 50. | 0.211 | 9 | Heptane..... | 24.0 | 0.0045 | 12 |
| "..... | 90. | 0.080 | 9 | Octane..... | 22.2 | 0.0053 | 12 |
| Linseed .925..... | 30. | 0.331 | 9 | Nonane..... | 22.3 | 0.0062 | 12 |
| "..... | 50. | 0.176 | 9 | Decane..... | 22.3 | 0.0077 | 12 |
| "..... | 90. | 0.071 | 9 | Undecane..... | 22.7 | 0.0095 | 12 |
| * Spindle oil .885..... | 15.6 | 0.453 | 10 | Dodecane..... | 23.3 | 0.0126 | 12 |
| "..... | 37.8 | 0.162 | 10 | Tridecane..... | 23.3 | 0.0155 | 12 |
| "..... | 100.0 | 0.033 | 10 | Tetradecane..... | 21.9 | 0.0213 | 12 |
| * Light machinery..... | 15.6 | 1.138 | 10 | Pentadecane..... | 22.0 | 0.0281 | 12 |
| * Light machinery..... | 37.8 | 0.342 | 10 | Hexadecane..... | 22.2 | 0.0359 | 12 |
| "..... | 100.0 | 0.049 | 10 | Phenol..... | 18.3 | 0.1274 | 13 |
| * "Solar red" engine..... | 15.6 | 1.915 | 10 | "..... | 90.0 | 0.0126 | 13 |
| "..... | 37.8 | 0.496 | 10 | Sulphur..... | 170. | 320.0 | 14 |
| * "Bayonne" engine..... | 15.6 | 2.172 | 10 | "..... | 180. | 550.0 | 14 |
| "..... | 37.8 | 0.572 | 10 | "..... | 187. | 560.0 | 14 |
| * "Queen's red" engine..... | 15.6 | 0.063 | 10 | "..... | 200. | 500.0 | 14 |
| "..... | 37.8 | 0.711 | 10 | "..... | 250. | 104.0 | 14 |
| "..... | 100.0 | 0.070 | 10 | "..... | 300. | 24.0 | 14 |
| * "Galena" axle oil..... | 15.6 | 4.366 | 10 | "..... | 340. | 6.2 | 14 |
| "..... | 37.8 | 0.909 | 10 | "..... | 380. | 2.5 | 14 |
| * Heavy machinery..... | 15.6 | 6.606 | 10 | "..... | 420. | 1.13 | 14 |
| "..... | 37.8 | 1.274 | 10 | "..... | 448. | 0.80 | 14 |
| * Filtered cylinder..... | 37.8 | 2.406 | 10 | † Tallow..... | 66. | 0.176 | 10 |
| "..... | 100.0 | 0.187 | 10 | "..... | 100. | 0.078 | 10 |
| * Dark cylinder..... | 37.8 | 4.224 | 10 | Zinc..... | 280. | 0.0168 | 4 |
| "..... | 100.0 | 0.240 | 10 | "..... | 357. | 0.0142 | 4 |
| | | | | "..... | 389. | 0.0131 | 4 |

* American mineral oils; based on water as .0028 at 20° C. † Based on water as per 1st footnote. ‡ Densities. References: (1) Thorpe and Rodger, 1894-7; (2) Verschaffelt, Sc. Ab. 1917; (3) Wijkander, 1879; (4) Plüss, Z. An. Ch. 93, 1915; (5) Metz, C. R. 1903; (6) Schöttner, Wien. Ber. 77, 1878, 79, 1879; (7) Heydweiller, W. Ann. 63, 1897; (8) Koch, W. Ann. 14, 1881; (9) White, Bul. Bur. Fish. 32, 1912; (10) Archbutt-Deeley, Lubrication and Lubricants, 1912; (11) Higgins, Nat. Phys. Lab. 11, 1914; (12) Bartolli, Stracciati, 1885-6; (13) Scarpa, 1902-4; (14) Rottinganz, Z. Ph. Ch. 62, 1908.

Ratio of Viscosity at High to that at Atmospheric Pressure.

| Pressure tons/in ² | Kg/cm ² | Bayonne oil (mineral) | FFF cylinder (mineral) | Trotter (animal) | Rape (vegetable) | castor | Sperm (fish) |
|----------------------------------|--------------------|--------------------------|---------------------------|---------------------|---------------------|--------|-----------------|
| 1 | 157.5 | 1.3 | 1.4 | 1.2 | 1.1 | 1.2 | 1.2 |
| 2 | 315. | 2.0 | 2.0 | 1.6 | 1.4 | 1.6 | 1.5 |
| 4 | 630. | 4.0 | 4.5 | 2.4 | 2.3 | 2.7 | 2.4 |
| 6 | 945. | 7.8 | 8.9 | 3.5 | 3.5 | 4.2 | 3.5 |
| 8 | 1260. | 10.1 | — | 5.0 | — | 5.8 | — |

Hyde, Pr. Roy. Soc. 97A, 240, 1920.

TABLE 179
SPECIFIC VISCOSITY OF SOLUTIONS

(Density and temperature variation)

This table shows the effect of change of concentration and change of temperature on the viscosity of solutions of salts in water. The specific viscosity $\times 100$ is given for one or more densities and for several temperatures in the case of each solution. μ stands for specific viscosity, and t for temperature Centigrade.

(Abridged from earlier editions of these tables.)

| Salt | Per-centage by weight of salt in solution | Density | μ | t | μ | t | μ | t | μ | t | Authority |
|---|---|---------|-------|-----|-------|-----|-------|-----|-------|-----|-----------|
| BaCl ₂ | 7.60 | | 77.9 | 10 | 44.0 | 30 | 35.2 | 50 | | .. | Sprung |
| " | 24.34 | | 100.7 | " | 66.2 | " | 47.7 | " | | .. | " |
| Ba(NO ₃) ₂ | 2.98 | 1.027 | 62.0 | 15 | 51.1 | 25 | 42.4 | 35 | 34.8 | 45 | Wagner |
| CaCl ₂ | 15.17 | | 110.9 | 10 | 71.3 | 30 | 50.3 | 50 | | .. | " |
| " | 31.60 | | 272.5 | " | 177.0 | " | 124.0 | " | | .. | Sprung |
| " | 39.75 | | 670.0 | " | 379.0 | " | 245.5 | " | | .. | " |
| " | 44.09 | | | .. | 593.1 | " | 363.2 | " | | .. | " |
| Ca(NO ₃) ₂ | 17.55 | 1.171 | 93.8 | 15 | 74.6 | 25 | 60.0 | 35 | 49.9 | 45 | Wagner |
| " | 40.13 | 1.386 | 242.6 | " | 217.1 | " | 156.5 | " | 128.1 | " | " |
| CdCl ₂ | 11.09 | 1.109 | 77.5 | " | 60.5 | " | 49.1 | " | 40.7 | " | " |
| Cd(NO ₃) ₂ | 7.81 | 1.074 | 61.9 | " | 50.1 | " | 41.1 | " | 34.0 | " | " |
| " | 22.36 | 1.241 | 85.1 | " | 69.0 | " | 57.3 | " | 47.5 | " | " |
| CoCl ₂ | 7.97 | 1.081 | 83.0 | " | 65.1 | " | 53.6 | " | 44.9 | " | " |
| " | 22.27 | 1.264 | 161.6 | " | 126.6 | " | 101.6 | " | 85.6 | " | " |
| Co(NO ₃) ₂ | 8.28 | 1.073 | 74.7 | " | 57.9 | " | 48.7 | " | 39.8 | " | " |
| " | 24.53 | 1.229 | 110.4 | " | 88.0 | " | 71.5 | " | 59.1 | " | " |
| CuCl ₂ | 12.01 | 1.104 | 87.2 | " | 67.8 | " | 55.1 | " | 45.6 | " | " |
| " | 21.35 | 1.215 | 121.5 | " | 95.8 | " | 77.0 | " | 63.2 | " | " |
| " | 33.03 | 1.331 | 178.4 | " | 137.2 | " | 107.6 | " | 87.1 | " | " |
| Cu(NO ₃) ₂ | 18.99 | 1.177 | 97.3 | " | 76.0 | " | 61.5 | " | 51.3 | " | " |
| " | 46.71 | 1.536 | 382.9 | " | 283.8 | " | 215.3 | " | 172.2 | " | " |
| CuSO ₄ | 6.79 | 1.055 | 79.6 | " | 61.8 | " | 49.8 | " | 41.4 | " | " |
| " | 12.57 | 1.115 | 98.2 | " | 74.0 | " | 59.7 | " | 52.0 | " | " |
| " | 17.49 | 1.163 | 124.5 | " | 96.8 | " | 75.9 | " | 61.8 | " | " |
| HCl | 8.14 | 1.037 | 71.0 | " | 57.9 | " | 48.3 | " | 40.1 | " | " |
| " | 16.12 | 1.084 | 80.0 | " | 66.5 | " | 56.4 | " | 48.1 | " | " |
| " | 23.04 | 1.114 | 91.8 | " | 79.9 | " | 65.9 | " | 56.4 | " | " |
| HgCl ₂ | 3.55 | 1.033 | 76.75 | 10 | 59.2 | 20 | 46.6 | 30 | 38.3 | 40 | " |
| HNO ₃ | 8.37 | 1.067 | 66.4 | 15 | 54.8 | 25 | 45.4 | 35 | 37.6 | 45 | " |
| " | 12.20 | 1.116 | 69.5 | " | 57.3 | " | 47.9 | " | 40.7 | " | " |
| " | 28.31 | 1.178 | 80.3 | " | 65.5 | " | 54.9 | " | 46.2 | " | " |
| H ₂ SO ₄ | 7.87 | 1.065 | 77.8 | " | 61.0 | " | 50.0 | " | 41.7 | " | " |
| " | 15.50 | 1.130 | 95.1 | " | 75.0 | " | 60.5 | " | 49.8 | " | " |
| " | 23.43 | 1.200 | 122.7 | " | 95.5 | " | 77.5 | " | 64.3 | " | " |
| KCl | 10.23 | | 70.0 | 10 | 46.1 | 30 | 33.1 | 50 | | .. | Sprung |
| " | 22.21 | | 70.0 | " | 48.6 | " | 36.4 | " | | .. | " |
| KBr | 23.16 | | 66.2 | " | 44.7 | " | 33.2 | " | | .. | " |
| " | 34.64 | | 66.6 | " | 47.0 | " | 35.7 | " | | .. | " |
| KI | 8.42 | | 69.5 | " | 44.0 | " | 31.3 | " | | .. | " |
| " | 33.03 | | 61.8 | " | 42.9 | " | 32.4 | " | | .. | " |
| " | 54.00 | | 68.8 | " | 48.5 | " | 37.6 | " | | .. | " |
| KClO ₃ | 5.69 | | | .. | 45.0 | " | 31.4 | " | | .. | " |
| KNO ₃ | 6.32 | | 70.8 | " | 44.6 | " | 31.8 | " | | .. | " |
| " | 17.60 | | 68.8 | " | 46.0 | " | 33.4 | " | | .. | " |
| K ₂ SO ₄ | 5.17 | | 77.4 | " | 48.6 | " | 34.3 | " | | .. | " |
| " | 9.77 | | 81.0 | " | 52.0 | " | 36.9 | " | | .. | " |
| K ₂ CrO ₄ | 11.93 | | 75.8 | " | 62.5 | " | 41.0 | 40 | | .. | " |
| " | 32.78 | | 109.5 | " | 88.9 | " | 62.6 | " | | .. | " |
| K ₂ Cr ₂ O ₇ | 6.97 | 1.049 | 73.1 | " | 56.4 | 20 | 45.5 | 30 | 37.7 | 40 | Slotte |
| Mg(NO ₃) ₂ | 18.62 | 1.102 | 99.8 | 15 | 81.3 | 25 | 66.5 | 35 | 56.2 | 45 | Wagner |
| " | 39.77 | 1.430 | 317.0 | " | 250.0 | " | 191.4 | " | 158.1 | " | " |
| MgSO ₄ | 4.98 | | 96.2 | 10 | 59.0 | 30 | 40.9 | 50 | | .. | Sprung |
| " | 19.32 | | 302.2 | " | 166.4 | " | 106.0 | " | | .. | " |
| MnCl ₂ | 8.01 | 1.096 | 92.8 | 15 | 71.1 | 25 | 57.5 | 35 | 48.1 | 45 | Wagner |
| " | 40.13 | 1.453 | 537.3 | " | 393.4 | " | 300.4 | " | 246.5 | " | " |

SPECIFIC VISCOSITY OF SOLUTIONS

(Density and temperature variation)

(Abridged from earlier editions)

| Salt | Per- centage by weight of salt in solution | Density | μ | t | μ | t | μ | t | μ | t | Authority |
|--|---|---------|-------|-----|-------|-----|-------|-----|-------|-----|-----------|
| Mn(NO ₃) ₂ | 18.31 | 1.148 | 96.0 | 15 | 76.4 | 25 | 64.5 | 35 | 55.6 | 45 | Wagner |
| " | 49.31 | 1.506 | 396.8 | " | 301.1 | " | 221.0 | " | 188.8 | " | " |
| MnSO ₄ | 11.45 | 1.147 | 129.4 | " | 98.6 | " | 78.3 | " | 63.4 | " | " |
| " | 22.08 | 1.306 | 661.8 | " | 474.3 | " | 347.9 | " | 266.8 | " | " |
| NaCl | 7.95 | | 82.4 | 10 | 52.0 | 30 | 31.8 | 50 | | .. | Sprung |
| " | 14.31 | | 94.8 | " | 60.1 | " | 36.9 | " | | .. | " |
| " | 23.22 | | 128.3 | " | 79.4 | " | 47.4 | " | | .. | " |
| NaBr | 9.77 | | 75.6 | " | 48.7 | " | 34.4 | " | | .. | " |
| " | 18.58 | | 82.6 | " | 53.5 | " | 38.2 | " | | .. | " |
| " | 27.27 | | 95.9 | " | 61.7 | " | 43.8 | " | | .. | " |
| NaI | 8.83 | | 73.1 | " | 46.0 | " | 32.4 | " | | .. | " |
| " | 17.15 | | 73.8 | " | 47.4 | " | 33.7 | " | | .. | " |
| " | 55.47 | | 157.2 | " | 96.4 | " | 66.9 | " | | .. | " |
| NaClO ₃ | 11.50 | | 78.7 | " | 50.0 | " | 35.3 | " | | .. | " |
| " | 33.54 | | 121.0 | " | 75.7 | " | 53.0 | " | | .. | " |
| NaNO ₃ | 7.25 | | 75.6 | " | 47.9 | " | 33.8 | " | | .. | " |
| " | 18.20 | | 87.0 | " | 55.9 | " | 39.3 | " | | .. | " |
| " | 31.55 | | 121.2 | " | 76.2 | " | 53.4 | " | | .. | " |
| Na ₂ SO ₄ | 4.98 | | 96.2 | " | 59.0 | " | 40.9 | " | | .. | " |
| " | 14.03 | | 187.9 | " | 107.4 | " | 71.1 | " | | .. | " |
| " | 19.32 | | 302.2 | " | 166.4 | " | 106.0 | " | | .. | " |
| Na ₂ CrO ₄ | 10.62 | 1.112 | 103.3 | " | 79.3 | " | 63.5 | 30 | 52.3 | 40 | Slotte |
| " | 14.81 | 1.164 | 127.5 | " | 97.1 | " | 77.3 | " | 63.0 | " | " |
| NH ₄ Cl | 3.67 | | 71.5 | " | 45.0 | " | 31.9 | 50 | | .. | Sprung |
| " | 15.68 | | 67.3 | " | 46.2 | " | 34.0 | " | | .. | " |
| " | 23.37 | | 67.4 | " | 47.7 | " | 36.1 | " | | .. | " |
| NH ₄ Br | 15.97 | | 65.2 | " | 43.2 | " | 31.5 | " | | .. | " |
| " | 36.88 | | 62.4 | " | 44.6 | " | 34.3 | " | | .. | " |
| NH ₄ NO ₃ | 5.97 | | 69.6 | " | 44.3 | " | 31.6 | " | | .. | " |
| " | 27.08 | | 67.0 | " | 47.7 | " | 34.9 | " | | .. | " |
| " | 49.83 | | 81.1 | " | 63.3 | " | 48.9 | " | | .. | " |
| (NH ₄) ₂ SO ₄ | 8.10 | | 107.9 | " | 52.3 | " | 37.0 | " | | .. | " |
| " | 25.51 | | 148.4 | " | 74.8 | " | 54.1 | " | | .. | " |
| (NH ₄) ₂ CrO ₄ | 19.75 | 1.120 | 88.2 | " | 70.0 | 20 | 57.8 | 30 | 48.4 | .. | Slotte |
| " | 28.04 | 1.173 | 101.1 | " | 80.7 | " | 60.8 | " | 56.4 | .. | " |
| (NH ₄) ₂ Cr ₂ O ₇ | 13.00 | 1.078 | 72.6 | " | 57.2 | " | 46.8 | " | 39.1 | 40 | " |
| " | 19.93 | 1.126 | 77.6 | " | 58.8 | " | 48.7 | " | 40.9 | " | " |
| NiCl ₂ | 11.45 | 1.109 | 90.4 | 15 | 70.0 | 25 | 57.5 | 35 | 48.2 | 45 | Wagner |
| " | 30.40 | 1.337 | 229.5 | " | 171.8 | " | 139.2 | " | 111.9 | " | " |
| Ni(NO ₃) ₂ | 16.49 | 1.136 | 90.7 | " | 70.1 | " | 57.4 | " | 48.9 | " | " |
| " | 40.95 | 1.388 | 222.6 | " | 169.7 | " | 128.2 | " | 152.4 | " | " |
| Pb(NO ₃) ₂ | 17.93 | 1.179 | 74.0 | " | 59.1 | " | 48.5 | " | 40.3 | " | " |
| " | 32.22 | 1.362 | 91.8 | " | 72.5 | " | 59.6 | " | 50.6 | " | " |
| Sr(NO ₃) ₂ | 10.29 | 1.088 | 69.3 | " | 56.0 | " | 45.9 | " | 39.1 | " | " |
| " | 32.61 | 1.307 | 116.9 | " | 93.3 | " | 76.7 | " | 62.3 | " | " |
| ZnCl ₂ | 15.33 | 1.146 | 93.6 | " | 72.7 | " | 57.8 | " | 48.2 | " | " |
| " | 23.49 | 1.229 | 111.5 | " | 86.6 | " | 69.8 | " | 57.5 | " | " |
| " | 33.78 | 1.343 | 151.7 | " | 117.9 | " | 90.0 | " | 72.6 | " | " |
| Zn(NO ₃) ₂ | 15.95 | 1.115 | 80.7 | " | 64.3 | " | 52.6 | " | 43.8 | " | " |
| " | 30.23 | 1.229 | 104.7 | " | 85.7 | " | 69.5 | " | 57.7 | " | " |
| " | 44.50 | 1.437 | 167.9 | " | 130.6 | " | 105.4 | " | 87.9 | " | " |
| ZnSO ₄ | 7.12 | 1.106 | 97.1 | " | 79.3 | " | 62.7 | " | 51.5 | " | " |
| " | 16.64 | 1.195 | 156.0 | " | 118.6 | " | 94.2 | " | 73.5 | " | " |
| " | 23.09 | 1.281 | 232.8 | " | 177.4 | " | 135.2 | " | 108.1 | " | " |

SPECIFIC VISCOSITY OF SOLUTIONS (VARIOUS CONCENTRATIONS, 25°C)

| Dissolved salt. | Normal solution. | | $\frac{1}{2}$ normal. | | $\frac{1}{4}$ normal. | | $\frac{1}{8}$ normal. | | Authority. |
|-------------------------------------|------------------|---------------------|-----------------------|---------------------|-----------------------|---------------------|-----------------------|---------------------|------------|
| | Density. | Specific viscosity. | Density. | Specific viscosity. | Density. | Specific viscosity. | Density. | Specific viscosity. | |
| Acids : Cl_2O_3 . . | 1.0562 | 1.012 | 1.0283 | 1.003 | 1.0143 | 1.000 | 1.0074 | 0.999 | Reyher |
| HCl . . . | 1.0177 | 1.067 | 1.0092 | 1.034 | 1.0045 | 1.017 | 1.0025 | 1.009 | " |
| HClO_3 . . | 1.0485 | 1.052 | 1.0244 | 1.025 | 1.0126 | 1.014 | 1.0064 | 1.006 | " |
| HNO_3 . . | 1.0332 | 1.027 | 1.0168 | 1.011 | 1.0086 | 1.005 | 1.0044 | 1.003 | " |
| H_2SO_4 . . | 1.0303 | 1.090 | 1.0154 | 1.043 | 1.0074 | 1.022 | 1.0035 | 1.008 | Wagner |
| Aluminium sulphate | 1.0550 | 1.406 | 1.0278 | 1.178 | 1.0138 | 1.082 | 1.0068 | 1.038 | " |
| Barium chloride . . | 1.0884 | 1.123 | 1.0441 | 1.057 | 1.0226 | 1.026 | 1.0114 | 1.013 | " |
| " nitrate . . | — | — | 1.0518 | 1.044 | 1.0259 | 1.021 | 1.0130 | 1.008 | " |
| Calcium chloride . . | 1.0446 | 1.156 | 1.0218 | 1.076 | 1.0105 | 1.036 | 1.0050 | 1.017 | " |
| " nitrate . . | 1.0596 | 1.117 | 1.0300 | 1.053 | 1.0151 | 1.022 | 1.0076 | 1.008 | " |
| Cadmium chloride . . | 1.0779 | 1.134 | 1.0394 | 1.063 | 1.0197 | 1.031 | 1.0098 | 1.020 | " |
| " nitrate . . | 1.0954 | 1.165 | 1.0479 | 1.074 | 1.0249 | 1.038 | 1.0119 | 1.018 | " |
| " sulphate . . | 1.0973 | 1.348 | 1.0487 | 1.157 | 1.0244 | 1.078 | 1.0120 | 1.033 | " |
| Cobalt chloride . . | 1.0571 | 1.204 | 1.0286 | 1.097 | 1.0144 | 1.048 | 1.0058 | 1.023 | " |
| " nitrate . . | 1.0728 | 1.166 | 1.0369 | 1.075 | 1.0184 | 1.032 | 1.0094 | 1.018 | " |
| " sulphate . . | 1.0750 | 1.354 | 1.0383 | 1.160 | 1.0193 | 1.077 | 1.0110 | 1.040 | " |
| Copper chloride . . | 1.0624 | 1.205 | 1.0313 | 1.098 | 1.0158 | 1.047 | 1.0077 | 1.027 | " |
| " nitrate . . | 1.0755 | 1.179 | 1.0372 | 1.080 | 1.0185 | 1.040 | 1.0092 | 1.018 | " |
| " sulphate . . | 1.0790 | 1.358 | 1.0402 | 1.160 | 1.0205 | 1.080 | 1.0103 | 1.038 | " |
| Lead nitrate . . . | 1.1380 | 1.101 | 0.6699 | 1.042 | 1.0351 | 1.017 | 1.0175 | 1.007 | " |
| Lithium chloride . . | 1.0243 | 1.142 | 1.0129 | 1.066 | 1.0062 | 1.031 | 1.0030 | 1.012 | " |
| " sulphate . . | 1.0453 | 1.290 | 1.0234 | 1.137 | 1.0115 | 1.065 | 1.0057 | 1.032 | " |
| Magnesium chloride | 1.1375 | 1.201 | 1.0188 | 1.094 | 1.0091 | 1.044 | 1.0043 | 1.021 | " |
| " nitrate . . | 1.0512 | 1.171 | 1.0259 | 1.082 | 1.0130 | 1.040 | 1.0066 | 1.020 | " |
| " sulphate . . | 1.0584 | 1.367 | 1.0297 | 1.164 | 1.0152 | 1.078 | 1.0076 | 1.032 | " |
| Manganese chloride | 1.0513 | 1.209 | 1.0259 | 1.098 | 1.0125 | 1.048 | 1.0063 | 1.023 | " |
| " nitrate . . | 1.0690 | 1.183 | 1.0349 | 1.087 | 1.0174 | 1.043 | 1.0093 | 1.023 | " |
| " sulphate . . | 1.0728 | 1.364 | 1.0365 | 1.169 | 1.0179 | 1.076 | 1.0087 | 1.037 | " |
| Nickel chloride . . | 1.0591 | 1.205 | 1.0308 | 1.097 | 1.0144 | 1.044 | 1.0067 | 1.021 | " |
| " nitrate . . | 1.0755 | 1.180 | 1.0381 | 1.084 | 1.0192 | 1.042 | 1.0096 | 1.019 | " |
| " sulphate . . | 1.0773 | 1.361 | 1.0391 | 1.161 | 1.0198 | 1.075 | 1.0017 | 1.032 | " |
| Potassium chloride . . | 1.0466 | 0.987 | 1.0235 | 0.987 | 1.0117 | 0.990 | 1.0059 | 0.993 | " |
| " chromate . . | 1.0935 | 1.113 | 1.0475 | 1.053 | 1.0241 | 1.022 | 1.0121 | 1.012 | " |
| " nitrate . . | 1.0605 | 0.975 | 1.0305 | 0.982 | 1.0161 | 0.987 | 1.0075 | 0.992 | " |
| " sulphate . . | 1.0664 | 1.105 | 1.0338 | 1.049 | 1.0170 | 1.021 | 1.0084 | 1.008 | " |
| Sodium chloride . . | 1.0401 | 1.097 | 1.0208 | 1.047 | 1.0107 | 1.024 | 1.0056 | 1.013 | Reyher |
| " bromide . . | 1.0786 | 1.064 | 1.0396 | 1.030 | 1.0190 | 1.015 | 1.0100 | 1.008 | " |
| " chloride . . | 1.0710 | 1.090 | 1.0359 | 1.042 | 1.0180 | 1.022 | 1.0092 | 1.012 | " |
| " nitrate . . | 1.0554 | 1.065 | 1.0281 | 1.026 | 1.0141 | 1.012 | 1.0071 | 1.007 | " |
| Silver nitrate . . . | 1.1386 | 1.058 | 1.0692 | 1.020 | 1.0348 | 1.006 | 1.0173 | 1.000 | Wagner |
| Strontium chloride . . | 1.0676 | 1.141 | 1.0336 | 1.067 | 1.0171 | 1.034 | 1.0084 | 1.014 | " |
| " nitrate . . | 1.0822 | 1.115 | 1.0419 | 1.049 | 1.0208 | 1.024 | 1.0104 | 1.011 | " |
| Zinc chloride . . . | 1.0590 | 1.189 | 1.0302 | 1.096 | 1.0152 | 1.053 | 1.0077 | 1.024 | " |
| " nitrate . . | 1.0758 | 1.164 | 1.0404 | 1.086 | 1.0191 | 1.039 | 1.0096 | 1.019 | " |
| " sulphate . . | 1.0792 | 1.367 | 1.0402 | 1.173 | 1.0198 | 1.082 | 1.0094 | 1.036 | " |

* In the case of solutions of salts it has been found (*vide* Arrhenius, Zeits. für Phys. Chem. vol. 1, p. 285) that the specific viscosity can, in many cases, be nearly expressed by the equation $\mu = \mu_1 n$, where μ_1 is the specific viscosity for a normal solution referred to the solvent at the same temperature, and n the number of gramme molecules in the solution under consideration. The same rule may of course be applied to solutions stated in percentages instead of gramme molecules. The table here given has been compiled from the results of Reyher (Zeits. für Phys. Chem. vol. 2, p. 749) and of Wagner (Zeits. für Phys. Chem. vol. 5, p. 31) and illustrates this rule. The numbers are all for 25°C.

VISCOSITY OF GASES AND VAPORS

The values of μ given in the table are 10^6 times the coefficients of viscosity in c.g.s. units.

| Substance. | Temp. °C | μ | Refer- ence. | Substance. | Temp. °C | | Refer- ence. |
|-----------------------|-------------|-------|-----------------|--------------------|-------------|-------|-----------------|
| Acetone..... | 18.0 | 78. | 1 | Ether..... | 16.1 | 73.2 | 1 |
| Air *..... | -21.4 | 163.9 | 2 | "..... | 36.5 | 79.3 | 1 |
| "..... | 0.0 | 173.3 | 2 | Ethyl chloride.... | 0. | 93.5 | 4 |
| "..... | 15.0 | 180.7 | 2 | Ethyl iodide..... | 72.3 | 216.0 | 3 |
| "..... | 99.1 | 220.3 | 2 | Ethylene..... | 0.0 | 96.1 | 2 |
| "..... | 182.4 | 255.9 | 2 | Helium..... | 0.0 | 189.1 | 5 |
| "..... | 302.0 | 299.3 | 2 | "..... | 15.3 | 196.9 | 5 |
| Alcohol, Methyl... | 66.8 | 135. | 3 | "..... | 66.6 | 234.8 | 5 |
| Alcohol, Ethyl.... | 78.4 | 142. | 3 | "..... | 184.6 | 269.9 | 5 |
| Alcohol, Propyl, | | | | Hydrogen..... | -20.6 | 81.9 | 2 |
| norm..... | 97.4 | 142. | 3 | "..... | 0.0 | 86.7 | 10 |
| Alcohol, Isopropyl.. | 82.8 | 162. | 3 | "..... | 15. | 88.9 | 2 |
| Alcohol, Butyl, norm. | 116.9 | 143. | 3 | "..... | 99.2 | 105.9 | 2 |
| Alcohol, Isobutyl... | 108.4 | 144. | 3 | "..... | 182.4 | 121.5 | 2 |
| Alcohol, Tert. butyl. | 82.9 | 160. | 3 | "..... | 302.0 | 139.2 | 2 |
| Ammonia..... | 0.0 | 96. | 4 | Krypton..... | 15.0 | 246. | 11 |
| "..... | 20.0 | 108. | 4 | Mercury..... | 270.0 | 489.† | 8 |
| Argon..... | 0.0 | 210.4 | 5 | "..... | 300.0 | 532.† | 8 |
| "..... | 14.7 | 220.8 | 5 | "..... | 330.0 | 582.† | 8 |
| "..... | 17.9 | 224.1 | 5 | "..... | 360.0 | 627.† | 8 |
| "..... | 99.7 | 273.3 | 5 | "..... | 390.0 | 671.† | 8 |
| "..... | 183.7 | 322.1 | 5 | Methane..... | 20.0 | 120.1 | 4 |
| Benzene..... | 0. | 70. | 10 | Methyl chloride... | 0.0 | 98.8 | 2 |
| "..... | 19.0 | 79. | 6 | "..... | 15.0 | 105.2 | 2 |
| "..... | 100.0 | 118. | 6 | "..... | 302.0 | 213.9 | 2 |
| Carbon bisulphide.. | 16.9 | 92.4 | 1 | Methyl iodide.... | 44.0 | 232. | 3 |
| Carbon dioxide..... | -20.7 | 129.4 | 2 | Nitrogen..... | -21.5 | 156.3 | 7 |
| "..... | 0. | 142. | 10 | "..... | 0. | 166. | 10 |
| "..... | 15.0 | 145.7 | 2 | "..... | 10.9 | 170.7 | 7 |
| "..... | 99.1 | 186.1 | 2 | "..... | 53.5 | 189.4 | 7 |
| "..... | 182.4 | 222.1 | 2 | Nitric oxide..... | 0. | 179. | 10 |
| "..... | 302.0 | 268.2 | 2 | Nitrous oxide..... | 0. | 138. | 10 |
| Carbon monoxide... | 0.0 | 163.0 | 10 | Oxygen..... | 0. | 189. | 10 |
| "..... | 20.0 | 184.0 | 4 | "..... | 15.4 | 195.7 | 7 |
| Chlorine..... | 0.0 | 128.7 | 4 | "..... | 53.5 | 215.9 | 7 |
| "..... | 20.0 | 147.0 | 4 | Water Vapor..... | 0.0 | 90.4 | 1 |
| Chloroform..... | 0.0 | 95.9 | 1 | "..... | 16.7 | 96.7 | 1 |
| "..... | 17.4 | 102.9 | 1 | "..... | 100.0 | 132.0 | 9 |
| "..... | 61.2 | 189.0 | 3 | Xenon..... | 15. | 222. | 11 |
| Ether..... | 0.0 | 68.9 | 1 | | | | |

1 Puluj, Wien. Ber. 69 (2), 1874.

2 Breitenbach, Ann. Phys. 5, 1901.

3 Steudel, Wied. Ann. 16, 1882.

4 Graham, Philos. Trans. Lond. 1846, III.

5 Schultze, Ann. Phys. (4), 5, 6, 1901.

6 Schumann, Wied. Ann. 23, 1884.

7 Obermayer, Wien. Ber. 71 (2a), 1875.

8 Koch, Wied. Ann. 14, 1881, 19, 1883.

9 Meyer-Schumann, Wied. Ann. 13, 1881.

10 Jeans, assumed mean, 1916.

11 Rankine, 1910.

12 Vogel (Eucken, Phys. Z. 14, 1913). For summaries see: Fisher, Phys. Rev. 24, 1904; Chapman, Phil. Tr. A. 211, 1911; Gilchrist, Phys. Rev. 1, 1913. Schmidt, Ann. d. Phys. 30, 1909.

* Gilchrist's value of the viscosity of air may be taken as the most accurate at present available. His value at 20.2°C is 1.812×10^{-4} . The temperature variation given by Holman (Phil. Mag. 1886) gives $\mu = 1715.50 \times 10^{-7} (1 + .00275t - .0000034t^2)$. See Phys. Rev. 1, 1913. Millikan (Ann. Phys. 41, 759, 1913) gives for the most accurate value $\mu_t = 0.00018240 - 0.00000493(23 - t)$ when $(23 > t > 12)$ whence $\mu_{20} = 0.0001809 \pm 0.1\%$. For μ_0 he gives 0.0001711 .

† The values here given were calculated from Koch's table (Wied. Ann. 19, p. 869, 1883) by the formula $\mu = 489 [1 + 746(t - 270)]$.

TABLE 182
VISCOSITY OF GASES

Variation of Viscosity with Pressure and Temperature

According to the kinetic theory of gases the coefficient of viscosity $\mu = \frac{1}{3}(\rho \bar{c} l)$, ρ being the density, \bar{c} the average velocity of the molecules, l the average path. Since l varies inversely as the number of molecules per unit volume, ρl is a constant and μ should be independent of the density and pressure of a gas (Maxwell's law). This has been found true for ordinary pressures; below $\frac{1}{80}$ atmosphere it may fail, and for certain gases it has been proved untrue for high pressures, e.g., CO_2 at 33° and above 50 atm. See Jeans, "Dynamical Theory of Gases."

If B is the amount of momentum transferred from a plane moving with velocity U and parallel to a stationary plane distant d , and s is a quantity (coefficient of slip) to allow for the slipping of the gas molecules over the plane, then $\mu = (B/U)(d + 2s)$; s is of the same magnitude as l , probably between .7 (Timiriacheff) and .9 (Knudsen) of it; at low pressures d becomes negligible compared with $2s$ and the viscosity should vary inversely as the pressure.

\bar{c} depends only on the temperature and the molecular weight. \bar{c} varies as the \sqrt{T} , but μ has been found to increase much more rapidly. Meyer's formula, $\mu_t = \mu_0(1 + at)$, where a is a constant and μ_0 the viscosity at 0°C , is a convenient approximate relation. Sutherland's formula (Phil. Mag. 31, 1893),

$$\mu_t = \mu_0 \frac{273 + C}{T + C} \left(\frac{T}{273} \right)^{\frac{3}{2}},$$

is the most accurate formula in use, taking in account the effect of molecular forces. It holds for temperatures above the critical and for pressures following approximately Boyle's law. It may be thrown into the form $T = KT^{\frac{3}{2}}/\mu - C$ which is linear in terms of T and $T^{\frac{3}{2}}/\mu$, with a slope equal to K and the ordinate intercept equal to $-C$. See Fisher, Phys. Rev. 24, 1907, from which most of the following table is taken. Onnes (see Jeans) shows that this formula does not represent Helium at low temperatures with anything like the accuracy of the simpler formula $\mu = \mu_0(T/273.1)^n$.

The following table contains the constants for the above three formulae, T being always the absolute temperature, Centigrade scale.

| Gas. | C | $K \times 10^7$ | a | n^* | Gas. | C | $K \times 10^7$ | a | n^* |
|----------------------|-----|-----------------|--------|-------|---|-----|-----------------|--------|-------|
| Air..... | 124 | 150 | — | .754 | Hydrogen..... | 72 | 66 | — | .69 |
| Argon..... | 172 | 206 | — | .819 | Krypton..... | 188 | — | — | — |
| Carbon monoxide..... | 102 | 135 | .00269 | .74 | Neon..... | 252 | — | — | — |
| Carbon dioxide..... | 240 | 158 | .00348 | .98 | Nitrogen..... | 110 | 143 | .00269 | .74 |
| Chloroform..... | 454 | 159 | — | — | Nitrous oxide, N ₂ O..... | 313 | 172 | .00345 | .93 |
| Ethylene..... | 226 | 106 | .00350 | — | Oxygen..... | 131 | 176 | — | .79 |
| Helium..... | 80 | 148 | — | .683 | Xenon..... | 252 | — | — | — |
| Helium..... | — | — | — | .647 | | | | | |

* The authorities for n are: Air, Rayleigh; Ar, Mean, Rayleigh, Schultze; CO , CO_2 , N_2 , N_2O , von Obermayer; Helium, Mean, Rayleigh, Schultze; 2d value, low temperature work of Onnes; H_2 , O_2 , Mean, Rayleigh, von Obermayer.

DIFFUSION OF AN AQUEOUS SOLUTION INTO PURE WATER

If k is the coefficient of diffusion, dS the amount of the substance which passes in the time dt at the place x , through q sq. cm. of a diffusion cylinder under the influence of a drop of concentration dc/dx , then

$$dS = -kq \frac{dc}{dx} dt.$$

k depends on the temperature and the concentration. c gives the gram-molecules per liter. The unit of time is a day.

| Substance. | c | t° | k | Refer- ence | Substance. | c | t° | k | Refer- ence |
|------------------------|-----|-----------|-------|----------------|-----------------------|-------|-----------|-------|----------------|
| Bromine . . . | 0.1 | 12. | 0.8 | 1 | Calcium chloride . . | 0.864 | 8.5 | 0.70 | 4 |
| Chlorine . . . | " | 12. | 1.22 | " | " " . . . | 1.22 | 9. | 0.72 | " |
| Copper sulphate . . | " | 17. | 0.39 | 2 | " " . . . | 0.060 | 9. | 0.64 | " |
| Glycerine . . . | " | 10.14 | 0.357 | 3 | " " . . . | 0.047 | 9. | 0.68 | " |
| Hydrochloric acid . . | " | 19.2 | 2.21 | 2 | Copper sulphate . . | 1.95 | 17. | 0.23 | 2 |
| Iodine . . . | " | 12. | (0.5) | 1 | " " . . . | 0.95 | 17. | 0.26 | " |
| Nitric acid . . . | " | 19.5 | 2.07 | 2 | " " . . . | 0.30 | 17. | 0.33 | " |
| Potassium chloride . . | " | 17.5 | 1.38 | 2 | " " . . . | 0.005 | 17. | 0.47 | " |
| " hydroxide . . . | " | 13.5 | 1.72 | 2 | Glycerine . . . | 2/8 | 10.14 | 0.354 | 3 |
| Silver nitrate . . . | " | 12. | 0.985 | 2 | " " . . . | 6/8 | 10.14 | 0.345 | " |
| Sodium chloride . . . | " | 15.0 | 0.94 | 2 | " " . . . | 10/8 | 10.14 | 0.329 | " |
| Urea . . . | " | 14.8 | 0.97 | 3 | " " . . . | 14/8 | 10.14 | 0.300 | " |
| Acetic acid . . . | 0.2 | 13.5 | 0.77 | 4 | Hydrochloric acid . . | 4.52 | 11.5 | 2.93 | 4 |
| Barium chloride . . . | " | 8. | 0.66 | 4 | " " . . . | 3.16 | 11. | 2.67 | " |
| Glycerine . . . | " | 10.1 | 3.55 | 3 | " " . . . | 0.945 | 11. | 2.12 | " |
| Sodium acetate . . . | " | 12. | 0.67 | 5 | " " . . . | 0.387 | 11. | 2.02 | " |
| " chloride . . . | " | 15.0 | 0.94 | 2 | " " . . . | 0.250 | 11. | 1.84 | " |
| Urea . . . | " | 14.8 | 0.969 | 3 | Magnesium sulphate . | 2.18 | 5.5 | 0.28 | 4 |
| Acetic acid . . . | 1.0 | 12. | 0.74 | 6 | " " . . . | 0.541 | 5.5 | 0.32 | " |
| Ammonia . . . | " | 15.23 | 1.54 | 7 | " " . . . | 3.23 | 10. | 0.27 | " |
| Formic acid . . . | " | 12. | 0.97 | 7 | " " . . . | 0.402 | 10. | 0.34 | " |
| Glycerine . . . | " | 10.14 | 0.339 | 3 | Potassium hydroxide . | 0.75 | 12. | 1.72 | 6 |
| Hydrochloric acid . . | " | 12. | 2.09 | 6 | " " . . . | 0.49 | 12. | 1.70 | " |
| Magnesium sulphate . | " | 7. | 0.30 | 4 | " " . . . | 0.375 | 12. | 1.70 | " |
| Potassium bromide . . | " | 10. | 1.13 | 8 | " nitrate . . . | 3.9 | 17.6 | 0.89 | 2 |
| " hydroxide . . . | " | 12 | 1.72 | 6 | " " . . . | 1.4 | 17.6 | 1.10 | " |
| Sodium chloride . . . | " | 15.0 | 0.94 | 2 | " " . . . | 0.3 | 17.6 | 1.26 | " |
| " " . . . | " | 14.3 | 0.964 | 3 | " " . . . | 0.02 | 17.6 | 1.28 | " |
| " hydroxide . . . | " | 12. | 1.11 | 2 | " sulphate . . . | 0.95 | 19.6 | 0.79 | " |
| " iodide . . . | " | 10. | 0.80 | 8 | " " . . . | 0.28 | 19.6 | 0.86 | " |
| Sugar . . . | " | 12. | 0.254 | 6 | " " . . . | 0.05 | 19.6 | 0.97 | " |
| Sulphuric acid . . . | " | 12. | 1.12 | 6 | " " . . . | 0.02 | 19.6 | 1.01 | " |
| Zinc sulphate . . . | " | 14.8 | 0.236 | 9 | Silver nitrate . . . | 3.9 | 12. | 0.535 | " |
| Acetic acid . . . | 2.0 | 12 | 0.69 | 6 | " " . . . | 0.9 | 12. | 0.88 | " |
| Calcium chloride . . . | " | 10. | 0.68 | 8 | " " . . . | 0.02 | 12. | 1.035 | " |
| Cadmium sulphate . . | " | 19.04 | 0.246 | 9 | Sodium chloride . . . | 2/8 | 14.33 | 1.013 | 3 |
| Hydrochloric acid . . | " | 12. | 2.21 | 6 | " " . . . | 4/8 | 14.33 | 0.996 | " |
| Sodium iodide . . . | " | 10. | 0.90 | 8 | " " . . . | 6/8 | 14.33 | 0.980 | 2 |
| Sulphuric acid . . . | " | 12. | 1.16 | 6 | " " . . . | 10/8 | 14.33 | 0.948 | " |
| Zinc acetate . . . | " | 18.05 | 0.210 | 9 | " " . . . | 14/8 | 14.33 | 0.917 | " |
| " " . . . | " | 0.04 | 0.120 | 9 | Sulphuric acid . . . | 9.85 | 18. | 2.36 | 2 |
| Acetic acid . . . | 3.0 | 12. | 0.68 | - | " " . . . | 4.85 | 18. | 1.90 | " |
| Potassium carbonate . | " | 10. | 0.60 | 8 | " " . . . | 2.85 | 18. | 1.60 | " |
| " hydroxide . . . | " | 12. | 1.89 | 6 | " " . . . | 0.85 | 18. | 1.34 | " |
| Acetic acid . . . | 4.0 | 12. | 0.66 | 6 | " " . . . | 0.35 | 18. | 1.32 | " |
| Potassium chloride . . | " | 10. | 1.27 | 8 | " " . . . | 0.005 | 18. | 1.30 | " |

1 Euler, Wied. Ann. 63, 1897.

2 Thovort, C. R. 133, 1901; 134, 1902.

3 Heimbrodt, Diss. Leipzig, 1903.

4 Scheffer, Chem. Ber. 15, 1882; 16, 1883;

Zeitschr. Phys. Chem. 2, 1888.

5 Kawalki, Wied. Ann. 52, 1894; 59, 1896.

6 Arrhenius, Zeitschr. Phys. Chem. 10, 1892.

7 Abegg, Zeitschr. Phys. Chem. 11, 1895.

8 Schuhmeister, Wien. Ber. 79 (2), 1879.

9 Seitz, Wied. Ann. 64, 1898

Compiled from Landolt-Börnstein-Meyerhoffer's Physikalisch-chemische Tabellen

DIFFUSION OF VAPORS

Coefficients of diffusion of vapors in C. G. S. units. The coefficients are for the temperatures given in the table and a pressure of 76 centimeters of mercury.*

| Vapor. | Temp. C. | k_1 for vapor diffusing into hydrogen. | k_2 for vapor diffusing into air. | k_3 for vapor diffusing into carbon dioxide. |
|----------------------------------|----------|--|-------------------------------------|--|
| Acids: Formic | 0.0 | 0.5131 | 0.1315 | 0.0879 |
| “ | 65.4 | 0.7873 | 0.2035 | 0.1343 |
| “ | 84.9 | 0.8830 | 0.2244 | 0.1519 |
| Acetic | 0.0 | 0.4040 | 0.1061 | 0.0713 |
| “ | 65.5 | 0.6211 | 0.1578 | 0.1048 |
| “ | 98.5 | 0.7481 | 0.1965 | 0.1321 |
| Isovaleric | 0.0 | 0.2118 | 0.0535 | 0.0375 |
| “ | 98.0 | 0.3934 | 0.1031 | 0.0696 |
| Alcohols: Methyl | 0.0 | 0.5001 | 0.1325 | 0.0880 |
| “ | 25.6 | 0.6015 | 0.1620 | 0.1046 |
| “ | 49.6 | 0.6738 | 0.1809 | 0.1234 |
| Ethyl | 0.0 | 0.3806 | 0.0994 | 0.0693 |
| “ | 40.4 | 0.5030 | 0.1372 | 0.0898 |
| “ | 66.9 | 0.5430 | 0.1475 | 0.1026 |
| Propyl | 0.0 | 0.3153 | 0.0803 | 0.0577 |
| “ | 66.9 | 0.4832 | 0.1237 | 0.0901 |
| “ | 83.5 | 0.5434 | 0.1379 | 0.0976 |
| Butyl | 0.0 | 0.2716 | 0.0681 | 0.0476 |
| “ | 99.0 | 0.5045 | 0.1265 | 0.0884 |
| Amyl | 0.0 | 0.2351 | 0.0589 | 0.0422 |
| “ | 99.1 | 0.4362 | 0.1094 | 0.0784 |
| Hexyl | 0.0 | 0.1998 | 0.0499 | 0.0351 |
| “ | 99.0 | 0.3712 | 0.0927 | 0.0651 |
| Benzene | 0.0 | 0.2940 | 0.0751 | 0.0527 |
| “ | 19.9 | 0.3409 | 0.0877 | 0.0609 |
| “ | 45.0 | 0.3993 | 0.1011 | 0.0715 |
| Carbon disulphide | 0.0 | 0.3690 | 0.0883 | 0.0629 |
| “ | 19.9 | 0.4255 | 0.1015 | 0.0726 |
| “ | 32.8 | 0.4626 | 0.1120 | 0.0789 |
| Esters: Methyl acetate | 0.0 | 0.3277 | 0.0840 | 0.0557 |
| “ | 20.3 | 0.3928 | 0.1013 | 0.0679 |
| Ethyl | 0.0 | 0.2373 | 0.0630 | 0.0450 |
| “ | 46.1 | 0.3729 | 0.0970 | 0.0666 |
| Methyl butyrate | 0.0 | 0.2422 | 0.0640 | 0.0438 |
| “ | 92.1 | 0.4308 | 0.1139 | 0.0809 |
| Ethyl | 0.0 | 0.2238 | 0.0573 | 0.0406 |
| “ | 96.5 | 0.4112 | 0.1064 | 0.0756 |
| “ valerate | 0.0 | 0.2050 | 0.0505 | 0.0366 |
| “ | 97.6 | 0.3784 | 0.0932 | 0.0676 |
| Ether | 0.0 | 0.2960 | 0.0775 | 0.0552 |
| “ | 19.9 | 0.3410 | 0.0893 | 0.0636 |
| Water | 0.0 | 0.6870 | 0.1980 | 0.1310 |
| “ | 49.5 | 1.0000 | 0.2827 | 0.1811 |
| “ | 92.4 | 1.1794 | 0.3451 | 0.2384 |

* Taken from Winkelmann's papers (Wied. Ann. vols. 22, 23, and 26). The coefficients for σ^2 were calculated by Winkelmann on the assumption that the rate of diffusion is proportional to the absolute temperature. According to the investigations of Loschmidt and of Obermeyer the coefficient of diffusion of a gas, or vapor, at 0° C and a pressure of 76 centimetres of mercury may be calculated from the observed coefficient at another temperature and pressure by the formula $k_0 = k_T \left(\frac{T_0}{T} \right)^n \frac{76}{p}$, where T is temperature absolute and p the pressure of the gas. The exponent n is found to be about 1.75 for the permanent gases and about 2 for condensable gases. The following are examples: Air— CO_2 , $n=1.068$; CO_2 — N_2O , $n=2.05$; CO_2 — H_2 , $n=1.742$; CO — O , $n=1.785$; H — O , $n=1.755$; O — N , $n=1.702$. Winkelmann's results, as given in the above table, seem to give about 2 for vapors diffusing into air, hydrogen or carbon dioxide.

DIFFUSION OF GASES, VAPORS AND METALS

TABLE 185.—Coefficients of Diffusion for Various Gases and Vapors *

| Gas or Vapor diffusing. | Gas or Vapor diffused into. | Temp. ° C. | Coefficient of Diffusion. | Authority. |
|-----------------------------|-----------------------------|---------------|------------------------------|------------|
| Air | Hydrogen | 0 | 0.661 | Schulze. |
| " | Oxygen | 0 | 0.1775 | Obermayer. |
| Carbon dioxide | Air | 0 | 0.1423 | Loschmidt. |
| " | " | 0 | 0.1360 | Waitz. |
| " | Carbon monoxide | 0 | 0.1405 | Loschmidt. |
| " | " | 0 | 0.1314 | Obermayer. |
| " | Hydrogen | 0 | 0.5437 | " |
| " | Methane | 0 | 0.1405 | " |
| " | Nitrous oxide | 0 | 0.0983 | Loschmidt. |
| " | Oxygen | 0 | 0.1802 | " |
| Carbon disulphide | Air | 0 | 0.0995 | Stefan |
| Carbon monoxide | Carbon dioxide | 0 | 0.1314 | Obermayer. |
| " | Ethylene | 0 | 0.101 | " |
| " | Hydrogen | 0 | 0.6422 | Loschmidt. |
| " | Oxygen | 0 | 0.1802 | " |
| " | " | 0 | 0.1872 | Obermayer. |
| Ether | Air | 0 | 0.0827 | Stefan. |
| " | Hydrogen | 0 | 0.3054 | " |
| Hydrogen | Air | 0 | 0.6340 | Obermayer. |
| " | Carbon dioxide | 0 | 0.5384 | " |
| " | " monoxide | 0 | 0.6488 | " |
| " | Ethane | 0 | 0.4593 | " |
| " | Ethylene | 0 | 0.4863 | " |
| " | Methane | 0 | 0.6254 | " |
| " | Nitrous oxide | 0 | 0.5347 | " |
| " | Oxygen | 0 | 0.6788 | " |
| Nitrogen | " | 0 | 0.1787 | " |
| Oxygen | Carbon dioxide | 0 | 0.1357 | " |
| " | Hydrogen | 0 | 0.7217 | Loschmidt. |
| " | Nitrogen | 0 | 0.1710 | Obermayer. |
| Sulphur dioxide | Hydrogen | 0 | 0.4828 | Loschmidt. |
| Water | Air | 8 | 0.2390 | Guglielmo. |
| " | " | 18 | 0.2475 | " |
| " | Hydrogen | 18 | 0.8710 | " |

* Compiled for the most part from a similar table in Landolt & Börnstein's Phys. Chem. Tab.

TABLE 186.—Diffusion of Metals into Metals

$\frac{dv}{dt} = k \frac{d^2v}{dx^2}$; where x is the distance in direction of diffusion; v , the degree of concentration of the diffusing metal; t , the time; k , the diffusion constant = the quantity of metal in grams diffusing through a sq. cm. in a day when unit difference of concentration (gr. per cu. cm.) is maintained between two sides of a layer one cm. thick.

| Diffusing Metal. | Dissolving Metal | Temperature ° C. | k | Diffusing Metal. | Dissolving Metal. | Temperature ° C. | k . |
|------------------|-------------------|------------------|---------|---------------------|-------------------|------------------|-------|
| Gold | Lead | 555 | 3.19 | Platinum | Lead | 492 | 1.69 |
| " | " | 492 | 3.00 | Lead | Tin | 555 | 3.18 |
| " | " | 251 | 0.03 | Rhodium | Lead | 550 | 3.04 |
| " | " | 200 | 0.008 | Tin | Mercury | 15 | 1.22* |
| " | " | 165 | 0.004 | Lead | " | 15 | 1.0* |
| " | " | 100 | 0.00002 | Zinc | " | 15 | 1.0* |
| " | Bismuth | 555 | 4.52 | Sodium | " | 15 | 0.45* |
| " | Tin | 555 | 4.65 | Potassium | " | 15 | 0.40* |
| Silver | " | 555 | 4.14 | Gold | " | 15 | 0.72* |

From Roberts-Austen, Philosophical Transactions, 187A, p. 383, 1896.

* These values are from Guthrie.

SOLUBILITY OF INORGANIC SALTS IN WATER
(TEMPERATURE VARIATION)

The numbers give the number of grams of the *anhydrous* salt soluble in 1000 grams of water at the given temperatures.

| Salt. | Temperature Centigrade. | | | | | | | | | | |
|---|-------------------------|------|------|------|-------|-------|-------|-------|------|------|------|
| | 0° | 10° | 20° | 30° | 40° | 50° | 60° | 70° | 80° | 90° | 100° |
| AgNO ₃ | 1150 | 1600 | 2150 | 2700 | 3350 | 4000 | 4700 | 5500 | 6500 | 7600 | 9100 |
| Al ₂ (SO ₄) ₃ | 313 | 335 | 362 | 404 | 457 | 521 | 591 | 662 | 731 | 808 | 891 |
| Al ₂ K ₂ (SO ₄) ₄ | 30 | — | — | 84 | — | — | 248 | — | — | — | 1540 |
| Al ₂ (NH ₄) ₂ (SO ₄) ₄ | 26 | 45 | 66 | 91 | 124 | 159 | 211 | 270 | 352 | — | — |
| B ₂ O ₃ | 11 | 15 | 22 | — | 40 | — | 62 | — | 95 | — | 157 |
| BaCl ₂ | 316 | 333 | 357 | 382 | 408 | 436 | 464 | 494 | 524 | 556 | 588 |
| Ba(NO ₃) ₂ | 50 | 70 | 92 | 116 | 142 | 171 | 203 | 236 | 270 | 306 | 342 |
| CaCl ₂ | 595 | 650 | 745 | 1010 | 1153 | — | 1368 | 1417 | 1470 | 1527 | 1590 |
| CoCl ₂ | 405 | 450 | 500 | 565 | 650 | 935 | 940 | 950 | 960 | — | 1030 |
| CsCl | 1614 | 1747 | 1865 | 1973 | 2080 | 2185 | 2290 | 2395 | 2500 | 2601 | 2705 |
| CsNO ₃ | 93 | 149 | 230 | 339 | 472 | 644 | 838 | 1070 | 1340 | 1630 | 1970 |
| Cs ₂ SO ₄ | 1671 | 1731 | 1787 | 1841 | 1899 | 1949 | 1999 | 2050 | 2103 | 2149 | 2203 |
| Cu(NO ₃) ₂ | 818 | — | 1250 | — | 1598 | — | 1791 | — | 2078 | — | — |
| CuSO ₄ | 149 | — | — | 255 | 295 | 336 | 390 | 457 | 535 | 627 | 735 |
| FeCl ₂ | — | — | 685 | — | — | 820 | — | — | 1040 | 1050 | 1060 |
| Fe ₂ Cl ₆ | 744 | 819 | 918 | — | — | 3151 | — | — | 5258 | — | 5357 |
| FeSO ₄ | 156 | 208 | 264 | 330 | 402 | 486 | 550 | 560 | 566 | 430 | — |
| HgCl ₂ | 43 | 66 | 74 | 84 | 96 | 113 | 139 | 173 | 243 | 371 | 540 |
| KBr | 540 | — | 650 | — | 760 | — | 860 | — | 955 | — | 1050 |
| K ₂ CO ₃ | 1050 | — | — | 1140 | 1170 | 1210 | 1270 | 1330 | 1400 | 1470 | 1560 |
| KCl | 285 | 312 | 343 | 373 | 401 | 429 | 455 | 483 | 510 | 538 | 566 |
| KClO ₃ | 33 | 50 | 71 | 101 | 145 | 197 | 260 | 325 | 396 | 475 | 560 |
| K ₂ CrO ₄ | 589 | 609 | 629 | 650 | 670 | 690 | 710 | 730 | 751 | 771 | 791 |
| K ₂ Cr ₂ O ₇ | 50 | 85 | 131 | — | 292 | — | 505 | — | 730 | — | 1020 |
| KHCO ₃ | 225 | 277 | 332 | 390 | 453 | 522 | 600 | — | — | — | — |
| KI | 1279 | 1361 | 1442 | 1523 | 1600 | 1680 | 1760 | 1840 | 1920 | 2010 | 2090 |
| KNO ₃ | 133 | 209 | 316 | 458 | 639 | 855 | 1099 | 1380 | 1690 | 2040 | 2460 |
| KOH | 970 | 1030 | 1120 | 1260 | 1360 | 1400 | 1460 | 1510 | 1590 | 1680 | 1780 |
| K ₂ PtCl ₆ | 7 | 9 | 11 | 14 | 18 | 22 | 26 | 32 | 38 | 45 | 52 |
| K ₂ SO ₄ | 74 | 92 | 111 | 130 | 148 | 165 | 182 | 198 | 214 | 228 | 241 |
| LiOH | 127 | 127 | 128 | 129 | 130 | 133 | 138 | 144 | 153 | — | 175 |
| MgCl ₂ | 528 | 535 | 545 | — | 575 | — | 610 | — | 660 | — | 730 |
| MgSO ₄ | 260 | 309 | 356 | 409 | 456 | — | — | — | — | — | — |
| " (7aq) | 408 | 422 | 439 | 453 | — | 504 | 550 | 596 | 642 | 689 | 738 |
| " (6aq) | 297 | 333 | 372 | 414 | 458 | 504 | 552 | 602 | 656 | 713 | 773 |
| NH ₄ Cl | 119 | 159 | 210 | 270 | — | — | — | — | — | — | — |
| NH ₄ HCO ₃ | 1183 | — | — | 2418 | 2970 | 3540? | 4300? | 5130? | 5800 | 7400 | 8710 |
| NH ₄ NO ₃ | 706 | 730 | 754 | 780 | 810 | 844 | 880 | 916 | 953 | 992 | 1033 |
| (NH ₄) ₂ SO ₄ | 795 | 845 | 903 | — | 1058 | 1160 | 1170 | — | 1185 | — | 1205 |
| NaBr | — | 16 | — | 39 | — | 105 | 200 | 244 | 314 | 408 | 523 |
| Na ₂ B ₄ O ₇ | 71 | 126 | 214 | 409 | — | — | — | — | — | — | — |
| Na ₂ CO ₃ | 204 | 263 | 335 | 435 | (1aq) | 475 | 464 | 458 | 452 | 452 | 452 |
| " (7aq) | 356 | 357 | 358 | 360 | 363 | 367 | 371 | 375 | 380 | 385 | 391 |
| NaCl | 820 | 890 | 990 | — | 1235 | — | 1470 | — | 1750 | — | 2040 |
| NaClO ₃ | 317 | 502 | 900 | — | 900 | 1050 | 1150 | — | 1240 | — | 1260 |
| Na ₂ CrO ₄ | 1630 | 1700 | 1800 | 1970 | 2200 | 2480 | 2830 | 3230 | 3860 | — | 4330 |
| Na ₂ Cr ₂ O ₇ | 69 | 82 | 96 | 111 | 127 | 145 | 164 | — | — | — | — |
| NaHCO ₃ | 25 | 39 | 93 | 241 | 639 | — | — | 949 | — | — | 988 |
| Na ₂ HPO ₄ | 1590 | 1690 | 1790 | 1900 | 2050 | 2280 | 2570 | — | 2950 | — | 3020 |
| NaI | 730 | 805 | 880 | 962 | 1049 | 1140 | 1246 | 1360 | 1480 | 1610 | 1755 |
| NaNO ₃ | — | — | — | — | — | — | — | — | — | — | — |

Compiled from Landolt-Börnstein-Meyerhoffer's Physikalisch-chemische Tabellen.

TABLE 187 (continued).—Solubility of Inorganic Salts in Water (Temperature Variation)

The numbers give the number of grams of the *anhydrous* salt soluble in 1000 grams of water at the given temperatures.

| Salt. | Temperature Centigrade. | | | | | | | | | |
|---|-------------------------|-----|------|------|------|------|------|------|------|------|
| | 0° | 10° | 20° | 30° | 40° | 50° | 60° | 70° | 80° | 100° |
| NaOH | 420 | 515 | 1090 | 1190 | 1290 | 1450 | 1740 | — | 3130 | — |
| Na ₄ P ₂ O ₇ | 32 | 39 | 62 | 99 | 135 | 174 | 220 | 255 | 300 | — |
| Na ₂ SO ₃ | 141 | — | 287 | — | 495 | — | — | — | — | 330 |
| Na ₂ SO ₄ (10aq) | 50 | 90 | 194 | 400 | 482 | 468 | 455 | 445 | 437 | 429 |
| “ (7aq) | 196 | 305 | 447 | — | — | — | — | — | — | 427 |
| Na ₂ S ₂ O ₃ | 525 | 610 | 700 | 847 | 1026 | 1697 | 2067 | — | 2488 | 2542 |
| NiCl ₂ | — | 600 | 640 | 680 | 720 | 760 | 810 | — | — | 2660 |
| NiSO ₄ | 272 | — | — | 425 | — | 502 | 548 | 594 | 632 | 688 |
| PbBr ₂ | 5 | 6 | 8 | 12 | 15 | 20 | 24 | 28 | 33 | — |
| Pb(NO ₃) ₂ | 365 | 444 | 523 | 607 | 694 | 787 | 880 | 977 | 1076 | 1174 |
| RbCl | 770 | 844 | 911 | 976 | 1035 | 1093 | 1155 | 1214 | 1272 | 1331 |
| RbNO ₃ | 195 | 330 | 533 | 813 | 1167 | 1556 | 2000 | 2510 | 3090 | 3750 |
| Rb ₂ SO ₄ | 364 | 426 | 482 | 535 | 585 | 631 | 674 | 714 | 750 | 787 |
| SrCl ₂ | 442 | 483 | 539 | 600 | 667 | 744 | 831 | 896 | 924 | 962 |
| SnI ₂ | — | — | 10 | 12 | 14 | 17 | 21 | 25 | 30 | 34 |
| Sr(NO ₃) ₂ | 395 | 549 | 708 | 876 | 913 | 926 | 940 | 956 | 972 | 990 |
| Th(SO ₄) ₂ (9aq) | 7 | 10 | 14 | 20 | 30 | 51 | — | — | — | — |
| “ (4aq) | — | — | — | — | 40 | 25 | 16 | 11 | — | — |
| TiCl ₃ | 2 | 2 | 3 | 5 | 6 | 8 | 10 | 13 | 16 | 20 |
| TiNO ₃ | 39 | 62 | 96 | 143 | 209 | 304 | 462 | 695 | 1110 | 2000 |
| Ti ₂ SO ₄ | 27 | 37 | 49 | 62 | 76 | 92 | 109 | 127 | 146 | 165 |
| Yb ₂ (SO ₄) ₃ | 442 | — | — | — | — | — | 104 | 72 | 69 | 58 |
| Zn(NO ₃) ₂ | 948 | — | — | — | 2069 | — | — | — | — | — |
| ZnSO ₄ | — | — | — | — | 700 | 768 | — | 890 | 860 | 920 |

TABLE 188.—Solubility of a Few Organic Salts in Water (Temperature Variation)

| Salt. | 0° | 10° | 20° | 30° | 40° | 50° | 60° | 70° | 80° | 90° | 100° |
|--|------|------|------|------|------|------|------|------|------|------|------|
| H ₂ (CO ₃) ₂ | 36 | 53 | 102 | 159 | 228 | 321 | 445 | 635 | 978 | 1200 | — |
| H ₂ (CH ₂ CO ₂) ₂ | 28 | 45 | 69 | 106 | 162 | 244 | 358 | 511 | 708 | — | 1209 |
| Tartaric acid | 1150 | 1260 | 1390 | 1560 | 1760 | 1950 | 2180 | 2440 | 2730 | 3070 | 3430 |
| Racemic “ | 92 | 140 | 206 | 291 | 433 | 595 | 783 | 999 | 1250 | 1530 | 1850 |
| K(HCO ₂) ₂ | 2900 | — | 3350 | — | 3810 | — | 4550 | — | 5750 | — | 7900 |
| KH(C ₄ H ₄ O ₆) | 3 | 4 | 6 | 9 | 13 | 18 | 24 | 32 | 45 | 57 | 69 |

TABLE 189.—Solubility of Gases in Water (Temperature Variation)

The table gives the weight in grams of the gas which will be absorbed in 1000 grams of water when the partial pressure of the gas plus the vapor pressure of the liquid at the given temperature equals 760 mm.

| Gas. | 0° | 10° | 20° | 30° | 40° | 50° | 60° | 70° | 80° |
|----------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| O ₂ | .0705 | .0551 | .0443 | .0368 | .0311 | .0263 | .0221 | .0181 | .0135 |
| H ₂ | .00192 | .00174 | .00160 | .00147 | .00138 | .00129 | .00118 | .00102 | .00079 |
| N ₂ | .0293 | .0230 | .0189 | .0161 | .0139 | .0121 | .0105 | .0089 | .0069 |
| Br ₂ | 431. | 248. | 148. | 94. | 62. | 40. | 28. | 18. | 11. |
| Cl ₂ | — | 9.97 | 7.29 | 5.72 | 4.59 | 3.93 | 3.30 | 2.79 | 2.23 |
| CO ₂ | 3.35 | 2.32 | 1.69 | 1.26 | 0.97 | 0.76 | 0.58 | — | — |
| H ₂ S | 7.10 | 5.30 | 3.98 | — | — | — | — | — | — |
| NH ₃ | 987. | 689. | 535. | 422. | — | — | — | — | — |
| SO ₂ | 228. | 162. | 113. | 78. | 54. | — | — | — | — |

Compiled from Landolt-Börnstein-Meyerhoffer's Physikalisch-chemische Tabellen.

Table 190.—Change of Solubility Produced by Uniform Pressure*

| Pressure in atmospheres. | CdSO ₄ · $\frac{8}{3}$ H ₂ O at 25° | | ZnSO ₄ ·7H ₂ O at 25° | | Mannite at 24.05° | | NaCl at 24.05° | |
|--------------------------|--|--------------------|--|--------------------|--|--------------------|---|--------------------|
| | Conc. of satd. soln. gs. CdSO ₄ per 100 gs. H ₂ O. | Percentage change. | Conc. of satd. soln. gs. ZnSO ₄ per 100 gs. H ₂ O. | Percentage change. | Conc. of satd. soln. gs. mannite per 100 gs. H ₂ O. | Percentage change. | Conc. of satd. soln. gs. NaCl per 100 gs. H ₂ O. | Percentage change. |
| 1 | 76.80 | — | 57.95 | — | 20.66 | — | 35.90 | — |
| 500 | 78.01 | + 1.57 | 57.87 | — 0.14 | 21.14 | + 2.32 | 36.55 | + 1.81 |
| 1000 | 78.84 | + 2.68 | 57.65 | — 0.52 | 21.40 | + 3.57 | 37.02 | + 3.12 |
| 1500 | — | — | — | — | 21.64 | + 4.72 | 37.36 | + 4.07 |

* E. Cohen and L. R. Sinnige, *Z. physik. Chem.* 67, p. 432, 1909; 69, p. 102, 1909. E. Cohen, K. Inouye and C. Euwen, *ibid.* 75, p. 257, 1911. These authors give a critical résumé of earlier work along this line.

Table 191.—Commonly Used Organic Solvents

Arranged in the order of their Boiling Points

(Table by Dr. J. W. H. Randall, reprinted with permission of Chemical Catalog Co.)

| Name | Boiling point °C | Name | Boiling point °C |
|---------------------------|------------------|--------------------------|------------------|
| Ethyl ether..... | 34.54 | Xylene (o)..... | 144 |
| Carbon disulphide..... | 46.25 | Amyl acetate..... | 147.6 |
| Acetone..... | 56.08 | Cellosolve acetate..... | 153 |
| Methyl acetate..... | 57.1 | Ethyl lactate..... | 154 |
| Chloroform..... | 61.2 | Cyclohexanone..... | 156.7 |
| Methyl alcohol..... | 64.5 | Furfural..... | 158-162 |
| Carbon tetrachloride..... | 76.74 | Butyl cellosolve..... | 170.6 |
| Ethyl acetate..... | 77.15 | Ethyl acetoacetate..... | 180.0 |
| Ethyl alcohol..... | 78.32 | Diethyl oxalate..... | 186.1 |
| Benzol..... | 79.6 | Ethylene glycol..... | 197.2 |
| Isopropyl alcohol..... | 82.26 | Carbitol..... | 198 |
| Ethylene dichloride..... | 83.5 | Benzyl alcohol..... | 205.8 |
| Trichlorethylene..... | 88 | Ethyl benzoate..... | 213.2 |
| Ethyl propionate..... | 99.1 | Butyl stearate..... | 223 (25mm) |
| Toluene..... | 110.7 | Butyl carbitol..... | 222 |
| Butyl alcohol (n)..... | 117.7 | Diethylene glycol..... | 245 |
| Ethyl butyrate..... | 121.3 | Triphenyl phosphate..... | 245 (11mm) |
| Methyl cellosolve..... | 124.5 | Triacetin..... | 259 |
| Diethyl carbonate..... | 125.8 | Diacetin..... | 261 |
| Butyl acetate..... | 126.5 | Dimethyl phthalate..... | 282 |
| Tetrachlorethane..... | 130 | Diethyl phthalate..... | 296 |
| Cellosolve..... | 134.8 | Dibutyl phthalate..... | 340 |
| Ethyl benzene..... | 136.1 | Diamyl phthalate..... | 344 |
| Amyl alcohol (n)..... | 137.9 | | |

For producers of solvents, see the following pages of Chemical Engineering Catalog:

1017, 1018, 1020, 1023, 1024, 1027, 1028-9, 1030, 1031, 1032, 1033, 1036-7, 1038, 1039, 1041, 1043, 1046-7, 1048, 1050, 1052, 1056, 1060, 1063, 1066, 1068-9, 1072-3, 1077, 1078, 1082-3, 1084, 1087, 1091, 1094, 1095.

ABSORPTION OF GASES BY LIQUIDS *

| Temperature Centigrade. <i>t</i> | ABSORPTION COEFFICIENTS, a_t , FOR GASES IN WATER | | | | | | |
|--|---|---------------------------|----------------|----------------|------------------------|---------------------------------------|--------------|
| | Carbon dioxide. CO ₂ | Carbon monoxide. CO | Hydrogen. H | Nitrogen. N | Nitric oxide. NO | Nitrous oxide. N ₂ O | Oxygen. O |
| 0 | 1.797 | 0.0354 | 0.02110 | 0.02399 | 0.0738 | 1.048 | 0.04925 |
| 5 | 1.450 | .0315 | .02022 | .02134 | .0646 | 0.8778 | .04335 |
| 10 | 1.185 | .0282 | .01944 | .01918 | .0571 | 0.7377 | .03852 |
| 15 | 1.002 | .0254 | .01875 | .01742 | .0515 | 0.6294 | .03456 |
| 20 | 0.901 | .0232 | .01809 | .01599 | .0471 | 0.5443 | .03137 |
| 25 | 0.772 | .0214 | .01745 | .01481 | .0432 | — | .02874 |
| 30 | — | .0200 | .01690 | .01370 | .0400 | — | .02646 |
| 40 | 0.506 | .0177 | .01644 | .01195 | .0351 | — | .02316 |
| 50 | — | .0161 | .01608 | .01074 | .0315 | — | .02080 |
| 100 | 0.244 | .0141 | .01600 | .01011 | .0263 | — | .01690 |

| Temperature Centigrade. <i>t</i> | Air. | Ammonia. NH ₃ | Chlorine. Cl | Ethylene. C ₂ H ₄ | Methane. CH ₄ | Hydrogen sulphide. H ₂ S | Sulphur dioxide. SO ₂ |
|--|---------|-----------------------------|-----------------|--|-----------------------------|---|--|
| 0 | 0.02471 | 1174.6 | 3.036 | 0.2563 | 0.05473 | 4.371 | 79.79 |
| 5 | .02179 | 971.5 | 2.808 | .2153 | .04889 | 3.905 | 67.48 |
| 10 | .01953 | 840.2 | 2.585 | .1837 | .04367 | 3.586 | 56.65 |
| 15 | .01795 | 756.0 | 2.388 | .1615 | .03903 | 3.233 | 47.28 |
| 20 | .01704 | 683.1 | 2.156 | .1488 | .03499 | 2.995 | 39.37 |
| 25 | — | 610.8 | 1.950 | — | .02542 | 2.604 | 32.79 |

| Temperature Centigrade. <i>t</i> | ABSORPTION COEFFICIENTS, a_t , FOR GASES IN ALCOHOL, C ₂ H ₅ OH | | | | | | | | |
|--|---|--|-----------------------------|----------------|----------------|------------------------|---------------------------------------|---|--|
| | Carbon dioxide. CO ₂ | Ethylene. C ₂ H ₄ | Methane. CH ₄ | Hydrogen. H | Nitrogen. N | Nitric oxide. NO | Nitrous oxide. N ₂ O | Hydrogen sulphide. H ₂ S | Sulphur dioxide. SO ₂ |
| 0 | 4.329 | 3.595 | 0.5226 | 0.0692 | 0.1263 | 0.3161 | 4.190 | 17.80 | 328.6 |
| 5 | 3.891 | 3.323 | .5086 | .0685 | .1241 | .2908 | 3.838 | 14.78 | 251.7 |
| 10 | 3.514 | 3.086 | .4953 | .0679 | .1228 | .2861 | 3.525 | 11.99 | 190.3 |
| 15 | 3.199 | 2.882 | .4828 | .0673 | .1214 | .2748 | 3.215 | 9.54 | 144.5 |
| 20 | 2.946 | 2.713 | .4710 | .0667 | .1204 | .2659 | 3.015 | 7.41 | 114.5 |
| 25 | 2.756 | 2.578 | .4598 | .0662 | .1196 | .2595 | 2.819 | 5.62 | 99.8 |

* This table contains the volumes of different gases, supposed measured at 0° C and 76 centimeters' pressure, which unit volume of the liquid named will absorb at atmospheric pressure and the temperature stated in the first column. The numbers tabulated are commonly called the absorption coefficients for the gases in water, or in alcohol, at the temperature *t* and under one atmosphere of pressure. The table has been compiled from data published by Bohr & Rock, Bunsen, Carius, Dittmar, Hamberg, Henrick, Pagliano & Emo, Raoult, Schönfeld, Satschenow, and Winkler. The numbers are in many cases averages from several of these authorities.

NOTE.—The effect of increase of pressure is generally to increase the absorption coefficient. The following is approximately the magnitude of the effect in the case of ammonia in alcohol at a temperature of 23° C :

$$\left\{ \begin{array}{l} P = 45 \text{ cms} \quad 50 \text{ cms} \quad 55 \text{ cms} \quad 60 \text{ cms} \quad 65 \text{ cms} \\ a_{23} = 69 \quad 74 \quad 79 \quad 84 \quad 88 \end{array} \right.$$

According to Satschenow the effect of varying the pressure from 45 to 85 centimeters in the case of carbonic acid in water is very small.

SMITHSONIAN TABLES.

CAPILLARITY AND SURFACE TENSION OF LIQUIDS

Table 193.—Water and Alcohol in Contact with Moist Air

Values represent means. See I.C.T. and L. and B. for more elaborate tables. Tension (γ) in dynes/cm.

| °C | H ₂ O | C ₂ H ₅ OH | °C | H ₂ O | C ₂ H ₅ OH | °C | H ₂ O |
|----|------------------|----------------------------------|----|------------------|----------------------------------|-----|------------------|
| -5 | 76.4 | | 35 | 70.3 | 21.0 | 75 | 64.3 |
| 0 | 75.6 | 24.0 | 40 | 69.5 | 20.6 | 80 | 62.5 |
| 5 | 74.8 | 23.5 | 45 | 68.7 | 20.2 | 85 | 61.6 |
| 10 | 74.2 | 23.1 | 50 | 67.9 | 19.8 | 90 | 60.7 |
| 15 | 73.4 | 22.7 | 55 | 67.0 | 19.4 | 95 | 59.8 |
| 20 | 72.7 | 22.3 | 60 | 66.1 | 19.0 | 100 | 58.8 |
| 25 | 71.9 | 21.8 | 65 | 67.0 | 18.6 | ... | ... |
| 30 | 71.1 | 21.4 | 70 | 64.3 | 18.2 | ... | ... |

Table 194.—Miscellaneous Liquids in Contact with Air

| Liquid | °C | γ Dynes per cm |
|---|----|--|
| Aceton, (CH ₃) ₂ CO... | 20 | 23.7 |
| Acetic acid, CH ₃ CO ₂ H. | 20 | 27.6 |
| Amyl alcohol, C ₆ H ₁₂ O. | 20 | 24 |
| Aniline, C ₆ H ₇ N..... | 20 | 43 |
| Benzene, C ₆ H ₆ | 0 | 27 Richards '21 |
| " | 20 | 28.9 Sudgen '24 |
| Bromoform, CHBr ₃ ... | 20 | 41.5 Mean |
| Butyric acid..... | 15 | 26.7 CH ₃ (CH ₂) ₂ CO ₂ H |
| Carbon disulphide.... | 20 | 32.3 CS ₂ |
| Carbon tetrachloride.. | 20 | 26.8 CCl ₄ |
| Chloroform, CHCl ₃ ... | 20 | 27.2 Mean |
| Ether, C ₄ H ₁₀ O..... | 20 | 17.01 |
| Ethyl chloride..... | 20 | 16.2 CH ₃ Cl |
| Glycerine..... | 18 | 63 C ₃ H ₅ (OH) ₃ |
| Methyl alcohol..... | 20 | 22.6 CH ₃ OH |
| Olive oil..... | 18 | 33.1 |
| Petroleum..... | 25 | 26 |
| Phenol, C ₆ H ₆ O..... | 20 | 41.0 |
| Propyl alcohol..... | 20 | 23 CH ₃ (CH ₂) ₂ OH |
| Silicon tetrachloride, | | |
| SiCl ₄ | 19 | 17.0 Ramsay '93 |
| Toluene, C ₇ H ₈ | 20 | 28.4 |
| Turpentine..... | 20 | 27 |

Table 195.—Solutions of Salts in Water

| Salt | % Salt | °C | Dynes cm |
|-------------------------------------|-----------|----|-------------|
| BaCl ₂ | 0 | 30 | 71.1 |
| | 24.6 | 30 | 75.6 |
| CaCl ₂ | 0 | 30 | 71.1 |
| | 12.3 | 30 | 75.7 |
| | 31.9 | 30 | 86.4 |
| HCl..... | 0 | 20 | 73.0 |
| | 15 | 20 | 72.0 |
| | 25 | 20 | 70.7 |
| KCl..... | 0 | 30 | 71.1 |
| | 23.3 | 30 | 76.8 |
| | 21.1 | 18 | 77.7 |
| NaCl..... | 0 | 18 | 72.4 |
| | 7.6 | 18 | 74.8 |
| | 13.7 | 18 | 76.9 |
| NH ₄ Cl... | 0 | 18 | 72.5 |
| | 11 | 18 | 74.9 |
| K ₂ CO ₃ | 0 | 30 | 71.1 |
| | 39.4 | 30 | 89.4 |
| | 53.6 | 30 | 107.2 |
| Na ₂ CO ₃ ... | 0 | 30 | 71.1 |
| | 10.5 | 30 | 73.9 |
| | 24.4 | 30 | 76.5 |
| | 63.1 | 30 | 80.6 |
| KNO ₃ | 0 | 18 | 72.6 |
| | 15.2 | 18 | 74.5 |
| | 21.5 | 18 | 75.4 |
| NaNO ₃ ... | 0 | 30 | 71.1 |
| | 35.6 | 30 | 78.4 |
| | 50.9 | 30 | 82.8 |
| CuSO ₄ | 0 | 30 | 71.1 |
| | 25.4 | 30 | 74.1 |
| H ₂ SO ₄ | 0 | 18 | 72.8 |
| | 12.7 | 18 | 73.5 |
| | 47.6 | 18 | 76.7 |
| | 80.3 | 18 | 71.2 |
| | 90 | 18 | 63.6 |
| K ₂ SO ₄ | 0 | 18 | 72.7 |
| | 9.1 | 18 | 74.6 |
| HNO ₃ | 7.2 | 20 | 73.1 |
| | 50 | 20 | 65.4 |
| | 70 | 20 | 59.4 |
| NaOH... | 0 | 20 | 72.8 |
| | 10 | 20 | 77.3 |
| | 20 | 20 | 85.8 |
| | 30 | 20 | 95.1 |
| KOH.... | 0 | 18 | 72.8 |
| | 3.8 | 18 | 74.1 |
| | 7.8 | 18 | 75.5 |

TABLE 196.—Surface Tension of Liquids *

| Liquid. | Specific gravity. | Surface tension in dynes per centimeter of liquid in contact with— | | |
|---|-------------------|--|--------|----------|
| | | Air. | Water. | Mercury. |
| Water | 1.0 | 75.0 | 0.0 | (392) |
| Mercury | 13.543 | 513.0 | 392.0 | 0 |
| Bisulphide of carbon | 1.2687 | 30.5 | 41.7 | (387) |
| Chloroform | 1.4878 | (31.8) | 26.8 | (415) |
| Ethyl alcohol | 0.7906 | (24.1) | — | 364 |
| Olive oil | 0.9136 | 34.6 | 18.6 | 317 |
| Turpentine | 0.8867 | 28.8 | 11.5 | 241 |
| Petroleum | .7977 | 29.7 | (28.9) | 271 |
| Hydrochloric acid | 1.10 | (72.9) | — | (392) |
| Hyposulphite of soda solution | 1.1248 | 69.9 | — | 429 |

TABLE 197.—Surface Tension of Liquids at Solidifying Point †

| Substance. | Temperature of solidification. Cent.° | Surface tension in dynes per centimeter. | Substance. | Temperature of solidification. Cent.° | Surface tension in dynes per centimeter. |
|---------------------|---------------------------------------|--|------------------------------|---------------------------------------|--|
| Platinum | 2000 | 1691 | Antimony | 432 | 249 |
| Gold | 1200 | 1003 | Borax | 1000 | 216 |
| Zinc | 360 | 877 | Carbonate of soda | 1000 | 210 |
| Tin | 230 | 599 | Chloride of sodium | — | 116 |
| Mercury | —40 | 588 | Water | 0 | 87.9† |
| Lead | 330 | 457 | Selenium | 217 | 71.8 |
| Silver | 1000 | 427 | Sulphur | 111 | 42.1 |
| Bismuth | 265 | 1390 | Phosphorus | 43 | 42.0 |
| Potassium | 58 | 371 | Wax | 68 | 34.1 |
| Sodium | 90 | 258 | | | |

* This table of tensions at the surface separating the liquid named in the first column and air, water or mercury as stated at the head of the last three columns, is from Quincke's experiments (Pogg. Ann. vol. 130, and Phil. Mag. 1871). The numbers given are the equivalent in dynes per centimeter of those obtained by Worthington from Quincke's results (Phil. Mag. vol. 20, 1885) with the exception of those in brackets, which were not corrected by Worthington; they are probably somewhat too high, for the reason stated by Worthington. The temperature was about 20° C.

† Quincke, "Pogg. Ann." vol. 135, p. 661.

‡ It will be observed that the value here given on the authority of Quincke is much higher than his subsequent measurements, as quoted above, give.

|| "Proc. Roy. Soc." 1877, and "Phil. Trans. Roy. Soc." 1881, 1883, and 1893.

NOTE.—Quincke points out that substances may be divided into groups in each of which the ratio of the surface tension to the density is nearly constant. Thus, if this ratio for mercury be taken as unit, the ratio for the bromides and iodides is about a half; that of the nitrates, chlorides, sugars, and fats, as well as the metals, lead, bismuth, and antimony, about 1; that of water, the carbonates, sulphates, and probably phosphates, and the metals platinum, gold, silver, cadmium, tin, and copper, 2; that of zinc, iron, and palladium, 3; and that of sodium, 6.

TABLE 198.—Vapor Pressure and Rate of Evaporation

| ° K. | Mo mm | W mm | Evaporation rate. g/cm²/sec. | | Platinum. | | |
|------|----------|----------|---------------------------------|----------|---|----------|------------|
| | | | Mo | W | ° K. | mm | g/cm²/sec. |
| 1800 | 0.08643 | — | 0.010863 | — | 1000 | 0.017324 | 0.019832 |
| 2000 | 0.06789 | 0.011645 | 0.07100 | 0.012114 | 1200 | 0.012111 | 0.014200 |
| 2200 | 0.04396 | 0.09849 | 0.06480 | 0.010144 | 1400 | 0.09188 | 0.011401 |
| 2400 | 0.021027 | 0.07492 | 0.04120 | 0.09798 | 1600 | 0.07484 | 0.09066 |
| 2600 | 0.0160 | 0.0511 | 0.03179 | 0.07236 | 1800 | 0.08350 | 0.07667 |
| 2800 | 0.1679 | 0.04286 | 0.02181 | 0.06429 | 2000 | 0.03107 | 0.08195 |
| 3000 | — | 0.03302 | — | 0.05523 | 4180 | 760 mm | — |
| 3200 | 3890° | 0.02333 | — | 0.04467 | Langmuir, MacKay, Phys. Rev. 2, 1913; 4, 1914. Order of vacuum, 0.001 mm. | | |
| 3500 | 760 mm | 0.0572 | — | 0.03769 | | | |

$$p = K.T^{-\lambda_0} e^{-\lambda_0/RT} \text{ dynes/cm}^2. \text{ Egerton, Phil. Mag. 33, p. 33, 1917.}$$

$$\text{Zn, } \lambda_0 = 3.28 \times 10^4; K = 1.17 \times 10^{14} \quad \text{Cd, } \lambda_0 = 2.77 \times 10^4; K = 5.27 \times 10^{13}$$

$$\text{Hg, } \lambda_0 = 1.60 \times 10^4; \quad = 3.72 \times 10^{13} \text{ (Knudsen)}$$

TABLE 199
VAPOR PRESSURE OF ELEMENTS

(Over liquid unless otherwise noted)

| Hydrogen °K. mm | Helium °K. mm | Neon °K. atm. | Argon °K. mm | Krypton °K. mm | Xenon °K. mm |
|---|--|---|---|---|---|
| 20.48 787 20.36 760 19.65 611 18.03 552 16.49 192 14.10 59.5 | 5.16 16680 4.9 1329 4.20 758 3.52 360 1.48 4.2 | 41.38 17.43 36.27 7.97 31.32 2.98 27.17 1.00 20.4 12.8 mm 15.6 2.4 | 90.35 1026 87.31 746 83.93 512 77.48 201 69.43 48.0 65.49 22.0 | 210.5 41240 201.5 31620 170.9 11970 112.7 387 88.6 17.4 84.2 9 | 287.7 44110 255.6 21970 244.2 15870 231.4 11130 237.4 13500 183.2 2020 |
| Onnes, 1923 | Onnes, 1915-6 | Onnes, 1917 Travers, 1902 | Born, 1922 | Ramsay, Travers, 1901 | |

| Nitron °K. mm | Oxygen °K. mm | Nitrogen °K. mm | Chlorine °C atm. | Bromine °C mm | Iodine °C mm |
|--|--|---|--|--|--|
| 377.5 62 364.4 53 321.7 26.4 290.3 13.2 262.8 6.6 212.4 1.05 202.6 .66 | 62.37 9.59 68.57 36.1 71.71 64 77.59 162.2 86.18 493 90.13 760 90.47 786.6 | 77.33 760 76.65 700 74.03 500 72.39 400 70.42 300 67.80 200 63.65 100 | +100 41.7 + 20 6.62 0 3.66 - 33.6 760 - 50 350 - 70 118 - 80 62 - 88 37 | +58.75 760 51.95 600 40.45 400 23.45 200 8.20 100 - 7.0 45 -12.0 30 -16.65 20 | +55 3.084 50 2.154 45 1.498 40 1.025 35 .699 30 .469 15 .131 0 .030 |
| Gray, Ramsay, 1909 | Cath, 1908 | Fischer, Alt., 1902 | Knietsch, 1890 | Ramsay, Young, 1886 | Baxter, Hickey, Holmes, 1907 |

| Ozone °K. mm | Arsenic, solid °C atm. | Bismuth °C atm. | Cadmium °C mm | Calcium °C mm | Caesium °C mm |
|---|--|--|--|--|--|
| 120 34 162 760 89.94 .089 86.01 .042 83.24 .0152 81.36 .0068 | 500 .076 616 1.00 697 4.85 790 22.3 | 2060 16.5 1950 11.7 1740 6.3 1420 1.0 1310 .338 1200 .134 | 793 1000 751 371 571 .52 350 .279 262 .013 | 982 6 1028 23 1049 41 1085 99 1129 287 1175 760 | 247 .30 276 1.00 316 3.02 353 6.68 397 15.9 670 760 |
| Spangenburg, 1926 Reisenfeld | Horiba, 1923 | Greenwood, 1910 | Braune, 1920 | Ruff, Hartmann, 1914 | Mears, 1913 |

| Copper °C mm | Gallium °C mm | Gold °C mm | Lead °C mm | Lead °C mm | Magnesium °C mm |
|---|-------------------------------------|--|---|---|--|
| 1875 20 1980 100 2180 257 2310 760 | 926 .0004 1009 .003 1125 .023 | 1155 .00007 1985 17 2315 130 2500 400 | 808 .08 996 1.75 1178 16.8 1275 73 | 1315 105 1410 266 1325 760 1870 6 atm. | 623 9 742 20 986 211 1080 751 |
| Greenwood, 1911 | Harteck, 1927 | Harteck, Ruff | Wartenberg, 1913 | Greenwood, 1911 | Ruff, Hartmann, 1924 |

| Nitron °C mm | Potassium °C mm | Rubidium °C mm | Silicon °C mm | Silver °C mm |
|---|--|---|---|---|
| -70.6 .66 -60.8 1.05 +17.1 13.2 +91.2 52.8 | 406.2 4.6 469.1 16.2 528.5 44.8 759.8 783 | 91 .00006 115 .0004 250 .98 366 5.82 | 1890 10 2085 110 2195 210 2442 760 | 1038 .011 1368 .82 1660 103 1758 200 |
| Gray, Ramsay, 1909 | Flock, Rodebush, 1926 | various | Ruff, Kenschak, 1926 | various |

VAPOR PRESSURE OF ORGANIC LIQUIDS

The vapor pressures on this page are in millimeters over a liquid phase unless distinguished by the subscript _s. They are generally means from various determinations.

| °C | Acetone C ₃ H ₆ O | Benzene C ₆ H ₆ | Camphor C ₁₀ H ₁₆ O | Carbon bisulphide CS ₂ | Carbon tetrachloride CCl ₄ | Chloroform CHCl ₃ | Ethane C ₂ H ₆ | Ethyl ether C ₄ H ₁₀ O | Ethyl bromide C ₂ H ₅ Br | Turpentine C ₁₀ H ₁₆ | |
|---|--|--|--|---|---|---|---|--|--|--|------|
| | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm | |
| -90 | .02 | ... | ... | ... | -70° | -60° | -100° | -101.3° | ... | ... | |
| -57 | 1.26 | -50°, 3 | ... | -80° | .14 | .8 | 390 | .058 | ... | ... | |
| -40 | ... | ... | ... | .6 | -50° | 4.8 | -90° | -60° | ... | ... | |
| -30 | ... | .3 | ... | -25° | .92 | 10 | 700 | 4 | ... | ... | |
| -20 | ... | ... | ... | .34 | ... | 19 | -80° | -40° | 59 | ... | |
| -10 | ... | 14 | ... | 80 | ... | ... | 1180 | 19 | 102 | ... | |
| 0 | ... | 26.5 | .06 | 127 | 33 | 610 | -75° | 186.1 | 166 | .2 | |
| +5 | ... | 34 | ... | 160 | 43 | ... | 1500 | ... | 207 | ... | |
| 10 | 116 | 45 | .10 | 198 | 56 | 100 | ... | 291.8 | 257 | .3 | |
| 15 | ... | 59 | ... | 244 | 71 | ... | ... | ... | 317 | ... | |
| 20 | 185 | 75 | .15 | 298 | 90 | 160 | ... | 442.4 | 386 | .4 | |
| 30 | 283 | 119 | .26 | 433 | 141 | 247 | ... | 648 | 564 | .7 | |
| 40 | 422 | 182 | .60 | 617 | 213 | 370 | ... | 921 | 802 | 1.1 | |
| 50 | 612 | 269 | 1.30 | 855 | 315 | 540 | ... | 1276 | 1113 | 1.7 | |
| 60 | 860 | 390 | 2.6 | 1170 | 448 | 750 | ... | 1728 | 1510 | 2.6 | |
| 70 | 1190 | 548 | 4.6 | 1570 | 620 | 1025 | ... | 2294 | 2015 | 4.1 | |
| 80 | 1860 | 750 | 9.2 | 2040 | 843 | 1400 | ... | 2991 | 2640 | 6.1 | |
| 90 | 2140 | 1010 | ... | 2620 | 1120 | 2130 | ... | 3840 | 3400 | 9.0 | |
| 100 | 2800 | 1340 | 26 | 3000 | 1460 | 2420 | ... | 4860 | 4310 | 13.1 | |
| 110 | 3590 | 1740 | ... | 4160 | 1880 | ... | ... | ... | 5390 | 18.6 | |
| 120 | 4550 | 2200 | ... | 5150 | 2390 | 3900 | ... | 7500 | 6660 | 25.7 | |
| 130 | 5670 | 2800 | ... | ... | 3000 | 4900 | ... | ... | 8120 | 34.9 | |
| 140 | 6970 | 3500 | ... | ... | 3700 | 6000 | ... | 11080 | 9780 | ... | |
| 150 | ... | 4300 | 170 | 9100 | 4500 | 7300 | ... | 160° 15800} | ... | ... | |
| 200 | ... | ... | ... | ... | 10900 | ... | ... | 180° 21800} | ... | ... | |
| | | | | | | | | | | | |
| Ethylene C ₂ H ₄ | | Glycerine C ₃ H ₈ O | | Methane CH ₄ | | Methyl ether (CH ₃) ₂ O | | Naphthalene C ₁₀ H ₈ | | Ethyl chloride C ₂ H ₅ Cl | |
| °C | mm | °C | mm | °C | mm | °C | mm | °C | mm | °C | mm |
| -150 | 14.9 | 118 | .24 | -180 | 119 | -67 | 78 | 0 | .02 _s | -30 | 110 |
| -190 | 45.6 | 161 | 6.5 | -175 | 212 | -60 | 120 | 20 | .06 _s | -20 | 188 |
| -145 | 26.7 | 175 | 13 | -170 | 353 | -41.4 | 326 | 50 | .81 _s | -10 | 302 |
| -135 | 74.4 | 190 | 32 | -165 | 559 | -30.9 | 524 | 70 | 4.0 _s | 0 | 465 |
| -130 | 117.2 | 220 | 100 | -160 | 848 | -241 | 782 | 80 | 10 | 10 | 691 |
| -120 | 260 | 260 | 385 | -155 | 1229 | 0 | 2.52 atm. | 90 | 13 | 20 | 1000 |
| -110 | 519 | | | -150 | 1720 | 25.4 | 6.05 | 100 | 20 | 30 | 1400 |
| -103 | 792 | | | | | 40.75 | 11.2 | 110 | 29 | 50 | 2580 |
| | | | | | | 80.1 | 22.1 | 120 | 43 | 75 | 4980 |
| | | | | | | 90.9 | 32.1 | 150 | 119 | 100 | 8720 |
| | | | | | | 125.0 | 51 | 200 | 490 | | |

Table 200 (continued).—Vapor Pressure of Organic Liquids

| °C | Ammonia NH ₃ | Carbon dioxide CO ₂ | Ethyl iodide C ₂ H ₅ I | Ethyl acetate | Hydrogen sulphide H ₂ S | Methyl chloride CH ₃ Cl | Napthalin C ₁₀ H ₈ | Sulphur dioxide SO ₂ | Toluol C ₁₀ H ₈ |
|-----|----------------------------|--------------------------------------|--|------------------|--|--|---|---------------------------------------|--|
| | atm. | atm. | mm | mm | mm | mm | mm | mm | °C mm |
| -50 | .403 | 6.74 | ... | ... | 1216 | ... | ... | 86 | -91.9 .002 |
| -30 | 1.180 | 14.10 | ... | ... | 2840 | 579 | ... | 286 | -81.7 .005 |
| -25 | 1.496 | 16.61 | ... | ... | ... | 718 | ... | 379 | -77.4 .007 |
| -20 | 1.877 | 19.44 | ... | 6.5 | 4100 | 883 | ... | 474 | -67.5 .020 |
| -15 | 2.332 | 22.60 | ... | ... | ... | 1079 | ... | ... | -57.7 .060 |
| -10 | 2.870 | 26.13 | ... | 12.9 | 5720 | 1310 | ... | 760 | -38.0 .39 |
| -5 | 3.502 | 30.05 | ... | ... | ... | 1579 | ... | ... | -24.2 1.47 |
| 0 | 4.238 | 34.38 | 41.5 | 24.3 | 7750 | 1891 | ... | 1155 | -2.9 5.72 |
| +5 | 5.090 | 39.16 | 53.5 | ... | ... | 2250 | ... | ... | 0 6.86 |
| 10 | 6.068 | 44.41 | 68.6 | 42.7 | 10300 | 2660 | ... | 1714 | +15.0 16.8 |
| 15 | 7.188 | 50.17 | ... | ... | ... | 3134 | ... | ... | +25.8 28.7 |
| 20 | 8.458 | 56.50 | 108.5 | 72.8 | 14000 | 3667 | ... | 2460 | ... |
| 25 | 9.896 | 63.45 | ... | ... | ... | 4267 | ... | ... | ... |
| 30 | 11.512 | 71.4 | 167.6 | 119 | 17500 | 4940 | ... | 3420 | ... |
| 35 | 13.321 | ... | ... | ... | ... | 5700 | ... | ... | ... |
| 40 | 15.339 | (I.C.T. 1928) | 250 | 186 | 22000 | 6650 | ... | 4650 | Drucker, Jumen, |
| 45 | 17.580 | ... | ... | ... | ... | ... | ... | ... | 1915 |
| 50 | 20.060 | ... | 362 | 282 | 27500 | 8510 | ... | 6210 | Barker, 1910 |
| 60 | 25.80 | ... | 510 | 415 | ... | 10900 | ... | 8150 | ... |
| 70 | 32.69 | ... | ... | 596 | 40400 | 14300 | ... | 10540 | ... |
| 80 | 40.90 | ... | ... | 833 | ... | 16800 | 9.6 | ... | ... |
| 90 | 50.56 | ... | ... | 1130 | ... | 21000 | 13.0 | ... | ... |
| 100 | 61.82 | ... | ... | 1515 | ... | 25800 | 19.7 | ... | 27.8 atm. |
| | Craigie 1920 | ... | ... | { 200° 15600 | ... | { 141° 53600 | { 200° 490 | { 150° 71.4 | ... |

Table 201.—Vapor Pressure at Low Temperatures

Many of the following values are extrapolations made by Langmuir by means of plots of $\log p$ against $1/T$. Gen. Elec. Rev. 23, 681, 1920. 1 bar = 0.00000987 atm. = 0.000750 mm Hg.

| Gas | °C | Mm | Gas | °C | Bars |
|-------------------------------|--------|--------|-----------------|------|-----------------------|
| O ₂ | -182.9 | 760 | CO ₂ | -148 | 100 |
| | -211.2 | 7.75 | | -168 | 1 |
| N ₂ | -195.8 | 760 | | -182 | .01 |
| | -210.5 | 86 | | -193 | .0001 |
| CO | -190 | 863 | Ice | -60 | 9.6 |
| | -200 | 249 | | -75 | 1.0 |
| CH ₄ | -185.8 | 79.8 | | -89 | .1 |
| | -201.5 | 50.2 | | -100 | .01 |
| A | -186.2 | 760 | | -110 | .001 |
| | -194.2 | 300 | Hg | +30 | 3.7 |
| C ₂ H ₄ | -175.7 | .76 | | +20 | 1.6 |
| | -188 | .076 | | +10 | .65 |
| | -197 | .0075 | | 0 | .25 |
| | -205 | .00076 | | -10 | .087 |
| C ₂ H ₆ | -150 | 7.6 | | -20 | .029 |
| | -180 | .076 | | -40 | .0023 |
| | -190 | .0076 | | -78 | 4.3×10^{-6} |
| | -198 | .00076 | | -180 | 2.3×10^{-24} |

TABLE 202.—Vapor Pressure of Ethyl Alcohol *

| Temp. C | 0° | 1° | 2° | 3° | 4° | 5° | 6° | 7° | 8° | 9° |
|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| Vapor pressure in millimeters of mercury at 0° C | | | | | | | | | | |
| 0° | 12.24 | 13.18 | 14.15 | 15.16 | 16.21 | 17.31 | 18.46 | 19.68 | 20.98 | 22.34 |
| 10 | 23.78 | 25.31 | 27.94 | 28.67 | 30.50 | 32.44 | 34.49 | 36.67 | 38.97 | 41.40 |
| 20 | 44.00 | 46.66 | 49.47 | 52.44 | 55.56 | 58.86 | 62.33 | 65.97 | 69.80 | 73.83 |
| 30 | 78.06 | 82.50 | 87.17 | 92.07 | 97.21 | 102.60 | 108.24 | 114.15 | 120.35 | 126.86 |
| 40 | 133.70 | 140.75 | 148.10 | 155.80 | 163.80 | 172.20 | 181.00 | 190.10 | 199.65 | 209.60 |
| 50 | 220.00 | 230.80 | 242.50 | 253.80 | 265.90 | 278.60 | 291.85 | 305.65 | 319.95 | 334.85 |
| 60 | 350.30 | 366.40 | 383.10 | 400.40 | 418.35 | 437.00 | 456.35 | 476.45 | 497.25 | 518.85 |
| 70 | 541.20 | 564.35 | 588.35 | 613.20 | 638.95 | 665.55 | 693.10 | 721.55 | 751.00 | 781.45 |

From the formula $\log p = a + \lambda a' + \epsilon \beta'$ Ramsay and Young obtain the following numbers.†

| Temp. C | 0° | 10° | 20° | 30° | 40° | 50° | 60° | 70° | 80° | 90° |
|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| Vapor pressure in millimeters of mercury at 0° C | | | | | | | | | | |
| 0° | 12.24 | 23.73 | 43.97 | 78.11 | 133.42 | 219.82 | 350.21 | 540.91 | 811.81 | 1186.5 |
| 100 | 1692.3 | 2359.8 | 3223.0 | 4318.7 | 5686.6 | 7368.7 | 9409.9 | 11858. | 14764. | 18185. |
| 200 | 22182. | 26825. | 32196. | 38389. | 45519. | | | | | |

TABLE 203.—Vapor Pressure of Methyl Alcohol †

| Temp. C | 0° | 1° | 2° | 3° | 4° | 5° | 6° | 7° | 8° | 9° |
|--|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Vapor pressure in millimeters of mercury at 0° C | | | | | | | | | | |
| 0° | 29.97 | 31.6 | 33.6 | 35.6 | 37.8 | 40.2 | 42.6 | 45.2 | 47.9 | 50.8 |
| 10 | 53.8 | 57.0 | 60.3 | 63.8 | 67.5 | 71.4 | 75.5 | 79.8 | 84.3 | 89.0 |
| 20 | 94.0 | 99.2 | 104.7 | 110.4 | 116.5 | 122.7 | 129.3 | 136.2 | 143.4 | 151.0 |
| 30 | 158.9 | 167.1 | 175.7 | 184.7 | 194.1 | 203.9 | 214.1 | 224.7 | 235.8 | 247.4 |
| 40 | 259.4 | 271.9 | 285.0 | 298.5 | 312.6 | 327.3 | 342.5 | 358.3 | 374.7 | 391.7 |
| 50 | 409.4 | 427.7 | 446.6 | 466.3 | 486.6 | 507.7 | 529.5 | 552.0 | 575.3 | 599.4 |
| 60 | 624.3 | 650.0 | 676.5 | 703.8 | 732.0 | 761.1 | 791.1 | 822.0 | — | — |

* This table has been compiled from results published by Ramsay and Young (Jour. Chem. Soc. vol. 47, and Phil. Trans. Roy. Soc., 1886).

† In this formula $a = 5.0720301$; $\log b = 2.6406131$; $\log c = 0.6050854$; $\log a = 0.003377538$; $\log \beta = 1.99682424$ (ϵ is negative).

‡ Taken from a paper by Dittmar and Fawsitt (Trans. Roy. Soc. Edin. vol. 33).

SMITHSONIAN TABLES.

TABLE 204
VAPOR PRESSURE *

Carbon Disulphide, Chlorobenzene, Bromobenzene, and Aniline

| Temp. C | 0° | 1° | 2° | 3° | 4° | 5° | 6° | 7° | 8° | 9° |
|-------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| (a) CARBON DISULPHIDE. | | | | | | | | | | |
| 0° | 127.90 | 133.85 | 140.05 | 146.45 | 153.10 | 160.00 | 167.15 | 174.60 | 182.25 | 190.20 |
| 10 | 198.45 | 207.00 | 215.80 | 224.95 | 234.40 | 244.15 | 254.25 | 264.65 | 275.40 | 286.55 |
| 20 | 298.05 | 309.90 | 322.10 | 334.70 | 347.70 | 361.10 | 374.95 | 389.20 | 403.90 | 419.00 |
| 30 | 434.60 | 450.65 | 467.15 | 484.15 | 501.65 | 519.65 | 538.15 | 557.15 | 576.75 | 596.85 |
| 40 | 617.50 | 638.70 | 660.50 | 682.90 | 705.90 | 729.50 | 753.75 | 778.60 | 804.10 | 830.25 |
| (b) CHLOROBENZENE. | | | | | | | | | | |
| 20° | 8.65 | 9.14 | 9.66 | 10.21 | 10.79 | 11.40 | 12.04 | 12.71 | 13.42 | 14.17 |
| 30 | 14.95 | 15.77 | 16.63 | 17.53 | 18.47 | 19.45 | 20.48 | 21.56 | 22.69 | 23.87 |
| 40 | 25.10 | 26.38 | 27.72 | 29.12 | 30.58 | 32.10 | 33.69 | 35.35 | 37.08 | 38.88 |
| 50 | 40.75 | 42.69 | 44.72 | 46.84 | 49.05 | 51.35 | 53.74 | 56.22 | 58.79 | 61.45 |
| 60 | 64.20 | 67.06 | 70.03 | 73.11 | 76.30 | 79.60 | 83.02 | 86.56 | 90.22 | 94.00 |
| 70 | 97.90 | 101.95 | 106.10 | 110.41 | 114.85 | 119.45 | 124.20 | 129.10 | 134.15 | 139.40 |
| 80 | 144.80 | 150.30 | 156.05 | 161.95 | 168.00 | 174.25 | 181.70 | 189.30 | 197.10 | 205.15 |
| 90 | 208.35 | 215.80 | 223.45 | 231.30 | 239.35 | 247.70 | 256.20 | 265.00 | 274.00 | 283.25 |
| 100 | 292.75 | 302.50 | 312.50 | 322.80 | 333.35 | 344.15 | 355.25 | 366.65 | 378.30 | 390.25 |
| 110 | 402.55 | 415.10 | 427.95 | 441.15 | 454.65 | 468.50 | 482.65 | 497.20 | 512.05 | 527.25 |
| 120 | 542.80 | 558.70 | 575.05 | 591.70 | 608.75 | 626.15 | 643.95 | 662.15 | 680.75 | 699.65 |
| 130 | 718.95 | 738.65 | 758.80 | — | — | — | — | — | — | — |
| (c) BROMOBENZENE. | | | | | | | | | | |
| 40° | — | — | — | — | — | 12.40 | 13.06 | 13.75 | 14.47 | 15.22 |
| 50 | 16.00 | 16.82 | 17.68 | 18.58 | 19.52 | 20.50 | 21.52 | 22.59 | 23.71 | 24.88 |
| 60 | 26.10 | 27.36 | 28.68 | 30.06 | 31.50 | 33.00 | 34.56 | 36.18 | 37.86 | 39.60 |
| 70 | 41.40 | 43.28 | 45.24 | 47.28 | 49.40 | 51.60 | 53.88 | 56.25 | 58.71 | 61.26 |
| 80 | 63.90 | 66.64 | 69.48 | 72.42 | 75.46 | 78.60 | 81.84 | 85.20 | 88.68 | 92.28 |
| 90 | 96.00 | 99.84 | 103.80 | 107.88 | 112.08 | 116.40 | 120.86 | 125.46 | 130.20 | 135.08 |
| 100 | 140.10 | 145.26 | 150.57 | 156.03 | 161.64 | 167.40 | 173.32 | 179.41 | 185.67 | 192.10 |
| 110 | 198.70 | 205.48 | 212.44 | 219.58 | 226.90 | 234.40 | 242.10 | 250.00 | 258.10 | 266.40 |
| 120 | 274.90 | 283.65 | 292.60 | 301.75 | 311.15 | 320.80 | 330.70 | 340.80 | 351.15 | 361.80 |
| 130 | 372.65 | 383.75 | 395.10 | 406.70 | 418.60 | 430.75 | 443.20 | 455.90 | 468.90 | 482.20 |
| 140 | 495.80 | 509.70 | 523.90 | 538.40 | 553.20 | 568.35 | 583.85 | 599.65 | 615.75 | 632.25 |
| 150 | 649.05 | 666.25 | 683.80 | 701.65 | 719.95 | 738.55 | 757.55 | 776.95 | 796.70 | 816.90 |
| (d) ANILINE. | | | | | | | | | | |
| 80° | 18.80 | 19.78 | 20.79 | 21.83 | 22.90 | 24.00 | 25.14 | 26.32 | 27.54 | 28.80 |
| 90 | 30.10 | 31.44 | 32.83 | 34.27 | 35.76 | 37.30 | 38.90 | 40.56 | 42.28 | 44.06 |
| 100 | 45.90 | 47.80 | 49.78 | 51.84 | 53.98 | 56.20 | 58.50 | 60.88 | 63.34 | 65.88 |
| 110 | 68.50 | 71.22 | 74.04 | 76.96 | 79.98 | 83.10 | 86.32 | 89.66 | 93.12 | 96.70 |
| 120 | 100.40 | 104.22 | 108.17 | 112.25 | 116.46 | 120.80 | 125.28 | 129.91 | 134.69 | 139.62 |
| 130 | 144.70 | 149.94 | 155.34 | 160.90 | 166.62 | 172.50 | 178.56 | 184.80 | 191.22 | 197.82 |
| 140 | 204.60 | 211.58 | 218.76 | 226.14 | 233.72 | 241.50 | 249.50 | 257.72 | 266.16 | 274.82 |
| 150 | 283.70 | 292.80 | 302.15 | 311.75 | 321.60 | 331.70 | 342.05 | 352.65 | 363.50 | 374.60 |
| 160 | 386.00 | 397.65 | 409.60 | 421.80 | 434.30 | 447.10 | 460.20 | 473.60 | 487.25 | 501.25 |
| 170 | 515.60 | 530.20 | 545.20 | 560.45 | 576.10 | 592.05 | 608.35 | 625.05 | 642.05 | 659.45 |
| 180 | 677.15 | 695.30 | 713.75 | 732.65 | 751.90 | 771.50 | — | — | — | — |

* These tables of vapor pressures are quoted from results published by Ramsay and Young (Jour. Chem. Soc. vol. 47). The tables are intended to give a series suitable for hot-jacket purposes.

SMITHSONIAN TABLES.

VAPOR PRESSURE

Methyl Salicylate, Bromonaphthalene, and Mercury

| Temp. C | 0° | 1° | 2° | 3° | 4° | 5° | 6° | 7° | 8° | 9° |
|------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| (e) METHYL SALICYLATE. | | | | | | | | | | |
| 70° | 2.40 | 2.58 | 2.77 | 2.97 | 3.18 | 3.40 | 3.62 | 3.85 | 4.09 | 4.34 |
| 80 | 4.60 | 4.87 | 5.15 | 5.44 | 5.74 | 6.05 | 6.37 | 6.70 | 7.05 | 7.42 |
| 90 | 7.80 | 8.20 | 8.62 | 9.06 | 9.52 | 9.95 | 10.41 | 10.95 | 11.48 | 12.03 |
| 100 | 12.60 | 13.20 | 13.82 | 14.47 | 15.15 | 15.85 | 16.58 | 17.34 | 18.13 | 18.95 |
| 110 | 19.80 | 20.68 | 21.60 | 22.55 | 23.53 | 24.55 | 25.61 | 26.71 | 27.85 | 29.03 |
| 120 | 30.25 | 31.52 | 32.84 | 34.21 | 35.63 | 37.10 | 38.67 | 40.24 | 41.84 | 43.54 |
| 130 | 45.30 | 47.12 | 49.01 | 50.96 | 52.97 | 55.05 | 57.20 | 59.43 | 61.73 | 64.10 |
| 140 | 66.55 | 69.68 | 71.69 | 74.38 | 77.15 | 80.00 | 82.94 | 85.97 | 89.09 | 92.30 |
| 150 | 95.60 | 99.00 | 102.50 | 106.10 | 109.80 | 113.60 | 117.51 | 121.53 | 125.66 | 129.90 |
| 160 | 134.25 | 138.72 | 143.31 | 148.03 | 152.88 | 157.85 | 162.95 | 168.19 | 173.56 | 179.06 |
| 170 | 184.70 | 190.48 | 196.41 | 202.49 | 208.72 | 215.10 | 221.65 | 228.30 | 235.15 | 242.15 |
| 180 | 249.35 | 256.70 | 264.20 | 271.90 | 279.75 | 287.80 | 296.00 | 304.48 | 313.05 | 321.85 |
| 190 | 330.85 | 340.05 | 349.45 | 359.05 | 368.85 | 378.90 | 389.15 | 399.60 | 410.30 | 421.20 |
| 200 | 432.35 | 443.75 | 455.35 | 467.25 | 479.35 | 491.70 | 504.35 | 517.25 | 530.40 | 543.80 |
| 210 | 557.50 | 571.45 | 585.70 | 600.25 | 615.05 | 630.15 | 645.55 | 661.25 | 677.25 | 693.60 |
| 220 | 710.10 | 727.05 | 744.35 | 761.90 | 779.85 | 798.10 | | | | |
| (f) BRONAPHTHALENE. | | | | | | | | | | |
| 110 | 3.60 | 3.74 | 3.89 | 4.05 | 4.22 | 4.40 | 4.59 | 4.79 | 5.00 | 5.22 |
| 120 | 5.45 | 5.70 | 5.96 | 6.23 | 6.51 | 6.80 | 7.10 | 7.42 | 7.76 | 8.12 |
| 130 | 8.50 | 8.89 | 9.29 | 9.71 | 10.15 | 10.60 | 11.07 | 11.56 | 12.07 | 12.60 |
| 140 | 13.15 | 13.72 | 14.31 | 14.92 | 15.55 | 16.20 | 16.87 | 17.56 | 18.28 | 19.03 |
| 150 | 19.80 | 20.59 | 21.41 | 22.25 | 23.11 | 24.00 | 24.92 | 25.86 | 26.83 | 27.83 |
| 160 | 28.85 | 29.90 | 30.98 | 32.09 | 33.23 | 34.40 | 35.60 | 36.83 | 38.10 | 39.41 |
| 170 | 40.75 | 42.12 | 43.53 | 44.99 | 46.50 | 48.05 | 49.64 | 51.28 | 52.96 | 54.68 |
| 180 | 56.45 | 58.27 | 60.14 | 62.04 | 64.06 | 66.10 | 68.19 | 70.34 | 72.55 | 74.82 |
| 190 | 77.15 | 79.54 | 81.99 | 84.51 | 87.10 | 89.75 | 92.47 | 95.26 | 98.12 | 101.05 |
| 200 | 104.05 | 107.12 | 110.27 | 113.50 | 116.81 | 120.20 | 123.67 | 127.22 | 130.86 | 134.59 |
| 210 | 138.40 | 142.30 | 146.29 | 150.38 | 154.57 | 158.85 | 163.25 | 167.70 | 172.30 | 176.95 |
| 220 | 181.75 | 186.05 | 191.65 | 196.75 | 202.00 | 207.35 | 212.80 | 218.40 | 224.15 | 230.00 |
| 230 | 235.95 | 242.05 | 248.30 | 254.65 | 261.20 | 267.85 | 274.65 | 281.60 | 288.70 | 295.95 |
| 240 | 303.35 | 310.90 | 318.65 | 326.50 | 334.55 | 342.75 | 351.10 | 359.65 | 368.40 | 377.30 |
| 250 | 386.35 | 395.60 | 405.05 | 414.65 | 424.45 | 434.45 | 444.65 | 455.00 | 465.60 | 476.35 |
| 260 | 487.35 | 498.55 | 509.90 | 521.50 | 533.35 | 545.35 | 557.60 | 570.05 | 582.70 | 595.60 |
| 270 | 608.75 | 622.10 | 635.70 | 649.50 | 663.55 | 677.85 | 692.40 | 707.15 | 722.15 | 737.45 |
| (g) MERCURY. | | | | | | | | | | |
| 270° | 123.02 | 126.97 | 130.08 | 133.26 | 136.50 | 139.81 | 143.18 | 146.61 | 150.12 | 153.70 |
| 280 | 157.35 | 161.07 | 164.86 | 168.73 | 172.67 | 176.79 | 180.88 | 185.05 | 189.30 | 193.63 |
| 290 | 198.04 | 202.53 | 207.10 | 211.76 | 216.50 | 221.33 | 226.25 | 231.25 | 236.34 | 241.53 |
| 300 | 246.81 | 252.18 | 257.65 | 263.21 | 268.87 | 274.63 | 280.48 | 286.43 | 292.49 | 298.66 |
| 310 | 304.93 | 311.30 | 317.78 | 324.37 | 331.08 | 337.89 | 344.81 | 351.85 | 359.00 | 366.28 |
| 320 | 373.67 | 381.18 | 388.81 | 396.56 | 404.43 | 412.44 | 420.58 | 428.83 | 437.22 | 445.75 |
| 330 | 454.41 | 463.20 | 472.12 | 481.19 | 490.40 | 499.74 | 509.22 | 518.85 | 528.63 | 538.56 |
| 340 | 548.64 | 558.87 | 569.25 | 579.78 | 590.48 | 601.33 | 612.34 | 623.51 | 634.85 | 646.36 |
| 350 | 658.03 | 669.86 | 681.86 | 694.04 | 706.40 | 718.94 | 731.65 | 744.54 | 757.61 | 770.87 |
| 360 | 784.31 | | | | | | | | | |

VAPOR PRESSURE OF SOLUTIONS OF SALTS IN WATER *

The first column gives the chemical formula of the salt. The headings of the other columns give the number of gram-molecules of the salt in a liter of water. The numbers in these columns give the lowering of the vapor pressure produced by the salt at the temperature of boiling water under 76 centimeters barometric pressure.

| Substance. | 0.5 | 1.0 | 2.0 | 3.0 | 4.0 | 5.0 | 6.0 | 8.0 | 10.0 |
|----------------------------------|------|------|-------|-------|-------|-------|-------|-------|-------|
| $\text{Al}_2(\text{SO}_4)_3$ | 12.8 | 36.5 | | | | | | | |
| AlCl_3 | 22.5 | 61.0 | 179.0 | 318.0 | | | | | |
| BaS_2O_8 | 6.6 | 15.4 | 34.4 | | | | | | |
| $\text{Ba}(\text{OH})_2$ | 12.3 | 22.5 | 39.0 | | | | | | |
| $\text{Ba}(\text{NO}_3)_2$ | 13.5 | 27.0 | | | | | | | |
| $\text{Ba}(\text{ClO}_3)_2$ | 15.8 | 33.3 | 70.5 | 108.2 | | | | | |
| BaCl_2 | 16.4 | 36.7 | 77.6 | | | | | | |
| BaBr_2 | 16.8 | 38.8 | 91.4 | 150.0 | 204.7 | | | | |
| CaS_2O_8 | 9.9 | 23.0 | 56.0 | 106.0 | | | | | |
| $\text{Ca}(\text{NO}_3)_2$ | 16.4 | 34.8 | 74.6 | 139.3 | 161.7 | 205.4 | | | |
| CaCl_2 | 17.0 | 39.8 | 95.3 | 166.6 | 241.5 | 319.5 | | | |
| CaBr_2 | 17.7 | 44.2 | 105.8 | 191.0 | 283.3 | 368.5 | | | |
| CdSO_4 | 4.1 | 8.9 | 18.1 | | | | | | |
| CdI_2 | 7.6 | 14.8 | 33.5 | 52.7 | | | | | |
| CdBr_2 | 8.6 | 17.8 | 36.7 | 55.7 | 80.0 | | | | |
| CdCl_2 | 9.6 | 18.8 | 36.7 | 57.0 | 77.3 | 99.0 | | | |
| $\text{Cd}(\text{NO}_3)_2$ | 15.9 | 36.1 | 78.0 | 122.2 | | | | | |
| $\text{Cd}(\text{ClO}_3)_2$ | 17.5 | | | | | | | | |
| CoSO_4 | 5.5 | 10.7 | 22.9 | 45.5 | | | | | |
| CoCl_2 | 15.0 | 34.8 | 83.0 | 136.0 | 186.4 | | | | |
| $\text{Co}(\text{NO}_3)_2$ | 17.3 | 39.2 | 89.0 | 152.0 | 218.7 | 282.0 | 332.0 | | |
| FeSO_4 | 5.8 | 10.7 | 24.0 | 42.4 | | | | | |
| H_3BO_3 | 6.0 | 12.3 | 25.1 | 38.0 | 51.0 | | | | |
| H_3PO_4 | 6.6 | 14.0 | 28.6 | 45.2 | 62.0 | 81.5 | 103.0 | 146.9 | 189.5 |
| H_3AsO_4 | 7.3 | 15.0 | 30.2 | 46.4 | 64.9 | | | | |
| H_2SO_4 | 12.9 | 26.5 | 62.8 | 104.0 | 148.0 | 198.4 | 247.0 | 343.2 | |
| KH_2PO_4 | 10.2 | 19.5 | 33.3 | 47.8 | 60.5 | 73.1 | 85.2 | | |
| KNO_3 | 10.3 | 21.1 | 40.1 | 57.6 | 74.5 | 88.2 | 102.1 | 126.3 | 148.0 |
| KClO_3 | 10.6 | 21.6 | 42.8 | 62.1 | 80.0 | | | | |
| KBrO_3 | 10.9 | 22.4 | 45.0 | | | | | | |
| KH_2SO_4 | 10.9 | 21.9 | 43.3 | 65.3 | 85.5 | 107.8 | 129.2 | 170.0 | |
| KNO_2 | 11.1 | 22.8 | 44.8 | 67.0 | 90.0 | 110.5 | 130.7 | 167.0 | 198.8 |
| KClO_4 | 11.5 | 22.3 | | | | | | | |
| KCl | 12.2 | 24.4 | 48.8 | 74.1 | 100.9 | 128.5 | 152.2 | | |
| KHCO_3 | 11.6 | 23.6 | 59.0 | 77.6 | 104.2 | 132.0 | 160.0 | 210.0 | 255.0 |
| KI | 12.5 | 25.3 | 52.2 | 82.6 | 112.2 | 141.5 | 171.8 | 225.5 | 278.5 |
| $\text{K}_2\text{C}_2\text{O}_4$ | 13.9 | 28.3 | 59.8 | 94.2 | 131.0 | | | | |
| K_2WO_4 | 13.9 | 33.0 | 75.0 | 123.8 | 175.4 | 226.4 | | | |
| K_2CO_3 | 14.4 | 31.0 | 68.3 | 105.5 | 152.0 | 209.0 | 258.5 | 350.0 | |
| KOH | 15.0 | 29.5 | 64.0 | 99.2 | 140.0 | 181.8 | 223.0 | 309.5 | 387.8 |
| K_2CrO_4 | 16.2 | 29.5 | 60.0 | | | | | | |
| LiNO_3 | 12.2 | 25.9 | 55.7 | 88.9 | 122.2 | 155.1 | 188.0 | 253.4 | 309.2 |
| LiCl | 12.1 | 25.5 | 57.1 | 95.0 | 132.5 | 175.5 | 219.5 | 311.5 | 393.5 |
| LiBr | 12.2 | 26.2 | 60.0 | 97.0 | 140.0 | 186.3 | 241.5 | 341.5 | 438.0 |
| Li_2SO_4 | 13.3 | 28.1 | 56.8 | 89.0 | | | | | |
| LiHSO_4 | 12.8 | 27.0 | 57.0 | 93.0 | 130.0 | 168.0 | | | |
| LiI | 13.6 | 28.6 | 64.7 | 105.2 | 154.5 | 206.0 | 264.0 | 357.0 | 445.0 |
| Li_2SiF_6 | 15.4 | 34.0 | 70.0 | 106.0 | | | | | |
| LiOH | 15.9 | 37.4 | 78.1 | | | | | | |
| Li_2CrO_4 | 16.4 | 32.6 | 74.0 | 120.0 | 171.0 | | | | |

* Compiled from a table by Tammann, "Mém. Ac. St. Petersburg," 35, No. 9, 1887. See also Referate, "Zeit. f. Phys." ch. 2, 42, 1886.

VAPOR PRESSURE OF SOLUTIONS OF SALTS IN WATER

| Substance. | 0.5 | 1.0 | 2.0 | 3.0 | 4.0 | 5.0 | 6.0 | 8.0 | 10.0 |
|--|------|------|-------|-------|-------|-------|-------|-------|-------|
| MgSO ₄ . . . | 6.5 | 12.0 | 24.5 | 47.5 | | | | | |
| MgCl ₂ . . . | 16.8 | 39.0 | 100.5 | 183.3 | 277.0 | 377.0 | | | |
| Mg(NO ₃) ₂ . . . | 17.6 | 42.0 | 101.0 | 174.8 | | | | | |
| MgBr ₂ . . . | 17.9 | 44.0 | 115.8 | 205.3 | 298.5 | | | | |
| MgH ₂ (SO ₄) ₂ . . . | 18.3 | 46.0 | 116.0 | | | | | | |
| MnSO ₄ . . . | 6.0 | 10.5 | 21.0 | | | | | | |
| MnCl ₂ . . . | 15.0 | 34.0 | 76.0 | 122.3 | 167.0 | 209.0 | | | |
| NaH ₂ PO ₄ . . . | 10.5 | 20.0 | 36.5 | 51.7 | 66.8 | 82.0 | 96.5 | 126.7 | 157.1 |
| NaHSO ₄ . . . | 10.9 | 22.1 | 47.3 | 75.0 | 100.2 | 126.1 | 148.5 | 189.7 | 231.4 |
| NaNO ₃ . . . | 10.6 | 22.5 | 46.2 | 68.1 | 90.3 | 111.5 | 131.7 | 167.8 | 198.8 |
| NaClO ₃ . . . | 10.5 | 23.0 | 48.4 | 73.5 | 98.5 | 123.3 | 147.5 | 196.5 | 223.5 |
| (NaPO ₃) ₆ . . . | 11.6 | | | | | | | | |
| NaOH . . . | 11.8 | 22.8 | 48.2 | 77.3 | 107.5 | 139.1 | 172.5 | 243.3 | 314.0 |
| NaNO ₂ . . . | 11.6 | 24.4 | 50.0 | 75.0 | 98.2 | 122.5 | 146.5 | 189.0 | 226.2 |
| Na ₂ HPO ₄ . . . | 12.1 | 23.5 | 43.0 | 60.0 | 78.7 | 99.8 | 122.1 | | |
| NaHCO ₃ . . . | 12.9 | 24.1 | 48.2 | 77.6 | 102.2 | 127.8 | 152.0 | 198.0 | 239.4 |
| Na ₂ SO ₄ . . . | 12.6 | 25.0 | 48.9 | 74.2 | | | | | |
| NaCl . . . | 12.3 | 25.2 | 52.1 | 80.0 | 111.0 | 143.0 | 176.5 | | |
| NaBrO ₃ . . . | 12.1 | 25.0 | 54.1 | 81.3 | 108.8 | 136.0 | | | |
| NaBr . . . | 12.6 | 25.9 | 57.0 | 89.2 | 124.2 | 159.5 | 197.5 | 268.0 | |
| NaI . . . | 12.1 | 25.6 | 60.2 | 99.5 | 136.7 | 177.5 | 221.0 | 301.5 | 370.0 |
| Na ₄ P ₂ O ₇ . . . | 13.2 | 22.0 | | | | | | | |
| Na ₂ CO ₃ . . . | 14.3 | 27.3 | 53.5 | 80.2 | 111.0 | | | | |
| Na ₂ C ₂ O ₄ . . . | 14.5 | 30.0 | 65.8 | 105.8 | 146.0 | | | | |
| Na ₂ WO ₄ . . . | 14.8 | 33.6 | 71.6 | 115.7 | 162.6 | | | | |
| Na ₃ PO ₄ . . . | 16.5 | 30.0 | 52.5 | | | | | | |
| (NaPO ₃) ₃ . . . | 17.1 | 36.5 | | | | | | | |
| NH ₄ NO ₃ . . . | 12.8 | 22.0 | 42.1 | 62.7 | 82.9 | 103.8 | 121.0 | 152.2 | 180.0 |
| (NH ₄) ₂ SiF ₆ . . . | 11.5 | 25.0 | 44.5 | | | | | | |
| NH ₄ Cl . . . | 12.0 | 23.7 | 45.1 | 69.3 | 94.2 | 118.5 | 138.2 | 179.0 | 213.8 |
| NH ₄ HSO ₄ . . . | 11.5 | 22.0 | 46.8 | 71.0 | 94.5 | 118. | 139.0 | 181.2 | 218.0 |
| (NH ₄) ₂ SO ₄ . . . | 11.0 | 24.0 | 46.5 | 69.5 | 93.0 | 117.0 | 141.8 | | |
| NH ₄ Br . . . | 11.9 | 23.9 | 48.8 | 74.1 | 99.4 | 121.5 | 145.5 | 190.2 | 228.5 |
| NH ₄ I . . . | 12.9 | 25.1 | 49.8 | 78.5 | 104.5 | 132.3 | 156.0 | 200.0 | 243.5 |
| NiSO ₄ . . . | 5.0 | 10.2 | 21.5 | | | | | | |
| NiCl ₂ . . . | 16.1 | 37.0 | 86.7 | 147.0 | 212.8 | | | | |
| Ni(NO ₃) ₂ . . . | 16.1 | 37.3 | 91.3 | 156.2 | 235.0 | | | | |
| Pb(NO ₃) ₂ . . . | 12.3 | 23.5 | 45.0 | 63.0 | | | | | |
| Sr(SO ₃) ₂ . . . | 7.2 | 20.3 | 47.0 | | | | | | |
| Sr(NO ₃) ₂ . . . | 15.8 | 31.0 | 64.0 | 97.4 | 131.4 | | | | |
| SrCl ₂ . . . | 16.8 | 38.8 | 91.4 | 156.8 | 223.3 | 281.5 | | | |
| SrBr ₂ . . . | 17.8 | 42.0 | 101.1 | 179.0 | 267.0 | | | | |
| ZnSO ₄ . . . | 4.9 | 10.4 | 21.5 | 42.1 | 66.2 | | | | |
| ZnCl ₂ . . . | 9.2 | 18.7 | 46.2 | 75.0 | 107.0 | 153.0 | 195.0 | | |
| Zn(NO ₃) ₂ . . . | 16.6 | 39.0 | 93.5 | 157.5 | 223.8 | | | | |

PRESSURE OF SATURATED AQUEOUS VAPOR

The following tables for the pressure of saturated aqueous vapor are taken principally from the Fourth Revised Edition (1918) of the Smithsonian Meteorological Tables.

TABLE 206.—At Low Temperatures.—69° to 0° C over Ice

| Temp. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm |
| -60 | 0.008 | 0.007 | 0.006 | 0.005 | 0.004 | 0.004 | 0.003 | 0.003 | 0.003 | 0.002 |
| -50 | 0.020 | 0.020 | 0.023 | 0.020 | 0.017 | 0.015 | 0.013 | 0.012 | 0.010 | 0.009 |
| -40 | 0.066 | 0.086 | 0.076 | 0.068 | 0.060 | 0.054 | 0.048 | 0.042 | 0.037 | 0.033 |
| -30 | 0.288 | 0.259 | 0.233 | 0.209 | 0.188 | 0.169 | 0.151 | 0.135 | 0.121 | 0.108 |
| -20 | 0.783 | 0.712 | 0.646 | 0.585 | 0.530 | 0.480 | 0.434 | 0.392 | 0.354 | 0.319 |
| -10 | 1.964 | 1.798 | 1.644 | 1.503 | 1.373 | 1.252 | 1.142 | 1.041 | 0.947 | 0.861 |
| - 0 | 4.580 | 4.220 | 3.887 | 3.578 | 3.291 | 3.025 | 2.778 | 2.550 | 2.340 | 2.144 |

TABLE 207.—At Low Temperatures, -16° to 0° C over Water

| Temp. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm |
| -10° | 2.144 | 1.979 | 1.826 | 1.684 | 1.551 | 1.429 | 1.315 | — | — | — |
| - 0° | 4.579 | 4.255 | 3.952 | 3.669 | 3.404 | 3.158 | 2.928 | 2.712 | 2.509 | 2.321 |

TABLE 208.—For Temperatures 0° to 374° C over Water

| Temp. | .0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm |
| 0° | 4.580 | 4.614 | 4.647 | 4.681 | 4.715 | 4.750 | 4.784 | 4.819 | 4.854 | 4.889 |
| 1 | 4.924 | 4.960 | 4.996 | 5.032 | 5.068 | 5.105 | 5.142 | 5.179 | 5.216 | 5.254 |
| 2 | 5.291 | 5.329 | 5.368 | 5.406 | 5.445 | 5.484 | 5.523 | 5.562 | 5.602 | 5.642 |
| 3 | 5.682 | 5.723 | 5.763 | 5.804 | 5.840 | 5.887 | 5.929 | 5.971 | 6.013 | 6.056 |
| 4 | 6.098 | 6.141 | 6.185 | 6.228 | 6.272 | 6.316 | 6.361 | 6.406 | 6.450 | 6.496 |
| 5 | 6.541 | 6.587 | 6.633 | 6.680 | 6.726 | 6.773 | 6.820 | 6.868 | 6.916 | 6.964 |
| 6 | 7.012 | 7.061 | 7.110 | 7.159 | 7.209 | 7.259 | 7.309 | 7.360 | 7.410 | 7.462 |
| 7 | 7.513 | 7.565 | 7.617 | 7.669 | 7.722 | 7.775 | 7.828 | 7.882 | 7.936 | 7.991 |
| 8 | 8.045 | 8.100 | 8.156 | 8.211 | 8.267 | 8.324 | 8.380 | 8.437 | 8.494 | 8.552 |
| 9 | 8.610 | 8.669 | 8.727 | 8.786 | 8.846 | 8.906 | 8.966 | 9.026 | 9.087 | 9.148 |
| 10 | 9.21 | 9.27 | 9.33 | 9.40 | 9.46 | 9.52 | 9.59 | 9.65 | 9.72 | 9.78 |
| 11 | 9.85 | 9.91 | 9.98 | 10.04 | 10.11 | 10.18 | 10.25 | 10.31 | 10.38 | 10.45 |
| 12 | 10.52 | 10.59 | 10.66 | 10.73 | 10.80 | 10.87 | 10.94 | 11.02 | 11.09 | 11.16 |
| 13 | 11.24 | 11.31 | 11.38 | 11.46 | 11.53 | 11.61 | 11.68 | 11.76 | 11.84 | 11.92 |
| 14 | 11.99 | 12.07 | 12.15 | 12.23 | 12.31 | 12.39 | 12.47 | 12.55 | 12.63 | 12.71 |
| 15 | 12.79 | 12.88 | 12.96 | 13.04 | 13.13 | 13.21 | 13.30 | 13.38 | 13.47 | 13.56 |
| 16 | 13.64 | 13.73 | 13.82 | 13.91 | 14.00 | 14.08 | 14.17 | 14.26 | 14.36 | 14.45 |
| 17 | 14.54 | 14.63 | 14.73 | 14.82 | 14.91 | 15.01 | 15.10 | 15.20 | 15.29 | 15.39 |
| 18 | 15.49 | 15.58 | 15.68 | 15.78 | 15.88 | 15.98 | 16.08 | 16.18 | 16.28 | 16.39 |
| 19 | 16.49 | 16.59 | 16.70 | 16.80 | 16.91 | 17.01 | 17.12 | 17.22 | 17.33 | 17.44 |
| 20 | 17.55 | 17.66 | 17.77 | 17.88 | 17.99 | 18.10 | 18.21 | 18.32 | 18.44 | 18.55 |
| 21 | 18.66 | 18.78 | 18.90 | 19.01 | 19.13 | 19.25 | 19.36 | 19.48 | 19.60 | 19.72 |
| 22 | 19.84 | 19.96 | 20.09 | 20.21 | 20.33 | 20.46 | 20.58 | 20.71 | 20.83 | 20.96 |
| 23 | 21.09 | 21.22 | 21.34 | 21.47 | 21.60 | 21.73 | 21.87 | 22.00 | 22.13 | 22.26 |
| 24 | 22.40 | 22.53 | 22.67 | 22.80 | 22.94 | 23.08 | 23.22 | 23.36 | 23.50 | 23.64 |
| 25 | 23.78 | 23.92 | 24.06 | 24.21 | 24.35 | 24.50 | 24.64 | 24.79 | 24.94 | 25.09 |

PRESSURE OF SATURATED AQUEOUS VAPOR

For Temperatures 0° to 374° C over Water

| Temp. C | .0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 |
|------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm |
| 25° | 23.78 | 23.92 | 24.06 | 24.21 | 24.35 | 24.50 | 24.64 | 24.79 | 24.94 | 25.09 |
| 26 | 25.24 | 25.38 | 25.54 | 25.69 | 25.84 | 25.99 | 26.13 | 26.30 | 26.46 | 26.61 |
| 27 | 26.77 | 26.92 | 27.08 | 27.24 | 27.40 | 27.56 | 27.72 | 27.89 | 28.05 | 28.22 |
| 28 | 28.38 | 28.55 | 28.71 | 28.88 | 29.05 | 29.22 | 29.39 | 29.56 | 29.73 | 29.90 |
| 29 | 30.08 | 30.25 | 30.43 | 30.60 | 30.78 | 30.96 | 31.14 | 31.32 | 31.50 | 31.68 |
| 30 | 31.86 | 32.04 | 32.23 | 32.41 | 32.60 | 32.79 | 32.97 | 33.16 | 33.35 | 33.54 |
| 31 | 33.74 | 33.93 | 34.12 | 34.32 | 34.51 | 34.71 | 34.91 | 35.10 | 35.30 | 35.50 |
| 32 | 35.70 | 35.91 | 36.11 | 36.32 | 36.52 | 36.73 | 36.94 | 37.14 | 37.35 | 37.56 |
| 33 | 37.78 | 37.99 | 38.20 | 38.42 | 38.63 | 38.85 | 39.06 | 39.28 | 39.50 | 39.72 |
| 34 | 39.95 | 40.17 | 40.39 | 40.62 | 40.85 | 41.07 | 41.30 | 41.53 | 41.76 | 41.99 |
| 35 | 42.23 | 42.46 | 42.70 | 42.93 | 43.17 | 43.41 | 43.65 | 43.89 | 44.13 | 44.37 |
| 36 | 44.62 | 44.86 | 45.11 | 45.36 | 45.61 | 45.86 | 46.11 | 46.36 | 46.62 | 46.87 |
| 37 | 47.13 | 47.38 | 47.64 | 47.90 | 48.16 | 48.43 | 48.69 | 48.95 | 49.22 | 49.49 |
| 38 | 49.76 | 50.02 | 50.30 | 50.57 | 50.84 | 51.12 | 51.39 | 51.67 | 51.95 | 52.23 |
| 39 | 52.51 | 52.79 | 53.08 | 53.39 | 53.65 | 53.92 | 54.23 | 54.52 | 54.81 | 55.10 |
| 40 | 55.40 | 55.69 | 55.99 | 56.29 | 56.59 | 56.89 | 57.19 | 57.50 | 57.80 | 58.11 |
| 41 | 58.42 | 58.73 | 59.04 | 59.35 | 59.66 | 59.98 | 60.30 | 60.62 | 60.94 | 61.26 |
| 42 | 61.58 | 61.90 | 62.23 | 62.56 | 62.89 | 63.22 | 63.55 | 63.88 | 64.22 | 64.55 |
| 43 | 64.89 | 65.23 | 65.57 | 65.91 | 66.25 | 66.60 | 66.95 | 67.30 | 67.64 | 68.00 |
| 44 | 68.35 | 68.70 | 69.06 | 69.42 | 69.78 | 70.14 | 70.50 | 70.87 | 71.23 | 71.60 |
| 45 | 71.97 | 72.34 | 72.71 | 73.09 | 73.46 | 73.84 | 74.22 | 74.60 | 74.98 | 75.36 |
| 46 | 75.75 | 76.14 | 76.53 | 76.92 | 77.31 | 77.70 | 78.10 | 78.50 | 78.90 | 79.30 |
| 47 | 79.70 | 80.11 | 80.51 | 80.92 | 81.33 | 81.74 | 82.16 | 82.57 | 82.99 | 83.41 |
| 48 | 83.83 | 84.25 | 84.68 | 85.10 | 85.53 | 85.96 | 86.39 | 86.83 | 87.26 | 87.70 |
| 49 | 88.14 | 88.58 | 89.02 | 89.47 | 89.92 | 90.36 | 90.82 | 91.27 | 91.72 | 92.18 |
| | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 50 | 92.6 | 97.3 | 102.2 | 107.3 | 112.7 | 118.2 | 124.0 | 130.0 | 136.3 | 142.8 |
| 60 | 149.6 | 156.6 | 164.0 | 171.6 | 179.5 | 187.8 | 196.3 | 205.2 | 214.4 | 224.0 |
| 70 | 233.9 | 244.2 | 254.9 | 266.0 | 277.4 | 289.3 | 301.6 | 314.4 | 327.6 | 341.2 |
| 80 | 355.4 | 370.0 | 385.2 | 400.8 | 417.0 | 433.7 | 451.0 | 468.8 | 487.3 | 506.3 |
| 90 | 526.0 | 546.3 | 567.2 | 588.8 | 611.1 | 634.1 | 657.8 | 682.2 | 707.4 | 733.3 |
| 100 | 760.0 | 787.5 | 815.9 | 845.0 | 875.1 | 906.0 | 937.8 | 970.5 | 1004.2 | 1038.8 |
| 110 | 1074 | 1111 | 1149 | 1187 | 1227 | 1268 | 1310 | 1353 | 1397 | 1442 |
| 120 | 1489 | 1536 | 1585 | 1636 | 1687 | 1740 | 1794 | 1850 | 1907 | 1965 |
| 130 | 2025 | 2086 | 2149 | 2214 | 2280 | 2347 | 2416 | 2487 | 2559 | 2633 |
| 140 | 2709 | 2786 | 2866 | 2947 | 3030 | 3115 | 3201 | 3290 | 3381 | 3473 |
| 150 | 3568 | 3665 | 3763 | 3864 | 3967 | 4072 | 4180 | 4290 | 4402 | 4516 |
| 160 | 4632 | 4751 | 4873 | 4997 | 5123 | 5252 | 5383 | 5515 | 5654 | 5794 |
| 170 | 5936 | 6080 | 6228 | 6378 | 6532 | 6688 | 6847 | 7009 | 7174 | 7342 |
| 180 | 7513 | 7688 | 7865 | 8046 | 8230 | 8417 | 8608 | 8802 | 8999 | 9200 |
| 190 | 9494 | 9692 | 9893 | 10096 | 10260 | 10480 | 10700 | 10940 | 11170 | 11410 |
| 200 | 11650 | 11890 | 12140 | 12400 | 12650 | 12920 | 13180 | 13450 | 13730 | 14010 |
| 210 | 14290 | 14580 | 14870 | 15160 | 15470 | 15770 | 16080 | 16400 | 16720 | 17040 |
| 220 | 17370 | 17710 | 18050 | 18390 | 18740 | 19100 | 19450 | 19820 | 20190 | 20560 |
| 230 | 20950 | 21330 | 21720 | 22120 | 22520 | 22930 | 23350 | 23770 | 24190 | 24620 |
| 240 | 25060 | 25500 | 25950 | 26410 | 26870 | 27340 | 27810 | 28290 | 28780 | 29270 |
| 250 | 29770 | 30280 | 30790 | 31310 | 31830 | 32360 | 32900 | 33450 | 34000 | 34560 |
| 260 | 35130 | 35700 | 36280 | 36870 | 37470 | 38070 | 38680 | 39300 | 39920 | 40560 |
| 270 | 41200 | 41840 | 42500 | 43160 | 43840 | 44520 | 45200 | 45900 | 46600 | 47320 |
| 280 | 48040 | 48760 | 49500 | 50250 | 51000 | 51770 | 52540 | 53320 | 54110 | 54910 |
| 290 | 55710 | 56530 | 57360 | 58190 | 59040 | 59890 | 60750 | 61620 | 62510 | 63400 |
| 300 | 64300 | 65210 | 66130 | 67060 | 68000 | 68960 | 69920 | 70890 | 71870 | 72860 |
| 310 | 73870 | 74880 | 75910 | 76940 | 77990 | 79050 | 80120 | 81200 | 82290 | 83390 |
| 320 | 84500 | 85600 | 86700 | 87910 | 89070 | 90250 | 91430 | 92610 | 93840 | 95060 |
| 330 | 99290 | 97530 | 98790 | 100060 | 101350 | 102660 | 103980 | 105320 | 106680 | 108060 |
| 340 | 109300 | 110700 | 112100 | 113500 | 114900 | 116300 | 117800 | 119200 | 120700 | 122200 |
| 350 | 123700 | 125200 | 126800 | 128300 | 129900 | 131400 | 133000 | 134600 | 136300 | 137900 |
| 360 | 139600 | 141200 | 142900 | 144600 | 146300 | 148100 | 149800 | 151600 | 153400 | 155200 |
| 370 | 157000 | 158800 | 160700 | 162600 | 164400 | — | — | — | — | — |

TABLE 209.—Weight in Grams of a Cubic Meter of Saturated Aqueous Vapor

| Temp. °C | 0° | 1° | 2° | 3° | 4° | 5° | 6° | 7° | 8° | 9° |
|-------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| -20° | 0.804 | 0.816 | 0.743 | 0.677 | 0.615 | 0.550 | 0.508 | 0.461 | 0.418 | 0.378 |
| -10 | 2.158 | 1.983 | 1.820 | 1.671 | 1.531 | 1.403 | 1.284 | 1.174 | 1.073 | 0.980 |
| -0 | 4.847 | 4.482 | 4.144 | 3.828 | 3.534 | 3.261 | 3.006 | 2.770 | 2.551 | 2.347 |
| +0° | 4.847 | 5.192 | 5.559 | 5.947 | 6.366 | 6.797 | 7.261 | 7.751 | 8.271 | 8.821 |
| +10 | 9.401 | 10.015 | 10.604 | 11.348 | 12.070 | 12.832 | 13.635 | 14.482 | 15.373 | 16.311 |
| +20 | 17.300 | 18.338 | 19.430 | 20.578 | 21.783 | 23.049 | 24.378 | 25.771 | 27.234 | 28.765 |
| +30 | 30.371 | 32.052 | 33.812 | 35.656 | 37.583 | 39.599 | 41.706 | 43.908 | 46.208 | 48.600 |

For higher temperatures, see Table 290.

TABLE 210.—Weight in Grains of a Cubic Foot of Saturated Aqueous Vapor

| Temp. ° F. | 0° | 1° | 2° | 3° | 4° | 5° | 6° | 7° | 8° | 9° |
|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| - 20° | 0.167 | 0.158 | 0.150 | 0.141 | 0.134 | 0.126 | 0.119 | 0.112 | 0.106 | 0.100 |
| - 10 | 0.286 | 0.272 | 0.258 | 0.244 | 0.232 | 0.220 | 0.208 | 0.197 | 0.187 | 0.176 |
| - 0 | 0.479 | 0.453 | 0.433 | 0.411 | 0.391 | 0.371 | 0.353 | 0.335 | 0.318 | 0.302 |
| + 0° | 0.479 | 0.503 | 0.520 | 0.536 | 0.554 | 0.573 | 0.594 | 0.616 | 0.639 | 0.664 |
| + 10 | 0.780 | 0.818 | 0.858 | 0.900 | 0.943 | 0.988 | 1.035 | 1.084 | 1.135 | 1.180 |
| + 20 | 1.244 | 1.301 | 1.362 | 1.425 | 1.490 | 1.558 | 1.620 | 1.703 | 1.770 | 1.850 |
| + 30 | 1.942 | 2.028 | 2.118 | 2.200 | 2.286 | 2.375 | 2.466 | 2.560 | 2.658 | 2.750 |
| + 40 | 2.863 | 2.970 | 3.082 | 3.196 | 3.315 | 3.430 | 3.503 | 3.693 | 3.828 | 3.965 |
| + 50 | 4.108 | 4.255 | 4.407 | 4.564 | 4.725 | 4.891 | 5.062 | 5.238 | 5.420 | 5.607 |
| + 60 | 5.800 | 5.999 | 6.203 | 6.413 | 6.630 | 6.852 | 7.082 | 7.317 | 7.560 | 7.800 |
| + 70 | 8.066 | 8.320 | 8.600 | 8.879 | 9.165 | 9.460 | 9.761 | 10.072 | 10.392 | 10.720 |
| + 80 | 11.056 | 11.401 | 11.756 | 12.121 | 12.494 | 12.878 | 13.272 | 13.676 | 14.090 | 14.515 |
| + 90 | 14.951 | 15.401 | 15.858 | 16.328 | 16.810 | 17.305 | 17.812 | 18.330 | 18.863 | 19.407 |
| 100° | 10.966 | 20.538 | 21.123 | 21.723 | 22.337 | 22.966 | 23.611 | 24.271 | 24.946 | 25.636 |
| 110 | 26.343 | 27.066 | 27.807 | 28.563 | 29.338 | 30.130 | 30.940 | 31.768 | 32.616 | 33.482 |

Tables are abridged from Smithsonian Meteorological Tables, fourth revised edition.

TABLE 211.—Pressure of Aqueous Vapor in the Atmosphere

For various altitudes (barometric readings).

The first column gives the depression of the wet-bulb temperature t_1 below the air temperature t . The value corresponding to the barometric height at the altitude of observation is to be subtracted from the vapor pressure corresponding to the wet-bulb temperature taken from Table 208. The temperature corresponding to this vapor pressure taken from Table 208 is the dew point. The wet bulb should be ventilated about 3 meters per second. For sea-level use Table 212. Example: $t = 35^\circ$, $t_1 = 30^\circ$, barometer 74 cm. Then $31.83 - 2.46 = 29.37$ mm = aqueous vapor pressure; the dew point is 28.6° C.

Abridged from Smithsonian Meteorological Tables, 1907.

| $t - t_h$ °C | | Barometric pressure in centimeters. | | | | | | | | | | | | | |
|-----------------|------|-------------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| | | 74 | 72 | 70 | 68 | 66 | 64 | 62 | 60 | 58 | 56 | 54 | 52 | 50 | 48 |
| | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm |
| 1° | 0.50 | 0.48 | 0.47 | 0.46 | 0.44 | 0.43 | 0.42 | 0.40 | 0.39 | 0.38 | 0.36 | 0.35 | 0.34 | 0.32 | 0.31 |
| 2 | 0.08 | 0.06 | 0.03 | 0.00 | 0.88 | 0.85 | 0.82 | 0.80 | 0.77 | 0.75 | 0.72 | 0.69 | 0.67 | 0.64 | 0.62 |
| 3 | 1.47 | 1.43 | 1.39 | 1.35 | 1.32 | 1.28 | 1.24 | 1.20 | 1.15 | 1.12 | 1.08 | 1.04 | 1.00 | 0.96 | 0.90 |
| 4 | 1.97 | 1.91 | 1.86 | 1.81 | 1.75 | 1.70 | 1.65 | 1.60 | 1.54 | 1.49 | 1.44 | 1.38 | 1.33 | 1.28 | 1.26 |
| 5 | 2.46 | 2.39 | 2.32 | 2.26 | 2.19 | 2.13 | 2.06 | 1.99 | 1.93 | 1.86 | 1.80 | 1.73 | 1.66 | 1.60 | 1.56 |
| 6 | 2.95 | 2.87 | 2.79 | 2.71 | 2.63 | 2.55 | 2.47 | 2.39 | 2.32 | 2.24 | 2.16 | 2.08 | 2.00 | 1.92 | 1.84 |
| 7 | 3.45 | 3.36 | 3.26 | 3.17 | 3.08 | 2.99 | 2.89 | 2.80 | 2.71 | 2.61 | 2.52 | 2.43 | 2.33 | 2.24 | 2.14 |
| 8 | 3.95 | 3.84 | 3.73 | 3.63 | 3.53 | 3.42 | 3.31 | 3.20 | 3.10 | 2.99 | 2.88 | 2.78 | 2.67 | 2.56 | 2.46 |
| 9 | 4.44 | 4.32 | 4.21 | 4.09 | 3.97 | 3.85 | 3.73 | 3.61 | 3.49 | 3.37 | 3.25 | 3.13 | 3.00 | 2.88 | 2.76 |
| 10 | 4.94 | 4.81 | 4.68 | 4.54 | 4.41 | 4.28 | 4.14 | 4.01 | 3.88 | 3.74 | 3.61 | 3.48 | 3.34 | 3.21 | 3.08 |
| 11 | 5.44 | 5.30 | 5.15 | 5.00 | 4.86 | 4.71 | 4.56 | 4.42 | 4.27 | 4.12 | 3.97 | 3.83 | 3.68 | 3.53 | 3.38 |
| 12 | 5.94 | 5.78 | 5.62 | 5.46 | 5.30 | 5.14 | 4.98 | 4.82 | 4.66 | 4.50 | 4.34 | 4.18 | 4.02 | 3.85 | 3.69 |
| 13 | 6.45 | 6.27 | 6.10 | 5.92 | 5.75 | 5.57 | 5.40 | 5.23 | 5.05 | 4.88 | 4.70 | 4.53 | 4.36 | 4.18 | 4.01 |
| 14 | 6.95 | 6.76 | 6.58 | 6.39 | 6.20 | 6.01 | 5.83 | 5.64 | 5.45 | 5.26 | 5.07 | 4.88 | 4.70 | 4.51 | 4.32 |
| 15 | 7.46 | 7.26 | 7.06 | 6.85 | 6.65 | 6.45 | 6.25 | 6.05 | 5.85 | 5.64 | 5.44 | 5.24 | 5.04 | 4.84 | 4.64 |
| 16 | 7.96 | 7.75 | 7.54 | 7.32 | 7.11 | 6.89 | 6.68 | 6.46 | 6.24 | 6.03 | 5.81 | 5.60 | 5.38 | 5.17 | 4.95 |
| 17 | 8.47 | 8.24 | 8.02 | 7.79 | 7.56 | 7.33 | 7.10 | 6.87 | 6.64 | 6.41 | 6.18 | 5.95 | 5.72 | 5.50 | 5.27 |

PRESSURE OF AQUEOUS VAPOR IN THE ATMOSPHERE; SEA-LEVEL

This table gives the vapor pressure corresponding to various values of the difference $t - t_1$ between the readings of dry and wet bulb thermometers and the temperature t_1 of the wet bulb thermometer. The difference $t - t_1$ is given by two-degree steps in the top line, and t_1 by degrees in the first column. Temperatures in Centigrade degrees, vapor pressures in millimeters of mercury are used throughout the table. The table was calculated for barometric pressure B equal to 76 centimeters. A correction is given for each centimeter at the top of the columns. Ventilating velocity of wet thermometer about 3 meters per second.

| t_1 | $t - t_1$ = ° | 2° | 4° | 6° | 8° | 10° | 12° | 14° | 16° | 18° | 20° | Difference for 0.1° in $t - t_1$ |
|-------------------------------|------------------|-------|-------|-------|-------|---|-------|-------|-------|-------|-------|---|
| Corrections for B per cm | | .013 | .026 | .040 | .053 | .066 | .079 | .092 | .106 | .119 | .132 | |
| -10 | 1.96 | 0.97 | — | — | — | <p>Example.</p> <p>$t = 17.2; t_1 = 10.0; B = 74.5$ cm</p> <p>$t - t_1 = 7.2$</p> <p>From table: $6.17 - 12 \times 0.050 = 5.57$</p> <p>For $B, 1.5 \times .048 = .07$</p> <p>Hence $p = 5.64$</p> | | | | | | 0.050 |
| -9 | 2.14 | 1.15 | 0.16 | — | — | | | | | | | 0.050 |
| -8 | 2.34 | 1.35 | 0.35 | — | — | | | | | | | 0.050 |
| -7 | 2.55 | 1.56 | 0.66 | — | — | | | | | | | 0.050 |
| -6 | 2.78 | 1.78 | 0.79 | — | — | | | | | | | 0.050 |
| -5 | 3.02 | 2.03 | 1.03 | 0.03 | — | — | — | — | — | — | — | 0.050 |
| -4 | 3.29 | 2.29 | 1.29 | 0.29 | — | — | — | — | — | — | — | 0.050 |
| -3 | 3.58 | 2.58 | 1.58 | 0.58 | — | — | — | — | — | — | — | 0.050 |
| -2 | 3.89 | 2.89 | 1.89 | 0.88 | — | — | — | — | — | — | — | 0.050 |
| -1 | 4.22 | 3.22 | 2.22 | 1.21 | 0.21 | — | — | — | — | — | — | 0.050 |
| 0 | 4.58 | 3.58 | 2.57 | 1.57 | 0.57 | — | — | — | — | — | — | 0.050 |
| 1 | 4.92 | 3.92 | 2.92 | 1.91 | 0.91 | — | — | — | — | — | — | 0.050 |
| 2 | 5.29 | 4.29 | 3.28 | 2.27 | 1.27 | 0.26 | — | — | — | — | — | 0.050 |
| 3 | 5.68 | 4.68 | 3.67 | 2.66 | 1.66 | 0.65 | — | — | — | — | — | 0.050 |
| 4 | 6.10 | 5.09 | 4.08 | 3.07 | 2.07 | 1.06 | 0.05 | — | — | — | — | 0.050 |
| 5 | 6.54 | 5.53 | 4.52 | 3.51 | 2.51 | 1.50 | 0.49 | — | — | — | — | 0.050 |
| 6 | 7.01 | 6.00 | 4.99 | 3.98 | 2.97 | 1.96 | 0.95 | — | — | — | — | 0.050 |
| 7 | 7.51 | 6.50 | 5.49 | 4.48 | 3.47 | 2.46 | 1.45 | 0.43 | — | — | — | 0.050 |
| 8 | 8.04 | 7.03 | 6.02 | 5.01 | 4.00 | 2.98 | 1.97 | 0.96 | — | — | — | 0.050 |
| 9 | 8.61 | 7.60 | 6.58 | 5.57 | 4.56 | 3.54 | 2.53 | 1.52 | 0.50 | — | — | 0.050 |
| 10 | 9.21 | 8.20 | 7.18 | 6.17 | 5.15 | 4.14 | 3.12 | 2.11 | 1.09 | 0.07 | — | 0.050 |
| 11 | 9.85 | 8.83 | 7.81 | 6.80 | 5.78 | 4.77 | 3.75 | 2.73 | 1.72 | 0.70 | — | 0.051 |
| 12 | 10.52 | 9.50 | 8.49 | 7.47 | 6.45 | 5.44 | 4.42 | 3.40 | 2.38 | 1.37 | 0.35 | 0.051 |
| 13 | 11.24 | 10.22 | 9.20 | 8.18 | 7.16 | 6.14 | 5.13 | 4.11 | 3.09 | 2.07 | 1.05 | 0.051 |
| 14 | 11.99 | 10.97 | 9.95 | 8.93 | 7.91 | 6.90 | 5.88 | 4.86 | 3.84 | 2.82 | 1.80 | 0.051 |
| 15 | 12.79 | 11.77 | 10.75 | 9.73 | 8.71 | 7.69 | 6.67 | 5.65 | 4.63 | 3.61 | 2.59 | 0.051 |
| 16 | 13.64 | 12.62 | 11.60 | 10.58 | 9.56 | 8.53 | 7.51 | 6.49 | 5.47 | 4.45 | 3.43 | 0.051 |
| 17 | 14.54 | 13.52 | 12.49 | 11.47 | 10.45 | 9.42 | 8.40 | 7.38 | 6.36 | 5.33 | 4.31 | 0.051 |
| 18 | 15.49 | 14.46 | 13.44 | 12.42 | 11.39 | 10.37 | 9.34 | 8.32 | 7.30 | 6.27 | 5.25 | 0.051 |
| 19 | 16.49 | 15.46 | 14.44 | 13.41 | 12.39 | 11.36 | 10.34 | 9.31 | 8.29 | 7.26 | 6.24 | 0.051 |
| 20 | 17.55 | 16.52 | 15.50 | 14.47 | 13.44 | 12.42 | 11.39 | 10.36 | 9.34 | 8.31 | 7.29 | 0.051 |
| 21 | 18.66 | 17.64 | 16.61 | 15.58 | 14.56 | 13.53 | 12.50 | 11.47 | 10.45 | 9.42 | 8.39 | 0.051 |
| 22 | 19.84 | 18.82 | 17.79 | 16.76 | 15.73 | 14.70 | 13.67 | 12.64 | 11.62 | 10.59 | 9.57 | 0.051 |
| 23 | 21.09 | 20.06 | 19.03 | 18.00 | 16.97 | 15.94 | 14.91 | 13.88 | 12.85 | 11.82 | 10.79 | 0.051 |
| 24 | 22.40 | 21.37 | 20.34 | 19.31 | 18.27 | 17.24 | 16.21 | 15.18 | 14.15 | 13.12 | 12.09 | 0.051 |
| 25 | 23.78 | 22.75 | 21.71 | 20.68 | 19.65 | 18.62 | 17.59 | 16.56 | 15.52 | 14.49 | 13.46 | 0.052 |
| 26 | 25.24 | 24.20 | 23.17 | 22.14 | 21.10 | 20.07 | 19.04 | 18.00 | 16.97 | 15.94 | 14.90 | 0.052 |
| 27 | 26.77 | 25.73 | 24.70 | 23.66 | 22.63 | 21.60 | 20.56 | 19.53 | 18.49 | 17.45 | 16.42 | 0.052 |
| 28 | 28.38 | 27.34 | 26.31 | 25.27 | 24.24 | 23.20 | 22.17 | 21.13 | 20.10 | 19.06 | 18.02 | 0.052 |
| 29 | 30.08 | 29.04 | 28.00 | 26.97 | 25.93 | 24.89 | 23.86 | 22.82 | 21.78 | 20.75 | 19.71 | 0.052 |
| 30 | 31.86 | 30.82 | 29.78 | 28.75 | 27.71 | 26.67 | 25.63 | 24.60 | 23.56 | 22.52 | 21.48 | 0.052 |
| 31 | 33.74 | 32.70 | 31.66 | 30.62 | 29.58 | 28.54 | 27.50 | 26.46 | 25.42 | 24.38 | 23.34 | 0.052 |
| 32 | 35.70 | 34.66 | 33.62 | 32.58 | 31.54 | 30.50 | 29.46 | 28.42 | 27.38 | 26.34 | 25.30 | 0.052 |
| 33 | 37.78 | 36.73 | 35.69 | 34.65 | 33.61 | 32.57 | 31.53 | 30.49 | 29.45 | 28.41 | 27.36 | 0.052 |
| 34 | 39.95 | 38.90 | 37.86 | 36.82 | 35.78 | 34.73 | 33.69 | 32.65 | 31.61 | 30.57 | 29.52 | 0.052 |
| 35 | 42.23 | 41.18 | 40.14 | 39.10 | 38.05 | 37.01 | 35.97 | 34.92 | 33.88 | 32.83 | 31.79 | 0.052 |
| 36 | 44.62 | 43.57 | 42.53 | 41.48 | 40.44 | 39.40 | 38.35 | 37.31 | 36.26 | 35.22 | 34.17 | 0.052 |
| 37 | 47.13 | 46.08 | 45.04 | 43.99 | 42.94 | 41.90 | 40.85 | 39.81 | 38.77 | 37.72 | 36.67 | 0.052 |
| 38 | 49.76 | 48.71 | 47.66 | 46.61 | 45.57 | 44.52 | 43.47 | 42.43 | 41.38 | 40.33 | 39.29 | 0.052 |
| 39 | 52.51 | 51.46 | 50.41 | 49.37 | 48.32 | 47.27 | 46.22 | 45.17 | 44.12 | 43.08 | 42.03 | 0.052 |
| 40 | 55.40 | 54.35 | 53.30 | 52.25 | 51.20 | 50.15 | 49.10 | 48.05 | 47.00 | 45.95 | 44.90 | 0.052 |

RELATIVE HUMIDITY, VAPOR PRESSURE AND DRY TEMPERATURE

Vertical argument is the observed vapor pressure which may be computed from the wet and dry-bulb readings through Table 211 or 212. The horizontal argument is the observed air temperature (dry-bulb reading). Based upon Table 43, p. 142, Smithsonian Meteorological Tables, 3d Revised Edition, 1907.

| Vapor Pressure mm. | Air Temperatures, dry bulb, ° Centigrade. | | | | | | | | | | | | | | | | | | |
|--------------------------|---|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|------|------|------|------|------|------|--|--|
| | 0° | -1° | -2° | -3° | -4° | -5° | -6° | -7° | -8° | -9° | -10° | -11° | -12° | -13° | -14° | -15° | -20° | | |
| 0.25 | 6 | 6 | 6 | 7 | 8 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 17 | 18 | 20 | 32 | | |
| 0.50 | 11 | 12 | 13 | 14 | 15 | 17 | 18 | 20 | 21 | 23 | 25 | 28 | 30 | 34 | 37 | 40 | 64 | | |
| 0.75 | 17 | 18 | 19 | 21 | 23 | 25 | 27 | 30 | 32 | 35 | 38 | 42 | 46 | 50 | 55 | 60 | 96 | | |
| 1.00 | 22 | 24 | 26 | 28 | 30 | 33 | 36 | 40 | 42 | 47 | 51 | 56 | 61 | 67 | 74 | 80 | | | |
| 1.25 | 27 | 30 | 32 | 35 | 38 | 42 | 45 | 49 | 54 | 58 | 64 | 70 | 76 | 84 | 92 | 100 | | | |
| 1.50 | 33 | 36 | 39 | 42 | 46 | 50 | 54 | 59 | 64 | 70 | 76 | 84 | 92 | 100 | | | | | |
| 1.75 | 38 | 42 | 45 | 49 | 53 | 58 | 63 | 69 | 75 | 82 | 89 | 98 | | | | | | | |
| 2.00 | 44 | 48 | 52 | 56 | 61 | 66 | 72 | 79 | 86 | 93 | | | mm. | 0° | -1° | -2° | -3° | | |
| 2.25 | 49 | 53 | 58 | 63 | 69 | 75 | 81 | 89 | 96 | - | | | | | | | | | |
| 2.50 | 55 | 59 | 65 | 70 | 76 | 83 | 90 | 99 | - | - | | | 3.50 | 77 | 83 | 90 | 98 | | |
| 2.75 | 60 | 65 | 71 | 77 | 84 | 91 | 100 | - | - | - | | | 3.75 | 82 | 89 | 97 | - | | |
| 3.00 | 66 | 71 | 78 | 84 | 92 | 100 | - | - | - | - | | | 4.00 | 88 | 95 | - | - | | |
| 3.25 | 71 | 77 | 84 | 91 | 99 | - | - | - | - | - | | | 4.25 | 93 | 100 | - | - | | |
| 3.50 | 77 | 83 | 90 | 98 | - | - | - | - | - | - | | | 4.50 | 99 | - | - | - | | |

| Vapor Pressure. mm. | Air Temperatures, dry bulb, ° Centigrade. | | | | | | | | | | | | | | | | | | | | | |
|---------------------------|---|----|----|----|----|-----|-----|-----|-----|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|--|
| | 0° | 1° | 2° | 3° | 4° | 5° | 6° | 7° | 8° | 9° | 10° | 11° | 12° | 13° | 14° | 15° | 16° | 17° | 18° | 19° | 20° | |
| 0.5 | 11 | 10 | 9 | 9 | 8 | 8 | 7 | 7 | 6 | 6 | 5 | 5 | 5 | 4 | 4 | 4 | 4 | 3 | 3 | 3 | 3 | |
| 1.0 | 22 | 20 | 19 | 18 | 16 | 15 | 14 | 13 | 13 | 12 | 11 | 10 | 10 | 9 | 8 | 8 | 7 | 7 | 7 | 6 | 6 | |
| 1.5 | 33 | 31 | 28 | 27 | 25 | 23 | 22 | 20 | 19 | 18 | 16 | 15 | 14 | 13 | 13 | 12 | 11 | 10 | 10 | 9 | 9 | |
| 2.0 | 44 | 41 | 38 | 35 | 33 | 31 | 29 | 27 | 25 | 23 | 22 | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 12 | |
| 2.5 | 55 | 51 | 47 | 44 | 41 | 38 | 36 | 33 | 31 | 29 | 27 | 26 | 24 | 22 | 21 | 20 | 18 | 17 | 16 | 15 | 14 | |
| 3.0 | 66 | 61 | 57 | 53 | 49 | 46 | 43 | 40 | 38 | 35 | 33 | 31 | 29 | 27 | 25 | 24 | 22 | 21 | 20 | 18 | 17 | |
| 3.5 | 77 | 71 | 66 | 62 | 58 | 54 | 50 | 47 | 44 | 41 | 38 | 36 | 34 | 31 | 29 | 28 | 26 | 24 | 23 | 21 | 20 | |
| 4.0 | 88 | 81 | 76 | 71 | 66 | 61 | 57 | 54 | 50 | 47 | 44 | 41 | 38 | 36 | 34 | 32 | 30 | 28 | 26 | 25 | 23 | |
| 4.5 | 99 | 92 | 85 | 80 | 74 | 69 | 65 | 60 | 56 | 53 | 49 | 46 | 43 | 40 | 38 | 36 | 33 | 31 | 29 | 28 | 26 | |
| 5.0 | - | - | 95 | 88 | 83 | 77 | 72 | 67 | 63 | 58 | 55 | 51 | 48 | 45 | 42 | 39 | 37 | 35 | 33 | 31 | 29 | |
| 5.5 | - | - | - | 97 | 91 | 85 | 79 | 74 | 69 | 64 | 60 | 56 | 53 | 49 | 46 | 43 | 41 | 38 | 36 | 34 | 32 | |
| 6.0 | - | - | - | - | 99 | 92 | 86 | 80 | 75 | 70 | 66 | 61 | 58 | 54 | 51 | 47 | 44 | 42 | 39 | 37 | 34 | |
| 6.5 | - | - | - | - | - | 100 | 93 | 87 | 81 | 76 | 71 | 67 | 62 | 58 | 55 | 51 | 48 | 45 | 42 | 40 | 37 | |
| 7.0 | - | - | - | - | - | - | 100 | 94 | 85 | 82 | 77 | 72 | 67 | 63 | 59 | 55 | 52 | 49 | 46 | 43 | 40 | |
| 7.5 | - | - | - | - | - | - | - | 100 | 94 | 88 | 82 | 77 | 72 | 67 | 63 | 59 | 55 | 52 | 49 | 46 | 43 | |
| 8.0 | - | - | - | - | - | - | - | - | 100 | 94 | 88 | 82 | 77 | 72 | 67 | 63 | 59 | 56 | 52 | 49 | 46 | |
| 8.5 | - | - | - | - | - | - | - | - | - | 99 | 93 | 87 | 82 | 76 | 72 | 67 | 63 | 59 | 55 | 52 | 49 | |
| 9.0 | - | - | - | - | - | - | - | - | - | - | 98 | 92 | 86 | 81 | 76 | 71 | 67 | 62 | 59 | 55 | 52 | |
| 9.5 | - | - | - | - | - | - | - | - | - | - | - | 97 | 91 | 85 | 80 | 75 | 70 | 66 | 62 | 58 | 55 | |
| 10.0 | - | - | - | - | - | - | - | - | - | - | - | - | 96 | 90 | 84 | 79 | 74 | 69 | 65 | 61 | 57 | |
| 11.0 | - | - | - | - | - | - | - | - | - | - | - | - | - | 94 | 93 | 87 | 81 | 76 | 72 | 67 | 63 | |
| 12.0 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 94 | 89 | 83 | 78 | 74 | 69 | |
| 13.0 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 96 | 90 | 85 | 80 | 75 | |
| 14.0 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 97 | 91 | 86 | 80 | |
| 15.0 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 97 | 92 | 86 | |
| 16.0 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 98 | 92 | |
| 17.0 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 98 | |

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RELATIVE HUMIDITY, VAPOR PRESSURE AND DRY TEMPERATURE

| Vapor Pressure. mm. | Air Temperatures, dry bulb, ° Centigrade. | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---------------------------|---|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|--|--|--|--|--|--|--|
| | 20° | 21° | 22° | 23° | 24° | 25° | 26° | 27° | 28° | 29° | 30° | 31° | 32° | 33° | 34° | 35° | 36° | 37° | 38° | 39° | 40° | | | | | | | |
| 1 | 6 | 5 | 5 | 5 | 5 | 4 | 4 | 4 | 4 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 2 | 2 | 2 | 2 | 2 | | | | | | | |
| 2 | 12 | 11 | 10 | 10 | 9 | 8 | 8 | 8 | 7 | 7 | 6 | 6 | 6 | 5 | 5 | 5 | 5 | 4 | 4 | 4 | 4 | | | | | | | |
| 3 | 17 | 16 | 15 | 14 | 14 | 13 | 12 | 11 | 11 | 10 | 10 | 9 | 9 | 8 | 8 | 7 | 7 | 6 | 6 | 6 | 5 | | | | | | | |
| 4 | 23 | 22 | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 13 | 12 | 11 | 11 | 10 | 10 | 9 | 9 | 8 | 8 | 7 | | | | | | | |
| 5 | 29 | 27 | 25 | 24 | 23 | 21 | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 13 | 12 | 11 | 11 | 10 | 10 | 9 | | | | | | | |
| 6 | 34 | 32 | 31 | 29 | 27 | 26 | 24 | 23 | 21 | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 14 | 13 | 12 | 12 | 11 | | | | | | | |
| 7 | 40 | 38 | 36 | 34 | 32 | 30 | 28 | 26 | 25 | 24 | 22 | 21 | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 13 | | | | | | | |
| 8 | 46 | 43 | 41 | 38 | 36 | 34 | 32 | 30 | 29 | 27 | 25 | 24 | 23 | 21 | 20 | 19 | 18 | 17 | 16 | 15 | 15 | | | | | | | |
| 9 | 52 | 49 | 46 | 43 | 41 | 38 | 36 | 34 | 32 | 30 | 29 | 27 | 25 | 24 | 23 | 22 | 20 | 19 | 18 | 17 | 16 | | | | | | | |
| 10 | 57 | 54 | 51 | 48 | 45 | 43 | 40 | 38 | 36 | 34 | 32 | 30 | 28 | 27 | 25 | 24 | 23 | 21 | 20 | 19 | 18 | | | | | | | |
| 11 | 63 | 60 | 56 | 53 | 50 | 47 | 44 | 42 | 39 | 37 | 35 | 33 | 31 | 29 | 28 | 26 | 25 | 24 | 22 | 21 | 20 | | | | | | | |
| 12 | 69 | 65 | 61 | 58 | 54 | 51 | 48 | 45 | 43 | 40 | 38 | 36 | 34 | 32 | 30 | 29 | 27 | 26 | 24 | 23 | 22 | | | | | | | |
| 13 | 75 | 70 | 66 | 62 | 59 | 55 | 52 | 49 | 46 | 44 | 41 | 39 | 37 | 35 | 33 | 31 | 29 | 28 | 26 | 25 | 24 | | | | | | | |
| 14 | 80 | 76 | 71 | 67 | 63 | 60 | 56 | 53 | 50 | 47 | 44 | 42 | 40 | 37 | 35 | 33 | 32 | 30 | 28 | 27 | 26 | | | | | | | |
| 15 | 86 | 81 | 76 | 72 | 68 | 64 | 60 | 57 | 53 | 50 | 48 | 45 | 42 | 40 | 38 | 36 | 34 | 32 | 30 | 29 | 27 | | | | | | | |
| 16 | 92 | 87 | 82 | 77 | 72 | 68 | 64 | 60 | 57 | 54 | 51 | 48 | 45 | 43 | 41 | 38 | 36 | 34 | 32 | 31 | 29 | | | | | | | |
| 17 | 98 | 92 | 87 | 81 | 77 | 72 | 68 | 64 | 61 | 57 | 54 | 51 | 48 | 45 | 43 | 41 | 38 | 36 | 34 | 33 | 31 | | | | | | | |
| 18 | - | 97 | 92 | 86 | 81 | 77 | 72 | 68 | 64 | 60 | 57 | 54 | 51 | 48 | 46 | 43 | 41 | 39 | 37 | 35 | 33 | | | | | | | |
| 19 | - | - | 97 | 91 | 86 | 81 | 76 | 72 | 68 | 64 | 60 | 57 | 54 | 51 | 48 | 45 | 43 | 41 | 39 | 36 | 35 | | | | | | | |
| 20 | - | - | - | 96 | 90 | 85 | 80 | 76 | 71 | 67 | 63 | 60 | 57 | 53 | 51 | 48 | 45 | 43 | 41 | 38 | 36 | | | | | | | |
| 21 | - | - | - | - | 95 | 89 | 84 | 79 | 75 | 71 | 67 | 63 | 59 | 56 | 53 | 50 | 48 | 45 | 43 | 40 | 38 | | | | | | | |
| 22 | - | - | - | - | 100 | 94 | 88 | 83 | 78 | 74 | 70 | 66 | 62 | 59 | 56 | 53 | 50 | 47 | 45 | 42 | 40 | | | | | | | |
| 23 | - | - | - | - | - | 98 | 92 | 87 | 82 | 77 | 73 | 69 | 65 | 62 | 58 | 55 | 52 | 49 | 47 | 44 | 42 | | | | | | | |
| 24 | - | - | - | - | - | - | 96 | 91 | 85 | 81 | 76 | 72 | 68 | 64 | 61 | 57 | 54 | 51 | 49 | 46 | 44 | | | | | | | |
| 25 | - | - | - | - | - | 100 | 94 | 89 | 84 | 79 | 75 | 71 | 67 | 63 | 60 | 56 | 54 | 51 | 48 | 46 | 44 | | | | | | | |
| 26 | - | - | - | - | - | - | 98 | 93 | 87 | 83 | 78 | 74 | 70 | 66 | 62 | 59 | 56 | 53 | 50 | 47 | 45 | | | | | | | |
| 27 | - | - | - | - | - | - | - | 96 | 91 | 86 | 81 | 76 | 72 | 68 | 65 | 61 | 58 | 55 | 52 | 49 | 47 | | | | | | | |
| 28 | - | - | - | - | - | - | - | 100 | 94 | 89 | 84 | 79 | 75 | 71 | 67 | 63 | 60 | 57 | 54 | 51 | 49 | | | | | | | |
| 29 | - | - | - | - | - | - | - | - | 97 | 92 | 87 | 82 | 78 | 73 | 69 | 65 | 62 | 59 | 56 | 53 | 51 | | | | | | | |
| 30 | - | - | - | - | - | - | - | - | - | 95 | 90 | 85 | 80 | 76 | 72 | 68 | 64 | 61 | 58 | 55 | 53 | | | | | | | |
| 31 | - | - | - | - | - | - | - | - | - | 98 | 93 | 88 | 83 | 78 | 74 | 70 | 66 | 63 | 60 | 56 | 54 | | | | | | | |
| 32 | - | - | - | - | - | - | - | - | - | - | 96 | 91 | 86 | 81 | 77 | 72 | 69 | 65 | 62 | 58 | 56 | | | | | | | |
| 33 | - | - | - | - | - | - | - | - | - | - | 99 | 93 | 88 | 84 | 79 | 75 | 71 | 67 | 63 | 60 | 57 | | | | | | | |
| 34 | - | - | - | - | - | - | - | - | - | - | - | 96 | 91 | 86 | 81 | 77 | 73 | 69 | 65 | 62 | 59 | | | | | | | |
| 35 | - | - | - | - | - | - | - | - | - | - | - | 99 | 94 | 89 | 84 | 79 | 75 | 71 | 67 | 64 | 61 | | | | | | | |
| 36 | - | - | - | - | - | - | - | - | - | - | - | - | 96 | 91 | 86 | 81 | 77 | 73 | 69 | 66 | 63 | | | | | | | |
| 37 | - | - | - | - | - | - | - | - | - | - | - | - | - | 99 | 94 | 89 | 84 | 79 | 75 | 71 | 67 | | | | | | | |
| 38 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 96 | 91 | 86 | 81 | 77 | 73 | 69 | | | | | | | |
| 39 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 99 | 93 | 88 | 83 | 79 | 75 | 71 | | | | | | | |
| 40 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 96 | 90 | 86 | 81 | 77 | 73 | | | | | | | |
| 41 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 98 | 93 | 88 | 83 | 79 | 75 | | | | | | | |
| 42 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 100 | 95 | 90 | 85 | 81 | 77 | | | | | | | |
| 43 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 97 | 92 | 87 | 83 | 78 | | | | | | | |
| 44 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 99 | 94 | 89 | 84 | 80 | | | | | | | |
| 45 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 96 | 91 | 86 | 82 | | | | | | | |
| 46 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 99 | 93 | 88 | 84 | | | | | | | |
| 47 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 95 | 90 | 86 | | | | | | | |
| 48 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 97 | 92 | 87 | | | | | | | |
| 49 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 99 | 94 | 89 | | | | | | | |
| 50 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 96 | 91 | | | | | | | |
| 51 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 98 | 93 | | | | | | | |
| 52 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 100 | 95 | | | | | | | |
| 53 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 97 | | | | | | | |
| 54 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 98 | | | | | | | |
| 55 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 100 | | | | | | | |

TABLE 213 (concluded) —Relative Humidity, Vapor Pressure and Dry Temperature

(Data from 20° to 60° C based upon Table 208.)

| Vapor Pressure. mm. | Air Temperatures, dry bulb, ° Centigrade. | | | | | | | | | | | | | | | | | | | | | | | |
|---------------------------|---|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|--|--|--|
| | 40° | 41° | 42° | 43° | 44° | 45° | 46° | 47° | 48° | 49° | 50° | 51° | 52° | 53° | 54° | 55° | 56° | 57° | 58° | 59° | 60° | | | |
| 5 | 9 | 9 | 8 | 8 | 7 | 7 | 7 | 6 | 6 | 6 | 5 | 5 | 5 | 5 | 4 | 4 | 4 | 4 | 4 | 4 | 3 | | | |
| 10 | 18 | 17 | 16 | 15 | 15 | 14 | 13 | 13 | 12 | 11 | 11 | 10 | 10 | 9 | 9 | 8 | 8 | 8 | 7 | 7 | 7 | | | |
| 15 | 27 | 26 | 24 | 23 | 22 | 21 | 20 | 19 | 18 | 17 | 16 | 15 | 15 | 14 | 13 | 13 | 12 | 12 | 11 | 10 | 10 | | | |
| 20 | 36 | 34 | 33 | 31 | 29 | 28 | 26 | 25 | 24 | 23 | 22 | 21 | 20 | 19 | 18 | 17 | 16 | 15 | 15 | 14 | 13 | | | |
| 25 | 45 | 43 | 41 | 39 | 37 | 35 | 33 | 31 | 30 | 28 | 27 | 26 | 24 | 23 | 22 | 21 | 20 | 19 | 18 | 18 | 17 | | | |
| 30 | 54 | 51 | 49 | 46 | 44 | 42 | 40 | 38 | 36 | 34 | 32 | 31 | 29 | 28 | 27 | 25 | 24 | 23 | 22 | 21 | 20 | | | |
| 35 | 63 | 60 | 57 | 54 | 51 | 49 | 46 | 44 | 42 | 40 | 38 | 36 | 34 | 33 | 31 | 30 | 28 | 27 | 26 | 25 | 23 | | | |
| 40 | 72 | 68 | 65 | 62 | 59 | 56 | 53 | 50 | 48 | 45 | 43 | 41 | 39 | 37 | 36 | 34 | 32 | 31 | 29 | 28 | 27 | | | |
| 45 | 81 | 77 | 73 | 69 | 66 | 63 | 59 | 57 | 54 | 51 | 49 | 46 | 44 | 42 | 40 | 38 | 36 | 35 | 33 | 32 | 30 | | | |
| 50 | 90 | 86 | 81 | 77 | 73 | 70 | 66 | 63 | 60 | 57 | 54 | 51 | 49 | 47 | 44 | 42 | 40 | 38 | 37 | 35 | 33 | | | |
| 55 | 99 | 94 | 89 | 85 | 81 | 76 | 73 | 69 | 66 | 62 | 59 | 57 | 54 | 51 | 49 | 46 | 44 | 42 | 40 | 39 | 37 | | | |
| 60 | - | - | 98 | 93 | 88 | 83 | 79 | 75 | 72 | 68 | 65 | 62 | 60 | 56 | 53 | 51 | 48 | 46 | 44 | 42 | 40 | | | |
| 65 | - | - | - | 100 | 95 | 90 | 86 | 82 | 78 | 74 | 70 | 67 | 64 | 61 | 58 | 55 | 52 | 50 | 48 | 46 | 43 | | | |
| 70 | - | - | - | - | - | 97 | 92 | 88 | 84 | 80 | 76 | 72 | 68 | 65 | 62 | 59 | 56 | 54 | 51 | 49 | 47 | | | |
| 75 | - | - | - | - | - | - | 99 | 94 | 90 | 85 | 81 | 77 | 74 | 70 | 67 | 64 | 60 | 58 | 55 | 53 | 50 | | | |
| 80 | - | - | - | - | - | - | - | 100 | 96 | 91 | 86 | 82 | 78 | 75 | 71 | 68 | 64 | 62 | 59 | 56 | 54 | | | |
| 85 | - | - | - | - | - | - | - | - | - | 97 | 92 | 87 | 84 | 79 | 75 | 72 | 69 | 65 | 62 | 60 | 57 | | | |
| 90 | - | - | - | - | - | - | - | - | - | - | 97 | 93 | 88 | 84 | 80 | 76 | 73 | 69 | 66 | 63 | 60 | | | |
| 95 | - | - | mm. | 57 | 58 | 59 | 60 | - | - | - | - | - | 98 | 94 | 89 | 84 | 80 | 77 | 73 | 70 | 67 | | | |
| 100 | - | - | 125 | 96 | 92 | 88 | 84 | - | - | - | - | - | - | 98 | 93 | 89 | 85 | 81 | 77 | 73 | 70 | | | |
| 105 | - | - | 130 | 100 | 95 | 91 | 87 | - | - | - | - | - | - | - | 98 | 93 | 89 | 85 | 81 | 77 | 74 | | | |
| 110 | - | - | 135 | - | 99 | 95 | 90 | - | - | - | - | - | - | - | - | 98 | 93 | 89 | 85 | 81 | 77 | | | |
| 115 | - | - | 140 | - | - | 98 | 94 | - | - | - | - | - | - | - | - | - | 97 | 93 | 88 | 84 | 81 | | | |
| 120 | - | - | 145 | - | - | - | 97 | - | - | - | - | - | - | - | - | - | - | 97 | 92 | 88 | 84 | | | |
| 125 | - | - | 150 | - | - | - | 100 | - | - | - | - | - | - | - | - | - | - | - | 96 | 92 | 88 | | | |

TABLE 214.—Relative Humidity, Wet and Dry Thermometers

This table gives the relative humidity direct from the difference between the reading of the dry (t° C) and the wet (t_1° C) thermometer. It is computed for a barometer reading of 76 cm. The wet thermometer should be ventilated about 3 meters per second. From manuscript tables computed at the U.S. Weather Bureau.

| t° | Depression of wet-bulb thermometer, t°-t ₁ °. | | | | | | | | | | | | | | | | | |
|-----|--|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|--|
| | 0.2° | 0.4° | 0.6° | 0.8° | 1.0° | 1.2° | 1.4° | 1.6° | 1.8° | 2.0° | 2.5° | 3.0° | 3.5° | 4.0° | 4.5° | 5.0° | 5.5° | |
| -15 | 90 | 91 | 72 | 62 | 53 | 44 | 35 | 25 | 16 | 7 | - | - | - | - | - | - | - | |
| -12 | 92 | 85 | 77 | 69 | 62 | 54 | 47 | 39 | 32 | 25 | 7 | - | - | - | - | - | - | |
| -9 | 94 | 88 | 81 | 75 | 70 | 62 | 56 | 50 | 44 | 39 | 23 | 9 | - | - | - | - | - | |
| -6 | 95 | 89 | 85 | 80 | 74 | 69 | 64 | 59 | 54 | 49 | 36 | 25 | 13 | 2 | - | - | - | |
| -3 | 96 | 91 | 87 | 82 | 78 | 74 | 69 | 66 | 61 | 57 | 46 | 36 | 26 | 17 | 7 | - | - | |
| 0 | 96 | 92 | 89 | 85 | 81 | 78 | 74 | 71 | 67 | 64 | 55 | 46 | 38 | 29 | 21 | 13 | 6 | |
| +3 | 97 | 94 | 91 | 87 | 84 | 81 | 78 | 75 | 72 | 69 | 62 | 54 | 46 | 40 | 32 | 25 | 18 | |
| | | | | | | | | | | | | | | | | | | |
| | 0.6° | 1.0° | 1.5° | 2.0° | 2.5° | 3.0° | 3.5° | 4.0° | 4.5° | 5.0° | 6.0° | 7.0° | 8.0° | 9.0° | 10.° | 11.° | 12.° | |
| +3 | 92 | 84 | 76 | 69 | 62 | 54 | 46 | 40 | 32 | 25 | 12 | - | - | - | - | - | - | |
| +6 | 94 | 87 | 80 | 73 | 66 | 60 | 54 | 47 | 41 | 35 | 23 | 11 | - | - | - | - | - | |
| +9 | 94 | 88 | 82 | 76 | 70 | 65 | 59 | 53 | 48 | 42 | 32 | 22 | 12 | 3 | - | - | - | |
| +12 | 94 | 89 | 84 | 78 | 73 | 68 | 63 | 58 | 53 | 48 | 38 | 30 | 21 | 12 | 4 | - | - | |
| +15 | 95 | 90 | 85 | 80 | 76 | 71 | 66 | 62 | 58 | 53 | 44 | 36 | 28 | 20 | 13 | 4 | - | |
| +18 | 95 | 90 | 86 | 82 | 78 | 73 | 69 | 65 | 61 | 57 | 49 | 42 | 35 | 27 | 20 | 13 | 6 | |
| +21 | 96 | 91 | 87 | 83 | 79 | 75 | 71 | 67 | 64 | 60 | 53 | 46 | 39 | 32 | 26 | 19 | 13 | |
| +24 | 96 | 92 | 88 | 85 | 81 | 77 | 74 | 70 | 66 | 63 | 56 | 49 | 43 | 37 | 31 | 26 | 21 | |
| +27 | 96 | 93 | 90 | 86 | 82 | 79 | 76 | 72 | 68 | 65 | 59 | 53 | 47 | 41 | 36 | 31 | 26 | |
| +30 | 96 | 93 | 90 | 86 | 82 | 79 | 76 | 73 | 70 | 67 | 61 | 55 | 50 | 44 | 39 | 35 | 30 | |
| +33 | 96 | 93 | 90 | 86 | 83 | 80 | 77 | 74 | 71 | 68 | 63 | 57 | 52 | 47 | 42 | 37 | 33 | |
| +36 | 97 | 93 | 90 | 87 | 84 | 81 | 78 | 75 | 72 | 70 | 64 | 57 | 54 | 50 | 45 | 41 | 36 | |
| +39 | 97 | 94 | 91 | 88 | 85 | 82 | 79 | 76 | 74 | 71 | 66 | 61 | 56 | 52 | 47 | 43 | 39 | |

THE INTERNATIONAL TEMPERATURE SCALE

(Adapted from G. K. Burgess, Bur. Standards Journ. Res., 1, 635, 1928.)

The Thermodynamic Centigrade Scale, on which the temperature of melting ice, and the temperature of condensing water vapor, both under the pressure of one standard atmosphere, are numbered 0° and 100° , respectively, is recognized as the fundamental scale to which all temperature measurements should ultimately be referable.

The experimental difficulties incident to the practical realization of the thermodynamic scale have made it expedient to adopt for international use a practical scale designated as the International Temperature Scale. This scale conforms with the thermodynamic scale as closely as is possible with present knowledge, and is designed to be definite, conveniently and accurately reproducible, and to provide means for uniquely determining any temperature within the range of the scale, thus promoting uniformity in numerical statements of temperature.

Temperatures on the international scale will ordinarily be designated as " $^{\circ}\text{C}$," but may be designated as " $^{\circ}\text{C}$ (Int.)" if it is desired to emphasize the fact that this scale is being used.

The International Temperature Scale is based upon a number of fixed and reproducible equilibrium temperatures to which numerical values are assigned, and upon the indications of interpolation instruments calibrated according to a specified procedure at the fixed temperatures.

The basic fixed points and the numerical values assigned to them for the pressure of one standard atmosphere are given in the following table, together with formulas which represent the temperature (t_p) as a function of vapor pressure (p) over the range 680 to 780 mm of mercury.

Basic Fixed Points of the International Temperature Scale

| | °C |
|---|---------|
| (a) Temperature of equilibrium between liquid and gaseous oxygen at the pressure of one standard atmosphere (oxygen point). | -182.97 |
| $t_p = t_{760} + 0.0126(p - 760) - 0.0000065(p - 760)^2$ | |
| (b) Temperature of equilibrium between ice and air-saturated water at normal atmospheric pressure (ice point)..... | 0.000 |
| (c) Temperature of equilibrium between liquid water and its vapor at the pressure of one standard atmosphere (steam point).. <td>100.000</td> | 100.000 |
| $t_p = t_{760} + 0.0367(p - 760) - 0.000023(p - 760)^2$ | |
| (d) Temperature of equilibrium between liquid sulphur and its vapor at the pressure of one standard atmosphere (sulphur point) | 444.60 |
| $t_p = t_{760} + 0.0909(p - 760) - 0.000048(p - 760)^2$ | |
| (e) Temperature of equilibrium between solid silver and liquid silver at normal atmospheric pressure (silver point)..... | 960.5 |
| (f) Temperature of equilibrium between solid gold and liquid gold at normal atmospheric pressure (gold point)..... | 1,063 |

THE INTERNATIONAL TEMPERATURE SCALE

Standard atmospheric pressure is defined as the pressure due to a column of mercury 760 mm high, having a mass of 13.5951 g/cm³, subject to a gravitational acceleration of 980.665 cm/sec.² and is equal to 1,013,250 dynes/cm².

It is an essential feature of a practical scale of temperature that definite numerical values shall be assigned to such fixed points as are chosen. It should be noted, however, that the last decimal place given for each of the values in the table is significant only as regards the degree of reproducibility of that fixed point on the International Temperature Scale. It is not to be understood that the values are necessarily known on the Thermodynamic Centigrade Scale to the corresponding degree of accuracy.

The means available for interpolation lead to a division of the scale into four parts.

(a) From the ice point to 660° C the temperature t is deduced from the resistance R_t of a standard platinum resistance thermometer by means of the formula

$$R_t = R_0(1 + A_t + Bt^2)$$

The constants R_0 , A , and B of this formula are to be determined by calibration at the ice, steam, and sulphur points, respectively.

The purity and physical condition of the platinum of which the thermometer is made should be such that the ratio R_t/R_0 shall not be less than 1.390 for $t=100^\circ$ and 2.645 for $t=444.6^\circ$.

(b) From -190° to the ice point, the temperature t is deduced from the resistance R_t of a standard platinum resistance thermometer by means of the formula

$$R_t = R_0[1 + At + Bt^2 + C(t-100)t^3]$$

The constants R_0 , A , and B are to be determined as specified above, and the additional constant C is determined by calibration at the oxygen point.

The standard thermometer for use below 0° C must, in addition, have a ratio R_t/R_0 less than 0.250 for $t=-183^\circ$.

(c) From 660° C to the gold point, the temperature t is deduced from the electromotive force e of a standard platinum *v.* platinum-rhodium thermocouple, one junction of which is kept at a constant temperature of 0° C while the other is at the temperature t defined by the formula

$$e = a + bt + ct^2$$

The constants a , b , and c are to be determined by calibration at the freezing point of antimony, and at the silver and gold points.

(d) Above the gold point the temperature t is determined by means of the ratio of the intensity J_2 of monochromatic visible radiation of wave length λ cm, emitted by a black body at the temperature t_2 , to the intensity J_1 of radiation of the same wave length emitted by a black body at the gold point, by means of the formula

$$\log_e \frac{J_2}{J_1} = \frac{c_2}{\lambda} \left[\frac{1}{1,336} - \frac{1}{(t+273)} \right]$$

The constant c_2 is taken as 1.432 cm degrees. The equation is valid if $\lambda(t+273)$ is less than 0.3 cm degrees.

THE INTERNATIONAL TEMPERATURE SCALE

Recommended Procedure for Calibration

1. OXYGEN

The temperature of equilibrium of liquid and gaseous oxygen has been best realized experimentally by the static method, the oxygen vapor-pressure thermometer being compared with the thermometer to be standardized in a suitable low temperature bath.

2. ICE

The temperature of melting ice is realized experimentally as the temperature at which pure, finely divided ice is in equilibrium with pure, air-saturated water under standard atmospheric pressure. The effect of increased pressure is to lower the freezing point to the extent of 0.007°C per atmosphere.

3. STEAM

The temperature of condensing water vapor is realized experimentally by the use of a hypsometer so constructed as to avoid superheat of the vapor around the thermometer, or contamination with air or other impurities. If the desired conditions have been attained, the observed temperature should be independent of the rate of heat supply to the boiler, except as this may affect the pressure within the hypsometer, and of the length of time the hypsometer has been in operation.

4. SULPHUR

For the purpose of standardizing resistance thermometers, the temperature of condensing sulphur vapor is realized by adherence to the following specifications relating to boiling apparatus, purity of sulphur, radiation shield, and procedure.

The boiling-tube is of glass, fused silica, or similar material, and has an internal diameter of not less than 4 nor more than 6 cm. The vapor column must be sufficiently long that the bottom of the radiation shield is not less than 6 cm above the free liquid surface and its top is not less than 2 cm below the top of the heat insulating material surrounding the tube. Electric heating is preferable, although gas may be used, but the source of heat and all good conducting material in contact with it must terminate at least 4 cm below the free surface of the liquid sulphur. Above the source of heat the tube is surrounded with insulating material. Any device used to close the end of the tube must allow a free opening for equalization of pressure.

The sulphur should contain not over 0.02 per cent of impurities. Selenium is the impurity most likely to be present in quantities sufficient to affect the temperature of the boiling point.

The radiation shield is cylindrical and open at the lower end, and is provided with a conical portion at the top, to fit closely to the protecting tube of the thermometer. The cylindrical part is 1.5 to 2.5 cm larger in diameter than the protecting tube of the thermometer and at least 1 cm smaller in diameter than the inside of the boiling tube. The cylinder should extend at least 1.5 cm

THE INTERNATIONAL TEMPERATURE SCALE

TABLE 216 (*continued*).—Recommended Procedure for Calibration

beyond each end of the thermometer coil. There should be ample opening at the top of the cylindrical and below the conical portion to permit free circulation of vapor. The inner surface of the shield should be a poor reflector. The shield may be made of sheet metal, graphite, etc.

In standardizing a thermometer the sulphur is heated to boiling and the heating so regulated that the condensation line is at least 1 cm above the top of the insulating material. The thermometer with its radiation shield is inserted in the vapor, and when the line of condensation again reaches its former level simultaneous observations of resistance and barometric pressure are made. In all cases care should be taken to prove that the temperature is independent of vertical displacements of the thermometer and shield.

5. SILVER AND GOLD

For standardizing a thermocouple, the metal to be used at its freezing point is contained in a crucible of pure graphite, refractory porcelain, or other material which will not react with the metal so as to contaminate it to an appreciable extent.

Silver must be protected from access of oxygen while heated.

The crucible and metal are placed in an electric furnace capable of heating the contents to a uniform temperature.

The metal is melted and brought to a uniform temperature a few degrees above its melting point, then allowed to cool slowly with the thermocouple immersed in it as described in the next paragraph.

The thermocouple, mounted in a porcelain tube with porcelain insulators separating the two wires, is immersed in the molten metal through a hole in the center of the crucible cover. The depth of immersion should be such that during the period of freezing the thermocouple can be lowered or raised at least 1 cm from its normal position without altering the indicated e.m.f. by as much as 1 microvolt. During freezing, the e.m.f. should remain constant within 1 microvolt for a period of at least five minutes.

As an alternative to displacing the couple, as a means of testing the absence of the influence of external conditions upon the observed temperature, both freezing and melting points may be observed and if these do not differ by more than 2 microvolts, the observed freezing point may be considered satisfactory.

TABLE 217.—The Standard Platinum Resistance Thermometer

The diameter of the wire should not be smaller than 0.05 or larger than 0.2 mm.

The platinum wire of the thermometer must be so mounted as to be subject to the minimum of mechanical constraint, so that dimensional changes accompanying changes of temperature may result in a minimum of mechanical strain being imposed upon the platinum.

The design of the thermometer should be such that the portion, the resistance of which is measured, shall consist only of platinum, and shall be at the uniform temperature which is to be measured. This may be accomplished by either of the accepted systems of current and potential, or compensating leads.

After completion, the thermometer should be annealed at a temperature of at least 660°.

THE INTERNATIONAL TEMPERATURE SCALE

TABLE 218.—The Standard Thermocouple

The platinum of the standard couple shall be of such purity that the ratio R_t/R_0 is initially not less than 1.390 for $t = 100^\circ$. The alloy is to consist of 90 per cent platinum with 10 per cent rhodium. The completed thermocouple must develop an electromotive force, when one junction is at 0° and the other at the freezing point of gold, not less than 10,200 nor more than 10,400 international microvolts. The diameter of the wires used for standard thermocouples should lie between the values 0.35 and 0.65 mm.

The freezing point of antimony, specified for the standardization of the thermocouple, lies within the range of 0° to 660° where the international scale is fixed by the indications of the standard resistance thermometer, and the numerical value of this temperature is therefore to be determined with the resistance thermometer. In the appendix the result of such determinations is given as 630.5° , but the temperature of any particular lot of antimony which is to be used for standardizing the thermocouple is to be determined with a standard resistance thermometer.

The procedure to be followed in using the freezing point of antimony as a fixed temperature is substantially the same as that specified for silver. Antimony has a marked tendency to undercool before freezing. The undercooling will not be excessive if the metal is heated only a few degrees above its melting point and if the liquid metal is stirred. During freezing the temperature should remain constant within 0.1° for a period of at least five minutes.

TABLE 219.—Secondary Calibration Points

These points and their temperatures on the international scale are listed below. The temperatures correspond to a pressure of one standard atmosphere. The formulas for variation of vapor pressure with temperature are for the range from 680 to 780 mm.

| | $^\circ\text{C}$ |
|--|------------------|
| Boiling hydrogen $t_p = t_{700} + 0.0044 (p - 760)$ | -252.75 |
| Equilibrium between solid and gaseous carbon dioxide $t_p = t_{700} + 0.1443$ ($t_p + 273.2$) $\log_{10} (p/760)$ | -78.5 |
| Freezing mercury | -38.87 |
| Transition of sodium sulphate..... | 32.38 |
| Condensing naphthalene vapor $t_p = t_{700} + 0.208 (t_p + 273.2) \log_{10} (p/760)$ | 217.96 |
| Freezing tin | 231.85 |
| Condensing benzophenone vapor $t_p = t_{700} + 0.194 (t_p + 273.2) \log_{10} (p/760)$ | 305.9 |
| Freezing cadmium | 320.9 |
| Freezing lead | 327.3 |
| Freezing zinc | 419.45 |
| Freezing antimony | 630.5 |
| Freezing copper in a reducing atmosphere..... | $1,083$ |
| Freezing palladium | $1,553$ |
| Melting tungsten | $3,400$ |
| Isopentane | -159.6 f* |
| Carbon dioxide | -111.6 f |
| Toluene | -95.1 f |
| Ethyl acetate | -83.6 f |
| Chloroform | -63.5 f |
| Carbon tetrachloride | -22.9 f |
| Li_2SO_4 | $1202.$ m † |
| Nickel | $1455.$ m, f |
| Cobalt | $1490.$ m, f |
| $\text{CaAl}_2\text{Si}_2\text{O}_8$ | $1555.$ m |
| Platinum | $1755.$ m |

* f, freezing. † m, melting.

DIRECTIONS FOR USE OF STANDARD THERMOELEMENT CALIBRATIONS

Deviation curves.—Standard tables such as are given on pages 245-247 have no absolute significance; they are reference curves that, while representing fairly well the e.m.f. functions for certain couples, are intended for use with an appropriate deviation curve. The correction curve is determined for each element by calibration at several fixed points—preferably three or more—given in the tables. It is constructed by plotting ΔE as ordinate ($\Delta E = E$ observed minus E standard) against E_{obs} . In order to obtain the temperatures corresponding to the measured e.m.f., the appropriate value of ΔE (obtained from its deviation curve by inspection) is subtracted algebraically from the observed value of E before the latter is converted into degrees by means of the table. The required accuracy may be secured by plotting the deviation curve on a small scale; coordinate paper 20 by 20 cm is ample. There need be no fear of error with this method even with deviations of several hundred μv , especially if sufficient calibration points are taken.

Fixed-junction correction.—Thermocouples have two junctions. The “business end” is usually called the hot junction, and the other, the cold junction.

The calibration tables are made on the assumption that the fixed junction is maintained at 0°C . The standard method is to use a vacuum-jacketed flask filled with ice into which is inserted the junction protected by a glass tube closed at one end and partly filled with kerosene. If it is not feasible to have the fixed junction at 0° , a fixed-junction correction must be applied. This correction, in general, is not equal to the temperature of the fixed junction and depends on both the temperature T_0 of the fixed junction and the temperature T of the variable junction. It may be applied by either of the following two methods.

(1) The e.m.f. corresponding to T_0 may be added directly to the e.m.f. E_{T-T_0} and the resultant e.m.f. E_T , converted into degrees by means of the proper table (Tables 221-225). Thus if a platinum-platinrhodium couple gives a reading of $6000\mu\text{v}$ (microvolts), T_0 being 50° , the value of E_{T_0} , according to Table 221, is $298\mu\text{v}$ which added to 6000 gives 6298 as the value of E_T , which by referring to the table corresponds to $T = 703.6^\circ$. This method of correction is mathematically exact. (2) Multiply the fixed junction temperature by a factor, $f = (dE/dt)_0 / (dE/dt)$, the ratio of the mean e.m.f. temperature gradient between 0° and t_f to the gradient at t , and add the product to t' , the uncorrected temperature, or $t = t' + ft_f$. The e.m.f. temperature gradients may be obtained by taking the reciprocals of the numbers corresponding in successive vertical difference of the numbers in the vertical columns.

TABLE 221.—Standard Calibration Curve for Pt—PtRh (10% Rh) Thermoelement

Giving the temperature for every 100 microvolts. For use in conjunction with a deviation curve determined by calibration of the particular element at some of the following fixed points:

| | | | | | | | |
|--------------|-------------|--------|-------|----------------------------------|-------------|--------|---------|
| Water | boiling-pt. | 100.0 | 643mv | Silver | melting-pt. | 960.2 | 9111mv. |
| Naphthalene | " | 171.95 | 1585 | Gold | " | 1062.6 | 10209 |
| Tin | melting-pt. | 231.9 | 1706 | Copper | " | 1082.8 | 10534 |
| Benzophenone | boiling-pt. | 305.0 | 2365 | Li ₂ SiO ₃ | " | 1201. | 11941 |
| Cadmium | melting-pt. | 320.0 | 2503 | Diopside | " | 1391.5 | 14230 |
| Zinc | " | 419.4 | 3430 | Nickel | " | 1452.6 | 14973 |
| Sulphur | boiling-pt. | 444.55 | 3672 | Palladium | " | 1549.5 | 16144 |
| Antimony | melting-pt. | 630.0 | 5530 | Platinum | " | 1755. | 18608 |
| Aluminum | " | 658.7 | 5827 | | | | |

| E micro-volts. | 0 | 1000. | 2000. | 3000. | 4000. | 5000. | 6000. | 7000. | 8000. | 9000. | E micro-volts. |
|-------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--------|----------------|
| TEMPERATURES, °C. | | | | | | | | | | | |
| 0. | 0.0 | 147.1 | 265.4 | 374.3 | 478.1 | 578.3 | 675.3 | 769.5 | 861.1 | 950.4 | 0. |
| 100. | 17.8 | 159.7 | 276.6 | 384.9 | 488.3 | 588.1 | 684.8 | 778.8 | 870.1 | 959.2 | 100. |
| 200. | 34.5 | 172.1 | 287.7 | 395.4 | 498.4 | 597.9 | 694.3 | 788.0 | 879.1 | 968.0 | 200. |
| 300. | 50.3 | 184.3 | 298.7 | 405.9 | 508.5 | 607.7 | 703.8 | 797.2 | 888.1 | 976.7 | 300. |
| 400. | 65.4 | 196.3 | 309.7 | 416.3 | 518.6 | 617.4 | 713.3 | 806.4 | 897.1 | 985.4 | 400. |
| 500. | 80.0 | 208.1 | 320.6 | 426.7 | 528.6 | 627.1 | 722.7 | 815.6 | 906.1 | 994.1 | 500. |
| 600. | 94.1 | 219.7 | 331.5 | 437.1 | 538.6 | 636.8 | 732.1 | 824.7 | 915.0 | 1002.8 | 600. |
| 700. | 107.8 | 231.2 | 342.3 | 447.4 | 548.6 | 646.5 | 741.5 | 833.8 | 923.9 | 1011.5 | 700. |
| 800. | 121.2 | 242.7 | 353.0 | 457.7 | 558.5 | 656.1 | 750.9 | 842.9 | 932.8 | 1020.1 | 800. |
| 900. | 134.3 | 254.1 | 363.7 | 467.9 | 568.4 | 665.7 | 760.2 | 852.0 | 941.6 | 1028.7 | 900. |
| 1000. | 147.1 | 265.4 | 374.3 | 478.1 | 578.3 | 675.3 | 769.5 | 861.1 | 950.4 | 1037.3 | 1000. |

| E micro-volts. | 10000. | 11000. | 12000. | 13000. | 14000. | 15000. | 16000. | 17000. | 18000. | E micro-volts. |
|-------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------|
| TEMPERATURES, °C. | | | | | | | | | | |
| 0. | 1037.3 | 1122.2 | 1205.9 | 1289.3 | 1372.4 | 1454.8 | 1537.5 | 1620.9 | 1704.3 | 0. |
| 100. | 1045.9 | 1130.6 | 1214.2 | 1297.7 | 1380.7 | 1463.0 | 1545.8 | 1629.2 | 1712.6 | 100. |
| 200. | 1054.4 | 1139.0 | 1222.6 | 1306.0 | 1389.0 | 1471.2 | 1554.1 | 1637.6 | 1721.0 | 200. |
| 300. | 1062.9 | 1147.4 | 1230.9 | 1314.3 | 1397.3 | 1479.4 | 1562.4 | 1645.9 | 1729.3 | 300. |
| 400. | 1071.4 | 1155.8 | 1239.3 | 1322.6 | 1405.6 | 1487.7 | 1570.8 | 1654.3 | 1737.7 | 400. |
| 500. | 1079.9 | 1164.2 | 1247.6 | 1330.9 | 1413.8 | 1496.0 | 1579.1 | 1662.6 | 1746.0 | 500. |
| 600. | 1088.4 | 1172.5 | 1255.9 | 1339.2 | 1422.0 | 1504.3 | 1587.5 | 1670.9 | 1754.3 | 600. |
| 700. | 1096.9 | 1180.9 | 1264.3 | 1347.5 | 1430.2 | 1512.6 | 1595.8 | 1679.3 | | 700. |
| 800. | 1105.4 | 1189.2 | 1272.6 | 1355.8 | 1438.4 | 1520.9 | 1604.2 | 1687.6 | | 800. |
| 900. | 1113.8 | 1197.6 | 1281.0 | 1364.1 | 1446.6 | 1529.2 | 1612.5 | 1696.0 | | 900. |
| 1000. | 1122.2 | 1205.9 | 1289.3 | 1372.4 | 1454.8 | 1537.5 | 1620.9 | 1704.3 | | 1000. |

TABLE 222.—Standard Calibration Curve for Copper—Constantan Thermoelement

For use in conjunction with a deviation curve determined by the calibration of the particular element at some of the following fixed points:

Water, boiling-point, 100°, 1276 microvolts; Naphthalene, boiling-point, 217.95, 10248 mv.; Tin, melting-point, 231.9, 11009 mv.; Benzophenone, boiling-point, 305.0, 15203 mv.; Cadmium, melting-point, 320.0, 16083 mv.

| E micro-volts. | 0 | 1000. | 2000. | 3000. | 4000. | 5000. | 6000. | 7000. | 8000. | 9000. | E micro-volts. |
|-------------------|-------|-------|-------|-------|--------|--------|--------|--------|--------|--------|----------------|
| TEMPERATURES, °C. | | | | | | | | | | | |
| 0. | 0.00 | 25.27 | 49.20 | 72.08 | 94.07 | 115.31 | 135.91 | 155.95 | 175.50 | 194.62 | 0. |
| 100. | 2.60 | 27.72 | 51.53 | 74.31 | 96.23 | 117.40 | 137.94 | 157.92 | 177.43 | 196.51 | 100. |
| 200. | 5.17 | 30.15 | 53.85 | 76.54 | 98.38 | 119.48 | 139.96 | 159.89 | 179.36 | 198.40 | 200. |
| 300. | 7.73 | 32.57 | 56.16 | 78.76 | 100.52 | 121.56 | 141.98 | 161.86 | 181.28 | 200.28 | 300. |
| 400. | 10.28 | 34.98 | 58.46 | 80.97 | 102.66 | 123.63 | 143.95 | 163.82 | 183.20 | 202.16 | 400. |
| 500. | 12.81 | 37.38 | 60.70 | 83.17 | 104.79 | 125.69 | 146.00 | 165.78 | 185.11 | 204.04 | 500. |
| 600. | 15.33 | 39.77 | 63.04 | 85.37 | 106.91 | 127.75 | 148.00 | 167.73 | 187.02 | 205.91 | 600. |
| 700. | 17.83 | 42.15 | 65.31 | 87.56 | 109.02 | 129.80 | 150.00 | 169.68 | 188.93 | 207.78 | 700. |
| 800. | 20.32 | 44.51 | 67.58 | 89.74 | 111.12 | 131.84 | 151.99 | 171.62 | 190.83 | 209.64 | 800. |
| 900. | 22.80 | 46.86 | 69.83 | 91.91 | 113.22 | 133.88 | 153.97 | 173.50 | 192.73 | 211.50 | 900. |
| 1000. | 25.27 | 49.20 | 72.08 | 94.07 | 115.31 | 135.91 | 155.95 | 175.50 | 194.62 | 213.36 | 1000. |

| E micro-volts. | 10000. | 11000. | 12000. | 13000. | 14000. | 15000. | 16000. | 17000. | 18000. | E micro-volts. |
|-------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------|
| TEMPERATURES, °C. | | | | | | | | | | |
| 0. | 213.36 | 231.74 | 249.82 | 267.60 | 285.13 | 302.42 | 319.49 | 336.36 | 353.09 | 0. |
| 100. | 215.21 | 233.50 | 251.61 | 269.36 | 286.87 | 304.14 | 321.19 | 338.04 | | 100. |
| 200. | 217.06 | 235.38 | 253.40 | 271.12 | 288.61 | 305.85 | 322.88 | 339.72 | | 200. |
| 300. | 218.91 | 237.20 | 255.18 | 272.88 | 290.35 | 307.56 | 324.57 | 341.40 | | 300. |
| 400. | 220.75 | 239.01 | 256.96 | 274.64 | 292.08 | 309.27 | 326.26 | 343.07 | | 400. |
| 500. | 222.59 | 240.82 | 258.74 | 276.40 | 293.81 | 310.98 | 327.95 | 344.74 | | 500. |
| 600. | 224.43 | 242.63 | 260.52 | 278.15 | 295.54 | 312.69 | 329.64 | 346.41 | | 600. |
| 700. | 226.26 | 244.43 | 262.29 | 279.90 | 297.26 | 314.39 | 331.32 | 348.08 | | 700. |
| 800. | 228.09 | 246.23 | 264.06 | 281.65 | 298.98 | 316.09 | 333.00 | 349.75 | | 800. |
| 900. | 229.92 | 248.03 | 265.83 | 283.39 | 300.70 | 317.79 | 334.68 | 351.42 | | 900. |
| 1000. | 231.74 | 249.82 | 267.60 | 285.13 | 302.42 | 319.49 | 336.36 | 353.09 | | 1000. |

Cf. Day and Sosman, Am. Jour. Sci. 29, p. 93, 32, p. 51; *ibid.* R. B. Sosman, 30, p. 1.

TABLE 223.—Standard Calibration Curve for Copper—Constantan Thermoelement, Temperatures Below 0°C

| E μV | -5000 | -4000 | -3000 | -2000 | -1000 | 0 |
|----------------------|---------|---------|---------|--------|--------|--------|
| 0 | -169.14 | -124.46 | -87.86 | -55.81 | -26.82 | 0 |
| | 5.20 | 4.01 | 3.42 | 3.05 | 2.79 | 2.60 |
| 100 | -174.34 | -128.47 | -91.28 | -58.86 | -29.61 | -2.60 |
| | 5.40 | 4.09 | 3.46 | 3.08 | 2.81 | 2.62 |
| 200 | -179.74 | -132.56 | -94.74 | -61.94 | -32.42 | -5.22 |
| | 5.64 | 4.18 | 3.51 | 3.11 | 2.84 | 2.63 |
| 300 | -185.38 | -136.74 | -98.25 | -65.05 | -35.26 | -7.85 |
| | 5.89 | 4.28 | 3.57 | 3.15 | 2.86 | 2.65 |
| 400 | -191.27 | -141.02 | -101.82 | -68.20 | -38.12 | -10.50 |
| | 6.17 | 4.39 | 3.63 | 3.19 | 2.89 | 2.67 |
| 500 | -197.44 | -145.41 | -105.45 | -71.39 | -41.01 | -13.17 |
| | 6.51 | 4.50 | 3.68 | 3.22 | 2.90 | 2.69 |
| 600 | -203.95 | -149.91 | -109.13 | -74.61 | -43.91 | -15.86 |
| | 6.97 | 4.61 | 3.74 | 3.26 | 2.93 | 2.71 |
| 700 | -210.92 | -154.52 | -112.87 | -77.87 | -46.84 | -18.57 |
| | 7.55 | 4.73 | 3.80 | 3.29 | 2.96 | 2.73 |
| 800 | -218.47 | -159.25 | -116.67 | -81.16 | -49.80 | -21.30 |
| | | 4.87 | 3.86 | 3.33 | 2.99 | 2.75 |
| 900 | | -164.12 | -120.53 | -84.49 | -52.79 | -24.05 |
| | | 5.02 | 3.93 | 3.37 | 3.02 | 2.77 |
| 1000 | | -169.14 | -124.46 | -87.86 | -55.81 | -26.82 |

TABLE 224.—Melting Points of Some Purified Salts, 400-1300°C

(Roberts, some new standard melting points at high temperatures, Phys. Rev., 2d ser., 23, 386, 1924, which see for technique of their use.)

| | | | |
|---|---------|--|---------|
| Potassium dichromate..... | 397.5°C | Sodium chloride..... | 800.4°C |
| 45 KCl + 55 Na ₂ SO ₄ by wt.... | 517.1 | Sodium sulphate | 884.7 |
| 30.5 NaCl + 69.5 Na ₂ SO ₄ by wt. | 627.0 | Potassium sulphate *..... | 1069.1 |
| Potassium chloride..... | 770.3 | Dicalcium borate (Ca ₂ B ₂ O ₆) | 1304 |

* Potassium sulphate has sharp inversion point at 583° ± 1.

STANDARD CALIBRATION CURVE FOR CHROMEL-ALUMEL THERMOELEMENT *

| E $m\phi$ | -0 | 0 | 10 | 20 | 30 | 40 |
|----------------|-----------------|---------------|---------------|---------------|---------------|------------------|
| 0 | 0.0 12.7 | 0.0 12.6 | 250.1 13.0 | 490.5 11.9 | 733.8 12.5 | 991.3 13.5 |
| 0.5 | - 12.7 13.1 | 12.6 12.4 | 263.1 12.9 | 502.4 12.0 | 746.3 12.5 | 1004.8 13.6 |
| 1.0 | - 25.8 13.4 | 25.0 12.3 | 276.0 12.7 | 514.4 12.0 | 758.8 12.5 | 1018.4 13.8 |
| 1.5 | - 39.2 13.8 | 37.3 12.2 | 288.7 12.5 | 526.4 12.0 | 771.3 12.6 | 1032.2 13.8 |
| 2.0 | - 53.0 14.4 | 49.5 12.2 | 301.2 12.3 | 538.4 12.0 | 783.9 12.6 | 1046.0 13.9 |
| 2.5 | - 67.4 15.0 | 61.7 12.1 | 313.5 12.1 | 550.4 12.0 | 796.5 12.7 | 1059.9 14.1 |
| 3.0 | - 82.4 15.8 | 73.8 12.1 | 325.6 11.9 | 562.4 12.1 | 809.2 12.7 | 1074.0 14.1 |
| 3.5 | - 98.2 16.8 | 85.9 12.2 | 337.5 11.6 | 574.5 12.1 | 821.9 12.7 | 1088.1 14.2 |
| 4.0 | - 115.0 18.1 | 98.1 12.2 | 349.1 11.5 | 586.6 12.1 | 834.6 12.8 | 1102.3 14.4 |
| 4.5 | - 133.1 20.1 | 110.3 12.1 | 360.6 11.5 | 598.7 12.1 | 847.4 12.8 | 1116.7 14.5 |
| 5.0 | - 153.2 22.8 | 122.7 12.5 | 372.1 11.7 | 610.8 12.2 | 860.2 12.9 | 1131.2 14.5 |
| 5.5 | - 176.0 28.5 | 135.2 12.6 | 383.8 11.8 | 623.0 12.2 | 873.1 12.9 | 1145.7 14.6 |
| 6.0 | - 204.5 | 147.8 12.6 | 395.6 11.8 | 635.2 12.2 | 886.0 13.0 | 1160.3 14.7 |
| 6.5 | | 160.4 12.7 | 407.4 11.8 | 647.4 12.3 | 899.0 13.0 | 1175.0 14.8 |
| 7.0 | | 173.1 12.7 | 419.2 11.8 | 659.7 12.3 | 912.0 13.1 | 1189.8 14.8 |
| 7.5 | | 185.8 12.8 | 431.0 11.9 | 672.0 12.3 | 925.1 13.1 | 1204.6 15.0 |
| 8.0 | | 198.6 12.8 | 442.9 11.9 | 684.3 12.3 | 938.2 13.2 | (1220.0) 15.0 |
| 8.5 | | 211.4 12.9 | 454.8 11.9 | 696.6 12.4 | 951.4 13.2 | (1235.0) 16.0 |
| 9.0 | | 224.3 12.9 | 466.7 11.9 | 709.0 12.4 | 964.6 13.3 | (1251.0) 16.0 |
| 9.5 | | 237.2 12.9 | 478.6 11.9 | 721.4 12.4 | 977.9 13.4 | (1267.0) 16.0 |
| 10.0 | | 250.1 | 490.5 | 733.8 | 991.3 | (1283.0) |

* Standard calibration curve for chromel-alumel (Hoskins) thermocouple giving the temperature and temperature differences for every 0.5 millivolt. Fixed junction is at 0°. For use in conjunction with a deviation curve determined by calibration of the particular couple at some of the following fixed points:

| | Degrees C | Milli- volts $m\phi$ | | Degrees C | Milli- volts $m\phi$ |
|------------------------|--------------|----------------------------|---------------------------|--------------|----------------------------|
| S, boiling point..... | 444.5 | 18.07 | Au, melting point..... | 1063.0 | 42.60 |
| Sb, melting point..... | 630.0 | 25.79 | Cu (in air), melting | | |
| Al, melting point..... | 660.0 | 27.00 | point..... | 1065.0 | 42.68 |
| Ag, melting point..... | 960.2 | 38.83 | Cu (pure), melting point. | 1082.8 | 43.31 |

OPTICAL PYROMETRY

(The following discussion is abbreviated from Dushman, *Rev. Mod. Phys.*, 2, 387, 1930.)

Data on various substances are now available by which accurate determinations may be made of the temperature of an emitting surface. For a comprehensive review see Lax and Pirani, *Handb. Phys.*, 19, 1-45; 21, 190-272, Julius Springer, Berlin, 1929. Data on total radiation from various bodies have been summarized by Coblenz (*I.C.T.* 5, 238-245, 1929).

Undoubtedly the most accurate method consists in determining the brilliancy (candles/cm²). The temperature coefficient $(dB/B)/(dT/T)$ where B = brightness in international candles/cm², for W varies from 22.75 at 1000° K. to 8.45 at 3000° K. (Jones, Langmuir, *Gen. Elec. Rev.*, 30, 310, 354, 408, 1927). With the exception of electron emission and the rate of evaporation, the candlepower shows the greatest temperature variation.

While the values of B as a function of T are available for several substances, a fair approximation is possible to the true T of a substance for which the average luminous emissivity is unknown by the following methods. (Average luminous emissivity means the ratio of the total normal brightness to that of a black-body at the same T . For W this value is from 0.464, $T=1000^\circ$ K. to 0.440, $T=3000^\circ$ K., Forsythe, *Worthing, Astrophys. Journ.*, 61, 126, 1925).

With a photometer determine the temperature T_c at which substance emits light of the *same color* as a black-body—a value higher than the true temperature. The following table is due to Worthing-Forsythe:

| T_c (tungsten) | True T | $(T_c - T)/T$ | T_s (tungsten) |
|------------------|----------|---------------|------------------|
| 1006° K. | 1000° K. | 0.006 | 966° K. |
| 1517 | 1500 | .011 | 1420 |
| 2033 | 2000 | .0165 | 1857 |
| 2557 | 2500 | .023 | 2274 |
| 3094 | 3000 | .031 | 2673 |

The brightness may be compared with a standard lamp for a given wave length, usually 0.665 μ . The temperature found is called the brightness temperature, T_s , lower than the true temperature, increasingly so with decrease in e_λ , the emissivity for this wave length, and increasing with the temperature. Thus for w , e_λ for $\lambda=0.665\mu$ varies from 0.456, $T=1000^\circ$ K. to 0.415, $T=3000^\circ$ K. and the observed values T_s are given in the preceding table. From these determinations of T_c and T_s fairly approximate values of T may be deduced.

It is possible to determine the actual value of e_λ by methods described by both Langmuir, Worthing and Forsythe, then calculate T , the true temperature from optical pyrometer measurements of T . See Forsythe, *Journ. Opt. Soc. Amer.*, 16, 307, 1928; *Journ. Amer. Ceram. Soc.*, 12, 780, 1929; Foote, Fairchild, *Symposium on Pyrometer*, Amer. Inst. Mining and Metallurg. Eng., 338, 324, 1920; also loc. cit., p. 291, 367, 285.

At temperatures below 1100-1200° K. optical methods become impractical, and radiation in watts radiated per unit area or resistance must be used. Data on energy radiated as a function of the temperature have been summarized by Lax and Pirani, *Handb. Phys.*, 21, 236-240, for W, Mo, Ta, Pr, Os, Au, Ni, Fe, C, Ag, Cu, and Zr.

TABLE 227.—Correction for Temperature of Emergent Mercurial Thermometer Thread

When the temperature of a portion of a thermometer stem with its mercury thread differs much from that of the bulb, a correction is necessary to the observed temperature unless the instrument has been calibrated for the experimental conditions. This stem correction is proportional to $n\beta(T-t)$, where n is the number of degrees in the exposed stem, β the apparent coefficient of expansion of mercury in the glass, T the measured temperature, and t the mean temperature of the exposed stem. For temperatures up to 100° C, the value of β is for Jena 16^{III} or Greiner and Friedrich resistance glass, 0.000159, for Jena 59^{III}, 0.000164, and when of unknown composition it is best to use a value of about 0.000155. The formula requires a knowledge of the temperature of the emergent stem. This may be approximated in one of three ways: (1) by a "fadenthermometer" (see Buckingham, Bulletin Bureau of Standards, 8, p. 239, 1912); (2) by exploring the temperature distribution of the stem and calculating its mean temperature; and (3) by suspending along the side of, or attaching to the stem, a single thermometer. Table 228 is taken from the Smithsonian Meteorological Tables.

TABLE 228.—Stem Correction for Centigrade Thermometers

Values of 0.000155 $n(T-t)$.

| n | $(T-t)$ | | | | | | | |
|-------|---------|------|------|------|------|------|------|------|
| | 10° | 20° | 30° | 40° | 50° | 60° | 70° | 80° |
| 10° C | 0.02 | 0.03 | 0.05 | 0.06 | 0.08 | 0.09 | 0.11 | 0.12 |
| 20 | 0.03 | 0.06 | 0.09 | 0.12 | 0.16 | 0.19 | 0.22 | 0.25 |
| 30 | 0.05 | 0.09 | 0.14 | 0.19 | 0.23 | 0.28 | 0.33 | 0.37 |
| 40 | 0.06 | 0.12 | 0.19 | 0.25 | 0.31 | 0.37 | 0.43 | 0.50 |
| 50 | 0.08 | 0.16 | 0.23 | 0.31 | 0.39 | 0.46 | 0.54 | 0.62 |
| 60 | 0.09 | 0.19 | 0.28 | 0.37 | 0.46 | 0.56 | 0.65 | 0.74 |
| 70 | 0.11 | 0.22 | 0.33 | 0.43 | 0.54 | 0.65 | 0.76 | 0.87 |
| 80 | 0.12 | 0.25 | 0.37 | 0.50 | 0.62 | 0.74 | 0.87 | 0.99 |
| 90 | 0.14 | 0.28 | 0.42 | 0.56 | 0.70 | 0.84 | 0.98 | 1.12 |
| 100 | 0.16 | 0.31 | 0.46 | 0.62 | 0.78 | 0.93 | 1.08 | 1.24 |

TABLE 229.—Reduction of Gas Thermometers to Thermodynamic Scale

The final standard scale is Kelvin's thermodynamic scale, independent of the properties of any substance, a scale resulting from the use of a gas thermometer using a perfect gas. A discussion of this is given by Buckingham, Bur. Standards Bull., 3, 237, 1907: "The thermodynamic correction of the centigrade constant-pressure scale at the given temperature is very nearly proportional to the constant pressure at which the gas is kept" and "the thermodynamic correction to the centigrade constant-volume scale is approximately proportional to the initial pressure at the ice point." These two rules are very convenient, since from the corrections for any one pressure, one can calculate approximately those for the same gas at any other pressure.

The highest temperature possible is limited by the container for the gas. Day and Sosman carried a platinum-rhodium gas thermometer up to the melting point of palladium. For most work, however, the region of the gas thermometer should be considered as ending at about 1000° C (1273° K.).

Note: All corrections in the following table are to be added *algebraically*.

273.1° C (ice point)

For a discussion of the various values and for the corrections of the various gas thermometers to the thermodynamic scale see Buckingham, Bull. Bureau Standards, 3, p. 237, 1907.

Scale Corrections for Gas Thermometers.

| Temp. °C | Constant pressure = 100 cm | | | Constant vol., $p_0 = 100$ cm, $t_0 = 0^\circ$ C | | |
|-------------|----------------------------|--------|--------|--|--------|--------|
| | He | H | N | He | H | N |
| -240° | — | +1.0 | — | +0.02 | +0.18 | — |
| -200 | +0.13 | +0.26 | — | +0.01 | +0.06 | — |
| -100 | +0.04 | +0.03 | +0.40 | .000 | +0.010 | +0.06 |
| -50 | +0.012 | +0.02 | +0.12 | .000 | +0.004 | +0.02 |
| +25 | —0.003 | —0.003 | —0.020 | .000 | .000 | —0.006 |
| +50 | —0.003 | —0.003 | —0.025 | .000 | .000 | —0.006 |
| +75 | —0.003 | —0.003 | —0.017 | .000 | .000 | —0.004 |
| +150 | +0.007 | +0.01 | +0.04 | +0.000 | +0.000 | +0.01 |
| +200 | +0.01 | +0.02 | +0.11 | .000 | +0.002 | +0.04 |
| +450 | +0.1 | +0.04 | +0.5 | 0.00 | +0.01 | +0.2 |
| +1000 | +0.3 | — | +1.7 | — | — | +0.7 |
| +1500 | — | — | +3. | — | — | +1.3 |

TABLE 230
PRACTICAL THERMOELECTRIC SCALES
 (Comparisons)

(Adapted from Roeser, Bur. Standards Res. Paper 99, 1929, which see for details of use.)

Prior to the adoption of the International Temperature Scale, the Pt-Pt10% Rh thermocouple was almost universally used for scales 450° to 1100°C, and defining equations were quadratic or cubic depending upon the number of calibration points.

The scale based on the work of Holborn and Day was calibrated at the freezing point of Zn (419.0°C), Sb (630.6°C) and Cu (1084.1°C) and a quadratic equation, $E = a + vt + ct^2$, for interpolation. This was almost universally used from 1900-1909. Work of Waidner, Burgess, 1909, and Day, Sosman, 1910-1912, necessitated a readjustment. In 1912 the Bureau of Standards redefined its scale, assigning values determined with the resistance thermometer to the Zn and Sb points, while the freezing point of Cu was taken as 1083.0°C. This 1912 scale, used from 1912-1916, will be called the Zn,Sb,Cu temperature scale.

A scale proposed by Sosman and revised by Adams (Journ. Amer. Chem. Soc., 36, 65, 1914) was realized by using a standard reference table, giving the average *t*, e.m.f. relation for thermocouple used by Day and Sosman. A deviation curve, determined by any other couple by calibration at several points would be plotted relating the difference between observed e.m.f. and the e.m.f. from the reference table against the obs. e.m.f. of the couple. This scale, although very convenient, is not completely defined and no comparison is made here.

In 1916, the Physikalische-Technische Reichsanstalt adopted a scale with the couple calibrated at the Cd point (320.9°C), Sb (630°C), An (1063°C) and Pd (1557°C). No comparison will be made here.

A scale adopted by the Bureau of Standards in 1916 was defined by calibration at the Zn and Al points with a Cu point (1083.0°C). This was used from 1916-1926 and is here designated the Zn,Al,Cu scale.

The scale adopted by the P.T.R. and the Bureau of Standards in 1924 was calibrated at Zn and Sb points (determined by resistance thermometer) and the Ag point (960.5°C) and the Au point (1063.0°C). It will be designated the Zn,Sb,Ag,Au scale.

The 1927 7th Annual Conference of Weights and Measures (31 nations) unanimously adopted what is between 660° and 1063°C the Zn,Sb,Ag,Cu scale with the Zn point omitted. The table below shows a comparison of the various scales. The following values for the freezing points were used:

Zn 419.47°C Al 659.23°C Au 1063.0°C
 Sb 630.52°C Ag 960.5°C Cu (reducing atm.°) 1083.0°C

Table 231 gives the corresponding difference of temperature.

Comparison of *t*°C—e.m.f. relations with International Temperature Scale. (Comparisons with two thermo-couples are given.)

| Temperature (°C) | E.m.f. in microvolts for temperature scales, Thermocouple A | | | | E.m.f. in microvolts for temperature scales, Thermocouple B | | | |
|------------------|---|----------------|--------------------|---------------------------------|---|----------------|--------------------|---------------------------------|
| | Zn, Sb, and Cu | Zn, Al, and Cu | Zn, Sb, Ag, and Au | International temperature scale | Zn, Sb, and Cu | Zn, Al, and Cu | Zn, Sb, Ag, and Au | International temperature scale |
| 419.47 | 3438.2 | 3438.2 | 3438.2 | 3447.5 | 3435.6 | 3435.6 | 3435.6 | 3444.7 |
| 450 | 3732.9 | 3732.8 | 3733.4 | 3740.5 | 3729.8 | 3729.6 | 3730.2 | 3737.2 |
| 500 | 4222.6 | 4222.2 | 4223.3 | 4227.6 | 4218.6 | 4218.2 | 4219.3 | 4223.5 |
| 550 | 4720.9 | 4720.4 | 4721.6 | 4723.7 | 4716 | 4715.4 | 4716.6 | 4718.7 |
| 600 | 5227.9 | 5227.2 | 5228.2 | 5228.8 | 5221.9 | 5221.2 | 5222.4 | 5222.9 |
| 630.52 | 5541.6 | 5540.9 | 5541.6 | 5541.6 | 5535 | 5534.2 | 5535 | 5535 |
| 650 | 5743.5 | 5742.8 | 5743.3 | 5743 | 5736.5 | 5735.7 | 5736.3 | 5736 |
| 659.23 | 5839.7 | 5838.9 | 5839.3 | 5838.9 | 5832.4 | 5831.6 | 5832.1 | 5831.6 |
| 700 | 6267.8 | 6267 | 6267 | 6266.1 | 6259.7 | 6258.8 | 6258.8 | 6258 |
| 750 | 6800.8 | 6800 | 6799.3 | 6798.3 | 6791.5 | 6790.6 | 6790.9 | 6789 |
| 800 | 7342.5 | 7341.7 | 7340.3 | 7339.4 | 7331.9 | 7331 | 7329.8 | 7328.9 |
| 850 | 7892.8 | 7892.1 | 7890.2 | 7889.6 | 7880.9 | 7880.1 | 7878.4 | 7877.7 |
| 900 | 8451.8 | 8451.2 | 8449.1 | 8448.8 | 8438.5 | 8437.8 | 8435.8 | 8435.5 |
| 950 | 9019.5 | 9019 | 9017 | 9016.9 | 9004.8 | 9004.2 | 9002.3 | 9002.2 |
| 960.50 | 9139.8 | 9139.3 | 9137.4 | 9137.4 | 9124.8 | 9124.2 | 9122.4 | 9122.4 |
| 1000 | 9595.8 | 9595.5 | 9594 | 9594.1 | 9579.6 | 9579.2 | 9577.8 | 9577.9 |
| 1050 | 10180.8 | 10180.7 | 10180.3 | 10180.3 | 10163.1 | 10162.8 | 10162.5 | 10162.5 |
| 1063 | 10334.4 | 10334.3 | 10334.2 | 10334.2 | 10316.1 | 10316 | 10316 | 10316 |
| 1083 | 10571.7 | 10571.7 | 10572.3 | 10572.1 | 10552.8 | 10552.8 | 10553.4 | 10553.3 |
| 1100 | 10774.5 | 10774.6 | 10775.8 | 10775.5 | 10755.1 | 10755.2 | 10756.4 | 10756.1 |

TABLE 231.—Temperature Differences between I.T.S. and various Older Scales

| °C | I.T.S.- ZnSb- Cu | I.T.S.- ZnAl- Cu | I.T.S.- ZnSb- AgAu | °C | I.T.S.- ZnSb- Cu | I.T.S.- ZnAl- Cu | I.T.S.- ZnSb- AgAu | °C | I.T.S.- ZnSb- Cu | I.T.S.- ZnAl- Cu | I.T.S.- ZnSb- AgAu |
|-----|------------------------|------------------------|--------------------------|-------|------------------------|------------------------|--------------------------|------|------------------------|------------------------|--------------------------|
| 600 | -.08 | .00 | -.04 | 900 | -.26 | -.21 | -.03 | 1050 | -.04 | -.03 | .00 |
| 700 | -.16 | .08 | -.08 | 950 | -.23 | -.18 | -.01 | 1063 | -.01 | .00 | .00 |
| 750 | -.24 | .16 | -.09 | 960.5 | -.21 | -.16 | .00 | 1083 | +.04 | +.03 | -.01 |
| 800 | -.28 | .20 | -.08 | 1000 | -.15 | -.12 | .01 | 1100 | +.08 | +.08 | -.03 |
| 850 | -.29 | .22 | -.06 | | | | | | | | |

TABLE 232.—Conversion Factors for Units of Work

| | Joules | Foot- pounds | Kilogram- meters | 15° Calories | British thermal units | Kilowatt- hours |
|-------------------------------------|------------|-----------------|---------------------|-----------------|-----------------------------|---------------------------|
| 1 Joule | 1 | 0.7376† | 0.1020† | 0.2391 | 0.0009486 | 0.2778×10^{-6} |
| 1 Foot-pound . . . | 1.356* | 1 | 0.1383 | 0.3241* | 0.001286* | 0.3767×10^{-6} * |
| 1 Kilogram-meter = | 9.807* | 7.234 | 1 | 2.345* | 0.009302* | 2.724×10^{-6} * |
| 1 15° Calorie . . . | 4.183 | 3.085† | 0.4267† | 1 | 0.003965 | 1.162×10^{-6} |
| 1 British thermal unit | 1054. | 777.5† | 107.5† | 251.9 | 1 | 0.0002928 |
| 1 Kilowatt-hour.. = | 3 600 000. | 2 655 000.† | 367 200.† | 860 800. | 3415. | 1 |

The value used for g is the standard value, 980.665 cm. per sec. per sec. = 32.174 feet per sec. per sec.

* The values thus marked vary directly with "g."

† The values thus marked vary inversely with "g." For values of "g" see Tables 706-709.

TABLE 233.—Value of the English and American Horsepower (746 watts) in Local Foot-pounds and Kilogram-meters per Second at Various Altitudes and Latitudes

| Altitude | Kilogram-meters per second | | | | | Foot-pounds per second | | | | |
|----------|----------------------------|--------|--------|--------|--------|------------------------|--------|--------|--------|--------|
| | Latitude | | | | | Latitude | | | | |
| | 0° | 30° | 45° | 60° | 90° | 0° | 30° | 45° | 60° | 90° |
| 0 km | 76.275 | 76.175 | 76.074 | 75.973 | 75.873 | 551.70 | 550.97 | 550.24 | 549.52 | 548.79 |
| 1.5 " | 76.297 | 76.197 | 76.095 | 75.995 | 75.895 | 551.86 | 551.13 | 550.41 | 549.68 | 548.95 |
| 3 " | 76.320 | 76.220 | 76.119 | 76.018 | 75.918 | 552.03 | 551.30 | 550.57 | 549.85 | 549.12 |

TABLE 234.—Nonflammable Liquids for Cryostats

(Taken from Kanolt, Bur. Standards Sci. Paper, 520, 1926.)

| | | | | | | | | | |
|--|--|-------------------|-------|----------------------------------|-------|-------|--------|-------|-------|
| Liquid..... | CCl ₄ | CHCl ₃ | 4* | C ₂ H ₅ Br | 32 | 39* | No. 40 | | |
| Freezing point..... °C | -23 | -63 | -81 | -119 | -139 | -145 | -150± | | |
| *Compositions: No. 4; CCl ₄ , 49.4%; CHCl ₃ , 50.6%. | | | | | | | | | |
| | No. 32; CHCl ₃ , 19.7%; C ₂ H ₅ Br, 44.9%; C ₂ H ₂ Cl ₂ , 13.8%; C ₂ HCl ₃ , 21.6%. | | | | | | | | |
| | No. 39; CHCl ₃ , 14.5%; C ₂ H ₅ Br, 33.4%; C ₂ H ₂ Cl ₂ , 10.4%; C ₂ HCl ₃ , 16.4%; CH ₂ Cl ₂ , 25.3%. | | | | | | | | |
| | No. 40; CHCl ₃ , 17.9%; C ₂ H ₅ Cl, 9.3%; C ₂ H ₅ Br, 40.7%; C ₂ H ₂ Cl ₂ , 125%; C ₂ HCl ₃ , 19.6%. | | | | | | | | |
| | -80°C | -90° | -100° | -110° | -120° | -130° | -140° | -145° | -150° |
| Viscosities in centipoises: | C ₂ H ₅ Br | 1.81 | 2.25 | 2.89 | 3.86 | 5.6 | ... | ... | ... |
| | No. 32 | ... | 3.03 | 4.57 | 7.4 | 13.7 | 29.3 | 81 | ... |
| | No. 34 | 1.97 | 2.57 | 3.69 | 5.6 | 10 | 22.3 | 85 | 242 |
| | No. 40 | ... | 2.88 | 3.89 | 5.9 | 10.2 | 22.5 | 71 | 170 |
| * Because of volatility and oxidation of some, these liquids should be kept in well stoppered bottles when not in use. | | | | | | | | | |

MELTING AND BOILING POINTS OF THE CHEMICAL ELEMENTS

| Element | Symbol and atomic no. | Melting point °C | Boiling point °C | Element | Symbol and atomic no. | Melting point °C | Boiling point °C |
|------------------------|-----------------------|------------------|------------------|-------------------------|-----------------------|------------------|------------------|
| Aluminum | Al 13 | 659.7 | 1800 | Molybdenum ... | Mo 42 | 2620 | 3700 |
| Antimony | Sb 51 | 630.5 | 1380 | Neodymium | Nd 60 | 840 | |
| Argon | A 18 | - 189.2 | - 185.7 | Neon | Ne 10 | - 248.67 | - 245.9 |
| Arsenic | As 33 | (820) | 615.5 | Nickel | Ni 28 | 1455 | 2900 |
| Barium | Ba 56 | 850 | 1140 | Nitrogen | N 7 | - 209.86 | - 195.81 |
| Beryllium | Be 4 | 1350 | (1500) | Osmium | Os 76 | 2700 | (> 5300) |
| Bismuth | Bi 83 | 271.3 | 1450 | Oxygen | O 8 | - 218.4 | - 183 |
| Boron | B 5 | 2300 | | Ozone | O ₃ | - 251.4 | - 112 |
| Bromine | Br 35 | - 7.2 | 58.8 | Palladium | Pd 46 | 1553 | 2200 |
| Cadmium | Cd 48 | 320.9 | 766 | Phosphorus ... | P 15 | 44.1 | 280 |
| Calcium | Ca 20 | 810 | 1170 | Platinum | Pt 78 | 1773.5 | 4300 |
| Carbon | C 6 | > 3500 | (4200) | Potassium | K 19 | 62.3 | 760 |
| Cerium | Ce 58 | 640 | 1400 | Praseodymium ... | Pr 59 | 940 | |
| Cesium | Cs 55 | 26 | 670 | Radium | Ra 88 | 960 | 1140 |
| Chlorine | Cl 17 | - 101.6 | - 34.7 | Radon | Rn 86 | - 110 | |
| Chromium | Cr 24 | 1615 | 2200 | Rhenium | Re 75 | (3000) | |
| Cobalt | Co 27 | 1480 | 3000 | Rhodium | Rh 45 | 1985 | > 2500 |
| Columbium ... | Cb 41 | 1950 | 2900 | Rubidium | Rb 37 | 38.5 | 700 |
| Copper | Cu 29 | 1083 | 2300 | Ruthenium | Ru 44 | 2450 | > 2700 |
| Dysprosium ... | Dy 66 | | | Samarium | Sm 62 | > 1300 | |
| Erbium | Er 68 | | | Scandium | Sc 21 | 1200 | (2400) |
| Europium | Eu 63 | | | Selenium | Se 34 | 220 | 688 |
| Fluorine | F 9 | - 223 | - 187 | Silicon | Si 14 | 1420 | 2600 |
| Gadolinium ... | Gd 64 | | | Silver | Ag 47 | 960.5 | 1950 |
| Gallium | Ga 31 | 29.7 | > 1600 | Sodium | Na 11 | 97.5 | 880 |
| Germanium ... | Ge 32 | 958.5 | (2700) | Strontium | Sr 38 | 800 | 1150 |
| Gold | Au 79 | 1063 | 2600 | Sulphur | S 16 | 113-119 | 444.6 |
| Hafnium | Hf 72 | (1700) | (> 3200) | Tantalum | Ta 73 | 2850 | (> 4100) |
| Helium | He 2 | < -272 | - 268.94 | Tellurium | Te 52 | 452 | 1390 |
| Holmium | Ho 67 | | | Terbium | Tb 65 | | |
| Hydrogen | H 1 | - 259.14 | - 252.8 | Thallium | Tl 81 | 303.5 | 1650 |
| Indium | In 49 | 155 | > 1450 | Thorium | Th 90 | 1845 | > 3000 |
| Iodine | I 53 | 113.5 | 184.35 | Thulium | Tm 69 | | |
| Iridium | Ir 77 | 2350 | (> 4800) | Tin | Sn 50 | 231.89 | 2260 |
| Iron | Fe 26 | 1535 | 3000 | Titanium | Ti 22 | 1800 | (> 3000) |
| Krypton | Kr 36 | - 169 | - 151.8 | Tungsten | W 74 | 3370 | 5900 |
| Lanthanum ... | La 57 | 826 | 1800 | Uranium | U 92 | < 1850 | |
| Lead | Pb 82 | 327.4 | 1620 | Vanadium | V 23 | 1710 | (3000) |
| Lithium | Li 3 | 186 | > 1200 | Xenon | Xe 54 | - 140 | - 109.1 |
| Lutecium | Lu 71 | | | Ytterbium | Yb 70 | | |
| Magnesium ... | Mg 12 | 651 | 1100 | Yttrium | Y 39 | 1490 | (2500) |
| Manganese ... | Mn 25 | 1260 | 1900 | Zinc | Zn 30 | 419.47 | 907 |
| Mercury | Hg 80 | - 38.87 | 356.00 | Zirconium ... | Zr 40 | 1900 | > 2900 |

(Metals in heavy type are often used as standard melting points.)

TABLE 236.—Effect of Pressure on Melting Point

| Substance. | Melting point at 1 kg./sq. cm | Highest experimental pressure: kg./sq. cm | dt/dp at 1 kg./sq. cm | Δt (observed) for 1000 kg./sq. cm | Reference |
|------------|----------------------------------|--|----------------------------|---|-----------|
| Hg | -38.85 | 12,000 | 0.00511 | 5.1 * | 1 |
| K | 59.7 | 2,800 | 0.0136 | 13.8 | 2 |
| Na | 97.62 | 12,000 | 0.00860 | +12.3† | 4 |
| Bi | 271.0 | 12,000 | -0.00342 | -3.5† | 4 |
| Sn | 231.9 | 2,000 | 0.00317 | 3.17 | 3 |
| Bi | 270.9 | 2,000 | -0.00344 | -3.44 | 3 |
| Cd | 320.9 | 2,000 | 0.00609 | 6.09 | 3 |
| Pb | 327.4 | 2,000 | 0.00777 | 7.77 | 3 |

* Δt (observed) for 10,000 kg./sq. cm is 50.8°.

† Na melts at 177.5° at 12,000 kg./cm²; K at 179.6°; Bi at 218.3°; Pb at 644°. Luckey obtains melting point for tungsten as follows: 1 atm, 3623° K; 8, 3594; 18, 3572; 28, 3564. Phys. Rev. 1917.

References: (1) P. W. Bridgman, Proc. Am. Acad. 47, pp. 391-06, 416-19, 1911; (2) G. Tammann, Kristallisieren und Schmelzen, Leipzig, 1903, pp. 98-99; (3) J. Johnston and L. H. Adams, Am. J. Sci. 31, p. 516, 1911; (4) P. W. Bridgman, Phys. Rev. 6, 1, 1915.

A large number of organic substances, selected on account of their low melting points, have also been investigated: by Tammann, *loc. cit.*; G. A. Hulett, Z. physik. Chem. 28, p. 629, 1899; F. Körber, *ibid.*, 82, p. 45, 1913; E. A. Block, *ibid.*, 82, p. 403, 1913; Bridgman, Phys. Rev. 3, 126, 1914; Pr. Am. Acad. 51, 55, 1915; 51, 581, 1916; 52, 57, 1916; 52, 91, 1916. The results for water are given in the following table.

TABLE 237.—Effect of Pressure on Freezing Point of Water *

| Pressure: † kg./sq. cm | Freezing point. | Phases in Equilibrium. |
|---------------------------|-----------------|--|
| 1 | 0.0 | Ice I — liquid. |
| 1,000 | -8.8 | Ice I — liquid. |
| 2,000 | -20.15 | Ice I — liquid. |
| 2,115 | -22.0 | Ice I — ice III — liquid (triple point). |
| 3,000 | -18.40 | Ice III — liquid. |
| 3,530 | -17.0 | Ice III — ice V — liquid (triple point). |
| 4,000 | -13.7 | Ice V — liquid. |
| 6,000 | -1.6 | Ice V — liquid. |
| 6,380 | + 0.16 | Ice V — ice VI — liquid (triple point). |
| 8,000 | 12.8 | Ice VI — liquid. |
| 12,000 | 37.9 | Ice VI — liquid. |
| 16,000 | 57.2 | Ice VI — liquid. |
| 20,000 | 73.6 | Ice VI — liquid. |

* P. W. Bridgman, Proc. Am. Acad. 47, pp. 441-558, 1912.

† 1 atm. = 1.033 kg./sq. cm.

TABLE 238.—Effect of Pressure on Boiling Point *

| Metal. | Pressure. | ° C | Metal. | Pressure. | ° C | Metal. | Pressure. | ° C |
|--------|-------------|------|--------|-------------|------|--------|-------------|------|
| Bi | 10.2 cm Hg. | 1200 | Ag | 26.3 cm Hg. | 1780 | Pb | 20.6 cm Hg. | 1410 |
| Bi | 25.7 cm Hg. | 1310 | Cu | 10.0 cm Hg. | 1980 | Pb | 6.3 atme. | 1870 |
| Bi | 6.3 atme. | 1740 | Cu | 25.7 cm Hg. | 2180 | Pb | 11.7 atme. | 2100 |
| Bi | 11.7 atme. | 1950 | Sn | 10.1 cm Hg. | 1970 | Zn | 11.7 atme. | 1230 |
| Bi | 16.5 atme. | 2060 | Sn | 26.2 cm Hg. | 2100 | Zn | 21.5 atme. | 1280 |
| Ag | 10.3 cm Hg. | 1660 | Pb | 10.5 cm Hg. | 1315 | Zn | 53.0 atme. | 1510 |

* Greenwood, Pr. Roy. Soc., p. 483, 1910.

DENSITIES AND MELTING AND BOILING POINTS OF INORGANIC COMPOUNDS

| Substance. | Chemical formula. | Density, about 20° C | Melting point C | Authority. | Boiling point C | Pres- sure mm | Authority. |
|----------------------------|--|----------------------------|-----------------------|------------|-----------------------|---------------------|------------|
| Aluminum chloride..... | AlCl ₃ | — | 190. | 1 | 183. ^o | 752 | 1 |
| “ nitrate..... | Al(NO ₃) ₃ + 9H ₂ O | — | 72.8 | 2 | 134.* | — | — |
| “ oxide..... | Al ₂ O ₃ | 4.00 | 2050. | 28 | — | — | — |
| Ammonia..... | NH ₃ | — | -75. | 3 | -33.5 | 760 | 7 |
| Ammonium nitrate..... | NH ₄ NO ₃ | 1.72 | 165. | — | 210.* | — | — |
| “ sulphate..... | (NH ₄) ₂ SO ₄ | 1.77 | 140. | 4 | — | — | — |
| “ phosphite..... | NH ₄ H ₂ PO ₃ | — | 123. | 5 | 150.* | — | — |
| Antimony trichloride..... | SbCl ₃ | 3.06 | 73. | — | 223. | 760 | — |
| “ pentachloride..... | SbCl ₅ | 2.35 | 3. | 11 | 102. | 68 | 14 |
| Arsenic trichloride..... | AsCl ₃ | 2.20 | -18. | 8 | 130.2 | 760 | 23 |
| Arsenic hydride..... | AsH ₃ | — | -113.5 | 6 | -54.8 | 760 | 6 |
| Barium chloride..... | BaCl ₂ | 3.86 | 960. | 11 | — | — | — |
| “ nitrate..... | Ba(NO ₃) ₂ | 3.24 | 575. | 24 | — | — | — |
| “ perchlorate..... | Ba(ClO ₄) ₂ | — | 505. | 10 | — | — | — |
| Bismuth trichloride..... | BiCl ₃ | 4.56 | 232.5 | — | 440. | 760 | — |
| Boric acid..... | H ₃ BO ₃ | 1.46 | 185. | — | — | — | — |
| “ anhydride..... | B ₂ O ₃ | 1.79 | 577. | — | — | — | — |
| Borax (sodium borate)..... | Na ₂ B ₄ O ₇ | 2.36 | 741. | 27 | — | — | — |
| Cadmium chloride..... | CdCl ₂ | 4.05 | 500. | 25 | 900 ± | — | 9 |
| “ nitrate..... | Cd(NO ₃) ₂ + 4H ₂ O | 2.45 | 59.5 | 2 | 132. | 760 | 4 |
| Calcium chloride..... | CaCl ₂ | 2.26 | 774.0 | — | — | — | — |
| “ chloride..... | CaCl ₂ + 6H ₂ O | 1.68 | 29.6 | — | — | — | — |
| “ nitrate..... | Ca(NO ₃) ₂ | 2.36 | 499. | 24 | — | — | — |
| “ nitrate..... | Ca(NO ₃) ₂ + 4H ₂ O | 1.82 | 42.3 | 26 | 132.* | — | — |
| “ oxide..... | CaO | 3.3 | 2570. | 28 | — | — | — |
| Carbon tetrachloride..... | CCl ₄ | 1.59 | -24. | 22 | 76.7 | 760 | 23 |
| “ trichloride..... | C ₂ Cl ₆ | 1.03 | 184. | — | — | — | — |
| “ monoxide..... | CO | — | -207. | 6 | -190. | 760 | 6 |
| “ dioxide..... | CO ₂ | 1.56 | -57. | 3 | -80. | subl. | — |
| “ disulphide..... | CS ₂ | 1.26 | -110. | 13 | 46.2 | 760 | — |
| Chloric(per) acid..... | HClO ₄ + H ₂ O | 1.81 | 50. | 15 | — | — | — |
| Chlorine dioxide..... | ClO ₂ | — | -76. | 3 | 9.9 | 731 | 21 |
| Chrome alum..... | KCr(SO ₄) ₂ + 12H ₂ O | 1.83 | 89. | 16 | — | — | — |
| “ nitrate..... | Cr ₂ (NO ₃) ₆ + 18H ₂ O | — | 37. | 2 | 170. | 760 | 2 |
| Chromium oxide..... | Cr ₂ O ₃ | 5.04 | 1990. | 28 | — | — | — |
| Cobalt sulphate..... | CoSO ₄ | 3.53 | 97. | 16 | 880.* | — | — |
| Cupric chloride..... | CuCl ₂ | 3.05 | 498. | 9 | * | — | — |
| Cuprous chloride..... | Cu ₂ Cl ₂ | 3.7 | 421. | — | 1000 ± | 760 | 9 |
| Cupric nitrate..... | Cu(NO ₃) ₂ + 3H ₂ O | 2.05 | 114.5 | 2 | 170.* | 760 | 2 |
| Hydrobromic acid..... | HBr | — | -80.7 | 3 | -68.7 | 760 | — |
| Hydrochloric acid..... | HCl | — | -111.3 | 17 | -83.1 | 755 | 17 |
| Hydrofluoric acid..... | HF | 0.99 | -92.3 | 6 | -36.7 | 755 | 17 |
| Hydriodic acid..... | HI | — | -51.3 | 17 | -35.7 | 760 | — |
| Hydrogen peroxide..... | H ₂ O ₂ | 1.5 | -2. | 18 | 80.2 | 47 | 20 |
| “ phosphide..... | PH ₃ | — | -132.5 | 6 | — | — | — |
| “ sulphide..... | H ₂ S | — | -86. | 3 | -62. | — | — |
| Iron chloride..... | FeCl ₃ | 2.80 | 301. | — | — | — | — |
| “ nitrate..... | Fe(NO ₃) ₃ + 9H ₂ O | 1.68 | 47.2 | 2 | — | — | — |
| “ sulphate..... | FeSO ₄ + 7H ₂ O | 1.90 | 64. | 16 | — | — | — |
| Lead chloride..... | PbCl ₂ | 5.8 | 500. | 9 | 900 ± | 760 | — |
| “ metaphosphate..... | Pb(PO ₃) ₂ | — | 800. | 9 | — | — | — |
| Magnesium chloride..... | MgCl ₂ | 2.18 | 708. | 9 | — | — | — |
| “ oxide..... | MgO | 3.4 | 2800. | 28 | — | — | — |
| “ nitrate..... | Mg(NO ₃) ₂ + 6H ₂ O | 1.46 | 90. | 2 | 143. | 760 | 2 |
| “ sulphate..... | MgSO ₄ + 5H ₂ O | 1.68 | 150. | 16 | — | — | — |
| Manganese chloride..... | MnCl ₂ + 4H ₂ O | 2.01 | 87.5 | 19 | 106. | 760 | 19 |
| “ nitrate..... | Mn(NO ₃) ₂ + 6H ₂ O | 1.82 | 26. | 2 | 129. | 760 | 2 |
| “ sulphate..... | MnSO ₄ + 5H ₂ O | 2.09 | 54. | 16 | — | — | — |
| Mercurous chloride..... | Hg ₂ Cl ₂ | 7.10 | 450 ± | — | — | — | — |
| Mercuric chloride..... | HgCl ₂ | 5.42 | 282. | — | 305. | — | — |

(1) Friedel and Crafts; (2) Ordway; (3) Faraday; (4) Marchand; (5) Amat; (6) Olszewski; (7) Gibbs; (8) Baskerville; (9) Carnelly; (10) Carnelly and O'Shea; (11) Ruff; (12) Wroblewski and Olszewski; (13) Anschutz; (14) Roscoe; (15) Tilden; (16) Ladenburg; (17) Stadel; (18) Clarke, Const. of Nature; (19) Bruhl; (20) Schacherl; (21) Tammann; (22) Thorpe; (23) Ramsay; (24) Lorenz; (25) Morgan; (26) Day; (27) Kanolt.

* Decomposes.

DENSITIES AND MELTING AND BOILING POINTS OF INORGANIC COMPOUNDS

| Substance. | Chemical formula. | Density, about 20° C | Melting point C | Authority. | Boiling point C | Pressure mm | Authority. |
|-----------------------------------|--|----------------------------|-----------------------|------------|-----------------------|----------------|------------|
| Nickel carbonyl | NiC ₄ O ₄ | 1.32 | -25. | 1 | 43.° | 760 | — |
| “ nitrate | Ni(NO ₃) ₂ + 6H ₂ O | 2.05 | 56.7 | 2 | 136.7 | 760 | 2 |
| “ oxide | NiO | 6.69 | — | — | — | — | — |
| “ sulphate | NiSO ₄ + 7H ₂ O | 1.98 | 99. | 3 | — | — | — |
| Nitric acid | HNO ₃ | 1.52 | -42. | 4 | 86. | 760 | 16 |
| “ anhydride | N ₂ O ₅ | 1.64 | 30. | 5 | 48. | 760 | 9 |
| “ oxide * | NO | 1.27 | -167. | — | -153. | 760 | 6 |
| “ peroxide | N ₂ O ₄ | 1.49 | -9.6 | 8 | 21.6 | 760 | — |
| Nitrous anhydride | N ₂ O ₃ | 1.45 | -111. | 7 | 3.5 | 760 | — |
| “ oxide | N ₂ O | — | -102.4 | 8 | -89.8 | 760 | 8 |
| Phosphoric acid (ortho) | H ₃ PO ₄ | 1.88 | 40 ± | — | — | — | — |
| Phosphorous acid | H ₃ PO ₃ | 1.65 | 72. | — | — | — | — |
| Phosphorus trichloride | PCl ₃ | 1.61 | -111.8 | 10 | 76. | 760 | 19 |
| “ oxychloride | POCl ₃ | 1.68 | +1.3 | — | 108. | 760 | — |
| “ disulphide | P ₂ S ₆ | — | 297. | 12 | — | 760 | — |
| “ pentasulphide | P ₂ S ₅ | — | 275. | 13 | 522. | 760 | — |
| “ sesquisulphide | P ₄ S ₃ | 2.00 | 168. | — | 400. | 760 | — |
| “ trisulphide | P ₂ S ₃ | — | 290 ± | 14 | 490. | 760 | 25 |
| Potassium carbonate | K ₂ CO ₃ | 2.29 | 909. | — | — | — | — |
| “ chlorate | KClO ₃ | 2.34 | 357. | 15 | — | — | — |
| “ chromate | K ₂ CrO ₄ | 2.72 | 975. | 17 | — | — | — |
| “ cyanide | KCN | 1.52 | red h't | — | — | — | — |
| “ perchlorate | KClO ₄ | 2.52 | 610. | 15 | 410.† | 760 | — |
| “ chloride | KCl | 1.99 | 772. | — | 1500. | 760 | — |
| “ nitrate | KNO ₃ | 2.10 | 341. | — | 400.† | — | — |
| “ acid phosphate | KH ₂ PO ₄ | 2.34 | 96. | 3 | — | — | — |
| “ acid sulphate | KHSO ₄ | 2.35 | 205. | — | dec. | — | — |
| Silver chloride | AgCl | 5.56 | 451. | 15 | — | — | — |
| “ nitrate | AgNO ₃ | 4.35 | 218. | — | dec. | — | — |
| “ perchlorate | AgClO ₄ | — | 486. | 18 | — | — | — |
| “ phosphate | Ag ₃ PO ₄ | 6.37 | 849. | 15 | — | — | — |
| “ metaphosphate | AgPO ₃ | — | 482. | 15 | — | — | — |
| “ sulphate | Ag ₂ SO ₄ | 5.45 | 655 ± | — | 1085.† | — | — |
| Sodium chloride | NaCl | 2.17 | 800. | 11 | 1490. | 760 | — |
| “ hydroxide | NaOH | 2.1 | 318. | 27 | — | — | — |
| “ nitrate | NaNO ₃ | 2.26 | 315. | — | 380.† | — | — |
| “ chlorate | NaClO ₃ | 2.48 | 248. | 28 | † | — | — |
| “ perchlorate | NaClO ₄ | — | 482. | 18 | — | — | — |
| “ carbonate | Na ₂ CO ₃ | 2.48 | 852. | — | † | — | — |
| “ carbonate | Na ₂ CO ₃ + 10H ₂ O | 1.46 | 34. | 3 | — | — | — |
| “ phosphate | Na ₂ HPO ₄ + 12H ₂ O | 1.54 | 38. | — | — | — | — |
| “ metaphosphate | NaPO ₃ | 2.48 | 617. | 15 | — | — | — |
| “ pyrophosphate | Na ₄ P ₂ O ₇ | 2.45 | 970. | 30 | — | — | — |
| “ phosphite | (H ₂ NaPO ₃) ₂ + 5H ₂ O | — | 42. | 20 | — | — | — |
| “ sulphate | Na ₂ SO ₄ | 2.67 | 884. | 11 | — | — | — |
| “ sulphate | Na ₂ SO ₄ + 10H ₂ O | 1.46 | 32.38 | 17 | — | — | — |
| “ hyposulphite | Na ₂ S ₂ O ₃ + 5H ₂ O | 1.73 | 48.16 | — | † | — | — |
| Sulphur dioxide | SO ₂ | — | -76. | — | -10. | 760 | — |
| Sulphuric acid | H ₂ SO ₄ | 1.83 | 10.4 | 21 | 338. | 760 | 22 |
| “ acid | 12H ₂ SO ₄ + H ₂ O | — | -0.5 | 22 | — | — | — |
| “ acid | H ₂ SO ₄ + H ₂ O | — | 8.5 | — | — | — | — |
| “ acid (pyro) | H ₂ S ₂ O ₇ | 1.89 | 35. | 22 | † | — | — |
| Sulphur trioxide | SO ₃ | 1.91 | 16.8 | — | 44.9 | 760 | — |
| Tin, stannic chloride | SnCl ₄ | 2.28 | -33. | 23 | 114. | 760 | 19 |
| “ stannous chloride | SnCl ₂ | — | 250. | 24 | 605. | 760 | — |
| Zinc chloride | ZnCl ₂ | 2.91 | 305. | 29 | 710. | 760 | — |
| “ chloride | ZnCl ₂ + 3H ₂ O | — | 6.5 | 26 | — | — | — |
| “ nitrate | Zn(NO ₃) ₂ + 6H ₂ O | 2.06 | 36.4 | 3 | 131. | 760 | 2 |
| “ sulphate | ZnSO ₄ + 7H ₂ O | 2.02 | 50. | 3 | — | — | — |

References: (1) Mond, Langer, Quincke; (2) Ordway; (3) Tilden; (4) Erdmann; (5) R. Weber; (6) Olszewski; (7) Birhauss; (8) Ramsay; (9) Deville; (10) Wroblewski; (11) Day, Sosman, White; (12) Ramme; (13) Meyer; (14) Lemoine; (15) Carnelly; (16) Mitscherlich; (17) LeChatelier; (18) Carnelly, O'Shea; (19) Thorpe; (20) Amat; (21) Mendelejeff; (22) Marignac; (23) Besson; (24) Clarke, Const. of Nature; (25) Isambert; (26) Mylius; (27) Hevesy; (28) Retgers; (29) Grünauer; (30) Richards and others.

* Under pressure 138 mm mercury. † Decomposes.

DENSITIES AND MELTING AND BOILING POINTS OF ORGANIC COMPOUNDS

| Substance | Chemical formula | Temp. °C | Density | Melting point | Boiling point | Authority or pressure for boiling point if not 760 mm |
|--|------------------|----------|---------|---------------|---------------|---|
| (a) Paraffin Series: C_nH_{2n+2} . Normal compounds only | | | | | | |
| Methane..... | CH_4 | -164 | 0.415 | -184 | -161.4 | |
| Ethane..... | C_2H_6 | -88 | .546 | -172.0 | -88.3 | |
| Propane..... | C_3H_8 | -44 | .595 | -189.9 | -44.5 | |
| Butane..... | C_4H_{10} | 0 | .601 I | -135.0 | + 0.6 | |
| Pentane..... | C_5H_{12} | 20 | .631 | -131.5 | + 36.2 | |
| Hexane..... | C_6H_{14} | 20 | .660 | -94.3 | 69.0 | |
| Heptane..... | C_7H_{16} | 20 | .684 | -90.0 | 98.4 | |
| Octane..... | C_8H_{18} | 17 | .707 | -56.5 | 124.6 | |
| Nonane..... | C_9H_{20} | 20 | .718 | -51 | 150.6 | |
| Decane..... | $C_{10}H_{22}$ | 20 | .747 | -32.0 | 174 | |
| Undecane..... | $C_{11}H_{24}$ | 20 | .741 | -26.5 | 197 | |
| Dodecane..... | $C_{12}H_{26}$ | 20 | .768 | -12 | 216 | |
| Tridecane..... | $C_{13}H_{28}$ | 20 | .757 | -6.2 | 234 | |
| Tetradecane..... | $C_{14}H_{30}$ | 20 | .765 | + 5.5 | 252.5 | |
| Pentadecane..... | $C_{15}H_{32}$ | 20 | .772 | + 10 | 270.5 | |
| Hexadecane..... | $C_{16}H_{34}$ | 20 | .775 | 20 | 287.5 | |
| Heptadecane..... | $C_{17}H_{36}$ | 20 | .778 | 22.5 | 303 | |
| Octadecane..... | $C_{18}H_{38}$ | 20 | .777 | 28 | 317 | |
| Nonadecane..... | $C_{19}H_{40}$ | 32 | .777 | 32 | 330 | |
| Eicosane..... | $C_{20}H_{42}$ | 37 | .778 | 38 | 305 | 15 mm |
| Heneicosane..... | $C_{21}H_{44}$ | 45 | .775 | 40.4 | 215 | 15 mm |
| Docosane..... | $C_{22}H_{46}$ | 44 | .778 | 44.4 | 224.5 | 15 mm |
| Tricosane..... | $C_{23}H_{48}$ | 48 | .779 | 47.7 | 320.7 | |
| Tetracosane..... | $C_{24}H_{50}$ | 61 | .779 | 54 | 324 | |
| Pentacosane..... | $C_{25}H_{52}$ | 20 | .779 | 54 | 284 | 40 mm |
| Hexacosane..... | $C_{26}H_{54}$ | 20 | .779 | 60 | 296 | 40 mm |
| Heptacosane..... | $C_{27}H_{56}$ | 60 | .779 | 59.5 | 270 | 15 mm |
| Octacosane..... | $C_{28}H_{58}$ | 20 | .779 | 65 | 318 | 40 mm |
| Nonacosane..... | $C_{29}H_{60}$ | 20 | .780 | 63.6 | 348 | 40 mm |
| Triacontane..... | $C_{30}H_{62}$ | 20 | .780 | 70 | 235 | 1.0 mm |
| Hentriacontane..... | $C_{31}H_{64}$ | 68 | .781 | 68.1 | 302 | 15 mm |
| Dotriacontane..... | $C_{32}H_{66}$ | 79 | .775 | 75 | 310 | 15 mm |
| Tetraatriacontane..... | $C_{34}H_{70}$ | 20 | .781 | 76.5 | 255 | 1.0 mm |
| Pentatriacontane..... | $C_{35}H_{72}$ | 75 | .782 | 74.7 | 331 | 15 mm |
| Hexatriacontane..... | $C_{36}H_{74}$ | 76 | .782 | 76.5 | 265 | 1.0 mm |
| (b) Olefines or the Ethylene Series: C_nH_{2n} . Normal compounds only | | | | | | |
| Ethylene..... | C_2H_4 | -102 | .566 | -169.4 | -103.8 | |
| Propylene..... | C_3H_6 | -47 | .609 | -185.2 | -47.0 | |
| Butylene..... | C_4H_8 | -13.5 | .635 | | | Sieben |
| Amylene..... | C_5H_{10} | 20 | .651 | -139 | + 36.4 | |
| Hexylene..... | C_6H_{12} | 0 | .76 | | 69 | Wreden or Znatowicz |
| Heptylene..... | C_7H_{14} | 20 | .703 | | 96-99 | Morgan or Schorlemmer |
| Octylene..... | C_8H_{16} | 17 | .722 | | 123 | Möslinger |
| Nonylene..... | C_9H_{18} | 15 | .754 | | 149.9 | |
| Decylene..... | $C_{10}H_{20}$ | 0 | .763 | | 172 | |
| Undecylene..... | $C_{11}H_{22}$ | 20 | .763 | | 188 | |
| Dodecylene..... | $C_{12}H_{24}$ | 15 | .762 | -31.5 | 96 | 15 mm |
| Tridecylene..... | $C_{13}H_{26}$ | 0 | .845 | | 232.7 | |
| Tetradecylene..... | $C_{14}H_{28}$ | 20 | .775 | -12 | 246 | |
| Pentadecylene..... | $C_{15}H_{30}$ | | .814 | | 247 | Bernthsen |
| Hexadecylene..... | $C_{16}H_{32}$ | 20 | .789 | + 4 | 274 | |
| Octadecylene..... | $C_{18}H_{36}$ | 20 | .791 | + 18 | 179 | 15 mm |
| Eicosylene..... | $C_{20}H_{40}$ | 0 | .871 | | 395 | Beilstein |
| Cerotene..... | $C_{27}H_{54}$ | | | 58 | | Bernthsen |
| Melene..... | $C_{30}H_{60}$ | 20 | .890 | 63 | 380 | |

DENSITIES AND MELTING AND BOILING POINTS OF ORGANIC COMPOUNDS

| Substance | Chemical formula | Temp. °C | Density | Melting point | Boiling point | Authority or pressure for boiling point if not 760 mm |
|---|------------------|----------|---------|---------------|---------------|---|
| (c) Acetylene Series: C_nH_{2n-2} . Normal compounds only | | | | | | |
| Acetylene..... | C_2H_2 | -80 | .613 | - 81.8 | - 83.6 | Villard |
| Allylene..... | C_3H_4 | -13 | .660 | -104.7 | - 27.5 | |
| Ethylacetylene.... | C_4H_6 | 0 | .668 | -130 | + 18.5 | |
| Propylacetylene.... | C_5H_8 | 0 | .722 | - 95 | + 40 | |
| Butylacetylene.... | C_6H_{10} | | | -150 | 71.5 | |
| Amylacetylene.... | C_7H_{12} | 13 | .738 | - 70 | 110.5 | |
| Hexylacetylene.... | C_8H_{14} | 0 | .770 | | 125 | |
| Undecylidene..... | | | | | 213 | Bruylant |
| Dodecylidene..... | | - 9 | .810 | - 9 | 105 | Krafft, 15 mm |
| Tetradecylidene.... | | + 6.5 | .806 | + 6.5 | 134 | " " " |
| Hexadecylidene.... | | 20 | .804 | 20 | 160 | " " " |
| Octadecylidene.... | | 30 | .802 | 30 | 184 | " " " |
| (d) Monatomic alcohols: $C_nH_{2n+1}OH$. Normal compounds only | | | | | | |
| Methyl alcohol.... | CH_3OH | 20 | .792 | - 97.8 | 64.5 | |
| Ethyl alcohol.... | C_2H_5OH | 20 | .789 | -117.3 | 78.5 | |
| Propyl alcohol.... | C_3H_7OH | 20 | .804 | -127 | 97.8 | |
| Butyl alcohol.... | C_4H_9OH | 20 | .810 | - 89.8 | 117.7 | |
| Amyl alcohol.... | $C_5H_{11}OH$ | 20 | .817 | - 78.5 | 137.9 | |
| Hexyl alcohol.... | $C_6H_{13}OH$ | 20 | .820 | - 51.6 | 155.8 | |
| Heptyl alcohol.... | $C_7H_{15}OH$ | 22 | .817 | - 34.6 | 175.8 | |
| Octyl alcohol.... | $C_8H_{17}OH$ | 20 | .827 | - 16.3 | 194 | |
| Nonyl alcohol.... | $C_9H_{19}OH$ | 20 | .828 | - 5 | 215 | |
| Decyl alcohol.... | $C_{10}H_{21}OH$ | 20 | .829 | + 7 | 231 | |
| Undecyl alcohol.... | $C_{11}H_{23}OH$ | 20 | .833 | + 19 | 146 | 30 mm |
| Dodecyl alcohol.... | $C_{12}H_{25}OH$ | 20 | .831 | 24 | 259 | |
| Tridecyl alcohol.... | $C_{13}H_{27}OH$ | 31 | .822 | 30.5 | 156 | 15 mm |
| Tetradecyl alcohol.... | $C_{14}H_{29}OH$ | 38 | .824 | 38 | 167 | 15 mm |
| Pentadecyl alcohol.... | $C_{15}H_{31}OH$ | | | 46 | | |
| Cetyl alcohol..... | $C_{16}H_{33}OH$ | 79 | .798 | 49.3 | 344 | |
| Octadecyl alcohol.... | $C_{18}H_{37}OH$ | 59 | .812 | 58.5 | 210.5 | 15 mm |
| (e) Alcoholic ethers: $C_nH_{2n+2}O$ | | | | | | |
| Dimethyl ether.... | C_2H_6O | 20 | .6606 | -138 | - 24.9 | |
| Diethyl ether.... | $C_4H_{10}O$ | 20 | .714 | -116.3 | + 34.5 | β -123.3 b. pt. |
| Dipropyl ether.... | $C_6H_{14}O$ | 20 | .747 | -122 | 89 | |
| Di-n-butyl ether.... | $C_8H_{18}O$ | 20 | .769 | | 149 | |
| Di-sec-butyl ether.. | " | 21 | .756 | | 121 | |
| Di-iso-butyl ether.. | " | 20 | .762 | | 122.5 | |
| Diamyl ether..... | $C_{10}H_{22}O$ | 20 | .774 | | 190 | |
| Di-iso-amyl ether.. | " | 12 | .783 | | 172.2 | |
| Diethyl ether..... | $C_{12}H_{26}O$ | | | | 208.8 | |
| Diheptyl ether.... | $C_{14}H_{30}O$ | 0 | .815 | | 260 | |
| Diocetyl ether..... | $C_{16}H_{34}O$ | 0 | .820 | | 291.8 | |
| (f) Ethyl ethers: $C_nH_{2n+2}O$ | | | | | | |
| Ethyl-methyl..... | C_3H_8O | 20 | .697 | | + 7.9 | |
| " -propyl..... | $C_6H_{12}O$ | 20 | .732 | < -79 | 61.4 | |
| " -isopropyl..... | " | 0 | .745 | | 54 | |
| " -n. butyl..... | $C_6H_{14}O$ | 20 | .752 | | 91.4 | |
| " -iso-butyl..... | " | 20 | .751 | | 80 | |
| " -iso-amyl..... | $C_7H_{16}O$ | 18 | .764 | | 112 | |
| " -n. hexyl..... | $C_8H_{18}O$ | | | | 137 | |
| " -n. heptyl..... | $C_9H_{20}O$ | 16 | .790 | | 166.6 | |
| " -n. octyl..... | $C_{10}H_{22}O$ | 17 | .794 | | 183 | |

Where no reference is given the data were compiled from the International Critical Tables.

DENSITIES AND MELTING AND BOILING POINTS OF ORGANIC COMPOUNDS

(g) MISCELLANEOUS

| Substance | Chemical formula. | Density and temperature. | | Melting point C | Boiling point C | Authority. |
|--------------------|--|--------------------------|-----|-----------------|-----------------|---------------------------------|
| Acetic acid | CH_3COOH | 1.115 | 0° | 16.7 | 118.5 | Young, '09 |
| Acetone | CH_3COCH_3 | 0.812 | 0 | -94.6 | 56.1 | |
| Aldehyde | $\text{C}_2\text{H}_4\text{O}$ | 0.806 | 0 | -120. | +20.8 | |
| Aniline | $\text{C}_6\text{H}_5\text{NH}_2$ | 1.038 | 0 | -8. | 183.9 | |
| Beeswax | | 0.96 ± | | 62. | | Richards Holborn- Henning |
| Benzoic acid | $\text{C}_7\text{H}_6\text{O}_2$ | 1.293 | 4 | 121. | 249. | |
| Benzene | C_6H_6 | 0.879 | 20 | 5.48 | 80.2 | |
| Benzophenone | $(\text{C}_6\text{H}_5)_2\text{CO}$ | 1.090 | 50 | 48. | 305.9 | |
| Butter | | 0.86-7 | | 30 ± | | |
| Camphor | $\text{C}_{10}\text{H}_{16}\text{O}$ | 0.99 | 10 | 176. | 209. | Young |
| Carbolic acid | $\text{C}_6\text{H}_5\text{OH}$ | 1.060 | 21 | 43. | 182. | |
| Carbon bisulphide | CS_2 | 1.292 | 0 | -110. | 46.2 | |
| “ tetrachloride | CCl_4 | 1.582 | 21 | -30. | 76.7 | |
| Chlorbenzene | $\text{C}_6\text{H}_5\text{Cl}$ | 1.111 | 15 | -40. | 132. | |
| Chloroform | CHCl_3 | 1.4989 | 15 | -63.3 | 61.2 | |
| Cyanogen | C_2N_2 | — | | -35. | -21. | |
| Ethyl bromide | $\text{C}_2\text{H}_5\text{Br}$ | 1.45 | 15 | -117. | 38.4 | |
| “ chloride | $\text{C}_2\text{H}_5\text{Cl}$ | 0.918 | 8 | -141.6 | 14. | |
| “ ether | $\text{C}_4\text{H}_{10}\text{O}$ | 0.736 | 0 | -118. | 34.6 | |
| “ iodide | $\text{C}_2\text{H}_5\text{I}$ | 1.944 | 14 | — | 72. | Holborn- Henning |
| Formic acid | HCOOH | 1.242 | 0 | 8.6 | 100.8 | |
| Gasolene | | 0.68 ± | | — | 70-90 | |
| Glucose | $\text{CHO}(\text{HCOH})_4\text{CH}_2\text{OH}$ | 1.56 | | 146. | — | |
| Glycerine | $\text{C}_3\text{H}_5\text{O}_3$ | 1.269 | 0 | 20. | 290. | |
| Iodoform | CHI_3 | 4.01 | 25 | 119. | — | |
| Lard | | | | 29 ± | — | |
| Methyl chloride | CH_3Cl | 0.902 | -24 | -103.6 | -24.1 | |
| Methyl iodide | CH_3I | 2.285 | 15 | -64. | 42.3 | |
| Naphthalene | C_{10}H_8 | 1.152 | 15 | 80. | 218. | |
| Nitrobenzene | $\text{C}_6\text{H}_5\text{O}_2\text{N}$ | 1.212 | 7.5 | 5. | 211. | Richards |
| Nitroglycerine | $\text{C}_3\text{H}_5\text{N}_3\text{O}_9$ | 1.60 | | — | — | |
| Olive oil | | 0.92 | | 20 ± | 300 ± | |
| Oxalic acid | $\text{C}_2\text{H}_2\text{O}_4 \cdot 2\text{H}_2\text{O}$ | 1.68 | | 190. | — | |
| Paraffin wax, soft | | — | | 38-52 | 350-390 | |
| “ hard | | — | | 52-56 | 390-430 | |
| Pyrogallol | $\text{C}_6\text{H}_3(\text{OH})_3$ | 1.46 | 40 | 133. | 293. | |
| Spermaceti | | 0.95 | 15 | 45 ± | — | |
| Starch | $\text{C}_6\text{H}_{10}\text{O}_5$ | 1.56 | | none | — | |
| Sugar, cane | $\text{C}_{12}\text{H}_{22}\text{O}_{11}$ | 1.588 | 20 | 160. | — | |
| Stearine | $(\text{C}_{15}\text{H}_{35}\text{O}_2)_3\text{C}_3\text{H}_5$ | 0.925 | 65 | 71. | — | Richards |
| Tallow, beef | | 0.94 | 15 | 27-38 | — | |
| “ mutton | | 0.94 | 15 | 32-41 | — | |
| Tartaric acid | $\text{C}_4\text{H}_6\text{O}_6$ | 1.754 | | 170. | — | |
| Toluene | $\text{C}_6\text{H}_5\text{CH}_3$ | 0.882 | 00 | -92. | 110.31 | |
| Xylene (o) | $\text{C}_6\text{H}_4(\text{CH}_3)_2$ | 0.863 | 20 | -28. | 142. | |
| “ (m) | $\text{C}_6\text{H}_4(\text{CH}_3)_2$ | 0.864 | 20 | 54. | 140. | Richards |
| “ (p) | $\text{C}_6\text{H}_4(\text{CH}_3)_2$ | 0.861 | 20 | 15. | 138. | |

MELTING POINTS

TABLE 241.—Melting Point of Mixtures of Metals

| Metals. | Melting-points, °C | | | | | | | | | | | Reference. | |
|---------|---------------------------------------|------|------|------|------|------|------|------|------|------|------|------------|----|
| | Percentage of metal in second column. | | | | | | | | | | | | |
| | 0% | 10% | 20% | 30% | 40% | 50% | 60% | 70% | 80% | 90% | 100% | | |
| Pb. Sn. | 326 | 295 | 276 | 262 | 240 | 220 | 190 | 185 | 200 | 216 | 232 | 1 | |
| Bi. | 322 | 290 | — | — | 179 | 145 | 126 | 168 | 205 | — | 268 | 7 | |
| Te. | 322 | 710 | 790 | 880 | 917 | 760 | 600 | 480 | 410 | 425 | 446 | 8 | |
| Ag. | 328 | 460 | 545 | 590 | 620 | 650 | 705 | 775 | 840 | 905 | 959 | 9 | |
| Na. | — | 300 | 420 | 400 | 370 | 330 | 290 | 250 | 200 | 130 | 96 | 13 | |
| Cu. | 326 | 870 | 920 | 925 | 945 | 950 | 953 | 985 | 1005 | 1020 | 1084 | 2 | |
| Sb. | 326 | 250 | 275 | 330 | 395 | 440 | 499 | 525 | 560 | 600 | 632 | 16 | |
| Al. | 650 | 750 | 840 | 925 | 945 | 950 | 970 | 1000 | 1040 | 1010 | 632 | 17 | |
| Cu. | 650 | 630 | 600 | 560 | 540 | 580 | 610 | 755 | 930 | 1055 | 1084 | 18 | |
| Au. | 655 | 675 | 740 | 800 | 855 | 915 | 970 | 1025 | 1055 | 675 | 1062 | 10 | |
| Ag. | 650 | 625 | 615 | 600 | 590 | 580 | 575 | 570 | 650 | 750 | 954 | 17 | |
| Zn. | 654 | 640 | 620 | 600 | 580 | 560 | 530 | 510 | 475 | 425 | 410 | 11 | |
| Fe. | 653 | 860 | 1015 | 1110 | 1145 | 1145 | 1220 | 1315 | 1425 | 1500 | 1515 | 3 | |
| Sn. | 650 | 645 | 635 | 625 | 620 | 605 | 590 | 570 | 560 | 540 | 232 | 17 | |
| Sb. | 632 | 610 | 590 | 575 | 555 | 540 | 520 | 470 | 465 | 330 | 268 | 16 | |
| Ag. | 630 | 595 | 570 | 545 | 520 | 500 | 505 | 545 | 680 | 850 | 950 | 9 | |
| Sn. | 622 | 600 | 570 | 525 | 480 | 430 | 395 | 350 | 310 | 255 | 232 | 19 | |
| Zn. | 632 | 555 | 510 | 540 | 570 | 565 | 540 | 525 | 510 | 470 | 419 | 17 | |
| Ni. | Sn. | 1455 | 1380 | 1290 | 1200 | 1235 | 1290 | 1305 | 1230 | 1060 | 800 | 232 | 17 |
| Na. | Bi. | 96 | 425 | 520 | 590 | 645 | 690 | 720 | 730 | 715 | 570 | 268 | 13 |
| Cd. | Cd. | 96 | 125 | 135 | 245 | 285 | 325 | 330 | 340 | 360 | 390 | 322 | 13 |
| Ag. | 322 | 420 | 520 | 610 | 700 | 760 | 805 | 850 | 805 | 940 | 954 | 17 | |
| Tl. | 321 | 300 | 285 | 270 | 262 | 258 | 245 | 230 | 210 | 235 | 302 | 14 | |
| Zn. | 322 | 280 | 270 | 295 | 313 | 327 | 340 | 355 | 370 | 390 | 419 | 11 | |
| Au. | Cu. | 1053 | 910 | 890 | 895 | 905 | 925 | 975 | 1000 | 1025 | 1060 | 1084 | 4 |
| Ag. | Ag. | 1064 | 1062 | 1061 | 1055 | 1054 | 1049 | 1039 | 1025 | 1006 | 982 | 963 | 5 |
| Pt. | 1075 | 1125 | 1190 | 1250 | 1320 | 1380 | 1455 | 1530 | 1610 | 1685 | 1775 | 20 | 15 |
| K. | Na. | 62 | 17.5 | — | —3.5 | 5 | 11 | 26 | 41 | 58 | 77 | 97.5 | 15 |
| Hg. | — | — | — | — | — | — | 90 | 110 | 135 | 162 | 265 | — | 13 |
| Tl. | 62.5 | 133 | 165 | 188 | 205 | 215 | 220 | 240 | 280 | 305 | 301 | 14 | 14 |
| Cu. | Ni. | 1080 | 1180 | 1240 | 1290 | 1320 | 1335 | 1380 | 1410 | 1430 | 1440 | 1455 | 17 |
| Ag. | Ag. | 1082 | 1035 | 990 | 945 | 910 | 870 | 830 | 788 | 814 | 875 | 960 | 9 |
| Sn. | 1084 | 1005 | 890 | 755 | 725 | 680 | 630 | 580 | 530 | 440 | 232 | 12 | 12 |
| Zn. | 1084 | 1040 | 995 | 930 | 900 | 880 | 820 | 780 | 700 | 580 | 419 | 6 | 6 |
| Ag. | Zn. | 959 | 850 | 755 | 705 | 690 | 660 | 630 | 610 | 570 | 505 | 419 | 11 |
| Sn. | 959 | 870 | 750 | 630 | 550 | 495 | 450 | 420 | 375 | 300 | 232 | 9 | 9 |
| Na. | Hg. | 97.5 | 90 | 80 | 70 | 60 | 45 | 22 | 55 | 95 | 215 | — | 13 |

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TABLE 242.—Melting Point of Alloys of Lead, Tin, and Bismuth

| | Per cent. | | | | | | | | |
|-------------------|-----------|------|------|------|------|------|------|------|------|
| Lead | 32.0 | 25.8 | 25.0 | 43.0 | 33.3 | 10.7 | 50.0 | 35.8 | 20.0 |
| Tin | 15.5 | 19.8 | 15.0 | 14.0 | 33.3 | 23.1 | 33.0 | 52.1 | 60.0 |
| Bismuth | 52.5 | 54.4 | 60.0 | 43.0 | 33.3 | 66.2 | 17.0 | 12.1 | 20.0 |
| Solidification at | 96° | 101° | 125° | 128° | 145° | 148° | 161° | 181° | 234° |

Charpy, Soc. d'Encours, Paris, 1901.

TABLE 243.—Melting Point of Low-melting-point Alloys

| | Per cent. | | | | | | |
|-------------------|-----------|-------|-------|-------|-------|-------|------|
| Cadmium | 10.8 | 10.2 | 14.8 | 13.1 | 6.2 | 7.1 | 6.7 |
| Tin | 14.2 | 14.3 | 7.0 | 13.8 | 9.4 | — | — |
| Lead | 24.9 | 25.1 | 26.0 | 24.3 | 34.4 | 39.7 | 43.4 |
| Bismuth | 50.1 | 50.4 | 52.2 | 48.8 | 50.0 | 53.2 | 49.9 |
| Solidification at | 65.5° | 67.5° | 68.5° | 68.5° | 76.5° | 89.5° | 95° |

Drewitz, Diss. Rostock, 1902.

All compiled from Landolt-Börnstein-Meyerhoffer's Physikalisch-chemische Tabellen.

MELTING POINT OF SOME REFRACTORY SUBSTANCES

(Compiled by F. C. Kracke, Geophysical Laboratory, Carnegie Institution, 1930.)

Symbols: m, melting point; r, reaction temperature, resulting in the break up of a compound into another and liquid; d, compound decomposes before melting with evolution of gas; vac, melting in vacuo.

| Compound | t°C | Type | Ref. | Compound | t°C | Type | Ref. |
|---|-----------|------|--------|---|-----------|------|--------|
| Al ₂ O ₃ | 2050 ± 10 | m | 22 | BINARY ALUMINATES | | | |
| BN..... | 1240 | d | 37 | 3CaO.Al ₂ O ₃ | 1535 ± 5 | r | 9 |
| BaO..... | 1923 ± 10 | m | 36 | 5CaO.3Al ₂ O ₃ | 1455 ± 5 | m | 9 |
| BeO..... | 2400 ± 50 | m | 34 | CaO.Al ₂ O ₃ | 1600 ± 5 | m | 9 |
| CaO..... | 2572 ± 10 | m | 36 | 3CaO.5Al ₂ O ₃ | 1720 ± 10 | m | 9 |
| Ce ₂ O ₃ | 1692 | m | 14 | Li ₂ O.Al ₂ O ₃ | > 1625 | m | 18 |
| FeO?..... | 1419 | vac | 15 | MgO.Al ₂ O ₃ | 2135 ± 20 | m | 32 |
| Fe ₂ O ₃ | 1560 | d | 15 | Na ₂ O.Al ₂ O ₃ | 1650 | m | 25 |
| Fe ₃ O ₄ | 1540 | d | 15 | ALUMINO-SILICATES | | | |
| La ₂ O ₃ | > 2000 | m | 39 | BaO.Al ₂ O ₃ .2SiO ₂ ... | > 1700 | .. | 11 |
| Li ₂ O..... | > 1650 | m | 19 | 2CaO.Al ₂ O ₃ .SiO ₂ ... | 1590 ± 2 | m | 13, 32 |
| MgO..... | 2800 ± 20 | m | 22, 34 | CaO.Al ₂ O ₃ .2SiO ₂ ... | 1550 ± 2 | m | 9 |
| MnO..... | > 1650 | vac | 39 | K ₂ O.Al ₂ O ₃ .2SiO ₂ ... | > 1755 | m | 4 |
| PbO..... | 888 ± 10 | m | 8 | K ₂ O.Al ₂ O ₃ .4SiO ₂ ... | 1686 ± 5 | m | 6 |
| SiO ₂ | 1713 ± 10 | m | 12, 16 | K ₂ O.Al ₂ O ₃ .6SiO ₂ ... | 1170 | r | 27 |
| SrO..... | 2430 ± 10 | m | 36 | Li ₂ O.Al ₂ O ₃ .2SiO ₂ ... | 1388 ± 5 | m | 18 |
| ThO ₂ | 3050 ± 25 | m | 35 | Li ₂ O.Al ₂ O ₃ .4SiO ₂ ... | 1400 ± 3 | m | 18 |
| TiO ₂ | < 1640 | d | 39 | Na ₂ O.Al ₂ O ₃ .2SiO ₂ ... | 1526 ± 2 | m | 4 |
| Yt ₂ O ₃ | 2410 | m | 34 | Na ₂ O.Al ₂ O ₃ .6SiO ₂ ... | 1100 ± 10 | m | 4 |
| ZnO..... | 1975 ± 25 | m | 7 | SrO.Al ₂ O ₃ .2SiO ₂ ... | > 1700 | m | 11 |
| ZrO ₂ | 2690 | m | 40 | 2SiO ₂ .3Al ₂ O ₃ | 1810 ± 10 | r | 5 |
| BINARY SILICATES | | | | TERNARY CALCIUM SILICATES | | | |
| 2BaO.SiO ₂ | > 1755 | m | 11 | BaO.2CaO.3SiO ₂ ... | 1320 ± 4 | r | 11 |
| BaO.SiO ₂ | 1604 ± 5 | m | 11 | K ₂ O.CaO.SiO ₂ | | m | 30 |
| 2BaO.3SiO ₂ | 1450 ± 2 | m | 11 | 2K ₂ O.CaO.3SiO ₂ ... | 1010 ± 5 | r | 30 |
| BaO.2SiO ₂ | 1420 ± 4 | m | 11 | K ₂ O.3CaO.6SiO ₂ ... | 1015 ± 5 | r | 30 |
| BeO.SiO ₂ | > 1755 | m | 21 | 4K ₂ O.CaO.10SiO ₂ ... | 946 ± 1 | m | 30 |
| 3CaO.SiO ₂ | 1900 ± 20 | r | 9 | 2K ₂ O.CaO.6SiO ₂ ... | 950 ± 1 | m | 30 |
| 2CaO.SiO ₂ | 2130 ± 20 | m | 9 | K ₂ O.2CaO.6SiO ₂ ... | 1115 ± 5 | r | 30 |
| 3CaO.2SiO ₂ | 1475 ± 5 | r | 9 | K ₂ O.2CaO.9SiO ₂ ... | 1025 ± 5 | r | 30 |
| CaO.SiO ₂ | 1540 ± 2 | m | 9 | MgO.CaO.SiO ₂ | 1498 ± 5 | r | 12 |
| 2CdO.SiO ₂ | 1242 ± 2 | m | 20 | 2MgO.2CaO.2SiO ₂ ... | 1458 ± 2 | m | 12 |
| CdO.SiO ₂ | 1242 ± 2 | m | 20 | 2MgO.5CaO.6SiO ₂ ... | 1365 ± 5 | r | 12 |
| K ₂ O.SiO ₂ | 976 | m | 26 | MgO.CaO.2SiO ₂ ... | 1391 ± 2 | m | 10, 2 |
| K ₂ O.2SiO ₂ | 1036 ± 1 | m | 24 | 2Na ₂ O.CaO.3SiO ₂ ... | 1141 ± 5 | r | 29 |
| K ₂ O.4SiO ₂ | 765 ± 0.5 | m | 24 | Na ₂ O.2CaO.3SiO ₂ ... | 1284 ± 5 | m | 29 |
| 2Li ₂ O.SiO ₂ | 1256 ± 5 | r | 19 | Na ₂ O.3CaO.6SiO ₂ ... | 1047 | r | 29 |
| Li ₂ O.SiO ₂ | 1201 ± 2 | m | 10 | MISCELLANEOUS COMPOUNDS | | | |
| Li ₂ O.2SiO ₂ | 1032 ± 5 | r | 19 | 2CaO.Fe ₂ O ₃ | 1436 ± 5 | r | 38 |
| 2MnO.SiO ₂ | 1323 | r | 20 | CaO.Fe ₂ O ₃ | 1216 ± 5 | r | 38 |
| MnO.SiO ₂ | 1273 ± 5 | m | 20 | 2CaO.B ₂ O ₃ | 1304 ± 5 | m | 33 |
| 2MgO.SiO ₂ | 1890 ± 20 | m | 3 | CaO.ZrO ₂ | 2350 ± 25 | m | 35 |
| MgO.SiO ₂ | 1557 ± 2 | r | 3 | K ₂ O.2TiO ₂ | 980 | m | 31 |
| 2Na ₂ O.SiO ₂ | 1120 ± 5 | r | 23 | Na ₂ O.Fe ₂ O ₃ .4SiO ₂ .. | 990 ± 10 | r | 6 |
| Na ₂ O.SiO ₂ | 1088 ± 2 | m | 17, 23 | | | | |
| Na ₂ O.2SiO ₂ | 875 ± 1 | m | 28, 23 | | | | |
| 2PbO.SiO ₂ | 746 ± 10 | m | 8 | | | | |
| PbO.SiO ₂ | 766 ± 10 | m | 8 | | | | |
| 2SrO.SiO ₂ | > 1755 | m | 21 | | | | |
| SrO.SiO ₂ | 1580 ± 4 | m | 11 | | | | |
| 2ZnO.SiO ₂ | 1512 ± 5 | m | 7 | | | | |
| ZnO.SiO ₂ ?..... | 1437 | r? | 21 | | | | |
| ZrO ₂ .SiO ₂ | 2550 ± 50 | m | 40 | | | | |

Author List (References may be located in Abstract Journals): (1), Bowen, 1913. (2) Bowen, 1914. (3) Bowen, Andersen, 1914. (4) Bowen, 1917. (5) Bowen, Greig, 1924. (6) Bowen, Schairer, 1929. (7) Bunting, 1926. (8) Cooper *et al.*, 1909. (9) Day, Shepherd, Rankin, Wright, 1909-15. (10) Day, Sosman, Allen, 1911. (11) Eskola, 1922. (12) Ferguson, Merwin, 1919. (13) Ferguson, Buddington, 1920. (14) Friedrich, Sittig, 1925. (15) Goetze, 1911. (16) Greig, 1927. (17) Jaeger, 1911. (18) Jaeger, Simek, 1914. (19) Jaeger, van Klooster, 1914. (20) Jaeger, van Klooster, 1916. (21) Jaeger, van Klooster, 1919. (22) Kanolt, 1914. (23) Kracke, 1930. (24) Kracke, Bowen, Morey, 1929. (25) Matignon, 1925. (26) Morey, 1917. (27) Morey, Bowen, 1922. (28) Morey, Bowen, 1924. (29) Morey, Bowen, 1925. (30) Morey, Kracke, Bowen, 1930. (31) Nigli, 1916. (32) Rankin, Merwin, 1916. (33) Roberts, 1924. (34) Ruff *et al.*, 1916. (35) Ruff *et al.*, 1929. (36) Schumacher, 1926. (37) Slade, Higson, 1919. (38) Sosman, Merwin, 1916. (39) Tiede, Birnbrauer, 1914. (40) Washburn, Libman, 1920.

ENANTISTROPIC INVERSIONS IN CRYSTALS

(Arranged by F. C. Kracek, Geophysical Laboratory, Carnegie Institution, 1931.)

Values are given, for the more important crystals, of the inversion temperature in °C, the heat of inversion in cal./g and the inversion volume change in cm³/g. No monotropic inversions have been included.

h, inversion temperature on heating; m, metastable inversion temperature; e, estimated; g, gradual inversion (not to be confused with slow retarded inversions).

| Substance | Phases | Inversion t°C | Pressure atm. | Inversion heat cal./g | Inversion volume change cm ³ /g | Reference |
|--|------------------------|------------------|------------------|-----------------------------|---|-----------|
| AgClO ₄ | | 158 | | | | 1 |
| AgBrO ₃ | | 98.5 | | | | 2 |
| AgI..... | I-II | { 146 | 1 | 5.72 | .0086 | 3 |
| | | { 99.4 | 2720 | 4.95 | .0101 | 3 |
| | I-III | { 99.4 | 2720 | 4.22 | .0140 | 3 |
| | | { 99.4 | 2720 | .76 | .0241 | 3 |
| Ag ₂ S..... | | 175 | | 3.85 | | 4 |
| Ag ₂ Se..... | | 133 | | 5.65 | | 5 |
| Ag ₂ SO ₄ | | 412 | | | | 6 |
| AgNO ₃ | | 159.5 | | 3.37 | .0025 | 7 |
| AlBr ₃ | | 70 | | | | 8 |
| As ₂ O ₃ | | 275 | | 6 | | 9 |
| As ₂ S ₂ | red-black | 267 | | | | 10 |
| As ₂ S ₃ | red-yellow | 170 | | | | 10 |
| Bi ₂ O ₃ | | 704* | | | | 11 |
| BaCl ₂ | | 924 | | | | 12 |
| BaClO ₄ | | 284 | | | | 1 |
| BaSO ₄ | | 1149 | | | | 13 |
| BaCO ₃ | | 811 & 982 | | | | 14 |
| Br ₂ O ₃ | | -35 | | | | 15 |
| C..... | diamond- β graphite | 25 | >8000 | 16 | | 16 |
| CO..... | g | -212.8 | | 5.4 | | 18 |
| CH ₄ | g | -252.7 | | 1.15 | | 18 |
| CH ₃ OH..... | g | -112 | | 4.8 | | 19 |
| CCl ₄ | I-II | { -48.5 | 1 | 7.1 | .026(e) | 20 |
| | | { 115 | 8460 | 9.8 | .0173 | 3 |
| | II-III | { 115 | 8460 | .9 | .0054 | 3 |
| | | { 115 | 8460 | 10.7 | .0227 | 3 |
| CBr ₄ | I-II | { 46.2 | 1 | 5.04 | .0205 | 3 |
| | | { 112.6 | 2110 | 4.58 | .0150 | 3 |
| | I-III | { 112.6 | 2110 | .25 | .0029 | 3 |
| | | { 112.6 | 2110 | 4.66 | .0121 | 3 |
| CH ₂ I ₂ | L-I-II | { 8.6 | 180 | | | 3 |
| | | { 42.8 | 1930 | | | 3 |
| | L-II-III | { 9.4 | 325 | | | 3 |
| | | { 38 | 1825 | | | 3 |
| CH ₃ N ₂ O.... (Urea) | I-II | { 102.3 | 6535 | 2.34 | .0480 | 3 |
| | | { 102.3 | 6535 | 10.14 | .0486 | 3 |
| | II-III | { 102.3 | 6535 | 7.80 | .0006 | 3 |
| | | { 16.68 | 1 | 45 | .1560 | 3 |
| CH ₃ COOH.. | L-I | { 55.7 | 2033 | 46.4 | .0862 | 3 |
| | | { 55.7 | 2033 | 48.2 | .0992 | 3 |
| | L-II | { 55.7 | 2033 | 1.85 | .0130 | 3 |
| | | { 127 | 5220 | 60.9 | .0319 | 7 |
| CH ₃ CONH ₂ . (Acetamide) | L-I | { 127 | 5220 | 58.5 | .0649 | 7 |
| | | { 127 | 5220 | 2.41 | .0330 | 7 |
| | L-II | { 127 | 5220 | | | 7 |
| | | { 140 to -150 | | <0.5 | | 19 |

* Third modification at room temperature. † Acetone.

ENANTISTROPIC INVERSIONS IN CRYSTALS

| Substance | Phases | Inversion t°C | Pressure atm. | Inversion heat cal./g | Inversion volume change cm ³ /g | Refer- ence |
|--|-------------------|------------------|----------------------|-----------------------------|---|----------------|
| C ₂ Cl ₆ | I-II | 71.1 | I | 6.93 | 0.0280 | 7 |
| (Perchlor ethane) | II-III | 42.7 | I | 2.63 | .0097 | 7 |
| C ₃ H ₇ NO ₂ (Urethane) | L-I | 47.9 | I | 40.7 | .0599 | 7 |
| | | 66.2 | 2270 | 37.9 | .0253 | 7 |
| | L-II | 66.2 | 2270 | 35.9 | .0355 | 7 |
| | | 76.8 | 4090 | 34.4 | .0184 | 7 |
| | L-III | 76.8 | 4090 | 40.6 | .0640 | 7 |
| | I-II | 66.2 | 2270 | 2.07 | .0102 | 7 |
| | | 25.5 | 3290 | 1.64 | .0092 | 7 |
| | II-III | 76.8 | 4090 | 6.12 | .0456 | 7 |
| | | 25.5 | 3290 | 5.50 | .0482 | 7 |
| | I-III | 25.5 | 3290 | 3.87 | .0574 | 7 |
| C ₆ H ₆ (Benzene) | I-II | 100 | 11680 | 8.68 | .0105 | 21 |
| | | 218 | 11680 | 7.73(e) | .0132(e) | 21 |
| | L-I | 5.4 | I | 30.2 | .1317 | 21 |
| | | 218 | 11680 | 33.25(e) | .0369(e) | 21 |
| | L-II | 218 | 11680 | 25.5(e) | .0501(e) | 21 |
| C ₆ H ₅ OH (Phenol) | L-I | 40.9 | I | 29.8 | .0567 | 22 |
| | | 64 | 2015 | 24.8 | .0270 | 7 |
| | L-II | 64 | 2015 | 30 | .0825 | 7 |
| | I-II | 64 | 2015 | 5.2 | .0555 | 7 |
| CH ₃ C ₆ H ₄ OH (o.Cresol) | L-I | 30.8 | I | 33.8 | .0838 | 21 |
| | | 103.2 | 5900 | 34.2 | .0317 | 21 |
| | L-II | 103.2 | 5900 | 35 | .0555 | 21 |
| | I-II | 103.2 | 5900 | .8 | .0238 | 21 |
| Camphor* | I-II | 87.1 | I | .25 | .00187 | 7 |
| C ₆ H ₁₁ OH† | I-II | -9 | I | 9.38 | ... | 19 |
| C ₆ H ₅ NH ₂ HNO ₃ † | | 97.6 | | | | 23 |
| CaSO ₄ | | 1193 | | | | 13 |
| CaCO ₃ § | I-II | 970 | high CO ₂ | | | 14 |
| CaO.SiO ₂ | | 1190 ± 10 | | Ca. 10 | | 25 |
| 2CaO.SiO ₂ | | 1420, 675 | | 10%, 675 | | 26 |
| Co | Curie point | ~ 1100 | | 1.3 | | 27 |
| | I-II | 1015 | | | | 28 |
| | II-III | 400 | | | | 28 |
| CoO | | 350 ± 10 | | | | 29 |
| CoOH | | 223 | | 11.8 | | 30 |
| CsCl | | 460 | | 8 | | 31 |
| CsClO ₄ | | 219 | | | | I |
| Cs ₂ SO ₄ | | 660 | | | | 32 |
| CsNO ₃ | | 153.5 | I | 4.3 | .00405 | 7 |
| Cs ₂ Ca ₂ (SO ₄) ₃ | | 722 | | | | 32 |
| Cu ₂ Br ₂ | I-II-III | 390, 470 | | | | 33 |
| Cu ₂ I ₂ | I-II-III | 402, 440 | I | | | 33 |
| | II-III | 200 | 9600 | 1.09I | .00485 | 3 |
| | II-III | 100 | 11560 | .948 | .00535 | 3 |
| Cu ₂ S | | 91 | | 5.6 | | 34 |
| Cu ₂ Se | | 110 | | 5.4 | | 34 |
| Cu ₂ Te | | 351, 387 | | | | 35 |
| Fe | Curie point | 730 | | 6.7 ± | | 27 |
| | β-γ | 920 | | 6.7 ± | | .. |
| | γ-δ | 1400 | | 2 | | .. |
| Fe ₂ O ₄ | Curie point | 570 ± | | | | 36 |
| Fe ₂ O ₃ | II-III | -163 to -148 | | 2.25 | | 37 |
| | I-II | 500 ± | | | | .. |
| FeS | | 140 | | | | 38 |
| FeS ₂ | pyrite, marcasite | | | | | 39 |

* Five other modifications; not accurately located. † Cyclo-hexanol.

§ Very beautiful for demonstration purposes.

ENANTISTROPIC INVERSIONS IN CRYSTALS

| Substance | Phases | Inversion $t^{\circ}\text{C}$ | Pressure atm. | Inversion heat cal./g | Inversion volume change cm^3/g | Reference |
|--|----------------------------|---|------------------|-----------------------------|---|-----------|
| Fe_2P | | 80 | | | | 40 |
| Fe_3P | | 440 | | | | 40 |
| FeTiO_3 | | 215 | | | | 41 |
| HgI_2 | red-yellow | 127.5 | | 1.3 | 0.00342 | 3 |
| Hg_2I_2 | green-yellow | | | .5 \pm | | 42 |
| HgS | {cinnabar metacinnabar} | 386 \pm | | | | 39 |
| ICl | ruby-brown | | | | | 43 |
| KOH | | 248 | | 27.1 | | 30 |
| KClO_3 | I-II | 255 | | | | 3 |
| | II-III | $P = 5500 + 10.9 t$ | | | | 3 |
| | | $\Delta v_i = 0.02510 - 2.2 t \times 10^{-6} \Delta h_i = 0.165 \text{ at } 0^{\circ}, 0.281 \text{ at } 200^{\circ}$ | | | | 3 |
| KClO_4 | | 295 | | | | 1 |
| K_2S | I-II | {146.4 $t = 146.4 + 0.0124 p$ | I | .765 | .00095 | 3 |
| KNO_3 | I-II | {127.7 128 | I 81 | 10.5 10.3 | .00484 .0049 | 7 44 |
| | I-III | 128 | 81 | 5.6 | .0138 | 44 |
| | II-III | {128 21.3 | 81 | 4.7 1.3 | .0089 .0156 | 44 7 |
| | III-IV | 21.3 | 2840 | 5.1 | .0284 | 7 |
| | II-IV | 21.3 | 2840 | 3.8 | .0440 | 7 |
| K_2SO_4 | | 588 | | 13 | | 45 |
| KHSO_4 | I-II | {180.5 198.6 | I 1773 | .71 2.29 | .00066 .00197 | 3 3 |
| | II-III | {164.2 118.2 | I 2810 | 3.61 3.30 | .00566 .00570 | 3 3 |
| | II-IV | {198.6 118.2 | 1773 2810 | .166 .134 | .00113 .00110 | 3 3 |
| | I-IV | 198.6 | 1773 | 2.03 | .00310 | 3 |
| | III-IV | 118.2 | 2810 | 3.44 | .00680 | 3 |
| KPO_3 | | 450 | | | | 46 |
| $\text{K}_4\text{P}_2\text{O}_7$ | | 278 | | | | 46 |
| K_2CO_3 | | 410 | | | | 22 |
| KCNS | | 143 | I | 3.10 | .00306 | 3 |
| $\text{K}_2\text{Pb}(\text{SO}_4)_2$ | | 544 | | | | 32 |
| K_2CdI_4 | | 215 | | | | 47 |
| K_2CrO_4 | | 666 | | 12.6 | | 48 |
| $\text{K}_2\text{Cr}_2\text{O}_7$ | | 243 | | 1.40 | | 45 |
| K_2MoO_4 | | 327, 454, 477 | | | | 49 |
| K_2WO_4 | | 388 | | 8.2 | | 45 |
| | | 575 | | 1.6 | | 45 |
| $\text{K}_2\text{Ca}_2(\text{SO}_4)_3$ | | 937 | | | | 32 |
| $\text{K}_2\text{Sr}(\text{SO}_4)_3$ | | 775 | | | | 32 |
| KLiSO_4 | | 435 | | | | 32 |
| KNO_2 | I-II | {-0.3 122.3 | 5000 10000 | 11.7 7.15 | .0315 .0378 | 3 3 |
| $\text{K}_2\text{O}(\text{SiO}_2)_2$ | | 290 | | | | 45 |
| $2\text{K}_2\text{O}(\text{Al}_2\text{O}_3)(\text{SiO}_2)_4^*$ | | 714 | | | | 50 |
| LiClO_3 | | 415.99 | | | | 51 |
| Li_2SO_4 | | 580 | | 55 \pm 1 | | 45 |
| $(\text{MgO})_6(\text{B}_2\text{O}_3)_3\text{MgCl}$ | | 266 | | 1.8 | | 52 |
| $\text{MgO} \cdot \text{SiO}_2^\dagger$ | | | | | | 53 |
| Mn | | 742, 1191 | | | | 54 |
| MnSO_4 | | 860 | | | | 55 |
| MnO_2 | | -185 to -175 | | .88 | | 37 |
| MnO | | -153 to -163 | | 2.08 | | 37 |
| N_2 | | -237.6 | | 1.9(g) | | 56 |
| NH_4Cl | | -30.5(g) | | | | 57 |
| | I-II | 184.3 | | 16.3 | .0985 | 3 |

* Leucite. \dagger Probably pentamorphic, inv. at 1150 and 1300 $^{\circ}$.

ENANTISTROPIC INVERSIONS IN CRYSTALS

| Substance | Phases | Inversion $t^{\circ}\text{C}$ | Pressure atm. | Inversion heat cal./g | Inversion volume change cm^3/g | Refer- ence |
|---|-------------|----------------------------------|------------------|-----------------------------|---|----------------|
| NH_4Br | | -38 (g) | | | | 57 |
| | I-II | 137.8 | 1 | 7.78 | 0.0647 | 3 |
| NH_4I | | -42.5(g) | | | | 57 |
| | I-II | -17.6 | 1 | 4.80 | .0561 | 3 |
| NH_4ClO_4 | | 240 | | | | 58 |
| NH_4HSO_4 | I-II-III | 126.2 | 1800 | | | 3 |
| | II-III-IV | 176.9 | 5480 | | | 3 |
| $(\text{NH}_4)_3\text{H}(\text{SO}_4)_2$ | | 134 | | | | 59 |
| NH_4CNS | I-II | 120 | | | | 60 |
| | II-III | 87.7 | 1 | 10.36 | .0409 | 3 |
| NH_4NO_3 | L-I | 169.5 | 1 | 16 | .051 | 7 |
| | I-II | 125.5 | 1 | 12.9 | .01351 | 7 |
| | I-VI | 186.7 | 8730 | 12.6 | .00475 | 7 |
| | I-VI | 186.7 | 8730 | 12.3 | .00855 | 7 |
| | II-VI | 169.2 | 8870 | .27 | .00309 | 7 |
| | II-VI | 186.7 | 8730 | .33 | .00380 | 7 |
| | II-III | 84 | 1 | 4 | .00758 | 7 |
| | II-III | 63.3 | 830 | 2.48 | .00925 | 7 |
| | III-IV | 32 | 1 | 4.67 | .02026 | 7 |
| | III-IV | 63.3 | 830 | 4.03 | .02135 | 7 |
| | II-IV | 63.3 | 830 | 6.51 | .01210 | 7 |
| | II-IV | 169.2 | 8870 | 11.84 | .01267 | 7 |
| | IV-VI | 169.2 | 8870 | 12.1 | .00958 | 7 |
| | IV-V | -18 | 1 | 1.6 | .017 | 7 |
| NaOH | | 300 | | 24.7 | | 30 |
| NaClO_4 | | 308 | | | | 58 |
| NaClO_3 | | 248 | | | | 61 |
| Na_2SO_4 | IV-III | 185 | | 8.6 | .0034 | 62 |
| | III-I | 241 | | 15.5 | .0070 | 62 |
| $\text{NaF} \cdot \text{Na}_2\text{SO}_4$ | | 105 | | | | .. |
| Na_2CO_3 | | 430 | | | | 22 |
| NaNO_3 | | 275(g) | | (8 \pm 2) | (.0081) | 45 |
| Na_3AlF_6 | | 568 | | 59 | | 63 |
| Na_2MoO_4 | | 424, 585, 623 | | | | 64 |
| Na_2WO_4 | I-II | 588 | | 33.6 | | 45 |
| | I-III | 586m | | 4.4 | | 45 |
| | III-II | m | | 29.2 | | 45 |
| NaAlSiO_4 | neph.—carn. | 1250 | | | | 65 |
| | carnegicite | 226, 650-690 | | ca1 | | 65 |
| $\text{NaC}_2\text{H}_2\text{O}_2^*$ | | 198† | | | | 58 |
| Ni | Curie pt. | 355 | | | | 27 |
| Ni_3S_2 | | 545 | | | | 66 |
| Ni_5As_2 | | 970 | | | | 67 |
| Oxygen | I-II | -229.5 | | 6.2 | | 18 |
| | II-III | -249.5 | | .75 | | 18 |
| Phosphorus | L-I | 44.2 | 1 | 4.90 | .0193 | 3 |
| | L-I | 196 | 6000 | 6.53 | .0120 | 3 |
| | I-II | 0.1 | 6000 | 43.9 | .00846 | 3 |
| | I-II | 68.4 | 12000 | 55.2 | .00684 | 3 |
| PbO | red-yellow | 587 | | | | 64 |
| PbSO_4 | | 870 | | 13.4 | | 68 |
| PbCrO_4 | | 707, 783 | | | | 64 |
| PbWO_4 | | 877 | | | | 64 |
| RbOH | | 245 | | 16.8 | | 30 |
| RbClO_4 | | 279 | | | | 1 |
| Rb_2SO_4 | | 653 | | | | 32 |
| $\text{Rb}_2\text{Ca}_2(\text{SO}_4)_3$ | | 787, 915 | | | | 32 |
| RbLiSO_4 | | 142 | | | | 32 |

* Acetate. † Sluggish.

ENANTISTROPIC INVERSIONS IN CRYSTALS

| Substance | Phases | Inversion °C | Pressure atm. | Inversion heat cal./g | Inversion volume change cm ³ /g | Reference |
|--------------------------------|--|-----------------|----------------------|-----------------------------|---|-----------|
| RbNO ₃ | I-II | 219 | | | | 69 |
| | II-III | 164.4 | I | 7.12 | 0.00688 | 7 |
| | | 218.6 | 5810 | 5.93 | .00434 | 7 |
| RbCl | | 50 | 5525 | | | 70 |
| RbBr | | 50 | 4925 | | | 70 |
| RbI | | 50 | 4050 | | | 70 |
| Sulphur | I-II | 95.5 | I | 2.7 | | 71 |
| | L-I-II | 155 | 1410 | | | 22 |
| Sb | expl.-common | | | 19 | | 72 |
| Sb ₂ O ₃ | rhomb.-reg. | 570 | | | | 73 |
| SbCl ₃ | I-II-III | 65, 69.5 | | | | 8 |
| SiO ₂ * | I-II | 573 | | 2.6 | | 45 |
| SiO ₂ † | I-II | 215 | | 2.7 | | 45 |
| SiO ₂ § | I-II | 150h | | .63 | | 45 |
| | II-III | 104h | | .96 | | 45 |
| | *-§ | 870 | | 8.7(e) | | 74 |
| SiO ₂ | *-† | 1250 | | 25 (e) | | 75 |
| | §-† | 1470 | | 7.5(e) | | 45 |
| | | 161 | | .2 | small | 77 |
| Sn | | 18 | | 4.4 | | 72 |
| | | 430, 540 | | | | .. |
| | | 1152 | | | | 13 |
| SrSO ₄ | | 925 | high CO ₂ | | | 14 |
| SrCO ₃ | | 226 | | | | I |
| TiClO ₄ | | 173 | | | | 79 |
| TiI | | 144.6 | I | 2.86 | .00244 | 7 |
| TiNO ₃ | I-II | 75 | I | .89 | .00073 | 7 |
| Ti picrate | II-III | 44 | | | .018 | 80 |
| | | 230 | | .3± | | 77 |
| | | | | | | |
| TiO ₂ | Rutile, anatase, brookite, stability relations unknown | | | | | |
| TiBr ₄ | | -15 | | | | 81 |
| W ₂ C | | 2400 | | | | 82 |
| Zn | | 175, 300 | | | | 83 |
| ZnS‡ | | 1020 | | | | 39 |
| ZrO ₂ | | ca 1000 | | | | 84 |

(1) Vorländer, 1923. (2) Reedy, 1921. (3) Bridgman, 1915. (4) Rinne, 1924. (5) Bellatti, 1880. (6) Nacken, 1907. (7) Bridgman, 1916. (8) Kendall, 1923. (9) Rushton, Daniels, 1926. (10) Borodorski, 1906. (11) Guertler, 1903. (12) Yortisch, 1914. (13) Grahmann, 1913. (14) Boeke, 1913. (15) Lewis, Schumacher, 1929. (16) Roth, 1925. (17) G. N. Lewis, 1923. (18) Clusius, 1929. (19) Kelley, 1929. (20) Latimer, 1922. (21) Bridgman, 1914. (22) Tammann, 1903. (23) Wallerant, 1915. (24) Bäckström, 1921, 1925. (25) White, 1910. (26) Day, 1906. (27) Various. (28) Hendrichs, 1930. (29) Emmett-Schulz, 1930. (30) Hevesy, 1910. (31) Zemczny, Rambach, 1910. (32) Müller, 1910. (33) Tubandt, 1928. (34) Bellatti, 1880. (35) Chicaschigé, 1907. (36) Baudisch-Welo, 1925. (37) Millar, 1928. (38) Rinne, Boeke, 1907. (39) Allen, 1912. (40) le Chatelier, 1909. (41) Königsberger, 1910. (42) Varet, 1896. (43) Stortenbeker, 1880. (44) Kracek, 1930. (45) Kracek, 1931. (46) Amadori, 1913. (47) Brand, 1912. (48) Hare, 1924. (49) Van Klooster, 1914. (50) Rinne, 1910. (51) Kraus, Burgess, 1927. (52) Kroecker, 1892. (53) Allen, White, 1900. (54) Persson, Ohmann, 1929. (55) Friedrichs, 1910. (56) Eucken, 1924. Clusius, 1929. (57) Simon, 1927. (58) Vorländer, 1923. (59) Fischer, 1911. (60) Vresnevsky. (61) Retgers. (62) Kracek, Gibson, 1929. (63) Roth, 1926. (64) Jaeger, Germis, 1921. (65) Bowen, Greig, 1925. (66) Friedrichs, 1914. (67) Friedrichs, 1907. (68) Hare, 1924. (69) Schwarz, 1892. (70) Bridgman, 1928. (71) Mondain, Monval, 1926. (72) Cohen, 1915. (73) Fenwick, 1927. (74) Fenner, 1913. (75) White, 1909, 1910. (76) Wietzel, 1921. (77) Werner, 1913. (78) Brönsted, 1913. (79) Gernez, 1904. (80) Cohen, 1920. (81) Baltz, Jelp, 1927. (82) Becker, 1928. (83) Saldan, 1930. (84) Böhm, 1925.

* Quartz. † Cristobalite. ‡ Zinblend and wurtzite. § Tridymite.

TRANSFORMATION AND MELTING TEMPERATURES OF LIME-ALUMINA-SILICA COMPOUNDS AND EUTECTIC MIXTURES

The majority of these determinations are by G. A. Rankin. (Part unpublished.)

| Substance. | % CaO | Al ₂ O ₃ | SiO ₂ | Transformation. | Temp. |
|--|-------|--------------------------------|------------------|---|------------|
| CaSiO ₃ . . . | 48.2 | — | 51.8 | Melting | 1540° ± 2° |
| CaSiO ₃ . . . | 48.2 | — | 51.8 | α to β and reverse | 1200 ± 2 |
| Ca ₂ SiO ₄ . . . | 65. | — | 35. | Melting | 2130 ± 10 |
| " . . . | 65. | — | 35. | γ to β and reverse | 675 ± 5 |
| " . . . | 65. | — | 35. | β to α and reverse | 1420 ± 2 |
| Ca ₃ Si ₂ O ₇ . . . | 58.2 | — | 41.8 | Dissociation into Ca ₂ SiO ₄ and liquid | 1475 ± 5 |
| Ca ₃ SiO ₅ . . . | 73.6 | — | 26.4 | Dissociation into Ca ₂ SiO ₄ and CaO | 1900 ± 5 |
| Ca ₃ Al ₂ O ₆ . . . | 62.2 | 37.8 | — | Dissociation into CaO and liquid | 1535 ± 5 |
| Ca ₅ Al ₆ O ₁₄ . . . | 47.8 | 52.2 | — | Melting | 1455 ± 5 |
| CaAl ₂ O ₄ . . . | 35.4 | 64.6 | — | Melting | 1600 ± 5 |
| Ca ₃ Al ₁₀ O ₁₈ . . . | 24.8 | 75.2 | — | Melting | 1720 ± 10 |
| Al ₂ SiO ₅ . . . | — | 62.8 | 37.1 | Melting | 1816 ± 10 |
| CaAl ₂ Si ₂ O ₈ . . . | 20.1 | 36.6 | 43.3 | Melting | 1550 ± 2 |
| Ca ₂ Al ₂ SiO ₇ . . . | 40.8 | 37.2 | 22.0 | Melting | 1590 ± 2 |
| Ca ₃ Al ₂ SiO ₈ . . . | 50.9 | 30.9 | 18.2 | Dissociation into Ca ₂ SiO ₄ +Ca ₂ Al ₂ SiO ₇ and liquid | 1335 ± 5 |

| EUTECTICS. | | | | | EUTECTICS. | | | | | | | | | | | | |
|---|-------|--------------------------------|------------------|---------------|--|-------|--------------------------------|------------------|---------------|------|------|------|------|---|------|------|--|
| Crystalline Phases. | % CaO | Al ₂ O ₃ | SiO ₂ | Melting Temp. | Crystalline Phases. | % CaO | Al ₂ O ₃ | SiO ₂ | Melting Temp. | | | | | | | | |
| CaSiO ₃ , SiO ₂ | 37. | — | 63. | 1436° | CaAl ₂ Si ₂ O ₈ | 38. | 20. | 42. | 1265° | | | | | | | | |
| Ca ₂ SiO ₄ | 54.5 | — | 45.5 | 1455± | Ca ₂ Al ₂ SiO ₇ | | | | | | | | | | | | |
| 3CaO, 2SiO ₂ | | | | | Ca ₂ SiO ₄ | | | | | | | | | | | | |
| Ca ₂ SiO ₄ | 67.5 | — | 32.5 | 2065± | CaAl ₂ Si ₂ O ₈ | 29.2 | 39. | 31.8 | 1380 | | | | | | | | |
| CaO. | | | | | Ca ₂ Al ₂ SiO ₇ | | | | | | | | | | | | |
| Al ₂ SiO ₅ , SiO ₂ | | | | | Al ₂ O ₃ | | | | | | | | | | | | |
| Al ₂ SiO ₅ , Al ₂ O ₃ | — | 13. | 87. | 1610 | Ca ₂ SiO ₄ | 49.5 | 43.7 | 6.8 | 1335 | | | | | | | | |
| CaAl ₂ Si ₂ O ₈ | 34.1 | 18.6 | 47.3 | 1299 | CaAl ₂ O ₄ | | | | | | | | | | | | |
| CaSiO ₃ | | | | | Ca ₅ Al ₆ O ₁₄ | | | | | | | | | | | | |
| CaAl ₂ Si ₂ O ₈ | 10.5 | 19.5 | 70. | 1359 | QUINTUPLE POINTS. | | | | | | | | | | | | |
| SiO ₂ | | | | | Ca ₂ Al ₂ SiO ₇ | 48.2 | 11.9 | 39.9 | 1335 | | | | | | | | |
| CaAl ₂ Si ₂ O ₈ | | | | | Ca ₂ SiO ₄ | | | | | | | | | | | | |
| SiO ₂ , CaSiO ₃ | 23.2 | 14.8 | 62. | 1165 | Ca ₂ Al ₂ SiO ₇ | | | | | | | | | | | | |
| Ca ₂ Al ₂ SiO ₇ | | | | | Ca ₂ SiO ₄ | 48.3 | 42. | 9.7 | 1380 | | | | | | | | |
| Ca ₂ SiO ₄ | | | | | CaAl ₂ O ₄ | | | | | | | | | | | | |
| Al ₂ O ₃ | 19.3 | 39.3 | 41.4 | 1547 | CaAl ₂ Si ₂ O ₈ | 15.6 | 36.5 | 47.9 | 1512 | | | | | | | | |
| CaAl ₂ Si ₂ O ₈ | | | | | Al ₂ O ₃ | | | | | | | | | | | | |
| CaAl ₂ Si ₂ O ₈ | | | | | Al ₂ SiO ₅ | 31.2 | 44.5 | 24.3 | 1475 | | | | | | | | |
| Al ₂ SiO ₅ , SiO ₂ | 9.8 | 19.8 | 70.4 | 1345 | QUADRUPLE POINTS. | | | | | | | | | | | | |
| Ca ₂ Al ₂ SiO ₇ | | | | | 35. | | | | | 50.8 | 14.2 | 1552 | 55.5 | — | 44.5 | 1475 | |
| Ca ₂ Al ₂ SiO ₇ | 37.8 | 52.9 | 9.3 | 1512 | | | | | | | | | | | | | |
| CaAl ₂ O ₄ | | | | | | | | | | | | | | | | | |
| Ca ₂ Al ₂ SiO ₇ | | | | | | | | | | | | | | | | | |
| CaAl ₂ O ₄ | 37.5 | 53.2 | 9.3 | 1505 | | | | | | | | | | | | | |
| Ca ₃ Al ₁₀ O ₁₈ | | | | | | | | | | | | | | | | | |
| CaAl ₂ Si ₂ O ₈ | | | | | | | | | | | | | | | | | |
| Ca ₂ Al ₂ SiO ₇ | 30.2 | 36.8 | 33. | 1385 | | | | | | | | | | | | | |
| Ca ₂ Al ₂ SiO ₇ | | | | | | | | | | | | | | | | | |
| Ca ₃ Si ₂ O ₇ | | | | | | | | | | | | | | | | | |
| CaSiO ₃ | 47.2 | 11.8 | 41. | 1310 | | | | | | | | | | | | | |
| Ca ₂ Al ₂ SiO ₇ | | | | | | | | | | | | | | | | | |
| CaSiO ₃ | | | | | | | | | | | | | | | | | |
| Ca ₂ Al ₂ SiO ₇ | 45.7 | 13.2 | 41.1 | 1316 | | | | | | | | | | | | | |
| CaSiO ₃ | | | | | | | | | | | | | | | | | |
| CaSiO ₃ | | | | | | | | | | | | | | | | | |

The accuracy of the melting-points is 5 to 10 units. Geophysical Laboratory. See also Day and Sosman, Am. J. of Sc. xxxi, p. 341, 1911.

LOWERING OF FREEZING POINTS BY SALTS IN SOLUTION

In the first column is given the number of gram-molecules (anhydrous) dissolved in 1000 grams of water; the second contains the molecular lowering of the freezing point; the freezing point is therefore the product of these two columns. After the chemical formula is given the molecular weight, then a reference number.

| $\frac{\text{g. mol.}}{1000 \text{ g. H}_2\text{O}}$ | Molecular Lowering | $\frac{\text{g. mol.}}{1000 \text{ g. H}_2\text{O}}$ | Molecular Lowering | $\frac{\text{g. mol.}}{1000 \text{ g. H}_2\text{O}}$ | Molecular Lowering | $\frac{\text{g. mol.}}{1000 \text{ g. H}_2\text{O}}$ | Molecular Lowering |
|--|--------------------|---|--------------------|--|--------------------|--|--------------------|
| Pb(NO₃)₂, 331.0: 1, 2. | | 0.0500 | 3.47° | 0.4978 | 2.02° | MgCl₂, 95.26: 6, 14. | |
| 0.000362 | 5.5° | .1000 | 3.42 | .8112 | 2.01 | 0.0100 | 5.1° |
| .001204 | 5.30 | .2000 | 3.32 | 1.5233 | 2.28 | .0500 | 4.98 |
| .002805 | 5.17 | .500 | 3.26 | BaCl₂, 208.3: 3, 6, 13. | | .1500 | 4.96 |
| .005570 | 4.97 | 1.000 | 3.14 | 0.00200 | 5.5° | .3000 | 5.186 |
| .01737 | 4.69 | LiNO₃, 69.07: 9. | | .00498 | 5.2 | .6099 | 5.69 |
| .5015 | 2.99 | 0.0398 | 3.4° | .0100 | 5.0 | KCl, 74.60: 9, 17-19. | |
| Ba(NO₃)₂, 261.5: 1. | | .1671 | 3.35 | .0200 | 4.95 | 0.02910 | 3.54° |
| 0.000383 | 5.6° | .4728 | 3.35 | .04805 | 4.80 | .05845 | 3.46 |
| .001259 | 5.28 | 1.0164 | 3.49 | .100 | 4.69 | .112 | 3.43 |
| .002681 | 5.23 | Al₂(SO₄)₃, 342.4: 10. | | .200 | 4.66 | .3139 | 3.41 |
| .005422 | 5.13 | 0.0131 | 5.6° | .500 | 4.82 | .476 | 3.37 |
| .008352 | 5.04 | .0261 | 4.9 | .586 | 5.03 | 1.000 * | 3.286 |
| Cd(NO₃)₂, 236.5: 3. | | .0543 | 4.5 | .750 | 5.21 | 1.989 | 3.25 |
| 0.00298 | 5.4° | .1086 | 4.03 | CdCl₂, 183.3: 3, 14. | | 3.269 | 3.25 |
| .00689 | 5.25 | .217 | 3.83 | 0.00299 | 5.0° | NaCl, 58.50: 3, 20, 12, 16. | |
| .01997 | 5.18 | CdSO₄, 208.5: 1, 11. | | .00690 | 4.8 | 0.00399 | 3.7° |
| .04873 | 5.15 | 0.000704 | 3.35° | .0200 | 4.64 | .01000 | 3.67 |
| AgNO₃, 169.0: 4, 5. | | .002685 | 3.05 | .0541 | 4.11 | .0221 | 3.55 |
| 0.1506 | 3.32° | .01151 | 2.69 | .0818 | 3.93 | .04049 | 3.51 |
| .5001 | 2.96 | .03120 | 2.42 | .214 | 3.39 | .1081 | 3.48 |
| .8645 | 2.87 | .1473 | 2.13 | .429 | 3.03 | .2325 | 3.42 |
| 1.749 | 2.27 | .4129 | 1.80 | .858 | 2.71 | .4293 | 3.37 |
| 2.953 | 1.85 | .7501 | 1.76 | 1.072 | 2.75 | .700 | 3.43 |
| 3.856 | 1.64 | 1.253 | 1.86 | CuCl₂, 134.5: 9 | | NH₄Cl, 53.52: 6, 15. | |
| 0.0560 | 3.82 | K₂SO₄, 174.4: 3, 5, 6, 10, 12. | | 0.0350 | 4.9° | 0.0100 | 3.6° |
| .1401 | 3.58 | 0.00200 | 5.4° | .1337 | 4.81 | .0200 | 3.56 |
| .3490 | 3.28 | .00398 | 5.3 | .3380 | 4.92 | .0350 | 3.50 |
| KNO₃, 101.9: 6, 7. | | .00865 | 4.9 | .7149 | 5.32 | .1000 | 3.43 |
| 0.0100 | 3.5 | .0200 | 4.76 | CoCl₂, 129.9: 9. | | .2000 | 3.396 |
| .0200 | 3.5 | .0500 | 4.60 | 0.0276 | 5.0° | .4000 | 3.393 |
| .0500 | 3.41 | .1000 | 4.32 | .1094 | 4.9 | .7000 | 3.41 |
| .100 | 3.31 | .200 | 4.07 | .2369 | 5.03 | LiCl, 42.48: 9, 15 | |
| .200 | 3.19 | .454 | 3.87 | .4399 | 5.30 | 0.00992 | 3.7° |
| .250 | 3.08 | CuSO₄, 159.7: 1, 4, 11. | | .538 | 5.5 | .0455 | 3.5 |
| .500 | 2.94 | 0.000286 | 3.3° | CaCl₂, 111.0: 5, 13-16. | | .09952 | 3.53 |
| .750 | 2.81 | .000843 | 3.15 | 0.0100 | 5.1° | .2474 | 3.50 |
| 1.000 | 2.66 | .002279 | 3.03 | .05028 | 4.85 | .5012 | 3.61 |
| NaNO₃, 85.09: 2, 6, 7 | | .006670 | 2.79 | .1006 | 4.79 | .7939 | 3.71 |
| 0.0100 | 3.6° | .01463 | 2.59 | .5977 | 5.33 | BaBr₂, 297.3: 14 | |
| .0250 | 3.46 | .1051 | 2.28 | .946 | 5.3 | 0.100 | 5.1° |
| .0500 | 3.44 | .2074 | 1.95 | 2.432 | 8.2 | .150 | 4.9 |
| .2000 | 3.345 | .4013 | 1.84 | 3.469 | 11.5 | .200 | 5.00 |
| .500 | 3.24 | .8898 | 1.76 | 3.829 | 14.4 | .500 | 5.18 |
| .5015 | 3.30 | MgSO₄, 120.4: 1, 4, 11. | | 0.0478 | 5.2 | AlBr₃, 267.0: 9. | |
| 1.000 | 3.15 | 0.000675 | 3.29 | .153 | 4.91 | 0.0078 | 1.4° |
| 1.0030 | 3.03 | .002381 | 3.10 | .331 | 5.15 | .0559 | 1.2 |
| NH₄NO₃, 80.11: 6, 8 | | .01263 | 2.72 | .612 | 5.47 | .1971 | 1.07 |
| 0.0100 | 3.6° | .0580 | 2.65 | .998 | 6.34 | .4355 | 1.07 |
| .0250 | 3.50 | .2104 | 2.23 | | | | |

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Compiled from Landolt-Börnstein-Meyerhoffer's Physikalisch-chemische Tabellen.

LOWERING OF FREEZING POINTS BY SALTS IN SOLUTION

| $\frac{\text{g. mol.}}{1000 \text{ g. H}_2\text{O}}$ | Molecular Lowering. | $\frac{\text{g. mol.}}{1000 \text{ g. H}_2\text{O}}$ | Molecular Lowering. | $\frac{\text{g. mol.}}{1000 \text{ g. H}_2\text{O}}$ | Molecular Lowering. | $\frac{\text{g. mol.}}{1000 \text{ g. H}_2\text{O}}$ | Molecular Lowering. |
|--|---------------------|--|---------------------|--|---------------------|--|---------------------|
| CdBr₂, 272.3: 3, 14. | | KOH, 56.16: 1, 15, 23. | | Na₂SiO₃, 122.5: 15. | | | |
| 0.00324 | 5.1° | 0.00352 | 3.60° | 0.01052 | 6.4° | 0.472 | 2.20° |
| .00718 | 4.6 | .00770 | 3.59 | .05239 | 5.86 | .944 | 2.27 |
| .03627 | 3.84 | .02002 | 3.44 | .1048 | 5.28 | 1.620 | 2.60 |
| .0719 | 3.39 | .05006 | 3.43 | .2099 | 4.60 | (COOH) ₂ , 90.02: 4, 15. | |
| .1122 | 3.18 | .1001 | 3.42 | .5233 | 3.99 | 0.01002 | 3.3° |
| .206 | 2.96 | .2003 | 3.424 | HCl, 36.46: | | .02005 | 3.19 |
| .440 | 2.76 | .230 | 3.50 | 1-3, 6, 13, 18, 22. | | .05019 | 3.03 |
| .800 | 2.59 | .405 | 3.57 | 0.00305 | 3.68° | .1006 | 2.83 |
| CuBr₂, 223.5: 9. | | C₂H₅OH, 32.03: 24, 25. | | .00695 | 3.66 | .2022 | 2.64 |
| 0.0242 | 5.1° | 0.0100 | 1.8° | .0100 | 3.6 | .366 | 2.56 |
| .0817 | 5.1 | .0301 | 1.82 | .01703 | 3.59 | .648 | 2.3 |
| .2255 | 5.27 | .2018 | 1.811 | .0500 | 3.59 | C₆H₅(OH)₃, 92.06: 24, 25. | |
| .6003 | 5.89 | 1.046 | 1.86 | .1025 | 3.50 | 0.0200 | 1.86° |
| CaBr₂, 200.0: 14. | | .341 | 1.88 | .2000 | 3.57 | .1008 | 1.86 |
| 0.0871 | 5.1° | 6.200 | 1.944 | .3000 | 3.612 | .2031 | 1.85 |
| .1742 | 5.18 | C₂H₅OH, 46.04: | | .464 | 3.68 | .535 | 1.91 |
| .3484 | 5.30 | 1, 12, 17, 24-27. | | .516 | 3.79 | 2.40 | 1.98 |
| .5226 | 5.64 | 0.000402 | 1.67° | 1.003 | 3.95 | 5.24 | 2.13 |
| MgBr₂, 184.28: 14. | | .004993 | 1.67 | 1.032 | 4.10 | (C ₂ H ₅) ₂ O, 74.08: 24 | |
| 0.0517 | 5.4° | .0100 | 1.81 | 1.500 | 4.42 | 0.0100 | 1.6° |
| .103 | 5.16 | .02892 | 1.707 | 2.000 | 4.97 | .0201 | 1.67 |
| .207 | 5.26 | .0705 | 1.85 | 2.115 | 4.52 | .1011 | 1.72 |
| .517 | 5.85 | .1292 | 1.829 | 3.000 | 6.03 | .2038 | 1.702 |
| KBr, 119.1: 9, 21. | | .2024 | 1.832 | 3.053 | 4.90 | Dextrose, 180.1: 24, 30. | |
| 0.0305 | 3.61° | .5252 | 1.834 | 4.065 | 5.67 | 0.0198 | 1.84° |
| .1850 | 3.49 | 1.0891 | 1.826 | 4.657 | 6.19 | .0470 | 1.85 |
| .6861 | 3.30 | 1.760 | 1.83 | HNO₃, 63.05: 3, 13, 15. | | .1326 | 1.87 |
| .250 | 3.78 | 3.901 | 1.92 | 0.02004 | 3.55° | .4076 | 1.804 |
| .500 | 3.56 | 7.91 | 2.02 | .05015 | 3.50 | 1.102 | 1.921 |
| CdI₂, 366.1: 3, 5, 22 | | 11.11 | 2.12 | .0510 | 3.71 | Levulose, 180.1: 24, 25 | |
| 0.00210 | 4.5° | 18.76 | 1.81 | .1004 | 3.48 | 0.0201 | 1.87° |
| .00626 | 4.0 | 0.0173 | 1.80 | .1059 | 3.53 | .2050 | 1.871 |
| .02062 | 3.52 | .0778 | 1.79 | .2015 | 3.45 | .554 | 2.01 |
| .04857 | 2.70 | K₂CO₃, 138.30: 6 | | .250 | 3.50 | 1.384 | 2.32 |
| .1360 | 2.35 | 0.0100 | 5.1° | 500 | 3.62 | 2.77 | 3.04 |
| .333 | 2.13 | .0200 | 4.93 | 1.000 | 3.80 | C₁₂H₂₂O₁₁, 342.2: 1, 24, 26. | |
| .684 | 2.23 | .0500 | 4.71 | 2.000 | 4.17 | 0.000332 | 1.90° |
| .888 | 2.51 | .100 | 4.54 | 3.000 | 4.64 | .001410 | 1.87 |
| KI, 166.0: 9, 2. | | .200 | 4.39 | H₃PO₂, 66.0: 29. | | .009978 | 1.86 |
| 0.0651 | 3.5° | Na₂CO₃, 106.10: 6. | | 0.1260 | 2.90° | .0201 | 1.88 |
| .2782 | 3.50 | 0.0100 | 5.1° | .2542 | 2.75 | .1305 | 1.88 |
| .6030 | 3.42 | .0200 | 4.93 | .5171 | 2.59 | H₂SO₄, 98.08: | |
| 1.003 | 3.37 | .0500 | 4.64 | 1.071 | 2.45 | 13, 20, 31-33. | |
| SrI₂, 341.3: 22. | | 1.000 | 4.42 | H₃PO₃, 82.0: 4, 5. | | 0.00461 | 4.8° |
| 0.054 | 5.1° | .2000 | 4.17 | 0.0745 | 3.0° | .0100 | 4.49 |
| .108 | 5.2 | Na₂SO₄, 126.2: 28 | | .1241 | 2.8 | .0200 | 4.32 |
| .216 | 5.35 | 0.1044 | 4.51° | .2482 | 2.6 | .0461 | 4.10 |
| .327 | 5.52 | .3397 | 3.74 | 1.00 | 2.39 | .100 | 3.96 |
| NaOH, 40.06: 15 | | .7080 | 3.38 | H₃PO₄, 98.0: 6, 22 | | .200 | 3.85 |
| 0.02002 | 3.45° | Na₂HPO₄, 142.1: 22, 29 | | 0.0100 | 2.8° | .400 | 3.98 |
| .05005 | 3.45 | 0.01001 | 5.0° | .0200 | 2.68 | 1.000 | 4.10 |
| .1001 | 3.41 | .02003 | 4.84 | .0500 | 2.49 | 1.500 | 4.96 |
| .2000 | 3.407 | .05008 | 4.60 | .1000 | 2.36 | 2.000 | 5.65 |
| | | .1002 | 4.34 | .2000 | 2.25 | 2.500 | 6.53 |

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RISE OF BOILING POINT PRODUCED BY SALTS DISSOLVED IN WATER

This table gives the number of grams of the salt which, when dissolved in 100 grams of water, will raise the boiling point by the amount stated in the headings of the different columns. The pressure is supposed to be 76 centimeters.

| Salt | 1° C | 2° | 3 | 4 | 5 | 7 | 10 | 15° | 20 | 25 |
|--|-------|--------|----------------------|--------|-------------------------------|-------|-----------------------------|--------|-------------------|---------|
| BaCl ₂ + 2H ₂ O . . . | 15.0 | 31.4 | 47.3 | 63.5 | (71.6 gives 4° rise of temp.) | | | | | |
| CaCl ₂ . . . | 6.0 | 11.5 | 16.5 | 21.0 | 25.0 | 32.0 | 41.5 | 55.5 | 69.0 | 84.5 |
| Ca(NO ₃) ₂ + 2H ₂ O . . . | 12.0 | 25.5 | 39.5 | 53.5 | 68.5 | 101.0 | 152.5 | 240.0 | 331.5 | 443.5 |
| KOH . . . | 4.7 | 9.3 | 13.6 | 17.4 | 20.5 | 26.4 | 34.5 | 47.0 | 57.5 | 67.3 |
| KC ₂ H ₃ O ₂ . . . | 6.0 | 12.0 | 18.0 | 24.5 | 31.0 | 44.0 | 63.5 | 98.0 | 134.0 | 171.5 |
| KCl . . . | 9.2 | 16.7 | 23.4 | 29.9 | 36.2 | 48.4 | (57.4 gives a rise of 8°.5) | | | |
| K ₂ CO ₃ . . . | 11.5 | 22.5 | 32.0 | 40.0 | 47.5 | 60.5 | 78.5 | 103.5 | 127.5 | 152.5 |
| KClO ₃ . . . | 13.2 | 27.8 | 44.6 | 62.2 | | | | | | |
| KI . . . | 15.0 | 30.0 | 45.0 | 60.0 | 74.0 | 99.5 | 134 | 185.0 | (220 gives 18°.5) | |
| KNO ₃ . . . | 15.2 | 31.0 | 47.5 | 64.5 | 82.0 | 120.5 | 188.5 | 338.5 | | |
| K ₂ C ₄ H ₄ O ₆ + ½ H ₂ O . . . | 18.0 | 36.0 | 54.0 | 72.0 | 90.0 | 126.5 | 182.0 | 284.0 | | |
| KNaC ₄ H ₄ O ₆ . . . | 17.3 | 34.5 | 51.3 | 68.1 | 84.8 | 119.0 | 171.0 | 272.5 | 390.0 | 510.0 |
| KNaC ₄ H ₄ O ₆ + 4H ₂ O . . . | 25.0 | 53.5 | 84.0 | 118.0 | 157.0 | 266.0 | 554.0 | 5510.0 | | |
| LiCl . . . | 3.5 | 7.0 | 10.0 | 12.5 | 15.0 | 20.0 | 26.0 | 35.0 | 42.5 | 50.0 |
| LiCl + 2H ₂ O . . . | 6.5 | 13.0 | 19.5 | 26.0 | 32.0 | 44.0 | 62.0 | 92.0 | 123.0 | 160.5 |
| MgCl ₂ + 6H ₂ O . . . | 11.0 | 22.0 | 33.0 | 44.0 | 55.0 | 77.0 | 110.0 | 170.0 | 241.0 | 334.5 |
| MgSO ₄ + 7H ₂ O . . . | 41.5 | 87.5 | 138.0 | 196.0 | 262.0 | | | | | |
| NaOH . . . | 4.3 | 8.0 | 11.3 | 14.3 | 17.0 | 22.4 | 30.0 | 41.0 | 51.0 | 60.1 |
| NaCl . . . | 6.6 | 12.4 | 17.2 | 21.5 | 25.5 | 33.5 | (40.7 gives 8°.8 rise) | | | |
| NaNO ₃ . . . | 9.0 | 18.5 | 28.0 | 38.0 | 48.0 | | 99.5 | 156.0 | 222.0 | |
| NaC ₂ H ₃ O ₂ + 3H ₂ O . . . | 14.9 | 30.0 | 46.1 | 62.5 | 79.7 | 118.1 | 194.0 | 480.0 | 6250.0 | |
| Na ₂ S ₂ O ₃ . . . | 14.0 | 27.0 | 39.0 | 49.5 | 59.0 | 77.0 | 104.0 | 152.0 | 214.5 | 311.0 |
| Na ₂ HPO ₄ . . . | 17.2 | 34.4 | 51.4 | 68.4 | 85.3 | | | | | |
| Na ₂ C ₄ H ₄ O ₆ + 2H ₂ O . . . | 21.4 | 44.4 | 68.2 | 93.9 | 121.3 | 183.0 | (237.3 gives 8°.4 rise) | | | |
| Na ₂ S ₂ O ₃ + 5H ₂ O . . . | 23.8 | 50.0 | 78.6 | 108.1 | 139.3 | 216.0 | 400.0 | 1765.0 | | |
| Na ₂ CO ₃ + 10H ₂ O . . . | 34.1 | 86.7 | 177.6 | 369.4 | 1052.9 | | | | | |
| Na ₂ B ₄ O ₇ + 10H ₂ O . . . | 39. | 93.2 | 254.2 | 898.5 | (5555.5 gives 4°.5 rise) | | | | | |
| NH ₄ Cl . . . | 6.5 | 12.8 | 19.0 | 24.7 | 29.7 | 39.6 | 56.2 | 88.5 | | |
| NH ₄ NO ₃ . . . | 10.0 | 20.0 | 30.0 | 41.0 | 52.0 | 74.0 | 108.0 | 172.0 | 248.0 | 337.0 |
| (NH ₄) ₂ SO ₄ . . . | 15.4 | 30.1 | 44.2 | 58.0 | 71.8 | 99.1 | (115.3 gives 108.2) | | | |
| SrCl ₂ + 6H ₂ O . . . | 20.0 | 40.0 | 60.0 | 81.0 | 103.0 | 150.0 | 234.0 | 524.0 | | |
| Sr(NO ₃) ₂ . . . | 24.0 | 45.0 | 63.6 | 81.4 | 97.6 | | | | | |
| C ₄ H ₆ O ₆ . . . | 17.0 | 34.4 | 52.0 | 70.0 | 87.0 | 123.0 | 177.0 | 272.0 | 374.0 | 484.0 |
| C ₂ H ₂ O ₄ + 2H ₂ O . . . | 19.0 | 40.0 | 62.0 | 86.0 | 112.0 | 166.0 | 262.0 | 540.0 | 1316.0 | 50000.0 |
| C ₆ H ₈ O ₇ + H ₂ O . . . | 29.0 | 58.0 | 87.0 | 116.0 | 145.0 | 208.0 | 320.0 | 553.0 | 952.0 | |
| Salt | 40° | 60° | 80° | 100° | 120 | 140 | 160° | 180 | 200 | 240 |
| CaCl ₂ . . . | 137.5 | 222.0 | 314.0 | | | | | | | |
| KOH . . . | 92.5 | 121.7 | 152.6 | 185.0 | 219.8 | 263.1 | 312.5 | 375.0 | 444.4 | 623.0 |
| NaOH . . . | 93.5 | 150.8 | 230.0 | 345.0 | 526.3 | 800.0 | 1333.0 | 2353.0 | 6452.0 | - |
| NH ₄ NO ₃ . . . | 682.0 | 1370.0 | 2400.0 | 4099.0 | 8547.0 | ∞ | | | | |
| C ₄ H ₆ O ₆ . . . | 980.0 | 3774.0 | (infinity gives 170) | | | | | | | |

* Compiled from a paper by Gerlach, "Zeit. f. Anal. Chem." vol. 26.

FREEZING MIXTURES *

Column 1 gives the name of the principal refrigerating substance, *A* the proportion of that substance, *B* the proportion of a second substance named in the column, *C* the proportion of a third substance, *D* the temperature of the substances before mixture, *E* the temperature of the mixture, *F* the lowering of temperature, *G* the temperature when all snow is melted, when snow is used, and *H* the amount of heat absorbed in heat units (small calories when *A* is grams). Temperatures are in Centigrade degrees.

| Substance. | <i>A</i> | <i>B</i> | <i>C</i> | <i>D</i> | <i>E</i> | <i>F</i> | <i>G</i> | <i>H</i> |
|---|----------|---------------------------|-----------------------------|----------|----------|----------|----------|----------|
| $\text{NaC}_2\text{H}_3\text{O}_2$ (cryst.) | 85 | $\text{H}_2\text{O}-100$ | - | 10.7 | -4.7 | 15.4 | - | - |
| NH_4Cl | 30 | " " | - | 13.3 | -5.1 | 18.4 | - | - |
| NaNO_3 | 75 | " " | - | 13.2 | -5.3 | 18.5 | - | - |
| $\text{Na}_2\text{S}_2\text{O}_3$ (cryst.) | 110 | " " | - | 10.7 | -8.0 | 18.7 | - | - |
| KI | 140 | " " | - | 10.8 | -11.7 | 22.5 | - | - |
| CaCl_2 (cryst.) | 250 | " " | - | 10.8 | -12.4 | 23.2 | - | - |
| NH_4NO_3 | 60 | " " | - | 13.6 | -13.6 | 27.2 | - | - |
| $(\text{NH}_4)_2\text{SO}_4$ | 25 | " 50 | $\text{NH}_4\text{NO}_3-25$ | - | - | 26.0 | - | - |
| NH_4Cl | 25 | " " | " " | - | - | 22.0 | - | - |
| CaCl_2 | 25 | " " | " " | - | - | 20.0 | - | - |
| KNO_3 | 25 | " " | $\text{NH}_4\text{Cl}-25$ | - | - | 20.0 | - | - |
| Na_2SO_4 | 25 | " " | " " | - | - | 19.0 | - | - |
| NaNO_3 | 25 | " " | " " | - | - | 17.0 | - | - |
| K_2SO_4 | 10 | Snow 100 | - | -1 | -1.9 | 0.9 | - | - |
| Na_2CO_3 (cryst.) | 20 | " " | - | -1 | -2.0 | 1.0 | - | - |
| KNO_3 | 13 | " " | - | -1 | -2.85 | 1.85 | - | - |
| CaCl_2 | 30 | " " | - | -1 | -10.9 | 9.9 | - | - |
| NH_4Cl | 25 | " " | - | -1 | -15.4 | 14.4 | - | - |
| NH_4NO_3 | 45 | " " | - | -1 | -16.75 | 15.75 | - | - |
| NaNO_3 | 50 | " " | - | -1 | -17.75 | 16.75 | - | - |
| NaCl | 33 | " " | - | -1 | -21.3 | 20.3 | - | - |
| $\text{H}_2\text{SO}_4 + \text{H}_2\text{O}$ (66.1 % H_2SO_4) | 1 | " 1.097 | - | -1 | -37.0 | 36.0 | -37.0 | 0.0 |
| | 1 | " 1.26 | - | -1 | -36.0 | 35.0 | -30.2 | 17.0 |
| | 1 | " 1.38 | - | -1 | -35.0 | 34.0 | -25.0 | 27.0 |
| | 1 | " 2.52 | - | -1 | -30.0 | 29.0 | -12.4 | 133.0 |
| | 1 | " 4.32 | - | -1 | -25.0 | 24.0 | -7.0 | 273.0 |
| | 1 | " 7.92 | - | -1 | -20.0 | 19.0 | -3.1 | 553.0 |
| | 1 | " 13.68 | - | -1 | -16.0 | 15.0 | -2.1 | 967.0 |
| $\text{CaCl}_2 + 6\text{H}_2\text{O}$ | 1 | " 0.35 | - | 0 | - | - | 0.0 | 52.1 |
| | 1 | " .49 | - | 0 | - | - | -19.7 | 49.5 |
| | 1 | " .61 | - | 0 | - | - | -39.0 | 40.3 |
| | 1 | " .70 | - | 0 | - | - | -54.9† | 30.0 |
| | 1 | " .81 | - | 0 | - | - | -40.3 | 46.8 |
| | 1 | " 1.23 | - | 0 | - | - | -21.5 | 88.5 |
| | 1 | " 2.46 | - | 0 | - | - | -9.0 | 192.3 |
| Alcohol at 4° | 1 | " 4.92 | - | 0 | - | - | -4.0 | 392.3 |
| | 77 | " 73 | - | 0 | -30.0 | - | - | - |
| | - | CO_2 solid | - | - | -72.0 | - | - | - |
| Chloroform | - | " " | - | - | -77.0 | - | - | - |
| Ether | - | " " | - | - | -77.0 | - | - | - |
| Liquid SO_2 | - | " " | - | - | -82.0 | - | - | - |
| NH_4NO_3 | 1 | $\text{H}_2\text{O}-75$ | - | 20 | 5.0 | - | - | 33.0 |
| | 1 | " .94 | - | 20 | -4.0 | - | - | 21.0 |
| | 1 | " " | - | 10 | -4.0 | - | - | 34.0 |
| | 1 | " " | - | 5 | -4.0 | - | - | 40.5 |
| | 1 | Snow " | - | 0 | -4.0 | - | - | 122.2 |
| | 1 | $\text{H}_2\text{O}-1.20$ | - | 10 | -14.0 | - | - | 17.9 |
| | 1 | Snow " | - | 0 | -14.0 | - | - | 129.5 |
| | 1 | $\text{H}_2\text{O}-1.31$ | - | 10 | -17.5† | - | - | 10.6 |
| | 1 | Snow " | - | 0 | -17.5† | - | - | 131.9 |
| | 1 | $\text{H}_2\text{O}-3.61$ | - | 10 | -8.0 | - | - | 0.4 |
| | 1 | Snow " | - | 0 | -8.0 | - | - | 327.0 |

* Compiled from the results of Cailliet and Colardeau, Hamnerl, Hanamann, Moritz, Pfandner, Rudolf, and Tollinger.

† Lowest temperature obtained.

SMITHSONIAN TABLES.

CRITICAL TEMPERATURES, PRESSURES, AND DENSITIES OF GASES

| Substance | t | P | d | Ref. |
|----------------------------|--------|-------|--------------------|---------|
| Acetylene..... | 36 | 62 | 0.231 | 1 |
| Air..... | -140.7 | 37.2 | .35 (a) .31 (b) | 1 1 |
| Alcohol (C_2H_6O)..... | 243.1 | 63.1 | .2755 | 6, 7 |
| Alcohol (CH_3O)..... | 240.0 | 78.7 | .272 | 7, 8 |
| Allylene..... | 128 | | | 1 |
| Ammonia..... | 132.4 | 111.5 | .235 | 1 |
| Argon..... | -122 | 48 | .531 | 1 |
| Benzene..... | 288.5 | 47.7 | .304 | 9 |
| Bromine..... | 302 | | | 9 |
| iso-Butane..... | 134 | 37 | | 1 |
| n-Butane..... | 153 | 36 | | 1 |
| Carbon dioxide..... | 31.1 | 73.0 | .4681 | 1, 2 |
| Carbon disulphide..... | 273 | 76 | | 9 |
| Carbon monoxide..... | -139 | 35 | .311 | 1 |
| Chlorine..... | 144.0 | 76.1 | .573 | 1 |
| Chloroform..... | 263 | | .516 | 9 |
| Cyanogen..... | 128 | 59 | | 1 |
| Ethane..... | 32.1 | 48.8 | .21? | 1 |
| Ether (ethyl)..... | 193.8 | 35.5 | .2625 | 10, 11 |
| Ethyl chloride..... | 187.2 | 52 | .33 | 1 |
| Ethylene..... | 9.7 | 50.9 | .2159 | 1, 3 |
| Helium..... | -267.9 | 2.26 | .0693 | 1 |
| Hydrogen..... | -239.9 | 12.8 | .0310 | 1 |
| Hydrogen bromide..... | 90 | 84 | | 1 |
| Hydrogen chloride..... | 51.4 | 81.6 | .42 | 1 |
| Hydrogen iodide..... | 151 | 82 | | 1 |
| Hydrogen sulphide..... | 100.4 | 88.9 | | 1 |
| Krypton..... | -63? | 54? | .78? | 1 |
| Methane..... | -82.5 | 45.8 | .162 | 1 |
| Methyl chloride..... | 143.1 | 65.8 | .37? | 1 |
| Neon..... | -228.7 | 25.9 | .484 | 1 |
| Nitric oxide..... | -94? | 65 | .52? | 1 |
| Nitrogen..... | -147.1 | 33.5 | .3110 | 1 |
| Nitrous oxide..... | 36.5 | 71.7 | .45? | 1 |
| Oxygen..... | -118.8 | 49.7 | .430 | 1 |
| Phosgene..... | 182 | 56 | .52 | 1 |
| Propane..... | 95.6 | 43 | | 1 |
| Propylene..... | 92.3 | 45.0 | | 1 |
| Sulphur dioxide..... | 157.4 | 77.8 | .5240 | 1, 4, 5 |
| Water..... | 374.0 | 217.7 | .4 | 9 |
| Xenon..... | 16.6 | 58.2 | 1.155 | 1 |

(a) "Plait point."

(b) "Critical point of contact."

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(Table prepared by Gas Chemistry Section, Bur. Standards, Feb. 19, 1929.)

THERMAL CONDUCTIVITY, METALS AND ALLOYS

The coefficient k is the quantity of heat in small calories which is transmitted per second through a plate one centimeter thick per square centimeter of its surface when the difference of temperature between the two faces of the plate is one degree Centigrade. The coefficient k is found to vary with the absolute temperature of the plate, and is expressed approximately by the equation $k_t = k_0[1 + \alpha(t - t_0)]$. k_0 is the conductivity at t_0 , the lower temperature of the bracketed pairs in the table, k_t that at temperature t , and α is a constant. k_t in g.-cal. per degree C per sec. across cm cube = $0.239 \times k_t$ in watts per degree C per sec. across cm cube.

| Substance | $t^\circ\text{C}$ | k_t | α | Refer- ence | Substance | $t^\circ\text{C}$ | k_t | α | Refer- ence |
|-----------------------------|-------------------|--------|----------|----------------|-----------------|-------------------|--------|----------|----------------|
| Aluminum.... | -160 | 0.514 | — | 1 | Mercury.... | 0 | 0.0148 | + 0055 | 7 |
| "..... | 18 | 0.480 | — | 2 | "..... | 50 | 0.0189 | — | 6 |
| "..... | 100 | 0.492 | + .0030 | 3 | Molybdenum | 17 | 0.346 | - .0001 | 1 |
| "..... | 200 | 0.545 | — | 3 | Nickel..... | -160 | 0.129 | — | 2 |
| "..... | 400 | 0.760 | — | 3 | "..... | 18 | 0.1420 | — | 3 |
| "..... | 500 | 0.885 | — | 3 | "..... | 0 | 0.1425 | - .00032 | 3 |
| "..... | 600 | 1.01 | + .0014 | 3 | "..... | 100 | 0.1380 | — | 3 |
| Antimony.... | 0 | 0.0442 | — | 4 | "..... | 200 | 0.1325 | - .00095 | 3 |
| "..... | 100 | 0.0396 | - .00104 | 4 | "..... | 700 | 0.069 | — | 3 |
| Bismuth..... | -186 | 0.025 | — | 5 | "..... | 1000 | 0.064 | - .00047 | 3 |
| "..... | 18 | 0.0194 | — | 5 | "..... | 1200 | 0.058 | — | 2 |
| "..... | 100 | 0.0161 | - .0021 | 2 | Palladium... | 18 | 0.1683 | + .0010 | 2 |
| Brass..... | -160 | 0.181 | — | 1 | "..... | 100 | 0.182 | — | 2 |
| "..... | 17 | 0.260 | — | 1 | Platinum.... | 18 | 0.1664 | + .00051 | 2 |
| "....., yellow... | 0 | 0.204 | + .0024 | 4 | "..... | 100 | 0.1733 | — | 6 |
| "....., red.... | 0 | 0.246 | + .0015 | 4 | Pt 10% Ir... | 17 | 0.074 | + .0002 | 6 |
| Cadmium, pure | -160 | 0.239 | — | 1 | Pt 10% Rh... | 17 | 0.072 | + .0002 | 6 |
| "..... | 18 | 0.222 | — | 1 | Platinoid... | 18 | 0.060 | — | 1 |
| "..... | 100 | 0.215 | - .00038 | 2 | Potassium.... | 5.0 | 0.232 | — | 8 |
| Constantan... (60 Cu+40 Ni) | 18 | 0.0540 | — | 2 | "..... | 57.4 | 0.216 | - .0013 | 8 |
| "..... | 100 | 0.0640 | + .00227 | 2 | Rhodium.... | 17 | 0.210 | - .0010 | 6 |
| Copper,* pure. | -160 | 1.079 | — | 1 | Silver, pure... | -160 | 0.998 | — | 1 |
| "..... | 18 | 0.918 | — | 1 | "..... | 18 | 1.006 | - .00017 | 2 |
| "..... | 100 | 0.908 | - .00013 | 2 | "..... | 100 | 0.992 | — | 2 |
| German silver. | 0 | 0.070 | + .0027 | 4 | Sodium..... | 5.7 | 0.321 | — | 8 |
| Gold..... | 17 | 0.795 | - .00007 | 6 | "..... | 88.1 | 0.288 | - .0012 | 8 |
| Graphite..... | 17 | 0.037 | + .0003 | 6 | Tantalum.... | 17 | 0.130 | - .0001 | 6 |
| Iridium..... | 17 | 0.141 | - .0005 | 8 | "..... | 1700 | 0.174 | — | 9 |
| Iron,† pure... | 18 | 0.161 | — | 2 | "..... | 1900 | 0.186 | + .00032 | 9 |
| "..... | 100 | 0.151 | - .0008 | 2 | "..... | 2100 | 0.198 | — | 4 |
| Iron, wrought. | -160 | 0.152 | — | 1 | Tin..... | 0 | 0.155 | - .00069 | 4 |
| "..... | 18 | 0.144 | — | 1 | "..... | 100 | 0.145 | — | 1 |
| "..... | 100 | 0.143 | - .00008 | 2 | "....., pure... | -160 | 0.192 | — | 6 |
| " steel, 1% C..... | 18 | 0.108 | — | 2 | Tungsten.... | 17 | 0.476 | - .0001 | 10 |
| "..... | 100 | 0.107 | - .0001 | 2 | "..... | 1600 | 0.249 | + .00023 | 10 |
| Lead, pure.... | -160 | 0.092 | — | 1 | "..... | 2000 | 0.272 | — | 10 |
| "..... | 18 | 0.083 | — | 1 | "..... | 2400 | 0.294 | + .00016 | 10 |
| "..... | 100 | 0.081 | - .0001 | 2 | "..... | 2800 | 0.313 | — | 7 |
| Magnesium.... | 0 to 100 | 0.376 | — | 4 | Wood's alloy | — | 0.319 | — | 1 |
| Manganin.... | -160 | 0.035 | — | 1 | Zinc, pure... | -160 | 0.278 | — | 2 |
| " (84 Cu+4 Ni 12 Mn) | 18 | 0.0519 | — | 1 | "..... | 18 | 0.2653 | - .00016 | 2 |
| "..... | 100 | 0.0630 | + .0026 | 2 | "..... | 100 | 0.2610 | — | 2 |

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* Copper: 100-197° C, $k_t = 1.043$; 100-268°, 0.969; 100-370°, 0.931; 100-541°, 0.902 (Hering; for reference see next page).

† Iron: 100-727° C, $k_t = 0.202$; 100-912°, 0.184; 100-1245°, 0.191 (Hering).

TABLE 252.—Thermal Conductivity of Insulators at High Temperatures

(See also Table 251 for metals; k in gram-calories per degree centigrade per second across a centimeter cube.)

| Material. | Temperature, °C | k | Reference. | Material. | Temperature, °C | k | Reference. |
|--------------------------|--------------------|-----------|------------|-----------------------|--------------------|-------------|------------|
| Amorphous carbon... | 37-163 | .028-.003 | 1 | Brick: Carborundum | 150-1200 | .0032-.027 | 3 |
| | 170-330 | .027-.004 | 1 | Building | | | |
| | 240-523 | .020-.003 | 1 | Terra-cotta | 15-1100 | .0018-.0038 | 3 |
| | 283-507 | .011-.004 | 1 | Fire-clay... | 125-1220 | .0032-.0054 | 3 |
| | 100-300 | .089 | 2 | Gas-retort... | 100-1125 | .0038 | 3 |
| | 100-751 | .124 | 2 | Graphite... | 300-700 | .024 | 3 |
| Graphite (artificial)... | 100-842 | .120 | 2 | Magnesia... | 50-1130 | .0027-.0072 | 3 |
| | 100-390 | .338 | 2 | Silica... | 100-1000 | .002-.0033 | 3 |
| | 100-740 | .324 | 2 | Granite..... | 100 | .0045-.0050 | 4 |
| | 100-720 | .306 | 2 | | 200 | .0043-.0097 | 4 |
| | 100-914 | .291 | 2 | | 500 | .0040 | 4 |
| | 30-2830 | .162 | 1 | Limestone..... | 40 | .0046-.0057 | 4 |
| | 2800-3200 | .002 | 1 | | 100 | .0039-.0040 | 4 |
| | 90-110 | .55-.45 | 1 | | 350 | .0032-.0035 | 4 |
| | 180-120 | .44-.34 | 1 | Porcelain (Sèvres)... | 165-1055 | .0039-.0047 | 3 |
| | 500-700 | .31-.22 | 1 | Stoneware mixtures. | 70-1000 | .0029-.0053 | 3 |

References: (1) Hansen, Tr. Am. Electrochem. Soc. 16, 329, 1909; (2) Hering, Tr. Am. Inst. Elect. Eng. 1910; (3) Bul. Soc. Encouragement, 111, 879, 1909; Electroch. and Met. Ind. 7, 383, 433, 1909; (4) Poole, Phil. Mag. 24, 45, 1912; see also Clement, EGY. Eng. Exp. Univ. Ill. Bull. 36, 1909; Dewey, Progressive Age, 27, 772, 1909; Woolson, Eng. News, 58, 166, 1907, heat transmission by concretes; Richards, Met. and Chem. Eng. 11, 575, 1913. The ranges in values under 1 do not depend on variability in material but on possible errors in method; reduced from values expressed in other units.

TABLE 253.—Thermal Conductivity of Various Substances

| Substance, temperature. | k | Reference. | Substance, temperature. | k | Reference. |
|--|----------|------------|--|--------|------------|
| Aniline BP 183° C, -160..... | .000112 | 1 | Naphthalene MP 79° C, -160..... | .0013 | 1 |
| Carbon, gas..... | .010 | — | Naphthalene MP 79° C, 0..... | .00081 | 1 |
| Carbon, graphite..... | .012 | — | Naphthol- β , MP 122° C, -160..... | .00068 | 1 |
| Carborundum..... | .00050 | 2 | Naphthol, 0..... | .00062 | 1 |
| Concrete, cinder..... | .00081 | — | Nitrophenol, MP 114° C, -160..... | .00106 | 1 |
| stone..... | .0022 | 3 | Nitrophenol, 0..... | .00065 | 1 |
| Diatomaceous earth..... | .00013 | 4 | Paraffin MP 54° C, -160..... | .00062 | 1 |
| Earth's crust..... | .004 | — | Paraffin, 0..... | .00050 | 1 |
| Fire-brick..... | .00028 | 4 | Porcelain..... | .0025 | — |
| Fluorite, -190..... | .093 | 5 | Quartz \perp to axis, -190..... | .0586 | 5 |
| Fluorite, 0..... | .025 | 5 | " 0..... | .0173 | 5 |
| Glass: window..... | .0025 | 5 | " 100..... | .0133 | 5 |
| crown, 0.572, -190..... | .00118 | — | Quartz \parallel to axis, 0..... | .0325 | 5 |
| crown, 0.572, 0..... | .00280 | 5 | Rock salt, 0..... | .0167 | 5 |
| crown, 0.572, 100..... | .00324 | 5 | Rock salt, 30..... | .0150 | 5 |
| h'vy flint 0.165, -190..... | .00031 | 5 | Rubber, vulcanized, -160..... | .00033 | 5 |
| h'vy flint 0.165, 0..... | .00170 | 5 | Rubber, 0..... | .00037 | 5 |
| h'vy flint 0.165, 100..... | .00181 | 5 | Rubber, para..... | .00045 | — |
| Glycerine, -160..... | .00077 | 1 | Sand, white, dry..... | .00093 | 0 |
| Granite..... | .0053 | 6 | Sandstone, dry..... | .0055 | 6 |
| Ice, -160..... | .0066 | 1 | Sawdust..... | .00012 | — |
| Ice, 0..... | .0050 | 1 | Slate \perp to cleavage..... | .0034 | 6 |
| Iceland spar, -190..... | .038 | 5 | Slate \parallel to cleavage..... | .0060 | 0 |
| Iceland spar, 0..... | .0103 | 5 | Snow, fresh, dens. = 0.11..... | .00026 | 7 |
| Lime..... | .00029 | 4 | Snow, old..... | .0012 | 7 |
| Limestones, calcite }..... | .0047 to | 0 | Soil, average, sl't moist..... | .0037 | — |
| Marbles, dolomite }..... | .0056 | 6 | Soil, very dry..... | .0037 | — |
| Mica..... | .00018 | — | Sulphur, rhombic, 0..... | .00070 | 5 |
| Flagstone \perp to cleavage..... | .0063 | 6 | Vaseline, 20..... | .00022 | 8 |
| Micaceous \parallel to cleavage..... | .0044 | 6 | Vulcanite..... | .00057 | 9 |

References: (1) Lees, Tr. R. S. 1905; (2) Lorenz; (3) Norton; (4) Hutton, Bland; (5) Eucken, Ann. d. Phys., 1911; (6) Herschel, Lebour, Dunn, B. A. Committee, 1879; (7) Jansson, 1904; (8) Melmer, 1911; (9) Stefan.

THERMAL CONDUCTIVITY OF INSULATING MATERIALS

(Compiled from the International Critical Tables, which see for more complete data.)

| No. | Material | Density g/cm ³ | t°C | Conductivity | |
|-----|--|------------------------------|------|-----------------------------|------------------------------|
| | | | | joule/cm ² /sec. | g-cal./cm ² /sec. |
| 1 | Air, 76 cm Hg. | .00129 | 0 | .00023 | .000055 |
| 2 | Asbestos wool. | .40 | -100 | .00068 | .000162 |
| 3 | " " | .40 | 0 | .00090 | .000215 |
| 4 | " " | .40 | +100 | .00101 | .00024 |
| 5 | " with 85 per cent MgO. | .3 | 30 | .00075 | .000179 |
| 6 | Brick, very porous, dry. | .71 | 20 | .00174 | .00042 |
| 7 | " machine made, dry. | 1.54 | 0 | .00038 | .000091 |
| 8 | " " moist | | | | |
| | 1.2% vol. | | 50 | .00096 | .00023 |
| 9 | Calorox, fluffy mineral matter. | .064 | 30 | .00032 | .000076 |
| 10 | Celluloid, white. | 1.4 | 30 | .00021 | .000050 |
| 11 | Cement mortar. | 2.0 | 90 | .0055 | .0013 |
| 12 | Chalk. | | | .0092 | .0022 |
| 13 | Charcoal. | .18 | 20 | .00055 | .00013 |
| 14 | Coke dust. | 1.0 | 20 | .0015 | .00036 |
| 15 | Concrete. | 1.6 | 0 | .008 | .002 |
| 16 | Cork. | .05 | 0 | .00032 | .000076 |
| 17 | " " | .05 | 100 | .00041 | .000098 |
| 18 | " " | .35 | 0 | .00061 | .000146 |
| 19 | " " | .35 | 100 | .00079 | .000189 |
| 20 | Cotton, tightly packed. | .08 | -150 | .00038 | .000091 |
| 21 | " " " | .08 | 0 | .00056 | .000133 |
| 22 | " " " | .08 | +150 | .00076 | .00018 |
| 23 | Cotton wool, tightly packed. | .08 | 30 | .00042 | .00010 |
| 24 | Diatomite, (binders may increase 100%) | .20 | 0 | .00052 | .00012 |
| 25 | Diatomite, ditto. | .20 | 400 | .00094 | .00022 |
| 26 | " " | .50 | 0 | .00086 | .00021 |
| 27 | " " | .50 | 400 | .00157 | .00037 |
| 28 | Ebonite. | 1.19 | -190 | .00138 | .00033 |
| 29 | " " | 1.19 | -78 | .00157 | .00038 |
| 30 | " " | 1.19 | 0 | .00160 | .00038 |
| 31 | Felt, flax fibers. | .18 | 30 | .00047 | .00011 |
| 32 | " hair. | .27 | 30 | .00036 | .000086 |
| 33 | " wool. | .15 | 40 | .00063 | .000151 |
| 34 | " " | .33 | 30 | .00052 | .000124 |
| 35 | Fuller's earth. | .53 | 30 | .00101 | .00024 |
| 36 | Glass, lead. | | 15 | .0060 | .00143 |
| 37 | " soda. | 2.59 | 20 | .0072 | .00172 |
| 38 | " " | 2.59 | 100 | .0076 | .00182 |
| 39 | " wool. | .22 | 50 | .00042 | .000100 |
| 40 | " " | .22 | 100 | .00050 | .000120 |
| 41 | " " | .22 | 200 | .00065 | .000155 |
| 42 | " " | .22 | 300 | .00081 | .000195 |
| 43 | Graphite, 100 mesh. | .48 | 40 | .0018 | .00044 |
| 44 | " 40 | .42 | 40 | .0038 | .00093 |
| 45 | " 20 to 40 mesh. | .70 | 40 | .0129 | .0031 |
| 46 | Horsehair, compressed. | .17 | 20 | .00051 | .000122 |
| 47 | Ice. | .92 | 0 | .022 | .0053 |
| 48 | Leather, chamois. | | 85 | .00063 | .000151 |
| 49 | " cowhide. | | 85 | .00176 | .000421 |
| 50 | " sole. | 1.0 | 30 | .0016 | .00038 |
| 51 | Linen. | | 20 | .00086 | .00021 |
| 52 | Linoleum, cork. | .54 | 20 | .00080 | .000191 |
| 53 | Mica, average. | | 50 | .0050 | .0012 |

THERMAL CONDUCTIVITY OF INSULATING MATERIALS

| No. | Material | Density g/cm ³ | t°C | Conductivity | |
|-----|---------------------------------|------------------------------|------|-----------------------------|------------------------------|
| | | | | joule/cm ² /sec. | g-cal./cm ² /sec. |
| 54 | Micanite..... | | 30 | .0021- | .000050- |
| 55 | Mineral wool..... | .15 | 30 | .0042 | .00010 |
| 56 | "..... | .30 | | .00042 | .00010 |
| 57 | Paper, rice..... | | 40 | .00052 | .00012 |
| 58 | " blotting..... | | 20 | .00046 | .00011 |
| 59 | Paraffin wax..... | .89 | 30 | .00063 | .00015 |
| 60 | Peat, dry..... | .19 | 30 | .0023 | .00055 |
| 61 | " blocks..... | .84 | 20 | .00052 | .00012 |
| 62 | Porcelain..... | | 90 | .0017 | .00041 |
| 63 | Rubber, rigid sponge, hard..... | .09 | 25 | .0104 | .0025 |
| 64 | " sponge, vulcanized..... | .22 | 20 | .00037 | .000088 |
| 65 | " commercial, 40% rubber..... | | 25 | .00054 | .00013 |
| 66 | " " 92% "..... | | 25 | .0028 | .00067 |
| 67 | Sawdust..... | .20 | 30 | .0016 | .00038 |
| 68 | Shellac..... | | | .00060 | .000143 |
| 69 | Silk..... | | | .0023 | .0006 |
| 70 | " scrap from spinning mill..... | .10 | -200 | .00040 | .00010 |
| 71 | " " " " " "..... | .10 | -100 | .00023 | .000055 |
| 72 | " " " " " "..... | .10 | 0 | .00037 | .000088 |
| 73 | " " " " " "..... | .10 | 50 | .000495 | .000118 |
| 74 | Snow..... | .25 | 0 | .00056 | .000134 |
| 75 | Steel wool..... | .15 | 55 | .0016 | .00038 |
| 76 | "..... | .08 | 55 | .00080 | .000191 |
| 77 | Wool, pure..... | .09 | 30 | .00090 | .00022 |
| 78 | " " very loose packing..... | .04 | 30 | .00036 | .000086 |
| 79 | Woods: Ash ⊥ to grain..... | .74 | 20 | .00042 | .00010 |
| 80 | " " " " " "..... | .74 | 20 | .0017 | .00041 |
| 81 | Balsa ⊥ to grain..... | .11 | 30 | .0031 | .00074 |
| 82 | Boxwood..... | .90 | 20 | .00045 | .000084 |
| 83 | Cedar ⊥ to grain..... | .48 | | .0015 | .00036 |
| 84 | Cypress ⊥ to grain..... | .46 | 30 | .0011 | .00027 |
| 85 | Fir ⊥ to grain..... | .54 | 20 | .00096 | .00023 |
| 86 | " " to grain..... | .54 | 20 | .0014 | .00033 |
| 87 | Lignum vitae..... | 1.16 | 20 | .0035 | .00081 |
| 88 | "..... | 1.16 | 100 | .0025 | .00060 |
| 89 | Mahogany, ⊥ to grain..... | .70 | 20 | .0030 | .00072 |
| 90 | " " to grain..... | .70 | 20 | .0016 | .00038 |
| 91 | Oak, ⊥ to grain..... | .82 | 15 | .0031 | .00074 |
| 92 | " " to grain..... | .82 | 15 | .0021 | .00050 |
| 93 | Pine, pitch, ⊥ to grain..... | | 30 | .0036 | .00086 |
| 94 | " Virginia, ditto..... | .55 | 30 | .0015 | .00036 |
| 95 | " white, ditto..... | .45 | 60 | .0014 | .00033 |
| 96 | " " to grain..... | .45 | 60 | .0011 | .00026 |
| 97 | Spruce, ⊥ to grain..... | .41 | | .0026 | .00062 |
| 98 | Teak, ⊥ to grain..... | .64 | 15 | .0011 | .00026 |
| 99 | " " to grain..... | .64 | 15 | .00175 | .00042 |
| 100 | Walnut, ⊥ to grain..... | .65 | 20 | .0038 | .00091 |
| 101 | Rocks: Basalt..... | | 20 | .0014 | .00033 |
| 102 | Chalk..... | | | .020 | .0048 |
| 103 | Granite..... | 2.8 | | .0092 | .0022 |
| 104 | Limestone, very variable..... | 2.0 | 20 | .022 | .0053 |
| 105 | Slate, ⊥ to cleavage..... | | 95 | .010 | .0024 |
| 106 | " " to cleavage..... | | 95 | .014 | .0033 |
| 107 | Sandstone, air-dried..... | 2.2 | 20 | .025 | .0060 |
| 108 | " freshly cut..... | 2.3 | 20 | .013 | .00031 |
| | | | | .017 | .00041 |

Running numbers arranged in order of increasing conductivity at room temperatures: .0002: 10, 1, 16, 9, 32, 77, 7, 63, 69, 30, 55, 78, 81, 37, 31, 50, 72, 81; .0005: 46, 24, 50, 34, 60, 04, 13, 21, 67, 18, 33, 58; .00075: 5, 52, 26, 51, 3, 76, 84; .001: 35, 83, 97, 85, 94, 100, 14, 82, 93, 30, 50, 60, 74, 89, 61, 79, 6, 43, 98, 54, 91, 59, 68; .0025: 87, 65, 80, 90, 86, 44, 36, 92, 99, 54; .005: 53, 36, 37, 15, 12, 102; .010: 104, 45, 107, 108, 101, 47, 103.

TABLE 255.—Thermal Conductivity of Various Insulators

k_t is the heat in gram-calories flowing in 1 sec. through a plate 1 cm thick per sq. cm for 1°C drop in temperature.

| Substance. | Density. | °C | k_t | Substance. | k_t | Authority. |
|--|----------|-----|---------|---------------------------------|---------|----------------|
| Asbestos fiber | 0.201 | 500 | .00019 | Asbestos paper | 0.00043 | Lees-Chorlton. |
| 85% magnesia asbestos | .216 | 100 | .00016 | Blotting paper | .00015 | |
| Cotton | .021 | 500 | .00017 | Portland cement | .00071 | Forbes. |
| " | .101 | 100 | .000111 | Cork, t, 60°C | .00072 | |
| Eiderdown | .0021 | " | .000071 | Chalk | .00020 | H, L, D, |
| " | .109 | 150 | .00015 | Ebonite, t, 49° | .00037 | see p. 205. |
| Lampblack, Cabot number 5 | .193 | " | .000046 | Glass, mean | .002 | |
| Quartz, mesh 200 | 1.05 | 100 | .000074 | Ice | .0057 | Neumann. |
| Poplox, popped Na_2SiO_3 | 0.093 | 500 | .000107 | Leather, cow-hide | .00042 | |
| Wool fibers | .015 | 300 | .00024 | Leather, horse | .00015 | Lees-Chorlton. |
| " | .054 | 200 | .000041 | Linen | .00021 | |
| " | .192 | 500 | .000160 | Silk | .000095 | H, L, D. |
| " | " | 100 | .000118 | Caen stone, limestone | .0043 | |
| " | " | " | .000085 | Free stone, sandstone | .0021 | |
| " | " | " | .000054 | | | |

Left-hand half of table from Randolph, Tr. Am. Electroch. Soc. XXI, p. 550, 1912; k_t (Randolph's values) is mean conductivity between given temperature and about 10°C. Note effect of compression (density). The following are from Barratt Proc. Phys. Soc., London, 27, 81, 1914.

| Substance. | Density. | k_t | | Substance. | Density. | k_t | |
|-------------------------|----------|---------|----------|----------------------|----------|---------|----------|
| | | at 20°C | at 100°C | | | at 20°C | at 100°C |
| Brick, fire | 1.73 | .00110 | .00109 | Boxwood | 0.90 | .00036 | .00041 |
| Carbon, gas | 1.42 | .00085 | .00095 | Greenheart | 1.08 | .00112 | .00110 |
| Ebonite | 1.19 | .00014 | .00013 | Lignumvite | 1.16 | .00060 | .00072 |
| Fiber, red | 1.29 | .00112 | .00119 | Mahogany | 0.55 | .00051 | .00060 |
| Glass, soda | 2.52 | .00172 | .00182 | Oak | 0.65 | .00058 | .00061 |
| Silica, fused | 2.17 | .00237 | .00255 | Whitewood | 0.58 | .00041 | .00045 |

The following values are from unpublished data furnished by C. F. Skinner of the Westinghouse Co., Pittsburgh, Penn. They give the mean conductivity in gram-calories per sec. per cm. cube per °C when the mean temperature of the cube is that stated in the table. Resistance in thermal ohms (watts/inch²/inch/°C) = $\frac{1}{10.6}$ conductivity.

| Substance. | Grams. per cm ³ | Conductivity. | | | | | Safe temp. |
|-------------------------------------|----------------------------|---------------|---------|---------|---------|---------|------------|
| | | 100° C | 200° C | 300° C | 400° C | 500° C | |
| Air-cell asbestos | 0.232 | 0.00034 | 0.00043 | 0.00050 | — | — | 320 |
| Cork, ground | .168 | .00015 | .00019 | — | — | — | 180 |
| Diatomit | .326 | .00028 | .00032 | .00037 | 0.00042 | 0.00046 | 600 |
| Infusorial earth, natural | .506 | .00034 | .00032 | .00040 | — | — | — |
| " " h'd pressed blocks | .321 | .00030 | .00029 | .00033 | .00036 | — | 400 |
| Magnesium carbonate | .450 | .00023 | .00025 | .00025 | — | — | 300 |
| Vitribestos | .362 | .00049 | .00066 | .00079 | .00090 | .00102 | 600 |

TABLE 256.—Thermal Conductivity of Water and Salt Solutions

| Substance. | °C | k_t | Authority. | Solution in water. | Density. | °C | k_t | Authority. |
|------------|----|---------|-----------------------|-------------------------|----------|------|---------|--------------|
| Water | 0 | 0.00150 | Goldschmidt, '11. | CuSO_4 | 1.160 | 4.4 | 0.00118 | H. F. Weber. |
| | 11 | .00147 | | KCl | 1.026 | 13. | .00116 | |
| | 25 | .00136 | Lees, '98. | NaCl | 1.178 | 4.4 | .00115 | H. F. Weber. |
| | 20 | .00143 | | " | " | 26.3 | .00135 | |
| | | | Müller, Chattock, '98 | H_2SO_4 | 1.054 | 20.5 | .00126 | Chree. |
| | | | | " | 1.180 | 21. | .00130 | |
| | | | | ZnSO_4 | 1.134 | 4.5 | .00118 | H. F. Weber. |
| | | | | " | 1.136 | 4.5 | .00115 | |

TABLE 257.—Thermal Conductivity of Organic Liquids

| Substance. | °C | k_t | Refer. | Substance. | °C | k_t | Refer. | Substance. | °C | k_t | Refer. |
|---------------------|------|--------|--------|--------------------|------|--------|--------|------------------|----|--------|--------|
| Acetic acid..... | 9-15 | .03472 | 1 | Carbon disulphide. | 0 | .03387 | 3 | Oils: olive..... | — | .03395 | 4 |
| Alcohols: methyl... | 11 | .0352 | 2 | Chloroform..... | 9-15 | .03283 | 1 | “ castor..... | — | .03425 | 4 |
| “ ethyl..... | 11 | .0346 | 2 | Ether..... | 9-15 | .03303 | 1 | Toluene..... | 0 | .03349 | 3 |
| “ amyl..... | 0 | .03345 | 3 | Glycerine..... | 25 | .0368 | 2 | Vaseline..... | 25 | .0344 | 2 |
| Aniline..... | 0 | .03434 | 1 | Oils: petroleum... | 13 | .03355 | 5 | Xylene..... | 0 | .03343 | 3 |
| Benzene..... | 9-15 | .03333 | 1 | “ turpentine... | 13 | .03325 | 5 | | | | |

References: (1) H. F. Weber; (2) Lees; (3) Goldschmidt; (4) Wachsmuth; (5) Graetz.

TABLE 258.—Thermal Conductivity of Gases

The conductivity of gases, $k_t = \frac{1}{3}(c\gamma - 5)\mu C_v$, where γ is the ratio of the specific heats, C_p/C_v , and μ is the viscosity coefficient (Jeans, Dynamical Theory of Gases, 1916). Theoretically k_t should be independent of the density and has been found to be so by Kundt and Warburg and others within a wide range of pressure below one atm. It increases with the temperature.

| Gas. | t° C | k_t | Ref. | Gas. | t° C | k_t | Ref. | Gas. | t° C | k_t | Ref. |
|-----------------|-------------|-----------|------|-------------------------------|-------------|-----------|------|------------------|-------------|-----------|------|
| Air*... | -191 | 0.0000180 | 1 | CO ₂ | 100 | 0.0000496 | 1 | Hg | 203 | 0.0000185 | 3 |
| “ | 0 | 0.0000566 | 1 | C ₂ H ₄ | 0 | 0.0000395 | 2 | N ₂ | -191 | 0.0000183 | 1 |
| “ | 100 | 0.0000719 | 1 | He | -193 | 0.000146 | 1 | “ | 0 | 0.0000568 | 1 |
| Ar | -183 | 0.0000142 | 1 | “ | 0 | 0.000344 | 4 | “ | 100 | 0.0000718 | 1 |
| “ | 0 | 0.0000388 | 1 | “ | 100 | 0.000398 | 1 | O ₂ | -191 | 0.0000172 | 1 |
| “ | 100 | 0.0000509 | 1 | H ₂ | -192 | 0.000133 | 1 | “ | 0 | 0.0000570 | 1 |
| CO | 0 | 0.0000542 | 1 | “ | 0 | 0.000416 | 4 | “ | 100 | 0.0000743 | 1 |
| CO ₂ | -78 | 0.0000219 | 1 | “ | 100 | 0.000499 | 1 | NO | 8 | 0.000046 | 2 |
| “ | 0 | 0.0000332 | 1 | CH ₄ | 0 | 0.0000720 | 4 | N ₂ O | 0 | 0.0000353 | 4 |

References: (1) Eucken, Phys. Z. 12, 1911; (2) Winkelmann, 1875; (3) Schwarze, 1903; (4) Weber, 1917.

* Air: $k_0 = 5.22 (10^{-6})$ cal. cm⁻¹ sec.⁻¹ deg. C⁻¹; 5.74 at 22°; temp. coef. = .0029; Hercus-Laby, Pr. R. Soc. Ags, 190, 1919.

TABLE 259.—Diffusivities

The diffusivity of a substance = $h^2 = k/c\rho$, where k is the conductivity for heat, c the specific heat and ρ the density (Kelvin). The values are mostly for room temperatures, about 18° C.

| Material. | Diffusivity. | Material. | Diffusivity. |
|--|--------------|---|--------------|
| Aluminum..... | 0.826 | Coal..... | 0.002 |
| Antimony..... | 0.139 | Concrete (cinder)..... | 0.0032 |
| Bismuth..... | 0.0678 | Concrete (stone)..... | 0.0058 |
| Brass (yellow)..... | 0.339 | Concrete (light slag)..... | 0.006 |
| Cadmium..... | 0.467 | Cork (ground)..... | 0.0017 |
| Copper..... | 1.133 | Ebonite..... | 0.0070 |
| Gold..... | 1.182 | Glass (ordinary)..... | 0.0057 |
| Iron (wrought, also mild steel)..... | 0.173 | Granite..... | 0.0155 |
| Iron (cast, also 1% carbon steel)..... | 0.121 | Ice..... | 0.0112 |
| Lead..... | 0.237 | Limestone..... | 0.0092 |
| Magnesium..... | 0.883 | Marble (white)..... | 0.0090 |
| Mercury..... | 0.0327 | Paraffin..... | 0.00098 |
| Nickel..... | 0.152 | Rock material (earth aver.)..... | 0.0118 |
| Palladium..... | 0.240 | Rock material (crustal rocks)..... | 0.0064 |
| Platinum..... | 0.243 | Sandstone..... | 0.0133 |
| Silver..... | 1.737 | Snow (fresh)..... | 0.0033 |
| Tin..... | 0.427 | Soil (clay or sand, slightly damp)..... | 0.005 |
| Zinc..... | 0.402 | Soil (very dry)..... | 0.0031 |
| Air..... | 0.179 | Water..... | 0.0014 |
| Asbestos (loose)..... | 0.0035 | Wood (pine, cross grain)..... | 0.00668 |
| Brick (average fire)..... | 0.0074 | Wood (pine with grain)..... | 0.0023 |
| Brick (average building)..... | 0.0050 | | |

Taken from An Introduction to the Mathematical Theory of Heat Conduction, Ingersoll and Zobel, 1913.

THERMAL CONDUCTIVITY—LIQUIDS, PRESSURE EFFECT

(P. W. Bridgman, Proc. Amer. Acad., 59, 158, 1923.)

| No. | Liquid | °C | Conductivity at 0 kg/cm ² | Conductivity relative to unity at 0 kg/cm ² as function of pressure in kg/cm ² | | | | | | | |
|-----|---------------------------|----|--------------------------------------|--|-------|-------|-------|-------|----------|---------|---------|
| | | | | 1000 | 2000 | 4000 | 6000 | 8000 | 10000 | 11000 | 12000 |
| 1 | Methyl alcohol..... | 30 | .000505 | 1.201 | 1.342 | 1.557 | 1.724 | 1.864 | 1.986 | 2.043 | 2.097 |
| | | 75 | .000493 | 1.212 | 1.365 | 1.601 | 1.785 | 1.939 | 2.072 | 2.133 | 2.191 |
| 2 | Ethyl alcohol..... | 30 | .000430 | 1.221 | 1.363 | 1.574 | 1.744 | 1.888 | 2.014 | 2.070 | 2.122 |
| | | 75 | .000416 | 1.233 | 1.400 | 1.650 | 1.845 | 2.007 | 2.152 | 2.217 | 2.278 |
| 3 | Isopropyl alcohol..... | 30 | .000367 | 1.205 | 1.352 | 1.570 | 1.743 | 1.894 | 2.028 | 2.091 | 2.150 |
| | | 75 | .000363 | 1.230 | 1.399 | 1.638 | 1.812 | 1.962 | 2.093 | 2.154 | 2.211 |
| 4 | Normal butyl alcohol..... | 30 | .000400 | 1.181 | 1.307 | 1.495 | 1.648 | 1.780 | 1.900 | 1.955 | 2.008 |
| | | 75 | .000391 | 1.218 | 1.358 | 1.559 | 1.720 | 1.859 | 1.985 | 2.043 | 2.099 |
| 5 | Isoamyl alcohol..... | 30 | .000354 | 1.184 | 1.320 | 1.524 | 1.686 | 1.828 | 1.955 | 2.013 | 2.069 |
| | | 75 | .000348 | 1.207 | 1.348 | 1.557 | 1.724 | 1.868 | 1.998 | 2.063 | 2.126 |
| 6 | Ether..... | 30 | .000329 | 1.305 | 1.509 | 1.800 | 2.009 | 2.177 | 2.322 | 2.388 | 2.451 |
| | | 75 | .000322 | 1.313 | 1.518 | 1.814 | 2.043 | 2.231 | 2.394 | 2.469 | 2.537 |
| 7 | Acetone..... | 30 | .000429 | 1.184 | 1.315 | 1.511 | 1.659 | 1.786 | 1.900 | Freezes | |
| | | 75 | .000403 | 1.181 | 1.325 | 1.554 | 1.738 | 1.891 | 2.024 | 2.083 | 2.137 |
| 8 | Carbon bisulphide.. | 30 | .000382 | 1.174 | 1.310 | 1.512 | 1.663 | 1.783 | 1.880 | 1.923 | 1.962 |
| | | 75 | .000362 | 1.208 | 1.366 | 1.607 | 1.789 | 1.935 | 2.054 | 2.107 | 2.154 |
| 9 | Ethyl bromide..... | 30 | .000286 | 1.193 | 1.327 | 1.517 | 1.657 | 1.768 | 1.858 | 1.895 | 1.928 |
| | | 75 | .000273 | 1.230 | 1.390 | 1.609 | 1.772 | 1.907 | 2.022 | 2.073 | 2.121 |
| 10 | Ethyl iodide..... | 30 | .000265 | 1.125 | 1.232 | 1.394 | 1.509 | 1.592 | 1.662 | 1.694 | 1.724 |
| | | 75 | .000261 | 1.148 | 1.265 | 1.442 | 1.570 | 1.671 | 1.757 | 1.799 | 1.837 |
| 11 | Water..... | 30 | .00144 | 1.058 | 1.113 | 1.210 | 1.293 | 1.366 | 1.428 | 1.456 | Freezes |
| | | 75 | .00154 | 1.065 | 1.123 | 1.225 | 1.308 | 1.379 | 1.445 | 1.476 | 1.506 |
| 12 | Toluol..... | 30 | .000364 | 1.159 | 1.286 | 1.470 | 1.604 | 1.716 | (2.394*) | | |
| | | 75 | .000339 | 1.210 | 1.355 | 1.573 | 1.738 | 1.872 | 1.987 | 2.039 | 2.089 |
| 13 | Normal pentane..... | 30 | .000322 | 1.281 | 1.483 | 1.777 | 1.987 | 2.163 | 2.325 | 2.404 | 2.481 |
| | | 75 | .000307 | 1.319 | 1.534 | 1.855 | 2.112 | 2.335 | 2.543 | 2.642 | 2.740 |
| 14 | Petroleum ether..... | 30 | .000312 | 1.266 | 1.460 | 1.752 | 1.970 | 2.143 | 2.279 | 2.333 | 2.379 |
| | | 75 | .000302 | 1.268 | 1.466 | 1.780 | 2.026 | 2.232 | 2.409 | 2.488 | 2.561 |
| 15 | Kerosene..... | 75 | .000333 | 1.185 | 1.314 | 1.502 | 1.654 | 1.792 | 1.925 | 1.990 | 2.054 |

1, 2, 6, 8, 12, 13, extreme purity; 3, 4, 5, 7, 9, 10, 11, very pure; 14, 15, commercial.

* Toluol freezes at 9900 kg/cm² at 30°. The figure at 11000 is for the solid.

TABLE 261.—The Unit of Thermal Resistance—the Fourier

The *fourier* is defined as that thermal resistance which will transfer heat energy at the rate of one joule per sec. (one watt) for each degree (centigrade) temperature difference between the terminal surfaces (equivalent roughly to a prism of Ag or Cu 4 cm long by 1 cm² cross section). (Harper, Journ. Wash. Acad. Sci., 18, 469, 1928.)

TABLE 262.—Factors to Reduce Heat Flow in Fouriers for a cm³ to Other Units

| To | watts/cm ² | cal./sec./cm ² | kilocal./hr./m ² | hp./ft. ² | hp./ft. ² | hp./ft. ² | watts/in. ² |
|-----------|-----------------------|---------------------------|-----------------------------|----------------------|----------------------|----------------------|------------------------|
| Gradient | °C/cm | °C/cm | °C/m | °C/in. | °F./ft. | °F./in. | °C/in. |
| Multiples | 1 | 4.18 | .0116 | 4.14 | 44 | 3.67 | .394 |

TABLE 263.—Conversion Factors Between Units of Current Density of Heat Flow. Quantity of Heat Energy Transferred Through Unit Area per Unit Time

| | Joules/ sec. cm ² watts/cm ² | Cal./sec. cm ² | Kilocal./hr./m ² | Hp./ft. ² | Watt/in. ² |
|---------------------------------|--|---------------------------|-----------------------------|----------------------|-----------------------|
| 1 watt/cm ² = | 1 | .2391 | 8606 | 1.246 | 6.452 |
| 1 cal./sec./cm ² = | 4.183 | 1 | 36000 | 5.211 | 26.99 |
| 1 kilocal./hr./m ² = | .0001162 | .0000278 | 1 | .0001448 | .0007497 |
| 1 hp./ft. ² = | .8027 | .1919 | 6908 | 1 | 5.178 |
| 1 watt/in. ² = | .1550 | .03705 | 1334 | .1931 | 1 |

The calorie is taken as 4.183 absolute joules.

TABLE 264.—Thermal Resistivities at 20°C Expressed in Fouriers for a Centimeter Cube

| | | | | | |
|----------------------|-------|--------------------|-----|--------------------|------|
| Silver | 0.239 | Water | 170 | Rubber* (over | |
| Copper | .258 | Mica* (1 to | | 90%) | 700 |
| Aluminum | .49 | laminations) . . | 200 | Wood (Virginia | |
| Brass (30% Zn) . . | .93 | Firebrick* | 200 | pine across | |
| Iron | 1.6 | [Firebrick 25°C | | grain) | 710 |
| Nickel | 1.7 | to 1000°C] . . . | 90 | Paper* | 1000 |
| Steel (1% C) . . . | 2.1 | Brick masonry* . | 250 | Asbestos* (wool) . | 1100 |
| Constantan | 4.4 | Leather* | 600 | Cork* | 2000 |
| Mercury | 12.0 | Hydrogen | 600 | Cotton batting | |
| [Ice at 0°C] | 45 | Hard rubber . . . | 610 | (loose) | 2500 |
| Glass* | 133 | Helium | 690 | Wool (loose) . . . | 2500 |
| Concrete* | 140 | | | Air | 4100 |
| | | | | Carbon dioxide . . | 6700 |

* Substances marked with the asterisk vary widely in thermal conductivity according to composition. For limits of such variation, consult International Critical Tables, Vol. 2. The figure listed above for any such material represents the author's estimate of the "best guess" for use in those cases where the composition of the material is not specified.

In preparing this table, the author has consulted Vol. 2, I.C.T. and has courteously been furnished advance values for some other materials by the editors of I.C.T. For still other materials, grateful acknowledgment is made to the staff of the Bureau of Standards, for advice in selecting most probable values in the light of present information.

TABLE 265.—Anti-Freezing Solutions (for automobile radiators, etc.)

(From Bur. Standards Letter Circulars No. 29, 1925.)

Per cent by vol. in water with freezing points and specific gravities.

| Per cent by vol. | 10% | 20% | 30% | 40% | 50% |
|--------------------------------|-------|-------|-------|-------|-------|
| Denatured alcohol | -3°C | -7°C | -12°C | -19°C | -28°C |
| (90% by vol.)* | .988 | .978 | .968 | .957 | .943 |
| Wood alcohol† | -5°C | -12°C | -19°C | -29°C | -40°C |
| (97% by vol.) | .987 | .975 | .963 | .952 | .937 |
| Distilled glycerine§ | -2°C | -6°C | -11°C | -18°C | -26°C |
| (95% by vol.) | 1.029 | 1.057 | 1.085 | 1.112 | 1.140 |
| Ethylene glycol§ | -3°C | -9°C | -16°C | -24°C | -35°C |
| (95% by vol.) | 1.016 | 1.031 | 1.045 | 1.058 | 1.070 |

* 90% by vol. indicates quality of alcohol (180° proof); if 188 proof (that is containing only 6% water) amount required will be about 4% less.

† The vapor from wood alcohol is harmful. §Glycerine and ethylene glycol are practically nonvolatile and noncorrosive.

LINEAR EXPANSION OF THE ELEMENTS

C is the true expansion coefficient at given temperature; R indicates reference to notes and authority, see page 282; M is the mean coefficient between given temperatures; where one temperature is given the true coefficient at that temperature is indicated; α and β are coefficients in formula $l_t = l_0 (1 + \alpha t + \beta t^2)$; l_0 is length at 0° centigrade (unless otherwise indicated, when if x is standard temp., $l_t = l_x (1 + \alpha(t - t_x) + \beta(t - t_x)^2)$; l_t is length at $t^\circ\text{C}$.

| Element | Temp. | $C \times 10^4$ | R | Temp. range | $M \times 10^4$ | R | Temp. range | $\alpha \times 10^4$ | $\beta \times 10^6$ | R |
|------------------|-------|-----------------|-----|-------------|-----------------|-----|-------------|----------------------|---------------------|-----|
| Aluminum | 20° | .224 | 1 | 100° | .235 | 1 | 0°, 500° | .22 | .009 | 2 |
| " | 300 | .284 | 1 | 500 | .311 | 1 | | | | |
| Antimony | 20 | .136 | 3a | 20 | .080 | 3b | | | | |
| Arsenic | 20 | .03 | 2 | | | | | | | |
| Bismuth | 20 | .014 | 3a | 20 | .103 | 3b | | | | |
| Cadmium | 0 | .54 | 4a | -180, -140 | .59 | 4a | 20, 140 | .526 | | 4a* |
| " | 0 | .20 | 4b | -180, -140 | .117 | 4b | 20, 140 | .214 | | 4b* |
| Carbon, diamond | 50 | .012 | 5 | | | | | | | |
| Carbon, graphite | 50 | .06 | 2 | | | | | | | |
| Chromium | | | | 20, 100 | .068 | 30 | 20, 500 | .086 | | 30 |
| Cobalt | 20 | .123 | 7 | | | | 6, 121 | .121 | .0064 | 7 |
| Copper | 20 | .162 | 8 | 100 | .166 | 9 | 0, 625 | .161 | .0049 | 8 |
| " | 200 | .170 | 9 | 300 | .175 | 9 | | | | |
| Gold | 20 | .140 | 2 | 17, 100 | .143 | 10 | 0, 520 | .142 | .0022 | 11 |
| " | | | | -191, 17 | .132 | 10 | | | | |
| Indium | 40 | .417 | 5 | | | | | | | |
| Iodine | | | | -190, 17 | .837 | 12 | | | | |
| Iridium | 20 | .065 | 13 | | | | 0, 80 | .0636 | .0032 | 13 |
| " | | | | | | | 1070, 1720 | .0679 | .0011 | 14 |
| Iron, soft | 40 | .1210 | 5 | 0, 100 | .11 | 15 | | | | |
| " cast | 20 | .118 | | | | | 0, 750 | .1158 | .0053 | 8 |
| " wrought | 20 | .119 | | | | | 0, 750 | .1170 | .0053 | 16 |
| " steel | 20 | .114 | | | | | 0, 750 | .1118 | .0053 | 8 |
| Lead (99.9) | 20 | .312 | 17 | 20, 100 | .286 | 17 | 100, 240 | .269 | .011 | 9 |
| " | 100 | .291 | 17 | 20, 200 | .295 | 17 | | | | |
| " | 280 | .343 | 9 | | | | | | | |
| Magnesium | 20 | .254 | 19 | -100, + 20 | .240 | 18 | + 20, 500 | .2480 | .0096 | 18 |
| " | | | | 20, 100 | .260 | 18 | | | | |
| Manganese | 20 | .233 | 2 | 0, 100 | .228 | 6 | | | | |
| " | | | | -190, 0 | .159 | 6 | 20, 300 | .216 | .0121 | 6 |
| Molybdenum† | 20 | .053 | 2 | 0, 100 | .052 | 6 | -142, 19 | .0515 | .0057 | 20 |
| " | | | | 25, 100 | .049 | 20 | 19, +305 | .0501 | .0014 | 20 |
| " | | | | 25, 500 | .055 | 20 | | | | |
| Nickel | 20 | .126 | 2 | 0, 100 | .130 | 6 | -190, + 20 | .1308 | .0166 | 6 |
| " | | | | | | | + 20, +300 | .1236 | .0066 | 6 |
| " | | | | | | | 500, 1000 | .1346 | .0033 | 16 |
| Osmium | 40 | .066 | 5 | | | | -190, +100 | .1152 | .00517 | 21 |
| Palladium | 20 | .1173 | 2 | | | | 0, 1000 | .1167 | .0022 | 16 |
| " | | | | | | | -190, -100 | .0875 | .00314 | 19 |
| Platinum | 20 | .0887 | 19 | -190, -100 | | | 0, + 80 | .0890 | .00121 | 13 |
| " | 20 | .0893 | 2 | | | | 0, 1000 | .0887 | .00132 | 16 |
| Potassium | | | | 0, 50 | .83 | 22 | | | | |
| Rhodium | 40 | .0850 | 5 | 6, 21 | .0876 | 23 | - 75, -112 | .0746 | | 23* |
| Ruthenium | 40 | .0963 | 5 | | | | | | | |
| Selenium | 0 | .439 | 24 | 0, 100 | .660 | 25 | - 75, - 67 | .0182 | | 23* |
| Silicon | 40 | .0763 | 5 | - 3, + 18 | .0249 | 23 | 0, 875 | .1827 | .00479 | 10 |
| Silver | 20 | .1846 | 16 | 0, 100 | .197 | 19 | 0, 50 | .1939 | .00295 | 19 |
| " | 20 | .195 | 19 | | | | 20, 500 | .72 | | 22* |
| Sodium | | | | -190, - 17 | .622 | 12 | 0, 50 | .72 | | 22* |
| Steel, 36.4 Ni | | | | 20, 260 | .031 | 17 | 260, 500 | .144 | | 17* |
| " | | | | 20, 340 | .035 | 17 | 340, 500 | .136 | | 17* |
| Tantalum† | 20 | .065 | 6 | - 78, 0 | .059 | 6 | 20, 400 | .0646 | .0009 | 6 |
| " | | | | 0, 100 | .0655 | 6 | | | | |
| Tellurium | 20 | .016 | 3a | 20 | .272 | 3b | | | | |
| Thallium | 40 | .302 | 5 | | | | | | | |
| Tin | 20 | .214 | 26 | | | | 8, 95 | .2033 | .0263 | 26 |
| " | 20 | .305 | 3a | 0, 20 | .154 | 3b | | | | |
| Tungsten† | 27 | .0444 | 27 | 0, 100 | .045 | 6 | -105, +502 | .0428 | .00058 | 28 |
| " | | | | 0, 100 | .045 | 6 | | | | |
| Zinc | 20 | .305 | 3b | -140, -100 | .656 | 4a | 0, 400 | .354 | .010 | 29a |
| " | 20 | .154 | 3b | + 20, 100 | .630 | 4a | | | | |
| " | 20 | .358 | 29 | + 20, 100 | .141 | 4b | | | | |

* For references, see page 282.

† Molybdenum, t_{300}° to 2500° $l_t = l_{300} [1 + 5.00 \times 10^{-6} (t - 300) + 10.5 \times 10^{-10} (t - 300)^2]$ Worthing, 1926

Tantalum, 300° to 2800° $l_t = l_{300} [1 + 6.60 \times 10^{-6} (t - 300) + 5.2 \times 10^{-10} (t - 300)^2]$ Worthing, 1926

Tungsten, 300° to 2700° $\log l_t = \log l_{300} [1 + 4.44 \times 10^{-6} (t - 300) + 4.5 \times 10^{-10} (t - 300)^2]$ Worthing, 1926

LINEAR EXPANSION OF MISCELLANEOUS SUBSTANCES

The coefficient of cubical expansion may be taken as three times the linear coefficient. t is the temperature or range of temperature, C the coefficient of expansion, and $A.$ the authority. For reference see page 282.

| Substance. | t | $C \times 10^4$ | A. | Substance. | t | $C \times 10^4$ | A. |
|---|--------------|-----------------|----|-----------------------------------|--------------|----------------------------|----|
| Brass: | | | | Platinum-silver: | | | |
| Cast..... | 0-100 | 0.1875 | 1 | 1 Pt + 2Ag..... | 0-100 | 0.1523 | 4 |
| Wire..... | " | 0.1930 | 1 | Porcelain..... | 20-790 | 0.0413 | 19 |
| "..... | " | .1785-.193 | 2 | " Bayeux..... | 1000-1400 | 0.0553 | 20 |
| 71.5 Cu + 27.7 Zn + | | | | Quartz: | | | |
| 0.3 Sn + 0.5 Pb..... | 40 | 0.1859 | 3 | Parallel to axis.... | 0-80 | 0.0707 | 6 |
| 71 Cu + 29 Zn..... | 0-100 | 0.1906 | 4 | " " "..... | -190 to + 16 | 0.0521 | 21 |
| Bronze: | | | | Perpend. to axis.... | 0-80 | 0.1337 | 6 |
| 3 Cu + 1 Sn..... | 16.6-100 | 0.1844 | 5 | Quartz glass..... | -190 to + 16 | 0.0026 | 13 |
| " " " "..... | 16.6-350 | 0.2116 | 5 | " " "..... | 16 to 500 | 0.0057 | 26 |
| " " " "..... | 16.6-957 | 0.1737 | 5 | Rock salt..... | 16-1000 | 0.0058 | 26 |
| 86.3 Cu + 9.7 Sn + | | | | Rubber, hard..... | 40 | 0.4040 | 3 |
| 4 Zn..... | 40 | 0.1782 | 3 | " " "..... | 0° | 0.691 | 27 |
| 97.6 Cu + { hard | 0-80 | 0.1713 | 6 | Speculum metal..... | -160 | 0.300 | 27 |
| 2.2 Sn + { soft | 0-80 | 0.1708 | 6 | Topaz: | 0-100 | 0.1933 | 1 |
| 0.2 P..... | — | 0.657-0.686 | 2 | Parallel to lesser | | | |
| Caoutchouc..... | 16.7-25.3 | 0.770 | 7 | horizontal axis.... | " | 0.0832 | 8 |
| Constantan..... | 4-20 | 0.1523 | 7 | Parallel to greater | " | 0.0836 | 8 |
| Ebonite..... | 25.3-35.4 | 0.842 | 7 | horizontal axis.... | " | 0.0472 | 8 |
| Fluor spar: CaF ₂ | 0-100 | 0.1950 | 8 | Parallel to vertical | " | 0.0937 | 8 |
| German silver..... | " | 0.1836 | 8 | axis..... | " | 0.0773 | 8 |
| Gold-platinum: | | | | Tourmaline: | | | |
| 2 Au + 1 Pt..... | " | 0.1523 | 4 | Parallel to longitudinal axis.... | " | 0.0937 | 8 |
| Gold-copper: | | | | Parallel to horizontal axis.... | " | 0.0773 | 8 |
| 2 Au + 1 Cu..... | " | 0.1552 | 4 | Type metal..... | 16.6-254 | 0.1952 | 5 |
| Glass: | | | | Vulcanite..... | 0-18 | 0.6100 | 22 |
| Tube..... | " | 0.0833 | 1 | Wedgwood ware.... | 0-100 | 0.0890 | 5 |
| "..... | " | 0.0828 | 9 | Wood: | | | |
| Plate..... | " | 0.0801 | 10 | Parallel to fiber: | | | |
| Crown (mean)..... | " | 0.0897 | 10 | Ash..... | " | 0.0951 | 23 |
| "..... | 50-60 | 0.0954 | 11 | Beech..... | 2-34 | 0.0237 | 24 |
| Flint..... | " | 0.0783 | 11 | Chestnut..... | " | 0.0649 | 24 |
| Jena ther-16 ^{III} } | 0-100 | 0.081 | 12 | Elm..... | " | 0.0365 | 24 |
| meter (normal) } | " | | | Mahogany..... | " | 0.0361 | 24 |
| " 50 ^{III} | " | 0.058 | 12 | Maple..... | " | 0.0638 | 24 |
| "..... | -191 to + 16 | 0.424 | 13 | Oak..... | " | 0.1023 | 24 |
| Gutta percha..... | 20 | 1.983 | 14 | Pine..... | " | 0.0511 | 24 |
| Ice..... | -20 to -1 | 0.51 | 15 | Walnut..... | " | 0.0658 | 24 |
| Iceland spar: | | | | Across the fiber: | | | |
| Parallel to axis.... | 0-80 | 0.2631 | 6 | Beech..... | " | 0.614 | 24 |
| Perpendicular to axis | " | 0.0544 | 6 | Chestnut..... | " | 0.325 | 24 |
| Lead-tin (solder) | | | | Elm..... | " | 0.443 | 24 |
| 2 Pb + 1 Sn..... | 0-100 | 0.2508 | 1 | Mahogany..... | " | 0.404 | 24 |
| Magnesium..... | 12-39 | 0.238 | 16 | Maple..... | " | 0.484 | 24 |
| Manganin..... | — | 0.181 | — | Oak..... | " | 0.544 | 24 |
| Marble..... | 15-100 | 0.117 | 17 | Pine..... | " | 0.341 | 24 |
| Paraffin..... | 0-16 | 1.0662 | 18 | Walnut..... | " | 0.484 | 24 |
| "..... | 16-38 | 1.3030 | 18 | Wax: White..... | 10-26 | 2.300 | 25 |
| "..... | 38-49 | 4.7797 | 18 | " "..... | 26-31 | 3.120 | 25 |
| Platinum-iridium | | | | " "..... | 31-43 | 4.860 | 25 |
| to Pt + 1 Ir..... | 40 | 0.0884 | 3 | " "..... | 43-57 | 15.227 | 25 |
| Duralumin, .94 Al,..... | 20-100°, | .000023 | | 20-300°, | .000025 | Hidnert, '22 | |
| Steel, .14 C, 34.5 Ni..... | 25-100°, | .0000037 | | 25-600°, | .0000136 | " | |
| Monel metal, | 25-100°, | .000014 | | 25-600°, | .000016 | | |
| Insulating materials, Souder-Hidnert, 1910: | | | | Marble, | 25-100°, | 10 - 16 × 10 ⁻⁶ | |
| Bakelite, bleached, | 20-60°, | .000022 | | Porcelain, | 20-200°, | 3 - 11 × 10 ⁻⁶ | |
| Celluloid, | 20-70°, | .000100 | | Hard rubber, .. | 20-60°, | .00008 | |
| Limestone, | 25-100°, | .000009 | | | | | |

CUBICAL EXPANSION OF SOLIDS

If v_2 and v_1 are the volumes at t_2 and t_1 respectively, then $v_2 = v_1 (1 + C\Delta t)$, C being the coefficient of cubical expansion and Δt the temperature interval. Where only a single temperature is stated C represents the true coefficient of cubical expansion at that temperature. The coefficient of cubical expansion may be taken as three times the linear coefficient.

| Substance. | t or Δt | $C \times 10^4$ | Authority. |
|--------------------------|-------------------|-----------------|---------------------|
| Antimony | 0-100 | 0.3167 | Matthiessen |
| Beryl | 0-100 | 0.0105 | Pfaff |
| Bismuth | 0-100 | 0.3948 | Matthiessen |
| Copper | 0-100 | 0.4998 | " |
| Diamond | 40 | 0.0354 | Fizeau |
| Emerald | 40 | 0.0108 | " |
| Galena | 0-100 | 0.558 | Pfaff |
| Glass, common tube . . | 0-100 | 0.276 | Regnault |
| " hard | 0-100 | 0.214 | " |
| " Jena, borosilicate . . | | | |
| 59 III | 20-100 | 0.156 | Scheel |
| " pure silica | 0-80 | 0.0129 | Chappuis |
| Gold | 0-100 | 0.4411 | Matthiessen |
| Ice | -20- -1 | 1.1250 | Brunner |
| Iron | 0-100 | 0.3550 | Dulong and Petit |
| Lead | 0-100 | 0.8399 | Matthiessen |
| Paraffin | 20 | 5.88 | Russner |
| Platinum | 0-100 | 0.265 | Dulong and Petit |
| Porcelain, Berlin . . . | 20 | 0.0814 | Chappuis and Harker |
| Potassium chloride . . | 0-100 | 1.094 | Playfair and Joule |
| " nitrate | 0-100 | 1.967 | " " " |
| " sulphate | 20 | 1.0754 | Tutton |
| Quartz | 0-100 | 0.3840 | Pfaff |
| Rock salt | 50-60 | 1.2120 | Pulfrich |
| Rubber | 20 | 4.87 | Russner |
| Silver | 0-100 | 0.5831 | Matthiessen |
| Sodium | 20 | 2.1364 | E. Hazen |
| Stearic acid | 33.8-45.5 | 8.1 | Kopp |
| Sulphur, native | 13.2-50.3 | 2.23 | " |
| Tin | 0-100 | 0.6889 | Matthiessen |
| Zinc | 0-100 | 0.8928 | " |

References to Table 266, page 280: (1) Uffelmann, 1930. (2) Mean. (3a) Bridgman, 1924-5, parallel to axis. (3b) ditto, perpendicular to axis. (4a) Grüneisen, paral. axis, hexag. (4b) ditto, perpendicular. (5) Fizeau. (6) Disch, 1921. (7) Tutton, 1899. (8) Dittenberger, 1902. (9) Uffelmann, 1930. (10) Grüneisen, 1910. (11) Müller, 1916. (12) Dewar, 1902. (13) Benoit, 1889. (14) Holborn, 1897. (15) Le Chatelier, 1899. (16) Holborn, Day, 1900. (17) Hidnert, Sweeney, 1930. (18) ditto, 1928. (19) Scheel, 1921. (20) Hidnert, Shad, 1919. (21) Scheel, 1907. (22) Hagen, 1883. (23) Valentiner, Wallot, 1915. (24) Dorsey, 1908. (25) Spring, 1881. (26) Matthiessen. (27) Worthing, 1917. (28) Hidnert, Sweeney, 1925. (29) Schulze, 1921. (30) Hidnert, 1931.

References to Table 267, page 281: (1) Smeaton. (2) Various. (3) Fizeau. (4) Matthiessen. (5) Daniell. (6) Benoit. (7) Kohlrausch. (8) Pfaff. (9) Deluc. (10) Lavoisier and Laplace. (11) Pulfrich. (12) Schott. (13) Henning. (14) Russner. (15) Mean. (16) Stadthagen. (17) Fröhlich. (18) Rodwell. (19) Braun. (20) Deville and Troost. (21) Scheel. (22) Mayer. (23) Glatzel. (24) Villari. (25) Kopp. (26) Randall. (27) Dorsey.

Note: Crucibles of thorium oxide may be used for $t < 3000^\circ \text{C}$; magnesium oxide, $< 1800^\circ \text{C}$; beryllium oxide, $< 2000^\circ \text{C}$. Swanger, Caldwell, Bur. Standards, Journ. Res., 6, 1131, 1931, which see for further information about use of crucibles.

CUBICAL EXPANSION OF LIQUIDS

If V_0 is the volume at 0° then at t° the expansion formula is $V_t = V_0 (1 + \alpha t + \beta t^2 + \gamma t^3)$. The table gives values of α , β and γ and of C , the true coefficient of cubical expansion, at 20° for some liquids and solutions. Δt is the temperature range of the observation and A, the authority.

| Liquid. | Δt | $\alpha \ 10^3$ | $\beta \ 10^6$ | $\gamma \ 10^8$ | $C \ 10^3$ at 20° | A. |
|----------------------|------------|-----------------|----------------|-----------------|-----------------------------|----|
| Acetic acid | 16-107 | 1.0630 | 0.12636 | 1.0876 | 1.071 | 3 |
| Acetone | 0-54 | 1.3240 | 3.8090 | -0.87983 | 1.487 | 3 |
| Alcohol: | | | | | | |
| Amyl | -15-80 | 0.9001 | 0.6573 | 1.18458 | 0.902 | 4a |
| Ethyl, 30% by vol. | 18-39 | 0.2928 | 10.790 | -11.87 | - | 6 |
| " 50% " | 0-39 | 0.7450 | 1.85 | 0.730 | - | 6 |
| " 99.3% " | 27-46 | 1.012 | 2.20 | - | 1.12 | 6 |
| " 500 atmo. press. | 0-40 | 0.866 | - | - | - | 1 |
| " 3000 " " | 0-40 | 0.524 | - | - | - | 1 |
| Methyl | 0-61 | 1.1342 | 1.3635 | 0.8741 | 1.199 | 5a |
| Benzene | 11-81 | 1.17626 | 1.27776 | 0.80648 | 1.237 | 5a |
| Bromine | 0-59 | 1.06218 | 1.87714 | -0.30854 | 1.132 | 2 |
| Calcium chloride: | | | | | | |
| 5.8% solution | 18-25 | 0.07878 | 4.2742 | - | 0.250 | 7 |
| 40.9% " | 17-24 | 0.42383 | 0.8571 | - | 0.458 | 7 |
| Carbon disulphide | -34-60 | 1.13980 | 1.37065 | 1.91225 | 1.218 | 4a |
| 500 atmos. pressure | 0-50 | 0.940 | - | - | - | 1 |
| 3000 " " | 0-50 | 0.581 | - | - | - | 1 |
| Carbon tetrachloride | 0-76 | 1.18384 | 0.89881 | 1.35135 | 1.236 | 4b |
| Chloroform | 0-63 | 1.10715 | 4.66473 | -1.74328 | 1.273 | 4b |
| Ether | -15-38 | 1.51324 | 2.35918 | 4.00512 | 1.656 | 4a |
| Glycerine | - | 0.4853 | 0.4895 | - | 0.505 | 8 |
| Hydrochloric acid: | | | | | | |
| 33.2% solution | 0-33 | 0.4460 | 0.215 | - | 0.455 | 9 |
| Mercury | 0-100 | 0.18182 | 0.0078 | - | 0.18186 | 13 |
| Olive oil | - | 0.6821 | 1.1405 | -0.539 | 0.721 | 10 |
| Pentane | 0-33 | 1.4646 | 3.09319 | 1.6084 | 1.608 | 14 |
| Potassium chloride: | | | | | | |
| 24.3% solution | 16-25 | 0.2695 | 2.080 | - | 0.353 | 7 |
| Phenol | 36-157 | 0.8340 | 0.10732 | 0.4446 | 1.090 | 11 |
| Petroleum: | | | | | | |
| Density 0.8467 | 24-120 | 0.8994 | 1.396 | - | 0.955 | 12 |
| Sodium chloride: | | | | | | |
| 20.6% solution | 0-29 | 0.3640 | 1.237 | - | 0.414 | 9 |
| Sodium sulphate: | | | | | | |
| 24% solution | 11-40 | 0.3599 | 1.258 | - | 0.410 | 9 |
| Sulphuric acid: | | | | | | |
| 10.9% solution | 0-30 | 0.2835 | 2.580 | - | 0.387 | 9 |
| 100.0% " | 0-30 | 0.5758 | -0.432 | - | 0.558 | 9 |
| Turpentine | -9-106 | 0.9003 | 1.9595 | -0.44998 | 0.973 | 5b |
| Water | 0-33 | -0.06427 | 8.5053 | -6.7900 | 0.207 | 13 |

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THERMAL EXPANSION OF GASES

Pressures are given in centimeters of mercury.

| Coefficient at Constant Volume. | | | | Coefficient at Constant Pressure. | | | |
|---|-----------------|--------------------------|------------|---|-----------------|--------------------------|------------|
| Substance. | Pressure cm. | Coefficient × 100. | Reference. | Substance. | Pressure cm. | Coefficient × 100. | Reference. |
| Air | .6 | .37666 | 1 | Air | 76. | .3671 | 3 |
| " | 1.3 | .37172 | " | " | 257. | .3693 | " |
| " | 10.0 | .36630 | " | " 0°-100° | 100.1 | .36728 | 2 |
| " | 25.4 | .36580 | " | Hydrogen 0°-100° | 100.0 | .36000 | " |
| " | 75.2 | .36060 | " | " | 200 Atm. | .332 | 9 |
| " 0°-100° | 100.1 | .36744 | 2 | " | 400 " | .295 | " |
| " | 76.0 | .36650 | 3 | " | 600 " | .261 | " |
| " | 200.0 | .36093 | " | " | 800 " | .242 | " |
| " | 2000. | .38866 | " | Carbon dioxide | 76. | .3710 | 3 |
| " | 10000. | .4100 | " | " " 0°-20° | 51.8 | .37128 | 2 |
| Argon | 51.7 | .3668 | 4 | " " 0°-40° | 51.8 | .37100 | " |
| Carbon dioxide | 76.0 | .36856 | 3 | " " 0°-100° | 51.8 | .37073 | " |
| " | 1.8 | .36753 | 1 | " " 0°-20° | 99.8 | .37602 | " |
| " | 5.6 | .36641 | " | " " 0°-100° | 99.8 | .37410 | " |
| " | 74.9 | .37264 | " | " " 0°-20° | 137.7 | .37972 | " |
| " " 0°-20° | 51.8 | .36985 | 2 | " " 0°-100° | 137.7 | .37703 | " |
| " " 0°-40° | 51.8 | .36972 | " | " " 0°-7.5° | 2621. | .1097 | 6 |
| " " 0°-100° | 51.8 | .36981 | " | " " 64°-100° | 2621. | .6574 | " |
| " " 0°-20° | 99.8 | .37335 | " | Carbon monoxide | 76. | .3669 | 3 |
| " " 0°-100° | 99.8 | .37262 | " | Nitrous oxide | 76. | .3719 | " |
| " " 0°-100° | 100.0 | .37248 | 5 | Sulphur dioxide | 76. | .3903 | " |
| Carbon monoxide | 76. | .36667 | 3 | " | 98. | .3980 | " |
| Helium | 50.7 | .3665 | 4 | " | 76. | .4187 | 10 |
| Hydrogen 10°-132° | .0077 | .3328 | 6 | Water- vapor { 0°-119° | 76. | .4189 | " |
| " " 15°-132° | .025 | .3623 | " | { 0°-162° | 76. | .4071 | " |
| " " 12°-185° | .47 | .3656 | " | { 0°-200° | 76. | .3938 | " |
| " | .93 | .37002 | 1 | { 0°-247° | 76. | .3799 | " |
| " | 11.2 | .36548 | " | Thomson has given, Encyc. Brit. "Heat," the following for the calculation of the ex- pansion, E, between 0° and 100° C. Expansion is to be taken as the change of volume under constant pressure: Hydrogen, $E = .3662(1 - .00049 I/v)$, Air, $E = .3662(1 - .0026 I/v)$, Oxygen, $E = .3662(1 - .0032 I/v)$, Nitrogen, $E = .3662(1 - .0031 I/v)$, CO ₂ $E = .3662(1 - .0164 V/v)$. I/v is the ratio of the actual density of the gas at 0° C. to what it would have at 0° C. and 1 Atm. pressure. | | | |
| " | 76.4 | .36504 | " | | | | |
| " " 0°-100° | 100.0 | .36626 | 2 | | | | |
| Nitrogen 13°-132° | .06 | .3621 | 6 | | | | |
| " " 9°-132° | .53 | .3290 | " | | | | |
| " " 0°-20° | 100.2 | .36754 | 2 | | | | |
| " " 0°-100° | 100.2 | .36744 | " | | | | |
| " | 76. | .36682 | 7 | | | | |
| Oxygen 11°-132° | .007 | .4161 | 6 | | | | |
| " " 9°-132° | .25 | .3984 | " | | | | |
| " " 11°-132° | .51 | .3831 | " | | | | |
| " | 1.9 | .36683 | 8 | | | | |
| " | 18.5 | .36600 | " | | | | |
| " | 75.9 | .36681 | " | | | | |
| Nitrous oxide | 76. | .3676 | 3 | | | | |
| Sulphur dioxide SO ₂ | 76. | .3845 | " | | | | |

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SPECIFIC HEAT OF THE CHEMICAL ELEMENTS

When one temperature is given the true specific heat is given, otherwise the mean specific heat between the given limits. See page 289 for references.

| Element | $t^{\circ}\text{C}$ | Sp.ht. | Ref. | Element | $t^{\circ}\text{C}$ | Sp.ht. | Ref. |
|------------------|---------------------|--------|------|-------------------|---------------------|--------|------|
| Aluminum..... | -250 | 0.0039 | .. | Carbon, graph.... | -183 | 0.0025 | 19 |
| | -200 | .076 | .. | | - 66 | .053 | 19 |
| | -150 | .1367 | 1 | | 11 | .112 | 19 |
| | -100 | .1676 | 1 | | 85 | .177 | 19 |
| | - 50 | .1914 | 1 | | 896 | .454 | 19 |
| | 0 | .2079 | 1 | C, diamond..... | 0 | .1044 | 20 |
| | 100 | .225 | .. | | 223 | .264 | 20 |
| | 300 | .248 | 2 | | 823 | .428 | 20 |
| | 600 | .277 | 2 | Cerium..... | -253, -196 | .033 | 21 |
| | 16, 100 | .212 | 3 | | 20, 100 | .0511 | 22 |
| Antimony*..... | -207.1 | .0322 | 4 | Chlorine..... | 0, 24 | .226 | 23 |
| | -150 | .0412 | 1 | Chromium..... | -150 | .0599 | 1 |
| | -100 | .0448 | 1 | | -100 | .0797 | 1 |
| | - 50 | .0476 | 1 | | - 50 | .0941 | 1 |
| | 0 | .0494 | 1 | | 0 | .1044 | 1 |
| | 28 | .0477 | 5 | | 100 | .112 | 25 |
| | 20, 100 | .0504 | 6 | | 500 | .150 | 7 |
| | 500 | .054 | * | | 600 | .187 | 25 |
| Arsenic..... | -216 | .032 | 4 | | 18, 100 | .111 | 24 |
| | -117.6 | .0666 | 4 | Cobalt..... | -150 | .0672 | 1 |
| | 18 | .078 | 4 | | -100 | .0809 | 1 |
| Barium..... | -185, +20 | .068 | 7 | | - 50 | .0914 | 1 |
| Beryllium..... | -202 | .017 | 8 | | 0 | .1028 | 1 |
| | 45, 50 | .445 | 9 | | 20 | .1001 | * |
| | 0, 100 | .425 | 10 | | 100 | .1067 | * |
| Bismuth*..... | -150 | .0264 | 1 | | 200 | .1134 | * |
| | -100 | .0273 | 1 | Copper..... | -189 | .0506 | 26 |
| | - 50 | .0282 | 1 | | -150 | .0674 | 1 |
| | 0 | .0291 | 1 | | -100 | .0783 | 1 |
| | 20 | .0294 | * | | - 50 | .0862 | 1 |
| | 100 | .0304 | * | | 0 | .0910 | 1 |
| fluid | 297 | .0292 | 4 | | 100 | .0939 | * |
| Boron..... | 100 | .287 | 11 | | 900 | .1259 | 27 |
| | 500 | .472 | 11 | | 18, 100 | .0928 | 24 |
| | 900 | .510 | 11 | | 18, 600 | .0994 | 24 |
| | -76, 0 | .168 | 12 | Gallium..... | -258.1 | .0049 | 29 |
| | 0, 100 | .307 | 13 | | -213.1 | .044 | 29 |
| Bromine,(s)..... | -253.1 | .0205 | 14 | | - 73.1 | .084 | 29 |
| (s)..... | -173.1 | .0659 | 14 | Germanium..... | 0, 100 | .074 | 10 |
| (s)..... | - 73.1 | .080 | 14 | Gold..... | -258.1 | .0018 | 29 |
| (s)..... | -13.1 | .088 | 14 | | -252.8 | .0040 | 29 |
| (l)..... | 13, 45 | .107 | 15 | | -209.5 | .0211 | 29 |
| Cadmium..... | -263 | .0019 | 16 | | -150 | .0266 | 1 |
| | -203.1 | .0415 | 16 | | -100 | .0281 | 1 |
| | -103.1 | .0518 | 16 | | - 50 | .0293 | 1 |
| | 27.9 | .0552 | 16 | | 0 | .0302 | 1 |
| | 107.9 | .0569 | 16 | | 18 | .0312 | 30 |
| | 277 | .060 | 16 | | 100 | .0314 | 30 |
| Caesium..... | 0, 26 | .0482 | 17 | Indium..... | 0, 100 | .057 | 31 |
| Calcium..... | 24 | .168 | 18 | Iodine..... | -263.2 | .0037 | 32 |
| | 100 | .1625 | 2 | | -255.9 | .0118 | 32 |
| | 300 | .1832 | 2 | | -221.1 | .0353 | 32 |
| | 600 | .188 | 2 | | -90, +17 | .0485 | 33 |
| Carbon, graph.. | -191, -79 | .057 | 12 | Iridium..... | -186, +18 | .0282 | 34 |
| | - 76, 0 | .126 | 12 | | 18, 100 | .0323 | 34 |

SPECIFIC HEAT OF THE CHEMICAL ELEMENTS

| Element | t°C | Sp.ht. | Ref. | Element | t°C | Sp.ht. | Ref. | |
|------------------|-------------------------------|-----------|--------|------------------|--------------------|-----------|-------|------|
| Iron, pure..... | -256.2 | 0.00067 | 26 | Molybdenum.... | - 34.5 | 0.0561 | 44 | |
| | -240.7 | .00355 | 26 | | 0 | .0589 | 45 | |
| | -214.0 | .0194 | 26 | | + 5.3 | .0589 | 44 | |
| | -172.6 | .0512 | 26 | | +100 | .0612 | 45 | |
| | - 67.5 | .0939 | 26 | 250 | .0632 | 45 | | |
| | 0 | .1043 | .. | Nickel..... | -258 | .0008 | 26 | |
| | α, β, γ | 100 | .115 | | 27 | -247.9 | .0024 | 26 |
| | | 500 | .163 | | 27 | -201.2 | .0363 | 42 |
| | | 760 | .320 | | 27 | -150 | .0660 | I |
| | | 1000 | .162 | | 27 | -100 | .0817 | I |
| γ | 100 | .127 | 26 | | - 50 | .0940 | I | |
| | 700 | .157 | 26 | | 0 | .1032 | I | |
| | 1000 | .162 | 26 | | 100 | .1146 | 35 | |
| Lanthanum..... | 0, 100 | .0448 | 36 | | 500 | .1270 | 35 | |
| Lead..... | -270 | .00001 | 37 | | 800 | .1413 | 35 | |
| | -267 | .00086 | 38 | Osmium..... | 19, 98 | .0311 | 46 | |
| | -259 | .0073 | 38 | | Palladium..... | -180, +18 | .0528 | 34 |
| | -150 | .0279 | I | | | 0 | .0538 | 47 |
| | -100 | .0283 | I | | | 100 | .0564 | 47 |
| | - 50 | .0289 | I | 500 | | .0653 | 47 | |
| | 0 | .0297 | I | 900 | .0717 | 47 | | |
| | 100 | .0320 | 35 | 1500 | .0766 | 47 | | |
| | (I)..... | 300 | .0356 | 35 | Phosphorus, yellow | -136 | .124 | 5 |
| | | 360 | .0375 | 35 | | - 40 | .165 | 5 |
| 500 | | .0370 | 35 | + 9 | | .189 | 5 | |
| -183 | | .3 | 39 | (red)..... | | -136 | .107 | 5 |
| Lithium..... | -100 | .600 | 40 | - 40 | .182 | 5 | | |
| | 50 | .96 | 39 | + 9 | .190 | 5 | | |
| | +190 | 1.374 | 40 | Platinum..... | -255.6 | .00123 | 44 | |
| | -150 | .1767 | I | | -237.7 | .0073 | 44 | |
| -100 | .2025 | I | -191.7 | | .0211 | 44 | | |
| - 50 | .2228 | I | -152.1 | | .0261 | 44 | | |
| 0 | .2316 | I | - 64.8 | | .0307 | 44 | | |
| 100 | .257 | 2 | 0 | | .03162 | I | | |
| (I)..... | 300 | .279 | 2 | 500 | .0349 | 47 | | |
| | 600 | .311 | 2 | 750 | .0365 | 47 | | |
| | 650, 775 | .284 | 41 | 1000 | .0381 | 47 | | |
| | Manganese..... | -188, -79 | .0820 | 33 | 1300 | .0400 | 47 | |
| -79, +15 | | .1091 | 33 | 20, 100 | .0319 | 47 | | |
| 60 | | .1211 | 33 | 20, 1000 | .0346 | 47 | | |
| 325 | | .1783 | 33 | Potassium..... | -258.4 | .032 | 44 | |
| 20, 100 | | .1211 | 33 | | -255.8 | .045 | 44 | |
| -100 | | .0979 | 40 | | -201.3 | .140 | 44 | |
| 0 | | .1072 | 40 | | - 53.1 | .172 | 44 | |
| 100 | | .1143 | 40 | | + 3.4 | .177 | 44 | |
| Mercury (s)..... | | -263.3 | .00552 | | 42 | (I)..... | 90 | .200 |
| | | -267.2 | .00620 | 42 | 181 | .196 | 48 | |
| | -259.8 | .00783 | 42 | Rhenium..... | 0, 20 | .035 | 49 | |
| | -245.6 | .0172 | 42 | Rhodium..... | 10, 97 | .058 | 46 | |
| | -220.2 | .0255 | 42 | Rubidium (s).... | 0 | .0802 | 50 | |
| | -163.7 | .0298 | 42 | (I)..... | 50 | .0908 | 50 | |
| | - 81.4 | .0324 | 42 | Ruthenium..... | 0, 100 | .0611 | 31 | |
| | - 43.1 | .0337 | 43 | Selenium..... | 3 | .072 | 51 | |
| | - 33.1 | .0338 | 43 | 16.5 | .075 | 52 | | |
| | (See Table 276) | - 3.1 | .0335 | 43 | 20.5 | .077 | 52 | |
| Molybdenum.... | + 17 | .0333 | 43 | 29.5 | .085 | 52 | | |
| | -257 | .0004 | 44 | 32 | .127 | 52 | | |
| | -239.1 | .0034 | 44 | 38 | .131 | 52 | | |
| | -181.5 | .0300 | 44 | 41.7 | .130 | 52 | | |
| | -152.7 | .0399 | 44 | 20 | .09 | .. | | |

TABLE 271 (concluded).—Specific Heat of the Chemical Elements

| Element | $t^{\circ}\text{C}$ | Sp.ht. | Ref. | Element | $t^{\circ}\text{C}$ | Sp.ht. | Ref. |
|----------------|---------------------|--------|------|---------------|---------------------|--------|------|
| Silicon..... | -212 | 0.029 | 53 | Thorium..... | -253, -196 | 0.0197 | 21 |
| | -143.3 | .087 | 53 | | 0, 100 | .0276 | 62 |
| | -86.2 | .126 | 53 | Tin..... | -203.5 | .0385 | 63 |
| | +13.9 | .168 | 53 | | -186.7 | .0422 | 63 |
| | 18.2, +99.1 | .181 | 54 | | -150 | .0450 | 1 |
| | 18.0, 900.6 | .210 | 54 | | -100 | .0483 | 1 |
| Silver..... | -238 | .0146 | 28 | | -50 | .0512 | 1 |
| | -150 | .0461 | 1 | | 0 | .0536 | 1 |
| | -100 | .0505 | 1 | | +25 | .0548 | 63 |
| | -50 | .0537 | 1 | | 100 | .0577 | * |
| | 0 | .0557 | 1 | | 1100 | .0758 | 64 |
| | 100 | .0564 | * | Titanium..... | -185, +20 | .082 | 7 |
| | 300 | .0601 | 2 | | 0, 100 | .1125 | 10 |
| | 900 | .0685 | 2 | Tungsten..... | -247.1 | .0012 | 32 |
| | 20-900 | .0650 | 55 | | -218.4 | .0098 | 32 |
| | 20-1200 | .0880 | 55 | | -173.1 | .0205 | 65 |
| Sodium..... | -256.1 | .026 | 44 | | -73.1 | .0288 | 65 |
| | -238.5 | .108 | 44 | | +26.9 | .0321 | 65 |
| | -155.5 | .245 | 44 | | 100 | .0320 | 66 |
| (l)..... | 100 | .32 | .. | | 500 | .0344 | 66 |
| Sulphur..... | -188, +18 | .137 | 57 | | 1000 | .0367 | 66 |
| (l)..... | 115, 160 | .220 | 56 | | 1500 | .0390 | 66 |
| rhombic..... | 15, 96 | .176 | 56 | Uranium..... | 0, 98 | .0280 | 67 |
| monochin..... | 0, 52 | .181 | 58 | Vanadium..... | 0, 100 | .1153 | 68 |
| Tantalum..... | -201.7 | .0205 | 8 | Zinc..... | 0, 100 | .095 | .. |
| | +380 | .035 | 59 | | -252.4 | .0071 | 69 |
| | 900 | .036 | 59 | | -201.3 | .0573 | 69 |
| | 1100 | .043 | 59 | | -150 | .0740 | 1 |
| | 1400 | .044 | 59 | | -100 | .0814 | 1 |
| Tellurium..... | -188, +18 | .047 | 57 | | -50 | .0871 | 1 |
| | 15, 100 | .0483 | 60 | | 0 | .0913 | 1 |
| | 15, 200 | .0487 | 60 | | 100 | .0957 | * |
| Thallium..... | -135 | .288 | .. | | 300 | .1043 | 2 |
| | 28 | .311 | 5 | | 400 | .1089 | 2 |
| | 20, 100 | .0326 | 61 | | | | |

TABLE 272.—Formulae for True Specific Heats

| Element | Range $^{\circ}\text{C}$ |
|-----------|---|
| Antimony | 0.0493 + 0.000012 t 0-500 |
| Bismuth | .0292 + .000012 t 0-200 |
| Chromium | .1055 + .00010 t - 0.00000015 t^2 0-400 |
| Cobalt | .1000 + .000067 t 0-400 |
| Copper | .0915 + .000024 t 0-300 |
| Iron | .1060 + .000096 t 0-400 |
| Lead | .0295 + .00002 t 0-300 |
| Magnesium | .2370 + .000142 t - .0000001 t^2 0-400 |
| Nickel | .1020 + .000118 t - .00000006 t^2 0-300 |
| Platinum | .03162 + .00000617 t + $2.33 \times 10^{10} t^2$ 0-1625 |
| Silver | .0556 + .000008 t 0-400 |
| Tin | .0525 + .000052 t 0-200 |
| Zinc | .0913 + .000044 t 0-300 |

Pt from Jaeger & Rosenbaum, 1928. Others recalculated by Dr. W. P. White (1931), mainly from Schübel.

HEAT CAPACITIES, TRUE AND MEAN SPECIFIC HEATS, AND LATENT HEATS AT FUSION (SEE PP. 285-287)

The following data are taken from a research and discussion entitled "Die Temperatur-Wärmeinhaltskurven der technisch wichtigen Metalle," Wüst, Meuthen und Durrer, Forschungsarbeiten herausgegeben vom Verein Deutscher Ingenieure, Springer, Heft 204, 1918.

(a) There follow the constants of the equation for the heat capacity: $W = a + bt + ct^2$; for the mean specific heat: $s = at^{-1} + b + ct$; and for the true specific heat: $s' = b + 2ct$; also the latent heats at fusion. Much greater faith should be given to tables on pages 285 to 287.

| Element | Temperature range, °C | a | b | c × 10 ⁶ | Latent heat, cal./g | Element | Temperature range, °C | a | b | c × 10 ⁶ | Latent heat, cal./g |
|---------|-----------------------|--------|---------|---------------------|---------------------|---------|-----------------------|--------|----------|---------------------|---------------------|
| Cr | 0-1500 | — | 0.10233 | 33.47 | — | Ag | 0-961 | — | 0.05725 | 5.48 | 26.0 |
| Mo | 0-1500 | — | 0.06162 | 10.99 | — | | 961-1300 | 53.17 | 0.00710 | 28.30 | — |
| W | 0-1500 | — | 0.03325 | 1.07 | — | Au | 0-1064 | — | 0.03171 | 1.30 | 15.9 |
| Pt | 0-1500 | — | 0.03121 | 3.54 | — | | 1064-1300 | 26.35 | 0.01420 | 8.52 | — |
| Sn | 0-232 | — | 0.06829 | — | 13.8 | Cu | 0-1084 | — | 0.10079 | 3.05 | 41.0 |
| | 232-1000 | 14.33 | 0.07020 | -18.30 | — | | 1084-1300 | 130.74 | -0.04150 | 65.6 | — |
| Bi | 0-270 | — | 0.03141 | 5.22 | 10.2 | Mn | 0-1070 | — | 0.12037 | 25.41 | 36.6 |
| | 270-1000 | 10.31 | 0.03107 | 5.41 | — | | 1130-1210 | -7.41 | 0.17700 | — | 24.14* |
| Cd | 0-321 | — | 0.05550 | 6.28 | 10.8 | | 1230-1250 | 3.83 | 0.10800 | — | — |
| | 321-1000 | 6.30 | 0.06952 | 6.37 | — | Ni | 0-320 | — | 0.10950 | 52.40 | 56.1 |
| Pb | 0-327 | — | 0.03591 | 11.47 | 5.47 | | 330-1451 | 0.41 | 0.12931 | 0.11 | 1.33* |
| | 327-1000 | 6.07 | 0.02020 | -3.30 | — | | 1451-1520 | 50.21 | 0.13380 | — | — |
| Zn | 0-419 | — | 0.08777 | 43.48 | 23.0 | Co | 0-950 | — | 0.09119 | 40.77 | 58.2 |
| | 419-1000 | 14.34 | 0.13340 | -16.10 | — | | 1100-1478 | 22.00 | 0.11043 | 14.57 | 14.70* |
| Sb | 0-630 | — | 0.05179 | 3.00 | 38.9 | | 1478-1600 | 57.72 | 0.14720 | — | — |
| | 630-1000 | 39.42 | 0.05090 | 2.96 | — | Fe | 0-725 | — | 0.10545 | 56.84 | 49.4 |
| Al | 0-657 | — | 0.22200 | 38.57 | 94.0 | | 785-919 | -1.63 | 0.1592 | — | 6.56* |
| | 657-1000 | 102.39 | 0.21870 | 24.00 | — | | 919-1404 | 18.31 | 0.14472 | 0.05 | 6.67* |
| | | | | | | | 1405-1528 | -77.18 | 0.21416 | — | 1.94* |
| | | | | | | | 1528-1600 | 70.03 | 0.15012 | — | — |

* Allotropic heat of transformation: Mn, 1070-1130°; Ni, 320-330°; Co, 950-1100°; Fe, 725-785°; 919° = 1; 1404.5° = 0.5.

(b) TRUE SPECIFIC HEATS

| ° C | Pb | Zn | Al | Ag | Au | Cu | Ni | Fe | Co | Silica glass |
|------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------------|
| 0 | 0.0359 | 0.0878 | 0.2220 | 0.0573 | 0.0317 | 0.1008 | 0.1095 | 0.1055 | 0.0912 | — |
| 100 | 0.0382 | 0.0965 | 0.2297 | 0.0583 | 0.0320 | 0.1014 | 0.1200 | 0.1168 | 0.0993 | 0.2372 |
| 200 | 0.0405 | 0.1052 | 0.2374 | 0.0594 | 0.0322 | 0.1020 | 0.1305 | 0.1282 | 0.1073 | 0.2416 |
| 300 | 0.0428 | 0.1139 | 0.2451 | 0.0605 | 0.0325 | 0.1026 | 0.1409 | 0.1306 | 0.1154 | 0.2460 |
| 400 | — | 0.1226 | 0.2520 | 0.0616 | 0.0328 | 0.1032 | 0.1509 | 0.1509 | 0.1235 | 0.2504 |
| 500 | — | 0.1173 | 0.2606 | 0.0627 | 0.0330 | 0.1038 | 0.1594 | 0.1623 | 0.1316 | 0.2548 |
| 600 | — | 0.1141 | 0.2683 | 0.0638 | 0.0333 | 0.1045 | 0.1594 | 0.1737 | 0.1396 | 0.2592 |
| 700 | — | 0.1100 | 0.2523 | 0.0649 | 0.0335 | 0.1051 | 0.1295 | 0.1850 | 0.1477 | 0.2636 |
| 800 | — | 0.1070 | 0.2571 | 0.0660 | 0.0338 | 0.1057 | 0.1295 | 0.1592 | 0.1558 | 0.2680 |
| 900 | — | 0.1044 | 0.2619 | 0.0671 | 0.0341 | 0.1063 | 0.1295 | 0.1592 | 0.1639 | 0.2724 |
| 1000 | — | 0.1012 | 0.2667 | 0.0637 | 0.0343 | 0.1060 | 0.1295 | 0.1448 | — | 0.2768 |
| 1100 | — | — | — | 0.0604 | 0.0329 | 0.1028 | 0.1296 | 0.1448 | 0.1424 | 0.2812 |
| 1200 | — | — | — | 0.0750 | 0.0340 | 0.1159 | 0.1296 | 0.1448 | 0.1454 | 0.2856 |
| 1300 | — | — | — | 0.0807 | 0.0364 | 0.1291 | 0.1296 | 0.1449 | 0.1483 | 0.2900 |
| 1400 | — | — | — | — | — | — | 0.1296 | 0.1449 | 0.1512 | 0.2944 |
| 1500 | — | — | — | — | — | — | 0.1338 | 0.2142 | 0.1472 | 0.2988 |
| 1600 | — | — | — | — | — | — | — | 0.1501 | 0.1472 | — |

For more elaborate tables and for all the elements in upper table, see original reference.

**ATOMIC HEATS (50°K.), SPECIFIC HEATS (50°K.),
ATOMIC VOLUMES OF THE ELEMENTS**

The atomic and specific heats are due to Dewar, Pr. Roy. Soc. 89A, 168, 1913

| Element. | Specific heat —223° C. | Atomic heat —223° C. | Atomic volume. | Element. | Specific heat —223° C. | Atomic heat —223° C. | Atomic volume. | Element. | Specific heat —223° C. | Atomic heat —223° C. | Atomic volume. |
|----------|---------------------------|-------------------------|----------------|----------|---------------------------|-------------------------|----------------|----------|---------------------------|-------------------------|----------------|
| Li | 0.1924 | 1.35 | 13.0 | Cr | 0.0142 | 0.70 | 7.6 | Sn | 0.0286 | 3.41 | 20.3 |
| Gl | 0.0137 | 0.125 | 4.9 | Mn | 0.0229 | 1.26 | 7.4 | Sb | 0.0240 | 2.89 | 18.2 |
| B | 0.0212 | 0.24 | 4.5 | Fe | 0.0175 | 0.98 | 7.1 | I | 0.0361 | 4.59 | 25.7 |
| C* | 0.0137 | 0.16 | 5.1 | Ni | 0.0208 | 1.22 | 6.7 | Te | 0.0288 | 3.68 | 21.2 |
| C† | 0.0028 | 0.03 | 3.4 | Co | 0.0207 | 1.22 | 6.8 | Cs | 0.0513 | 6.82 | 71.0 |
| Na | 0.1519 | 3.50 | 23.6 | Cu | 0.0245 | 1.56 | 7.1 | Ba‡ | 0.0350 | 4.80 | 36.6 |
| Mg | 0.0713 | 1.74 | 14.1 | Zn | 0.0384 | 2.52 | 9.2 | La | 0.0322 | 4.60 | 22.6 |
| Al | 0.0413 | 1.12 | 10.0 | As | 0.0258 | 1.94 | 15.9 | Ce | 0.0330 | 4.64 | 20.3 |
| Si† | 0.0303 | 0.86 | 14.2 | Se | 0.0361 | 2.86 | 18.5 | W | 0.0095 | 1.75 | 9.8 |
| Si§ | 0.0303 | 0.77 | 11.4 | Br | 0.0453 | 3.62 | 24.9 | Os | 0.0078 | 1.49 | 8.5 |
| P | | | | Rb | 0.0711 | 6.05 | 55.8 | Ir | 0.0099 | 1.92 | 8.6 |
| yel. P | 0.0774 | 2.40 | 17.0 | Sr¶ | 0.0550 | 4.82 | 34.5 | Pt | 0.0135 | 2.63 | 9.2 |
| | | | | Zr | 0.0262 | 2.38 | 21.8 | Au | 0.0160 | 3.16 | 10.2 |
| red S | 0.0431 | 1.34 | 13.5 | Mo | 0.0141 | 1.36 | 9.3 | Hg | 0.0232 | 4.65 | 14.8 |
| S | 0.0546 | 1.75 | 16. | Ru | 0.0109 | 1.11 | 9.0 | Tl | 0.0235 | 4.80 | 17.2 |
| Cl | 0.0967 | 3.43 | 24.6 | Rh | 0.0134 | 1.38 | 8.5 | Pb | 0.0240 | 4.96 | 18.3 |
| K | 0.1280 | 5.01 | 44.7 | Pd | 0.0190 | 2.03 | 9.2 | Bi | 0.0218 | 4.54 | 21.3 |
| Ca | 0.0714 | 2.86 | 25.9 | Ag | 0.0242 | 2.62 | 10.2 | Th | 0.0197 | 4.58 | 21.1 |
| Ti | 0.0205 | 0.99 | 10.7 | Cd | 0.0308 | 3.46 | 13.0 | U | 0.0138 | 3.30 | 12.8 |

* Graphite. † Diamond. ‡ Fused. § Crystallized. ¶ Impure.

References to Table 271: * Values derived from formulae recalculated by Dr. W. P. White from Schübel's results. The Pt formula is from Jaeger and Rosenbaum. (1) Schimpff values interpolated by White. (2) Eastman, William Young, 1924. (3) Magnus, 1910. (4) Anderson, 1930. (5) Ewald, 1914. (6) Linnavuori, 1922. (7) Nordmeyer, Bernoulli, 1907-8. (8) Simon-Rubemann, 1927. (9) Humpidge, 1883. (10) Nilson, Pettersson, 1880. (11) Magnus and Danz, 1926. (12) Kosef, 1911. (13) Moisson, Gautier, 1896. (14) Suhrmann, Lüde, 1924. (15) Andrews, 1848. (16) Lange, Simon, 1928. (17) Eckardt, Graefe, 1900. (18) Eastman, Rodebush. (19) Nernst, Lindemann, 1911. (20) Magnus, Hodler, 1926. (21) Dewar, 1913. (22) Hirsch, 1912. (23) Kneitsch. (24) Schübel, 1914. (25) Adler, 1903. (26) Eucken, Werth, 1930. (27) Richards, 1893. (28) Griffiths, 1894. (29) Clusius, Harteck, 1928. (30) Jaeger, Diesselhorst, 1900. (31) Bunsen, 1870. (32) Lange, 1924. (33) Estreicher, Straniewski, 1912. (34) Behn, 1900. (35) Kleinkhardt, 1927. (36) Hillebrand, 1876. (37) Keesom, 1927. (38) v. d. Eude. (39) Bidwell, 1925. (40) Laemmel, 1905. (41) Zulinski, 1928. (42) Simon, 1922. (43) Carpenter, Stoodley, 1930. (44) Simon, Zeidler, 1926. (45) Cooper, Langstroth, 1929. (46) Regnault, 1849, 1861. (47) White, 1918. (48) Dixon, Rodebush, 1927. (49) Noddeck, 1928. (50) Rengade, 1913. (51) Tammann. (52) Gronow. (53) Anderson, 1930. (54) Magnus, 1923. (55) Umino, 1926. (56) Mondain, Monval, 1926. (57) Dewar, 1905. (58) Wilgard, 1906. (59) Pirani, 1912. (60) Tilden, 1904. (61) Schmitz, 1903. (62) Wilson, 1883. (63) Rodebush, 1923. (64) Pionchon, 1886. (65) Zwikker, 1928. (66) Jaeger, Rosenbaum, 1930. (67) Blümcke, 1885. (68) Mache, 1897. (69) Clusius, Harteck, 1928.

References to Table 276: R, Regnault. L, Lorentz. T, Tomlinson. JD, Jaeger, Diesselhorst. M, Mazotto. S, Schüz. P, Person. W, Wachsmuth. Z, Zouloff. HM, H. Meyer. B, Batelli. GT, Gee and Terry. RW, R. W. Weber.

TABLE 275.—Specific Heat of Various Solids

| Solid | Temperature °C | Specific heat | Authority See p. 289 |
|---|-------------------|------------------|-------------------------|
| Alloys: | | | |
| Bell metal. | 15-98 | .0858 | R |
| Brass, red. | 0 | .08991 | L |
| " yellow. | 0 | .08831 | " |
| 80 Cu + 20 Sn. | 14-98 | .0862 | R |
| Constantan, 60 "Cu, 40 "Ni. | 18 | .0977 | J D |
| " | 100 | .1018 | " |
| German silver. | 0-100 | .09464 | T |
| Lipowitz alloy: 24.97 Pb + 10.13 Cd + 50.66 Bi + 14.24 Sn. | 5-50 | .0345 | M |
| Lipowitz alloy. | 100-150 | .0426 | " |
| Manganin: 84 "Cu, 4 "Ni, 12 "Mn. | 18 | .0973 | J D |
| " | 100 | .1004 | " |
| Monel metal. | 20-1300 | .127 | — |
| Rose's alloy: 27.5 Pb + 48.9 Bi + 23.6 Sn. | 77-20 | .0356 | S |
| " | 20-89 | .0552 | " |
| Wood's alloy: 25.85 Pb + 6.99 Cd + 52.43 Bi + 14.73 Sn. | 5-50 | .0352 | M |
| Wood's alloy: (fluid). | 100-150 | .0426 | " |
| Miscellaneous alloys: | | | |
| 17.5 Sb + 29.9 Bi + 18.7 Zn + 33.9 Sn. | 20-99 | .05657 | R |
| 37.1 Sb + 62.9 Pb. | 10-98 | .03880 | " |
| 39.9 Pb + 60.1 Bi. | 16-99 | .03165 | P |
| 63.8 Bi + 36.2 Sn. | 20-99 | .04001 | R |
| 46.9 Bi + 53.1 Sn. | 20-99 | .04504 | " |
| Gas coal. | 20-1040 | .3145 | — |
| Glass, normal thermometer 16 ^m | 19-100 | .1988 | W |
| " French hard thermometer. | | .1869 | Z |
| " crown. | 10-50 | .161 | H M |
| " flint. | 10-50 | .117 | " |
| Ice. | — 80 | .350 | B M |
| " | — 40 | .434 | " |
| " | — 20 | .465 | " |
| " | 0 | .487 | " |
| India rubber (Para). | ?-100 | .481 | G T |
| Mica. | 20 | .10 | — |
| Paraffin. | — 20- + 3 | .3768 | R W |
| " | — 19- + 20 | .5251 | " |
| " | 0-20 | .6939 | " |
| " | 35-40 | .622 | B |
| " fluid. | 60-63 | .712 | " |
| Woods. | 20 | .327 | — |

TABLE 276.—Specific Heat of Water and of Mercury

| Specific Heat of Water. | | | | | | | Specific Heat of Mercury. | | | |
|-------------------------|---------|----------|----------------------|-----------------------|--------|----------------------|---------------------------|-------------------|-----------------------|-------------------|
| Temper- ature, °C. | Barnes. | Rowland. | Barnes- Regnault. | Temper- ature, °C. | Barnes | Barnes- Regnault. | Temper- ature, °C. | Specific Heat. | Temper- ature, °C. | Specific Heat. |
| −5 | 1.0155 | — | — | 60 | 0.9988 | 0.9994 | 0 | 0.03346 | 90 | 0.03277 |
| 0 | 1.0091 | 1.0070 | 1.0094 | 65 | .9994 | 1.0004 | 5 | .03340 | 100 | .03269 |
| +5 | 1.0050 | 1.0039 | 1.0053 | 70 | 1.0001 | 1.0015 | 10 | .03335 | 110 | .03262 |
| 10 | 1.0020 | 1.0016 | 1.0023 | 80 | 1.0014 | 1.0042 | 15 | .03330 | 120 | .03255 |
| 15 | 1.0000 | 1.0000 | 1.0003 | 90 | 1.0028 | 1.0070 | 20 | .03325 | 130 | .03248 |
| 20 | 0.9987 | .9991 | 0.9990 | 100 | 1.0043 | 1.0101 | 25 | .03320 | 140 | .03241 |
| 25 | .9978 | .9989 | .9981 | 120 | — | 1.0162 | 30 | .03316 | 150 | .0324 |
| 30 | .9973 | .9990 | .9976 | 140 | — | 1.0223 | 35 | .03312 | 170 | .0322 |
| 35 | .9971 | .9997 | .9974 | 160 | — | 1.0285 | 40 | .03308 | 190 | .0320 |
| 40 | .9971 | 1.0006 | .9974 | 180 | — | 1.0348 | 50 | .03300 | 210 | .0319 |
| 45 | .9973 | 1.0018 | .9976 | 200 | — | 1.0410 | 60 | .03294 | — | — |
| 50 | .9977 | 1.0031 | .9980 | 220 | — | 1.0476 | 70 | .03289 | — | — |
| 55 | .9982 | 1.0045 | .9985 | — | — | — | 80 | .03284 | — | — |

Barnes's results: Phil. Trans. (A) 199, 1902; Phys. Rev. 15, 1902; 16, 1903. (H thermometer.)

Bousfield, Phil. Trans. A 211, p. 199, 1911.

Barnes-Regnault's as revised by Peabody; Steam Tables.

The mercury data from 0° C to 80, Barnes-Cooke (H thermometer); from 90° to 140, mean of Winklemann, Naccari and Mithaler (air thermometer); above 140°, mean of Naccari and Mithaler.

TABLE 277.—Specific Heat of Various Liquids

| Liquid. | Temp. °C. | Spec. heat. | Auth- ority. | Liquid. | Temp. °C. | Spec. heat. | Auth- ority. |
|---|--------------|----------------|-----------------|--|--------------|----------------|-----------------|
| Alcohol, ethyl. | -20 | 0.5053 | R | Ethyl ether. | 0 | 0.529 | R |
| " " " " " " " " " " | 0 | 0.548 | " | Glycerine. | 15-50 | 0.576 | E |
| " " " " " " " " " " | 40 | 0.648 | " | KOH + 30H ₂ O. | 18 | 0.876 | TH |
| Alcohol, methyl. | 5-10 | 0.590 | " | " + 100 " " " " " " | 18 | 0.975 | " |
| " " " " " " " " " " | 15-20 | 0.601 | " | NaOH + 50H ₂ O. | 18 | 0.942 | " |
| Anilin. | 15 | 0.514 | G | " + 100 " " " " " " | 18 | 0.983 | " |
| " " " " " " " " " " | 30 | 0.520 | " | NaCl + 10H ₂ O. | 18 | 0.791 | " |
| " " " " " " " " " " | 50 | 0.529 | " | " + 200 " " " " " " | 18 | 0.978 | " |
| Benzole, C ₆ H ₆ | 10 | 0.340 | H-D | Naphthalene, C ₁₀ H ₈ | 80-85 | 0.396 | B |
| " " " " " " " " " " | 40 | 0.423 | " | Nitrobenzole. | 90-95 | 0.409 | " |
| " " " " " " " " " " | 65 | 0.482 | " | " " " " " " " " " " | 14 | 0.350 | A |
| CaCl ₂ , sp. gr. 1.14. | -15 | 0.764 | DMG | " " " " " " " " " " | 28 | 0.362 | " |
| " " " " " " " " " " | 0 | 0.775 | " | Oils: castor. | — | 0.434 | W |
| " " " " " " " " " " | +20 | 0.787 | " | " citron. | 5.4 | 0.438 | HW |
| " " " " " " " " " " | -20 | 0.695 | " | " olive. | 6.6 | 0.471 | " |
| " " " " " " " " " " | 0 | 0.712 | " | " sesame. | — | 0.387 | " |
| " " " " " " " " " " | +20 | 0.725 | " | " turpentine. | 0 | 0.411 | R |
| " " " " " " " " " " | -20 | 0.651 | " | Petroleum. | 21-58 | 0.511 | Pa |
| " " " " " " " " " " | 0 | 0.663 | " | Sea water, sp. gr. 1.0043. | 17.5 | 0.980 | " |
| " " " " " " " " " " | +20 | 0.676 | " | " " " " " " " " " " | 17.5 | 0.938 | " |
| CuSO ₄ + 50 H ₂ O. | 12-15 | 0.848 | Pa | " " " " " " " " " " | 17.5 | 0.903 | " |
| " + 200 " " " " " " " " | 12-14 | 0.951 | " | Toluol, C ₆ H ₅ | 10 | 0.364 | H-D |
| " + 400 " " " " " " " " | 13-17 | 0.975 | " | " " " " " " " " " " | 65 | 0.490 | " |
| Diphenylamine, | | | | " " " " " " " " " " | 85 | 0.534 | " |
| C ₁₂ H ₁₁ N. | 53 | 0.464 | B | ZnSO ₄ + 50 H ₂ O. | 20-52 | 0.842 | Ma |
| " " " " " " " " " " | 65 | 0.482 | " | " + 200 " " " " " " | 20-52 | 0.952 | " |

References: (A) Abbot; (B) Batelli; (E) Emo; (G) Griffiths; (DMG) Dickinson, Mueller, and George; (H-D) de Heen and Deruyts; (Ma) Marignac; (Pa) Pagliani; (R) Regnault; (Th) Thomsen; (W) Wachsmuth; (Z) Zouloff; (HW) H. F. Weber.

TABLE 278.—Specific Heat of Liquid Ammonia under Saturation Conditions

Expressed in Calories₂₀ per Gram per Degree C. Osborne and van Dusen, Bul. Bureau of Standards, 1918.

| Temp. °C. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|--------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| -40 | 1.062 | 1.061 | 1.060 | 1.059 | 1.058 | 1.058 | 1.057 | 1.056 | 1.055 | 1.055 |
| -30 | 1.070 | 1.069 | 1.068 | 1.067 | 1.066 | 1.065 | 1.064 | 1.064 | 1.063 | 1.062 |
| -20 | 1.078 | 1.077 | 1.076 | 1.075 | 1.074 | 1.074 | 1.073 | 1.072 | 1.071 | 1.070 |
| -10 | 1.088 | 1.087 | 1.086 | 1.085 | 1.084 | 1.083 | 1.082 | 1.081 | 1.080 | 1.079 |
| -0 | 1.099 | 1.098 | 1.097 | 1.096 | 1.094 | 1.093 | 1.092 | 1.091 | 1.090 | 1.089 |
| +0 | 1.099 | 1.100 | 1.101 | 1.103 | 1.104 | 1.105 | 1.106 | 1.108 | 1.109 | 1.110 |
| +10 | 1.112 | 1.113 | 1.114 | 1.116 | 1.117 | 1.118 | 1.120 | 1.122 | 1.123 | 1.125 |
| +20 | 1.126 | 1.128 | 1.129 | 1.131 | 1.132 | 1.134 | 1.136 | 1.137 | 1.139 | 1.141 |
| +30 | 1.142 | 1.144 | 1.146 | 1.148 | 1.150 | 1.152 | 1.154 | 1.156 | 1.158 | 1.160 |
| +40 | 1.162 | 1.164 | 1.166 | 1.169 | 1.171 | 1.173 | 1.176 | 1.178 | 1.181 | 1.183 |

TABLE 279.—Heat Content of Saturated Liquid Ammonia

Heat content = $H = \epsilon + pv$, where ϵ is the internal or intrinsic energy. Osborne and van Dusen, Bul. Bureau of Standards, 1918.

| Temperature . . . | -50° | -40° | -30° | -20° | -10° | 0° | +10° | +20° | +30° | +40° | +50° |
|-----------------------------|-------|-------|-------|-------|-------|-----|-------|-------|-------|-------|-------|
| $H = \epsilon + pv$ | -53.8 | -43.3 | -32.6 | -21.8 | -11.0 | 0.0 | +11.1 | +22.4 | +33.9 | +45.5 | +57.4 |

TABLE 280.—Specific Heat of Minerals and Rocks

| Substance. | Temperature °C. | Specific Heat. | Reference. | Substance. | Temperature °C. | Specific Heat. | Reference. |
|---|-----------------|----------------|------------|---------------------------------------|-----------------|----------------|------------|
| Andalusite | 0-100 | .01684 | 1 | Rock-salt | 13-45 | 0.219 | 6 |
| Anhydrite, CaSO ₄ | 0-100 | .1753 | 1 | Serpentine | 16-98 | .2586 | 2 |
| Apatite | 15-99 | .1903 | 2 | Siderite | 9-98 | .1934 | 4 |
| Asbestos | 20-98 | .195 | 3 | Spinel | 15-47 | .194 | 6 |
| Augite | 20-98 | .1931 | 3 | Talc | 20-98 | .2092 | 3 |
| Barite, BaSO ₄ | 10-98 | .1128 | 4 | Topaz | 0-100 | .2097 | 1 |
| Beryl | 15-99 | .1979 | 2 | Wollastonite | 19-51 | .178 | 6 |
| Borax, Na ₂ B ₄ O ₇ fused | 16-98 | .2382 | 4 | Zinc blende, ZnS | 0-100 | .1146 | 1 |
| Calcite, CaCO ₃ | 0-50 | .1877 | 1 | Zircon | 21-51 | .132 | 6 |
| “ “ | 0-100 | .2005 | 1 | Rocks: | | | |
| “ “ | 0-300 | .2204 | 1 | Basalt, fine, black | 12-100 | .1996 | 6 |
| Cassiterite SnO ₂ | 16-98 | .0933 | 4 | “ “ “ | 20-470 | .199 | 9 |
| Chalcopyrite | 15-99 | .1291 | 2 | “ “ “ | 470-750 | .243 | 9 |
| Corundum | 9-98 | .1976 | 4 | “ “ “ | 750-880 | .626 | 9 |
| Cryolite, Al ₂ F ₆ .6NaF | 16-99 | .2522 | 2 | “ “ “ | 880-1190 | .323 | 9 |
| Fluorite, CaF ₂ | 15-99 | .2154 | 4 | Dolomite | 20-98 | .222 | 3 |
| Galena, PbS | 0-100 | .0466 | 5 | Gneiss | 17-99 | .196 | 10 |
| Garnet | 16-100 | .1758 | 2 | “ “ “ | 17-213 | .214 | 10 |
| Hematite, Fe ₂ O ₃ | 15-99 | .1645 | 2 | Granite | 12-100 | .192 | 7 |
| Hornblende | 20-98 | .1952 | 3 | Kaolin | 20-98 | .224 | 3 |
| Hypersthene | 20-98 | .1914 | 3 | Lava, Aetna | 23-100 | .201 | 11 |
| Labradorite | 20-98 | .1949 | 3 | “ “ “ | 31-776 | .259 | 11 |
| Magnetite | 18-45 | .156 | 6 | “ Kilauea | 25-100 | .197 | 11 |
| Malachite, Cu ₂ CO ₄ H ₂ O | 15-99 | .1763 | 2 | Limestone | 15-100 | .216 | 12 |
| Mica (Mg) | 20-98 | .2061 | 3 | Marble | 0-100 | .21 | — |
| “ (K) | 20-98 | .2080 | 3 | Quartz sand | 20-98 | .191 | 3 |
| Oligoclase | 20-98 | .2048 | 3 | Sandstone | — | .22 | — |
| Orthoclase | 15-99 | .1877 | 2 | | | | |
| Pyrolusite, MnO ₂ | 17-48 | .159 | 6 | 1 Lindner. 6 Kopp. 11 Bartoli. | | | |
| Quartz, SiO ₂ | 12-100 | .188 | 7 | 2 Oeberg. 7 Joly. 12 Morano. | | | |
| “ “ | 0 | .1737 | 8 | 3 Ulrich. 8 Pionchon. | | | |
| “ “ | 350 | .2786 | 8 | 4 Regnault. 9 Roberts-Austen, Rücker. | | | |
| “ “ | 400-1200 | .305 | 8 | 5 Tilden. 10 R. Weber. | | | |

Compiled from Landolt-Börnstein-Meyerhoffer's Physikalisch-chemische Tabellen.

TABLE 281.—Specific Heat of Silicates

| Silicate. | Mean specific heats. 0° C to | | | | True specific heats. at | | | | |
|-----------------------------------|---------------------------------|-------|-------|--------|----------------------------|------|------|-------|-------|
| | 100° | 500° | 900° | 1400° | 0° C | 100° | 500° | 1000° | 1300° |
| Albite | .1948 | .2363 | .2561 | — | .178 | .211 | .269 | .294 | — |
| “ glass | .1977 | .2410 | .2640 | — | — | — | — | — | — |
| Amphibole, Mg. silicate | .2033 | .2461 | .2661 | .2731* | .185 | .219 | .279 | .304 | — |
| “ glass | .2040 | .2474 | — | — | — | — | — | — | — |
| Andesine | .1925 | .2330 | .2525 | — | — | — | .265 | — | — |
| “ glass | .1934 | — | .2615 | — | — | — | — | — | — |
| Anorthite | .1901 | .2296 | .2481 | .2674 | .174 | .205 | .260 | .286 | .318 |
| “ glass | .1883 | .2305 | — | — | — | — | — | — | — |
| Cristobalite | .1883 | .2426 | .2568 | .2680 | — | — | — | — | — |
| Diopside | .1924 | .2314 | .2500 | .2604† | .176 | .207 | .262 | .284 | — |
| “ glass | .1939 | .2332 | — | — | — | — | — | — | — |
| Microcline | .1871 | .2262 | .2450 | — | .171 | .201 | .258 | .279 | — |
| “ glass | .1919 | .2321 | .2514 | .2598* | .176 | .206 | .264 | .299 | — |
| Pyroxene | .2039 | .2484 | — | — | — | — | — | — | — |
| Quartz | .1868 | .2379 | .2596 | .2640* | .168 | .204 | .294 | .285 | — |
| Silica glass | .1845 | .2302 | .2512 | — | .166 | .202 | .266 | .29 | — |
| Wollastonite | — | — | .2344 | — | — | — | — | — | — |
| “ glass | .1852 | .2206 | — | — | — | — | — | — | — |
| “ pseudo | .1844 | .2170 | .2324 | .2448 | .171 | .197 | .243 | .262 | .272 |

*0°-1100°; †0°-1250°;

Taken from White, Am. J. Sc. 47, 1, 1919.

SPECIFIC HEAT OF GASES AND VAPORS

| Substance. | Range of temp. °C | Sp. ht. constant pres- sure. | Authority. | Range of temp. °C | Mean ratio of specific heats. C_p/C_v | Authority. |
|----------------------------------|-------------------|------------------------------|----------------|-------------------|---|------------------------|
| Acetone, C_3H_6O | 26-110 | 0.3468 | Wiedemann. | | | |
| Air..... | -30-+10 | 0.2377 | Regnault. | 20 | 1.4011 | Moody. |
| "..... | 0-200 | 0.2375 | " | -79.3 | 1.405 | Koch, 1907. |
| "..... | 20-440 | 0.2366 | Holborn and | -79.3 | 2.333 | " 200 atm |
| "..... | 20-630 | 0.2429 | Austin. | 0 | 1.828 | " |
| "..... | 20-800 | 0.2430 | " | 500 | 1.399 | Fürstenau. |
| Alcohol, C_2H_5OH | 108-220 | 0.4534 | Regnault. | 53 | 1.133 | Jaeger. |
| "..... | — | — | — | 100 | 1.134 | Stevens. |
| " CH_3OH | 101-223 | 0.4580 | Regnault. | 100 | 1.256 | " |
| Ammonia..... | 23-100 | 0.5202 | Wiedemann. | 0 | 1.3172 | Wüllner. |
| "..... | 27-200 | 0.5356 | " | 100 | 1.2770 | " |
| Argon..... | 20-90 | 0.1233 | Dittlenberger. | 0 | 1.667 | Niemeyer. |
| Benzene, C_6H_6 | 34-115 | 0.2900 | Wiedemann. | 20 | 1.403 | Pagliani. |
| "..... | 35-180 | 0.3325 | " | 60 | 1.403 | " |
| "..... | 116-218 | 0.3754 | Regnault. | 99.7 | 1.105 | Stevens. |
| Bromine..... | 83-228 | 0.0555 | " | 20-388 | 1.293 | Strecker. |
| Carbon dioxide, CO_2 | -28-+7 | 0.1843 | " | 4-11 | 1.2995 | Lummer and Pringsheim. |
| "..... | 15-100 | 0.2025 | " | | | |
| "..... | 11-214 | 0.2169 | " | 0 | 1.3003 | Moody, 1912. |
| " monoxide, CO | 23-99 | 0.2425 | Wiedemann. | 0 | 1.403 | Wüllner. |
| "..... | 26-198 | 0.2426 | " | 100 | 1.395 | " |
| " disulphide, CS_2 | 86-190 | 0.1506 | Regnault. | 3-67 | 1.205 | Beyme. |
| Chlorine..... | 16-343 | 0.1125 | Strecker. | 0 | 1.336 | Martini. |
| Chloroform, $CHCl_3$ | 27-118 | 0.1441 | Wiedemann. | 22-78 | 1.102 | Beyme. |
| "..... | 28-189 | 0.1489 | " | 99.8 | 1.150 | Stevens. |
| Ether, $C_4H_{10}O$ | 69-224 | 0.4797 | Regnault. | 42-45 | 1.020 | Müller. |
| "..... | 25-111 | 0.4280 | Wiedemann. | 12-20 | 1.024 | Low, 1804. |
| Helium..... | — | — | — | 0 | 1.64 | Mean, Jeans |
| Hydrochloric acid, HCl | 13-100 | 0.1940 | Strecker. | 20 | 1.380 | Strecker. |
| "..... | 22-214 | 0.1867 | Regnault. | 100 | 1.400 | " |
| Hydrogen..... | -28-+9 | 3.3996 | " | 4-16 | 1.4080 | Lummer and Pringsheim. |
| "..... | 12-198 | 3.4090 | " | | | |
| "..... | 21-100 | 3.4100 | Wiedemann. | — | 1.410 | Hartmann. |
| " sulphide, H_2S | 20-206 | 0.2451 | Regnault. | — | 1.324 | Capstick. |
| Krypton..... | — | — | — | 19 | 1.666 | Ramsay, '12. |
| Mercury..... | — | — | — | 310 | 1.666 | Kundt and Warburg. |
| Methane, CH_4 | 18-208 | 0.5929 | Regnault. | 11-30 | 1.316 | Müller. |
| Neon..... | — | — | — | 19 | 1.642 | Ramsay, '12 |
| Nitrogen..... | 0-200 | 0.2438 | Regnault. | — | 1.41 | Cazin. |
| "..... | 20-440 | 0.2419 | Holborn and | — | 1.405 | Masson. |
| "..... | 20-630 | 0.2464 | Austin. | | | |
| "..... | 20-800 | 0.2497 | " | | | |
| Nitric oxide, NO | 13-172 | 0.2317 | Regnault. | — | 1.394 | " |
| Nitrogen tetroxide, NO_2 | 27-67 | 1.625 | Berthelot and | — | 1.31 | Natanson. |
| "..... | 27-150 | 1.115 | Olger. | | | |
| "..... | 27-280 | 0.65 | " | | | |
| Nitrous oxide, N_2O | 16-207 | 0.2262 | Regnault. | 0 | 1.311 | Wüllner. |
| "..... | 26-103 | 0.2126 | Wiedemann. | 100 | 1.272 | " |
| "..... | 27-206 | 0.2241 | " | — | 1.324 | Leduc, '98. |
| Oxygen..... | 13-207 | 0.2175 | Regnault. | 5-14 | 1.3077 | Lummer and Pringsheim. |
| "..... | 20-440 | 0.2240 | Holborn and | | | |
| "..... | 20-630 | 0.2300 | Austin. | | | |
| Sulphur dioxide, SO_2 | 16-202 | 0.1544 | Regnault. | 16-34 | 1.256 | Müller. |
| Water vapor, H_2O | 0 | 0.4655 | Thiesen. | 78 | 1.274 | Beyme. |
| "..... | 100 | 0.421 | " | 04 | 1.33 | Jaeger. |
| "..... | 180 | 0.51 | " | 100 | 1.305 | Makower. |
| Xenon..... | — | — | — | 19 | 1.666 | Ramsay, '12. |

LATENT HEAT OF FUSION

The values indicated by * were chosen by Dr. W. P. White of the Carnegie Geophysical Laboratory.

| Element | Temp. °C | Cal./g | Ref. | Element | Temp. °C | Cal./g | Ref. |
|---------|-------------|--------|------|---------|-------------|--------|------|
| Al | 657 | 93 | * | Li | ... | 33 | (6) |
| Sb | 630 | 39 | † | Mg | 650 | 72 | * |
| A | -190 | 6.64 | (1) | Hg | -387 | 2.78 | * |
| Bi | 269 | 12.8 | * | Ni | 1450 | 73 | (7) |
| Br | -7 | 16 | (2) | N | -210 | 6.1 | † |
| Cd | 321 | 12.8 | † | O | -219 | 3.33 | † |
| Cs | 285 | 3.8 | (3) | K | 58 | 14.6 | † |
| Ca | 809 | 78 | (4) | Rb | 39 | 6.1 | † |
| Cr | 1600 | 70 | (5) | Se | 217 | 13 | (8) |
| Co | 1489 | 64 | † | Ag | 960 | 25.9 | * |
| Cu | 1083 | 49.3 | * | Na | 98 | 27 | † |
| Au | 1063 | 15.9 | * | S, mc. | 115 | 9.3 | † |
| H | -249 | 14 | † | Sn | 232 | 14.4 | * |
| Fe | 1528 | 49.3 | * | Zn | 420 | 26.6 | * |
| Pb | 327 | 6 | * | | | | |

* Via Dr. W. P. White. † Mean of several. (1) Eucken-Ilauck, 1928. (2) Regnault. (3) Rengade, 1913. (4) Zalesinski, Zulinski, 1928. (5) Umino, 1926. (6) Thun. (7) White, 1921. (8) Monval.

| Compound | Cal./g | Ref. | Compound | Cal./g | Ref. |
|-------------------|--------|-------------|--------------|--------|--------------|
| BaCl ₂ | 28 | Plato, 1906 | Anorthite | 104 | Bowen, 1922 |
| CaCl ₂ | 54 | " " | Albite | 48.5 | " " |
| KCl | 86 | " " | Diopside | 100 | White |
| NaCl | 124 | " " | Quartz | 50 | Sosman |
| SrCl ₂ | 26 | " " | Cristobalite | 305 | Kracek, 1930 |

| Substance | Composition | T | Cal./g | Authority |
|--|--|-------|-------------------|--|
| Alloys: 30.5Pb + 69.5Sn | PbSn ₄ | 183 | 17 | Spring |
| 36.9Pb + 63.1Sn | PbSn ₃ | 179 | 15.5 | " |
| 63.7Pb + 36.3Sn | PbSn | 177.5 | 11.6 | " |
| 77.8Pb + 22.2Sn | Pb ₂ Sn | 176.5 | 9.54 | " |
| Britannia metal, 9Sn + 1Pb | | 236 | 28.0 ¹ | Ledebur |
| Rose's alloy, | | | | |
| 24Pb + 27.3Sn + 48.7Bi | | 98.8 | 6.85 | Mazzotto |
| Wood's alloy { 25.8Pb + 14.7Sn } { + 52.4Bi + 7Cd } | | 75.5 | 8.40 | " |
| Ammonia | NH ₃ | -75 | 108 | Massol |
| Benzole | C ₆ H ₆ | 5.4 | 30.6 | Mean |
| Ice | H ₂ O | 0 | 79.63 | Dickinson, Harper, Osborne ² |
| " | " | 0 | 79.59 | Smith ³ |
| " (from sea water) | { H ₂ O + 3.535 } of solids | -8.7 | 54.0 | Pettersson |
| Naphthalene | C ₁₀ H ₈ | 79.87 | 35.62 | Pickering |
| Potassium nitrate | KNO ₃ | 333.5 | 48.9 | Person |
| Phenol | C ₆ H ₅ O | 25.37 | 24.93 | Pettersson |
| Paraffin | | 52.40 | 35.10 | Batelli |
| Sodium | Na | 97 | 31.7 | Joannis |
| " nitrate | NaNO ₃ | 305.8 | 64.87 | " |
| " phosphate | { Na ₂ HPO ₄ } { 12H ₂ O } | 36.1 | 66.8 | " |
| Spermaceti | | 43.9 | 36.98 | Batelli |
| Wax (bees) | | 61.8 | 42.3 | Mean |

¹ Total heat from 0°C.

² Bureau of Standards, 1913, in terms of 15° calorie.

³ 1903, based on electrical measurements, assuming mechanical equivalent = 4.187, and in terms of the value of the international volt in use after 1911.

TABLE 284.—Latent Heat of Vaporization of Elements

| Element | $t^{\circ}\text{C}$ | Cal./g | Ref. | Element | $t^{\circ}\text{C}$ | Cal./g | Ref. |
|----------------|---------------------|--------|------|----------------|---------------------|--------|------|
| Sb | 755 | 320 | 1 | I | 174 | 24 | 7 |
| A | 1 atm. | 37.6 | 2 | Kr | -151 | 28 | 8 |
| Ba, 1 | 1537 | 308 | 3 | Pb | 1170 | 175 | 1 |
| Bi | 920 | 190 | 1 | Li | 1336 | 511 | 3 |
| Br | 60± | 43 | † | Mg | 1110 | 136 | † |
| Cd | 778 | 240 | 4 | Hg | 358 | 71 | † |
| Ca | 143.9 | 101 | 3 | N | -195.6 | 476 | 9 |
| Cl | -63 | 63 | † | O ₂ | -182.9 | 50.9 | 9 |
| Fl | -188.2 | 40.5 | 5 | Sr | 1336 | 410 | 11 |
| He | -271.3 | 5.6 | 6 | X | -108.6 | 25.1 | 3 |
| H ₂ | -253 | 108 | † | Zn | 918 | 475 | 4 |

† Mean; (1) Tait, 1914. (2) Eucken, 1916. (3) Hartmann, Schneider, 1929. (4) Egerton, 1917. (5) Cady Hildebrand, 1930. (6) Dana, Onnes, 1925. (7) Favre, Silbermann (old). (8) Peters, Weil, 1930. (9) Alt, 1906. (10) Peters, Weil, 1930.

TABLE 285.—Latent Heat of Vaporization of Liquids

| Substance | Formula | $t^{\circ}\text{C}$ | Latent heat vaporization cal./g | Total heat from 0°C cal./g | Authority |
|-----------------------|-----------------------------------|---------------------|---------------------------------|--|-----------------------|
| Alcohol: Ethyl | $\text{C}_2\text{H}_5\text{O}$ | 78.1 | 205 | 255 | Wirtz |
| " | " | 0 | 236 | 236 | Regnault |
| " | " | 100 | ... | 267 | " |
| " | " | 150 | ... | 285 | " |
| Methyl | CH_4O | 64.5 | 267 | 307 | Wirtz |
| " | " | 0 | 289 | ... | Ramsay and Young |
| " | " | 100 | 246 | ... | " " " |
| " | " | 150 | 206 | ... | " " " |
| " | " | 200 | 152 | ... | " " " |
| " | " | 238.5 | 44.2 | ... | " " " |
| Aniline | $\text{C}_6\text{H}_7\text{N}$ | 184 | 110 | ... | Mean |
| Benzene | C_6H_6 | 80.1 | 92.9 | 127.9 | Wirtz |
| Carbon dioxide, solid | CO_2 | ... | ... | 138.7 | Favre |
| " " liquid | " | -25 | 72.23 | ... | Cailletet and Mathias |
| " " " | " | 0 | 57.48 | ... | " " " |
| " " " | " | 12.35 | 44.97 | ... | Mathias |
| " " " | " | 22.04 | 31.8 | ... | " |
| " " " | " | 30.82 | 3.72 | ... | " |
| " disulphide | CS_2 | 46.1 | 83.8 | 94.8 | Wirtz |
| " " " | " | 0 | 90 | 90 | Regnault |
| " " " | " | 100 | ... | 100.5 | " |
| Chloroform | CHCl_3 | 60.9 | 58.5 | 72.8 | Wirtz |
| Ether | $\text{C}_4\text{H}_{10}\text{O}$ | 34.5 | 88.4 | 107 | " |
| " | " | 0 | 94 | 94 | Regnault |
| " | " | 50 | ... | 115.1 | " |
| " | " | 120 | ... | 140 | " |
| Ethyl bromide | $\text{C}_2\text{H}_5\text{Br}$ | 38.2 | 60.4 | ... | Wirtz |
| " chloride | $\text{C}_2\text{H}_5\text{Cl}$ | 12.5 | ... | 98 | Regnault |
| " iodide | $\text{C}_2\text{H}_5\text{I}$ | 71 | 47 | ... | Mean |
| Heptane | C_7H_{16} | 90 | 77.8 | ... | Young |
| Hexane | C_6H_{14} | 70 | 79.2 | ... | " |
| Octane | C_8H_{18} | 130 | 70.0 | ... | " |
| Pentane | C_5H_{12} | 30 | 85.8 | ... | " |
| Sulphur dioxide | SO_2 | 0 | 91.2 | ... | Cailletet and Mathias |
| " " " | " | 65 | 68.4 | ... | " " " |
| Toluol | C_7H_8 | 111 | 86.0 | ... | Mean |
| Turpentine | $\text{C}_{10}\text{H}_{10}$ | 159.3 | 74.04 | ... | Brix |

TABLE 286.—Latent and Total Heat of Vaporization, Formulae

r = latent heat of vaporization at $t^\circ\text{C}$; H = total heat from fluid at 0° to vapor at $t^\circ\text{C}$. T° refers to Kelvin scale. Same units as preceding table.

| | | | | |
|--|---|---|-------------------|-------------|
| Acetone, $\text{C}_3\text{H}_6\text{O}$ | $H = 140.5 + 0.3664t - 0.000516t^2$ $r = 139.9 + 0.23350t + 0.00055358t^2$ $r = 139.9 - 0.27287t + 0.0001571t^2$ | -3° to 147° —3 —3 —3 | 147 147 147 | R W W |
| Benzene C_6H_6 | $H = 100.0 + 0.24429t - 0.0001315t^2$ | 7 215 | | R |
| Carbon dioxide..... | $r^2 = 118.485(31 - t) - 0.4707(31 - t)^2$ | —25 | 31 | C |
| Carbon bisulphide, CS_2 | $H = 90.0 + 0.14601t - 0.0004123t^2$ $H = 89.5 + 0.10993t - 0.0010161t^2 + 0.03342t^3$ $r = 89.5 - 0.06530t - 0.0010976t^2 + 0.03342t^3$ | —6 —6 —6 | 143 143 143 | R W W |
| Carbon tetrachloride, CCl_4 | $H = 52.0 + 0.14625t - 0.000172t^2$ $H = 51.9 + 0.17867t - 0.0009599t^2 + 0.033733t^3$ $r = 51.9 - 0.01931t - 0.0010505t^2 + 0.033733t^3$ | 8 8 8 | 163 163 163 | R W W |
| Chloroform, CHCl_3 | $H = 67.0 + 0.1375t$ $H = 67.0 + 0.14716t - 0.0000937t^2$ $r = 67.0 - 0.08519t - 0.0001444t^2$ | —5 —5 —5 | 159 159 159 | R W W |
| Ether, $\text{C}_4\text{H}_{10}\text{O}$ | $H = 04.0 + 0.45000t - 0.000556t^2$ $r = 04.0 - 0.07900t - 0.0008514t^2$ | —4 —4 | 121 121 | R R |
| Molybdenum..... | $r = 177000 - 2.5T(\text{cal g-atom})$ | — | — | L |
| Nitrogen, N_2 | $r = 68.85 - 0.2736T$ | — | — | A |
| Nitrous oxide, N_2O | $r^2 = 131.75(36.4 - t) - 0.928(36.4 - t)^2$ | —20 | 36 | C |
| Oxygen, O_2 | $r = 69.67 - 0.2680T$ | — | — | A |
| Platinum..... | $r = 128000 - 2.5T(\text{cal g-atom})$ | — | — | L |
| Sulphur dioxide..... | $r = 61.87 - 0.3842t - 0.000340t^2$ | 0 | 20 | M |
| Tungsten..... | $r = 217800 - 1.8T(\text{cal g-atom})$ | — | — | L |
| Water, H_2O | $H = 638.9 + 0.3745(t - 100) - 0.00099(t - 100)^2$ $r = 94.210(365 - t)^{0.31249}$ (See Table 290) | — 0 | — 100 | D H |

R, Regnault; W, Winkelmann; C, Cailliet and Mathias; A, Alt; D, Davis; H, Henning; L, Langmuir.

TABLE 287.—Latent Heat of Vaporization of Ammonia

CALORIES PER GRAM

| $^\circ\text{C}$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| —40 | 331.7 | 332.3 | 333.0 | 333.6 | 334.3 | 334.9 | 335.5 | 336.2 | 336.8 | 337.5 |
| —30 | 324.8 | 325.5 | 326.2 | 326.9 | 327.6 | 328.3 | 329.0 | 329.7 | 330.3 | 331.0 |
| —20 | 317.6 | 318.3 | 319.1 | 319.8 | 320.6 | 321.3 | 322.0 | 322.7 | 323.4 | 324.1 |
| —10 | 309.9 | 310.7 | 311.5 | 312.2 | 313.0 | 313.8 | 314.6 | 315.3 | 316.1 | 316.8 |
| —0 | 301.8 | 302.6 | 303.4 | 304.3 | 305.1 | 305.9 | 306.7 | 307.5 | 308.3 | 309.1 |
| +0 | 301.8 | 300.9 | 300.1 | 299.2 | 298.4 | 297.5 | 296.6 | 295.7 | 294.9 | 294.0 |
| +10 | 293.1 | 292.2 | 291.3 | 290.4 | 289.5 | 288.6 | 287.6 | 286.7 | 285.7 | 284.8 |
| +20 | 283.8 | 282.8 | 281.8 | 280.9 | 279.9 | 278.9 | 277.9 | 276.9 | 275.9 | 274.9 |
| +30 | 273.9 | 272.8 | 271.8 | 270.7 | 269.7 | 268.6 | 267.5 | 266.4 | 265.3 | 264.2 |
| +40 | 263.1 | 262.0 | 260.8 | 259.7 | 258.5 | 257.4 | 256.2 | 255.0 | 253.8 | 252.6 |

Osborne and van Dusen, Bul. Bureau Standards, 14, p. 439, 1918.

TABLE 288.—“Latent Heat of Pressure Variation” of Liquid Ammonia

When a fluid undergoes a change of pressure, there occurs a transformation of energy into heat or vice versa, which results in a change of temperature of the substance unless a like amount of heat is abstracted or added. This change expressed as the heat so transformed per unit change of pressure is the “latent heat of pressure variation.” It is expressed below as Joules per gram per kg cm². Osborne and van Dusen, *loc. cit.*, p. 433, 1918.

| | | | | | | | | |
|------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| Temperature $^\circ\text{C}$ | —44.1 | —39.0 | —24.2 | —0.2 | +16.5 | +26.5 | +35.4 | +40.3 |
| Latent heat.... | —0.055 | —0.057 | —0.068 | —0.088 | —0.107 | —0.123 | —0.140 | —0.150 |

THERMAL PROPERTIES OF SATURATED WATER AND STEAM

(Osborne, Stimson, Fiock, Bur. Standards Journ. Res., 5, 411, 1930.)

Accuracy: It is estimated that there is only one chance in 100 that the values given for H differ from the truth by as much as one part in 2000; it is equally unlikely that the values for L and H' are as much as 1.5 joules/g from the truth in the range of the experiments, 100°-270°C.

| Temperature, °C | Heat con- tent of liquid, H | Latent heat, L | Heat con- tent of vapor, H' | Entropy— | |
|-----------------|-------------------------------------|---------------------|-------------------------------------|---|--|
| | Int. joules/g | Int. joules/g | Int. joules/g | of liquid Φ Int. joules/g°C | of vapor Φ Int. joules/g°C |
| 0 | 0 | 2494.02 | 2494.02 | 0 | 9.132 |
| 10 | 42.02 | 2472.26 | 2514.28 | .1511 | 8.884 |
| 20 | 83.83 | 2450.17 | 2534.00 | .2962 | 8.656 |
| 30 | 125.59 | 2427.73 | 2553.32 | .4363 | 8.446 |
| 40 | 167.34 | 2404.90 | 2572.24 | .5719 | 8.253 |
| 50 | 209.11 | 2381.64 | 2590.75 | .7032 | 8.074 |
| 60 | 250.90 | 2357.91 | 2608.81 | .8305 | 7.909 |
| 70 | 292.75 | 2333.65 | 2626.40 | .9543 | 7.756 |
| 80 | 334.66 | 2308.32 | 2643.48 | 1.0746 | 7.613 |
| 90 | 376.65 | 2283.38 | 2660.03 | 1.1918 | 7.480 |
| 100 | 418.75 | 2257.24 | 2675.99 | 1.3064 | 7.356 |
| 110 | 460.97 | 2230.35 | 2691.32 | 1.4177 | 7.240 |
| 120 | 503.36 | 2202.65 | 2706.01 | 1.5268 | 7.130 |
| 130 | 545.93 | 2174.04 | 2719.97 | 1.6335 | 7.027 |
| 140 | 588.71 | 2144.44 | 2733.15 | 1.7381 | 6.929 |
| 150 | 631.75 | 2113.76 | 2745.51 | 1.8407 | 6.837 |
| 160 | 675.06 | 2081.89 | 2756.95 | 1.9416 | 6.749 |
| 170 | 718.66 | 2048.72 | 2767.38 | 2.0406 | 6.664 |
| 180 | 762.72 | 2014.10 | 2776.82 | 2.1384 | 6.584 |
| 190 | 807.15 | 1977.89 | 2785.04 | 2.2348 | 6.506 |
| 200 | 852.02 | 1939.93 | 2791.95 | 2.3299 | 6.430 |
| 210 | 897.35 | 1900.00 | 2797.35 | 2.4239 | 6.357 |
| 220 | 943.24 | 1857.89 | 2801.13 | 2.5169 | 6.285 |
| 230 | 989.75 | 1813.33 | 2803.08 | 2.6091 | 6.213 |
| 240 | 1036.97 | 1766.02 | 2802.99 | 2.7007 | 6.143 |
| 250 | 1084.97 | 1715.59 | 2800.56 | 2.7919 | 6.072 |
| 260 | 1133.87 | 1661.60 | 2795.47 | 2.8828 | 6.000 |
| 270 | 1184.32 | 1603.51 | 2787.83 | 2.9746 | 5.927 |

PROPERTIES OF SATURATED STEAM

Metric and Common Units 0° to 220° C

Reprinted by permission of the author and publishers from "Tables of the Properties of Steam," Cecil H. Peabody, 8th edition, rewritten in 1909. Calorie used is heat required to raise 1 Kg. water from 15° to 16° C. B. T. U. is heat required to raise 1 pd. water from 62° to 63° F. Mechanical Equiv. of heat used, 778 ft. pds. or 427 m. Kg. Specific heats, see Barnes-Regnault-Peabody results, p. 227. Heat of Liquid, q, heat required to raise 1 Kg. (1 lb.) to corresponding temperature from 0° C. Heat of vaporization, r, heat required to vaporize 1 Kg. (1 lb.) at corresponding temperature to dry saturated vapor against corresponding pressure; see Henning, Ann. der Phys., 21, p. 849, 1906. Total Heat, H = r + q, see Davis, Tr. Am. Soc. Mech. Eng., 1908.

| Temperature Degrees Centigrade. t. | Pressure. | | | Heat of the Liquid. | | Heat of Vaporization. | | Heat Equivalent of Internal Work. | | Temperature Degrees Fahrenheit t. |
|---|-------------------------|------------------------|---------------------------|------------------------|----------------|--------------------------|----------------|---|----------------|--|
| | Mm of Mercury. p. | Kg per sq. cm p. | Pds. per sq. in. p. | Calories. q. | B. T. U. q. | Calories. r. | B. T. U. r. | Calories. p. | B. T. U. p. | |
| | | | | | | | | | | |
| 0 | 4.579 | 0.00623 | 0.0886 | 0.00 | 0.0 | 595.4 | 1071.7 | 565.3 | 1017.5 | 32.0 |
| 5 | 6.541 | .00889 | .1265 | 5.04 | 9.1 | 592.8 | 1067.1 | 562.2 | 1011.9 | 41.0 |
| 10 | 9.205 | .01252 | .1780 | 10.06 | 18.1 | 590.2 | 1062.3 | 559.0 | 1006.2 | 50.0 |
| 15 | 12.779 | .01737 | .2471 | 15.06 | 27.1 | 587.6 | 1057.6 | 555.9 | 1000.5 | 59.0 |
| 20 | 17.51 | .02381 | .3386 | 20.06 | 36.1 | 584.9 | 1052.8 | 552.7 | 994.8 | 68.0 |
| 25 | 23.69 | .03221 | .4581 | 25.05 | 45.1 | 582.3 | 1048.1 | 549.5 | 989.1 | 77.0 |
| 30 | 31.71 | .04311 | .6132 | 30.04 | 54.1 | 579.6 | 1043.3 | 546.3 | 983.4 | 86.0 |
| 35 | 42.02 | .05713 | .8126 | 35.03 | 63.1 | 576.9 | 1038.5 | 543.1 | 977.6 | 95.0 |
| 40 | 55.13 | .07495 | 1.0661 | 40.02 | 72.0 | 574.2 | 1033.5 | 539.9 | 971.7 | 104.0 |
| 45 | 71.66 | .09743 | 1.3858 | 45.00 | 81.0 | 571.3 | 1028.4 | 536.5 | 965.7 | 113.0 |
| 50 | 92.30 | .12549 | 1.7849 | 49.99 | 90.0 | 568.4 | 1023.2 | 533.0 | 959.6 | 122.0 |
| 55 | 117.85 | .16023 | 2.279 | 54.98 | 99.0 | 565.6 | 1018.1 | 529.7 | 953.5 | 131.0 |
| 60 | 149.10 | .20284 | 2.885 | 59.97 | 108.0 | 562.8 | 1013.1 | 526.4 | 947.5 | 140.0 |
| 65 | 187.36 | .2547 | 3.623 | 64.98 | 117.0 | 559.9 | 1007.8 | 523.0 | 941.3 | 149.0 |
| 70 | 233.53 | .3175 | 4.516 | 69.98 | 126.0 | 556.9 | 1002.5 | 519.5 | 935.0 | 158.0 |
| 75 | 289.0 | .3929 | 5.589 | 74.99 | 135.0 | 554.0 | 997.3 | 516.0 | 928.8 | 167.0 |
| 80 | 355.1 | .4828 | 6.867 | 80.01 | 144.0 | 551.1 | 991.9 | 512.6 | 922.6 | 176.0 |
| 85 | 433.5 | .5894 | 8.383 | 85.04 | 153.1 | 548.1 | 986.5 | 509.1 | 916.3 | 185.0 |
| 90 | 525.8 | .7149 | 10.167 | 90.07 | 162.1 | 544.9 | 980.9 | 505.4 | 909.9 | 194.0 |
| 91 | 546.1 | .7425 | 10.560 | 91.08 | 163.9 | 544.3 | 979.8 | 504.7 | 908.5 | 195.8 |
| 92 | 567.1 | .7710 | 10.966 | 92.08 | 165.7 | 543.7 | 978.7 | 504.0 | 907.2 | 197.6 |
| 93 | 588.7 | .8004 | 11.384 | 93.09 | 167.5 | 543.1 | 977.6 | 503.3 | 906.0 | 199.4 |
| 94 | 611.0 | .8307 | 11.815 | 94.10 | 169.3 | 542.5 | 976.5 | 502.6 | 904.7 | 201.2 |
| 95 | 634.0 | .8620 | 12.260 | 95.11 | 171.2 | 541.9 | 975.4 | 501.9 | 903.4 | 203.0 |
| 96 | 657.7 | .8942 | 12.718 | 96.12 | 173.0 | 541.2 | 974.2 | 501.1 | 902.1 | 204.8 |
| 97 | 682.1 | .9274 | 13.190 | 97.12 | 174.8 | 540.6 | 973.1 | 500.4 | 900.8 | 206.6 |
| 98 | 707.3 | .9616 | 13.678 | 98.13 | 176.6 | 539.9 | 971.9 | 499.6 | 899.4 | 208.4 |
| 99 | 733.3 | .9970 | 14.180 | 99.14 | 178.5 | 539.3 | 970.8 | 498.9 | 898.2 | 210.2 |
| 100 | 760.0 | 1.0333 | 14.697 | 100.2 | 180.3 | 538.7 | 969.7 | 498.2 | 896.9 | 212.0 |
| 101 | 787.5 | 1.0707 | 15.229 | 101.2 | 182.1 | 538.1 | 968.5 | 497.5 | 895.5 | 213.8 |
| 102 | 815.9 | 1.1093 | 15.778 | 102.2 | 183.9 | 537.4 | 967.3 | 496.8 | 894.1 | 215.6 |
| 103 | 845.1 | 1.1490 | 16.342 | 103.2 | 185.7 | 536.8 | 966.2 | 496.1 | 892.9 | 217.4 |
| 104 | 875.1 | 1.1898 | 16.923 | 104.2 | 187.6 | 536.2 | 965.1 | 495.4 | 891.6 | 219.2 |
| 105 | 906.1 | 1.2319 | 17.522 | 105.2 | 189.4 | 535.6 | 964.0 | 494.7 | 890.3 | 221.0 |
| 106 | 937.9 | 1.2752 | 18.137 | 106.2 | 191.2 | 534.9 | 962.8 | 493.9 | 889.0 | 222.8 |
| 107 | 970.6 | 1.3196 | 18.769 | 107.2 | 193.0 | 534.2 | 961.6 | 493.1 | 887.6 | 224.6 |
| 108 | 1004.3 | 1.3653 | 19.420 | 108.2 | 194.8 | 533.6 | 960.5 | 492.4 | 886.3 | 226.4 |
| 109 | 1038.8 | 1.4123 | 20.089 | 109.3 | 196.7 | 532.9 | 959.3 | 491.6 | 885.0 | 228.2 |
| 110 | 1074.5 | 1.4608 | 20.777 | 110.3 | 198.5 | 532.3 | 958.1 | 490.9 | 883.6 | 230.0 |
| 111 | 1111.1 | 1.5106 | 21.486 | 111.3 | 200.3 | 531.6 | 956.9 | 490.2 | 882.3 | 231.8 |
| 112 | 1148.7 | 1.5617 | 22.214 | 112.3 | 202.1 | 530.9 | 955.7 | 489.4 | 880.9 | 233.6 |
| 113 | 1187.4 | 1.6144 | 22.962 | 113.3 | 203.9 | 530.3 | 954.5 | 488.7 | 879.5 | 235.4 |
| 114 | 1227.1 | 1.6684 | 23.729 | 114.3 | 205.8 | 529.6 | 953.3 | 487.9 | 878.2 | 237.2 |
| 115 | 1267.9 | 1.7238 | 24.518 | 115.3 | 207.6 | 528.9 | 952.1 | 487.1 | 876.8 | 239.0 |
| 116 | 1309.8 | 1.7808 | 25.328 | 116.4 | 209.4 | 528.2 | 950.8 | 486.3 | 875.4 | 240.8 |
| 117 | 1352.8 | 1.8393 | 26.160 | 117.4 | 211.2 | 527.5 | 949.5 | 485.5 | 873.9 | 242.6 |
| 118 | 1397.0 | 1.8993 | 27.015 | 118.4 | 213.0 | 526.9 | 948.4 | 484.8 | 872.6 | 244.4 |
| 119 | 1442.4 | 1.9611 | 27.893 | 119.4 | 214.9 | 526.2 | 947.2 | 484.0 | 871.3 | 246.2 |

PROPERTIES OF SATURATED STEAM

Metric and Common Units 0° to 220° C

If a is the reciprocal of the Mechanical Equivalent of Heat, p the pressure, s and σ the specific volumes of the liquid and the saturated vapor, $s - \sigma$, the change of volume, then the heat equivalent of the external work is $Apu = Ap(s - \sigma)$. Heat equivalent of internal work, $p = r - Apu$. For experimental sp. vols. see Knoblauch, Linde and Klebe, Mitt. über Forschungsarbeiten, 21, p. 33, 1905. Entropy $\equiv S dQ/T$, where dQ = amount of heat added at absolute temperature T . For pressures of saturated steam see Holborn and Henning, Ann. der Phys. 26, p. 833, 1908; for temperatures above 205° C corrected from Regnault.

| Temperature Degrees Centigrade. t. | Heat Equivalent of External Work. | | Entropy of the Liquid. θ | Entropy of Evap- oration. $\frac{r}{T}$ | Specific Volume. | | Density. | | Temperature Degrees Fahrenheit. t. |
|---|---|--------|--|--|--|--------------------------------------|---|---|---|
| | Calories. | B.T.U. | | | Cubic Meters per Kilo- gram s | Cubic Feet per Pound. s | Kilograms per Cubic Meter. $\frac{1}{s}$ | Pounds per Cubic Foot. $\frac{1}{s}$ | |
| | Apu. | Apu. | | | | | | | |
| 0 | 30.1 | 54.2 | 0.0000 | 2.1804 | 206.3 | 3304. | 0.00485 | 0.000303 | 32.0 |
| 5 | 30.6 | 55.2 | .0183 | 2.1320 | 147.1 | 2356. | .00680 | .000424 | 41.0 |
| 10 | 31.2 | 56.1 | .0361 | 2.0850 | 106.3 | 1703. | .00941 | .000587 | 50.0 |
| 15 | 31.7 | 57.1 | .0537 | 2.0396 | 77.9 | 1248. | .01283 | .000801 | 59.0 |
| 20 | 32.2 | 58.0 | .0709 | 1.9959 | 57.8 | 926. | .01730 | .001080 | 68.0 |
| 25 | 32.8 | 59.0 | .0878 | 1.9536 | 43.40 | 695. | .02304 | .001439 | 77.0 |
| 30 | 33.3 | 59.9 | .1044 | 1.9126 | 32.95 | 528. | .03035 | .001894 | 86.0 |
| 35 | 33.8 | 60.9 | .1207 | 1.8728 | 25.25 | 404.7 | .03960 | .002471 | 95.0 |
| 40 | 34.3 | 61.8 | .1368 | 1.8341 | 19.57 | 313.5 | .0511 | .003190 | 104.0 |
| 45 | 34.8 | 62.7 | .1526 | 1.7963 | 15.25 | 244.4 | .0656 | .004092 | 113.0 |
| 50 | 35.4 | 63.6 | .1682 | 1.7597 | 12.02 | 192.6 | .0832 | .00519 | 122.0 |
| 55 | 35.9 | 64.6 | .1835 | 1.7242 | 9.56 | 153.2 | .1046 | .00653 | 131.0 |
| 60 | 36.4 | 65.6 | .1986 | 1.6899 | 7.66 | 122.8 | .1305 | .00814 | 140.0 |
| 65 | 36.9 | 66.5 | .2135 | 1.6563 | 6.19 | 99.2 | .1615 | .01008 | 149.0 |
| 70 | 37.4 | 67.4 | .2282 | 1.6235 | 5.04 | 80.7 | .1984 | .01239 | 158.0 |
| 75 | 38.0 | 68.5 | .2427 | 1.5918 | 4.130 | 66.2 | .2421 | .01510 | 167.0 |
| 80 | 38.5 | 69.3 | .2570 | 1.5609 | 3.404 | 54.5 | .2938 | .01835 | 176.0 |
| 85 | 39.0 | 70.2 | .2711 | 1.5307 | 2.824 | 45.23 | .3541 | .02211 | 185.0 |
| 90 | 39.5 | 71.0 | .2851 | 1.5010 | 2.358 | 37.77 | .4241 | .02648 | 194.0 |
| 91 | 39.6 | 71.3 | .2879 | 1.4952 | 2.275 | 36.45 | .4395 | .02743 | 195.8 |
| 92 | 39.7 | 71.5 | .2906 | 1.4894 | 2.197 | 35.19 | .4552 | .02842 | 197.6 |
| 93 | 39.8 | 71.6 | .2934 | 1.4836 | 2.122 | 34.00 | .4713 | .02941 | 199.4 |
| 94 | 39.9 | 71.8 | .2961 | 1.4779 | 2.050 | 32.86 | .4878 | .03043 | 201.2 |
| 95 | 40.0 | 72.0 | .2989 | 1.4723 | 1.980 | 31.75 | .505 | .03149 | 203.0 |
| 96 | 40.1 | 72.1 | .3016 | 1.4666 | 1.913 | 30.67 | .523 | .03260 | 204.8 |
| 97 | 40.2 | 72.3 | .3043 | 1.4609 | 1.849 | 29.63 | .541 | .03375 | 206.6 |
| 98 | 40.3 | 72.5 | .3070 | 1.4552 | 1.787 | 28.64 | .560 | .03492 | 208.4 |
| 99 | 40.4 | 72.6 | .3097 | 1.4496 | 1.728 | 27.69 | .579 | .03611 | 210.2 |
| 100 | 40.5 | 72.8 | .3125 | 1.4441 | 1.671 | 26.78 | .598 | .03734 | 212.0 |
| 101 | 40.6 | 73.0 | .3152 | 1.4386 | 1.617 | 25.90 | .618 | .03861 | 213.8 |
| 102 | 40.6 | 73.2 | .3179 | 1.4330 | 1.564 | 25.06 | .639 | .03990 | 215.6 |
| 103 | 40.7 | 73.3 | .3205 | 1.4275 | 1.514 | 24.25 | .661 | .04124 | 217.4 |
| 104 | 40.8 | 73.5 | .3232 | 1.4220 | 1.465 | 23.47 | .683 | .04261 | 219.2 |
| 105 | 40.9 | 73.7 | .3259 | 1.4165 | 1.419 | 22.73 | .705 | .04400 | 221.0 |
| 106 | 41.0 | 73.8 | .3286 | 1.4111 | 1.374 | 22.01 | .728 | .04543 | 222.8 |
| 107 | 41.1 | 74.0 | .3312 | 1.4057 | 1.331 | 21.31 | .751 | .04692 | 224.6 |
| 108 | 41.2 | 74.2 | .3339 | 1.4003 | 1.289 | 20.64 | .776 | .04845 | 226.4 |
| 109 | 41.3 | 74.3 | .3365 | 1.3949 | 1.248 | 19.99 | .801 | .05000 | 228.2 |
| 110 | 41.4 | 74.5 | .3392 | 1.3895 | 1.209 | 19.37 | .827 | .0516 | 230.0 |
| 111 | 41.4 | 74.6 | .3418 | 1.3842 | 1.172 | 18.77 | .853 | .0533 | 231.8 |
| 112 | 41.5 | 74.8 | .3445 | 1.3789 | 1.136 | 18.20 | .880 | .0550 | 233.6 |
| 113 | 41.6 | 75.0 | .3471 | 1.3736 | 1.101 | 17.64 | .908 | .0567 | 235.4 |
| 114 | 41.7 | 75.1 | .3498 | 1.3683 | 1.068 | 17.10 | .936 | .0585 | 237.2 |
| 115 | 41.8 | 75.3 | .3524 | 1.3631 | 1.036 | 16.59 | .965 | .0603 | 239.0 |
| 116 | 41.9 | 75.4 | .3550 | 1.3579 | 1.005 | 16.09 | .995 | .0622 | 240.8 |
| 117 | 42.0 | 75.6 | .3576 | 1.3527 | 0.9746 | 15.61 | 1.026 | .0641 | 242.6 |
| 118 | 42.1 | 75.8 | .3602 | 1.3475 | 0.9460 | 15.16 | 1.057 | .0659 | 244.4 |
| 119 | 42.2 | 75.9 | .3628 | 1.3423 | 0.9183 | 14.72 | 1.089 | .0679 | 246.2 |

PROPERTIES OF SATURATED STEAM

Metric and Common Units 0° to 220° C

| Temperature Degrees Centigrade. t. | Pressure | | | Heat of the Liquid. | | Heat of Vaporization. | | Heat Equivalent of Internal Work. | | Temperature Degrees Fahrenheit. t. |
|---|--------------------------------|---------------------------------|----------------------------------|------------------------|--------------------|--------------------------|-------------------|--------------------------------------|--------------------|---|
| | Mm. of Mercury p. | Kg. per sq. cm. p. | Pds. per sq. in. p. | Calories. q. | B. T. U. q. | Calories. r. | B. T. U. r | Calories p | B. T. U. p. | |
| | | | | | | | | | | |
| 120 | 1489 | 2.024 | 28.79 | 120.4 | 216.7 | 525.6 | 946.0 | 483.4 | 870.0 | 248.0 |
| 121 | 1537 | 2.089 | 29.72 | 121.4 | 218.5 | 524.9 | 944.8 | 482.6 | 868.6 | 249.8 |
| 122 | 1586 | 2.156 | 30.66 | 122.5 | 220.4 | 524.2 | 943.5 | 481.8 | 867.1 | 251.6 |
| 123 | 1636 | 2.224 | 31.64 | 123.5 | 222.2 | 523.5 | 942.3 | 481.0 | 865.8 | 253.4 |
| 124 | 1688 | 2.294 | 32.64 | 124.5 | 224.1 | 522.8 | 941.0 | 480.2 | 864.3 | 255.2 |
| 125 | 1740 | 2.366 | 33.66 | 125.5 | 225.9 | 522.1 | 939.9 | 479.4 | 863.0 | 257.0 |
| 126 | 1795 | 2.440 | 34.71 | 126.5 | 227.7 | 521.4 | 938.6 | 478.6 | 861.6 | 258.8 |
| 127 | 1850 | 2.516 | 35.78 | 127.5 | 229.5 | 520.7 | 937.3 | 477.8 | 860.2 | 260.6 |
| 128 | 1907 | 2.593 | 36.88 | 128.6 | 231.4 | 520.0 | 936.1 | 477.0 | 858.8 | 262.4 |
| 129 | 1966 | 2.673 | 38.01 | 129.6 | 233.3 | 519.3 | 934.8 | 476.3 | 857.4 | 264.2 |
| 130 | 2026 | 2.754 | 39.17 | 130.6 | 235.1 | 518.6 | 933.6 | 475.5 | 856.0 | 266.0 |
| 131 | 2087 | 2.837 | 40.36 | 131.6 | 236.9 | 517.9 | 932.3 | 474.7 | 854.6 | 267.8 |
| 132 | 2150 | 2.923 | 41.57 | 132.6 | 238.7 | 517.3 | 931.1 | 474.0 | 853.2 | 269.6 |
| 133 | 2214 | 3.010 | 42.81 | 133.7 | 240.6 | 516.6 | 929.8 | 473.3 | 851.8 | 271.4 |
| 134 | 2280 | 3.100 | 44.09 | 134.7 | 242.4 | 515.9 | 928.5 | 472.5 | 850.4 | 273.2 |
| 135 | 2348 | 3.192 | 45.39 | 135.7 | 244.2 | 515.1 | 927.2 | 471.6 | 848.9 | 275.0 |
| 136 | 2416 | 3.285 | 46.73 | 136.7 | 246.0 | 514.4 | 925.9 | 470.8 | 847.5 | 276.8 |
| 137 | 2487 | 3.382 | 48.10 | 137.7 | 247.9 | 513.7 | 924.6 | 470.1 | 846.1 | 278.6 |
| 138 | 2560 | 3.480 | 49.50 | 138.8 | 249.7 | 513.0 | 923.3 | 469.3 | 844.6 | 280.4 |
| 139 | 2634 | 3.581 | 50.93 | 139.8 | 251.6 | 512.3 | 922.1 | 468.5 | 843.3 | 282.2 |
| 140 | 2710 | 3.684 | 52.39 | 140.8 | 253.4 | 511.5 | 920.7 | 467.6 | 841.8 | 284.0 |
| 141 | 2787 | 3.789 | 53.89 | 141.8 | 255.3 | 510.7 | 919.3 | 466.8 | 840.2 | 285.8 |
| 142 | 2866 | 3.897 | 55.43 | 142.8 | 257.1 | 510.1 | 918.1 | 466.1 | 838.9 | 287.6 |
| 143 | 2948 | 4.008 | 57.00 | 143.9 | 259.0 | 509.3 | 916.7 | 465.3 | 837.4 | 289.4 |
| 144 | 3030 | 4.121 | 58.60 | 144.9 | 260.8 | 508.6 | 915.4 | 464.4 | 835.9 | 291.2 |
| 145 | 3115 | 4.236 | 60.24 | 145.9 | 262.7 | 507.8 | 914.1 | 463.6 | 834.5 | 293.0 |
| 146 | 3202 | 4.354 | 61.92 | 146.9 | 264.5 | 507.1 | 912.8 | 462.8 | 833.1 | 294.8 |
| 147 | 3291 | 4.474 | 63.64 | 148.0 | 266.4 | 506.4 | 911.5 | 462.0 | 831.6 | 296.6 |
| 148 | 3381 | 4.597 | 65.39 | 149.0 | 268.2 | 505.6 | 910.1 | 461.2 | 830.1 | 298.4 |
| 149 | 3474 | 4.723 | 67.18 | 150.0 | 270.1 | 504.9 | 908.8 | 460.4 | 828.7 | 300.2 |
| 150 | 3569 | 4.852 | 69.01 | 151.0 | 271.9 | 504.1 | 907.4 | 459.5 | 827.2 | 302.0 |
| 151 | 3665 | 4.984 | 70.88 | 152.1 | 273.8 | 503.4 | 906.1 | 458.7 | 825.7 | 303.8 |
| 152 | 3764 | 5.118 | 72.79 | 153.1 | 275.6 | 502.6 | 904.7 | 457.9 | 824.2 | 305.6 |
| 153 | 3865 | 5.255 | 74.74 | 154.1 | 277.4 | 501.9 | 903.3 | 457.1 | 822.7 | 307.4 |
| 154 | 3968 | 5.395 | 76.73 | 155.1 | 279.2 | 501.1 | 901.9 | 456.3 | 821.2 | 309.2 |
| 155 | 4073 | 5.538 | 78.76 | 156.2 | 281.1 | 500.3 | 900.5 | 455.4 | 819.6 | 311.0 |
| 156 | 4181 | 5.684 | 80.84 | 157.2 | 283.0 | 499.6 | 899.2 | 454.6 | 818.2 | 312.8 |
| 157 | 4290 | 5.833 | 82.96 | 158.2 | 284.8 | 498.8 | 897.8 | 453.8 | 816.7 | 314.6 |
| 158 | 4402 | 5.985 | 85.12 | 159.3 | 286.7 | 498.1 | 896.5 | 453.0 | 815.3 | 316.4 |
| 159 | 4517 | 6.141 | 87.33 | 160.3 | 288.5 | 497.3 | 895.1 | 452.1 | 813.7 | 318.2 |
| 160 | 4633 | 6.300 | 89.59 | 161.3 | 290.4 | 496.5 | 893.7 | 451.2 | 812.2 | 320.0 |
| 161 | 4752 | 6.462 | 91.89 | 162.3 | 292.2 | 495.7 | 892.3 | 450.4 | 810.7 | 321.8 |
| 162 | 4874 | 6.628 | 94.25 | 163.4 | 294.1 | 494.9 | 890.9 | 449.5 | 809.2 | 323.6 |
| 163 | 4998 | 6.796 | 96.65 | 164.4 | 295.9 | 494.2 | 889.5 | 448.7 | 807.7 | 325.4 |
| 164 | 5124 | 6.967 | 99.09 | 165.4 | 297.7 | 493.4 | 888.1 | 447.9 | 806.2 | 327.2 |
| 165 | 5253 | 7.142 | 101.6 | 166.5 | 299.6 | 492.6 | 886.7 | 447.0 | 804.7 | 329.0 |
| 166 | 5384 | 7.320 | 104.1 | 167.5 | 301.5 | 491.9 | 885.4 | 446.3 | 803.3 | 330.8 |
| 167 | 5518 | 7.502 | 106.5 | 168.5 | 303.3 | 491.1 | 883.9 | 445.4 | 801.7 | 332.6 |
| 168 | 5655 | 7.688 | 109.4 | 169.5 | 305.1 | 490.3 | 882.5 | 444.6 | 800.1 | 334.4 |
| 169 | 5794 | 7.877 | 112.0 | 170.6 | 307.0 | 489.5 | 881.0 | 443.7 | 798.5 | 336.2 |

PROPERTIES OF SATURATED STEAM

Metric and Common Units 0° to 220° C

| Temperature Degrees Centigrade. t. | Heat Equivalent of External Work. | | Entropy of the Liquid. θ | Entropy of Evapo- ration. $\frac{r}{T}$ | Specific Volume. | | Density. | | Temperature Degrees Fahrenheit. t. |
|---|--------------------------------------|----------|--|--|---|--------------------------------------|---|---|---|
| | Calories. | B. T. U. | | | Cubic Meters per Kilogram. s | Cubic Feet per Pound. s | Kilograms per Cubic Meter. $\frac{1}{s}$ | Pounds per Cubic Foot. $\frac{1}{s}$ | |
| | Apu. | Apu. | | | | | | | |
| 120 | 42.2 | 76.0 | .3654 | 1.3372 | .8914 | 14.28 | 1.122 | 0.0700 | 248.0 |
| 121 | 42.3 | 76.2 | .3680 | 1.3321 | .8653 | 13.86 | 1.156 | .0721 | 249.8 |
| 122 | 42.4 | 76.4 | .3705 | 1.3269 | .8401 | 13.46 | 1.190 | .0743 | 251.6 |
| 123 | 42.5 | 76.5 | .3731 | 1.3218 | .8158 | 13.07 | 1.226 | .0765 | 253.4 |
| 124 | 42.6 | 76.7 | .3756 | 1.3167 | .7924 | 12.69 | 1.262 | .0788 | 255.2 |
| 125 | 42.7 | 76.8 | .3782 | 1.3117 | .7698 | 12.33 | 1.299 | .0811 | 257.0 |
| 126 | 42.8 | 77.0 | .3807 | 1.3067 | .7479 | 11.98 | 1.337 | .0835 | 258.8 |
| 127 | 42.9 | 77.1 | .3833 | 1.3017 | .7267 | 11.64 | 1.376 | .0859 | 260.6 |
| 128 | 43.0 | 77.3 | .3858 | 1.2967 | .7063 | 11.32 | 1.416 | .0883 | 262.4 |
| 129 | 43.0 | 77.4 | .3884 | 1.2917 | .6867 | 11.00 | 1.456 | .0909 | 264.2 |
| 130 | 43.1 | 77.6 | .3909 | 1.2868 | .6677 | 10.70 | 1.498 | .0935 | 266.0 |
| 131 | 43.2 | 77.7 | .3934 | 1.2818 | .6493 | 10.40 | 1.540 | .0961 | 267.8 |
| 132 | 43.3 | 77.9 | .3959 | 1.2769 | .6315 | 10.12 | 1.583 | .0988 | 269.6 |
| 133 | 43.3 | 78.0 | .3985 | 1.2720 | .6142 | 9.839 | 1.628 | .1016 | 271.4 |
| 134 | 43.4 | 78.1 | .4010 | 1.2672 | .5974 | 9.569 | 1.674 | .1045 | 273.2 |
| 135 | 43.5 | 78.3 | .4035 | 1.2623 | .5812 | 9.309 | 1.721 | .1074 | 275.0 |
| 136 | 43.6 | 78.4 | .4060 | 1.2574 | .5656 | 9.060 | 1.768 | .1104 | 276.8 |
| 137 | 43.6 | 78.5 | .4085 | 1.2526 | .5506 | 8.820 | 1.816 | .1134 | 278.6 |
| 138 | 43.7 | 78.7 | .4110 | 1.2479 | .5361 | 8.587 | 1.865 | .1165 | 280.4 |
| 139 | 43.8 | 78.8 | .4135 | 1.2431 | .5219 | 8.360 | 1.916 | .1196 | 282.2 |
| 140 | 43.9 | 78.9 | .4160 | 1.2383 | .5081 | 8.140 | 1.968 | .1229 | 284.0 |
| 141 | 43.9 | 79.1 | .4185 | 1.2335 | .4948 | 7.926 | 2.021 | .1262 | 285.8 |
| 142 | 44.0 | 79.2 | .4209 | 1.2288 | .4819 | 7.719 | 2.075 | .1296 | 287.6 |
| 143 | 44.0 | 79.3 | .4234 | 1.2241 | .4694 | 7.519 | 2.130 | .1330 | 289.4 |
| 144 | 44.2 | 79.5 | .4259 | 1.2194 | .4574 | 7.326 | 2.186 | .1365 | 291.2 |
| 145 | 44.2 | 79.6 | .4283 | 1.2147 | .4457 | 7.139 | 2.244 | .1401 | 293.0 |
| 146 | 44.3 | 79.7 | .4307 | 1.2100 | .4343 | 6.957 | 2.303 | .1437 | 294.8 |
| 147 | 44.4 | 79.9 | .4332 | 1.2054 | .4232 | 6.780 | 2.363 | .1475 | 296.6 |
| 148 | 44.4 | 80.0 | .4356 | 1.2008 | .4125 | 6.609 | 2.424 | .1513 | 298.4 |
| 149 | 44.5 | 80.1 | .4380 | 1.1962 | .4022 | 6.443 | 2.486 | .1552 | 300.2 |
| 150 | 44.6 | 80.2 | .4405 | 1.1916 | .3921 | 6.282 | 2.550 | .1592 | 302.0 |
| 151 | 44.6 | 80.4 | .4429 | 1.1870 | .3824 | 6.126 | 2.615 | .1632 | 303.8 |
| 152 | 44.7 | 80.5 | .4453 | 1.1824 | .3729 | 5.974 | 2.682 | .1674 | 305.6 |
| 153 | 44.8 | 80.6 | .4477 | 1.1778 | .3637 | 5.826 | 2.750 | .1716 | 307.4 |
| 154 | 44.8 | 80.7 | .4501 | 1.1733 | .3548 | 5.683 | 2.818 | .1759 | 309.2 |
| 155 | 44.9 | 80.9 | .4525 | 1.1688 | .3463 | 5.546 | 2.888 | .1803 | 311.0 |
| 156 | 45.0 | 81.0 | .4549 | 1.1644 | .3380 | 5.413 | 2.959 | .1847 | 312.8 |
| 157 | 45.0 | 81.1 | .4573 | 1.1599 | .3298 | 5.282 | 3.032 | .1893 | 314.6 |
| 158 | 45.1 | 81.2 | .4596 | 1.1554 | .3218 | 5.154 | 3.108 | .1940 | 316.4 |
| 159 | 45.2 | 81.4 | .4620 | 1.1509 | .3140 | 5.029 | 3.185 | .1988 | 318.2 |
| 160 | 45.3 | 81.5 | .4644 | 1.1465 | .3063 | 4.906 | 3.265 | .2038 | 320.0 |
| 161 | 45.3 | 81.6 | .4668 | 1.1421 | .2989 | 4.789 | 3.345 | .2088 | 321.8 |
| 162 | 45.4 | 81.7 | .4692 | 1.1377 | .2920 | 4.677 | 3.425 | .2138 | 323.6 |
| 163 | 45.5 | 81.8 | .4715 | 1.1333 | .2855 | 4.571 | 3.503 | .2188 | 325.4 |
| 164 | 45.5 | 81.9 | .4739 | 1.1289 | .2792 | 4.469 | 3.582 | .2238 | 327.2 |
| 165 | 45.6 | 82.0 | .4763 | 1.1245 | .2729 | 4.368 | 3.664 | .2289 | 329.0 |
| 166 | 45.6 | 82.1 | .4786 | 1.1202 | .2666 | 4.268 | 3.751 | .2343 | 330.8 |
| 167 | 45.7 | 82.2 | .4810 | 1.1159 | .2603 | 4.168 | 3.842 | .2399 | 332.6 |
| 168 | 45.7 | 82.4 | .4833 | 1.1115 | .2540 | 4.070 | 3.937 | .2457 | 334.4 |
| 169 | 45.8 | 82.5 | .4857 | 1.1072 | .2480 | 3.975 | 4.032 | .2516 | 336.2 |

PROPERTIES OF SATURATED STEAM

Metric and Common Units 0° to 220° C

| Temperature Degrees Centigrade. t. | Pressure. | | | Heat of the Liquid. | | Heat of Vaporization. | | Heat Equivalent of Internal Work. | | Temperature Degrees Fahrenheit. t. |
|---|--------------------------------|---------------------------------|----------------------------------|------------------------|----------|--------------------------|----------|--------------------------------------|----------|---|
| | Mm. of Mercury. p | Kg. per sq. cm. p. | Pds. per sq. in. p. | Calories. | B. T. U. | Calories. | B. T. U. | Calories. | B. T. U. | |
| | | | | q. | q. | r. | r. | ρ. | ρ. | |
| 170 | 5937 | 8.071 | 114.8 | 171.6 | 308.9 | 488.7 | 879.6 | 442.8 | 797.0 | 338.0 |
| 171 | 6081 | 8.268 | 117.6 | 172.6 | 310.7 | 487.9 | 878.3 | 441.9 | 795.6 | 339.8 |
| 172 | 6229 | 8.469 | 120.4 | 173.7 | 312.6 | 487.1 | 876.9 | 441.1 | 794.1 | 341.6 |
| 173 | 6379 | 8.673 | 123.4 | 174.7 | 314.5 | 486.3 | 875.4 | 440.2 | 792.5 | 343.4 |
| 174 | 6533 | 8.882 | 126.3 | 175.7 | 316.3 | 485.5 | 873.9 | 439.4 | 790.9 | 345.2 |
| 175 | 6689 | 9.094 | 129.4 | 176.8 | 318.2 | 484.7 | 872.4 | 438.5 | 789.3 | 347.0 |
| 176 | 6848 | 9.310 | 132.4 | 177.8 | 320.0 | 483.9 | 871.0 | 437.7 | 787.8 | 348.8 |
| 177 | 7010 | 9.531 | 135.6 | 178.8 | 321.8 | 483.1 | 869.5 | 436.8 | 786.2 | 350.6 |
| 178 | 7175 | 9.755 | 138.8 | 179.9 | 323.7 | 482.3 | 868.1 | 436.0 | 784.7 | 352.4 |
| 179 | 7343 | 9.983 | 142.0 | 180.9 | 325.6 | 481.4 | 866.6 | 435.0 | 783.1 | 354.2 |
| 180 | 7514 | 10.216 | 145.3 | 181.9 | 327.5 | 480.6 | 865.1 | 434.2 | 781.5 | 356.0 |
| 181 | 7688 | 10.453 | 148.7 | 183.0 | 329.3 | 479.8 | 863.6 | 433.3 | 779.9 | 357.8 |
| 182 | 7866 | 10.695 | 152.1 | 184.0 | 331.2 | 479.0 | 862.2 | 432.5 | 778.4 | 359.6 |
| 183 | 8046 | 10.940 | 155.6 | 185.0 | 333.0 | 478.2 | 860.7 | 431.6 | 776.9 | 361.4 |
| 184 | 8230 | 11.189 | 159.2 | 186.1 | 334.9 | 477.4 | 859.2 | 430.8 | 775.3 | 363.2 |
| 185 | 8417 | 11.44 | 162.8 | 187.1 | 336.8 | 476.6 | 857.7 | 429.9 | 773.7 | 365.0 |
| 186 | 8608 | 11.70 | 166.5 | 188.1 | 338.6 | 475.7 | 856.3 | 429.0 | 772.2 | 366.8 |
| 187 | 8802 | 11.97 | 170.2 | 189.2 | 340.5 | 474.8 | 854.7 | 428.0 | 770.5 | 368.6 |
| 188 | 8999 | 12.24 | 174.0 | 190.2 | 342.4 | 474.0 | 853.2 | 427.2 | 768.9 | 370.4 |
| 189 | 9200 | 12.51 | 177.9 | 191.2 | 344.2 | 473.2 | 851.7 | 426.3 | 767.4 | 372.2 |
| 190 | 9404 | 12.79 | 181.8 | 192.3 | 346.1 | 472.3 | 850.2 | 425.4 | 765.8 | 374.0 |
| 191 | 9612 | 13.07 | 185.9 | 193.3 | 347.9 | 471.5 | 848.7 | 424.5 | 764.2 | 375.8 |
| 192 | 9823 | 13.36 | 190.0 | 194.4 | 349.8 | 470.6 | 847.1 | 423.6 | 762.5 | 377.6 |
| 193 | 10038 | 13.65 | 194.1 | 195.4 | 351.7 | 469.8 | 845.6 | 422.8 | 761.0 | 379.4 |
| 194 | 10256 | 13.94 | 198.3 | 196.4 | 353.5 | 468.9 | 844.1 | 421.9 | 759.4 | 381.2 |
| 195 | 10480 | 14.25 | 202.6 | 197.5 | 355.4 | 468.1 | 842.5 | 421.0 | 757.7 | 383.0 |
| 196 | 10700 | 14.55 | 207.0 | 198.5 | 357.3 | 467.2 | 841.0 | 420.1 | 756.1 | 384.8 |
| 197 | 10930 | 14.87 | 211.4 | 199.5 | 359.2 | 466.4 | 839.5 | 419.2 | 754.6 | 386.6 |
| 198 | 11170 | 15.18 | 216.0 | 200.6 | 361.1 | 465.6 | 838.0 | 418.4 | 753.0 | 388.4 |
| 199 | 11410 | 15.51 | 220.6 | 201.6 | 362.9 | 464.7 | 836.4 | 417.4 | 751.3 | 390.2 |
| 200 | 11650 | 15.84 | 225.2 | 202.7 | 364.8 | 463.8 | 834.8 | 416.5 | 749.7 | 392.0 |
| 201 | 11890 | 16.17 | 229.0 | 203.7 | 366.7 | 462.9 | 833.3 | 415.6 | 748.1 | 393.8 |
| 202 | 12140 | 16.51 | 234.8 | 204.7 | 368.5 | 462.1 | 831.8 | 414.8 | 746.6 | 395.6 |
| 203 | 12400 | 16.85 | 239.7 | 205.8 | 370.4 | 461.2 | 830.2 | 413.8 | 744.9 | 397.4 |
| 204 | 12650 | 17.20 | 244.7 | 206.8 | 372.3 | 460.3 | 828.6 | 412.9 | 743.3 | 399.2 |
| 205 | 12920 | 17.56 | 249.8 | 207.9 | 374.1 | 459.4 | 827.0 | 412.0 | 741.6 | 401.0 |
| 206 | 13180 | 17.92 | 254.9 | 208.9 | 376.0 | 458.6 | 825.4 | 411.1 | 740.0 | 402.8 |
| 207 | 13450 | 18.29 | 260.1 | 210.0 | 377.9 | 457.7 | 823.8 | 410.2 | 738.3 | 404.6 |
| 208 | 13730 | 18.66 | 265.4 | 211.0 | 379.8 | 456.8 | 822.2 | 409.3 | 736.7 | 406.4 |
| 209 | 14010 | 19.04 | 270.8 | 212.0 | 381.6 | 455.9 | 820.6 | 408.4 | 735.1 | 408.2 |
| 210 | 14290 | 19.43 | 276.3 | 213.1 | 383.5 | 455.0 | 819.1 | 407.5 | 733.6 | 410.0 |
| 211 | 14580 | 19.82 | 281.9 | 214.1 | 385.4 | 454.1 | 817.4 | 406.6 | 731.9 | 411.8 |
| 212 | 14870 | 20.22 | 287.6 | 215.2 | 387.3 | 453.2 | 815.8 | 405.7 | 730.2 | 413.6 |
| 213 | 15170 | 20.62 | 293.3 | 216.2 | 389.2 | 452.4 | 814.3 | 404.9 | 728.7 | 415.4 |
| 214 | 15470 | 21.03 | 299.2 | 217.3 | 391.1 | 451.5 | 812.7 | 404.0 | 727.1 | 417.2 |
| 215 | 15780 | 21.45 | 305.1 | 218.3 | 392.9 | 450.6 | 811.0 | 403.1 | 725.4 | 419.0 |
| 216 | 16090 | 21.88 | 311.1 | 219.3 | 394.8 | 449.6 | 809.3 | 402.1 | 723.7 | 420.8 |
| 217 | 16410 | 22.31 | 317.3 | 220.4 | 396.7 | 448.7 | 807.7 | 401.2 | 722.1 | 422.6 |
| 218 | 16730 | 22.74 | 323.5 | 221.4 | 398.5 | 447.8 | 806.1 | 400.3 | 720.5 | 424.4 |
| 219 | 17060 | 23.19 | 329.8 | 222.5 | 400.4 | 446.9 | 804.5 | 399.4 | 718.9 | 426.2 |
| 220 | 17390 | 23.64 | 336.2 | 223.5 | 402.3 | 446.0 | 802.9 | 398.5 | 717.3 | 428.0 |

PROPERTIES OF SATURATED STEAM

Metric and Common Units 0° to 220 °C

| Temperature Degrees Centigrade. t. | Heat Equivalent of External Work. | | Entropy of the Liquid. θ | Entropy of Evapo- ration. $\frac{r}{T}$ | Specific Volume. | | Density. | | Temperature Degrees Fahrenheit. t. |
|---|--------------------------------------|----------------------|--|--|---|--------------------------------------|---|---|---|
| | Calories. Apu. | B. T. U. Apu. | | | Cubic Meters per Kilogram. s | Cubic Feet per Pound. s | Kilograms per Cubic Meter. $\frac{1}{s}$ | Pounds per Cubic Foot. $\frac{1}{s}$ | |
| | | | | | | | | | |
| 170 | 45.9 | 82.6 | 0.4880 | 1.1029 | 0.2423 | 3.883 | 4.127 | 0.2575 | 338.0 |
| 171 | 46.0 | 82.7 | .4903 | 1.0987 | .2368 | 3.794 | 4.223 | .2636 | 339.8 |
| 172 | 46.0 | 82.8 | .4926 | 1.0944 | .2314 | 3.709 | 4.322 | .2696 | 341.6 |
| 173 | 46.1 | 82.9 | .4949 | 1.0901 | .2262 | 3.626 | 4.421 | .2758 | 343.4 |
| 174 | 46.1 | 83.0 | .4972 | 1.0859 | .2212 | 3.545 | 4.521 | .2821 | 345.2 |
| 175 | 46.2 | 83.1 | .4995 | 1.0817 | .2164 | 3.467 | 4.621 | .2884 | 347.0 |
| 176 | 46.2 | 83.2 | .5018 | 1.0775 | .2117 | 3.391 | 4.724 | .2949 | 348.8 |
| 177 | 46.3 | 83.3 | .5041 | 1.0733 | .2072 | 3.318 | 4.826 | .3014 | 350.6 |
| 178 | 46.3 | 83.4 | .5064 | 1.0691 | .2027 | 3.247 | 4.933 | .3080 | 352.4 |
| 179 | 46.4 | 83.5 | .5087 | 1.0649 | .1983 | 3.177 | 5.04 | .3148 | 354.2 |
| 180 | 46.4 | 83.6 | .5110 | 1.0608 | .1941 | 3.109 | 5.15 | .3217 | 356.0 |
| 181 | 46.5 | 83.7 | .5133 | 1.0567 | .1899 | 3.041 | 5.27 | .3288 | 357.8 |
| 182 | 46.5 | 83.8 | .5156 | 1.0525 | .1857 | 2.974 | 5.38 | .3362 | 359.6 |
| 183 | 46.6 | 83.8 | .5178 | 1.0484 | .1817 | 2.911 | 5.50 | .3435 | 361.4 |
| 184 | 46.6 | 83.9 | .5201 | 1.0443 | .1778 | 2.849 | 5.62 | .3510 | 363.2 |
| 185 | 46.7 | 84.0 | .5224 | 1.0403 | .1740 | 2.787 | 5.75 | .3588 | 365.0 |
| 186 | 46.7 | 84.1 | .5246 | 1.0362 | .1702 | 2.727 | 5.88 | .3667 | 366.8 |
| 187 | 46.8 | 84.2 | .5269 | 1.0321 | .1666 | 2.669 | 6.00 | .3746 | 368.6 |
| 188 | 46.8 | 84.3 | .5291 | 1.0280 | .1632 | 2.614 | 6.13 | .3826 | 370.4 |
| 189 | 46.9 | 84.3 | .5314 | 1.0240 | .1598 | 2.560 | 6.26 | .3906 | 372.2 |
| 190 | 46.9 | 84.4 | .5336 | 1.0200 | .1565 | 2.507 | 6.39 | .3989 | 374.0 |
| 191 | 47.0 | 84.5 | .5358 | 1.0160 | .1533 | 2.456 | 6.52 | .4072 | 375.8 |
| 192 | 47.0 | 84.6 | .5381 | 1.0120 | .1501 | 2.405 | 6.66 | .4158 | 377.6 |
| 193 | 47.0 | 84.6 | .5403 | 1.0080 | .1470 | 2.355 | 6.80 | .4246 | 379.4 |
| 194 | 47.0 | 84.7 | .5426 | 1.0040 | .1440 | 2.306 | 6.94 | .4336 | 381.2 |
| 195 | 47.1 | 84.8 | .5448 | 1.0000 | .1411 | 2.259 | 7.09 | .4426 | 383.0 |
| 196 | 47.1 | 84.9 | .5470 | 0.9960 | .1382 | 2.214 | 7.23 | .4516 | 384.8 |
| 197 | 47.2 | 84.9 | .5492 | .9922 | .1354 | 2.169 | 7.38 | .4610 | 386.6 |
| 198 | 47.2 | 85.0 | .5514 | .9882 | .1327 | 2.126 | 7.53 | .4704 | 388.4 |
| 199 | 47.3 | 85.1 | .5536 | .9843 | .1300 | 2.083 | 7.69 | .4801 | 390.2 |
| 200 | 47.3 | 85.1 | .5558 | .9804 | .1274 | 2.041 | 7.84 | .4900 | 392.0 |
| 201 | 47.3 | 85.2 | .5580 | .9765 | .1249 | 2.001 | 8.00 | .4998 | 393.8 |
| 202 | 47.3 | 85.2 | .5602 | .9727 | .1225 | 1.962 | 8.16 | .510 | 395.6 |
| 203 | 47.4 | 85.3 | .5624 | .9688 | .1201 | 1.923 | 8.33 | .520 | 397.4 |
| 204 | 47.4 | 85.3 | .5646 | .9650 | .1177 | 1.885 | 8.50 | .531 | 399.2 |
| 205 | 47.4 | 85.4 | .5668 | .9611 | .1153 | 1.847 | 8.67 | .541 | 401.0 |
| 206 | 47.5 | 85.4 | .5690 | .9572 | .1130 | 1.810 | 8.85 | .552 | 402.8 |
| 207 | 47.5 | 85.5 | .5712 | .9534 | .1108 | 1.774 | 9.03 | .564 | 404.6 |
| 208 | 47.5 | 85.5 | .5733 | .9496 | .1086 | 1.739 | 9.21 | .575 | 406.4 |
| 209 | 47.5 | 85.5 | .5755 | .9458 | .1065 | 1.705 | 9.39 | .587 | 408.2 |
| 210 | 47.5 | 85.5 | .5777 | .9420 | .1044 | 1.673 | 9.58 | .598 | 410.0 |
| 211 | 47.5 | 85.5 | .5799 | .9382 | .1024 | 1.640 | 9.77 | .610 | 411.8 |
| 212 | 47.5 | 85.6 | .5820 | .9344 | .1004 | 1.608 | 9.96 | .622 | 413.6 |
| 213 | 47.5 | 85.6 | .5842 | .9307 | .0984 | 1.577 | 10.16 | .634 | 415.4 |
| 214 | 47.5 | 85.6 | .5863 | .9269 | .0965 | 1.546 | 10.36 | .647 | 417.2 |
| 215 | 47.5 | 85.6 | .5885 | .9232 | .0947 | 1.516 | 10.56 | .660 | 419.0 |
| 216 | 47.5 | 85.6 | .5906 | .9195 | .0928 | 1.486 | 10.78 | .673 | 420.8 |
| 217 | 47.5 | 85.6 | .5927 | .9157 | .0910 | 1.458 | 10.99 | .686 | 422.6 |
| 218 | 47.5 | 85.6 | .5948 | .9120 | .0893 | 1.430 | 11.20 | .699 | 424.4 |
| 219 | 47.5 | 85.6 | .5969 | .9084 | .0876 | 1.403 | 11.41 | .713 | 426.2 |
| 220 | 47.5 | 85.6 | .5991 | .9047 | .0860 | 1.376 | 11.62 | .727 | 428.0 |

PROPERTIES OF SATURATED STEAM

Common Units, 400° to 700° F.

Abridged from Steam Tables and Mollier's Diagram by Keenan. Printed by permission of the publisher, The American Society of Mechanical Engineers. For detailed discussion see Mechanical Engineering, Feb., 1929, *v.*, specific vol., ft.³/lb.; *h*, total heat, enthalpy, B.t.u./lb.; *s*, entropy, B.t.u./°F./lb. The strict definition of total heat (internal energy + 144/*J*) is adhered to; zeros of both *h* and *s* are arbitrarily placed on the sat. liq. line at 32°F. No internal energy values are tabulated but may be easily found by subtracting 144 *pv*/*J* from the total heat. The energy unit, the B.t.u., is 778.57 ft.-lb. (*J*) is 1/180 of the change in total heat along the saturated liquid line between 32° and 212°F. (Osborne, Fiock, Stimson.)

| Temp. F. <i>t</i> | Abs. <i>p</i> . lb./in. ² | Specific Volume | | | Total Heat | | | Entropy | | |
|-------------------------|---|-----------------------------------|--------------------------------|------------------------------------|-----------------------------------|--------------------------------|------------------------------------|-----------------------------------|--------------------------------|------------------------------------|
| | | Sat. liq. <i>v_f</i> | Evap. <i>v_{fg}</i> | Sat. vapor <i>v_g</i> | Sat. liq. <i>h_f</i> | Evap. <i>h_{fg}</i> | Sat. vapor <i>h_g</i> | Sat. liq. <i>s_f</i> | Evap. <i>s_{fg}</i> | Sat. vapor <i>s_g</i> |
| 400 | 247.25 | 0.01865 | 1.8421 | 1.8608 | 375.0 | 826 | 1200 | 0.5668 | 0.9602 | 1.5270 |
| 405 | 261.67 | .01873 | 1.7428 | 1.7615 | 380.4 | 821 | 1201 | .5730 | .9491 | 1.5221 |
| 410 | 276.72 | .01880 | 1.6493 | 1.6681 | 385.9 | 816 | 1202 | .5792 | .9381 | 1.5173 |
| 415 | 292.44 | .01888 | 1.5615 | 1.5804 | 391.3 | 811 | 1202 | .5854 | .9271 | 1.5125 |
| 420 | 308.82 | .01896 | 1.4792 | 1.4982 | 396.8 | 806 | 1203 | .5916 | .9161 | 1.5077 |
| 425 | 325.91 | .01904 | 1.4022 | 1.4212 | 402.4 | 801 | 1203 | .5978 | .9052 | 1.5029 |
| 430 | 343.71 | .01911 | 1.3295 | 1.3486 | 407.9 | 796 | 1203 | .6039 | .8942 | 1.4982 |
| 435 | 362.27 | .01919 | 1.2610 | 1.2802 | 413.5 | 790 | 1204 | .6101 | .8833 | 1.4934 |
| 440 | 381.59 | .01928 | 1.1965 | 1.2158 | 419.1 | 785 | 1204 | .6162 | .8724 | 1.4887 |
| 445 | 401.70 | .01936 | 1.1356 | 1.1550 | 424.7 | 779 | 1204 | .6224 | .8616 | 1.4839 |
| 450 | 422.61 | .0195 | 1.0782 | 1.0977 | 430 | 774 | 1204 | .6284 | .8507 | 1.4792 |
| 455 | 444.35 | .0195 | 1.0241 | 1.0436 | 436 | 768 | 1204 | .6346 | .8398 | 1.4744 |
| 460 | 466.94 | .0196 | .9730 | .9927 | 442 | 762 | 1204 | .6407 | .8290 | 1.4696 |
| 465 | 490.40 | .0197 | .9249 | .9446 | 447 | 756 | 1204 | .6468 | .8180 | 1.4649 |
| 470 | 514.76 | .0198 | .8793 | .8991 | 453 | 750 | 1204 | .6530 | .8071 | 1.4601 |
| 475 | 540.04 | .0199 | .8361 | .8560 | 459 | 744 | 1203 | .6592 | .7962 | 1.4554 |
| 480 | 566.26 | .0200 | .7951 | .8151 | 465 | 738 | 1203 | .6654 | .7852 | 1.4506 |
| 485 | 593.47 | .0201 | .7563 | .7764 | 471 | 731 | 1202 | .6716 | .7742 | 1.4458 |
| 490 | 621.67 | .0202 | .7195 | .7398 | 477 | 725 | 1202 | .6779 | .7632 | 1.4410 |
| 495 | 650.87 | .0204 | .6847 | .7050 | 483 | 718 | 1201 | .6842 | .7521 | 1.4362 |
| 500 | 681.09 | .0205 | .6516 | .6721 | 489 | 711 | 1200 | .6904 | .7410 | 1.4314 |
| 505 | 712.40 | .0206 | .6201 | .6408 | 495 | 704 | 1199 | .6968 | .7299 | 1.4266 |
| 510 | 744.74 | .0207 | .5903 | .6110 | 502 | 697 | 1198 | .7031 | .7187 | 1.4218 |
| 515 | 778.16 | .0209 | .5618 | .5826 | 508 | 690 | 1197 | .7094 | .7075 | 1.4170 |
| 520 | 812.72 | .0210 | .5347 | .5557 | 514 | 682 | 1196 | .7158 | .6963 | 1.4121 |
| 525 | 848.43 | .0211 | .5090 | .5301 | 521 | 675 | 1195 | .7222 | .6851 | 1.4073 |
| 530 | 885.31 | .0213 | .4845 | .5058 | 527 | 667 | 1193 | .7286 | .6738 | 1.4024 |
| 535 | 923.39 | .0214 | .4614 | .4828 | 533 | 659 | 1192 | .7350 | .6625 | 1.3975 |
| 540 | 962.73 | .0216 | .4394 | .4610 | 540 | 651 | 1191 | .7414 | .6512 | 1.3926 |
| 545 | 1003.4 | .0218 | .4184 | .4401 | 547 | 643 | 1189 | .7478 | .6399 | 1.3877 |
| 550 | 1045.4 | .0219 | .3982 | .4201 | 553 | 634 | 1188 | .7543 | .6285 | 1.3828 |
| 555 | 1088.7 | .0221 | .3789 | .4010 | 560 | 626 | 1186 | .7607 | .6170 | 1.3778 |
| 560 | 1133.4 | .0223 | .3605 | .3828 | 567 | 618 | 1184 | .7672 | .6056 | 1.3728 |
| 565 | 1179.7 | .0225 | .3429 | .3654 | 574 | 609 | 1182 | .7737 | .5940 | 1.3677 |
| 570 | 1227.6 | .0227 | .3261 | .3488 | 580 | 600 | 1180 | .7802 | .5825 | 1.3626 |
| 575 | 1276.7 | .0229 | .3101 | .3330 | 587 | 591 | 1178 | .7867 | .5709 | 1.3576 |
| 580 | 1327.2 | .0231 | .2949 | .3180 | 594 | 581 | 1176 | .7932 | .5592 | 1.3524 |
| 585 | 1379.2 | .0234 | .2804 | .3037 | 602 | 572 | 1173 | .7998 | .5474 | 1.3472 |
| 590 | 1432.7 | .0236 | .2664 | .2900 | 609 | 562 | 1171 | .8064 | .5356 | 1.3420 |
| 595 | 1487.8 | .0239 | .2530 | .2769 | 616 | 552 | 1168 | .8131 | .5237 | 1.3368 |
| 600 | 1544.6 | .0241 | .2401 | .2642 | 623 | 542 | 1166 | .8198 | .5118 | 1.3316 |
| 610 | 1663.2 | .0247 | .2159 | .2406 | 638 | 521 | 1160 | .8332 | .4875 | 1.3208 |
| 620 | 1788.8 | .0254 | .1933 | .2186 | 653 | 499 | 1153 | .8470 | .4623 | 1.3093 |
| 630 | 1921.9 | .0261 | .1721 | .1982 | 670 | 475 | 1144 | .8612 | .4358 | 1.2970 |
| 640 | 2062.8 | .0269 | .1522 | .1791 | 687 | 448 | 1135 | .8763 | .4073 | 1.2836 |
| 650 | 2211.4 | .0278 | .1331 | .1610 | 705 | 417 | 1122 | .8924 | .3764 | 1.2688 |
| 660 | 2368.6 | .0290 | .1148 | .1437 | 725 | 384 | 1109 | .9097 | .3426 | 1.2523 |
| 670 | 2534.2 | .0304 | .0966 | .1269 | 748 | 344 | 1092 | .9287 | .3049 | 1.2336 |
| 680 | 2709.7 | .0322 | .0781 | .1102 | 773 | 299 | 1071 | .9499 | .2619 | 1.2119 |
| 690 | 2896.8 | .0347 | .0589 | .0936 | 803 | 241 | 1044 | .9755 | .2098 | 1.1852 |
| 700 | 3096.4 | .0394 | .0353 | .0747 | 846 | 157 | 1003 | 1.0117 | .1354 | 1.1471 |
| 705 | 3202.0 | .0462 | .0135 | .0597 | 888 | 73 | 962 | 1.0472 | .0630 | 1.1102 |
| 706.1 | 3226.0 | .0522 | 0 | .0522 | 925 | 0 | 925 | 1.0785 | 0 | 1.0785 |

Common Units, 212° to 3000°F.

(Abridged from Steam Tables and Mollier's Diagram by Keenan, 1930. Printed by permission of publisher, The American Society of Mechanical Engineers.)

| Abs. <i>P</i> , lb./in. ² (Sat. <i>t</i> , °F.) | Sat. water | Sat. steam | 200°F. | 300°F. | 400°F. | 500°F. | 600°F. | 700°F. | 800°F. | 900°F. | 1000°F. | | | |
|---|---------------|---------------|----------|---------------------|----------|----------|--------|--------|--------|----------|---------|--------|--------|---------|
| | 0.02 | 26.82 | 27.16 | 30.52 | 34.65 | 38.75 | 42.83 | 46.91 | 50.97 | 55.03 | 59.09 | | | |
| 14.696 (212.00) | 180.0 | 1150.2 | 1154. | 1192. | 1239. | 1286. | 1334. | 1382. | 1432. | 1483. | 1535. | | | |
| | 0.3119 | 1.7564 | 1.762 | 1.815 | 1.873 | 1.925 | 1.972 | 2.016 | 2.057 | 2.096 | 2.133 | | | |
| | 0.017 | 8.514 | <i>v</i> | 8.78 | 10.06 | 11.30 | 12.53 | 13.74 | 14.93 | 16.14 | 17.34 | | | |
| 50 (281.01) | 250.0 | 1173.5 | <i>h</i> | 1184. | 1234. | 1283. | 1331. | 1381. | 1431. | 1482. | 1534. | | | |
| | 0.4111 | 1.6580 | <i>s</i> | 1.672 | 1.734 | 1.787 | 1.836 | 1.880 | 1.922 | 1.961 | 1.998 | | | |
| | 0.018 | 4.426 | <i>v</i> | | 4.93 | 5.58 | 6.21 | 6.83 | 7.44 | 8.04 | 8.64 | | | |
| 100 (327.83) | 298.3 | 1186.6 | <i>h</i> | | 1227. | 1278. | 1328. | 1378. | 1429. | 1481. | 1533. | | | |
| | 0.4742 | 1.6022 | <i>s</i> | | 1.651 | 1.708 | 1.757 | 1.802 | 1.844 | 1.884 | 1.921 | | | |
| | 0.018 | 3.010 | <i>v</i> | | 3.22 | 3.68 | 4.11 | 4.53 | 4.94 | 5.34 | 5.75 | | | |
| 150 (358.43) | 330.4 | 1194. | <i>h</i> | | 1219. | 1273. | 1324. | 1376. | 1427. | 1479. | 1532. | | | |
| | 0.5140 | 1.569 | <i>s</i> | | 1.599 | 1.659 | 1.710 | 1.756 | 1.799 | 1.838 | 1.876 | | | |
| | 0.018 | 2.285 | <i>v</i> | | 2.358 | 2.722 | 3.06 | 3.38 | 3.69 | 4.00 | 4.30 | | | |
| 200 (381.82) | 355. | 1198. | <i>h</i> | | 1210. | 1268. | 1321. | 1373. | 1426. | 1478. | 1531. | | | |
| | 0.543 | 1.545 | <i>s</i> | | 1.559 | 1.623 | 1.676 | 1.723 | 1.766 | 1.806 | 1.8438 | | | |
| | 0.0189 | 1.541 | <i>v</i> | | | 1.765 | 2.002 | 2.224 | 2.438 | 2.646 | 2.849 | | | |
| 300 (417.33) | 394. | 1202. | <i>h</i> | | | 1257. | 1313. | 1368. | 1422. | 1475. | 1529. | | | |
| | 0.5883 | 1.510 | <i>s</i> | | | 1.569 | 1.626 | 1.675 | 1.719 | 1.760 | 1.798 | | | |
| | 0.0194 | 1.160 | <i>v</i> | | | 1.283 | 1.474 | 1.647 | 1.812 | 1.970 | 2.125 | | | |
| 400 (444.58) | 424. | 1204. | <i>h</i> | | | 1244. | 1306. | 1362. | 1418. | 1472. | 1527. | | | |
| | 0.622 | 1.484 | <i>s</i> | | | 1.528 | 1.588 | 1.640 | 1.685 | 1.727 | 1.766 | | | |
| | 0.0198 | 0.926 | <i>v</i> | <i>=</i> sp. vol. | | 0.991 | 1.156 | 1.301 | 1.436 | 1.566 | 1.690 | | | |
| 500 | 450. | 1204. | <i>h</i> | <i>=</i> total heat | | 1230. | 1297. | 1357. | 1414. | 1469. | 1525. | | | |
| | 0.649 | 1.463 | <i>s</i> | <i>=</i> entropy | | 1.491 | 1.558 | 1.611 | 1.659 | 1.701 | 1.740 | | | |
| | | | | 500°F. | 550°F. | 600°F. | 650°F. | 700°F. | 750°F. | 800°F. | 850°F. | 900°F. | 950°F. | 1000°F. |
| | 0.0202 | 0.768 | 0.792 | 0.873 | 0.943 | 1.008 | 1.069 | | 1.186 | <i>v</i> | 1.295 | | 1.400 | |
| 600 (486.17) | 472. | 1202. | 1215. | 1255. | 1289. | 1320. | 1351. | | 1409. | <i>h</i> | 1466. | | 1523. | |
| | 0.673 | 1.445 | 1.458 | 1.499 | 1.532 | 1.561 | 1.587 | | 1.636 | <i>s</i> | 1.679 | | 1.720 | |
| | 0.0206 | 0.653 | <i>v</i> | 0.725 | 0.791 | 0.849 | 0.904 | | 1.006 | | 1.103 | | 1.193 | |
| 700 (503.04) | 493. | 1200. | <i>h</i> | 1242. | 1280. | 1313. | 1345. | | 1405. | | 1463. | | 1521. | |
| | 0.694 | 1.429 | <i>s</i> | 1.472 | 1.508 | 1.539 | 1.567 | | 1.617 | | 1.661 | | 1.702 | |
| | 0.0209 | 0.565 | <i>v</i> | 0.613 | 0.675 | 0.729 | 0.779 | | 0.872 | 0.916 | 0.958 | 0.998 | 1.037 | |
| 800 (518.18) | 512. | 1197. | <i>h</i> | 1229. | 1270. | 1305. | 1338. | | 1400. | 1430. | 1460. | 1489. | 1519. | |
| | 0.714 | 1.414 | <i>s</i> | 1.446 | 1.486 | 1.519 | 1.548 | | 1.599 | 1.623 | 1.645 | 1.666 | 1.686 | |
| | 0.0213 | 0.497 | <i>v</i> | 0.523 | 0.584 | 0.636 | 0.682 | | 0.768 | 0.807 | 0.845 | 0.882 | 0.917 | |
| 900 (531.95) | 530. | 1193. | <i>h</i> | 1214. | 1260. | 1297. | 1332. | | 1396. | 1427. | 1457. | 1487. | 1517. | |
| | 0.731 | 1.401 | <i>s</i> | 1.421 | 1.466 | 1.500 | 1.530 | | 1.583 | 1.607 | 1.630 | 1.652 | 1.672 | |
| | 0.0217 | 0.442 | <i>v</i> | 0.450 | 0.511 | 0.560 | 0.604 | 0.645 | 0.684 | 0.720 | 0.755 | 0.788 | 0.820 | |
| 1000 (544.58) | 546. | 1190. | <i>h</i> | 1197. | 1249. | 1289. | 1325. | 1358. | 1391. | 1423. | 1454. | 1484. | 1515. | |
| | 0.747 | 1.388 | <i>s</i> | 1.395 | 1.446 | 1.483 | 1.514 | 1.538 | 1.569 | 1.593 | 1.617 | 1.639 | 1.660 | |
| | 0.0239 | 0.274 | .. | <i>v</i> | 0.279 | 0.330 | 0.368 | 0.401 | 0.432 | 0.459 | 0.484 | 0.508 | 0.530 | |
| 1500 (596.08) | 618. | 1168. | .. | <i>h</i> | 1174. | 1240. | 1287. | 1327. | 1365. | 1402. | 1438. | 1472. | 1505. | |
| | 0.815 | 1.336 | .. | <i>s</i> | 1.342 | 1.403 | 1.444 | 1.478 | 1.509 | 1.537 | 1.564 | 1.589 | 1.612 | |
| | 0.0265 | 0.188 | .. | .. | <i>v</i> | 0.204 | 0.247 | 0.278 | 0.305 | 0.327 | 0.349 | 0.367 | 0.384 | |
| 2000 (635.61) | 679. | 1139. | .. | .. | <i>h</i> | 1169. | 1241. | 1291. | 1337. | 1380. | 1421. | 1459. | 1495. | |
| | 0.870 | 1.290 | .. | .. | <i>s</i> | 1.317 | 1.380 | 1.423 | 1.460 | 1.493 | 1.524 | 1.552 | 1.577 | |
| | 0.0301 | 0.130 | .. | .. | .. | <i>v</i> | 0.168 | 0.202 | 0.227 | 0.248 | 0.267 | 0.282 | 0.298 | |
| 2500 (667.98) | 743. | 1096. | .. | .. | .. | <i>h</i> | 1178. | 1250. | 1306. | 1357. | 1404. | 1446. | 1484. | |
| | 0.925 | 1.238 | .. | .. | .. | <i>s</i> | 1.310 | 1.371 | 1.416 | 1.456 | 1.491 | 1.521 | 1.548 | |
| | 0.0367 | 0.084 | .. | .. | .. | <i>v</i> | .0983 | 1.176 | 1.174 | 1.1947 | 0.212 | 0.227 | 0.240 | |
| 3000 (695.25) | 823. | 1026. | .. | .. | .. | <i>h</i> | 1066. | 1199. | 1271. | 1331. | 1384. | 1432. | 1473. | |
| | 0.992 | 1.168 | .. | .. | .. | <i>s</i> | 1.203 | 1.316 | 1.374 | 1.420 | 1.460 | 1.494 | 1.521 | |

TABLE 293.—Properties of Mercury Vapor

402° to 1000° F.

| Pressure abs. lbs./in. ² | Tem- perature °F. | Heat of liquid above 32° F. B.t.u. | Heat of vaporization B.t.u. | Total heat B.t.u. | Entropy of liquid above 32° F. | Entropy of vaporization | Total entropy | Specific volume cu. ft./lb. | Weight lbs./cu. ft. |
|---|-------------------------|--|-----------------------------------|-------------------------|---|-------------------------------|------------------|-----------------------------------|------------------------|
| 0.4 | 402 | 13.81 | 128.15 | 141.96 | .0209 | .1487 | .1696 | 114.50 | 0.008733 |
| 0.8 | 444 | 15.36 | 127.24 | 142.60 | .0227 | .1408 | .1635 | 59.72 | .016745 |
| 1.0 | 458 | 15.89 | 126.02 | 142.81 | .0233 | .1383 | .1616 | 48.45 | .02064 |
| 1.5 | 485 | 16.90 | 126.33 | 143.23 | .0244 | .1337 | .1581 | 33.14 | .03017 |
| 2.0 | 505 | 17.65 | 125.89 | 143.54 | .0251 | .1305 | .1556 | 25.32 | .03948 |
| 4.0 | 558 | 19.62 | 124.72 | 144.34 | .0271 | .1226 | .1497 | 13.26 | .07540 |
| 6.0 | 591 | 20.87 | 123.99 | 144.86 | .0283 | .1179 | .1462 | 9.096 | .10093 |
| 8.0 | 617 | 21.81 | 123.43 | 145.24 | .0292 | .1147 | .1439 | 6.9630 | .14361 |
| 10.0 | 637 | 22.58 | 122.98 | 145.56 | .0299 | .1121 | .1420 | 5.6610 | .17664 |
| 15.0 | 676 | 24.04 | 122.12 | 146.16 | .0312 | .1075 | .1387 | 3.8923 | .25691 |
| 20.0 | 706 | 25.15 | 121.46 | 146.61 | .0322 | .1042 | .1364 | 2.983 | .3352 |
| 25.0 | 730 | 26.05 | 120.93 | 146.98 | .0330 | .1016 | .1346 | 2.429 | .4117 |
| 30.0 | 751 | 26.81 | 120.48 | 147.29 | .0336 | .0995 | .1331 | 2.053 | .4871 |
| 35.0 | 769 | 27.49 | 120.08 | 147.57 | .0342 | .0977 | .1319 | 1.7815 | .5613 |
| 40.0 | 785 | 28.08 | 119.73 | 147.81 | .0346 | .0962 | .1308 | 1.5762 | .6344 |
| 45.0 | 799 | 28.62 | 119.42 | 148.04 | .0351 | .0949 | .1300 | 1.4147 | .7069 |
| 50 | 812 | 29.11 | 119.13 | 148.24 | .0355 | .0936 | .1291 | 1.284 | .7788 |
| 60 | 836 | 29.99 | 118.61 | 148.60 | .0361 | .0915 | .1276 | 1.086 | .9204 |
| 70 | 857 | 30.75 | 118.15 | 148.90 | .0367 | .0898 | .1265 | .9436 | 1.0597 |
| 80 | 875 | 31.44 | 117.75 | 149.19 | .0372 | .0882 | .1254 | .8349 | 1.1977 |
| 90 | 892 | 32.00 | 117.38 | 149.44 | .0377 | .0870 | .1247 | .7497 | 1.3338 |
| 100 | 907 | 32.63 | 117.05 | 149.68 | .0381 | .0856 | .1237 | .6811 | 1.4682 |
| 110 | 921 | 33.10 | 116.74 | 149.90 | .0385 | .0845 | .1230 | .6242 | 1.6020 |
| 120 | 934 | 33.66 | 116.44 | 150.10 | .0389 | .0835 | .1224 | .5767 | 1.7340 |
| 130 | 947 | 34.12 | 116.17 | 150.29 | .0392 | .0826 | .1218 | .5360 | 1.8656 |
| 140 | 958 | 34.55 | 115.92 | 150.47 | .0395 | .0818 | .1213 | .5012 | 1.9952 |
| 150 | 969 | 34.96 | 115.67 | 150.63 | .0398 | .0809 | .1207 | .4706 | 2.125 |
| 180 | 1000 | 36.09 | 115.01 | 151.10 | .0406 | .0788 | .1194 | .3990 | 2.506 |

(Adapted from Emmet Mercury Vapor Process, Emmet and Sheldon, Amer. Soc. Mech. Eng., May, 1924.)

TABLE 294.—Properties of Liquid Ammonia

-100° to +250° F.

| Temp. °F. <i>t</i> | Saturation | | | | | | Latent heat of pressure variation B.t.u./lb. $\frac{B.t.u./lb.}{l}$ | Variation of <i>h</i> with <i>p</i> <i>t</i> constant B.t.u./lb. $\frac{lb./in.^2}{(\frac{\partial h}{\partial p})_t}$ | Compressi- bility per lb./in. ² × 10 ⁶ $-\frac{1}{v}(\frac{\partial v}{\partial p})_t$ |
|--------------------------|---|---|--|---|---|--|--|--|--|
| | Pressure (abs.) lbs./in. ² <i>p</i> | Volume ft. ³ /lb. <i>v</i> | Density lb./ft. ³ $\frac{1}{v}$ | Specific heat B.t.u./lb. °F. <i>c</i> | Heat content B.t.u./lb. <i>h</i> | Latent heat B.t.u./lb. <i>L</i> | | | |
| -100 | 1.24 | .02197 | 45.52 | (1.040) | (-63.0) | (633) | | | |
| -90 | 1.86 | .02216 | 45.12 | (1.043) | (-52.6) | (628) | | | |
| -80 | 2.74 | .02236 | 44.72 | (1.046) | (-42.2) | (622) | | | |
| -70 | 3.94 | .02256 | 44.32 | (1.050) | (-31.7) | (616) | | | |
| -60 | 5.55 | .02278 | 43.91 | 1.054 | -21.18 | 610.8 | -.0016 | .0026 | 4.4 |
| -50 | 7.67 | .02299 | 43.40 | 1.058 | -10.61 | 604.3 | -.0017 | .0026 | 4.6 |
| -40 | 10.41 | .02322 | 43.08 | 1.062 | 0.00 | 597.6 | -.0018 | .0025 | 4.8 |
| -30 | 13.90 | .02345 | 42.65 | 1.066 | +10.66 | 590.7 | -.0019 | .0025 | 5.1 |
| -20 | 18.30 | .02369 | 42.22 | 1.070 | +21.36 | 583.6 | -.0020 | .0024 | 5.4 |
| -10 | 23.74 | .02393 | 41.78 | 1.075 | 32.11 | 576.4 | -.0021 | .0023 | 5.7 |
| 0 | 30.42 | .02419 | 41.34 | 1.080 | 42.92 | 568.9 | -.0022 | .0022 | 6.0 |
| +10 | 38.51 | .02446 | 40.89 | 1.085 | 53.79 | 561.1 | -.0024 | .0021 | 6.4 |
| +20 | 48.21 | .02474 | 40.43 | 1.091 | 64.71 | 553.1 | -.0025 | .0020 | 6.8 |
| 30 | 59.74 | .02503 | 39.96 | 1.097 | 75.71 | 544.8 | -.0027 | .0019 | 7.3 |
| 40 | 73.32 | .02533 | 39.49 | 1.104 | 86.77 | 536.2 | -.0029 | .0018 | 7.8 |
| 50 | 89.19 | .02564 | 39.00 | 1.112 | 97.93 | 527.3 | -.0031 | .0017 | 8.4 |
| 60 | 107.6 | .02597 | 38.50 | 1.120 | 109.18 | 518.1 | -.0033 | .0015 | 9.1 |
| 70 | 128.8 | .02632 | 38.00 | 1.129 | 120.54 | 508.6 | -.0035 | .0013 | 10.0 |
| 80 | 153.9 | .02668 | 37.48 | 1.138 | 131.99 | 498.7 | -.0038 | .0011 | 10.9 |
| 90 | 186.6 | .02707 | 36.95 | 1.147 | 143.54 | 488.5 | -.0041 | .0009 | 12.0 |
| +100 | 211.9 | .02747 | 36.40 | 1.156 | 155.21 | 477.8 | -.0045 | .0006 | 13.3 |
| 125 | 307.8 | .02860 | 34.96 | (1.189) | (185) | (449) | | | |
| 150 | 433.2 | .02995 | 33.39 | (1.23) | (216) | (416) | | | |
| 175 | 593.5 | .03160 | 31.65 | (1.29) | (248) | (377) | | | |
| 200 | 794.7 | .03375 | 29.63 | (1.38) | (283) | (332) | | | |
| 250 | 1347 | .0422 | 23.7 | (1.90) | (395) | (192) | | | |

(Abridged from Bur. Standards, Circ. 142, 1923.)

TABLE 295.—Heats of Combustion of Some Carbon Compounds

Given in kg.cal.₁₅ at constant pressure per gram-molecular weight in vacuo. When referred to constant volume the values should be 0.58 kg.cal.₁₅ smaller (at about 18°C) for each condensed gaseous molecule. Combustion products are CO₂, liquid H₂O, etc. Benzoic acid was adopted at Lyons as a primary standard, its heat of combustion, 6324 g.cal.₁₅ per gram in air, 6319 in vacuo. This is tacitly assumed as heat of isothermal combustion at 20°C. In absolute joules, 26,466 and 26,445 respectively. The following ratios may be taken as standard: Naphthalene/benzoic acid = 1.5201 (air); benzoic acid/sucrose = 1.6028 (air); naphthalene/sucrose = 2.4364 (air). The following values are from Kharasch, Bur. Standards, Journ. Res., 2, 359, 1929, which see for further values.

| Compound | Formula | Molecular weight | Kg.cal. ₁₅ per g.mol. | Compound | Formula | Molecular weight | Kg.cal. ₁₅ per g.mol. |
|-------------------------------|---------------------------------|------------------|----------------------------------|--------------------------|---|------------------|----------------------------------|
| Methane (g)..... | CH ₄ | 16 | 216.8 | Formaldehyde (g).... | CH ₂ O | 30.02 | 134.1 |
| Ethane (g)..... | C ₂ H ₆ | 30 | 368.4 | Acetone (v)..... | C ₃ H ₆ O | 58 | 435.8 |
| Propane (g)..... | C ₃ H ₈ | 44 | 526.3 | Camphor (s)..... | C ₁₀ H ₁₆ O | 152.13 | 1411 |
| Isobutane (g)..... | C ₄ H ₁₀ | 58 | 683.4 | Sucrose, cane (s).... | C ₁₂ H ₂₂ O ₁₁ | 342.18 | 1349.6 |
| n-Hexane..... | C ₆ H ₁₄ | 86.11 | 990.6 | " milk (s), | " | " | " |
| n-Heptane..... | C ₇ H ₁₆ | 100.13 | 1143.6 | " anhd..... | " | " | 1350.8 |
| n-Octane..... | C ₈ H ₁₈ | 114.14 | 1304.2 | " malt (s) | " | " | 1351 |
| Decane..... | C ₁₀ H ₂₂ | 142.18 | 1610.2 | Starch..... | | | 4178.8 |
| Hexadecane (s)..... | C ₁₆ H ₃₄ | 226.27 | 2559.1 | Glycogen..... | | | 4186.8 |
| Eicosane (s)..... | C ₂₀ H ₄₂ | 282.34 | 3183.1 | Cellulose..... | | | 4180.8 |
| Ethylene (g)..... | C ₂ H ₄ | 28 | 331.6 | Formic acid..... | CH ₂ O ₂ | 46.02 | 62.8 |
| Propylene (g)..... | C ₃ H ₆ | 42 | 490.2 | Acetic..... | C ₂ H ₄ O ₂ | 60.03 | 208.2 |
| Isobutylene (g)..... | C ₄ H ₈ | 56 | 647.2 | Propionic acid..... | C ₃ H ₆ O ₂ | 74.05 | 367.2 |
| Amylene..... | C ₅ H ₁₀ | 70 | 803.4 | n-butyric "..... | C ₄ H ₈ O ₂ | 88.06 | 524.3 |
| Hexylene..... | C ₆ H ₁₂ | 84.10 | 952.6 | n-valeric "..... | C ₅ H ₁₀ O ₂ | 102.08 | 681.6 |
| Acetylene (g)..... | C ₂ H ₂ | 26.02 | 312.0 | Palmitic " (s)..... | C ₁₆ H ₃₂ O ₂ | 256.20 | 2391 |
| Allylene (g)..... | C ₃ H ₄ | 40 | 409 | Stearic " (s)..... | C ₁₈ H ₃₆ O ₂ | 284.29 | 2706 |
| Trimethylene (g)..... | C ₃ H ₆ | 42 | 496.8 | Lactic " (s)..... | C ₃ H ₄ O ₃ | 90.05 | 326.0 |
| Benzene..... | C ₆ H ₆ | 78.05 | 782.8 | Aniline..... | C ₆ H ₅ N | 93.07 | 813.7 |
| (v)..... | | | 787.2 | Urea (s)..... | CH ₄ N ₂ O | 60.05 | 151.6 |
| Toluene..... | C ₇ H ₈ | 92.06 | 935.6 | Nicotine..... | C ₁₀ H ₁₄ N ₂ | 162.13 | 1427.7 |
| Naphthalene (s)..... | C ₁₀ H ₈ | 128.06 | 1231.4 | Cyanogen (g)..... | C ₂ N ₂ | 52.0 | 266.0 |
| Methyl-chloride (g)..... | CH ₃ Cl | 50.5 | 168.7 | Trinitrotoluene (s)..... | C ₇ H ₅ N ₃ O ₆ | 227.06 | 826 |
| Methylene- (v)..... | CH ₂ Cl ₂ | 85.0 | 166.8 | n-propyl "..... | C ₃ H ₇ O | 60.06 | 482.6 |
| Chloroform (l)..... | CHCl ₃ | 119.5 | 89.2 | n-butyl "..... | C ₄ H ₉ O | 74.08 | 639.4 |
| (v)..... | | | 70.3 | n-heptyl "..... | C ₇ H ₁₅ O | 116.13 | 1104.9 |
| Carbon-tetrachloride (l)..... | CCl ₄ | 154.0 | 37.3 | Octyl "..... | C ₈ H ₁₇ O | 130.14 | 1262.0 |
| Carbon-tetrachloride (v)..... | " | " | " | Cetyl " (s)..... | C ₁₈ H ₃₇ O | 242.27 | 2504.5 |
| Carbon di-sulphide (l)..... | CS ₂ | 76.0 | 394.5 | Menthol (s)..... | C ₁₀ H ₁₈ O | 156.16 | 1508.8 |
| (v)..... | | | 246.6 | Phenol (s)..... | C ₆ H ₅ O | 94.05 | 732.2 |
| Methyl alcohol..... | CH ₄ O | 32.03 | 170.9 | Thymol..... | C ₁₀ H ₁₄ O | 150.11 | 1353.4 |
| Ethyl "..... | C ₂ H ₅ O | 46.05 | 328.5 | Dimethyl ether (g)..... | C ₂ H ₆ O | 46 | 347.6 |
| Allyl "..... | C ₃ H ₅ O | 58.05 | 442.4 | Methylethyl " (v)..... | C ₃ H ₇ O | 60 | 593.4 |
| | | | | Diethyl " (v)..... | C ₄ H ₁₀ O | 74.08 | 660.3 |

TABLE 296.—Heats of Combustion of Miscellaneous Compounds

| Substance. | Small calories per g substance. | Reference. | Substance. | Small calories per g substance. | Reference. |
|--|---------------------------------|------------|---|---------------------------------|------------|
| Asphalt..... | 9530 | 1 | Oils: petroleum: | | |
| Butter..... | 9200 | 1 | crude..... | 11500 | 2 |
| Carbon: amorphous..... | 8080 | 2 | light..... | 10000 | 2 |
| charcoal..... | 8100 | 2 | heavy..... | 10200 | 2 |
| diamond..... | 7860 | 3 | rape..... | 9500 | 6 |
| graphite..... | 7900 | 3 | sperm..... | 10000 | 7 |
| Copper (to CuO)..... | 590 | 5 | Paraffin (to CO ₂ , H ₂ O l)..... | 11140 | 6 |
| Dynamite, 75%..... | 1290 | 4 | Paraffin (to CO ₂ , H ₂ O g)..... | 10340 | 6 |
| Egg, white of..... | 5700 | 1 | Pitch..... | 8400 | 1 |
| Egg, yolk of..... | 8100 | 1 | Sulphur, rhombic..... | 2200 | 2 |
| Fats, animal..... | 9500 | 2 | Sulphur, monoclinic..... | 2240 | 5 |
| Hemoglobin..... | 5900 | 1 | Tallow..... | 9500 | 6 |
| Hydrogen..... | 33900 | 2 | Woods: beech, 13% H ₂ O..... | 4170 | 8 |
| Iron (to Fe ₂ O ₃)..... | 1582 | 1 | birch, 12% H ₂ O..... | 4210 | 8 |
| Magnesium (to MgO)..... | 6080 | 1 | oak, 13% H ₂ O..... | 3900 | 8 |
| Oils: cotton-seed..... | 9500 | 1 | pine, 12% H ₂ O..... | 4420 | 8 |
| lard..... | 9300 | 2 | | | |
| olive..... | 9400 | 2 | | | |

References: (1) Slossen, Colburn; (2) Mean; (3) Berthelot; (4) Roux, Sarrau; (5) Thomsen; (6) Stohmann; (7) Gibson; (8) Gottlieb.

TABLE 297
HEAT VALUES AND ANALYSES OF VARIOUS FUELS

| (a) COALS | | | | | | | | | | | | |
|-------------------------------|-----------|------------------|---------------|-------|----------|-----------|---------|-----------|---------|--------------------|-----------------------|--|
| Coal. | Moisture. | Volatile matter. | Fixed Carbon. | Ash. | Sulphur. | Hydrogen. | Carbon. | Nitrogen. | Oxygen. | Calories per gram. | B. T. U.'s per pound. | |
| Lignite { Low grade. | 38.81 | 35.48 | 27.29 | 8.42 | 0.97 | 7.09 | 37.45 | 0.50 | 45.57 | 3526 | 6347 | |
| Lignite { High grade. | 33.38 | 27.44 | 29.62 | 9.56 | 0.04 | 6.77 | 41.31 | 0.67 | 40.75 | 3904 | 7139 | |
| Sub-bituminous { Low grade. | 22.71 | 34.78 | 36.60 | 5.01 | 0.29 | 6.14 | 52.51 | 1.03 | 34.00 | 5115 | 9207 | |
| Sub-bituminous { High grade. | 15.54 | 33.03 | 46.06 | 5.37 | 0.58 | 5.80 | 60.08 | 1.05 | 27.03 | 8365 | 10557 | |
| Bituminous { Low grade. | 11.44 | 33.93 | 43.92 | 10.71 | 4.94 | 5.39 | 60.06 | 1.02 | 17.88 | 6088 | 10958 | |
| Bituminous { High grade. | 3.42 | 34.36 | 58.83 | 3.39 | 0.58 | 5.25 | 77.98 | 1.20 | 11.51 | 7852 | 14134 | |
| Semi-bituminous { Low grade. | 2.7 | 14.5 | 75.5 | 7.3 | 0.90 | 4.58 | 80.65 | 1.82 | 4.66 | 7845 | 14121 | |
| Semi-bituminous { High grade. | 3.26 | 14.57 | 78.20 | 3.07 | 0.54 | 4.76 | 81.62 | 1.02 | 5.00 | 8166 | 14600 | |
| Semi-anthracite { Low grade. | 2.07 | 9.81 | 78.82 | 9.30 | 1.74 | 3.62 | 80.28 | 1.47 | 3.50 | 7612 | 13702 | |
| Semi-anthracite { High grade. | 2.76 | 2.48 | 82.07 | 12.09 | 0.54 | 2.23 | 79.22 | 0.68 | 4.64 | 6987 | 12577 | |
| Anthracite { Low grade. | 3.33 | 3.27 | 84.28 | 9.12 | 0.60 | 3.08 | 81.35 | 0.70 | 5.06 | 7417 | 13351 | |
| Oven coke { Low grade. | 1.02 | 1.58 | 88.87 | 8.09 | 1.18 | — | — | — | — | 7046 | 14300 | |
| Oven coke { High grade. | 1.14 | 0.04 | 94.66 | 3.57 | 0.69 | — | — | — | — | 8006 | 14410 | |

| (b) PEATS AND WOODS (air dried) | | | | | | | | | | | | |
|---------------------------------|--------------------|---------------|-------|----------|-----------|---------|-----------|---------|--------------------|---------------------|--|--|
| | Vol. hydro-carbon. | Fixed carbon. | Ash. | Sulphur. | Hydrogen. | Carbon. | Nitrogen. | Oxygen. | Calories per gram. | B.T.U.'s per pound. | | |
| Peats: | | | | | | | | | | | | |
| Franklin Co., N. Y. | 67.10 | 28.99 | 3.91 | 0.15 | 5.93 | 57.17 | 1.48 | 31.36 | 5726 | 10397 | | |
| Sawyer Co., Wis. | 50.54 | 27.92 | 15.54 | 0.29 | 4.71 | 51.00 | 1.92 | 26.54 | 4867 | 8761 | | |
| Woods: | | | | | | | | | | | | |
| Oak, dry. | — | — | 0.37 | — | 6.02 | 50.16 | 0.00 | 43.36 | 4620 | 8316 | | |
| Birch, dry. | — | — | 0.29 | — | 6.06 | 48.88 | 0.10 | 44.67 | 4771 | 8388 | | |
| Pine, dry. | — | — | 0.37 | — | 6.20 | 50.31 | 0.04 | 43.08 | 5085 | 9153 | | |

| (c) LIQUID FUELS | | | | | | | | | | | | |
|--|----------------------------|--|--------------------|--|----------------------------------|--|--|--|--|--|--|--|
| Fuel. | Specific gravity at 15° C. | | Calories per gram. | | British thermal units per pound. | | | | | | | |
| Petroleum ether. | .684-.604 | | 12210-12220 | | 21978-21996 | | | | | | | |
| Gasoline. | .710-.730 | | 11100-11400 | | 19980-20520 | | | | | | | |
| Kerosene. | .790-.800 | | 11000-11200 | | 19800-20160 | | | | | | | |
| Fuel oils, heavy petroleum or refinery residue | .960-.970 | | 10200-10500 | | 18360-18900 | | | | | | | |
| Alcohol, fuel or denatured with 7 to 9 per cent water and denaturing material. | .8196-.8202 | | 6440-6470 | | 11592-11646 | | | | | | | |

| (d) GASES | | | | | | | | | | | | |
|--------------------------------|----------------|-----------------|-------------------------------|------------|-----------------|-------|----------------|----------------|-------------------------|--------------------|--|--|
| Gas. | H ₂ | CH ₄ | C ₂ H ₂ | lumi-ants. | CO ₂ | CO | O ₂ | N ₂ | Cal. per m ³ | B.T.U. per cu. ft. | | |
| Natural gas, Cal. | — | 88.0 | — | — | 11.10 | — | — | 0.90 | 8330 | 937 | | |
| Natural gas, Pa. | — | 53.3 | 45.8* | — | — | — | — | 0.90 | 12035 | 1420 | | |
| Natural gas, France. | — | 98.81 | — | — | 0.58 | — | 0.1 | 0.48 | 9364 | 1052 | | |
| Coal gas, high grade. | 34.80 | 28.80 | 9.50 | 1.70 | 0.20 | 10.40 | 0.40 | 14.20 | 6151 | 657 | | |
| Coal gas, low grade. | 57.2 | 18.8 | — | 0.8 | 2.00 | 3.20 | — | 18.0 | 3736 | 390 | | |
| Water gas, low grade. | 52.88 | 2.16 | — | 3.47 | — | 36.8 | — | 4.60 | 2642 | 283 | | |
| Water gas, high grade. | 36.4 | 23.2 | — | 14.05 | 3.02 | 19.1 | 1.15 | 3.08 | 6140 | 657 | | |

* C₂H₂. Data from the Geological Survey, Poole's The Calorific Power of Fuels, and for natural gas from Snelling (Van Nostrand's Chemical Annual).

CHEMICAL AND PHYSICAL PROPERTIES OF FIVE DIFFERENT CLASSES OF EXPLOSIVES

| Explosive. | Specific gravity. | | Number of large calories developed by 1 kilogram of the explosive. | Pressure developed in own volume after elimination of surface influence. | Unit disruptive charge by ballistic pendulum. | Rate of detonation. Cartridges $\frac{1}{4}$ in. diam. | Duration of flame from 100 grams of explosive. | Length of flame from 100 grams. | Cartridge $\frac{1}{4}$ in. transmitted explosion at a distance of | Products of combustion from 200 grams; gaseous, solid, and liquid, respectively. | Ignition occurred in $\frac{1}{4}$ in. fire damp & coal dust mixture with |
|---|-------------------|--------|--|--|---|--|--|---------------------------------|--|--|---|
| | | | | | | | | | | | |
| | | | | Kg per sq. cm. | Grams. | Meters per second. | Milli-seconds. | Inches. | Inches. | Grams. | Grams. |
| (A) Forty-per-cent nitro-glycerin dynamite | 1.22 | 1221.4 | 8235 | 227* | 4688 | .358 | 24.63 | 12 | 88.4 79.7 14.5 | 25 | |
| (B) FFF black blasting powder | 1.25 | 789.4 | 4817 | 374† 458* | 469.1† | 925. | 54.32 | - | 154.4 126.9 4.1 | 25 | |
| (C) Permissible explosive; nitroglycerin class | 1.10 | 760.5 | 5912 | 301* | 3008 | .471 | 27.79 | 4 | 103.9 65.1 15.4 | 1000 | |
| (D) Permissible explosive; ammonium nitrate class | 0.97 | 992.8 | 7300 | 279* | 3438§ | .483 | 25.68 | 1 | 89.8 27.5 75.5 | 800 | |
| (E) Permissible explosive; hydrated class | 1.54 | 610.6 | 6597 | 434* | 2479 | .338 | 17.49 | 3 | 86.1 56.0 33.0 | Over 1000 | |

Chemical Analyses.

| | | | |
|---|-------|---|-------|
| (A) Moisture | 0.91 | (D) Moisture | 0.23 |
| Nitroglycerin | 39.68 | Ammonium nitrate | 83.10 |
| Sodium nitrate | 42.46 | Sulphur | 0.46 |
| Wood pulp | 13.58 | Starch | 2.61 |
| Calcium carbonate | 3.37 | Wood pulp | 1.89 |
| (B) Moisture | 0.80 | Poisonous matter | 2.54 |
| Sodium nitrate | 70.57 | Manganese peroxide | 2.64 |
| Charcoal | 17.74 | Sand | 6.53 |
| Sulphur | 10.89 | (E) Moisture | 2.34 |
| (C) Moisture | 7.89 | Nitroglycerin | 30.85 |
| Nitroglycerin | 24.02 | Ammonium nitrate | 9.94 |
| Sodium nitrate | 36.25 | Sand | 1.75 |
| Wood pulp and crude fibre from grains | 9.20 | Coal | 11.98 |
| Starch | 21.31 | Clay | 7.64 |
| Calcium carbonate | 0.97 | Ammonium sulphate | 8.96 |
| Magnesium " | 0.36 | Zinc sulphate (7H ₂ O) | 6.89 |
| | | Potassium sulphate | 19.65 |

* One pound of clay tamping used.

† Two pounds of clay tamping used.

‡ Rate of burning.

§ Cartridges $\frac{1}{4}$ in. diam.

|| For 300 grammes.

Compiled from U. S. Geological Survey Results, — "Investigation of Explosives for use in Coal Mines, 1909."

TABLE 299.—Additional Data on Explosives

| Explosive. (Ref. Young, Nature, 102, 216, 1918.) | Vol. gas per g in cc = V | Calories per g = Q | Coefficient = $\frac{QV}{1000}$ | Coefficient $GP = 1$ | Calculated Temperature $\frac{Q}{C}$ C, sp. ht. gases = 0.24 |
|---|--------------------------------|--------------------------|------------------------------------|-------------------------|--|
| | cc | | | | |
| Gunpowder..... | 280 | 738 | 207 | 1 | 2240° C |
| Nitroglycerine..... | 741 | 1652 | 1224 | 6 | 6880 |
| Nitrocellulose, 13% N..... | 923 | 931 | 850 | 4.3 | 3876 |
| Cordite, Mk. I (NG, 57; NC, 38; Vaseline, 5)..... | 871 | 1242 | 1082 | 5.2 | 5175 |
| Cordite, MD (NG, 30; NC, 65; Vaseline, 5)..... | 888 | 1031 | 915 | 4.4 | 4225 |
| Ballistite (NG, 50; NC, 50; Stabilizer, 5)..... | 817 | 1349 | 1102 | 5.3 | 5621 |
| Picric acid (Lyddite)..... | 877 | 810 | 710 | 3.4 | 3375 |

Shattering power of explosive = vol. gas per g \times cal./g $\times V_d \times$ density where V_d is the velocity of detonation. Trinitrotoluene: $V_d = 7000$ m/sec. Shattering effect = .87 picric acid.

Amatol (Ammonium nitrate + trinitrotoluene, TNT): $V_d = 4500$ m/sec.

Ammonal (Ammonium nitrate, TNT, Al): 1578 cal/g; 682 cc gas; $V_d = 4000$ m/sec.

Sabulite (Ammonium nitrate, 78, TNT 8, Ca silicide 14): about same as ammonal.

TABLE 300.—Ignition Temperatures of Gaseous Mixtures

Ignition temperature taken as temperature necessary for hot body immersed in gas to cause ignition; slow combination may take place at lower temperatures. McDavid, J. Ch. Soc. Trans. 111, 1003, 1917. Gases were mixed with air. Practically same temperatures as with O_2 (Dixon, Conrad, *loc. cit.* 95, 1900).

| | | | |
|-----------------------|---------|-----------------------|---------|
| Benzene and air..... | 1062° C | Ether and air..... | 1033° C |
| Coal gas and air..... | 878 | Ethylene and air..... | 1000 |
| CO and air..... | 931 | Hydrogen and air..... | 747 |

TABLE 301.—Time of Heating for Explosive Decomposition

| Temperature ° C. | 170 | 180 | 190 | 200 | 220 | Ignition temperature. | |
|--------------------------|------|------|------|------|------|-----------------------|-------|
| Time. | sec. | sec. | sec. | sec. | sec. | ° C † | ° C ‡ |
| Black powder..... | n | n | n | n | n | 440 | — |
| Smokeless powder A..... | 600 | 195 | 130 | 45 | 23 | 300 | — |
| Smokeless powder B..... | 190 | 130 | — | 90 | 23 | — | — |
| Celluloid Pyroxylin..... | 170 | 60 | — | 21 | 9 | — | — |
| Collodion cotton..... | 870 | 165 | 67 | 56 | 18 | 300 | — |
| Celluloid *..... | 160 | 100 | 60 | 50 | 30 | 590 | 450 |
| Safety matches..... | n | 340 | 240 | 150 | 60 | — | — |
| Parlor matches..... | n | n | n | 590 | 480 | — | — |
| Cotton wool..... | — | — | — | — | — | 900 | — |

n, failure to explode in twenty minutes. * The decomposition of nitrocellulose in celluloid commences at about 100° C; above that the heat of decomposition may raise the mass to the ignition point if loss of heat is prevented. Above 170° decomposition occurs with explosive violence as with nitrocellulose. Rate of combustion is 5 to 10 times that of poplar, pine, or paper of the same size and conditions.

† Measured by contact with porcelain tube of given temperature. Average.

‡ Measured by contact with molten lead. Average.

Taken from Technologic Paper of Bureau of Standards, No. 98, 1917.

TABLE 302.—Flame Temperatures

Measures made with optical pyrometer by Féry, J. de Phys. (4) 6, 1907.

| | | | |
|--------------------------------------|---------|-----------------------|---------|
| Alcohol, with NaCl..... | 1705° C | Hydrogen flame..... | 1900° C |
| Bunsen flame, no air..... | 1712 | Hydrogen-oxygen..... | 2420 |
| Bunsen flame, $\frac{1}{2}$ air..... | 1812 | Acetylene burner..... | 2458 |
| Bunsen flame, full air..... | 1871 | Acetylene-oxygen..... | 3000 |
| Illuminating gas-oxygen..... | 2200 | Cooper-Hewitt Hg..... | 3500 |

THERMOCHEMISTRY. CHEMICAL ENERGY DATA

The total heat generated in a chemical reaction is independent of the steps from initial to final state. Heats of formation may therefore be calculated from steps chemically impracticable. Chemical symbols now represent the chemical energy in a gram-molecule or mol(e); treat reaction equations like algebraic equations: $\text{CO} + \text{O} = \text{CO}_2 + 68 \text{ Kg-cal}$; subtract $\text{C} + 2 \text{ O} = \text{CO}_2 + 97 \text{ Kg-cal}$, then $\text{C} + \text{O} = \text{CO} + 29 \text{ Kg-cal}$. We may substitute the negative values of the formation heats in an energy equation and solve $\text{MgCl}_2 + 2 \text{ Na} = 2 \text{ NaCl} + \text{Mg} + x \text{ Kg-cal}$; $-151 = -196 + x$; $x = 45 \text{ Kg-cal}$. Heats of formation of organic compounds can be found from the heats of combustion since burned to H_2O and CO_2 . When changes are at constant volume, energy of external work is negligible; also generally for solid or liquid changes in volume. When a gas forms a solid or liquid at constant pressure, or vice versa, it must be allowed for. For N mols of gas formed (disappearing) at T_K° the energy of the substance is decreased (increased) by $0.002 \cdot N \cdot T_K \text{ Kg-cal}$. $\text{H}_2 + \text{O} = \text{H}_2\text{O} + 67.5 \text{ Kg-cal}$, at 18°C at constant volume; $\frac{1}{2}(2 \text{ H}_2 + \text{O}_2 - 2 \text{ H}_2\text{O} = 135.0 + 0.002 \times 3 \times 291 = 136.7) = 68.4 \text{ Kg-cal}$.

The heat of solution is the heat, + or -, liberated by the solution of 1 mol of substance in so much water that the addition of more water will produce no additional heat effects. Aq. signifies this amount of water; H_2O , one mol.; $\text{NH}_3 + \text{Aq} = \text{NH}_4\text{OH} + \text{Aq} + 8 \text{ Kg-cal}$.

Heats of Formation from Elements in Kilogram-Calories
At ordinary temperatures.

| Compound. | Heat of Formation. | Compound. | Heat of Formation. | Compound. | Heat of Formation. | Compound. | Heat of Formation. |
|------------------------------------|--------------------|------------------------------------|--------------------|---|--------------------|---|--------------------|
| Al_2O_3 | 380. | HgO | 21.4 | KCl | 105.7 | Li_2SO_4 | 334.2 |
| Ag_2O | 6.5 | Na_2O | 100. | LiCl | 93.8 | $(\text{NH}_4)_2\text{SO}_4$ | 283. |
| BaO | 126. | Nd_2O_3 | 435. | MgCl_2 | 151.0 | Na_2SO_4 | 328.3 |
| BaO_2 | 142. | NiO | 57.9 | MnCl_2 | 112.3 | MgSO_4 | 301.6 |
| Bi_2O_3 | 138. | $\text{P}_2\text{O}_5 \text{ sgs}$ | 370. | NaCl | 97.8 | PbSO_4 | 216.2 |
| CO am | 29.0 | PbO | 50.3 | NdCl_3 | 250. | Ti_2SO_4 | 221.0 |
| CO di | 26.1 | PbO_2 | 62.4 | NH_4Cl | 76.3 | ZnSO_4 | 229.6 |
| $\text{CO}_2 \text{ am}$ | 97.0 | Pr_2O_3 | 412. | NiCl_2 | 74.5 | CaCO_3 | 270. |
| $\text{CO}_2 \text{ gr}$ | 94.8 | Rb_2O | 89.2 | PbCl_2 | 83.4 | CuCO_3 | 143. |
| $\text{CO}_2 \text{ di}$ | 94.3 | $\text{SO}_2 \text{ rh sgg}$ | 70. | PdCl_2 | 40.5 | FeCO_3 | 179. |
| CaO | 152. | SiO_2 | 191.0 | PtCl_4 | 60.4 | K_2CO_3 | 280. |
| CeO_2 | 225. | SnO | 66.9 | SnCl_2 | 80.8 | MgCO_3 | 267. |
| $\text{Cl}_2\text{O g}$ | -16.5 | $\text{SnO}_2 \text{ cr}$ | 137.5 | SnCl_4 | 128. | Na_2CO_3 | 272. |
| CoO am | 50.5 | SrO_2 | 135. | SrCl_2 | 185. | ZnCO_3 | 194. |
| CoO cr | 57.5 | ThO_2 | 326. | ThCl_4 | 300. | AgNO_3 | 28.7 |
| Co_3O_4 | 193.4 | $\text{TiO}_2 \text{ am}$ | 215.6 | TiCl_3 | 48.6 | $\text{Ca(NO}_3)_2$ | 209. |
| CrO_3 | 140. | $\text{TiO}_2 \text{ cr}$ | 218.4 | RbCl | 105.9 | $\text{Cu(NO}_3)_2 \cdot \text{H}_2\text{O}$ | 92.9 |
| Cr_2O_3 | 91.3 | TiCl_3 | 42.2 | ZnCl_2 | 97.3 | $\text{HNO}_3 \text{ ggg}$ | 41.6 |
| Cu_2O | 42.3 | WO_2 | 131. | HBr glg | 8.6 | KNO_3 | 119.2 |
| CuO | 37.2 | WO_3 | 194. | NH_4Br | 66. | LiNO_3 | 112. |
| FeO | 65.7 | ZnO | 85.2 | HI gsg | -6.2 | NH_4NO_3 | 88.3 |
| Fe_2O_3 | 196.5 | AgCl | 29.2 | HF ggg | 38. | NaNO_3 | 111.0 |
| Fe_3O_4 | 270.8 | Ag_2Cl | 29.5 | Ag_2S | 3.3 | TiNO_3 | 58.2 |
| $\text{H}_2\text{O ggl}$ | 68.4 | AlCl_3 | 161.4 | $\text{CS}_2 \text{ sgg}$ | -26.0 | $\text{CH}_4 \text{ sgg}$ | 20. |
| $\text{H}_2\text{O}_2 \text{ ggl}$ | 46.8 | AuCl y | 5.81 | CaS | 90.8 | $\text{C}_2\text{H}_6 \text{ sgg}$ | 25. |
| Hg_2O | 22.2 | $\text{AuCl}_3 \text{ y}$ | 22.8 | $(\text{NH}_4)_2\text{S}$ | 66.2 | $\text{C}_2\text{H}_2 \text{ sgg}$ | -53. |
| HgO | 21.4 | BaCl_2 | 197. | Cu_2S | 18.3 | HCN di gsgg | -30.5 |
| K_2O | 91. | BiCl_3 | 90.6 | CuS | 11.6 | $\text{NH}_3 \text{ ggg}$ | 12.0 |
| La_2O_3 | 447. | $\text{CCl}_4 \text{ am}$ | 21.0 | $\text{H}_2\text{S gsg}$ | 2.73 | Ca(OH)_2 | 230. |
| LiO_2 | 141.6 | CaCl_2 | 187. | K_2S | 103.4 | NH_4OH | 88.8 |
| MgO | 143.6 | CdCl_2 | 93.2 | MgS | 79.4 | NaOH | 102. |
| MnO | 90.8 | CoCl_2 | 76.5 | Na_2S | 89.3 | $\text{Na} \cdot \text{H}_2\text{O} \cdot \text{Aq} - \text{H}$ | 44.* |
| MnO_2 | 123. | CuCl_2 | 51.5 | PbS | 19.3 | $\frac{1}{2}(2 \text{ Na} \cdot \text{O} \cdot \text{H}_2\text{O})$ | 68.* |
| Mn_2O_4 | 325. | CuCl | 34.1 | CaSO_4 | 262. | $\frac{1}{3}(\text{Na}_2\text{O} \cdot \text{H}_2\text{O} \cdot \text{Aq})$ | 30.* |
| MoO_2 | 143. | FeCl_2 | 82.1 | CuSO_4 | 111.5 | KOH | 103.5 |
| MoO_3 | 174. | FeCl_3 | 96.0 | $\text{H}_2\text{SO}_4 \text{ sggg}$ | 193. | $\text{K} \cdot \text{H}_2\text{O} \cdot \text{Aq} - \text{H}$ | 45.* |
| $\text{N}_2\text{O ggg}$ | -18.2 | GICl_2 | 155. | $-\text{SO}_3 \cdot \text{H}_2\text{O}^*$ | 21.3 | $\frac{1}{4}(2 \text{ K} \cdot \text{O} \cdot \text{H}_2\text{O})$ | 69.* |
| NO ggg | -21.6 | HCl ggl | 22. | Hg_2SO_4 | 17.5 | $\frac{1}{2}(\text{K}_2\text{O} \cdot \text{H}_2\text{O} \cdot \text{Aq})$ | 35.5* |
| NO_2 | - 8.1 | HgCl | 31.3 | HgSO_4 | 165. | | |
| Na_2O_4 | - 2.6 | HgCl_2 | 53.3 | K_2SO_4 | 344.3 | | |

am = amorphous; di = diamond; gr = graphite; cr = crystal; g = gas; l = liquid; s = solid; y = yellow (gold); rh = rhombic (sulphur). * Heats of formation not from elements but as indicated.

TABLE 304.—Heats of Formation of Ions in Kilogram-Calories

+ and — signs indicate signs of ions and the number of these signs the valency. For the ionization of each gram-molecule of an element divide the numbers in the table by the valency, e. g., 9.03 gr. Al = 9.03 gr. Al⁺ + 40.3 Kg. cal. When a solution is of such dilution that further dilution does not increase its conductivity, then the heats of formation of substances in such solutions may be found as follows: FeCl₂Aq = + 22.2 + 2 × 39.1 = 100.4 Kg. cal. CuSO₄Aq = — 15.8 + 214.0 = 198.2 Kg. cal.

| | | | | | | | |
|----------|---------|---------------------|---------|----------------------|---------|-----------------------------------|---------|
| Ag + | — 25.3 | NH ₄ + | + 32.7 | AsO ₄ — — | + 215.0 | IO ₃ — | + 55.8 |
| Al + + + | + 121.0 | NH ₄ O + | + 37.5 | Br — | + 28.2 | IO ₄ — | + 46.5 |
| Co + + | + 170.0 | Na + | + 57.3 | BrO ₃ — | + 11.2 | OH — | + 54.4 |
| Ca + + | + 133.2 | Ni + + | + 16.0 | CO ₃ — — | + 160.8 | PO ₄ — — — | + 298.0 |
| Cd + + | + 18.4 | Mg + + | + 108.8 | Cl — | + 39.1 | S ₂ O ₃ — — | + 138.6 |
| Cu + + | — 16.0 | Mn + + | + 50.2 | ClO — | + 26.0 | S ₂ O ₆ — — | + 278.2 |
| Cu + | — 15.8? | Pb + + | + 4.0 | ClO ₃ — | + 23.4 | S ₄ O ₆ — — | + 260.8 |
| Fe + + | + 22.2 | Rb + | + 625.0 | ClO ₄ — | — 38.7 | SO ₃ — — | + 151.0 |
| Fe + + + | — 9.3 | Sn + + + | + 3.3 | HCO ₃ — | + 163.0 | SO ₄ — — | + 214.0 |
| H + | 0.0 | Sr + + | + 119.6 | HPO ₂ — | + 143.9 | Se — | — 35.6 |
| Hg + | — 19.8 | Tl + | + 1.7 | HPO ₃ — — | + 229.6 | SeO ₃ — — | + 119.6 |
| K + | + 61.8 | Zn + + | + 35.0 | HPO ₄ — — | + 304.8 | SeO ₄ — — | + 144.8 |
| Li + | + 62.8 | | | HS — | + 1.2 | Te — | — 34.8 |
| | | | | NO ₂ — | + 27.0 | TeO ₃ — — | + 77.0 |
| | | | | NO ₃ — | + 48.9 | TeO ₄ — — | + 98.4 |
| | | | | I — | + 13.1 | S — | — 12.6 |

TABLE 305.—Heats of Neutralization in Kilogram-Calories

The heat generated by the neutralization of an acid by a base is equal, for each gram-molecule of water formed, to 13.7 Kg. cal. plus the heat produced by the amount of un-ionized salt formed, plus the sum of the heats produced in the completion of the ionizations of the acid and the base.

| Base. | HCl·aq | HNO ₃ ·aq | H ₂ SO ₄ ·aq | HCN·aq | CH ₃ COOH·aq | H ₂ ·CO ₃ ·aq |
|--|--------|----------------------|------------------------------------|--------|-------------------------|-------------------------------------|
| KOH · aq | 13.7 | 13.8 | 15.7 | 2.9 | 13.3 | 10.1 |
| NaOH · aq | 13.7 | 13.7 | 15.7 | 2.9 | 13.3 | 10.2 |
| NH ₄ OH · aq | 12.4 | 12.5 | 14.5 | 1.3 | 12.0 | 8. |
| $\frac{1}{2}$ Ca(OH) ₂ · aq | 14.0 | 13.9 | 15.6 | 3.2 | 13.4 | 9.5 |
| $\frac{1}{2}$ Zn(OH) ₂ · aq | 9.9 | 9.9 | 11.7 | 8.1 | 8.9 | 5.5 |
| $\frac{1}{2}$ Cu(OH) ₂ · aq | 7.5 | 7.5 | 9.2 | — | 6.2 | — |

TABLE 306.—Heats of Dilution of H₂SO₄

In Kilogram-calories by the dilution of one gram-molecule of sulphuric acid by m gram-molecules of water.

| | | | | | | | | | | |
|--------------|------|------|-------|-------|-------|-------|-------|-------|-------|-------|
| m | 1 | 2 | 3 | 5 | 19 | 49 | 99 | 199 | 399 | 1599 |
| Kg. Cal. . . | 6.38 | 9.42 | 11.14 | 13.11 | 16.26 | 16.68 | 16.86 | 17.06 | 17.31 | 17.86 |

TABLE 307.—Radiation Constants and Formulae for Black Body

The radiation per cm^2 from a "black body" (exclusive of convection losses) at the temperature $T^\circ \text{K.}$ (Centigrade degrees) to one at $T_0^\circ \text{K.}$ is $J = \sigma (T^4 - T_0^4)$, (Stefan, Boltzman) where $\sigma = 2\pi^5 k^4 / 15 c^2 h^3 = (5.713 \pm 0.006) \times 10^{-5} \text{ erg-cm}^2 \cdot \text{deg}^{-4} \text{ sec}^{-1}$ (Birge) (indirect) $= (5.735 \pm 0.011) \times 10^{-5} \text{ erg-cm}^2 \cdot \text{deg}^{-4} \text{ sec}^{-1}$ (Birge) (experimental).

The distribution of this energy in the spectrum is represented by Planck's formula:

$$J_{\lambda} = c_1 \lambda^{-5} (e^{\frac{c_2}{\lambda T}} - 1)^{-1} d\lambda$$

where J_λ represents the intensity at wave length λ

* $c_1 = (3.697 \pm 0.005) \times 10^{-5} \text{ erg}\cdot\text{cm}^2\cdot\text{sec}^{-1}$, unpolarized radiation over solid angle 2π .

$$= (3.194 \pm 0.004) \text{ erg} \cdot \text{cm}^2 \cdot \text{day}^{-1}$$

$$= (8.832 \pm 0.01) \times 10^{-13} \text{ g cal.}_{15} \text{ cm}^2 \cdot \text{deg.}$$

$$= (3.697 \pm 0.005) \times 10^{-12} \text{ watts}\cdot\text{cm}^2$$

$$c_2 = (1.432 \pm 0.003) \text{ cm} \cdot \text{deg.}$$

$$J_{\text{max.}} = 3.11 \times 10^{-6} T^5$$

$$\lambda_{\max} T = c_2/4.9651 = (0.28836 \pm 0.00011) \text{ cm} \cdot \text{deg.}$$

* $c_1 = 2\pi hc^2 = 3.697 \times 10^{-5}$ erg-cm²-sec.⁻¹ when E_λ denotes the emission of unpolarized radiation in range $d\lambda$, per unit surface in all directions (2π solid angle).

$c_1 = 8\pi\hbar c = 4.932 \times 10^{-15} \text{ cm} \cdot \text{deg.}$, when $E_\lambda d\lambda$ denotes energy density of unpolarized radiation.

$c_1 = hc^2 = 0.5884 \times 10^{-5} \text{ erg}\cdot\text{cm}^2\cdot\text{sec}^{-1}$, when $E_\lambda d\lambda$ denotes intensity of linearly polarized radiation in range $d\lambda$, perpendicularly to a surface, per unit surface, per unit solid angle.

TABLE 308.—Radiation in ergs ($R \times 10^n$) and gram-calories ($R^1 \times 10^n$) per cm² per sec. from a perfect radiator at $t^\circ\text{C}$ to absolutely cold space (-273°C)

Computed from Stefan-Boltzman formula, $\sigma = 5.73 \times 10^{-5}$ erg. cm.⁻²deg.⁻⁴

| Temp. °C | erg/cm ² / sec. | | cal./cm ² / sec. | | Temp. °C | erg/cm ² / sec. | | cal./cm ² / sec. | | Temp. °C | erg/cm ² / sec. | | cal./cm ² / sec. | |
|-------------|-------------------------------|----|--------------------------------|-----|-------------|-------------------------------|---|--------------------------------|----|-------------|-------------------------------|----|--------------------------------|----|
| | R | n | R ¹ | n | | R | n | R ¹ | n | | R | n | R ¹ | n |
| -270 | 5.29 | -3 | 1.27 | -10 | 4 | 3.38 | 5 | 8.11 | -3 | 58 | 6.89 | 5 | 1.65 | -2 |
| -250 | 1.61 | 1 | 3.86 | -7 | 6 | 3.48 | 5 | 8.35 | -3 | 60 | 7.05 | 5 | 1.69 | -2 |
| -200 | 1.64 | 3 | 3.94 | -5 | 8 | 3.58 | 5 | 8.59 | -3 | 70 | 7.94 | 5 | 1.91 | -2 |
| -190 | 2.73 | 3 | 6.55 | -5 | 10 | 3.68 | 5 | 8.83 | -3 | 80 | 8.91 | 5 | 2.14 | -2 |
| -180 | 4.31 | 3 | 1.03 | -4 | 12 | 3.78 | 5 | 9.07 | -3 | 90 | 9.96 | 5 | 2.39 | -2 |
| -160 | 9.37 | 3 | 2.25 | -4 | 14 | 3.89 | 5 | 9.33 | -3 | 100 | 1.11 | 6 | 2.66 | -2 |
| -150 | 1.31 | 4 | 3.14 | -4 | 16 | 4.00 | 5 | 9.60 | -3 | 200 | 2.87 | 6 | 6.89 | -2 |
| -140 | 1.82 | 4 | 4.37 | -4 | 18 | 4.11 | 5 | 9.86 | -3 | 300 | 6.18 | 6 | 1.48 | -1 |
| -130 | 2.40 | 4 | 5.76 | -4 | 20 | 4.22 | 5 | 1.01 | -2 | 400 | 1.18 | 7 | 2.83 | -1 |
| -120 | 3.15 | 4 | 7.56 | -4 | 22 | 4.34 | 5 | 1.04 | -2 | 500 | 2.05 | 7 | 4.92 | -1 |
| -110 | 4.05 | 4 | 9.72 | -4 | 24 | 4.46 | 5 | 1.07 | -2 | 600 | 3.33 | 7 | 7.99 | -1 |
| -100 | 5.15 | 4 | 1.24 | -3 | 26 | 4.59 | 5 | 1.10 | -2 | 700 | 5.14 | 7 | 1.23 | 0 |
| -90 | 6.44 | 4 | 1.55 | -3 | 28 | 4.71 | 5 | 1.13 | -2 | 800 | 7.60 | 7 | 1.82 | 0 |
| -80 | 7.97 | 4 | 1.91 | -3 | 30 | 4.84 | 5 | 1.16 | -2 | 900 | 1.11 | 8 | 2.66 | 0 |
| -70 | 9.74 | 4 | 2.34 | -3 | 32 | 4.96 | 5 | 1.19 | -2 | 1000 | 1.50 | 8 | 3.60 | 0 |
| -60 | 1.18 | 5 | 2.83 | -3 | 34 | 5.10 | 5 | 1.22 | -2 | 1500 | 5.66 | 8 | 1.36 | +1 |
| -50 | 1.42 | 5 | 3.41 | -3 | 36 | 5.23 | 5 | 1.26 | -2 | 2000 | 1.53 | 9 | 3.67 | +1 |
| -40 | 1.69 | 5 | 4.06 | -3 | 38 | 5.37 | 5 | 1.29 | -2 | 3000 | 6.57 | 9 | 1.58 | +2 |
| -30 | 2.00 | 5 | 4.80 | -3 | 40 | 5.51 | 5 | 1.32 | -2 | 4000 | 1.91 | 10 | 4.58 | +2 |
| -20 | 2.35 | 5 | 5.64 | -3 | 42 | 5.65 | 5 | 1.36 | -2 | 5000 | 4.43 | 10 | 1.06 | +3 |
| -10 | 2.74 | 5 | 6.58 | -3 | 44 | 5.79 | 5 | 1.39 | -2 | 6000 | 8.87 | 10 | 2.13 | +3 |
| -8 | 2.83 | 5 | 6.79 | -3 | 46 | 5.94 | 5 | 1.42 | -2 | 7000 | 1.63 | 11 | 3.91 | +3 |
| -6 | 2.92 | 5 | 7.01 | -3 | 48 | 6.09 | 5 | 1.46 | -2 | 8000 | 2.68 | 11 | 6.43 | +3 |
| -4 | 3.00 | 5 | 7.20 | -3 | 50 | 6.24 | 5 | 1.50 | -2 | 9000 | 4.24 | 11 | 1.02 | +4 |
| -2 | 3.09 | 5 | 7.42 | -3 | 52 | 6.40 | 5 | 1.54 | -2 | 10000 | 6.38 | 11 | 1.53 | +4 |
| 0 | 3.19 | 5 | 7.66 | -3 | 54 | 6.56 | 5 | 1.57 | -2 | 15000 | 3.12 | 12 | 7.49 | +4 |
| +2 | 3.28 | 5 | 7.87 | -3 | 56 | 6.72 | 5 | 1.61 | -2 | 20000 | 9.68 | 12 | 2.32 | +5 |
| | | | | | | | | | | 25000 | 2.34 | 13 | 5.62 | +5 |

NOTE: Above table correct probably to one per cent.

BLACK-BODY SPECTRUM INTENSITIES (J_λ), 50° TO 20000° K.

Values of J_λ using for C_1 , 0.23×10^3 , C_2 , 14350, λ in μ . If the figures given for J_λ are plotted in cms as ordinates to a scale of abscissae of 1 cm to 1 μ , then the area in cm^2 between the smooth curve through the resulting points and the axis of abscissae is equivalent to the radiation in calories per sec. from 1 cm^2 of a black body at the corresponding temperature, radiating to absolute zero. The intensities when radiating to a body at a lower temperature may be obtained by subtracting the intensities corresponding to the lower temperature from those of the higher. The nature of the black-body formula is such that when λT is small, a small change in C_2 produces a great change in J_λ ; e.g., when $C_2/\lambda T$ is 100 or 10, the change is 100 and 10 fold respectively; as λT increases, the change becomes proportional; e.g., when $C_2/\lambda T$ is less than 0.05, the change in J_λ is proportional to the change in C_2 .

| λ | 50° K. | 100° K. | 150° K. | 200° K. | 250° K. | 273° K. | 300° K. | 373° K. | 400° K. | 500° K. | 600° K. |
|-----------|--------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| μ | | | | | | | | | | | |
| 1.0 | — | .0083 | .0372 | .026 | .0201 | .0181 | .0161 | .0122 | .01124 | .0831 | .0638 |
| 1.5 | — | .0383 | .0242 | .0172 | .0133 | .0127 | .0102 | .008 | .00749 | .0058 | .00443 |
| 2.0 | .0091 | .0282 | .0185 | .0137 | .011 | .0111 | .00712 | .00513 | .0046 | .00168 | .00184 |
| 2.5 | .0471 | .0221 | .0142 | .0103 | .0110 | .017 | .0646 | .0419 | .0450 | .0397 | .0066 |
| 3.0 | .0409 | .0196 | .0125 | .0082 | .0618 | .069 | .0445 | .03102 | .03242 | .00265 | .0131 |
| 3.5 | .0344 | .0163 | .0102 | .0072 | .0613 | .055 | .0420 | .0329 | .03620 | .00482 | .0189 |
| 4.0 | .0306 | .0142 | .0094 | .0084 | .0052 | .0418 | .0457 | .0360 | .00115 | .00600 | .0220 |
| 5.0 | .0243 | .0111 | .0074 | .0057 | .0430 | .048 | .0321 | .00134 | .00226 | .00952 | .0240 |
| 6.0 | .02019 | .0105 | .0064 | .005 | .048 | .0318 | .0341 | .00195 | .00301 | .01001 | .0224 |
| 7.0 | .01883 | .009 | .006 | .0049 | .0315 | .0330 | .0359 | .00225 | .00328 | .00925 | .0186 |
| 8.0 | .01672 | .0085 | .0058 | .0036 | .0322 | .0339 | .0371 | .00232 | .00321 | .00801 | .0149 |
| 9.0 | .01422 | .00718 | .0038 | .00454 | .0327 | .0345 | .0377 | .00220 | .00395 | .00672 | .0118 |
| 10.0 | .01331 | .00754 | .00695 | .0471 | .0330 | .0348 | .0378 | .00201 | .00262 | .00554 | .00020 |
| 12.0 | .01115 | .00624 | .0043 | .00404 | .0331 | .0347 | .0370 | .00157 | .00166 | .00374 | .00585 |
| 14.0 | .01021 | .0061 | .0048 | .00402 | .0329 | .0341 | .0358 | .00117 | .00144 | .00254 | .00380 |
| 16.0 | .00914 | .00511 | .00422 | .00400 | .0325 | .0334 | .0346 | .00087 | .00105 | .00176 | .00254 |
| 18.0 | .00957 | .00517 | .00424 | .00402 | .0321 | .0328 | .03368 | .00053 | .00060 | .00124 | .00176 |
| 20.0 | .00916 | .00522 | .00424 | .00402 | .0317 | .03224 | .03290 | .000493 | .000575 | .000902 | .00125 |
| 25.0 | .0007 | .0030 | .0021 | .0057 | .00122 | .00131 | .00164 | .00258 | .00295 | .00430 | .00580 |
| 30.0 | .0036 | .0032 | .0016 | .0038 | .006 | .0079 | .009 | .00146 | .00164 | .00237 | .00311 |
| 40.0 | .0069 | .0036 | .009 | .0018 | .00282 | .0033 | .00391 | .00058 | .00060 | .00085 | .00110 |
| 50.0 | .0095 | .0018 | .0051 | .0062 | .00450 | .00458 | .00484 | .00255 | .00281 | .00481 | .00482 |
| 75.0 | .0087 | .0067 | .0015 | .0024 | .00338 | .00383 | .00436 | .00580 | .00634 | .00834 | .00103 |
| 100.0 | .0055 | .0020 | .0057 | .0088 | .00119 | .00134 | .00150 | .00197 | .00214 | .00277 | .00342 |

| λ | 800° K. | 1000° K. | 1500° K. | 2000° K. | 3000° K. | 4000° K. | 5000° K. | 6000° K. | 8000° K. | 10000° K. | 20000° K. |
|-----------|---------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|-----------|
| μ | | | | | | | | | | | |
| 0.1 | — | — | — | .0.026 | .0.0115 | .0.0624 | .0.0331 | .0.038 | 15. | 510. | 710000. |
| 0.2 | — | — | — | .0.097 | .0.0012 | .0.46 | 15.4 | 184. | 3660. | 22100. | 820000. |
| 0.3 | — | — | — | .0.0315 | .0.44 | 24.2 | 263. | 1370. | 9640. | 31000. | 382000. |
| 0.4 | — | — | — | .0.0145 | 5.75 | 115. | 690. | 2280. | 10300. | 25600. | 180000. |
| 0.5 | — | — | — | .0.172 | 20.6 | 226. | 952. | 2490. | 8400. | 17800. | 92300. |
| 0.6 | — | .0648 | .0.014 | .0.757 | 40.8 | 301. | 1000. | 2240. | 6290. | 11950. | 51460. |
| 0.7 | .0640 | .0468 | .0.064 | 1.93 | 59.2 | 328. | 925. | 1800. | 4590. | 8110. | 30700. |
| 0.8 | .0651 | .00015 | .0.180 | 3.58 | 71.5 | 321. | 800. | 1490. | 3350. | 5620. | 19400. |
| 0.9 | .0434 | .00183 | .0.378 | 5.35 | 77.3 | 295. | 671. | 1177. | 2470. | 3980. | 12820. |
| 1.0 | .00015 | .00538 | .0.645 | 7.06 | 77.8 | 262. | 554. | 928. | 1842. | 2880. | 8800. |
| 1.5 | .00775 | .0848 | 2.07 | 10.25 | 52.2 | 122. | 210. | 309. | 527. | 758. | 1980. |
| 2.0 | .0367 | .221 | 2.43 | 8.10 | 20.0 | 57.6 | 90.2 | 125. | 198. | 275. | 668. |
| 2.5 | .0710 | .305 | 2.10 | 5.68 | 16.4 | 29.5 | 43.9 | 58.9 | 90.1 | 121.9 | 281. |
| 3.0 | .0604 | .320 | 1.64 | 3.82 | 9.66 | 16.4 | 23.7 | 31.1 | 46.4 | 61.9 | 140.7 |
| 3.5 | .1050 | .296 | 1.22 | 2.60 | 6.02 | 9.84 | 13.8 | 17.9 | 26.3 | 34.7 | 77.3 |
| 4.0 | .1027 | .256 | .0.007 | 1.80 | 3.90 | 6.20 | 8.50 | 11.0 | 15.9 | 20.9 | 45.9 |
| 5.0 | .0830 | .178 | .0.511 | .0.023 | 1.84 | 2.81 | 3.81 | 4.81 | 6.84 | 8.80 | 19.15 |
| 6.0 | .0620 | .110 | .0.302 | .0.514 | .0.073 | 1.45 | 1.035 | 2.42 | 3.40 | 4.39 | 9.34 |
| 7.0 | .0450 | .0811 | .0.188 | .0.307 | .0.560 | .0.820 | 1.105 | 1.348 | 1.88 | 2.41 | 5.00 |
| 8.0 | .0335 | .0562 | .0.122 | .0.194 | .0.344 | .0.498 | .0.653 | 0.808 | 1.20 | 1.43 | 3.00 |
| 9.0 | .0247 | .0308 | .0.0824 | .0.128 | .0.223 | .0.319 | .0.416 | .0.513 | .0.709 | .0.90 | 1.87 |
| 10.0 | .0184 | .0288 | .0.0575 | .0.0880 | .0.151 | .0.214 | .0.278 | .0.342 | .0.470 | .0.598 | 1.24 |
| 12.0 | .01072 | .0160 | .0.0304 | .0.0553 | .0.0757 | .0.107 | .0.1373 | .0.168 | .0.230 | .0.292 | .0.602 |
| 14.0 | .00600 | .0090 | .0.0175 | .0.0256 | .0.0421 | .0.0587 | .0.0754 | .0.0921 | .0.125 | .0.159 | .0.326 |
| 16.0 | .00425 | .00060 | .0.0108 | .0.0155 | .0.0253 | .0.0350 | .0.0448 | .0.0546 | .0.0742 | .0.0938 | .0.192 |
| 18.0 | .00285 | .00400 | .0.00697 | .0.00907 | .0.0160 | .0.0221 | .0.0282 | .0.0344 | .0.0466 | .0.0585 | .0.120 |
| 20.0 | .00198 | .00275 | .0.00470 | .0.00668 | .0.01068 | .0.0147 | .0.01868 | .0.0227 | .0.0307 | .0.0388 | .0.0780 |
| 25.0 | .00090 | .00122 | .0.00203 | .0.00284 | .0.00448 | .0.00612 | .0.00777 | .0.00941 | .0.0127 | .0.0160 | .0.0325 |
| 30.0 | .00464 | .00610 | .0.00101 | .0.00141 | .0.00220 | .0.00290 | .0.00378 | .0.00455 | .0.00616 | .0.00775 | .0.0157 |
| 40.0 | .00159 | .00200 | .0.00344 | .0.00459 | .0.00710 | .0.00960 | .0.0121 | .0.0146 | .0.0167 | .0.0247 | .0.00408 |
| 50.0 | .00684 | .00888 | .0.00140 | .0.00191 | .0.00204 | .0.00307 | .0.00400 | .0.00603 | .0.00808 | .0.0101 | .0.00204 |
| 75.0 | .00444 | .00484 | .0.00286 | .0.00387 | .0.00501 | .0.00794 | .0.00907 | .0.0120 | .0.0161 | .0.0201 | .0.0046 |
| 100.0 | .00470 | .00598 | .0.00910 | .0.0124 | .0.0188 | .0.0252 | .0.0317 | .0.04381 | .0.04510 | .0.06030 | .0.0128 |

See Forsythe, J. Opt. Soc., 4, 331, 1920, relative values, 0.4 to 0.76 μ (steps 0.01 μ), 12 temperatures, 1000 to 5000° K.

TABLE 310
BLACK-BODY SPECTRUM INTENSITIES

(J_λ) , 25° to 600°K.

Values computed by editor using for C_1 , 3.703×10^{-5} erg·cm²·sec.⁻¹, C_2 1.433 cm·°K,
 J_λ = tabular $J_\lambda \times 10^n$.

| λ | 25°K. | | 15°K. | | 75°K. | | 100°K. | | 150°K. | | 200°K. | | 250°K. | | 273°K. | |
|-----------|-------------|------|-------------|------|-------------|-----|-------------|-----|-------------|-----|-------------|-----|-------------|-----|-------------|-----|
| | J_λ | n | J_λ | n | J_λ | n | J_λ | n | J_λ | n | J_λ | n | J_λ | n | J_λ | n |
| 1.0 | 3.7 | -234 | 1.3 | -109 | 4.1 | -68 | 2.2 | -47 | 1.2 | -26 | 2.8 | -16 | 4.7 | -10 | 5.9 | -8 |
| 1.5 | 4.9 | -152 | 4.9 | -69 | 2.3 | -41 | 1.6 | -27 | 1.1 | -13 | 8.8 | -7 | 1.23 | -2 | 3.1 | -1 |
| 2.0 | 3.9 | -111 | 6.8 | -49 | 3.8 | -28 | 8.8 | -18 | 2.1 | -7 | 3.2 | -2 | 4.2 | 1 | 4.6 | 2 |
| 2.5 | 9.9 | -87 | 6.4 | -37 | 2.4 | -20 | 4.8 | -12 | 9.6 | -4 | 1.36 | 1 | 4.2 | 3 | 2.88 | 4 |
| 3.0 | 1.6 | -70 | 5.0 | -29 | 3.3 | -15 | 2.7 | -8 | 2.26 | -1 | 6.5 | 2 | 7.7 | 4 | 3.84 | 5 |
| 3.5 | 5.1 | -59 | 1.9 | -23 | 1.4 | -11 | 1.17 | -5 | 9.8 | 0 | 9.1 | 3 | 5.4 | 5 | 2.16 | 6 |
| 4 | 2.1 | -50 | 2.8 | -19 | 6.5 | -9 | 1.00 | -3 | 1.54 | 2 | 6.0 | 4 | 2.16 | 6 | 7.2 | 6 |
| 5 | 1.9 | -38 | 1.5 | -13 | 3.0 | -5 | 4.2 | -1 | 5.9 | 3 | 7.1 | 5 | 1.25 | 7 | 3.26 | 7 |
| 6 | 1.6 | -30 | 8.6 | -10 | 7.1 | -3 | 2.03 | 1 | 5.8 | 4 | 3.11 | 6 | 3.38 | 7 | 7.56 | 7 |
| 7 | 6.1 | -25 | 3.7 | -7 | 3.1 | -1 | 2.84 | 2 | 2.60 | 5 | 7.87 | 6 | 6.13 | 7 | 1.22 | 8 |
| 8 | 8.6 | -21 | 3.1 | -5 | 4.8 | 0 | 1.88 | 3 | 7.4 | 5 | 1.46 | 7 | 8.75 | 7 | 1.60 | 8 |
| 9 | 1.4 | -17 | 9.3 | -4 | 3.8 | 1 | 7.6 | 3 | 1.55 | 6 | 2.19 | 7 | 1.08 | 8 | 1.84 | 8 |
| 10 | 4.7 | -15 | 1.32 | -2 | 1.87 | 2 | 2.21 | 4 | 2.63 | 6 | 2.87 | 7 | 1.20 | 8 | 1.96 | 8 |
| 12 | 2.7 | -11 | 6.3 | -1 | 1.81 | 3 | 9.7 | 4 | 5.20 | 6 | 3.81 | 7 | 1.26 | 8 | 1.90 | 8 |
| 14 | 1.1 | -8 | 8.9 | 0 | 8.1 | 3 | 2.46 | 5 | 7.50 | 6 | 4.15 | 7 | 1.16 | 8 | 1.66 | 8 |
| 16 | 9.8 | -7 | 5.9 | 1 | 2.30 | 4 | 4.56 | 5 | 9.02 | 6 | 4.06 | 7 | 1.01 | 8 | 1.38 | 8 |
| 18 | 2.90 | -5 | 2.39 | 2 | 4.84 | 4 | 6.84 | 5 | 9.76 | 6 | 3.73 | 7 | 8.47 | 7 | 1.12 | 8 |
| 20 | 4.14 | -4 | 6.9 | 2 | 8.2 | 4 | 8.95 | 5 | 9.83 | 6 | 3.31 | 7 | 6.99 | 7 | 9.04 | 7 |
| 25 | 4.18 | -2 | 4.00 | 3 | 1.82 | 5 | 1.23 | 6 | 8.49 | 6 | 2.28 | 7 | 4.26 | 7 | 5.29 | 7 |
| 30 | 7.68 | -1 | 1.08 | 4 | 2.62 | 5 | 1.30 | 6 | 6.58 | 6 | 1.52 | 7 | 2.65 | 7 | 3.21 | 7 |
| 40 | 2.16 | 1 | 2.80 | 4 | 3.07 | 5 | 1.04 | 6 | 3.62 | 6 | 7.24 | 6 | 1.13 | 7 | 1.33 | 7 |
| 50 | 1.25 | 2 | 3.85 | 4 | 2.65 | 5 | 7.15 | 5 | 2.06 | 6 | 3.71 | 6 | 5.52 | 6 | 6.38 | 6 |
| 75 | 7.5 | 2 | 3.50 | 4 | 1.32 | 5 | 2.71 | 5 | 6.06 | 5 | 9.77 | 5 | 1.36 | 6 | 1.54 | 6 |
| 100 | 1.20 | 3 | 2.24 | 4 | 6.43 | 4 | 1.16 | 5 | 2.32 | 5 | 3.54 | 5 | 4.78 | 5 | 5.37 | 5 |

| λ | 275°K. | | 300°K. | | 350°K. | | 373°K. | | 400°K. | | 500°K. | | 600°K. | |
|-----------|-------------|-----|-------------|-----|-------------|-----|-------------|-----|-------------|-----|-------------|-----|-------------|-----|
| | J_λ | n | J_λ | n | J_λ | n | J_λ | n | J_λ | n | J_λ | n | J_λ | n |
| 1.0 | 8.8 | -8 | 6.7 | -6 | 6.1 | -3 | 7.6 | -2 | 1.03 | -1 | 1.32 | 3 | 1.58 | 5 |
| 1.5 | 4.0 | -1 | 7.2 | 0 | 6.8 | 2 | 3.7 | 3 | 2.08 | 4 | 2.46 | 6 | 5.94 | 7 |
| 2.0 | 5.6 | 2 | 4.9 | 3 | 1.51 | 5 | 5.3 | 5 | 1.93 | 6 | 6.92 | 7 | 7.55 | 8 |
| 2.5 | 3.37 | 4 | 1.91 | 5 | 2.92 | 6 | 8.0 | 6 | 2.27 | 7 | 4.00 | 8 | 2.69 | 9 |
| 3.0 | 4.36 | 5 | 1.86 | 6 | 1.80 | 7 | 4.16 | 7 | 9.94 | 7 | 1.08 | 9 | 5.32 | 9 |
| 3.5 | 2.41 | 6 | 8.3 | 6 | 5.85 | 7 | 1.20 | 8 | 2.52 | 8 | 1.96 | 9 | 7.68 | 9 |
| 4 | 7.9 | 6 | 2.36 | 7 | 1.30 | 8 | 2.44 | 8 | 4.66 | 8 | 2.80 | 9 | 9.25 | 9 |
| 5 | 3.54 | 7 | 8.4 | 7 | 3.30 | 8 | 5.45 | 8 | 9.17 | 8 | 3.85 | 9 | 1.01 | 10 |
| 6 | 8.05 | 7 | 1.66 | 8 | 5.19 | 8 | 7.90 | 8 | 1.22 | 9 | 4.04 | 9 | 9.07 | 9 |
| 7 | 1.29 | 8 | 2.40 | 8 | 6.37 | 8 | 9.15 | 8 | 1.33 | 9 | 3.73 | 9 | 7.51 | 9 |
| 8 | 1.68 | 8 | 2.89 | 8 | 6.81 | 8 | 9.36 | 8 | 1.30 | 9 | 3.23 | 9 | 6.01 | 9 |
| 9 | 1.92 | 8 | 3.12 | 8 | 6.70 | 8 | 8.90 | 8 | 1.19 | 9 | 2.71 | 9 | 4.75 | 9 |
| 10 | 2.03 | 8 | 3.14 | 8 | 6.28 | 8 | 8.12 | 8 | 1.06 | 9 | 2.24 | 9 | 3.71 | 9 |
| 12 | 1.96 | 8 | 2.83 | 8 | 5.07 | 8 | 6.32 | 8 | 7.92 | 8 | 1.49 | 9 | 2.36 | 9 |
| 14 | 1.70 | 8 | 2.35 | 8 | 3.90 | 8 | 4.73 | 8 | 5.78 | 8 | 1.02 | 9 | 1.53 | 9 |
| 16 | 1.41 | 8 | 1.88 | 8 | 2.96 | 8 | 3.52 | 8 | 4.22 | 8 | 7.07 | 8 | 1.02 | 9 |
| 18 | 1.15 | 8 | 1.48 | 8 | 2.25 | 8 | 2.63 | 8 | 3.10 | 8 | 5.01 | 8 | 7.08 | 8 |
| 20 | 9.24 | 7 | 1.16 | 8 | 1.72 | 8 | 1.99 | 8 | 2.32 | 8 | 3.62 | 8 | 5.03 | 8 |
| 25 | 5.39 | 7 | 6.59 | 7 | 9.15 | 7 | 1.04 | 8 | 1.19 | 8 | 1.77 | 8 | 2.37 | 8 |
| 30 | 3.26 | 7 | 3.89 | 7 | 5.23 | 7 | 5.86 | 7 | 6.63 | 7 | 9.53 | 7 | 1.25 | 8 |
| 40 | 1.35 | 7 | 1.57 | 7 | 2.03 | 7 | 2.24 | 7 | 2.50 | 7 | 3.45 | 7 | 4.43 | 7 |
| 50 | 6.46 | 6 | 7.41 | 6 | 9.35 | 6 | 1.02 | 7 | 1.13 | 7 | 1.53 | 7 | 1.94 | 7 |
| 75 | 1.56 | 6 | 1.75 | 6 | 2.15 | 6 | 2.34 | 6 | 2.55 | 6 | 3.36 | 6 | 4.17 | 6 |
| 100 | 5.42 | 5 | 6.05 | 5 | 7.32 | 5 | 7.91 | 5 | 8.60 | 5 | 1.12 | 6 | 1.37 | 6 |

BLACK-BODY SPECTRUM INTENSITIES

 $(J\lambda)$, 800° to 25000°K.

(Same origin and data as Table 310.)

| λ | 800°K. $J\lambda$ n | 1000°K. $J\lambda$ n | 1200°K. $J\lambda$ n | 1400°K. $J\lambda$ n | 1600°K. $J\lambda$ n | 1800°K. $J\lambda$ n | 2000°K. $J\lambda$ n | 2200°K. $J\lambda$ n |
|-----------|---------------------------|---------------------------|---------------------------|---------------------------|----------------------------|----------------------------|----------------------------|----------------------------|
| 0.10 | 6 -58 | 2.1 -42 | 5.1 -32 | 1.3 -24 | 4.7 -19 | 1.0 -14 | 2.8 -11 | 1.9 -8 |
| .20 | 1.5 -20 | 9 -13 | 1.4 -7 | 6.9 -4 | 4.1 -1 | 6.0 1 | 3.2 3 | 8.3 4 |
| .30 | 1.8 -8 | 2.7 -3 | 7.9 0 | 2.3 3 | 1.65 5 | 4.5 6 | 6.5 7 | 5.7 8 |
| .40 | 1.28 -2 | 1 | 3.9 4 | 2.8 6 | 6.8 7 | 8.2 8 | 6.0 9 | 3.08 10 |
| .45 | 1.04 0 | 3 3 | 6.0 5 | 2.67 7 | 4.6 8 | 4.17 9 | 2.45 10 | 1.04 11 |
| .50 | 3.3 1 | 4.2 4 | 5.0 6 | 1.53 8 | 1.97 9 | 1.44 10 | 7.1 10 | 2.60 11 |
| .55 | 5.3 2 | 3.50 5 | 2.74 7 | 6.1 8 | 6.3 9 | 3.80 10 | 1.62 11 | 5.30 11 |
| .60 | 5.2 3 | 2.02 6 | 1.08 8 | 1.86 9 | 1.56 10 | 8.2 10 | 3.10 11 | 9.2 11 |
| .65 | 3.44 4 | 8.5 6 | 3.36 8 | 4.61 9 | 3.31 10 | 1.53 11 | 5.21 11 | 1.42 12 |
| .70 | 1.69 5 | 2.84 7 | 8.6 8 | 9.9 9 | 6.1 10 | 2.53 11 | 7.91 11 | 2.00 12 |
| .75 | 6.6 5 | 7.9 7 | 1.90 9 | 1.84 10 | 1.02 11 | 3.83 11 | 1.11 12 | 2.64 12 |
| .80 | 2.13 6 | 1.88 8 | 3.71 9 | 3.14 10 | 1.55 11 | 5.39 11 | 1.46 12 | 3.29 12 |
| .90 | 1.43 7 | 7.6 8 | 1.08 10 | 7.21 10 | 2.99 11 | 9.03 11 | 2.19 12 | 4.51 12 |
| 1.00 | 6.17 7 | 2.21 9 | 2.41 10 | 1.33 11 | 4.78 11 | 1.29 12 | 2.86 12 | 5.50 12 |
| 1.50 | 3.18 9 | 3.46 10 | 1.70 11 | 5.30 11 | 1.25 12 | 2.43 12 | 4.15 12 | 6.44 12 |
| 2.00 | 1.49 10 | 8.96 10 | 2.96 11 | 6.98 11 | 1.33 12 | 2.20 12 | 3.31 12 | 4.63 12 |
| 2.50 | 2.94 10 | 1.23 11 | 3.22 11 | 6.43 11 | 1.08 12 | 1.64 12 | 2.29 12 | 3.03 12 |
| 3.00 | 3.90 10 | 1.29 11 | 2.90 11 | 5.20 11 | 8.11 11 | 1.15 12 | 1.52 12 | 1.96 12 |
| 4.00 | 4.16 10 | 1.04 11 | 1.93 11 | 3.03 11 | 4.31 11 | 5.72 11 | 7.24 11 | 8.83 11 |
| 5.00 | 3.39 10 | 7.15 10 | 1.19 11 | 1.76 11 | 2.37 11 | 3.03 11 | 3.71 11 | 4.42 11 |
| 10.00 | 7.41 9 | 1.16 10 | 1.61 10 | 2.08 10 | 2.56 10 | 3.04 10 | 3.54 10 | 4.03 10 |
| 50.00 | | | | | | | | |
| 100.00 | | | | | | | | |
| λ | 4000°K. $J\lambda$ n | 5000°K. $J\lambda$ n | 6000°K. $J\lambda$ n | 8000°K. $J\lambda$ n | 10000°K. $J\lambda$ n | 15000°K. $J\lambda$ n | 20000°K. $J\lambda$ n | 25000°K. $J\lambda$ n |
| 0.10 | 1.02 5 | 1.32 8 | 1.57 10 | 6.2 12 | 2.21 14 | 2.63 16 | 2.86 17 | 1.20 18 |
| .20 | 1.92 11 | 6.9 12 | 7.5 13 | 1.49 15 | 8.95 15 | 9.84 16 | 3.31 17 | 6.98 17 |
| .30 | 9.9 12 | 1.08 14 | 5.32 14 | 3.90 15 | 1.30 16 | 6.58 16 | 1.52 17 | 2.64 17 |
| .40 | 4.66 13 | 2.80 14 | 9.25 14 | 4.16 15 | 1.03 16 | 3.62 16 | 7.24 16 | 1.13 17 |
| .45 | 7.00 13 | 3.45 14 | 9.98 14 | 3.82 15 | 8.67 15 | 2.73 16 | 5.13 16 | 7.79 16 |
| .50 | 9.16 13 | 3.85 14 | 1.00 15 | 3.39 15 | 7.15 15 | 2.06 16 | 3.71 16 | 5.52 16 |
| .55 | 1.09 14 | 4.04 14 | 9.72 14 | 2.95 15 | 5.87 15 | 1.57 16 | 2.74 16 | 4.00 16 |
| .60 | 1.22 14 | 4.05 14 | 9.06 14 | 2.53 15 | 4.80 15 | 1.22 16 | 2.07 16 | 2.98 16 |
| .65 | 1.30 14 | 3.93 14 | 8.31 14 | 2.16 15 | 3.96 15 | 9.53 15 | 1.58 16 | 2.26 16 |
| .70 | 1.32 14 | 3.74 14 | 7.51 14 | 1.84 15 | 3.26 15 | 7.55 15 | 1.23 16 | 1.73 16 |
| .75 | 1.32 14 | 3.49 14 | 6.74 14 | 1.56 15 | 2.71 15 | 6.06 15 | 9.76 15 | 1.36 16 |
| .80 | 1.30 14 | 3.23 14 | 6.01 14 | 1.34 15 | 2.26 15 | 4.91 15 | 7.80 15 | 1.08 16 |
| .90 | 1.19 14 | 2.71 14 | 4.75 14 | 9.93 14 | 1.60 15 | 3.32 15 | 5.15 15 | 7.04 15 |
| 1.00 | 1.06 14 | 2.23 14 | 3.70 14 | 7.41 14 | 1.16 15 | 2.32 15 | 3.54 15 | 4.78 15 |
| 1.50 | 4.88 13 | 8.47 13 | 1.24 14 | 2.12 14 | 3.04 14 | 5.48 14 | 7.96 14 | 1.04 15 |
| 2.00 | 2.32 13 | 3.62 13 | 5.03 13 | 7.99 13 | 1.10 14 | 1.88 14 | 2.68 14 | 3.48 14 |
| 2.50 | 1.18 13 | 1.76 13 | 2.37 13 | 3.62 13 | 4.90 13 | 8.15 13 | 1.14 14 | 1.47 14 |
| 3.00 | 6.63 12 | 9.53 12 | 1.25 13 | 1.86 13 | 2.48 13 | 4.06 13 | 5.65 13 | 7.24 13 |
| 4.00 | 2.50 12 | 3.45 12 | 4.42 12 | 6.40 12 | 8.40 12 | 1.34 13 | 1.84 13 | 2.34 13 |
| 5.00 | 1.13 12 | 1.53 12 | 1.93 12 | 2.75 12 | 3.57 12 | 5.62 12 | 7.70 12 | 9.76 12 |
| 10.00 | 8.60 10 | 1.12 11 | 1.37 11 | 1.88 11 | 2.40 11 | 3.66 11 | 4.98 11 | 6.28 11 |
| 50.00 | | | | | | | | |
| 100.00 | | | | | | | | |

TABLE 312.—Black Body Spectrum Intensities

Auxilliary table for J_λ at any temperature (Menzel, Harvard Observatory)

Let J_0 = intensity for $T_0 = 10,000^\circ \text{K.}$; for another temperature $T^\circ \text{K.}$, we have the relationship

$$J/J_0 = [\lambda^5_0 (e^{c_2/\lambda_0 T_0} - 1)] / [\lambda^5 (e^{c_2/\lambda T} - 1)].$$

Let $\lambda = \lambda_0 T_0/T$. Then $J_0 (T/T_0)^5$, e. g., to find J_λ for 0.5μ , 6000°K. , we take $0.5\mu = \lambda_0 \times 10,000/6,000$ or $\lambda_0 = 0.3\mu$, J_0 for $0.3\mu = 1.2977 \times 10^{16}$, whence $J = 1.2977 \times 10^{16} \times (6000/10000)^5$ or 1.01×10^{15} .

In the following table J_λ is for $10,000^\circ \text{K.}$; $J_\lambda \times 10^n$ is intensity at wave length $\lambda\mu$. λ is given in μ but in plotting it should be used in cm (one $\mu = 10^{-4} \text{cm}$) that the area under curve be in ergs.

$hc/k = 1.43187$; $2\pi hc^2 = 3.69728 \text{ c.g.s. units.}$ A change in c_1 may be allowed for by a constant factor, in c_2 by taking a different value for T so that $1.4319 \times 10,000 = c_2 T$. One $\text{erg.cm}^{-2}.\text{sec}^{-1} = 2.389 \times 10^{-8} \text{ cal.}^{-1} \text{ cm}^{-2} \text{ sec}^{-1}$.

| λ | J_λ (ergs) n | λ | J_λ (ergs) n | λ | J_λ (ergs) n | λ | J_λ (ergs) n |
|-----------|------------------------|-----------|------------------------|-----------|------------------------|-----------|------------------------|
| μ | | μ | | μ | | μ | |
| .0100 | 2.4131 -37 | .1450 | 2.9673 15 | .5500 | 5.8731 15 | 4.500 | 5.3480 12 |
| .0150 | 4.7932 -26 | .1500 | 3.4824 15 | .6000 | 4.8153 15 | 5.000 | 3.5680 12 |
| .0200 | 9.3330 -1 | .1600 | 4.5307 15 | .6500 | 3.9579 15 | 6.000 | 1.7645 12 |
| .0250 | 5.0592 -1 | .1700 | 5.7244 15 | .7000 | 3.2677 15 | 7.000 | 9.6897 11 |
| .0300 | 2.8437 -2 | .1800 | 6.8702 15 | .7500 | 2.7735 15 | 8.000 | 5.7562 11 |
| .0350 | 1.2932 5 | .1900 | 7.9697 15 | .8000 | 2.2620 15 | 9.000 | 3.6298 11 |
| .0400 | 1.0261 7 | .2000 | 8.9902 15 | .8500 | 1.9165 15 | 10.00 | 2.4018 11 |
| .0450 | 3.0403 8 | .2100 | 9.9908 15 | .9000 | 1.6018 15 | 12.00 | 1.1727 11 |
| .0500 | 4.3245 9 | .2200 | 1.0711 16 | .9500 | 1.3596 15 | 14.00 | 6.3824 10 |
| .0550 | 3.6280 10 | .2300 | 1.1387 16 | 1.0000 | 1.1601 15 | 16.00 | 3.7652 10 |
| .0600 | 2.0556 11 | .2400 | 1.1938 16 | 1.1000 | 8.5810 14 | 18.00 | 2.3634 10 |
| .0650 | 8.6361 11 | .2500 | 1.2365 16 | 1.2000 | 6.4670 14 | 20.00 | 1.5569 10 |
| .0700 | 2.8766 12 | .2600 | 1.2680 16 | 1.3000 | 4.9587 14 | 25.00 | 6.4241 9 |
| .0750 | 7.9649 12 | .2700 | 1.2883 16 | 1.4000 | 3.8600 14 | 30.00 | 3.1121 9 |
| .0800 | 1.9021 13 | .2800 | 1.2996 16 | 1.5000 | 3.0472 14 | 35.00 | 1.6858 9 |
| .0850 | 4.0261 13 | .2900 | 1.3023 16 | 1.6000 | 2.2038 14 | 40.00 | 9.9057 8 |
| .0900 | 7.7120 13 | .3000 | 1.2977 16 | 1.7000 | 1.9702 14 | 45.00 | 6.1974 8 |
| .0950 | 1.3598 14 | .3200 | 1.2700 16 | 1.8000 | 1.6096 14 | 50.00 | 4.0718 8 |
| .1000 | 2.2355 14 | .3400 | 1.2246 16 | 1.9000 | 1.3276 14 | 55.00 | 2.7860 8 |
| .1050 | 3.4637 14 | .3600 | 1.1673 16 | 2.0000 | 1.1046 14 | 60.00 | 1.9697 8 |
| .1100 | 5.1028 14 | .3800 | 1.1031 16 | 2.200 | 7.8206 13 | 65.00 | 1.3983 8 |
| .1150 | 7.1944 14 | .4000 | 1.0358 16 | 2.400 | 5.6907 13 | 70.00 | 1.0643 8 |
| .1200 | 9.7255 14 | .4200 | 9.9002 15 | 2.600 | 4.2361 13 | 80.00 | 6.2476 7 |
| .1250 | 1.2839 15 | .4400 | 9.0036 15 | 2.800 | 3.2185 13 | 90.00 | 3.9036 7 |
| .1300 | 1.6394 15 | .4600 | 8.3551 15 | 3.000 | 2.6973 13 | 100.00 | 2.5640 7 |
| .1350 | 2.0414 15 | .4800 | 7.7401 15 | 3.500 | 1.3927 13 | | |
| .1400 | 2.4858 15 | .5000 | 7.1589 15 | 4.000 | 8.3888 12 | | |

TABLE 313.—Values of J_λ for Various Temperatures CentigradeEkholm, Met. Z. 1902, used $C_1 = 8346$ and $C_2 = 14349$, and for the unit of time the day.For 100° , the values for J_λ have been multiplied by 10, for the other temperatures by 100.

| λ | $T=100^\circ \text{C}$ | 30°C | 15°C | 0°C | -30°C | -80°C | λ | 100°C | 30°C | 15°C | 0°C | -30°C | -80°C |
|-----------|------------------------|---------------------|---------------------|--------------------|----------------------|----------------------|-----------|----------------------|---------------------|---------------------|--------------------|----------------------|----------------------|
| μ | | | | | | | μ | | | | | | |
| 2 | 1 | 0 | 0 | 0 | 0 | 0 | 18 | 511 | 2961 | 2557 | 2175 | 1491 | 623 |
| 3 | 80 | 41 | 18 | 7 | 1 | 0 | 19 | 443 | 2626 | 2281 | 1954 | 1363 | 594 |
| 4 | 469 | 508 | 272 | 138 | 27 | 1 | 20 | 386 | 2329 | 2034 | 1754 | 1242 | 561 |
| 5 | 1047 | 1777 | 1085 | 628 | 172 | 8 | 21 | 337 | 2068 | 1816 | 1574 | 1129 | 527 |
| 6 | 1526 | 3464 | 2296 | 1454 | 493 | 39 | 22 | 295 | 1840 | 1622 | 1413 | 1026 | 494 |
| 7 | 1768 | 4954 | 3481 | 2353 | 931 | 105 | 23 | 259 | 1639 | 1448 | 1270 | 931 | 460 |
| 8 | 1810 | 5928 | 4352 | 3088 | 1372 | 203 | 24 | 228 | 1462 | 1298 | 1141 | 846 | 428 |
| 9 | 1724 | 6382 | 4834 | 3646 | 1730 | 316 | 25 | 202 | 1307 | 1165 | 1028 | 768 | 398 |
| 10 | 1573 | 6386 | 4979 | 3781 | 1971 | 426 | 26 | 179 | 1170 | 1047 | 926 | 698 | 369 |
| 11 | 1398 | 6127 | 4833 | 3798 | 2098 | 520 | 28 | 142 | 947 | 850 | 757 | 579 | 317 |
| 12 | 1225 | 5712 | 4633 | 3676 | 2114 | 592 | 30 | 114 | 771 | 696 | 623 | 482 | 272 |
| 13 | 1063 | 5222 | 4300 | 3467 | 2090 | 640 | 40 | 44 | 311 | 285 | 259 | 209 | 130 |
| 14 | 918 | 4713 | 3930 | 3215 | 2004 | 666 | 50 | 20 | 146 | 135 | 124 | 102 | 67 |
| 15 | 792 | 4220 | 3556 | 2944 | 1889 | 673 | 60 | 10 | 77 | 72 | 66 | 55 | 38 |
| 16 | 683 | 3759 | 3198 | 2674 | 1760 | 663 | 80 | 4 | 27 | 25 | 24 | 20 | 14 |
| 17 | 590 | 3340 | 2862 | 2417 | 1626 | 649 | 100 | 2 | 12 | 11 | 10 | 9 | 7 |

SPECTRAL ENERGY DISTRIBUTION AND LUMINOSITY DATA

For use in computing light transmissions and relative brightnesses from spectrometric data. Range of color temperatures 2000°K. to 3000°K. Considerably abridged from Skogland, Bur. Standards, Misc. Publ., No. 86; see also No. 56, 1925, range, 1000° to 28000°K. Planck's formula used with C_2 , 14330 μ deg. The constant of Wien's displacement law has been determined as 2886.3 μ deg.

TABLE 314.—Relative J_λ , based on J at $\lambda = 0.59\mu$ or 590 μ

EXAMPLE: At color temperature 2296°K. and λ , 0.65 μ , the energy radiated relative to that at 0.59 μ is 1.6361.

| λ in μ | 2000°K. | 2100°K. | 2200°K. | 2300°K. | 2400°K. | 2500°K. | 2600°K. | 2700°K. | 2800°K. | 2900°K. | 3000°K. |
|-----------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| .32 | 0.0007 | 0.0012 | 0.0019 | 0.0020 | 0.0042 | 0.0059 | 0.0080 | 0.0108 | 0.0141 | 0.0182 | 0.0230 |
| .34 | 21 | 31 | 47 | 67 | 92 | .0124 | .0164 | 211 | 267 | 333 | 409 |
| .36 | 50 | 73 | .0102 | .0130 | .0184 | 239 | 303 | 378 | 463 | 561 | 666 |
| .38 | .0110 | .0151 | 203 | 264 | 336 | 420 | 517 | 626 | 747 | 882 | .1029 |
| .40 | 218 | 287 | 369 | 463 | 571 | 691 | 826 | 973 | .1134 | .1306 | .1492 |
| .42 | 402 | 507 | 628 | 762 | 910 | .1073 | .1248 | .1435 | .1634 | .1844 | .2060 |
| .44 | 690 | 841 | .1006 | .1185 | .1376 | .1580 | .1794 | .2019 | .2252 | .2494 | .2743 |
| .46 | .1122 | .1321 | .1533 | .1755 | .1988 | .2228 | .2477 | .2731 | .2991 | .3254 | .3520 |
| .48 | .1735 | .1981 | .2235 | .2494 | .2760 | .3028 | .3298 | .3570 | .3843 | .4116 | .4388 |
| .50 | .2571 | .2852 | .3136 | .3420 | .3701 | .3981 | .4257 | .4531 | .4800 | .5066 | .5326 |
| .52 | .3667 | .3964 | .4254 | .4538 | .4815 | .5085 | .5347 | .5602 | .5849 | .6090 | .6322 |
| .54 | .5058 | .5336 | .5602 | .5856 | .6100 | .6333 | .6556 | .6739 | .6973 | .7170 | .7356 |
| .56 | .6773 | .6986 | .7186 | .7373 | .7549 | .7714 | .7871 | .8017 | .8156 | .8289 | .8413 |
| .58 | .8835 | .8923 | .9006 | .9080 | .9148 | .9213 | .9272 | .9327 | .9379 | .9428 | .9473 |
| .59 | .00007 | .00013 | .0002 | .0004 | .0006 | .0008 | .0012 | .0017 | .0024 | .0032 | .0043 |
| .60 | 1.1256 | 1.1148 | 1.1051 | 1.0963 | 1.0885 | 1.0810 | 1.0743 | 1.0681 | 1.0624 | 1.0571 | .0523 |
| .62 | 1.4044 | 1.3657 | 1.3314 | 1.3009 | 1.2734 | 1.2486 | 1.2263 | 1.2060 | 1.1875 | 1.1704 | 1.1549 |
| .64 | 1.7195 | 1.6435 | 1.5773 | 1.5193 | 1.4680 | 1.4223 | 1.3815 | 1.3449 | 1.3114 | 1.2812 | 1.2537 |
| .66 | 2.0608 | 1.9468 | 1.8410 | 1.7498 | 1.6699 | 1.5998 | 1.5378 | 1.4824 | 1.4329 | 1.3882 | 1.3479 |
| .68 | 2.4534 | 2.2727 | 2.1199 | 1.9895 | 1.8770 | 1.7792 | 1.6934 | 1.6177 | 1.5505 | 1.4905 | 1.4366 |
| .70 | 2.8679 | 2.6189 | 2.4110 | 2.2361 | 2.0869 | 1.9584 | 1.8468 | 1.7493 | 1.6633 | 1.5872 | 1.5193 |
| .72 | 3.310 | 2.7086 | 2.7120 | 2.4872 | 2.2972 | 2.1357 | 1.9905 | 1.8757 | 1.7704 | 1.6776 | 1.5955 |
| .74 | 3.777 | 3.300 | 3.020 | 2.7493 | 2.5068 | 2.3095 | 2.1413 | 1.9966 | 1.8710 | 1.7614 | 1.6648 |
| .76 | 4.265 | 3.748 | 3.332 | 2.9931 | 2.7126 | 2.4786 | 2.2801 | 2.1105 | 1.9647 | 1.8380 | 1.7272 |

TABLE 315.—Luminosity Relative to Maximum Value at Each Temperature

EXAMPLE: At color temperature 2680°K. and $\lambda = 0.55\mu$, the luminosity relative to that at 0.5720 μ is 0.8874.

| λ in μ | 2000°K. | 2200°K. | 2400°K. | 2600°K. | 2800°K. | 3000°K. | Equal energy = visibility |
|--------------------|-------------|---------|---------|---------|---------|---------|------------------------------|
| 0.40 | .0000 | .0000 | .0000 | .0000 | .0001 | .0001 | .0004 |
| .42 | .0002 | .0003 | .0005 | .0006 | .0008 | .0010 | .004 |
| .44 | .0021 | .0029 | .0040 | .0050 | .0062 | .0074 | .023 |
| .46 | .0087 | .0123 | .0149 | .0182 | .0215 | .0248 | .03 |
| .48 | .0314 | .0397 | .0480 | .0501 | .0640 | .0716 | .139 |
| 0.50 | .1079 | .1292 | .1495 | .1683 | .1850 | .2021 | .323 |
| .52 | .3383 | .3853 | .4274 | .4645 | .4977 | .5260 | .710 |
| .54 | .6270 | .6816 | .7275 | .7655 | .7972 | .8230 | .954 |
| .56 | .8758 | .9120 | .9390 | .9584 | .9726 | .9826 | .995 |
| .58 | .9988 | .9994 | .9950 | .9873 | .9780 | .9676 | .870 |
| 0.60 | .9231 | .8897 | .8585 | .8299 | .8035 | .7796 | .631 |
| .62 | .6954 | .6473 | .6066 | .5722 | .5422 | .5166 | .381 |
| .64 | .3910 | .3524 | .3212 | .2960 | .2751 | .2576 | .175 |
| .66 | .1641 | .1433 | .1273 | .1148 | .1048 | .0966 | .061 |
| .68 | .0542 | .0400 | .0399 | .0352 | .0316 | .0287 | .017 |
| 0.70 | .0153 | .0126 | .0107 | .0093 | .0082 | .0073 | .0041 |
| 2 | .0045 | .0035 | .0030 | .0026 | .0022 | .0020 | .0010 |
| 4 | .0012 | .0010 | .0008 | .0007 | .0006 | .0005 | .0002 |
| 6 | .0003 | .0003 | .0002 | .0002 | .0001 | .0001 | .0001 |
| Sum | 10.464 | 10.593 | 10.535 | 10.556 | 10.572 | 10.581 | 10.686 |
| Max. at | .5818 μ | .5788 | .5758 | .5730 | .5705 | .5682 | .555 |

SPECTRAL ENERGY DISTRIBUTION AND LUMINOSITY DATA (concluded)

Factors proportional to the values of Table 315 adjusted so that the area of each complete curve of luminosity factors between 0.40 and 0.76μ is equal to unity. To obtain the light transmission of a screen, multiply the spectrum transmission at each λ by the corresponding tabulated or interpolated factor, obtaining in each case an element of light transmission for the wave-length interval $\lambda - .01\mu$ to $\lambda + .01\mu$. The integral light transmission is obtained as the sum of these elements. The same process is followed for spectrum reflection.

TABLE 316.—Luminosity Factors

| λ in μ | 2000°K. | 2100°K. | 2200°K. | 2300°K. | 2400°K. | 2500°K. | 2600°K. | 2700°K. | 2800°K. | 2900°K. | 3000°K. |
|--------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| 0.40 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| .42 | .0000 | .0000 | .0000 | .0000 | .0000 | .0000 | .0000 | .0001 | .0001 | .0001 | .0001 |
| .44 | .0002 | .0002 | .0003 | .0003 | .0004 | .0004 | .0005 | .0005 | .0006 | .0007 | .0007 |
| .46 | .0008 | .0010 | .0011 | .0012 | .0014 | .0016 | .0017 | .0019 | .0020 | .0021 | .0023 |
| .48 | .0030 | .0034 | .0038 | .0042 | .0046 | .0049 | .0052 | .0056 | .0061 | .0064 | .0067 |
| .50 | .0103 | .0114 | .0123 | .0133 | .0142 | .0151 | .0160 | .0168 | .0176 | .0184 | .0191 |
| .52 | .0323 | .0347 | .0367 | .0386 | .0406 | .0424 | .0440 | .0455 | .0471 | .0486 | .0498 |
| .54 | .0599 | .0627 | .0649 | .0669 | .0690 | .0710 | .0725 | .0740 | .0754 | .0768 | .0779 |
| .56 | .0837 | .0855 | .0868 | .0880 | .0891 | .0901 | .0908 | .0914 | .0920 | .0925 | .0929 |
| .58 | .0954 | .0954 | .0954 | .0949 | .0944 | .0939 | .0935 | .0930 | .0925 | .0919 | .0914 |
| .60 | .0882 | .0863 | .0847 | .0832 | .0815 | .0799 | .0786 | .0773 | .0760 | .0747 | .0737 |
| .62 | .0664 | .0638 | .0616 | .0596 | .0576 | .0558 | .0542 | .0527 | .0513 | .0499 | .0488 |
| .64 | .0374 | .0352 | .0335 | .0320 | .0305 | .0292 | .0280 | .0270 | .0260 | .0251 | .0243 |
| .66 | .0157 | .0145 | .0136 | .0129 | .0121 | .0115 | .0109 | .0104 | .0099 | .0095 | .0091 |
| .68 | .0052 | .0047 | .0044 | .0041 | .0038 | .0035 | .0033 | .0032 | .0030 | .0028 | .0027 |
| .70 | .0015 | .0013 | .0012 | .0011 | .0010 | .0009 | .0009 | .0008 | .0008 | .0007 | .0007 |
| .72 | .0004 | .0004 | .0003 | .0003 | .0003 | .0003 | .0002 | .0002 | .0002 | .0002 | .0002 |
| .74 | .0001 | .0001 | .0001 | .0001 | .0001 | .0001 | .0001 | .0001 | .0001 | .0000 | .0000 |
| .76 | .0000 | .0000 | .0000 | .0000 | .0000 | .0000 | .0000 | .0000 | .0000 | .0000 | .0000 |
| Max. value | .0956 | .0953 | .0952 | .0950 | .0949 | .0948 | .0947 | .0947 | .0946 | .0945 | .0945 |
| Max. at μ | .5818 | .5802 | .5788 | .5774 | .5758 | .5743 | .5730 | .5718 | .5705 | .5693 | .5683 |
| Cantroid μ | .5830 | .5814 | .5800 | .5786 | .5770 | .5757 | .5742 | .5730 | .5717 | .5705 | .5695 |

TABLE 317.—Percentage Change in J for Change of ± 30 in Planck's C_2 (14330)

EXAMPLE: At color temperature 2300°K. , the value below for 0.44μ is 0.8% , due to a change of 30 in C_2 . For a change of 20 in C_2 the change in $J_{0.44}$ is $\frac{2}{3}$ of $0.8 = 0.5\%$; for a change of 15 in C_2 , $\frac{1}{2}$ of $0.8 = 0.4\%$, etc.

Algebraic sign of tabulated values:

| Change in C_2 —Increase..... | Tabulated values | |
|--------------------------------|------------------|-------------|
| | 1st 6 col. | Next 6 col. |
| Decrease..... | — | + |
| | + | — |

In line "all λ " are given values for adjustment of the percentage values above in Table 315 to obtain the $\%$ change in the luminosity factors of Table 316. Each of these constants applies to all values given above it in the table; that is, one constant for each temperature. Combine the given constant by algebraic addition with the individual values at each wave length.

EXAMPLE: Color temp. 2600°K. ; $\lambda = 0.52\mu$; C_2 changed from 14330 to 14310 . At 0.52μ , 2600°K. , 0.3% is tabulated. Its sign is $+$, and C_2 is decreased. The corresponding constant in line "all λ " is -0.07 , the minus sign corresponding to a decrease in C_2 . For a change of -30 in C_2 , the $\%$ change for Table 317 is $0.3 - 0.1\% = 0.2\%$. For the assigned change of -20 in C_2 , the required adjustment to the value in Table 316 is $\frac{2}{3}$ of $0.2 = 0.1\%$. At $\lambda = .71\mu$, the adjustment would be $\frac{2}{3}$ ($-0.3 - 0.1$) = -0.2% , etc.

| λ in μ | 2000°K. | 2300°K. | 2600°K. | 2900°K. | 3200°K. | λ in μ | 2000°K. | 2300°K. | 2600°K. | 2900°K. | 3200°K. |
|--------------------|---------|---------|---------|---------|---------|--------------------|---------|---------|---------|---------|---------|
| 0.32 | 2.0% | 1.9% | 1.7% | 1.5% | 1.3% | 0.60 | | | | | |
| .34 | 1.8 | 1.6 | 1.5 | 1.3 | 1.1 | .62 | | | 0.1 | 0.1 | 0.1 |
| .36 | 1.6 | 1.4 | 1.3 | 1.1 | 1.0 | .64 | | 0.2 | .2 | | |
| .38 | 1.4 | 1.2 | 1.1 | .9 | .9 | .66 | 0.3 | | | .2 | .2 |
| | | | | | | .68 | .3 | .3 | .3 | .2 | .2 |
| .40 | 1.2 | 1.0 | .9 | .8 | .8 | | | | | | |
| .42 | 1.0 | .9 | .8 | .7 | .7 | .70 | .4 | .3 | .3 | .3 | .2 |
| .44 | .9 | .8 | .7 | .6 | .6 | .72 | .4 | .4 | .4 | .3 | .3 |
| .46 | .7 | .6 | .5 | .5 | .5 | .74 | .5 | .4 | .4 | .4 | .3 |
| .48 | .6 | .5 | .4 | .4 | .4 | .76 | .6 | .5 | .4 | .4 | .4 |
| .50 | .5 | .4 | .4 | .3 | .3 | all λ | .04 | .06 | .07 | .07 | .07 |
| .52 | .3 | .3 | .3 | .2 | .2 | | | | | | |
| .54 | .2 | .2 | .2 | .2 | .2 | | | | | | |
| .56 | .1 | .1 | .1 | .1 | .1 | | | | | | |
| .58 | .0 | .0 | .0 | .0 | .0 | | | | | | |

RADIATION EMISSIVITIES

TABLE 318.—Relative Emissive Powers for Total Radiation

Emissive power of black body = 1. Receiving surface platinum black at 25° C; oxidized surfaces oxidized at 600 + ° C. Randolph and Overholzer, Phys. Review, 2, p. 144, 1913.

| | Temperature, Deg. C | | |
|---------------------------------|---------------------|-------|-------|
| | 200 | 400 | 600 |
| Silver..... | 0.020 | 0.030 | 0.038 |
| Platinum (r)..... | 0.060 | 0.086 | 0.110 |
| Oxidized zinc..... | — | 0.110 | — |
| Oxidized aluminum..... | 0.113 | 0.153 | 0.192 |
| Calorized copper, oxidized..... | 0.180 | 0.185 | 0.190 |
| Cast iron..... | 0.210 | — | — |
| Oxidized nickel..... | 0.369 | 0.424 | 0.478 |
| Oxidized monel..... | 0.411 | 0.439 | 0.461 |
| Calorized steel, oxidized..... | 0.521 | 0.547 | 0.570 |
| Oxidized copper..... | 0.568 | 0.568 | 0.568 |
| Oxidized brass..... | 0.610 | 0.600 | 0.589 |
| Oxidized lead..... | 0.631 | — | — |
| Oxidized cast iron..... | 0.643 | 0.710 | 0.777 |
| Oxidized steel..... | 0.790 | 0.788 | 0.787 |
| Black body..... | 1.00 | 1.00 | 1.00 |

Remark: For radiation properties of bodies at temperatures so low that the radiations of wave length greater than 20μ or thereabouts are important, doubt must exist because of the possible and perhaps probable lack of blackness of the receiving body to radiations of those wave lengths or greater. For instance, see Tables 455 and 460 for the transparency of soot.

TABLE 319.—Emissivities of Metals and Oxides

Emissivities for radiation of wave-length 0.55 and 0.65 μ . Burgess and Waltenberg, Bul. Bureau of Standards, 11, 591, 1914.

In the solid state, practically all the metals examined appear to have a negligible or very small temperature coefficient of emission for $\lambda = 0.55$ and 0.65 μ within the temperature range 20° C to melting point. Nickel oxide has a well-defined negative coefficient, at least to the melting point. There is a discontinuity in emissivity, for $\lambda = 0.65 \mu$ at the melting point for some but not all the metals and oxides. This effect is most marked for gold, copper, and silver, and is appreciable for platinum and palladium. Palladium, in addition, possesses for radiation a property analogous to sulfusion, in that the value of emissivity ($\lambda = 0.65 \mu$) natural to the liquid state may persist for a time after solidification of the metal. The Violle unit of light does not appear to define a constant standard. Article contains bibliography.

| Metals | Cu | Ag | Au | Pd | Pt | Ir | Rh | Ni | Co | Fe | Mn | Ti |
|-----------------------------------|------|--------------------------------|--------------------------------|--------------------------------|------------------|------------------|-------------------------------|------|------------------|-------------------------------|--------------------------------|-------------------------------|
| $e_{\lambda}, 0.55 \mu$ solid.... | 0.38 | 0.35 | 0.38 | 0.38 | 0.38 | — | 0.29 | 0.41 | — | — | — | 0.75 |
| 0.55 μ liquid... | 0.36 | 0.35 | 0.38 | — | — | — | — | 0.46 | — | — | — | 0.75 |
| 0.65 μ solid.... | 0.10 | 0.04 | 0.14 | 0.33 | 0.33 | 0.30 | 0.29 | 0.36 | 0.36 | 0.37 | 0.59 | 0.63 |
| liquid.... | 0.15 | 0.07 | 0.22 | 0.37 | 0.38 | — | 0.30 | 0.37 | 0.37 | 0.37 | 0.59 | 0.65 |
| Metals | Zr | Th | Y | Er | Be | Cb | V | Cr | Mo | W | U | |
| $e_{\lambda}, 0.55 \mu$ solid.... | — | 0.36 | — | — | 0.61 | 0.61 | 0.29 | 0.53 | — | — | 0.77 | |
| liquid.... | — | — | — | 0.30 | 0.81 | — | — | — | — | — | — | |
| 0.65 μ solid.... | 0.32 | 0.36 | 0.35 | 0.55 | 0.61 | 0.49 | 0.35 | 0.39 | 0.43 | 0.39 | 0.54 | |
| liquid.... | 0.30 | 0.40 | 0.35 | 0.38 | 0.61 | 0.40 | 0.32 | 0.39 | 0.40 | — | 0.34 | |
| Oxides: 0.65 μ | NiO | Co ₃ O ₄ | Fe ₂ O ₃ | Mn ₂ O ₃ | TiO ₂ | ThO ₂ | Y ₂ O ₃ | BeO | CbO ₂ | V ₂ O ₃ | Cr ₂ O ₃ | U ₃ C ₈ |
| e_{λ} , solid..... | 0.89 | 0.77 | 0.63 | — | 0.52 | 0.57 | 0.61 | 0.37 | 0.71 | 0.69 | 0.60 | 0.30 |
| liquid..... | 0.68 | 0.63 | 0.53 | 0.47 | 0.51 | 0.69 | — | — | — | — | — | 0.31 |

TABLE 320
SOME INTRINSIC PROPERTIES OF TUNGSTEN

(Jones, Langmuir, Gen. Electr. Rev., July-August, 1927)

| T°K. | Resis- tivity $\rho \times 10^6$ ohm.cm | Power radiated P watts/ cm ² | Bright- ness B int. cand./ cm ² | Effi- ciency E | Electron emission | Evapora- tion | Vapor pressure p baryes $\times 10^6$ | Power emis- sivity black body = 1 | Thermal expan- sion in per cent at 293° | Atomic heat cal./g. atom./°C | Heat content cal.10 ⁻² gram |
|------|--|---|--|------------------------|----------------------|------------------|--|---|--|---------------------------------------|---|
| | | | | | $i \times 10^6$ | $M \times 10^6$ | $p \times 10^6$ | | | | |
| | | | | | i | n | M | n | p | n | |
| 300 | 5.65 | 3×10^{-5} | | | amp./cm ² | | g/cm ² sec. | | dynes/cm ² | | |
| 400 | 8.06 | 2×10^{-3} | | | | | | | | | |
| 500 | 10.56 | 1×10^{-2} | | | | | | | | | |
| 600 | 13.23 | .030 | | | | | | | | | |
| 700 | 16.09 | .076 | | | | | | | | | |
| 800 | 19.00 | .169 | | | | | | | | | |
| 900 | 21.94 | .322 | | | | | | | | | |
| 1000 | 24.93 | .602 | 1×10^{-4} | 17.3 | 1.07 | -15 | 5.32 | -34 | 1.98 | -29 | 54 |
| 1100 | 27.94 | 1.027 | 1×10^{-3} | 15.6 | 1.52 | -13 | 2.17 | -30 | 1.22 | -25 | 60 |
| 1200 | 30.98 | 1.66 | 6×10^{-3} | 14.2 | 9.73 | -12 | 3.21 | -27 | 1.87 | -22 | 66 |
| 1300 | 34.08 | 2.57 | 3×10^{-2} | 13.1 | 3.21 | -10 | 1.35 | -24 | 8.18 | -20 | 75 |
| 1400 | 37.19 | 3.83 | 1×10^{-1} | 12.0 | 6.62 | -9 | 2.51 | -22 | 1.62 | -17 | 82 |
| 1500 | 40.36 | 5.52 | 0.33 | 11.1 | 0.14 | -8 | 2.37 | -20 | 1.54 | -15 | 89 |
| 1600 | 43.55 | 7.74 | 0.93 | 10.3 | 0.27 | -7 | 1.25 | -18 | 8.43 | -14 | 96 |
| 1700 | 46.78 | 10.62 | 2.33 | 9.5 | 7.08 | -6 | 4.17 | -17 | 2.82 | -12 | 103 |
| 1800 | 50.05 | 14.19 | 5.12 | 8.8 | 4.47 | -5 | 8.81 | -16 | 6.31 | -11 | 110 |
| 1900 | 53.35 | 18.64 | 10.93 | 8.2 | 2.28 | -4 | 1.41 | -14 | 1.01 | -9 | 118 |
| 2000 | 56.67 | 24.04 | 20.66 | 7.6 | 1.00 | -3 | 1.76 | -13 | 1.33 | -8 | 125 |
| 2100 | 60.06 | 30.5 | 37.75 | 7.1 | 3.93 | -3 | 1.66 | -12 | 1.28 | -7 | 133 |
| 2200 | 63.48 | 38.2 | 64.0 | 6.7 | 1.33 | -2 | 1.25 | -11 | 9.88 | -7 | 141 |
| 2300 | 66.91 | 47.2 | 103.7 | 6.2 | 4.07 | -2 | 8.00 | -11 | 6.47 | -6 | 149 |
| 2400 | 70.39 | 57.7 | 164.4 | 5.8 | 1.16 | -1 | 4.26 | -10 | 3.52 | -5 | 157 |
| 2500 | 73.91 | 69.8 | 248 | 5.5 | 2.98 | -1 | 2.03 | -9 | 1.71 | -4 | 166 |
| 2600 | 77.49 | 83.8 | 364 | 5.1 | 7.16 | -1 | 8.41 | -9 | 7.24 | -4 | 174 |
| 2700 | 81.04 | 99.6 | 532 | 4.8 | 1.63 | 0 | 3.19 | -8 | 2.86 | -3 | 183 |
| 2800 | 84.70 | 117.6 | 732 | 4.5 | 3.54 | 0 | 1.10 | -7 | 9.84 | -3 | 192 |
| 2900 | 88.33 | 137.8 | 987 | 4.2 | 7.31 | 0 | 3.30 | -7 | 3.00 | -2 | 201 |
| 3000 | 92.04 | 160.5 | 1326 | 4.0 | 1.42 | +1 | 9.95 | -7 | 9.20 | -2 | 210 |
| 3100 | 95.76 | 185.8 | 1745 | 3.7 | 2.64 | +1 | 2.60 | -6 | 2.50 | -1 | 219 |
| 3200 | 99.54 | 214.0 | 2252 | 3.5 | 4.78 | +1 | 6.38 | -6 | 6.13 | -1 | 228 |
| 3300 | 103.3 | 245.4 | 2893 | 3.3 | 8.44 | +1 | 1.56 | -5 | 1.51 | 0 | 238 |
| 3400 | 107.2 | 280.0 | 3660 | 3.1 | 1.42 | +2 | 3.47 | -5 | 3.41 | 0 | 248 |
| 3500 | 111.1 | 318.0 | 4540 | 2.9 | 2.33 | +2 | 7.54 | -5 | 7.52 | 0 | 258 |
| 3600 | 115.0 | 360.0 | 5530 | 2.8 | 3.73 | +2 | 1.51 | -4 | 1.53 | 1 | 268 |
| 3655 | 117.1 | 382.6 | 6163 | 2.7 | 4.79 | +2 | 2.28 | -4 | 2.33 | 1 | 273 |

ITHSONIAN TABLES

TABLE 321.—Spectrum Emissivity of Tungsten (Percentage)

Weniger and Pfund (Phys. Rev., 14, 427, 1919) verified Drude's formula for tungsten, $100 - R_\lambda = e_\lambda = 3650 \sqrt{\rho/\lambda}$, valid for $\lambda > 2\mu$, where R_λ = reflectivity, λ , the wave length in μ , ρ , the specific resistance at the temperature considered. The following u.v. data is from Hulburt (Astrophys. Journ. 45, 149, 1917, via Forsythe, Christison, Gen. Electr. Rev., p. 622, 1929), from which the data for 0.2 to 4.2μ , 2800° are taken.

| | 0.34 μ | 0.38 μ | 0.42 μ | 0.48 μ | 0.50 μ | 0.54 μ | | | | | | |
|-------|------------|------------|------------|------------|------------|------------|-----|-----|-----|-----|-----------|--|
| 1800 | 49.3 | 49.2 | 48.8 | 48.0 | 46.0 | 44.2 | | | | | | |
| 2200 | 48.7 | 48.5 | 47.8 | 46.7 | 45.0 | 43.0 | | | | | | |
| 2600 | 48.3 | 48.0 | 47.2 | 46.0 | 44.2 | 42.1 | | | | | | |
| 3000 | 48.0 | 47.7 | 46.8 | 45.4 | 43.5 | 41.4 | | | | | | |
| 3400 | 47.7 | 47.4 | 46.5 | 44.8 | 42.7 | 40.7 | | | | | | |
| | 0.2 μ | 0.6 | 1.0 | 1.4 | 1.8 | 2.2 | 2.6 | 3.0 | 3.4 | 3.8 | 4.2 μ | |
| 2800° | 51 | 43 | 36 | 30 | 26 | 23 | 21 | 19 | 18 | 17 | 17 | |

TABLE 322.—Temperature Scale for Tungsten

Hyde, Cady, Forsythe, Journ. Franklin Inst. 181, 418, 1916. See also Phys. Rev. 10, 395, 1917. The color temperature = temperature of black body at which its color matches the given radiation.

| Lumens/ watt | Color temperature | Black-body temperature | True temperature | True temperature | True- color | True- brightness |
|-----------------|----------------------|---------------------------|---------------------|---------------------|----------------|---------------------|
| 1 | 1763°K. | 1627°K. | 1729°K. | 1700° | 12° | 100° |
| 2 | 1917 | 1753 | 1875 | 1800 | 20 | 115 |
| 3 | 2025 | 1840 | 1976 | 1900 | 26 | 128 |
| 4 | 2109 | 1909 | 2056 | 2000 | 31 | 142 |
| 5 | 2179 | 1967 | 2125 | 2100 | 36 | 158 |
| 6 | 2237 | 2017 | 2184 | 2200 | 39 | 175 |
| 7 | 2290 | 2062 | 2238 | 2300 | 41 | 191 |
| 8 | 2338 | 2102 | 2286 | 2400 | 43 | 208 |
| 9 | 2383 | 2140 | 2332 | | .. | ... |
| 10 | 2425 | 2174 | 2373 | | .. | ... |

TABLE 323.—Radiation Characteristics of Tungsten

(Forsythe, Worthing, Astrophys. Journ., 61, 146, 1925.)

| Temp. °K. | Emissivity | | | | Temperature °K. | | |
|--------------|-------------|-------------|---------------------|--------|---------------------------|--------|-----------|
| | 0.665 μ | 0.467 μ | Average luminous | Color | Brightness 0.665 μ | Color | Radiation |
| 500 | 0.466 | 0.498 | | | ... | | |
| 1000 | .456 | .486 | 0.464 | 0.396 | 966 | 1006 | 581 |
| 1500 | .445 | .476 | .457 | .383 | 1420 | 1517 | 991 |
| 2000 | .435 | .469 | .452 | .370 | 1857 | 2033 | 1428 |
| 2500 | .425 | .462 | .446 | .356 | 2274 | 2557 | 1859 |
| 3000 | .415 | .455 | .440 | .343 | 2673 | 3094 | 2286 |
| 3500 | (.405) | (.449) | (.434) | (.329) | 3053 | (3646) | (2704) |

TABLE 324.—Radiation and Other Properties of Tantalum

(Worthing, Phys. Rev., 28, 190, 1926.)

| °K. | Emissivity | | Temperature | | | Resis- tivity μ -ohm- cm | Radiation Watt/ cm ² | $\frac{Tdn}{n dT}$ | Total emis- sivity |
|---------|------------|------------|-------------------------------|-------|-----------|---------------------------------------|---------------------------------------|--------------------|--------------------------|
| | .665 μ | .463 μ | Bright- ness .665 μ | Color | Radiation | | | | |
| | | | °K. | °K. | °K. | | | | |
| 300 | 0.493 | 0.56 | | | | | | | |
| 1000 | .459 | .52 | 966 | | | | | | |
| 1200 | .450 | .51 | 1149 | | | | | | |
| 1400 | .442 | .50 | 1329 | | | | | | |
| 1600 | .434 | .49 | 1506 | 1642 | 1062 | 67.6 | 7.3 | 4.80 | 0.194 |
| 1800 | .426 | .48 | 1680 | 1859 | 1222 | 74.1 | 12.8 | 4.80 | .213 |
| 2000 | .418 | .47 | 1851 | 2075 | 1390 | 80.5 | 21.2 | 4.80 | .232 |
| 2200 | .411 | .46 | 2018 | 2288 | 1556 | 86.9 | 33.4 | 4.80 | .251 |
| 2400 | .404 | .45 | 2180 | 2497 | 1730 | 92.9 | 50.7 | 4.80 | .269 |
| 2600 | .397 | .44 | 2339 | 2705 | 1901 | 99.1 | 75 | 4.80 | .287 |
| 2800 | .390 | .. | 2495 | 2911 | 2080 | 105.0 | 106 | 4.80 | .304 |
| 3000 | .384 | .. | 2647 | | | | | | |
| 3300 mp | .375 | .. | 2870 | | | | | | |

TABLE 325.—Radiation and Other Properties of Molybdenum

(Worthing, Phys. Rev., 28, 190, 1926.)

| °K. | Emissivity | | Temperature | | | Resis- tivity μ -ohm- cm | Brightness normally candles/ cm ² | Radiation intensity watts/ cm ² | Luminous efficiency lumens/ watt |
|------|------------|------------|--|-------|-----------|---------------------------------------|---|---|---|
| | .665 μ | .475 μ | Bright- ness S _{.665μ} | Color | Radiation | | | | |
| | | | °K. | °K. | °K. | | | | |
| 273 | 0.420 | 0.425 | | | | 5.14 | | | |
| 1000 | .390 | .403 | 958 | | 557 | 23.9 | 0.0001 | 0.55 | |
| 1400 | .375 | .393 | 1316 | 1411 | 864 | 35.2 | .089 | 3.18 | 0.093 |
| 1600 | .367 | .388 | 1489 | 1616 | 1024 | 41.1 | .765 | 6.30 | .40 |
| 1800 | .360 | .383 | 1658 | 1823 | 1187 | 47.0 | 4.13 | 11.3 | 1.22 |
| 2000 | .353 | .379 | 1824 | 2032 | 1354 | 53.1 | 15.9 | 19.2 | 2.75 |
| 2200 | .347 | .375 | 1986 | 2244 | 1523 | 59.2 | 48.5 | 30.7 | 5.28 |
| 2400 | .341 | .371 | 2143 | 2456 | 1693 | 65.5 | 123 | 47.0 | 8.70 |
| 2600 | .336 | .368 | 2297 | 2672 | 1866 | 71.8 | 270 | 69.5 | 13.0 |
| 2800 | .331 | .365 | 2448 | 2891 | 2039 | 78.2 | 540 | 98 | 18.4 |
| 2895 | .328 | .363 | 2519 | 2997 | 2122 | 81.4 | 730 | 116 | |

TABLE 326.—Relation between Brightness Temperature and Color Temperature for Various Substances

| Brightness temperature | Corresponding color temperature for— | | | | | | |
|---------------------------|--------------------------------------|------|----------|------------------|--------|----------|----------|
| | Untreated carbon | Gem | Platinum | Nernst glower | Osmium | Tantalum | Tungsten |
| 1400°K. | 1414 | | 1568°K. | 1538 | 1444 | 1507 | 1492 |
| 1500 | 1515 | | 1692 | 1642 | 1562 | 1631 | 1607 |
| 1600 | 1616 | 1620 | 1821 | 1747 | 1680 | 1758 | 1723 |
| 1700 | 1718 | 1735 | 1952 | 1852 | 1799 | 1883 | 1841 |
| 1800 | 1820 | 1852 | 2086 | 1954 | 1919 | 2010 | 1961 |
| 1900 | 1923 | 1962 | | 2053 | 2045 | 2137 | 2082 |
| 2000 | 2028 | 2064 | | 2146 | 2168 | 2265 | 2206 |
| 2200 | 2240 | 2255 | | 2310 | 2427 | 2500 | 2457 |
| 2400 | | | | | 2688 | 2785 | 2718 |
| 2600 | | | | | | | 2988 |
| 3000 | | | | | | | 3564 |

TABLE 327.—Color Minus Brightness Temperature for Carbon

(Hyde, Cady, Forsythe, Phys. Rev. 10, 395, 1917.)

| | | | | | | | |
|---------------------------|-------|-------|-------|-------|-------|-------|-------|
| Brightness temp. °K. | 1600° | 1700° | 1800° | 1900° | 2000° | 2100° | 2200° |
| Color—brightness. | 2 | 7 | 12 | 16 | 22 | 28 | 33 |

TABLE 328.—Percentage Emissivities of Metals and Oxides
Emissivity of black body taken as 100

| True temperature C. | 500° | 600° | 700° | 800° | 900° | 1000° | 1100° | 1200° | Ref. |
|--|------|------|------|------|------|-------|-------|-------|------|
| 60 FeO.40 Fe ₂ O ₃ Total | 85 | 85 | 86 | 87 | 87 | 88 | 88 | 89 | 1 |
| = Fe heated in air..... $\lambda = 0.65 \mu$ | — | — | — | 98 | 97 | 95 | 93 | 92 | 1 |
| NiOTotal | — | 54 | 62 | 68 | 72 | 75 | 81 | 86 | 2 |
| $\lambda = 0.65 \mu$ | — | — | 98 | 96 | 94 | 92 | 88 | 87 | 2 |

| | | | | | | | | | | | | | |
|----------------------|-----|-----|-----|-----|-----|-----|------|------|------|------|------|------|---|
| Platinum: | | | | | | | | | | | | | |
| True temp. C..... | 0 | 100 | 200 | 300 | 400 | 500 | 750 | 1000 | 1200 | 1400 | 1600 | 1700 | 3 |
| App.* temp. C..... | — | — | — | — | — | — | — | 486 | 630 | 780 | 930 | 1005 | 3 |
| Total emiss. Pt..... | 3.1 | 4.0 | 5.1 | 6.1 | 7.0 | 8.0 | 10.3 | 12.4 | 14.0 | 15.5 | 16.9 | 17.5 | 3 |

| | | | | | | | | | | | | | |
|-----------------------------|------|------|------|------|------|------|------|------|------|------|--|--|---|
| Tungsten: | | | | | | | | | | | | | |
| True temp. K (abs.)..... | 200 | 600 | 1000 | 1400 | 1800 | 2200 | 2600 | 3000 | 3400 | 3800 | | | 4 |
| $\lambda = 0.467 \mu$ | 51.8 | 50.8 | 49.8 | 48.9 | 47.9 | 47.0 | 46.0 | 45.0 | 44.1 | 43.0 | | | 4 |
| $\lambda = 0.665 \mu$ | 48.2 | 47.2 | 46.3 | 45.3 | 44.3 | 43.3 | 42.4 | 41.4 | 40.4 | 39.5 | | | 4 |

* As observed with total radiation pyrometer sighted on the platinum.

References: (1) Burgess and Foote, Bul. Bureau of Standards, 12, 83, 1915; (2) Burgess and Foote, *loc. cit.* 11, 41, 1914; (3) Foote, *loc. cit.* 11, 607, 1914; (4) Worthing, Phys. Rev. 10, 377, 1917.

TABLE 329.—Emissivities, Metals (Black body = 1)
(Worthing, Phys. Rev., 28, 174, 1926.)

| | $t^{\circ}\text{C}$ | 0.460 μ | 0.535 μ | 0.665 μ | | $T^{\circ}\text{K}$. | 0.460 μ | 0.535 μ | 0.665 μ |
|---------------|---------------------|-------------|-------------|-------------|----------------|-----------------------|-------------|-------------|-------------|
| Gold..... | 20 | 0.635 | 0.352 | 0.062 | 1275..... | 0.632 | 0.448 | 0.140 | |
| Nickel..... | " | .45 | | .375 | 1200-1650..... | .45 | .425 | .375 | |
| Tantalum..... | " | | | .48 | 1400..... | | | .442 | |
| | | | | | 2100..... | | | .415 | |
| | | | | | 2800..... | | | .390 | |

| Platinum | 0.665 .463 | 1100°K. 0.292 | 1300° 0.297 | 1500° 0.302 1500° .370 | 1700° 0.307 1700° .381 | 1900° 0.312 1900° .392 |
|----------|---------------|---------------|-------------|---------------------------|---------------------------|---------------------------|
|----------|---------------|---------------|-------------|---------------------------|---------------------------|---------------------------|

Total radiation = $C'T^n$ watt/cm², nichrome values poor, Suydam, Phys. Rev., 5, 497, 1915.

| | | | | |
|---|---|--|--|---|
| Ag 610°- 980°K. $C' 3.0 \times 10^{-13}$ $n 4.1$ | Pt 640°- 1150°K. 2.3×10^{-15} 5.0 | Ni 463°- 1280°K. 1.0×10^{-14} 4.65 | Fe 700°- 1300°K. 3.2×10^{-17} 5.55 | Nichrome 325°- 1310°K. 1.8×10^{-12} 4.1 |
|---|---|--|--|---|

Specific values are given in this paper for various temperatures of both radiator and absorber. Also for electrical resistances.

TABLE 330.—Total Radiation from Bare and Soot-Covered Nickel (Watts/cm²)
(Barnes, Phys. Rev., 34, 1026, 1929.)

| $^{\circ}\text{K}$. | 400 | 500 | 600 | 700 | 800 | 900 | 1000 | 1200 | 1400 |
|------------------------------|-------|------|------|------|-----|-----|------|------|------|
| Soot-covered Ni..... | 0.096 | 0.28 | 0.59 | 1.87 | 3 | 3 | 4.8 | | |
| Polished Ni initial heat.... | .0092 | .032 | .079 | .166 | .31 | .55 | .91 | 2.17 | 4.49 |
| " " after above.... | .0066 | .023 | .058 | .123 | .24 | .44 | .76 | 2.04 | 4.49 |

COOLING BY RADIATION AND CONVECTION

TABLE 331.—At Ordinary Pressures

According to McFarlane* the rate of loss of heat by a sphere placed in the centre of a spherical enclosure which has a blackened surface, and is kept at a constant temperature of about 14°C , can be expressed by the equations

$$e = .000238 + 3.06 \times 10^{-6}t - 2.6 \times 10^{-8}t^2,$$

when the surface of the sphere is blackened, or

$$e = .000168 + 1.98 \times 10^{-6}t - 1.7 \times 10^{-8}t^2,$$

when the surface is that of polished copper. In these equations e is the amount of heat lost in c. g. s. units, that is, the quantity of heat, small calories, radiated per second per square centimeter of surface of the sphere, per degree difference of temperature t , and t is the difference of temperature between the sphere and the enclosure. The medium through which the heat passed was moist air. The following table gives the results.

| Difference of temperature t | Value of e . | | Ratio. |
|----------------------------------|-------------------|--------------------|--------|
| | Polished surface. | Blackened surface. | |
| 5 | .000178 | .000252 | .707 |
| 10 | .000186 | .000266 | .699 |
| 15 | .000193 | .000279 | .692 |
| 20 | .000201 | .000289 | .695 |
| 25 | .000207 | .000298 | .694 |
| 30 | .000212 | .000306 | .693 |
| 35 | .000217 | .000313 | .693 |
| 40 | .000220 | .000319 | .693 |
| 45 | .000223 | .000323 | .690 |
| 50 | .000225 | .000326 | .690 |
| 55 | .000226 | .000328 | .690 |
| 60 | .000226 | .000328 | .690 |

TABLE 332.—At Different Pressures

Experiments made by J. P. Nicol in Tait's Laboratory show the effect of pressure of the enclosed air on the rate of loss of heat. In this case the air was dry and the enclosure kept at about 8°C .

| Polished surface. | | Blackened surface. | |
|--------------------------------|--------|--------------------|--------|
| t | et | t | et |
| PRESSURE 76 CMS. OF MERCURY. | | | |
| 63.8 | .00087 | 61.2 | .01746 |
| 57.1 | .00862 | 50.2 | .01360 |
| 50.5 | .00736 | 41.6 | .01078 |
| 44.8 | .00628 | 34.4 | .00860 |
| 40.5 | .00562 | 27.3 | .00640 |
| 34.2 | .00438 | 20.5 | .00455 |
| 29.6 | .00378 | — | — |
| 23.3 | .00278 | — | — |
| 18.6 | .00210 | — | — |
| PRESSURE 10.2 CMS. OF MERCURY. | | | |
| 67.8 | .00492 | 62.5 | .01298 |
| 61.1 | .00433 | 57.5 | .01158 |
| 55 | .00383 | 53.2 | .01048 |
| 49.7 | .00340 | 47.5 | .00898 |
| 44.9 | .00302 | 43.0 | .00791 |
| 40.8 | .00268 | 28.5 | .00490 |
| PRESSURE 1 CM. OF MERCURY. | | | |
| 65 | .00388 | 62.5 | .01182 |
| 60 | .00355 | 57.5 | .01074 |
| 50 | .00286 | 54.2 | .01003 |
| 40 | .00219 | 41.7 | .00726 |
| 30 | .00157 | 37.5 | .00639 |
| 23.5 | .00124 | 34.0 | .00569 |
| — | — | 27.5 | .00446 |
| — | — | 24.2 | .00391 |

* "Proc. Roy. Soc." 1872.

† "Proc. Roy. Soc." Edinb. 1869.

See also Complan, Annal. de chim. et phys. 26, p. 526.

COOLING BY RADIATION AND CONVECTION

TABLE 333.—Cooling of Platinum Wire in Copper Envelope

Bottomley gives for the radiation of a bright platinum wire to a copper envelope when the space between is at the highest vacuum attainable the following numbers:—

$$t = 408^{\circ} \text{ C.}, \quad et = 378.8 \times 10^{-4}, \quad \text{temperature of enclosure } 16^{\circ} \text{ C.}$$

$$t = 505^{\circ} \text{ C.}, \quad et = 726.1 \times 10^{-4}, \quad \text{“ “ “ } 17^{\circ} \text{ C.}$$

It was found at this degree of exhaustion that considerable relative change of the vacuum produced very small change of the radiating power. The curve of relation between degree of vacuum and radiation becomes asymptotic for high exhaustions. The following table illustrates the variation of radiation with pressure of air in enclosure.

| Temp. of enclosure 16° C. , $t = 408^{\circ} \text{ C.}$ | | Temp. of enclosure 17° C. , $t = 505^{\circ} \text{ C.}$ | |
|---|-------------------------|---|-------------------------|
| Pressure in mm | et | Pressure in mm | et |
| 740. | 8137.0×10^{-4} | 0.094 | 1688.0×10^{-4} |
| 440. | 7971.0 “ | .053 | 1255.0 “ |
| 140. | 7875.0 “ | .034 | 1126.0 “ |
| 42. | 7591.0 “ | .013 | 920.4 “ |
| 4. | 6036.0 “ | .0046 | 831.4 “ |
| 0.444 | 2683.0 “ | .00052 | 767.4 “ |
| .070 | 1045.0 “ | .00019 | 746.4 “ |
| .034 | 727.3 “ | Lowest reached } but not measured } | 726.1 “ |
| .012 | 530.2 “ | | |
| .0051 | 430.4 “ | | |
| .00007 | 378.8 “ | | |

TABLE 334.—Effect of Pressure on Loss of Heat at Different Temperatures

The temperature of the enclosure was about 15° C. The numbers give the total radiation in therms per square centimeter per second.

| Temp. of wire in $^{\circ} \text{ C.}$ | Pressure in mm | | | | |
|--|----------------|------|------|-------|-----------------|
| | 10.0 | 1.0 | 0.25 | 0.025 | About 0.1μ |
| 100 ^o | 0.14 | 0.11 | 0.05 | 0.01 | 0.005 |
| 200 | .31 | .24 | .11 | .02 | .0055 |
| 300 | .50 | .38 | .18 | .04 | .0105 |
| 400 | .75 | .53 | .25 | .07 | .025 |
| 500 | — | .60 | .33 | .13 | .055 |
| 600 | — | .85 | .45 | .23 | .13 |
| 700 | — | — | — | .37 | .24 |
| 800 | — | — | — | .56 | .40 |
| 900 | — | — | — | — | .61 |

NOTE. — An interesting example (because of its practical importance in electric lighting) of the effect of difference of surface condition on the radiation of heat is given on the authority of Mr. Evans and himself in Bottomley's paper. The energy required to keep up a certain degree of incandescence in a lamp when the filament is dull black and when it is “flashed” with coating of hard bright carbon, was found to be as follows:—

Dull black filament, 57.9 watts.

Bright “ “ 39.8 watts.

TABLE 335.—Conduction of Heat across Air Spaces (Ordinary Temperatures)

Loss of heat by air from surfaces takes place by radiation (dependent upon radiating power of surface; for small temperature differences proportional to temperature difference; follows Stefan-Boltzmann formula, see p. 313), conduction, and convection. The two latter are generally inextricably mixed. For horizontal air spaces, upper surface warm, the loss is all radiation and conduction; with warm lower surface the loss is greater than for similar vertical space.

Vertical spaces: The following table shows that for spaces of less than 1 cm width the loss is nearly proportional to the space width, when the radiation is allowed for; for greater widths the increase is less rapid, then reaches a maximum, and for yet greater widths is slightly less. The following table is from Dickinson and van Dusen, A. S. Refrigerating Engineers J. 3, 1916.

HEAT CONDUCTION AND THERMAL RESISTANCES, RADIATION ELIMINATED,
AIR SPACE 20 CM HIGH

| Air space, cm. | Heat conduction. Cal./hour/cm ² /° C. | | | | Thermal resistance. Same units. | | | |
|----------------|---|-------|-------|-------|------------------------------------|------|------|------|
| | Temperature difference. | | | | Temperature difference. | | | |
| | 10° | 15° | 20° | 25° | 10° | 15° | 20° | 25° |
| 0.5 | 0.46 | 0.46 | 0.46 | 0.46 | 2.17 | 2.17 | 2.17 | 2.17 |
| 1.0 | 0.24 | 0.24 | 0.24 | 0.24 | 4.25 | 4.20 | 4.15 | 4.10 |
| 1.5 | 0.160 | 0.172 | 0.182 | 0.192 | 6.25 | 5.80 | 5.50 | 5.20 |
| 2.0 | 0.161 | 0.178 | 0.200 | 0.217 | 6.20 | 5.60 | 5.00 | 4.60 |
| 3.0 | 0.172 | 0.196 | 0.208 | 0.217 | 5.80 | 5.10 | 4.80 | 4.60 |

Variation with height of air space: Max. thermal resistance = 4.0 at 1.4 cm air space, 10 cm high; 6.0 at 1.6 cm, 20 cm high; 8.9 at 2.5 cm, 60 cm high.

TABLE 336.—Convection of Heat in Air at Ordinary Temperatures

In very narrow layers of air between vertical surfaces at different temperatures the convection currents, in the main, flow up one side and down the other, with eddyless (stream-line) motion. It follows that these currents transport heat to or from the surfaces only when they turn and flow horizontally, from which fact it follows, in turn, that the convective heat transfer is independent of the height of the surface. It is, according to the laws of eddyless flow, proportional to the square of the temperature difference, and to the cube of the distance between the surfaces. As the flow becomes more rapid (e.g., for a 20° difference and a distance of 1.2 cm) turbulence enters, and the above relations begin to change. For the dimensions tested, convection in horizontal layers was a little over twice that in vertical.

Taken from White, Physical Review, 10, 743, 1917.

Heat Transfer, in the Usual C.G.S. Unit, i.e., Calories per Second per Degree of Thermal Head per Square Cm. of Flat Surface, at 22.8° Mean Temperature.

Where two values are given, they show the range among determinations with different methods of getting the temperature of the outer plate. It will be seen that the value of the convection is practically unaffected by this difference of method.

| Thermal head. | 8 mm gap. | | 12 mm gap. | | 24 mm gap. | |
|---------------|-------------------|-----------------|--------------------------|----------------------|------------|---------------|
| | Total. | Convection. | Total. | Convection. | Total. | Convection. |
| 0.99° | — | — | .000 083 9 .000 084 8 | — | .000 095 | — |
| 1.98° | { .000 109 110 | — | .000 084 0 .000 085 2 | .000 000 1 000 4 | — | — |
| 4.95° | .000 111 | .000 001 | .000 086 6 88 1 | .000 002 8 003 7 | .000 090 | over .000 025 |
| 9.89° | { .000 112 113 | .000 003 003 | .000 093 7 95 2 | .000 010 .000 011 | .000 106 | over .000 010 |
| 19.76° | .000 116 | .000 007 | .000 107 7 100 4 | .000 024 020 | .000 126 | over .000 000 |

CONVECTION AND CONDUCTION OF HEAT BY GASES AT HIGH TEMPERATURES *

The loss of heat from wires at high temperatures occurs as if by conduction across a thin film of stationary gas adhering to the wire (vertical and horizontal losses very similar). Thickness of film is apparently independent of temperature of wire, but probably increases with the temperature of the gas and varies with the diameter of the wire according to the formula $b \cdot \log b/a = 2B$, where B = constant for any gas, b = diameter of film, a , of wire. The rate of convection (conduction) of heat is the product of two factors, one the shape factor, s , involving only a and B , the other a function ϕ of the heat conductivity of the gas. If W = the energy loss in watts/cm, then $W = s(\phi_2 - \phi_1)$. s may be found from the relation

$$\frac{s}{\pi} e^{-\frac{2\pi}{B}} = \frac{a}{B}; \quad \phi = 4.19 \int_0^T k dt,$$

where k is the heat conductivity of the gas at temperature T in calories/cm °C. ϕ_2 is taken at the temperature T_2 of the wire, ϕ_1 at that of the atmosphere. The following may be taken as the conductivities of the corresponding gases at high temperatures:

| | |
|--------------------|--|
| For hydrogen..... | $k = 28 \times 10^{-6} \sqrt{T} \{ (1 + .0002T)/(1 + 77T^{-1}) \}$ |
| air..... | $k = 4.6 \times 10^{-6} \sqrt{T} \{ (1 + .0002T)/(1 + 124T^{-1}) \}$ |
| mercury vapor..... | $k = 2.4 \times 10^{-6} \sqrt{T} \{ 1/(1 + 960T^{-1}) \}$ |

To obtain the heat loss: B may be assumed proportional to the viscosity of the gas and inversely proportional to the density. For air (see Table 338(b)) B may be taken as 0.43 cm; for H_2 , 3.05 cm; for Hg vapor as 0.073. Obtain s from section (a) below from a/B ; then from section (b) obtain ϕ_2 and ϕ_1 for the proper temperatures; the loss will be $s(\phi_2 - \phi_1)$ in watts/cm.

(a) s AS FUNCTION OF a/B

| s | a/B | s | a/B | s | a/B | s | a/B |
|-----|------------------------|------|-------|-----|-------|-----|-------|
| 0.0 | 0.0 | 5.0 | 0.453 | 10 | 1.696 | 30 | 7.738 |
| 0.5 | 0.735×10^{-6} | 5.5 | 0.558 | 12 | 2.263 | 32 | 8.370 |
| 1.0 | 0.594×10^{-3} | 6.0 | 0.671 | 14 | 2.844 | 34 | 8.995 |
| 1.5 | 0.725×10^{-2} | 6.5 | 0.788 | 16 | 3.438 | 36 | 9.622 |
| 2.0 | 2.75×10^{-2} | 7.0 | 0.908 | 18 | 4.040 | 38 | 10.25 |
| 2.5 | 0.0044 | 7.5 | 1.032 | 20 | 4.645 | 40 | 10.87 |
| 3.0 | 0.1176 | 8.0 | 1.160 | 22 | 5.263 | 42 | 11.50 |
| 3.5 | 0.185 | 8.5 | 1.291 | 24 | 5.877 | 44 | 12.14 |
| 4.0 | 0.265 | 9.0 | 1.424 | 26 | 6.505 | 46 | 12.77 |
| 4.5 | 0.354 | 9.5 | 1.561 | 28 | 7.122 | 48 | 13.44 |
| 5.0 | 0.453 | 10.0 | 1.696 | 30 | 7.738 | 50 | 14.03 |

(b) TABLE OF ϕ IN WATTS PER CM AS FUNCTION OF ABSOLUTE TEMP. (°K.)

| $T^\circ K.$ | H_2 | Air | Hg | $T^\circ K.$ | H_2 | Air | Hg |
|--------------|--------|--------|--------|--------------|-------|-------|--------|
| 0° | 0.0000 | 0.0000 | — | 1500° | 4.787 | 0.744 | 0.1783 |
| 100 | 0.0329 | 0.0041 | — | 1700 | 5.945 | 0.931 | 0.228 |
| 200 | 0.1294 | 0.0168 | — | 1900 | 7.275 | 1.138 | 0.284 |
| 300 | 0.278 | 0.0387 | — | 2100 | 8.655 | 1.363 | 0.345 |
| 400 | 0.470 | 0.0669 | — | 2300 | 10.18 | 1.608 | 0.411 |
| 500 | 0.700 | 0.1017 | 0.0165 | 2500 | 11.82 | 1.871 | 0.481 |
| 700 | 1.261 | 0.189 | 0.0356 | 2700 | 13.56 | — | 0.556 |
| 900 | 1.961 | 0.297 | 0.0621 | 2900 | 15.54 | — | 0.636 |
| 1100 | 2.787 | 0.426 | 0.0941 | 3100 | 17.42 | — | 0.719 |
| 1300 | 3.726 | 0.576 | 0.1333 | 3300 | 19.50 | — | 0.807 |
| 1500 | 4.787 | 0.744 | 0.1783 | 3500 | 21.79 | — | 0.898 |

* Langmuir Physical Review, 34, p. 401, 1912.

TABLE 338

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HEAT LOSSES FROM INCANDESCENT FILAMENTS

(a) WIRES OF PLATINUM SPONGE SERVED AS RADIATORS TO ROOM-TEMPERATURE SURROUNDINGS, HARTMAN, PHYSICAL REVIEW, 7, p. 431, 1916

| Diameter wire, cm. | (A) Observed heat losses in watts per cm. | | | | | | | | | |
|---|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | Absolute temperatures. | | | | | | | | | |
| | 900° | 1000° | 1100° | 1200° | 1300° | 1400° | 1500° | 1600° | 1700° | 1800° |
| 0.0690 | 1.70 | 2.26 | 3.01 | 3.88 | 4.92 | 6.18 | 7.70 | 9.63 | 12.15 | 15.33 |
| 0.0420 | 1.35 | 1.75 | 2.26 | 2.84 | 3.53 | 4.20 | 5.33 | 6.60 | 8.25 | 10.20 |
| 0.0275 | 1.12 | 1.40 | 1.70 | 2.23 | 2.73 | 3.23 | 3.91 | 4.67 | 5.72 | 7.00 |
| 0.0194 | 0.92 | 1.15 | 1.39 | 1.74 | 2.12 | 2.54 | 3.04 | 3.64 | 4.32 | 5.10 |
| | | | | | | | | | | 6.10 |
| | | | | | | | | | | 7.35 |
| (B) Heat losses corrected for radiation, watts per cm (A-C). | | | | | | | | | | |
| 0.0690 | 0.01 | 1.05 | 1.23 | 1.36 | 1.45 | 1.51 | 1.51 | 1.66 | 2.00 | 2.56 |
| 0.0420 | 0.87 | 1.02 | 1.17 | 1.31 | 1.42 | 1.45 | 1.57 | 1.76 | 2.08 | 2.43 |
| 0.0275 | 0.80 | 0.92 | 1.05 | 1.22 | 1.35 | 1.37 | 1.46 | 1.50 | 1.67 | 1.91 |
| 0.0194 | 0.70 | 0.81 | 0.89 | 1.03 | 1.15 | 1.23 | 1.31 | 1.40 | 1.47 | 1.51 |
| | | | | | | | | | | 1.64 |
| | | | | | | | | | | 1.88 |
| (C) Computed radiation, watts per cm, $\sigma = 5.61 \times 10^{-12}$ * | | | | | | | | | | |
| 0.0690 | 0.79 | 1.21 | 1.78 | 2.52 | 3.47 | 4.67 | 6.16 | 7.97 | 10.15 | 12.77 |
| 0.0420 | 0.48 | 0.73 | 1.09 | 1.53 | 2.11 | 2.84 | 3.74 | 4.84 | 6.17 | 7.77 |
| 0.0275 | 0.32 | 0.48 | 0.71 | 1.01 | 1.38 | 1.86 | 2.45 | 3.17 | 4.05 | 5.00 |
| 0.0195 | 0.22 | 0.34 | 0.50 | 0.71 | 0.97 | 1.31 | 1.73 | 2.24 | 2.85 | 3.59 |
| | | | | | | | | | | 4.46 |
| | | | | | | | | | | 5.47 |
| (D) Conduction loss by silver leads, watts per cm. | | | | | | | | | | |
| 0.0420 | 0.42 | 0.46 | 0.49 | 0.61 | 0.75 | 0.83 | 1.00 | 1.07 | 1.13 | 1.22 |
| 0.0275 | 0.13 | 0.21 | 0.28 | 0.35 | 0.43 | 0.48 | 0.55 | 0.57 | 0.60 | 0.67 |
| 0.0195 | 0.06 | 0.08 | 0.08 | 0.09 | 0.11 | 0.12 | 0.14 | 0.15 | 0.22 | 0.23 |
| | | | | | | | | | | — |
| | | | | | | | | | | — |
| (E) Convection loss by air, watts per cm. | | | | | | | | | | |
| 0.0420 | 0.45 | 0.56 | 0.63 | 0.70 | 0.67 | 0.57 | 0.59 | 0.69 | 0.95 | 1.21 |
| 0.0275 | 0.62 | 0.71 | 0.77 | 0.87 | 0.92 | 0.89 | 0.91 | 0.93 | 1.07 | 1.24 |
| 0.0195 | 0.64 | 0.73 | 0.81 | 0.94 | 1.04 | 1.11 | 1.17 | 1.25 | 1.29 | 1.30 |
| | | | | | | | | | | — |
| | | | | | | | | | | — |

* This value is lower than the presently (1919) accepted value of 5.72.

(b) WIRES OF BRIGHT PLATINUM 40-50 CM LONG SERVED AS RADIATORS TO SURROUNDINGS AT 300° K. LANGMUIR, PHYSICAL REVIEW, 34, p. 401, 1912

| Diameter wire, cm. | Observed energy losses in watts per cm. | | | | | | | |
|---|---|-------|-------|-------|-------|-------|-------|--------|
| | Absolute temperatures. | | | | | | | |
| | 500° | 700° | 900° | 1100° | 1300° | 1500° | 1700° | 1900° |
| 0.0510 | 0.22 | 0.52 | 0.90 | 1.42 | 2.03 | 2.89 | 4.10 | 5.65 |
| 0.02508 | 0.17 | 0.39 | 0.68 | 1.02 | 1.45 | 2.00 | 2.68 | 3.55 |
| 0.01262 | 0.13 | 0.31 | 0.53 | 0.79 | 1.11 | 1.46 | 1.95 | 2.71 |
| 0.00691 | 0.12 | 0.29 | 0.48 | 0.72 | 0.99 | 1.33 | 1.79 | 2.48 |
| 0.00404 | 0.11 | 0.24 | 0.41 | 0.61 | 0.84 | 1.14 | 1.54 | 2.13 |
| Energy radiated in watts per cm.* | | | | | | | | |
| 0.0510 | 0.002 | 0.013 | 0.049 | 0.137 | 0.323 | 0.67 | 1.25 | 2.15 |
| 0.02508 | 0.001 | 0.007 | 0.024 | 0.067 | 0.150 | 0.33 | 0.62 | 1.06 |
| 0.01262 | 0.001 | 0.003 | 0.012 | 0.034 | 0.080 | 0.17 | 0.31 | 0.53 |
| 0.00691 | 0.000 | 0.002 | 0.007 | 0.019 | 0.044 | 0.09 | 0.17 | 0.29 |
| 0.00404 | 0.000 | 0.001 | 0.004 | 0.011 | 0.026 | 0.05 | 0.10 | 0.17 |
| "Convection" losses in watts per cm. | | | | | | | | |
| 0.0510 | 0.22 | 0.51 | 0.85 | 1.28 | 1.71 | 2.22 | 2.85 | 3.50 |
| 0.02508 | 0.17 | 0.38 | 0.66 | 0.95 | 1.29 | 1.67 | 2.06 | 2.49 |
| 0.01262 | 0.13 | 0.31 | 0.52 | 0.75 | 1.03 | 1.29 | 1.64 | 2.18 |
| 0.00691 | 0.12 | 0.29 | 0.47 | 0.70 | 0.95 | 1.24 | 1.62 | 2.10 |
| 0.00404 | 0.11 | 0.24 | 0.41 | 0.60 | 0.81 | 1.09 | 1.44 | 1.96 |
| Thickness of theoretical conducting air film. | | | | | | | | |
| 0.0510 | 0.28 | 0.30 | 0.33 | 0.33 | 0.36 | 0.37 | 0.35 | Means. |
| 0.02508 | 0.30 | 0.37 | 0.37 | 0.41 | 0.45 | 0.45 | 0.51 | 0.34 |
| 0.01262 | 0.42 | 0.42 | 0.44 | 0.49 | 0.50 | 0.69 | 0.60 | 0.43 |
| 0.00691 | 0.31 | 0.32 | 0.38 | 0.40 | 0.43 | 0.47 | 0.38 | 0.47 |
| 0.00404 | 0.27 | 0.43 | 0.43 | 0.47 | 0.50 | 0.47 | 0.40 | 0.26 |
| Means. | 0.31 | 0.37 | 0.39 | 0.42 | 0.49 | 0.49 | 0.47 | 0.25 |
| | | | | | | | | 0.41 |
| | | | | | | | | 10.43 |

* Computed with $\sigma = 5.32$, black-body efficiency of platinum as follows (Lummer and Kurlbaum): 492° K. 0.039; 654° 0.060; 795° 0.075; 1108° 0.112; 1481° 0.154; 1761° K., 0.180. † Weighted mean.

TABLES 339 AND 340

THE SENSITIVITY OF THE EYE

Definitions: A meter-candle is the intensity of illumination due to a standard candle at a meter distance. The millilambert (0.001 lambert) measures the brightness of a perfectly diffusing (according to Lambert's cosine law) surface diffusing .001 lumen/cm². A brightness of 10 meter-candles equals 1 millilambert. 0.001 ml corresponds roughly to night exteriors, 0.1, to night interiors, 10 ml to daylight interiors and 1000, to daylight exteriors. A brightness of 100,000 meter-candles is about that of a horizontal plane for summer day with sun in zenith, 500, on a cloudy day. 4, 1st magnitude stars just visible. 0.2, full moon in zenith, .001, by starlight; in winter the intensity at noon may drop about $\frac{1}{3}$.

TABLE 339.—Spectral Variation of Sensitiveness as a Function of Intensity

Radiation is easily visible to most eyes from 0.330 μ (violet) to 0.770 μ (red). At low intensities near threshold values (gray, rod vision) the maximum of spectral sensibility lies near 0.503 μ (green) for 95% of all persons. At higher intensities, after the establishment of cone vision, the max. shifts as far as 0.500 μ . See Table 340 for more accurate values of sensitiveness after this shift has been accomplished. The ratio of optical sensation to the intensity of energy increases with increasing energy more rapidly for the red than for the shorter wave-lengths (Purkinje phenomenon); i.e., a red light of equal intensity to the eye with a green one will appear darker as the intensities are equally lowered. This phenomenon disappears above a certain intensity (above 10 millilamberts). Table due to Nutting, Bulletin Bureau of Standards.

The intensity is given for the spectrum at 0.535 μ (green).

| Intensity (meter-candles) = Ratio to preceding step = | .00024 — | .00225 9.38 | .0360 16 | .575 16 | 2.30 4 | 9.22 4 | 36.9 4 | 147.6 4 | 590.4 4 |
|---|----------------|----------------|-------------|------------|-----------|-----------|-----------|------------|------------|
| Wave-length, λ . | Sensitiveness. | | | | | | | | |
| 0.430 μ | 0.081 | 0.003 | 0.127 | 0.128 | 0.114 | 0.114 | — | — | — |
| 0.450 | 0.33 | 0.30 | 0.20 | 0.31 | 0.23 | 0.175 | 0.16 | — | — |
| 0.470 | 0.63 | 0.59 | 0.54 | 0.58 | 0.51 | 0.29 | 0.26 | 0.23 | — |
| 0.490 | 0.96 | (0.80) | (0.76) | (0.89) | (0.83) | 0.50 | 0.45 | 0.38 | 0.35 |
| 0.505 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | (0.76) | 0.66 | 0.61 | 0.54 |
| 0.520 | 0.88 | 0.86 | 0.86 | 0.94 | 0.90 | (0.85) | 0.85 | 0.85 | 0.82 |
| 0.535 | 0.61 | 0.62 | 0.63 | 0.72 | 0.91 | (0.98) | 0.98 | 0.99 | 0.98 |
| 0.555 | 0.26 | 0.30 | 0.34 | 0.41 | 0.62 | 0.84 | 0.93 | 0.97 | 0.98 |
| 0.575 | 0.074 | 0.102 | 0.122 | 0.168 | (0.39) | (0.63) | (0.76) | (0.82) | (0.84) |
| 0.590 | 0.025 | 0.034 | 0.054 | 0.091 | 0.27 | 0.49 | 0.61 | 0.68 | 0.69 |
| 0.605 | 0.008 | 0.012 | 0.024 | 0.056 | 0.173 | 0.35 | (0.45) | 0.54 | 0.55 |
| 0.625 | 0.004 | 0.004 | 0.011 | 0.027 | 0.098 | 0.20 | 0.27 | 0.35 | 0.35 |
| 0.650 | 0.000 | 0.000 | 0.003 | 0.007 | 0.025 | 0.060 | 0.085 | 0.122 | 0.133 |
| 0.670 | 0.000 | 0.000 | 0.001 | 0.002 | 0.007 | 0.017 | 0.025 | 0.030 | 0.030 |
| λ , maximum sensitiveness | 0.503 | 0.504 | 0.504 | 0.508 | 0.513 | 0.530 | 0.541 | 0.543 | 0.544 |

TABLE 340.—Threshold Sensibility as Related to Field Brightness

The eye perceives with ease and comfort a billion-fold range of intensities. The following data were obtained with the eye fully adapted to the sensitizing field, B , the field flashed off, and immediately the intensity, T , of a test spot (angular size at eye about 5°) adjusted to be just visible. This table gives a measure of the brightness, T , necessary to just pick up objects when the eye is adapted to a brightness, B . Intensities are indicated log intensities in millilamberts. Blanchard, Physical Review, 11, p. 81, 1918.

| | | | | | | | | | | | |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Log B | -7.0 | -6.0 | -5.0 | -4.0 | -3.0 | -2.0 | -1.0 | 0.0 | +1.0 | +2.0 | +3.0 |
| { Log T , white..... | — | -5.81 | -5.42 | -4.87 | -4.17 | -3.30 | -2.59 | -2.02 | -1.42 | -0.75 | +0.28 |
| { T/B | — | 1.5 | 0.38 | .13 | .068 | .050 | .026 | .0096 | .0038 | .0018 | .0019 |
| Log T , blue..... | -6.70 | -6.38 | -5.84 | -5.12 | -4.23 | -3.46 | -2.70 | -2.18 | -1.62 | — | — |
| Log T , green..... | -6.42 | -6.20 | -5.62 | -5.00 | -4.23 | -3.39 | -2.60 | -2.08 | -1.62 | -0.90 | — |
| Log T , yellow..... | — | -5.47 | -5.17 | -4.61 | -4.03 | -3.33 | -2.57 | -1.97 | -1.62 | — | — |
| Log T , red..... | — | — | -4.27 | -4.00 | -3.47 | -2.96 | -2.43 | -1.92 | -1.37 | -0.90 | — |

THE SENSIBILITY OF THE EYE

TABLE 341.—Heterochromatic Threshold Sensibility

The following table shows the decrease in sensitiveness of the eye for comparing intensities of different colors. The numbers in the body of the table correspond to the line marked *T/B* of Table 340. The intensity of the field was probably between 10 and 100 millilamberts (25 photons).

| Comparison color. | | 0.693 μ | 0.640 μ | 0.575 μ | 0.505 μ | 0.475 μ | 0.430 μ |
|--------------------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Standard color: red..... | 0.693 μ | 0.044 | 0.088 | 0.165 | 0.180 | 0.107 | 0.150 |
| yellow..... | 0.575 μ | 0.174 | 0.100 | 0.032 | 0.166 | 0.174 | 0.134 |
| green..... | 0.505 μ | 0.211 | 0.180 | 0.138 | 0.030 | 0.116 | 0.126 |
| blue..... | 0.475 μ | 0.168 | 0.180 | 0.130 | 0.130 | 0.068 | 0.142 |

TABLE 342.—Contrast or Photometric Sensibility

For the following table the eye was adapted to a field of 0.1 millilambert and the sensitizing field flashed off. A neutral gray test spot (angular size at eye, $5 \times 2.5^\circ$) the two halves of which had the contrast indicated ($\frac{1}{3}$ transparent, $\frac{2}{3}$ covered with neutral screen of transparency = contrast indicated) was then observed and the brightness of the transparent part measured necessary to just perceive the contrast after the lapse of the various times. One eye only used, natural pupil. Blanchard, *Physical Review*, 11, p. 88, 1918. Values are log brightness of brighter field in millilamberts.

| Time in seconds. | 0 | 1 | 2 | 5 | 10 | 20 | 40 | 60 |
|---------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| Contrast: 0.00..... | -2.80 | -3.47 | -3.82 | -4.30 | -4.49 | -4.60 | -4.80 | -5.03 |
| 0.30..... | -2.63 | -3.36 | -3.58 | -3.74 | -3.85 | -3.97 | -4.06 | -4.23 |
| 0.67..... | -2.40 | -3.00 | -3.13 | -3.22 | -3.21 | -3.33 | -3.46 | -3.48 |
| 0.87..... | -2.10 | -2.46 | -2.49 | -2.48 | -2.55 | -2.54 | -2.67 | -2.73 |
| 0.97..... | -1.20 | -1.57 | -1.67 | -1.69 | -1.59 | -1.63 | -1.73 | -1.78 |

TABLE 343.—Glare Sensibility

When an eye is adapted to a certain brightness and is then exposed suddenly to a much greater brightness, the latter may be called glaring if uncomfortable and instinctively avoided. Observers naturally differ widely. The data are the means of three observers, and are log brightnesses in millilamberts. The glare intensity may be taken as roughly 1700 times the cube root of the field intensity in millilamberts. Angle of glare spot, 4° . Blanchard, *Physical Review*, *loc. cit.*

| | | | | | | | | | |
|----------------|------|------|------|------|------|------|------|------|------|
| Log. field.... | -6.0 | -4.0 | -2.0 | -1.0 | 0.0 | +1.0 | 2.0 | 3.0 | 4.0 |
| Log. glare.... | 1.35 | 1.90 | 2.60 | 2.90 | 3.28 | 3.60 | 3.90 | 4.18 | 4.48 |

TABLE 344.—Rate of Adaptation of Sensibility

This table furnishes a measure of the rate of increase of sensibility after going from light into darkness, and the values were obtained immediately from the instant of turning off the sensitizing field. Both eyes were used, natural pupil, angular size of test spot, 4.0° , viewed at 35 cm. Blanchard, *loc. cit.* Retinal light persists only 10 to 20 m when one has been recently in darkness, then in a dimly lighted room; it persists fully an hour when a subject has been in bright sunlight for some time. A person who has worked much in the dark "gets his eyes" quicker than one who has not, but his final sensitiveness may be no greater.

| Sensitizing field. | Logarithmic thresholds in millilamberts after | | | | | | | | | | |
|--------------------|---|--------|--------|--------|---------|---------|---------|---------|--------|---------|---------|
| | 0 sec. | 1 sec. | 2 sec. | 5 sec. | 10 sec. | 20 sec. | 40 sec. | 60 sec. | 5 min. | 30 min. | 60 min. |
| White, 0.1 ml..... | -2.79 | -3.82 | -4.13 | -4.50 | -4.75 | -4.96 | -5.16 | -5.32 | -5.68 | -5.91 | -6.06 |
| 1.0 ml..... | -2.20 | -2.90 | -3.27 | -3.79 | -4.15 | -4.51 | -4.82 | -5.06 | -5.52 | -5.86 | -6.04 |
| 10.0 ml..... | -1.60 | -2.30 | -2.53 | -3.08 | -3.54 | -3.94 | -4.31 | -4.61 | -5.22 | -5.83 | -6.01 |
| 100.0 ml..... | -0.90 | -1.66 | -2.00 | -2.46 | -2.64 | -2.88 | -3.29 | -3.84 | -4.76 | -5.77 | -5.97 |
| Blue 0.1 ml..... | -2.82 | -3.92 | -4.36 | -4.91 | -5.27 | -5.53 | -5.68 | -5.81 | -6.23 | — | — |
| Green 0.1 ml..... | -2.69 | -4.08 | -4.39 | -4.82 | -5.11 | -5.26 | -5.43 | -5.56 | -5.80 | — | — |
| Yellow 0.1 ml..... | -2.61 | -3.84 | -4.17 | -4.41 | -4.65 | -4.78 | -5.02 | -5.00 | -5.30 | — | — |
| Red 0.1 ml..... | -2.32 | -2.69 | -2.98 | -3.37 | -3.57 | -3.65 | -3.73 | -3.80 | -4.02 | — | — |

VARIOUS PROPERTIES OF THE EYE

TABLE 345.—Apparent Diameter of Pupil and Flux Density at Retina

Flashlight measures of the pupil (both eyes open) viewed through the eye lens and adapted to various light intensities. For eye accommodated to 25 cm, ratio apparent to true pupil, 1.02, for the unaccommodated eye, 1.14. The pupil size varies considerably with the individual. It is greater with one eye closed; e.g., it was found to be for 0.01 millilambert, 6.7 and 7.2 mm; for 0.6 ml, 5.3 and 6.5; for 6.3 ml, 4.1 and 5.7; for 12.6 ml, 4.1 and 5.7 mm for both and one eye open respectively for a certain individual. At the extreme intensities the two values approach each other. The ratio of the extreme pupil openings is about 1/10, whereas the light intensities investigated vary over 1,000,000-fold (Blanchard and Reeves, partly unpublished data).

| Field millilamberts | Observed | (1.14/1.02) × Obs. | Effective area | Flux at retina, lumens per mm ² |
|------------------------|----------|-----------------------|--------------------|---|
| 0.00001 | 8 mm | 8.96 mm | 64 mm ² | 8.4×10^{-12} |
| 0.001 | 7.6 | 8.51 | 57 | 7.6×10^{-10} |
| 0.1 | 6.5 | 7.28 | 42 | 5.6×10^{-8} |
| 10 | 4.0 | 4.48 | 16 | 2.1×10^{-6} |
| 1000 | 2.07 | 2.35 | 4.3 | 5.8×10^{-5} |

TABLE 346.—Relative Visibility of Radiation (International Standard—Geneva, 1924)

(See Gibson, Tyndall, Bur. Standards Sci. Paper 475, 1923; Judd, Journ. Opt. Soc. Amer., 21, 267, 1931.) This table gives the relation between luminous sensation (light) and radiant energy. Data determined for intensities above Purkinje effect. See Table 339. Ratio of light unit (lumens) to energy unit (watt) at .55μ, 0.00162 (Ives, Coblentz, Kingsbury).

| λ μ | V_λ | λ μ | V_λ | λ μ | V_λ | λ μ | V_λ | λ μ | V_λ | λ μ | V_λ |
|----------------|-------------|----------------|-------------|----------------|-------------|----------------|-------------|----------------|-------------|----------------|-------------|
| .380 | .00004 | 5 | .030 | .510 | .503 | 5 | .915 | .640 | .175 | .710 | .0021 |
| 5 | .00006 | .450 | .038 | 5 | .608 | .580 | .870 | 5 | .138 | 5 | .0015 |
| .390 | .00012 | 5 | .048 | .520 | .710 | 5 | .816 | .650 | .107 | .720 | .00105 |
| 5 | .0002 | .460 | .060 | 5 | .793 | .590 | .757 | 5 | .082 | 5 | .00074 |
| .400 | .0004 | 5 | .074 | .530 | .862 | 5 | .695 | .660 | .061 | .730 | .00052 |
| 5 | .0006 | .470 | .091 | 5 | .915 | .600 | .631 | 5 | .045 | 5 | .00036 |
| .410 | .0012 | 5 | .113 | .540 | .954 | 5 | .567 | .670 | .032 | .740 | .00025 |
| 5 | .0022 | .480 | .139 | 5 | .980 | .610 | .503 | 5 | .023 | 5 | .00017 |
| .420 | .0040 | 5 | .169 | .550 | .995 | 5 | .441 | .680 | .017 | .750 | .00012 |
| 5 | .0073 | .490 | .208 | 5 | 1.000 | .620 | .381 | 5 | .012 | 5 | .00008 |
| .430 | .0116 | 5 | .259 | .560 | .995 | 5 | .321 | .690 | .0082 | .760 | .00006 |
| 5 | .0168 | .500 | .323 | 5 | .979 | .630 | .265 | 5 | .0057 | 5 | .00004 |
| .440 | .023 | 5 | .407 | .570 | .952 | 5 | .217 | .700 | .0041 | .770 | .00003 |
| | | | | | | | | 5 | .0029 | | |

TABLE 347.—Miscellaneous Eye Data

Light passing to the retina traverses in succession (a) front surface of the cornea (curvature, 7.0 mm); (b) cornea (equivalent water path for energy absorption, .06 cm); (c.) back surface cornea (curv., 7.9 mm); (d) aqueous humour (equiv. 11.0, .34 cm, $n = 1.337$); (e) front surface lens (c. 10 mm); (f) lens (equiv. H₂O, .42 cm, $n = 1.445$); (g) back surface lens (c., 6 mm); (h) vitreous humour (equiv. H₂O, 1.16 cm, $n = 1.337$). An equivalent simple lens has its principal point 2.34 mm behind (a), nodal point 0.48 mm in front of (g), posterior principal focus 22.73 mm behind (a), anterior principal focus 12.83 mm in front of (a), curvature, 5.125 mm. At the rear surface of the retina (.15 mm thick) are the rods (30 × 2μ) and cones (10 (6 outside fovea) μ long). Rods are more numerous, 2 to 3 between 2 cones, over 3,000,000 cones in eye. Macula lutea, yellow spot, on temporal side, 4 mm from center of retina, long axis 2 mm. Central depression, fovea centralis, .3 mm diameter, 7000 cones alone present, 6 × 2 or 3μ. In region of distinct vision (fovea centralis) smallest angle at which two objects are seen separate is 50" to 70" = 3.65 to 5.14μ at retina; 50 cones in 100μ here; 4μ between centers, 3μ to cone, 1μ to interval. Distance apart for separation greater as depart from fovea. No vision in blind spot, nasal side, 2.5 mm from center of eye, 15 mm in diam.

Persistence of vision as related to color (Allen, Phys. Rev. 11, 257, 1900) and intensity (Porter, Pr. Roy. Soc. 70, 313, 1912) is measured by increasing speed of rotating sector until flicker disappears: for color, .3μ, .031 sec.; .45μ, .020 sec.; .5μ, .015 sec.; .57μ, .012 sec.; .68μ, .011 sec.; .76μ, .018 sec.; for intensity, .06 meter-candle, .028 sec.; 1 mc, .020 sec.; 6 mc, .014 sec.; 100 mc, .010 sec.; 142 mc., .007 sec.

Sensitivity to small differences in color has two pronounced maxima (in yellow and green) and two slight ones (extreme blue, extreme red). The sensitivity to small differences in intensity is nearly independent of the intensity (Fechner's law) as indicated by the following data due to König:

| I/I_0 | 1,000,000 | 100,000 | 10,000 | 1000 | 100 | 50 | 10 | 5 | 1 | 0.1 | I_0 in mc |
|---------------------------|-----------|---------|--------|------|------|------|------|------|------|------|-------------|
| dI/I , white, | .036 | .019 | .018 | .018 | .030 | .032 | .048 | .059 | .123 | .377 | .00072 |
| .60 μ | — | .024 | .016 | .020 | .028 | .038 | .061 | .103 | .212 | — | .0050 |
| .50 μ | — | — | .018 | .018 | .024 | .025 | .036 | .049 | .080 | .133 | .00017 |
| .43 μ | — | — | — | .018 | .025 | .027 | .040 | .049 | .074 | .137 | .00012 |

PHOTOMETRIC DEFINITIONS AND UNITS

Radiant flux = Φ = rate of flow of radiation as energy, measured as ergs per second or watts.

Luminous flux = F or Ψ = rate of flow of radiation measured according to power to produce visual sensation. Although strictly thus defined, for photometric purposes it may be regarded as an entity, since the rate of flow for such purposes is invariable. Unit is the *lumen*, the flux emitted in a unit solid angle (steradian) by a point source of unit candle power.

Visibility of radiation of wave-length λ = K_λ = ratio of luminous to radiant flux for that λ , = F_λ / Φ_λ .

Mechanical equivalent of light = ratio of Φ / F for the λ of max. visibility expressed in ergs/sec / lumen or watts/lumen; it is the reciprocal of max. visibility. See p. 335.

Luminosity at wave-length λ = $(K_\lambda) (\Phi_\lambda)$. Spectral luminosity curve expresses this as a function of λ and is different for various sources.

Luminous efficiency = F / Φ expressed in lumens/watt.

Luminous intensity of (approximate) point source = I = solid-angle (ω) density of luminous flux in direction considered = $dF / d\omega$, or F / ω when the intensity is uniform. Unit, the *candle*.

Illumination on surface = E = flux density on surface = dF / dS (S is surface area) = F / S when uniform. Units, meter-candle, foot-candle, phot, lux.

Lux = one lumen per m^2 ; phot one lumen per cm^2 .

Brightness of a luminous surface may be expressed in two ways:

- (1) $b_I = dI / dS \cdot \cos \theta$ where θ is the angle between normal to surface and the line of sight; normal brightness when θ is zero.
- (2) $b_F = dF / dS'$ assuming that the surface is a perfect diffuser, obeying cos. law of emission or reflection. Unit, the lambert.

Specific luminous radiation, E' = luminous flux density emitted by a surface, or the flux emitted per unit of emissive area, expressed in lumens per cm^2 . For surfaces obeying Lambert's cosine law, $E' = \pi b_0$.

The lambert, the cgs unit of brightness, is the brightness of a perfectly diffusing surface radiating or reflecting one lumen per cm^2 . Equivalent to a perfectly diffusing surface with illumination of one phot. A perfectly diffusing surface emitting one lumen per ft^2 has a brightness of 1.076 millilamberts. Brightness in candles per cm^2 is reduced to lamberts by multiplying by π .

A uniform point source of one candle emits 4π lumens.

One lumen is emitted by .07058 spherical candle power.

One lumen emitted per ft^2 = 1.076 millilamberts (perfect diffusion).

One spherical candle power emits 12.57 lumens.

One lux = 1 lumen incident per m^2 = .0001 phot = .1 milliphot.

One phot = 1 lumen incident per cm^2 = 10,000 lux = 1000 milliphots.

One milliphot = .001 phot = .020 foot-candle.

One foot-candle = 1 lumen incident per ft^2 = 1.076 milliphots = 10.76 lux.

One lambert = 1 lumen emitted per cm^2 of a perfectly diffusing surface.

One millilambert = .020 lumen emitted per ft^2 (perfect diffusion).

One lambert = .3183 candle per cm^2 = 2.054 candles per in^2 .

One candle per cm^2 = 3.1416 lamberts.

One candle per in^2 = .4868 lambert = 486.8 millilamberts.

Adapted from Reports of Committee on Nomenclature and Standards of Illuminating Engineering Society. 1916 to 1918.

TABLE 349.—Photometric Standards

In Germany the Hefner lamp is most used; in England the Pentane lamp and sperm candles; in France the Carcel lamp is preferred; in America the Pentane and Hefner lamps are used to some extent, but candles are largely employed in gas photometry. For the photometry of electric lamps, and in accurate photometric work, electric lamps, standardized at a national standardizing institution, are employed.

The "International candle" designates the value of the candle as maintained by cooperative effort between the national laboratories of England, France, and America; and the value of various photometric units in terms of this is given in the following table (Circular No. 15 of the Bureau of Standards).

- 1 International Candle = 1 Pentane Candle.
- 1 International Candle = 1 Bougie Decimale.
- 1 International Candle = 1 American Candle.
- 1 International Candle = 1.11 Hefner Unit.
- 1 International Candle = 0.104 Carcel Unit.

- 1. Standard Pentane Lamp, burning pentane..... 10.0 candles.
- 2. Standard Hefner Lamp, burning amyl acetate..... 0.9 candles.
- 3. Standard Carcel Lamp, burning colza oil..... 9.6 candles.
- 4. Standard English Sperm Candle, approximately..... 1.0 candles.

TABLE 350.—The Waidner-Burgess Standard of Light

The Waidner-Burgess standard light consists in immersing a hollow inclosure in a bath of molten platinum and observing the light from the inclosure during the period of freezing. The exceptionally pure Pt was in a thorium oxide crucible heated by an induction furnace. At all times before and after test the Pt was 99.997% pure. Reproducible to 0.1% the brightness is

58.84 International Candles per cm^2

(Wensel, Roeser, Barbrow, Caldwell, Bur. Standards Journ. Res., 6, 1103, 1931.)

TABLE 351.—Intrinsic Brightness of Various Light Sources

| | Barrows. | Ives & Luckiesh. | | National Electric Lamp Association. |
|---|--|--|--|--|
| | C. P. per Sq. In. of surface of light. | C. P. per Sq. In. of surface of light. | C. P. per Sq. Mm. of surface of light. | C. P. per Sq. In. of surface of light. |
| Sun at Zenith | 600,000 | — | — | 600,000 |
| Crater, carbon arc | 200,000 | 84,000 | 130. | 200,000 |
| Open carbon arc | 10,000-50,000 | — | — | 10,000-50,000 |
| Flaming arc | 5,000 | — | — | 5,000 |
| Magnetite arc | — | 4,000 | 6.2 | — |
| Nernst Glowler | 800-1,000 | (115v.6 amp. d.c.) 3,010 | 4.7 | (1.5 w.p.c.) 2,200 |
| Tungsten incandescent, 1.15 w. p. c. | — | — | — | 1,000 |
| Tungsten incandescent, 1.25 w. p. c. | 1,000 | 1,000 | 1.64 | 875 |
| Tantalum incandescent, 2.0 w. p. c. | 750 | 580 | 0.9 | 750 |
| Graphitized carbon filament, 2.5 w. p. c. | 625 | 750 | 1.2 | 625 |
| Carbon incandescent, 3.1 w. p. c. | 450 | 485 | 0.75 | 480 |
| Carbon incandescent, 3.5 w. p. c. | 375 | 400 | 0.63 | 375 |
| Carbon incandescent, 4.0 w. p. c. | 300 | 325 | 0.50 | — |
| Inclosed carbon arc (d. c.) | 100-500 | — | — | 100-500 |
| Inclosed carbon arc (a. c.) | — | — | — | 75-200 |
| Acetylene flame (1 ft. burner) | 75-100 | 53.0 | 0.082 | 75-100 |
| Acetylene flame ($\frac{1}{3}$ ft. burner) | — | 33.0 | 0.057 | — |
| Welsbach mantle | 20-25 | 31.9 | 0.048 | 20-50 |
| Welsbach (mesh) | — | 56.0 | 0.067 | — |
| Cooper Hewitt mercury vapor lamp | 16.7 | 14.9 | 0.023 | 17 |
| Kerosene flame | 4-8 | 9.0 | 0.014 | 3-8 |
| Candle flame | 3-4 | — | — | 3-4 |
| Gas flame (fish tail) | 3-8 | 2.7 | 0.004 | 3-8 |
| Frosted incandescent lamp | 4-8 | — | — | 2-5 |
| Moore carbon-dioxide tube lamp | 0.6 | — | — | 0.3-1.75 |

Taken from *Data*, 1911.

BRIGHTNESS OF BLACK BODY. CROVA WAVE-LENGTH. MECHANICAL EQUIVALENT OF LIGHT. LUMINOUS INTENSITY AND EFFICIENCY OF BLACK BODY

The values of L , the luminous intensity, are given in light watts/steroradian/cm² of radiating surface = $(1/\pi) \int_0^\infty V_\lambda E_\lambda d\lambda$, where V_λ is the visibility of radiation function.

Mechanical equivalent. The unit of power is the watt; of luminous flux, the lumen. The ratio of these two quantities for light of maximum visibility, $\lambda = 0.556 \mu$, is the stimulus coefficient V_m ; its reciprocal is the (least) mechanical equivalent of light, i.e., least since applicable to radiation of maximum visibility. A better term is "luminous equivalent of radiation of maximum visibility." One lumen = 0.001406 watts (Hyde, Forsythe, Cady); or 1 watt of radiation of maximum visibility ($\lambda = 0.556 \mu$) = 0.698 lumen.

White light has sometimes been defined as that emitted by a black body at 6000° K. The Crova wave-length for a black body is that wave-length, λ , at which the luminous intensity varies by the same fractional part that the total luminous intensity varies for the same change in temperature.

TABLE 352.—Brightness, Crova Wave-length of Black Body, Mechanical Equivalent of Light *

| Temp. ° K. | Bright- ness, candles per cm ² | Crova wave- length, μ | Mech. equiv. watts per l . |
|---------------|--|------------------------------------|---------------------------------------|
| 1700° | 5.1 | 0.584 | 0.001478 |
| 1750 | 7.6 | 0.583 | — |
| 1800 | 11.3 | 0.582 | 0.001491 |
| 1850 | 16.3 | 0.581 | — |
| 1900 | 23.1 | 0.580 | 0.001498 |
| 1950 | 32.2 | 0.579 | — |
| 2000 | 44.3 | 0.578 | 0.001498 |
| 2050 | 60.0 | 0.577 | — |
| 2100 | 80.1 | 0.576 | 0.001497 |
| 2150 | 105.7 | 0.576 | — |
| 2200 | 137.6 | 0.575 | 0.001496 |
| 2250 | 177. | 0.574 | — |
| 2300 | 226. | 0.574 | 0.001497 |
| 2350 | 284. | 0.573 | — |
| 2400 | 351. | 0.572 | 0.001497 |
| 2450 | 438. | 0.572 | — |
| 2500 | 537. | 0.571 | 0.001502 |
| 2550 | 651. | 0.570 | — |
| 2600 | 785. | 0.570 | 0.001511 |
| 2650 | 939. | 0.569 | — |
| Mean..... | | | 0.001496 |

* Hyde, Forsythe, Cady, Phys. Rev. 13, p. 45, 1916.

TABLE 353.—Luminous and Total Intensity and Radiant Luminous Efficiency of Black Body *

| T , degrees absolute. | Luminous intensity L watt cm ² | Total intensity σT^4 watt/cm ² | Radiant luminous efficiency. |
|----------------------------|---|--|------------------------------------|
| 1,200 | 2.34×10^{-5} | 3.762 | .000006 |
| 1,600 | 3.45×10^{-3} | 1.189 | .000290 |
| 1,700 | 8.46×10^{-3} | 1.515×10 | .000558 |
| 1,800 | 1.88×10^{-2} | 1.905×10 | .000987 |
| 1,900 | 3.85×10^{-2} | 2.365×10 | .00163 |
| 2,000 | 7.34×10^{-2} | 2.903×10 | .00253 |
| 2,100 | 1.32×10^{-1} | 3.520×10 | .00374 |
| 2,200 | 2.26×10^{-1} | 4.250×10 | .00532 |
| 2,300 | 3.69×10^{-1} | 5.077×10 | .00727 |
| 2,400 | 5.79×10^{-1} | 6.020×10 | .00962 |
| 2,500 | 8.77×10^{-1} | 7.087×10 | .0124 |
| 2,600 | 1.29 | 8.291×10 | .0156 |
| 3,000 | 4.60 | 1.470×10^2 | .0317 |
| 4,000 | 3.85×10 | 4.645×10^2 | .0820 |
| 5,000 | 1.36×10^2 | 1.134×10^3 | .1201 |
| 6,000 | 3.26×10^2 | 2.351×10^3 | .1386 |
| 7,000 | 6.03×10^2 | 4.356×10^3 | .1385 |
| 8,000 | 9.59×10^2 | 7.432×10^3 | .1290 |
| 10,000 | 1.84×10^3 | 1.814×10^4 | .1014 |

* Coblentz, Emerson, Bul. Bureau of Standards, 14, p. 255, 1917.

NOTE.—Minimum energy necessary to produce the sensation of light: Ives, 38×10^{-10} ; Russell, 7.7×10^{-10} ; Reeves, 19.5×10^{-10} ; Buisson, 12.6×10^{-10} erg. sec. (Buisson, J. de Phys. 7, 63, 1917.)

Color temperature (temp. black-body same color) 500 w. gas-filled lamp (32 l/w) 3682°K; 900 w. gas-filled movie lamp, 22.7 l w, 3686°K. crater 65v. 10 amp. arc, solid carbon, 3786°K. cratered carbon 3420°K. Priest, 1922.

TABLE 354.—Color of Light Emitted by Various Sources *

| Source. | Color, per cent white. | Hue. | Source. | Color, per cent white. | Hue. |
|-----------------------------------|------------------------------|------|------------------------------------|------------------------------|------|
| Sunlight..... | 100 | — | N-filled tungsten, 0.50 wpc..... | 45 | 584 |
| Average clear sky..... | 60 | 472 | N-filled tungsten, 0.35 wpc..... | 53 | 584 |
| Standard candle..... | 13 | 593 | Mercury vapor arc..... | 79 | 490 |
| Hefner lamp..... | 14 | 593 | Helium tube..... | 32 | 598 |
| Pentane lamp..... | 15 | 592 | Neon tube..... | 6 | 605 |
| Tungsten glow lamp, 1.25 wpc..... | 35 | 588 | Crater of carbon arc, 1.8 amp..... | 59 | 585 |
| Carbon, low lamp, 3.8 wpc..... | 25 | 592 | Crater of carbon arc, 3.2 amp..... | 62 | 585 |
| Nernst glower, 1.50 wpc..... | 31 | 587 | Crater of carbon arc, 5.0 amp..... | 67 | 583 |
| N-filled tungsten, 1.00 wpc..... | 34 | 586 | Acetylene flame (flat)..... | 36 | 580 |

* Jones, L. A., Trans. Ill. Eng. Soc., Vol. 9 (1914).

RELATIVE BLUE BRIGHTNESS, B , AND BRIGHTNESS IN CANDLES PER CM.² C , OF SOME INCANDESCENT OXIDES AT VARIOUS RED (0.665 μ) BRIGHTNESS TEMPERATURES, S_R

| Material | $S_R = 1500$ | | 1700 | | 1800 | | 1900 | | 2000 | |
|--------------------------------|--------------|------|------|------|------|-----|------|-----|------|------|
| | B | C | B | C | B | C | B | C | B | C |
| Black body | .026 | 0.79 | 0.27 | 5.0 | 0.74 | 11. | 1.80 | 23. | 3.9 | 44. |
| Tungsten | .038 | .84 | .41 | 5.9 | 1.11 | 14. | 2.7 | 33. | 6.3 | 74. |
| Urania, gas air and oxy-gas... | .028 | 1.02 | .31 | 6.6 | .84 | 15. | 2.0 | 35. | 4.5 | 78. |
| Ceria, pure: Oxy-gas..... | .035 | 1.08 | .32 | 6.3 | .83 | 14. | 1.9 | 31. | 4.0 | 62. |
| “ , yellow: “ | .032 | 1.04 | .32 | 7.1 | .85 | 17. | 2.0 | 40. | 4.0 | 88. |
| “ , brown: “ | .033 | 1.15 | .30 | 6.7 | .83 | 15. | 1.68 | 33. | 3.5 | 68. |
| Oxides of Ce group: Oxy-gas. | .031 | .97 | .34 | 6.3 | .92 | 14. | 2.3 | 33. | 5.0 | 71. |
| Neodymia: Oxy-gas | .032 | 1.17 | .33 | 6.9 | .92 | 15. | 2.3 | 33. | 5.0 | 64. |
| Lanthana: “ | .033 | 1.11 | .34 | 6.6 | .89 | 15. | 2.1 | 33. | 4.5 | 64. |
| Erbia: “ | .047 | 1.71 | .45 | 8.1 | 1.17 | 16. | 2.7 | 33. | 5.6 | 63. |
| Yttria, pure: Oxy-gas..... | .067 | 1.18 | .61 | 7.3 | 1.56 | 17. | 3.6 | 32. | 7.3 | 63. |
| “ , 95% pure: “ | .047 | 1.20 | .46 | 7.3 | 1.19 | 16. | 2.8 | 36. | 5.9 | 75. |
| Zirconia: Oxy-gas | .058 | .73 | .55 | 3.6 | 1.43 | 8. | 3.3 | 15. | 7.0 | 30. |
| Thoria: “ | .033 | 1.44 | .56 | 7.5 | 1.40 | 16. | 3.1 | 32. | 6.3 | 63. |
| Alumina: “ | .076 | 1.45 | .87 | 9.4 | 2.5 | 22. | 6.1 | 49. | 13.6 | 103. |
| Beryllia: “ | .086 | 1.62 | .99 | 9.7 | 2.8 | 22. | 6.9 | 49. | 15.4 | 104. |
| Magnesia: “ | .21 | 2.4 | 1.31 | 11.0 | 2.8 | 22. | 5.6 | 43. | 10.2 | 79. |
| Thoria 1% ceria: Oxy-gas... | .078 | 1.45 | .70 | 8.6 | 1.71 | 19. | 4.1 | 43. | 8.4 | 90. |
| “ “ urania: “ ... | .069 | 1.33 | .67 | 8.3 | 1.77 | 19. | 4.1 | 44. | 8.7 | 93. |
| “ trace urania: “ ... | .059 | 1.33 | .68 | 8.3 | 1.93 | 19. | 4.8 | 44. | 10.5 | 93. |
| “ 1% neodymia: “ ... | .046 | 1.43 | .43 | 7.1 | 1.14 | 15. | 2.6 | 29. | 5.5 | 56. |
| “ “ Mn oxide: “ ... | .035 | 1.13 | .37 | 6.1 | 1.01 | 13. | 2.4 | 28. | 5.3 | 56. |

NOTE.—1 microcalorie through 1 cm² at 1 m = 0.034 sperm calorie = 0.0385 Hefner unit (no diaphragm) = 0.043 Hefner unit (diaphragm 14 × 50 mm). Coblenz, Bull. Bur. of Stds., 11, 87, 1914.

EFFICIENCY OF VARIOUS ELECTRIC LIGHTS

| Bryant and Hake, Eng. Exp. Station, Univ. of Ill. | Amperes. | Terminal Watts. | Lumens. | Kw-hours for 100,000 lumen- hours. | Total cost per 100,000 Lumen-hours at 10 cts. per Kw-hour. |
|--|----------|--------------------|---------|---|--|
| Regenerative d.-c., series arc | 5.5 | 385 | 11,670 | 3.3 | 0.339 |
| Regenerative d.-c., multiple arc | 5.5 | 605 | 11,670 | 5.18 | 0.527 |
| Magnetite d.-c., series arc | 6.6 | 528 | 7,370 | 7.16 | 0.729 |
| Flame arc, d.-c., inclined electrodes | 10.0 | 550 | 8,640 | 6.37 | 0.837 |
| Mercury arc, d.-c., multiple | 3.5 | 385 | 4,400 | 15.92 | 0.89 |
| Flame arc, d.-c., inclined electrodes | 8.0 | 440 | 6,140 | 7.16 | 0.966 |
| Flame arc, d.-c., vertical electrodes | 8.0 | 440 | 6,140 | 7.16 | 0.966 |
| Luminous arc, d.-c., multiple | 6.6 | 726 | 7,370 | 9.85 | 0.988 |
| Open arc, d.-c., series | 9.6 | 480 | 5,025 | 9.55 | 1.079 |
| Magnetite arc, d.-c., series | 4.0 | 320 | 2,870 | 11.15 | 1.13 |
| Flame arc, a.-c., vertical electrodes | 10.0 | 467 | 5,340 | 8.75 | 1.275 |
| Flame arc, a.-c., inclined electrodes | 10.0 | 467 | 5,340 | 8.75 | 1.275 |
| Open arc, d.-c., series | 6.6 | 325 | 2,920 | 11.15 | 1.305 |
| Tungsten series | 6.6 | 75 | 626 | 12.0 | 1.384 |
| Flame arc, a.-c., inclined electrodes | 8.0 | 374 | 3,910 | 9.55 | 1.405 |
| Inclosed arc, d.-c., series | 6.6 | 475 | 3,315 | 14.32 | 1.459 |
| Luminous arc, d.-c., multiple | 4.0 | 440 | 2,870 | 15.32 | 1.547 |
| Tungsten, multiple | 0.545 | 60 | 475 | 12.6 | 1.55 |
| Nernst, a.-c., 3-glowler | 1.87 | 414 | 2,160 | 19.2 | 1.88 |
| Nernst, d.-c., 3-glowler | 1.87 | 414 | 2,160 | 19.2 | 1.90 |
| Inclosed arc, a.-c., series | 7.5 | 480 | 2,410 | 19.9 | 2.05 |
| Inclosed arc, a.-c., series | 6.6 | 425 | 2,020 | 21.3 | 2.193 |
| Tantalum, d.-c., multiple | — | 40 | 199 | 21.1 | 2.31 |
| Tantalum, a.-c., multiple | — | 40 | 199 | 21.1 | 2.504 |
| Carbon, 3.1 w. p. c., multiple | — | 49.6 | 166 | 29.9 | 3.24 |
| Carbon, 3.5 w. p. c., series | 6.6 | 210 | 626 | 33.6 | 3.47 |
| Carbon, 3.5 w. p. c., multiple | — | 56 | 166 | 33.7 | 3.59 |
| Inclosed arc, d.-c., multiple | 5.0 | 550 | 1,535 | 35.8 | 3.66 |
| Inclosed arc, d.-c., multiple | 3.5 | 385 | 1,030 | 37.4 | 3.84 |
| Inclosed arc, a.-c., multiple | 6.0 | 430 | 1,124 | 38.3 | 3.94 |
| Inclosed arc, a.-c., multiple | 4.0 | 285 | 688 | 41.4 | 4.265 |

| Ives, Phys. Rev., V, p. 390, 1915 (see also VI, p. 332, 1915); computed assuming 1 lumen = 0.00159 watt. | Commercial Rating | Lumens per Watt. | Luminous Watts Flux ÷ Watts In- put or True Efficiency. |
|--|----------------------------------|------------------------|---|
| Open flame gas burner | Bray 6' high pressure | 0.22 | 0.00035 |
| Petroleum lamp | | .26 | .0004 |
| Acetylene | 1.0 liters per hour | .67 | .0011 |
| Incandescent gas (low pressure) | .350 lumens per B. t. u. per hr. | 1.2 | .0019 |
| Incandescent gas (high pressure) | .578 lumens per B. t. u. per hr. | 2.0 | .0031 |
| Nernst lamp | | 4.8 | .0076 |
| Moore nitrogen vacuum tube | 220-v. 60-cycle, 113 ft. | 5.21 | .0083 |
| Carbon incandescent (treated filament) | 4-watts per mean hor. C. P. | 2.6 | .0041 |
| Tungsten incandescent (vacuum) | 1.25 watts per hor. C. P. | 8. | .013 |
| Carbon arc, open arc | 9.6 amp. clear globe | 11.8 | .019 |
| Mazda, type C | 500-watt multiple .7 w. p. c. | 15. | .024 |
| Mazda, type C | 600 C. P. -20 amp. .5 w. p. c. | 19.6 | .031 |
| Magnetite arc, series | 6.6 amp. direct current | 21.6 | .034 |
| Glass mercury arc | 40-70 volt; 3.5 amperes | 23. | .036 |
| Quartz mercury arc | 174-197 volt; 4.2 amperes | 42. | .067 |
| Enclosed white flame carbon arc | 10 ampere, A. C. | 26.7 | .042 |
| “ “ “ “ “ | 6.5 ampere, D. C. | 35.5 | .057 |
| Open arc “ “ “ “ “ | 10 ampere, A. C. | 29. | .046 |
| “ “ “ “ “ | 10 ampere, D. C. | 27.7 | .044 |
| Enclosed yellow flame carbon arc | 10 ampere, A. C. | 31.4 | .050 |
| “ “ “ “ “ | 6.5 ampere, D. C. | 34.2 | .054 |
| Open arc, “ “ “ “ “ | 10 ampere, A. C. | 41.5 | .066 |
| “ “ “ “ “ | 10 ampere, D. C. | 44.7 | .071 |

TABLE 357.—Color Temperature, Brightness Temperature, and Brightness of Various Illuminants

| Source | T_c | S ($\lambda = .665$) | Brightness c/cm^2 |
|----------------------------------|-------|--------------------------|------------------------|
| Gas flame | | | |
| Batswing | 2160 | | |
| Candle shape about 10 cm high | 1875 | | |
| Hefner as a whole | 1880 | | |
| Candle | | | |
| Sperm | 1930 | | |
| Paraffin | 1925 | | |
| Pentane | | | |
| 10-cp. std. | 1920 | | |
| Kerosene | | | |
| Flat wick | 2055 | 1500 | 1.27 |
| Round wick | 1920 | 1530 | 1.51 |
| 4 w p. c. carbon | 2080 | 2030 | 54.9 |
| 3.1 w p. c. treated carbon | 2165 | 2065 | 70.6 |
| 2.5 w p. c. gem | 2195 | 2130 | 78.1 |
| 2 w p. c. osmium | 2185 | 2035 | 60.8 |
| 2 w p. c. tantalum | 2260 | 2000 | 53.1 |
| Acetylene as a whole | 2380 | | |
| One spot | 2465 | 1660 | 6.69 |
| Mees burner | 2360 | 1730 | 10.8 |
| 1.25 w p. c. tungsten | 2400 | 2150 | 125 |
| 2.3 w p. c. Nernst | 2400 | 2320 | 258 |
| Sun | | | |
| Outside atmosphere | 6500 | | 224000 |
| At earth's surface | 5600 | | 165000 |

TABLE 358.—Temperature, Efficiency, and Brightness of Vacuum Lamps

| Lamp | Lumens per watt | Maximum temperature, K. | Maximum brightness candles/cm ² |
|-----------------------|--------------------|-------------------------------|--|
| 50-watt carbon..... | 3.3 | 2115° | 55 |
| 50-watt gem..... | 4.0 | 2180 | 78 |
| 50-watt tantalum..... | 4.9 | 2160 | 53 |
| 10-watt tungsten..... | 7.7 | 2355 | 128 |
| 25-watt tungsten..... | 9.8 | 2450 | 193 |
| 40-watt tungsten..... | 10 | 2460 | 206 |
| 60-watt tungsten..... | 10.1 | 2465 | 211 |

TABLE 359.—Temperature, Efficiency, and Brightness of Gas-Filled Tungsten Lamps

| Lamp | Lumens per watt | Maximum temperature, K. | Average color temperature, K. | Maximum brightness of filament candles/cm ² |
|-----------------------------|--------------------|-------------------------------|--|---|
| Regular gas-filled lamps: | | | | |
| 50-watt..... | 10.0 | 2685° | 2670° | 469 |
| 75-watt..... | 11.8 | 2735 | 2705 | 563 |
| 100-watt..... | 12.9 | 2760 | 2740 | 605 |
| 200-watt..... | 15.2 | 2840 | 2810 | 781 |
| 300-watt..... | 16.3 | 2870 | 2840 | 862 |
| 500-watt..... | 18.1 | 2930 | 2920 | 1015 |
| 1000-watt..... | 20.0 | 2990 | 2980 | 1225 |
| 2000-watt..... | 21.2 | 3020 | 3000 | 1350 |
| Special lamps: | | | | |
| 1000-watt stereopticon..... | 24.2 | 3185 | 3175 | 2065 |
| 900-watt movie..... | 27.3 | 3200 | 3220 | 2660 |
| 10-kw..... | 31.0 | 3350 | 3300 | 3050 |
| 30-kw..... | 31.0 | 3350 | 3300 | 3050 |
| Daylight lamps: | | | | |
| 200-watt..... | 10.0 | 2860 | | |
| 500-watt..... | 11.2 | 2960 | | |
| Photographic: | | | | |
| 750-watt..... | | 3065 | | |
| 1500-watt..... | | 3105 | | |

TABLE 360.—Energy Distribution for Some Tungsten Lamps

(Taken from Forsythe, Christison, Gen. Electr. Rev., p. 662, 1929.)

| | 500 w, 1000 hr. | | 500 w, 100 hr. | | 900 w movie | | tungsten arc* | |
|-------------------|-----------------|-------------|----------------|-------------|-------------|-------------|---------------|-------------|
| | % | milli-watts | % | milli-watts | % | milli-watts | % | milli-watts |
| 0.31–0.29 μ | 0.011 | 0.00044 | 0.015 | 0.006 | 0.030 | 0.0028 | 0.095 | 0.0108 |
| below 0.325 μ | .032 | .0013 | .042 | .0017 | .083 | .0076 | .26 | .030 |
| “ 0.35.... | .08 | .003 | .10 | .004 | .18 | .017 | .52 | .059 |
| “ 0.40.... | .31 | .012 | .38 | .015 | .63 | .058 | 1.53 | .17 |
| 0.40–0.76.... | 15.7 | .63 | 16.7 | .67 | 19.4 | 1.8 | 27.0 | 3.1 |
| Total..... | | 4.0 | | 4.0 | | 9.2 | | 11.4 |

* Calculated for cm² of molten tungsten.

TABLE 361.—Brightness of Filaments and Bulbs of Some Tungsten Lamps and of Some Other Sources for Comparison

| Lamp | Brightness measured at— | Brightness candles/cm ² |
|---|-------------------------|------------------------------------|
| Kerosene flame..... | Flat wick | 1.2 |
| 4-watt per candle carbon lamp..... | Filament | 55.0 |
| 40-watt vacuum tungsten lamp..... | Filament | 206 |
| 40-watt vacuum tungsten lamp..... | Bulb-frosted | 2.5 |
| 40-watt golden Mazda..... | Bulb | 2.0 |
| 50-watt white Mazda..... | Filament | 408 |
| 50-watt white Mazda..... | Bulb | 1.3 |
| 75-watt white Mazda sprayed..... | Filament | 563 |
| 75-watt white Mazda sprayed..... | Bulb | 2.1 |
| 2000-watt gas-filled Mazda..... | Filament | 1,350 |
| 2000-watt gas-filled Mazda..... | Between coil | 3,000 |
| 2000-watt gas-filled Mazda..... | Bulb-frosted | 130 |
| Sun as observed at earth's surface..... | | 165,000 |
| Clear sky, average..... | | .4 |

TABLE 362.—Characteristics of Some Miniature Lamps

(Forsythe, Watson, Gen. Electr. Rev., 34, 734, 1931.)

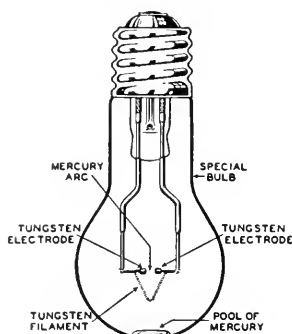
| Automobile Mazda lamps | | | | | | Flash-light lamps | | | | | |
|------------------------|---------------------------|-------|--------------|-----------------------|-------------|-------------------|-------|--------------|-----------------------|-------------|--|
| No. | Service | Volts | Candle power | Watts per sph. candle | Max. T. °K. | No. | Volts | Candle power | Watts per sph. candle | Max. T. °K. | |
| 63 | Rear, instrument bd.... | 6.85 | 2.9 | 1.32 | 2820 | 19 | 1.25 | 0.19 | 4.10 | 2570 | |
| 67 | Step, aux. headlight.... | 13.5 | 2.9 | 1.27 | 2810 | 1 | 2.25 | .40 | 1.39 | 2665 | |
| 81 | Dome, panel..... | 6.9 | 6.3 | 1.01 | 2915 | 11 | 2.33 | .46 | 1.36 | 2665 | |
| 87 | Signal..... | 6.75 | 14.4 | .80 | 2980 | 35 | 2.40 | 1.45 | 1.35 | 2635 | |
| 89 | Dome, panel..... | 13.5 | 6.3 | .99 | 2870 | 14 | 2.47 | .54 | 1.41 | 2700 | |
| 1110 | Headlight, depres. beam | 6.5 | 21.5 | .76 | 2975 | 16 | 2.47 | .52 | 1.39 | 2565 | |
| 1129 | Head and spotlight.... | 6.5 | 20.5 | .76 | 2930 | 13 | 3.70 | .98 | 1.11 | 2670 | |
| 1133 | “ “ “ “ “ “ “ “ “ “ | 6 | 31.9 | .70 | 3045 | 17 | 3.70 | 1.02 | 1.06 | 2595 | |
| 1141 | Headlight..... | 13 | 21.9 | .70 | 2960 | 31 | 6.15 | 2.14 | .87 | 2770 | |
| 1142 | Motor coach..... | 12.5 | 20.6 | .80 | 2885 | | | | | | |
| 1150 | Side and headlight.... | 44 | 21.7 | .99 | 2815 | * | 1.5 | .028 | 6.0 | 2115 | |
| 1158 | Ford 2 fil. headlight.... | 6.5 | 20.9 | .81 | 2925 | † | 10 | 80 | .62 | 3160 | |
| 1183 | Spotlight..... | 5.5 | 1.9 | 2.2 | 2500 | | 5 | .48 | .63 | 3200 | |
| 1000 | Headlight, depres. beam | 6 | 49.1 | .72 | 3055 | § | 8.5 | .55 | .62 | 3120 | |
| | | | 31 | .73 | 2965 | ** | 6 | .60 | 1.52 | 2485 | |

* Surgical (grain-o'-wheat) 2 mm diam., 8.7 mm long, 0.06 g. † RCA photophone photo-tube exciter. || R C A recorder. § Western Electric sound-picture photo-tube exciter. ** Radio 40.

Feb., 1932, Gen. Electr. Rev., 50 K watt; 120 v; 3300°K.; 1,400,000 lumens; max. candle power 166,000 24 lumens/watt. 10 K watt; 120 v; 3300°K.; 280,000 lumens; max. candle power 33,000; 24 lumens/watt.

TABLE 363.—Characteristics of Sunlight Mazda Lamp (S1) 300 Watts a.c. Combined Incandescent Tungsten, Mercury Arc, Special High Transmission Bulb

For more detailed data see Taylor, Journ. Opt. Soc. Amer., 21, 20, 1931; Forsythe, Barnes, Easley, loc.cit. p. 30, Gen. Electr. Rev., 33, 358, 1930.



Characteristics of S1 lamp: distance between electrodes 5.4 mm. Current 31 + amp., voltage 11 volts; light output 5670 lumens. Efficiency, 17.6 lumens/watt; % light from mercury arc, 20; light from filament 100 lumens; max. temp. electrodes 3200° K, of filament 2330° K. Temp. of Hg 285° C, pressure of Hg vapor, 177 mm Hg.

Transmission of 1 mm of glass used:

| | | | | | | | | | | |
|-----------------------------|------|------|------|------|------|------|------|------|------|------|
| λ in Angstroms..... | 2500 | 2600 | 2700 | 2800 | 2900 | 3100 | 3300 | 3500 | 4000 | 5000 |
| % transmissible | 10 | 20 | 33 | 52 | 67.5 | 88 | 89 | 90 | 92 | 92 |

Energy Flux in Microvolts/cm²

| | S1 Lamp * | Sunlamp Unit * † | Quartz Hg Arc * § | Sun ‡ |
|--------------------|--------------|---------------------|----------------------|----------|
| Below 2000 Å | 0.6 | 2.6 | 37 | 0.0 |
| 2900-3000 | 2.4 | 12. | 12 | 0.64 |
| 2800-3100 | 7.7 | 41. | 39 | 24. |
| 2900-3200 | 19.3 | 103. | 70 | 140. |

* 1m from center of arc.

† 3.75 amp. 72 v in lamp, no reflector.

§ In center of beam.

‡ Directly overhead.

Per cent Total Energy Flux in various Spectrum Regions

| | <3200Å | 3200-4000Å | 4000-7600Å | 7600-17000Å | >17000Å |
|---------------------------|--------|------------|------------|-------------|---------|
| Continuous spectrum . . . | .03 | .22 | 8.8 | | |
| Line spectrum | .95 | .79 | (1.37)* | | |
| Both | .98 | 1.01 | 10.2 | 45.8 | 42.0 |

* Includes Hg red lines.

TABLE 364.—Characteristics of Photoflash Lamp

(Forsythe, Earley, Journ. Opt. Soc. Amer., 21, 685, 1931.)

G. E. Photoflash lamp burns electrically ignited 65 mg Al foil, .00004 cm thick in closed glass bulb with excess of O₂.

Light output, 47,000 lumens, sec.

Light equals that of 100-watt Mazda for 37 sec. { Max. intensity 4,500,000 lumens

Flashes start in 0.01 sec. with 110 v. Flash lasts 0.066 sec. Time to max. 0.014 sec.

TABLE 365.—Visibility of White Lights

| Range | Candle Power | |
|--------------------------------|--------------|-----|
| | 1 | 2 |
| 1 sea-mile = 1855 meters | .47 | .41 |
| 2 " " | 1.0 | 1.6 |
| 5 " " | 11.8 | 10 |

1 Paterson, Dudding. 2. Deutsche Seewarte.

TABLE 366.—Sensitometric Constants of Type Plates and Films, Definitions

Ordinates are density (D); abscissae, logs of exposure ($\log E$).

Density (D) is the absorbing power of the silver deposit.

If F_0 is the luminous flux incident upon the deposit,

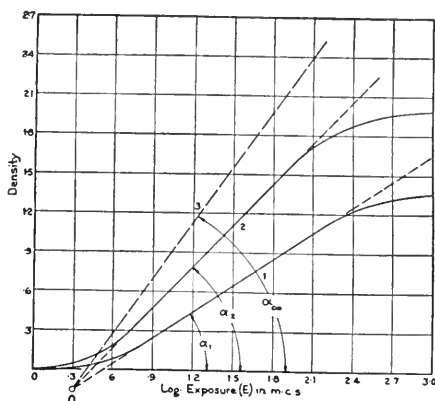
F_1 the luminous flux transmitted,

T , the transmission, O , the opacity,

D , the density, then

$T = F_1/F_0$; $O = 1/T = F_0/F_1$

$D = \log_{10} O = \log_{10} 1/T = \log_{10} F_0/F_1$



Typical Characteristic Curves

Exposure (E): $E = It$ (expressed in meter-candle seconds, mcs), I = illumination (meter-candles, mc) incident on the photographic material during exposure, t = exposure time in seconds.

Speeds given in the following table were obtained with a light approximately equivalent to mean noon sunlight in spectral composition.

Gamma (γ): Gamma is defined as the tangent of angle alpha (α).

Gamma infinity (γ_∞): γ_∞ is defined as a theoretical limiting value to which gamma approaches as the development time is increased.¹

$$\gamma_\infty = \frac{\gamma_1}{1 - e^{-Kt_1}}$$

Velocity Constant of Development (K): $K = \frac{1}{t} \log_e \frac{\gamma_1}{\gamma_2 - \gamma_1}$.

Time of Development for Gamma of Unity ($t_\gamma = 1.0$): A convenient practical specification of development rate.

Fog (F): Fog is the density produced when material is developed without exposure. Values in the table are when development is carried to a gamma of unity.

Latitude (L): L = length of the projection (expressed in exposure units) of the straight line portion on the $\log_{10} E$ axis, assuming development to a gamma of unity.

Inertia (i): i = the value of exposure where the straight line portion of the characteristic curve extended cuts the $\log_{10} E$ axis. The inertia is in general a function of the extent to which development is carried. Values of i given in the table were determined for a gamma of unity.

Speed (S): $S = \frac{1}{i} \times 10$.

In the determination of the values given in Table 368 a developing solution made up according to the following formula was used:

TABLE 367.—Formula for Laboratory Pyrogallol Developer

| Solution A | | Solution B | |
|--------------------------------|------|-----------------------------|------|
| Na_2SO_3 | 70 g | NaCO_3 anhyd. | 75 g |
| NaHSO_3 | 17 | KBr | 1 |
| Pyrogallol | 20 | Water to 1 liter | |
| Water to 1 liter | | | |

Temperature 20° C. For use, mix equal volumes of A and B.

¹ Sheppard and Mees, Investigations on the theory of the photographic process. London, Longmans, 1907.

TABLE 368.—Sensitometric Constants of Type Plates and Films

| Material | F_{02} | K | γ_{∞} | $T_{\gamma} = 1.0$ | Lat. | i | Speed |
|--------------------------------|----------|------|-------------------|--------------------|------|-------|-------|
| Motion picture film: | | | | | | | |
| Extra fast..... | 0.15 | 0.15 | 1.4 | 8.5 | 200 | 0.011 | 900 |
| Normal..... | .10 | .16 | 1.6 | 6.0 | 200 | .020 | 500 |
| Panchromatic..... | .12 | .16 | 1.6 | 6.0 | 300 | .017 | 600 |
| Positive..... | .03 | .30 | 2.7 | 1.5 | 50 | .33 | 30 |
| Portrait extra fast..... | .15 | .14 | 1.4 | 8.5 | 200 | .011 | 900 |
| Portrait normal..... | .10 | .15 | 1.8 | 6.0 | 200 | .020 | 500 |
| Amateur film..... | .10 | .15 | 1.8 | 5.5 | 100 | .025 | 400 |
| "Focal plane" plate..... | .15 | .15 | 1.8 | 5.5 | 100 | .012 | 800 |
| Commercial ordinary..... | .05 | .17 | 2.2 | 3.5 | 75 | .040 | 250 |
| Commercial orthochromatic..... | .10 | .17 | 2.2 | 3.5 | 75 | .033 | 300 |
| Commercial panchromatic..... | .12 | .17 | 2.2 | 3.5 | 75 | .025 | 400 |
| Process ordinary..... | .03 | .30 | 3.0 | 1.5 | 25 | .33 | 30 |
| Process panchromatic..... | .10 | .30 | 3.0 | 1.5 | 25 | .10 | 100 |
| Lantern slide plate..... | .03 | .34 | 3.2 | 1.0 | 25 | .65 | 15 |

TABLE 369.—Resolving Power, Sharpness, and Astro Gamma, Definitions

Resolving Power. (R). The capacity of a photographic plate or film to render fine detail is known as its resolving power. It is usually found by photographing a series of gratings of alternate parallel transparent and opaque lines, each line of a width equal to the space between the lines. The grating constant, (width of line plus width of space), is variable for different line groups over a relatively wide range. Resolving power is specified by stating the number of lines per mm resolvable by the material.^{1,2}

Resolving power depends upon exposure, development time, the developing solution, the spectrum composition of the exposing radiation, and the contrasts in the test object. The values of resolving power given are for the optimal exposure values and optimal time of development in a particular developing solution (laboratory pyrogallol). The exposing radiation used had a spectral composition close to that of average daylight and the contrast between the elements of the test object was very high (greater than 10,000).

Sharpness. The sharpness characteristics of a photographic material is defined as the differential of density (D) with respect to distance (s) in a direction perpendicular to the edge of the image; sharpness (S) = dD/ds , where s is expressed in microns (0.001 mm).

Images used are obtained by making a contact print of a very carefully prepared knife edge. The exposing radiation is carefully collimated and incident normal to the surface.

Sharpness of the developed image depends upon the extent to which development is carried and this is specified by one value of gamma (γ), $dD/d \log E$. It is dependent upon the quality of radiation. The values given in the table were obtained by exposure to light, approximately equivalent to average daylight, and the exposure was so adjusted that development to a gamma of unity in pyrogallol at 20°C gave an image density of unity. These values of sharpness express the diffuse-density gradient (dD/ds) of the straight line portion of the sharpness curve obtained by plotting diffuse density (D) as a function of the distance (s) from the geometrical edge of the image.

Astro gamma. Astro gamma is defined as the coefficient (b) of $\log_{10} E$ in the Scheiner equation, which gives the relation between the diameter (D) of a stellar image and the exposure (E).

$$D = a + b \log_{10} E$$

Since exposure (E) = intensity (I) \times time (t) this equation offers a means of determining the relative brightness of stars by measurement of the diameter of the stellar images obtained under known conditions of exposure and development.

In the table are given values of astro gamma for a group of typical photographic materials. These values were determined by photographing with a highly corrected lens, using a magnification of 0.05, a circular aperture (diameter of 0.56 mm). Exposing radiation was of daylight quality, and intensity was so adjusted that an exposure of 1 second was just above the threshold value. Keeping the intensity factor constant, the exposure time was increased by consecutive powers of 2 from 1 to 512 seconds. The exposed plates were developed to a gamma of unity in standard pyrogallol at 20°C.

¹ Mees, Proc. Roy. Soc. (London), 83, 10, 1909.

² Ross, Physics of the developed photographic image, New York, Van Nostrand, 1924.

TABLE 370.—Resolving Power, Sharpness, and Astro Gamma

| Material | Resolving Power | Sharpness | Astro gamma |
|--|-----------------|-----------|-------------|
| Motion picture film extra fast | 50 | 0.080 | 35 |
| Motion picture film normal | 55 | .085 | 35 |
| Motion picture film panchromatic | 50 | .080 | 35 |
| Motion picture film positive | 80 | .120 | 25 |
| Portrait extra fast | 50 | .065 | 40 |
| Portrait normal | 60 | .070 | 50 |
| Amateur film | 65 | .090 | 40 |
| "Focal plane" plate | 55 | .080 | 45 |
| Commercial ordinary | 65 | .092 | 35 |
| Commercial orthochromatic | 65 | .097 | 40 |
| Commercial panchromatic | 60 | .085 | 37 |
| Process ordinary | 90 | .130 | 25 |
| Process panchromatic | 75 | .110 | 30 |
| Lantern slide plate | 100 | .140 | 20 |

TABLE 371.—Spectrographs Showing Relative Spectrum Sensitivity of Various Plates and Films



Ordinary, blue sensitive.

Orthochromatic, blue
and green sensitive.

Panchromatic.



Dicyanine sensitized.



Kryptocyanine sensitized.



Neocyanine sensitized.

40 50 60 70 80 90

(See following page)

TABLE 372.—Spectrum Sensitivity of Photographic Materials

The spectrum distribution of sensitivity may be shown qualitatively by wedge spectrograms. These (see preceding page) are made with a spectrograph over whose slit is mounted a wedge of neutral gray glass, the transmission of which increases logarithmically from the thin to the thick end. The boundary of the exposed area outlines approximately a curve which is the resultant of the *spectral sensitivity* function of the material and the *spectral distribution of energy* in the radiation emitted by the source illuminating the slit of the instrument. The source used is an acetylene flame operating at a color temperature of 2360°K. All plates had the same exposure. By the application of a correction based on the spectral emission of a black body at 2360°K., an approximation to the actual spectral sensitivity of these materials may be obtained. The neutral glass wedge, while fairly non-selective in absorption for radiation of wave lengths longer than 450 mμ, increases in density for radiation of wave lengths shorter than 450 mμ. The apparent falling off in sensitivity at wave lengths less than 450 mμ is therefore due to excessive absorption of the neutral wedge rather than to a decrease in the spectral sensitivity of the materials. (Mees, Journ. Franklin Inst., 201, 525, 1926. Walters and Davis, Bur. Standards Bull., 17, 353, 1921.)

Note: Photo plates for spectroscopy and astronomy. Mees, Journ. Opt. Soc. Amer., 21, 753, 1931.

TABLE 373.—Relative Photographic Efficiency of Illuminants

C = luminous efficiency of source (lumen/watt). E_r = relative photographic efficiency of source evaluated on basis of equal visual intensities, sunlight = 100%. E_s = relative photographic efficiency of source evaluated on basis of equal energy consumption by the source, sunlight = 100%. (Jones, Hodgson, and Huse. Trans. Illum. Eng. Soc., 10, 963, 1915.)

| Source | C | Photographic material | | | | | |
|----------------------------------|------|-----------------------|-------|----------------|-------|--------------|-------|
| | | Ordinary | | Orthochromatic | | Panchromatic | |
| | | E_r | E_s | E_r | E_s | E_r | E_s |
| Sun..... | 150 | 100 | 100 | 100 | 100 | 100 | 100 |
| Sky..... | | 181 | | 155 | | 130 | |
| Acetylene..... | .7 | 30 | .14 | 44 | .21 | 52 | .24 |
| Acetylene (screened)*..... | .07 | 81 | .037 | 85 | .040 | 89 | .042 |
| Pentane..... | .45 | 18 | .053 | 28 | .086 | 42 | .13 |
| Mercury arc in quartz..... | 40.0 | 600 | 158 | 500 | 132 | 367 | 99 |
| Mercury arc in nultra glass..... | 35.0 | 218 | 50 | 195 | 46 | 165 | 39 |
| Mercury arc in crown glass..... | 37.0 | 324 | 79 | 275 | 68 | 249 | 62 |
| Carbon arc, ordinary..... | 12.0 | 126 | 10 | 112 | 9 | 104 | 8.5 |
| Carbon arc, white flame..... | 29.0 | 257 | 52 | 234 | 45 | 215 | 4.2 |
| Carbon arc, enclosed..... | 9.0 | 175 | 11 | 177 | 11 | 165 | 10 |
| Carbon arc, "Aristo"..... | 12.0 | 796 | 62 | 1070 | 86 | 744 | 60 |
| Magnetite arc..... | 18.0 | 106 | 12 | 115 | 14 | 82 | 10 |
| Carbon glow lamp..... | 2.4 | 23 | .37 | 32 | .52 | 42 | .68 |
| Carbon glow lamp..... | 3.2 | 25 | .51 | 35 | .74 | 45 | .95 |
| Tungsten (vacuum)..... | 8.0 | 33 | 1.7 | 41 | 2.2 | 50 | 2.7 |
| Tungsten (vacuum)..... | 9.9 | 37 | 2.4 | 45 | 3.0 | 53 | 3.5 |
| Tungsten (gas filled)..... | 16.6 | 56 | 6.1 | 62 | 6.8 | 70 | 7.7 |
| Tungsten (gas filled)..... | 21.6 | 64 | 8.9 | 68 | 9.8 | 76 | 11 |
| Tungsten (C ₃)..... | 8.9 | 95 | 5.5 | 87 | 5.2 | 95 | 5.6 |
| Tungsten (C ₃)..... | 11.0 | 108 | 7.8 | 99 | 7.3 | 106 | 7.9 |
| Mercury vapor..... | 23.0 | 316 | 47 | 354 | 54.2 | 273 | 42.0 |

* Screened with Wratten No. 79 filter.

TABLE 374.—Variation of Resolving Power with Plate and Developer

The resolving power is expressed as the number of lines per millimeter which is just resolvable, the lines being opaque and separated by spaces of the same width. The developer used for the comparison of plates was Pyro-soda; the plate for the comparison of developers, Seed Lantern. The numbers are all in the same units. Huse, J. Opt. Soc. America, July, 1917.

| Plate. | Albumen. | Resolution. | Process. | Lantern. | Medium speed. | High speed. |
|----------------------|----------|-------------|----------|----------|---------------|-------------|
| Resolving power..... | 125 | 81 | 67 | 62 | 35 | 27 |

| Developer. | Resolving power. | Developer. | Resolving power. | Developer. | Resolving power. |
|-------------------|------------------|---------------------------|------------------|---------------------------|------------------|
| Pyro-caustic..... | 77 | Pyrocatechin..... | 62 | Amidol..... | 51 |
| Glycin..... | 69 | Pyro-metol..... | 62 | Process hydroquinone..... | 50 |
| Hydroquinone..... | 64 | Eikon-hydroquinone..... | 61 | Ortol..... | 49 |
| Pyro..... | 64 | Ferrous oxalate..... | 61 | Rodinal..... | 49 |
| MQs..... | 64 | Caustic hydroquinone..... | 57 | X-ray powders..... | 49 |
| Metol..... | 63 | Eikonogen..... | 57 | Edinol..... | 47 |
| Nepera..... | 62 | Kachin..... | 54 | | |

TABLE 375.—Relative Intensification of Various Intensifiers

| Bleaching solution. | Blackening solution. | Reference | Intensification. |
|---|--------------------------|--|------------------|
| Mercuric bromide..... | Amidol developer | HgBr ₂ solution (Monckhoven sol. A).* | 1.15 |
| Mercuric chloride..... | Ammonia | Bleach according to Bennett; blackener.* | 1.15 |
| Potassium bichromate + hydrochloric acid..... | Amidol developer | Piper.* | 1.45 |
| Mercuric iodide..... | Schlippe's salt | Debenham, B. J., † p. 186, '17. | 2.50 |
| Lead ferricyanide..... | Sodium sulphide | B. J. Almanac.* | 2.28 |
| Uranium formula..... | — | B. J. Almanac.* | 3.50 |
| Potassium permanganate + hydrochloric acid..... | Sodium stannate | | 2.05 |
| Cupric chloride..... | Sodium stannate | Desalme, B. J., † p. 215, '12. | 1.93 |
| Potassium ferricyanide + potassium bromide..... | Sodium sulphide | Ordinary sepia developer. | 1.33 |
| Mercuric iodide..... | Paraminophenol developer | HgI ₂ according to Bennett. | 1.23 |

See Nietz and Huse, J. Franklin Inst. March 3, 1918.

* B. J. Almanac, see annual Almanac of British Journal of Photography.

† B. J. refers to British Journal of Photography.

TABLE 376.—Reflection and Transmission by Photographic Plates

Plates used, Eastman 40. emulsion, 2637; for red, green, and blue light, Wratten filters customarily used for 3-color work, see Wratten light filters, Eastman Kodak Co.; for "actinic" data, average transmission of plate for a band of wave length corresponding to the sensitivity curve of the plate was obtained by photographing the transmission of light upon a plate of the same type. (McRae, R. C. Tolman, Journ. Opt. Soc. Amer., 20, 565, 1930.)

| | Red | Green | Blue | "Actinic" |
|-------------------------|-----|-------|------|-----------|
| Per cent reflected..... | 58 | 57 | 25 | 28 |
| “ “ transmitted ... | 43 | 34 | 9 | 15 |
| “ “ absorbed | —1 | 9 | 66 | 57 |

For "Instruments and Methods used for Measuring Spectral Light Intensities by Photography," see George R. Harrison, Journ. Opt. Soc. Amer., 19, 267, 1929. This reference contains bibliography of subject matter.

The Eberhard effect is due to the fact that when a heavily exposed area of an emulsion is being developed, a large quantity of soluble bromide is set free which acts as a restrainer and slows the development of surrounding regions.

WAVE LENGTHS OF FRAUNHOFER LINES

For convenience of reference the values of the wave lengths corresponding to the Fraunhofer lines usually designated by the letters in the column headed "index letters," are here tabulated separately. The values are in International Angstrom units. The table is for the most part taken from St. John's revision of Rowland's table of standard wave lengths (1928).

| Index letter | Line due to— | Wave length in centimeters $\times 10^8$ | Index letter | Line due to— | Wave length in centimeters $\times 10^8$ |
|------------------------|--------------|--|-----------------------|--------------|--|
| [A] | { O | 7621 | [G] | { Fe | 4307.914 |
| | { O | 7594 | | { Ca | 4307.749 |
| [a] | | 7164.449 | [g] | Ca | 4226.742 |
| [B] | O | 6869.955 | [h] or H _δ | H | 4101.750 |
| [C] or H _α | H | 6562.816 | [H] | Ca | 3968.494 |
| a | O | 6278.101 | [K] | Ca | 3933.684 |
| [D ₁] | Na | 5895.944 | [L] | Fe | 3820.438 |
| [D ₂] | Na | 5889.977 | [M] | Fe | 3727.636 |
| [D ₃] | He | 5875.618 | [N] | Fe | 3581.210 |
| [E ₁] | { Fe | 5270.390 | [O] | Fe | 3441.020 |
| | { Ca | 5270.270 | [P] | Ti | 3361.194 |
| [E ₂] | Fe | 5269.557 | [Q] | Fe | 3286.773 |
| [b ₁] | Mg | 5183.621 | [R] | { Ca | 3181.277 |
| [b ₂] | Mg | 5172.700 | | { Ca | 3179.343 |
| [b ₃] | { Fe | 5169.052 | [S ₁] | { Fe | 3100.683 |
| | { Fe | 5168.910 | [S ₂] | { Fe | 3100.326 |
| [b ₄] | { Fe | 5167.510 | | { Fe | 3099.943 |
| | { Mg | 5167.330 | [s] | Fe | 3047.623 |
| [F] or H _β | H | 4861.344 | [T] | Fe | 3021.067 |
| [d] | Fe | 4383.559 | [t] | Fe | 2994 |
| [G'] or H _γ | H | 4340.477 | [U] | Fe | 2948 |
| [f] | Fe | 4325.777 | | | |

The solar intensities of the lines of the 4th column are: G, 6, 3; g, 20; h, 40; H, 700; K, 1000; L, 25; M, 4; N, 30; O, 15; P, 3; Q, 7; R, 3, 5; S, 3, 4, 6; s, 20; T, 3.

STANDARD WAVE LENGTHS

TABLE 378.—Primary Wave-Length Standard. Definition of Angstrom

The wave length of the red cadmium line in dry air, 15° C (hydrogen thermometer), 760 mm of Hg pressure, gravity at latitude 45° being 980.67, shall be taken as

6438.4696 Angstroms

The cadmium light shall be produced by a high-voltage, internal electrode vacuum tube, volume greater than 25 cm³, exciting current less than 0.05 amp., temperature not higher than 320° C. When connected to usual high voltage the tube shall be nonluminous at room temperatures. (Trans. Int. Union Solar Res., 2, 20, 1907. Trans. Int. Astron. Union, 2, 40, 1925.)

TABLE 379.—International Secondary Standards. Iron Arc Lines

The wave lengths are observed in air at 15° C, 760 mm pressure. The arc should have its anode below, consisting of a bead of iron oxide supported in the hollowed upper end of a rod of iron or copper at least 10 or 15 mm diameter. The cathode is to be a rod of steel 6 or 7 mm in diameter having a massive cylinder of brass or copper fitted close to the end, so that only 2 or 3 mm of the rod protrude. The arc is to be not less than 12 mm long, preferably 15 to 18 mm. The line voltage may be 110 or more and the current strength 5 amperes or less. A horizontal central cone at right angles to the axis of the arc not exceeding 1.5 mm in vertical dimension is to be used. (See Trans. Int. Astron. Union, 3, 11, 1929, for further details.)

The wave lengths are in International Angstroms. They have been newly referred to the red cadmium line. The results indicate the need of a slight revision of the standards formerly adopted upon which all wave lengths in the International System hitherto made have been based. The corrections to be applied to the previously adopted standards and measures based upon them to reduce them to the new standards are:

| | |
|---------------------------------------|-----------|
| λ 3370. to λ 4000. Å. | —0.001 Å. |
| 4005 to 5506 | —0.002 |
| 6027 to 6085 | —0.005 |
| 6127 to 6260 | —0.006 |
| 6207 to 6430 | —0.007 |
| 6475 to 6609 | —0.008 |
| 6663 to 6750 | —0.009 |

Significance of small letters in following table: (a) Low-temperature lines; always sharp and symmetrical; energy level low; pressure displacement small; limits of upper terms for Fe 19,700 to 32,500 cm⁻¹. (b) Symmetrical under pressure, but showing a slight dissymmetry toward red, or an unsymmetrical reversal under high pressure and in the high-current arc; energy level and pressure displacement medium; limits of upper terms for Fe 32,500 to 41,500 cm⁻¹. (d) High-temperature lines; asymmetrical toward violet; pole-effect large and negative; energy level high; pressure displacement large; limits of upper terms for Fe 53,500 to 55,000 cm⁻¹. (Carnegie Publ. 396, Mt. Wilson Obs.) The letters r and R indicate narrow and wide reversals, respectively, as observed by Burns.

STANDARD WAVE LENGTHS (Continued)

TABLE 379 (continued).—International Secondary Standards. Iron Arc Lines

Measured in air at 15°C, 760 mm

| λ_{Fe} | Int. | Class | λ_{Fe} | Int. | Class | λ_{Fe} | Int. | Class | λ_{Fe} | Int. | Class |
|----------------|------|-------|----------------|------|-------|----------------|------|-------|----------------|------|-------|
| 3370.787 | 6 | | 3797.517 | 5 | b | 4107.492 | 5 | b | 4494.568 | 5 | b |
| 3401.522 | 4 | b | 3798.513 | 6r | b | 4114.449 | 4 | b | 4517.530 | 2 | d? |
| 3465.863 | 6R | a | 3799.549 | 6r | b | 4118.549 | 6 | b | 4528.619 | 7 | b |
| 3476.705 | 5r | a | 3805.345 | 6 | b | 4121.806 | 2 | b | 4531.152 | 5 | b |
| 3497.844 | 5r | a | 3815.842 | 7R | b | 4127.612 | 4 | b | 4547.851 | 3 | b |
| 3513.820 | 5 | b | 3824.444 | 6R | a | 4132.060 | 7 | b | 4592.655 | 4 | b |
| 3521.264 | 5r | b | 3825.884 | 8R | b | 4134.681 | 5 | b | 4602.944 | 4 | b |
| 3558.518 | 5r | b | 3827.825 | 6R | b | 4143.871 | 7 | b | 4647.437 | 4 | b |
| 3565.381 | 6R | b | 3834.225 | 7R | b | 4147.673 | 4 | b | 4667.459 | 4 | b? |
| 3576.760 | 4 | | 3839.259 | 5 | a? | 4156.803 | 4 | b | 4678.852 | 5 | b? |
| 3581.195 | 8R | b | 3840.439 | 6R | b | 4170.906 | 2 | b | 4691.414 | 4 | b? |
| 3584.663 | 5 | | 3841.051 | 6R | b | 4175.640 | 4 | b | 4707.281 | 5 | d |
| 3585.320 | 6r | b | 3843.259 | 5 | b | 4184.895 | 4 | b | 4710.286 | 3 | b |
| 3586.114 | 5 | | 3846.803 | 5 | b? | 4202.031 | 7r | b | 4733.596 | 3 | b |
| 3589.107 | 4 | b | 3849.969 | 5 | b | 4203.987 | 3 | b | 4741.533 | 3 | b |
| 3608.861 | 6R | b | 3850.820 | 5 | b | 4213.650 | 2 | b | 4745.806 | 3 | b |
| 3617.788 | 6 | b | 3856.373 | 6R | a | 4216.186 | 4 | a | 4772.817 | 3 | b |
| 3618.769 | 6R | b | 3859.913 | 7R | a | 4219.364 | 5 | b | 4786.810 | 3 | b |
| 3621.463 | 6 | | 3865.526 | 6R | b | 4250.790 | 8 | b | 4789.654 | 3 | b |
| 3631.464 | 6R | b | 3867.219 | 3 | b | 4267.830 | 2 | b | 4859.748 | 5 | d |
| 3647.844 | 6R | b | 3872.504 | 6r | b | 4271.764 | 8r | b | 4878.218 | 5 | d |
| 3649.508 | 6 | | 3873.763 | 4 | b | 4282.416 | 6 | a | 4903.317 | 5 | d |
| 3651.469 | 6 | b | 3878.021 | 6r | b | 4285.445 | 2 | b | 4918.999 | 8 | d |
| 3669.523 | 6 | b | 3878.575 | 6R | a | 4294.128 | 6 | b | 4924.776 | 3 | b |
| 3676.314 | 6 | b | 3886.284 | 7R | a | 4298.040 | 2 | | 4939.690 | 3 | a |
| 3677.630 | 6 | | 3887.051 | 6r | b | 4305.455 | 2 | b | 4966.096 | 5 | d |
| 3679.915 | 5r | a | 3888.517 | 7 | b | 4307.906 | 8r | b | 4994.133 | 3 | a |
| 3687.458 | 6R | b | 3895.658 | 5r | a | 4315.087 | 5 | a | 5001.871 | 5 | d |
| 3695.054 | 3 | b | 3899.709 | 6r | a | 4325.765 | 9r | b | 5012.071 | 4 | a |
| 3704.463 | 5 | b | 3902.948 | 7r | b | 4337.049 | 5 | b | 5041.759 | 4 | a |
| 3705.567 | 6R | a | 3906.482 | 5r | a | 4352.737 | 4 | a | 5049.825 | 5 | b |
| 3719.935 | 8R | a | 3907.937 | 3 | b | 4358.505 | 2 | b | 5051.636 | 4 | a |
| 3722.564 | 6R | a | 3917.185 | 5 | b | 4369.774 | 3 | b | 5083.342 | 4 | a |
| 3724.380 | 6 | b? | 3920.260 | 6r | a | 4375.932 | 5 | a | 5110.414 | 4 | a |
| 3727.621 | 6R | b | 3922.914 | 6R | a | 4383.547 | 10R | b | 5123.723 | 4 | a |
| 3732.399 | 6 | b | 3927.922 | 6r | a | 4390.954 | 3 | b | 5127.363 | 3 | a |
| 3733.319 | 6R | a | 3930.299 | 7R | a | 4404.752 | 8r | b | 5150.843 | 4 | a |
| 3734.867 | 9R | b | 3935.815 | 4 | b | 4408.419 | 4 | b | 5167.491 | 8 | a |
| 3737.133 | 7R | a | 3940.882 | 4 | b | 4415.125 | 8r | b | 5168.901 | 3 | a |
| 3738.308 | 4 | b | 3942.443 | 3 | b | 4422.570 | 4 | b | 5171.599 | 7 | a |
| 3748.264 | 6R | a | 3948.779 | 4 | b | 4427.312 | 5 | a | 5198.714 | 4 | b |
| 3749.487 | 8R | b | 3956.681 | 4 | b | 4430.618 | 4 | b | 5202.339 | 5 | b |
| 3758.235 | 7R | b | 3966.066 | 7 | b | 4442.343 | 5 | b | 5216.278 | 5 | a |
| 3760.052 | 5 | b | 3967.423 | 4 | b | 4443.197 | 3 | b | 5227.192 | 8 | a |
| 3763.790 | 6R | b | 3969.261 | 7r | b | 4447.722 | 5 | b | 5242.495 | 3 | a? |
| 3765.542 | 6 | b | 4005.246 | 7 | b | 4454.383 | 3 | b | 5250.650 | 3 | b |
| 3767.194 | 6R | b | 4014.534 | 4 | b | 4459.121 | 5 | b | 5270.360 | 8 | a |
| 3787.883 | 6R | b | 4045.815 | 8R | b | 4461.654 | 4 | a | 5307.365 | 4 | a |
| 3790.095 | 4 | b | 4066.979 | 4 | b | 4466.554 | 5 | b | 5328.534 | 4 | a |
| 3795.004 | 6r | b | 4067.275 | 3 | b | 4489.741 | 3 | a | 5341.026 | 5 | a |

STANDARD WAVE LENGTHS (concluded)

TABLE 379 (concluded).—International Secondary Standards. Iron Arc Lines

| λ_{Fe} | Int. | Class | λ_{Fe} | Int. | Class | λ_{Fe} | Int. | Class | λ_{Fe} | Int. | Class |
|----------------|------|-------|----------------|------|-------|----------------|------|-------|----------------|------|-------|
| 5371.493 | 7 | a | 5506.782 | 4 | a | 6065.487 | 4 | b | 6393.605 | 5 | b |
| 5397.131 | 6 | a | 5569.625 | 5 | d | 6136.620 | 4 | b | 6421.355 | 4 | b |
| 5405.778 | 6 | a | 5572.849 | 5 | d | 6137.696 | 4 | b | 6430.851 | 5 | b |
| 5429.699 | 6 | a | 5586.763 | 6 | d | 6191.562 | 5 | b | 6494.985 | 5 | b |
| 5434.527 | 6 | a | 5615.652 | 6 | d | 6230.728 | 5 | b | 6546.245 | 5 | b |
| 5446.920 | 6 | a | 5624.549 | 5 | d | 6252.561 | 4 | b | 6592.919 | 5 | b |
| 5455.613 | 6 | a | 5658.826 | 4 | d | 6265.140 | 3 | b | 6663.446 | 4 | b |
| 5497.519 | 4 | a | 5662.525 | 3 | d | 6318.022 | 4 | b | 6677.993 | 5 | b |
| 5501.469 | 4 | a | 6027.057 | 2 | b | 6335.335 | 4 | b | | | |

(Values taken from Trans. Int. Astron. Union, 3, 86, 1929.)

TABLE 380.—Computed Wave Lengths of Iron Arc Lines

Based on Term Values derived from Table 379. λ s in air, 15°C, 760 mm.

| λ_{Fe} | Int. | Class | λ_{Fe} | Int. | Class | λ_{Fe} | Int. | Class | λ_{Fe} | Int. | Class |
|----------------|------|-------|----------------|------|-------|----------------|------|-------|----------------|------|-------|
| 2858.896 | 4 | b | 2966.898 | 6R | b | 3083.742 | 4r | b | 3161.370 | 2 | d |
| 2874.172 | 7 | b | 2983.571 | 4r | b | 3091.577 | 4r | b | 3171.343 | 4 | d |
| 2912.158 | 8 | b | 3021.073 | 6R | b | 3100.303 | 4r | b | 3180.756 | 4 | a |
| 2929.007 | 7 | b | 3037.389 | 5r | b | 3100.666 | 4r | b | 3184.895 | 4 | a |
| 2936.904 | 7r | b | 3047.605 | 6r | b | 3116.632 | 5 | b | 3199.501 | 6 | a |
| 2941.342 | 8 | b | 3057.448 | 5r | b | 3125.651 | 6 | b | 3226.714 | 1 | a |
| 2947.876 | 5r | b | 3059.086 | 5r | b | 3129.333 | 4 | d | 3229.121 | 4 | a |
| 2953.940 | 5r | b | 3067.245 | 5r | b | 3134.111 | 5 | b | 3236.223 | 5 | a |
| | | | 3075.719 | 5r | b | 3143.243 | 2 | a | | | |

(For significance of designations see preliminary remarks to next preceding table. Values taken from same source, 3, 92, 1929. The following actual measures of the lines of this table may be compared with the above figures: Buisson and Fabry, 1908, 2874.176; 2941.347; 3075.725; 3125.661. Burns, 1915, 2941.348; 3075.726; 3083.747; 3091.582; 3116.638; 3125.665; 3129.340; 3134.115; 3184.900; 3199.527; 3236.227.)

TABLE 381.—Neon Wave Lengths

The lines starred in the following table were adopted in 1922 and 1925 as standards by the International Astronomical Union.

| Inten- sity | Wave length | Inten- sity | Wave length | Inten- sity | Wave length | Inten- sity | Wave length | Inten- sity | Wave length |
|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|
| 5 | 3369.904 | 5 | 3515.192 | 2 | 5820.155 | 4 | 6217.280 | 5 | 6717.043 |
| 6 | 3417.906 | 8 | 3520.474 | 10 | 5852.488 | 7 | 6266.495 | 8 | 6929.468 |
| 6 | 3447.705 | 4 | 3593.526 | 6 | 5881.895 | 4 | 6304.789 | 3 | 7024.049 |
| 6 | 3454.197 | 4 | 3593.634 | 8 | 5944.834 | 8 | 6334.428 | 9 | 7032.413 |
| 5 | 3460.526 | 5 | 3600.170 | 4 | 5975.534 | 8 | 6382.991 | 3 | 7059.111 |
| 4 | 3464.340 | 5 | 3633.664 | 4 | 6029.997 | 10 | 6402.245 | 5 | 7173.939 |
| 5 | 3466.581 | 8 | 5330.779 | 7 | 6074.338 | 9 | 6506.528 | 8 | 7245.167 |
| 6 | 3472.578 | 7 | 5341.096 | 8 | 6096.163 | 4 | 6532.883 | 6 | 7438.902 |
| 4 | 3498.067 | 6 | 5400.562 | 9 | 6143.062 | 5 | 6598.953 | 5 | 7488.885 |
| 4 | 3501.218 | 4 | 5764.419 | 5 | 6163.594 | 8 | 6678.276 | 5 | 7535.784 |

International Units (Angstroms). Burns, Meggers, Merrill, Bull. Bur. Stds. 14, 765, 1918.

STANDARD SOLAR WAVE LENGTHS. INTERNATIONAL ANGSTROMS

Adopted at the Leyden Meeting of the International Astronomical Union.

See Trans. Int. Astron. Union. 3, 93, 1929.

The solar wave lengths in the Rowland Revision by St. John (and others) are based upon the former arc standards and require the following corrections to reduce them to the scale of the following adopted lines:

| λ 3592 to λ 5625 A. | — 0.002 A. | at λ 6350 A. | — 0.007 A. |
|-------------------------------------|------------|----------------------|------------|
| at 2850 | — .003 | 6500 | — .008 |
| 5950 | — .004 | 6700 | — .009 |
| 6050 | — .005 | 6850 | — .011 |
| 6200 | — .006 | 7100 | — .014 |

In the following table the + sign following the designation of an element indicates the state of ionization; an indication like Fe —, solar line too strong to be due to iron alone; Fe, Co, coincidences of like order; Fe Co, coincidence closer for preceding element; Fe-Co, Fe line to the red, Co, to the violet; an italicized element indicates predominance of that element.

| λ_{solar} | Elements | Int. | λ_{solar} | Elements | Int. | λ_{solar} | Elements | Int. |
|--------------------------|----------|------|--------------------------|----------|------|--------------------------|----------|------|
| 3592.027 | V+ | 2 | 4079.843 | Fe | 3 | 4439.888 | Fe | 1 |
| 3635.469 | TiFe | 4 | 4082.943 | MnV | 4 | 4451.588 | Mn | 3 |
| 3650.538 | | 2 | 4091.557 | Fe | 3 | 4454.388 | Fe | 3 |
| 3672.712 | Fe— | 3 | 4094.938 | Ca | 4 | 4459.755 | Cr—V | 1 |
| 3695.056 | Fe | 5 | 4107.492 | Fe | 5 | 4470.485 | Ni | 2 |
| 3710.292 | Y+ | 3 | 4120.212 | Fe | 4 | 4481.616 | Fe | 1 |
| 3725.406 | Fe | 3 | 4136.527 | Fe | 4 | 4502.221 | Mn | 2 |
| 3741.065 | Ti | 4 | 4139.936 | Fe | 6 | 4508.289 | Fe+ | 4 |
| 3752.418 | Fe | 3 | 4154.814 | Fe | 4 | 4512.741 | Ti | 3 |
| 3760.537 | Fe | 4 | 4163.654 | Ti+Cr—Fe | 4 | 4517.534 | Fe | 3 |
| 3769.994 | Fe | 4 | 4168.620 | Fe | 2 | 4525.146 | Fe | 5 |
| 3781.190 | Fe | 3 | 4178.859 | Fe+ | 3 | 4531.631 | Fe | 2 |
| 3793.876 | CrFe | 2 | 4184.900 | Fe, Cr | 4 | 4534.785 | Ti | 4 |
| 3804.015 | Fe | 3 | 4191.683 | Fe | 3 | 4541.523 | CrFe+ | 2 |
| 3821.187 | Fe | 4 | 4198.638 | V—Fe | 3 | 4547.853 | Fe | 3 |
| 3836.090 | Ti+ | 2 | 4208.608 | Fe | 3 | 4548.770 | Ti | 2 |
| 3843.264 | Fe | 4 | 4220.347 | Fe | 3 | 4550.773 | Fe | 2 |
| 3897.458 | Fe | 2 | 4233.612 | Fe | 6 | 4563.766 | Ti+ | 4 |
| 3906.752 | FeV | 4 | 4241.123 | Fe— | 2 | 4571.102 | Mg | 5 |
| 3916.737 | Fe | 5 | 4246.837 | Sc+ | 5 | 4571.982 | Ti+ | 6 |
| 3937.336 | Fe | 3 | 4257.661 | Mn | 2 | 4576.339 | Fe+ | 2 |
| 3949.959 | Fe | 5 | 4266.968 | Fe | 3 | 4578.559 | Ca | 3 |
| 3953.861 | Fe— | 3 | 4267.680 | Fe | 2 | 4587.134 | Fe | 2 |
| 3960.284 | Fe | 4 | 4282.412 | Fe | 5 | 4589.953 | Ti+ | 3 |
| 3963.691 | Cr | 3 | 4291.472 | Fe | 2 | 4598.125 | Fe | 3 |
| 3977.747 | Fe | 6 | 4318.659 | CaTi | 4 | 4602.008 | Fe | 3 |
| 3991.121 | Cr—Zr+ | 3 | 4331.651 | Ni | 2 | 4602.949 | Fe | 6 |
| 4003.769 | FeCe+—Ti | 3 | 4337.925 | Ti+ | 4 | 4607.654 | Fe | 4 |
| 4016.423 | Fe | 2 | 4348.947 | Fe | 2 | 4617.276 | Ti | 3 |
| 4029.642 | Fe—Zr+ | 5 | 4365.904 | Fe | 2 | 4625.052 | Fe | 5 |
| 4030.190 | Fe | 2 | 4389.253 | Fe | 2 | 4630.128 | Fe | 4 |
| 4037.121 | | 2 | 4398.020 | Y+ | 1 | 4635.853 | Fe | 2 |
| 4053.824 | Ti+Fe | 3 | 4416.828 | Fe+ | 2 | 4637.510 | Fe | 5 |
| 4062.447 | Fe | 5 | 4425.444 | Ca | 4 | 4638.017 | Fe | 4 |
| 4073.767 | FeCe+ | 4 | 4430.622 | Fe | 3 | 4643.470 | Fe | 4 |

STANDARD SOLAR WAVE LENGTHS. INTERNATIONAL ANGSTROMS

| λ_{solar} | Elements | Int. | λ_{solar} | Elements | Int. | λ_{solar} | Elements | Int. |
|--------------------------|----------|----------------|--------------------------|----------|------|--------------------------|----------|------|
| 4647.442 | Fe | 4 | 5415.210 | Fe | 5 | 6003.022 | Fe | 6 |
| 4656.474 | Ti | 3 | 5432.955 | Fe | 2 | 6008.566 | Fe | 6 |
| 4664.794 | —CrNa? | 3 | 5445.053 | Fe | 4 | 6013.497 | Mn | 6 |
| 4678.172 | | 3 ^N | 5462.970 | Fe | 3 | 6016.647 | Mn | 6 |
| 4678.854 | Fe | 6 | 5473.910 | Fe | 3 | 6024.068 | Fe | 7 |
| 4683.567 | Fe | 3 | 5487.755 | Fe | 3 | 6027.059 | Fe | 4 |
| 4690.144 | —Fe | 4 | 5501.477 | Fe | 5 | 6042.104 | Fe | 3 |
| 4700.162 | | 4 | 5512.989 | Ca | 4 | 6065.494 | Fe | 7 |
| 4704.954 | Fe | 4 | 5525.552 | Fe | 2 | 6078.499 | Fe | 5 |
| 4720.999 | Fe | 2 | 5534.848 | Fe+ | 2 | 6079.016 | Fe | 2 |
| 4728.552 | Fe | 4 | 5546.514 | Fe | 2 | 6082.718 | Fe | 1 |
| 4733.598 | Fe | 4 | 5590.126 | Ca | 3 | 6085.257 | Ti—Fe | 2 |
| 4735.848 | Fe | 3 | 5601.286 | Ca | 3 | 6086.288 | Ni | 1 |
| 4736.783 | Fe | 6 | 5624.558 | Fe | 4 | 6089.574 | Fe | 1 |
| 4741.535 | Fe | 3 | 5641.448 | Fe | 2 | 6090.216 | V | 2 |
| 4745.807 | Fe | 4 | 5655.500 | Fe | 2 | 6093.649 | Fe | 3 |
| 4772.823 | Fe | 4 | 5667.524 | Fe | 2 | 6096.671 | Fe | 3 |
| 4788.765 | Fe | 3 | 5679.032 | Fe | 3 | 6102.183 | Fe | 6 |
| 4789.658 | Fe | 3 | 5690.433 | Si | 3 | 6102.727 | Ca | 9 |
| 4802.887 | Fe | 2 | 5701.557 | Fe | 4 | 6111.078 | Ni | 2 |
| 4824.143 | Cr+—Fe | 3 | 5731.772 | Fe | 4 | 6116.198 | Ni | 4 |
| 4832.719 | Ni—Fe | 3 | 5741.856 | Fe | 2 | 6122.226 | Ca | 10 |
| 4839.551 | Fe | 3 | 5752.042 | Fe | 4 | 6127.912 | Fe | 3 |
| 4939.694 | Fe | 3 | 5760.841 | Ni | 2 | 6128.984 | Ni | 1 |
| 4983.260 | Fe | 3 | 5805.226 | Ni | 4 | 6136.624 | Fe | 8 |
| 4994.138 | Fe | 3 | 5809.224 | Fe | 4 | 6137.002 | Fe | 3 |
| 5002.798 | Fe | 2 | 5816.380 | Fe | 5 | 6137.702 | Fe | 7 |
| 5014.951 | Fe | 3 | 5853.688 | Ba+ | 5 | 6141.727 | Ba+—Fe | 7 |
| 5028.133 | Fe | 2 | 5857.459 | Ca | 8 | 6145.020 | | 2 |
| 5079.745 | Fe | 4 | 5859.596 | Fe | 5 | 6149.249 | Fe+ | 2 |
| 5090.782 | Fe | 5 | 5862.368 | Fe | 6 | 6151.623 | Fe | 4 |
| 5109.657 | Fe | 2 | 5866.461 | Ti | 3 | 6154.230 | Na | 2 |
| 5150.852 | Fe | 4 | 5867.572 | Ca | 2 | 6157.733 | Fe | 5 |
| 5159.065 | Fe | 2 | 5892.883 | Ni | 4 | 6161.295 | Ca | 4 |
| 5198.718 | Fe | 3 | 5898.166 | Atm.wv | 4 | 6162.180 | Ca | 15 |
| 5225.534 | Fe | 2 | 5905.680 | Fe | 4 | 6165.363 | Fe | 3 |
| 5242.500 | Fe | 2 | 5916.257 | Fe | 3 | 6166.440 | Ca | 5 |
| 5253.468 | Fe | 2 | 5919.054 | Atm.wv | 5 | 6169.564 | Ca | 7 |
| 5273.389 | Fe—Nd+ | 2 | 5919.644 | Atm.wv | 7 | 6170.516 | Fe—Ni | 6 |
| 5288.533 | Fe | 2 | 5927.797 | Fe | 4 | 6173.341 | Fe | 5 |
| 5300.751 | Cr | 2 | 5930.191 | Fe | 6 | 6175.370 | Ni | 3 |
| 5307.369 | Fe | 3 | 5932.092 | Atm.wv | 5 | 6176.816 | Ni | 5 |
| 5322.049 | Fe | 3 | 5934.665 | Fe | 5 | 6180.209 | Fe | 5 |
| 5332.908 | Fe | 4 | 5946.006 | Atm.wv | 3 | 6186.717 | Ni | 2 |
| 5348.326 | Cr | 4 | 5952.726 | Fe | 4 | 6187.995 | Fe | 4 |
| 5365.407 | Fe | 3 | 5956.706 | Fe | 4 | 6191.571 | Fe | 9 |
| 5379.581 | Fe | 3 | 5975.353 | Fe | 3 | 6200.321 | Fe | 6 |
| 5389.486 | Fe | 3 | 5976.787 | Fe | 4 | 6213.437 | Fe | 6 |
| 5398.287 | Fe | 3 | 5983.688 | Fe | 5 | 6215.149 | Fe | 5 |
| 5409.799 | Cr | 4 | 5984.826 | Fe | 6 | 6216.358 | V | 1 |

STANDARD SOLAR WAVE LENGTHS. INTERNATIONAL ANGSTROMS

| λ_{solar} | Elements | Int. | λ_{solar} | Elements | Int. | λ_{solar} | Elements | Int. |
|--------------------------|--------------------|------|--------------------------|--------------------|------|--------------------------|-----------------------|------|
| 6219.287 | Fe | 6 | 6301.508 | Fe | 7 | 6482.809 | Ni | 1 |
| 6226.740 | Fe | 1 | 6302.499 | Fe | 5 | 6493.788 | Ca | 6 |
| 6229.232 | Fe | 1 | 6302.764 | Atm.O ₂ | 2 | 6494.994 | Fe | 8 |
| 6230.736 | Fe-V | 8 | 6305.810 | Atm.O ₂ | 2 | 6498.945 | Fe | 1 |
| 6232.648 | Fe | 3 | 6306.565 | Atm.O ₂ | 2 | 6499.654 | Ca | 4 |
| 6240.653 | Fe | 3 | 6309.886 | Atm.O ₂ | 2 | 6516.083 | Fe+ | 2 |
| 6244.476 | | 2 | 6315.314 | Fe | 2 | 6518.373 | Fe | 2 |
| 6245.620 | Sc+ | 1 | 6315.814 | Fe | 1 | 6569.224 | Fe | 5 |
| 6246.327 | Fe | 8 | 6318.027 | Fe | 6 | 6592.926 | Fe | 6 |
| 6247.562 | Fe+ | 2 | 6322.694 | Fe | 4 | 6609.118 | Fe | 3 |
| 6252.565 | Fe | 7 | 6327.604 | Ni | 2 | 6643.638 | Ni | 5 |
| 6254.253 | Fe | 5 | 6330.852 | Fe | 2 | 6677.997 | Fe | 5 |
| 6256.367 | FeNi | 6 | 6335.337 | Fe | 6 | 6717.687 | Ca | 5 |
| 6258.110 | Ti | 2 | 6336.830 | Fe | 7 | 6810.267 | Fe | 3 |
| 6258.713 | Ti | 3 | 6344.155 | Fe | 4 | 6858.155 | Fe | 2 |
| 6265.141 | Fe | 5 | 6355.035 | Fe | 4 | 6870.946 | Atm.O ₂ | 8 |
| 6270.231 | Fe | 3 | 6358.687 | Fe | 6 | 6879.928 | Atm.O ₂ | 6 |
| 6279.101 | Atm.O ₂ | 3 | 6378.256 | Ni | 2 | 6918.122 | Atm.O ₂ | 9 |
| 6279.896 | Atm.O ₂ | 2 | 6380.750 | Fe | 4 | 6919.002 | Atm.O ₂ | 9 |
| 6280.393 | Atm.O ₂ | 2 | 6393.612 | Fe | 7 | 6923.302 | Atm.O ₂ | 9 |
| 6280.622 | Fe | 3 | 6400.009 | Fe | 8 | 6924.172 | Atm.O ₂ Cr | 9 |
| 6281.178 | Atm.O ₂ | 1 | 6400.323 | Fe | 2 | 6928.728 | Atm.O ₂ | 4 |
| 6281.956 | Atm.O ₂ | 2 | 6408.026 | Fe | 5 | 6934.422 | Atm.O ₂ | 2 |
| 6283.796 | Atm.O ₂ | 1 | 6411.658 | Fe | 7 | 6959.452 | Atm.wv | 3 |
| 6289.398 | Atm.O ₂ | 1 | 6419.956 | Fe | 4 | 6961.260 | Atm.wv | 4 |
| 6290.221 | Atm.O ₂ | 2 | 6421.360 | Fe | 7 | 6978.862 | Fe | 2 |
| 6292.162 | Atm.O ₂ | 2 | 6430.856 | Fe | 5 | 6986.579 | Atm.wv | 3N |
| 6292.958 | Atm.O ₂ | 3 | 6449.820 | Ca | 6 | 6988.986 | Atm.wv | 3 |
| 6295.178 | Atm.O ₂ | 3 | 6455.605 | Ca | 2 | 7022.957 | Fe | 2 |
| 6295.960 | Atm.O ₂ | 3 | 6456.391 | Fe+ | 3 | 7023.504 | Atm.wv | 2 |
| 6297.799 | Fe | 5 | 6471.668 | Ca | 5 | 7027.478 | Atm.wv | 2 |
| 6299.228 | Atm.O ₂ | 3 | 6475.632 | Fe | 2 | 7034.910 | -Fe | 2N |
| | | | | | | 7122.206 | Ni | 4 |

PROVISIONAL ULTRA-VIOLET AND INFRA-RED SOLAR WAVE LENGTHS

Suggested at the 1928 meeting of the International Astronomical Union for further measurements leading to the use of them as standards. Trans. Int. Astron. Union, 3, 101 and 102, 1929. Wave lengths in International Angstroms.

| λ_{solar} | Elements | Int. | λ_{solar} | Elements | Int. | λ_{solar} | Elements | Int. |
|--------------------------|----------|------|--------------------------|----------|------|--------------------------|----------|------|
| 2990.421 | Fe | 1 | 3199.528 | Fe | 4 | 3389.749 | Fe | 2 |
| 2998.815 | Cr— | 2 | 3210.226 | Co—Fe | 3 | 3396.982 | Fe | 3 |
| 3005.061 | Cr | 3 | 3217.393 | Fe | 2 | 3401.531 | Fe | 3 |
| 3021.067 | Fe | 3 | 3225.805 | Fe | 3 | 3412.350 | Co | 5 |
| 3035.745 | | 5 | 3232.291 | Ti+ | 2 | 3419.705 | Fe | 2 |
| 3046.676 | Ti+ | 5 | 3243.415 | Fe | 1 | 3425.584 | | 2 |
| 3061.825 | Co | 3 | 3254.762 | Fe—V, V+ | 5d? | 3431.587 | Co | 4 |
| 3070.266 | Mn | 3 | 3262.289 | Fe | 3 | 3445.126 | —Fe | 5 |
| 3086.788 | Co | 4 | 3273.053 | Zr+ | 2 | 3450.335 | Fe | 5 |
| 3094.898 | Fe?— | 4 | 3278.296 | Ti+ | 5 | 3455.246 | Co— | 5 |
| 3109.334 | OH—Cr | 3 | 3293.150 | Fe | 2 | 3462.359 | Fe | 1 |
| 3121.161 | V+ | 4 | 3295.825 | —Fe+Mn | 6 | 3466.505 | Fe | 3 |
| 3126.208 | Fe—V+ | 5 | 3301.226 | Fe | 1 | 3477.866 | Fe—Ni | 4 |
| 3140.758 | CoOH—Ca | 3 | 3318.032 | Ti+ | 6 | 3485.903 | Ni | 5 |
| 3142.471 | Fe—V+ | 5 | 3323.753 | Fe | 3 | 3509.126 | Fe | 2 |
| 3152.263 | Ti+ | 5 | 3333.396 | Co | 2 | 3517.307 | V+ | 3 |
| 3161.775 | Ti+ | 3 | 3344.524 | Ca—La+ | 2 | 3540.127 | Fe | 5 |
| 3162.571 | Ti+ | 4 | 3355.231 | Fe | 4 | 3549.873 | Fe | 3 |
| 3170.345 | Fe+Mo | 2 | 3365.774 | Ni | 6 | 3564.127 ^w | Fe—Co | 4 |
| 3187.714 | V+ | 2 | 3381.354 | Fe | 2 | 3583.340 ^w | Fe— | 5 |
| 7005.903 | | 1 | 7583.796 | Fe | 1 | 8233.905 | Atm. | 5 |
| 7011.323 | Atm. Fe | 2 | 7676.563 | Atm. | 4 | 8252.727 | Atm. | 2 |
| 7052.776 | Atm. | 1 | 7677.618 | Atm. | 4 | 8272.041 | Atm. | 4 |
| 7068.423 | Fe | 2 | 7682.756 | Atm. | 3 | 8289.533 | Atm. | 4 |
| 7090.390 | Fe | 2 | 7696.868 | Atm. | 0 | 8300.406 | Atm. | 3 |
| 7130.925 | Fe | 3 | 7714.309 | Ni | 3 | 8327.060 | Fe | 2 |
| 7181.509 | Atm. | 2 | 7727.616 | Ni | 3 | 8329.682 | Atm. | 3 |
| 7195.044 | Atm. | 2 | 7742.722 | Fe | 2 | 8342.289 | Atm. | 1 |
| 7204.306 | Atm. | 5 | 7780.567 | Fe | 3 | 8357.041 | Atm. | 1 |
| 7216.527 | Atm. | 2 | 7797.587 | Ni | 2 | 8367.333 | Atm. | 2 |
| 7227.493 | Atm. | 3 | 7807.915 | Fe | 1 | 8387.783 | Fe | 3 |
| 7236.136 | Atm. | 1 | 7832.207 | Fe | 2 | 8426.518 | Ti | 0 |
| 7245.676 | Atm. | 2 | 7849.984 | | 1 | 8439.583 | Fe | 0 |
| 7265.594 | Atm. | 5 | 7887.117 | Atm. | 1 | 8468.420 | Fe, Ti | 2 |
| 7303.197 | Atm. | 2 | 7901.780 | Atm. | 3 | 8514.081 | Fe | 1 |
| 7323.972 | Atm. | 1 | 7918.383 | Si | 1 | 8515.121 | Fe | 0 |
| 7326.164 | Ca | 0 | 7937.149 | Fe | 3 | 8556.795 | Si? | 1 |
| 7335.334 | Atm. | 1 | 7945.857 | Fe | 2 | 8582.271 | Fe | 1 |
| 7355.893 | Cr | 1 | 7984.343 | Atm. | 1 | 8611.813 | Fe | 1 |
| 7369.208 | Atm. | 1 | 8012.940 | Atm. | 1 | 8621.619 | Fe | 1 |
| 7383.722 | Atm. | 1 | 8034.293 | Atm. | 1 | 8648.472 | | 2 |
| 7389.391 | Fe | 2 | 8046.056 | Fe | 2 | 8674.756 | Fe | 1 |
| 7393.610 | Ni | 2 | 8085.175 | Fe | 2 | 8688.642 | Fe | 2 |
| 7405.790 | Si | 1 | 8107.841 | Atm. | 1 | 8699.459 | Fe | 1 |
| 7411.158 | Fe | 1 | 8125.444 | Atm. | 1 | 8717.832 | | 0 |
| 7422.286 | Ni | 1 | 8139.718 | Atm. | 2 | 8736.043 | | 1 |
| 7445.755 | Fe | 2 | 8158.019 | Atm. | 6 | 8752.024 | Si | 1 |
| 7491.652 | Fe | 1 | 8176.976 | Atm. | 10 | 8763.974 | Fe | 1 |
| 7511.030 | Fe | 2 | 8186.371 | Atm. | 5 | 8793.346 | Fe | 1 |
| 7525.115 | Ni | 1 | 8194.835 | Na | 2 | 8806.768 | Mg | 4 |
| 7555.608 | Ni | 2 | 8212.132 | Atm. | 4 | 8824.233 | Fe | 2 |
| 7568.906 | Fe | 1 | 8223.990 | Atm. | 5 | | | |

REDUCTION OF WAVE-LENGTH MEASURES TO STANDARD CONDITIONS

The international wave-length standards are measured in dry air at 15° C, 76 cm pressure. Density variations of the air appreciably affect the absolute wave-lengths when obtained at other temperatures and pressures. The following tables give the corrections for reducing measures to standard conditions, viz.: $\delta = \lambda_0(n_0 - n'_0)(d - d_0)/d_0$ in ten-thousandths of an Angstrom, when the temperature t° C, the pressure B in cm of Hg, and the wave-length λ in Angstroms are given; n and d are the indices of refraction and densities, respectively; the subscript 0 refers to standard conditions: none, to the observed; the prime ' to the standard wave-length, none, to the new wave-length. The tables were constructed for the correction of wave-length measures in terms of the fundamental standard 6438.4696 Å of the cadmium red radiation in dry air, 15° C, 76 cm pressure. The density factor is, therefore, zero for 15° C and 76 cm, and the correction always zero for $\lambda = 6438$ Å. As an example, find the correction required for λ when measured as 3000.0000 Å in air at 25° C and 72 cm. Section (a) of table gives $(d - d_0)/d_0 = -.085$ and for this value of the density factor section (b) gives the correction to λ of $-.0038$ Å. Again, if λ , under the same atmospheric conditions, is measured as 8000.0000 Å in terms of a standard λ' of wave-length 4000.000 Å, say, the measurement will require a correction of $(0.0020 + 0.0008) = +.0028$ Å. Taken from Meggers and Peters, Bulletin Bureau of Standards, 14, p. 728, 1918.

(a). — $1000 \times (d - d_0)/d_0$

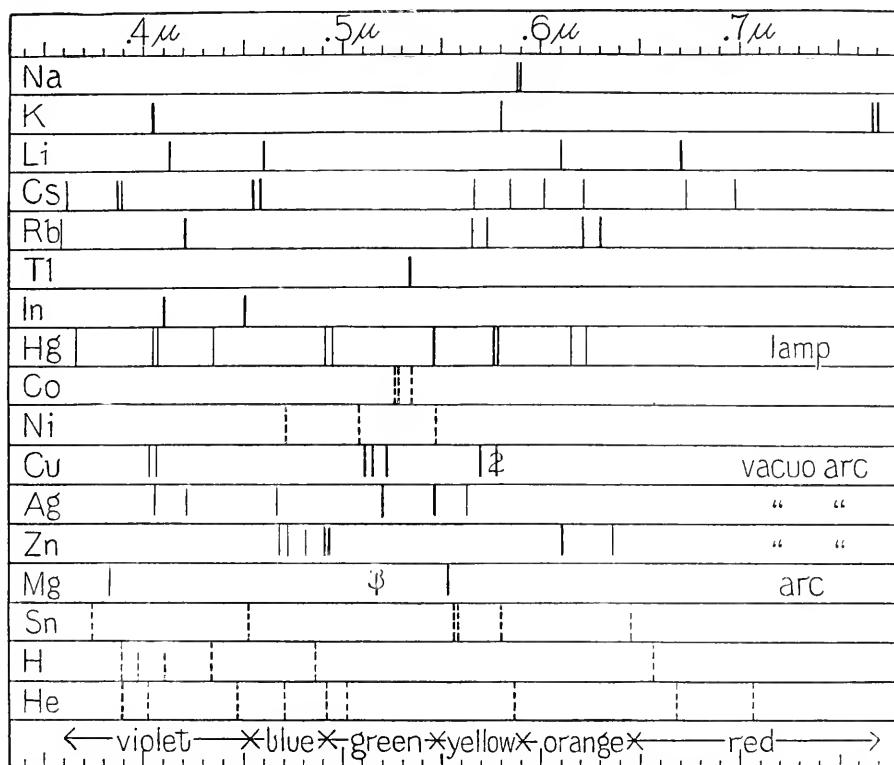
| B cm | 60.0 | 62.5 | 65.0 | 67.5 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 |
|--------|------|------|------|------|------|------|------|------|-----|-----|-----|-----|-----|
| 9° C | -102 | -100 | -126 | -92 | -50 | -46 | -32 | -19 | -5 | +8 | +22 | +35 | +48 |
| 11 | -200 | -107 | -133 | -100 | -67 | -53 | -40 | -27 | -13 | 0 | +13 | +27 | +40 |
| 13 | -206 | -172 | -139 | -106 | -73 | -60 | -46 | -33 | -20 | -7 | +6 | +20 | +33 |
| 15 | -211 | -178 | -145 | -112 | -79 | -66 | -53 | -39 | -26 | -13 | 0 | +13 | +26 |
| 17 | -216 | -184 | -151 | -118 | -86 | -73 | -60 | -47 | -34 | -21 | -8 | +5 | +19 |
| 19 | -222 | -189 | -156 | -124 | -92 | -79 | -66 | -53 | -40 | -27 | -14 | -1 | +12 |
| 21 | -227 | -195 | -163 | -130 | -98 | -85 | -72 | -59 | -46 | -33 | -21 | -8 | +5 |
| 23 | -232 | -200 | -168 | -136 | -104 | -91 | -78 | -65 | -52 | -40 | -27 | -14 | -1 |
| 25 | -238 | -206 | -174 | -143 | -111 | -98 | -85 | -72 | -60 | -47 | -34 | -22 | -9 |
| 27 | -243 | -211 | -179 | -148 | -116 | -104 | -91 | -78 | -66 | -53 | -40 | -28 | -15 |
| 29 | -248 | -216 | -185 | -154 | -122 | -109 | -97 | -84 | -72 | -59 | -46 | -34 | -21 |
| 31 | -253 | -222 | -190 | -159 | -128 | -116 | -103 | -91 | -78 | -66 | -54 | -41 | -20 |
| 33 | -258 | -227 | -196 | -165 | -134 | -121 | -109 | -97 | -84 | -72 | -59 | -47 | -34 |
| 35 | -262 | -231 | -200 | -170 | -139 | -127 | -114 | -102 | -90 | -77 | -65 | -53 | -41 |

(b). — $\delta = \lambda_0(n_0 - n'_0)(d - d_0)/d_0$, in Ten-thousandth Angstroms

| | Wave-lengths in Angstroms. | | | | | | | | | | | | | | |
|-----------------------------------|--|------|------|------|------|------|------|------|------|------|------|------|------|------|-------|
| $1000 \times \frac{d - d_0}{d_0}$ | 2500 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 7500 | 8000 | 9000 | 10000 |
| | Corrections in ten-thousandth Angstroms. | | | | | | | | | | | | | | |
| -260 | -259 | -166 | -116 | -84 | -61 | -44 | -30 | -18 | -8 | +1 | +9 | +17 | +24 | +37 | +50 |
| -245 | -239 | -154 | -107 | -78 | -57 | -41 | -28 | -17 | -7 | +1 | +9 | +16 | +22 | +35 | +46 |
| -220 | -219 | -141 | -98 | -71 | -52 | -37 | -26 | -15 | -7 | +1 | +8 | +14 | +20 | +32 | +42 |
| -200 | -199 | -128 | -89 | -65 | -47 | -34 | -23 | -14 | -6 | +1 | +7 | +13 | +19 | +29 | +38 |
| -180 | -179 | -115 | -80 | -58 | -42 | -30 | -21 | -13 | -6 | +1 | +6 | +12 | +17 | +26 | +34 |
| -165 | -159 | -102 | -71 | -52 | -38 | -27 | -19 | -11 | -5 | +1 | +6 | +10 | +15 | +23 | +31 |
| -140 | -139 | -90 | -62 | -45 | -33 | -24 | -16 | -10 | -4 | +1 | +5 | +9 | +13 | +20 | +27 |
| -120 | -119 | -77 | -54 | -39 | -28 | -20 | -14 | -8 | -4 | +2 | +4 | +8 | +11 | +17 | +23 |
| -100 | -100 | -64 | -45 | -32 | -24 | -17 | -12 | -7 | -3 | +0 | +4 | +7 | +9 | +14 | +19 |
| -80 | -80 | -51 | -36 | -26 | -19 | -14 | -9 | -6 | -2 | +0 | +3 | +5 | +7 | +12 | +15 |
| -60 | -60 | -38 | -27 | -19 | -14 | -10 | -7 | -4 | -2 | +0 | +2 | +4 | +6 | +9 | +11 |
| -40 | -40 | -26 | -18 | -13 | -9 | -7 | -5 | -3 | -1 | +0 | +1 | +3 | +4 | +6 | +8 |
| -20 | -20 | -13 | -9 | -6 | -5 | -3 | -2 | -1 | -1 | 0 | +1 | +1 | +2 | +3 | +4 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| +20 | +20 | +13 | +9 | +6 | +5 | +3 | +2 | +1 | +1 | 0 | -1 | -2 | -2 | -3 | -4 |
| +40 | +40 | +26 | +18 | +13 | +9 | +7 | +5 | +3 | +1 | 0 | -1 | -3 | -4 | -6 | -8 |

SPECTRA OF THE ELEMENTS

The following figure gives graphically the positions of some of the more prominent lines in the spectra of some of the elements. Flame spectra are indicated by lines in the lower parts of the panels, arc spectra in the upper parts, and spark spectra by dotted lines.



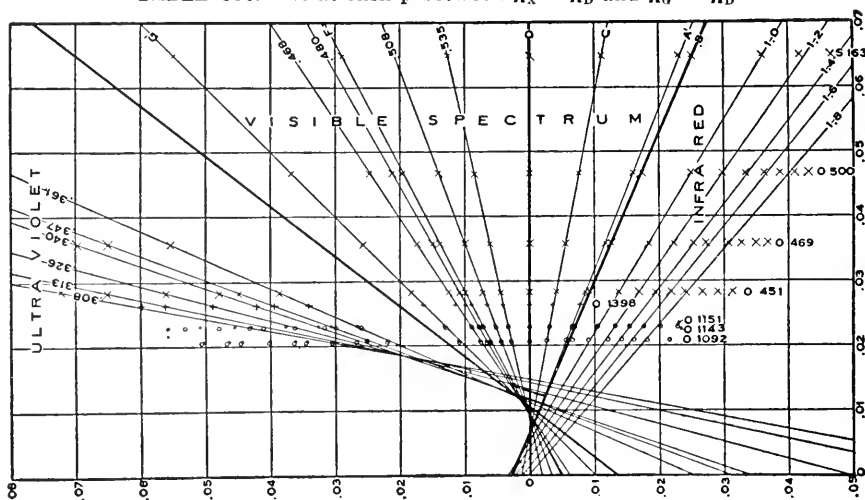
Line spectra of the elements. For bibliography see Gibbs, Rev. Mod. Phys., 4, 205, 1932.

The following wave lengths are in Angstroms

| | | | | | | | |
|----|-----------|----|-----------|----|-----------|----|-----------|
| Na | 5889.965 | Rb | 4202 | Cu | 4023 | Mg | 5168 |
| | 5895.932 | | 4216 | | 4063 | | 5173 |
| K | 4044 | | 5648 | | 5105.543* | | 5184 |
| | 4047 | | 5724 | | 5153.251* | | 5520 |
| | 5802 | | 6207 | | 5218.202* | Sn | 4825 |
| | 7668 | | 6299 | | 5700 | | 5503 |
| Li | 7702 | Tl | 5351 | | 5782.095* | | 5580 |
| | 4132 | In | 4102 | | 5782.150* | | 5799 |
| | 4602 | | 4511 | Ag | 4055 | | 6453 |
| | 6104 | Hg | 4046.8 | | 4212 | II | 3970 |
| | 6707.846* | | 4078.1 | | 4669 | | 4102 |
| Cs | 4555 | | 4358.3 | | 5209.081* | | 4340 |
| | 4593 | | 4916.4 | | 5165.489* | | 4861 |
| | 5664 | | 4959.7 | | 5472 | | 6503 |
| | 5945 | | 5460.742* | | 5623 | | 3187.743† |
| | 6011 | | 5769.508* | Zn | 4680.138* | He | 3888.616† |
| | 6213 | | 5790.659* | | 4722.164* | | 4026.189† |
| | 6724 | | 6152 | | 4810.535* | | 4471.477† |
| | 6974 | | 6232 | | 4912 | | 4713.143† |
| | | | | | 4925 | | 4921.920† |
| | | | | | 6103 | | 5015.675† |
| | | | | | 6362.345* | | 5875.618† |
| | | | | | | | 6678.140† |
| | | | | | | | 7065.188† |

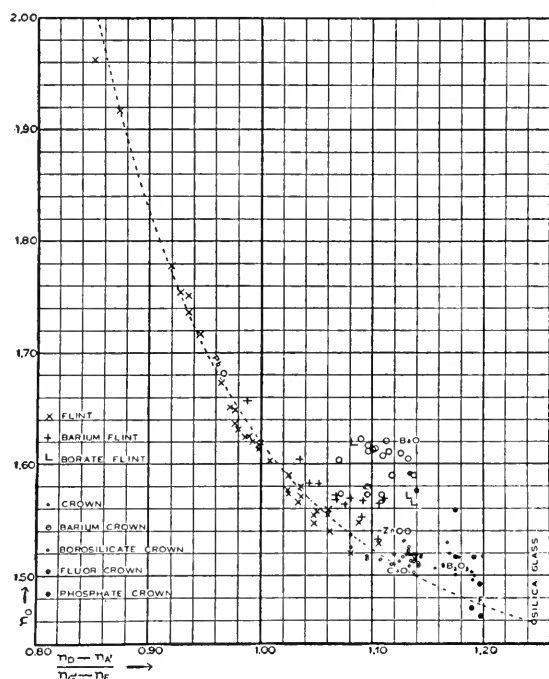
For other elements, see Kayser's Handbuch der Spectroscopie.

* Fabry and Perot. † Merrill.

TABLE 386.—Relationship between $n_x - n_D$ and $n_{D'} - n_D$ 

Abscissae are $n_x - n_D$, $x = 2.4, 2.2, 2.0, 1.8, 1.6, 1.4, 1.2, 1.0, 0.8, .768, .656, .589, .535, .509, .486, .480, .468, .434, .361, .347, .327, .313, .308, .298, .288, .284, 276\mu$. Ordinates $n_{D'} - n_D$ for glasses measured by Rubens and Simons. Various Schott glasses included: O1092, light barium crown, ($n_D = 1.51698$); S204, borate glass, ($n_D = 1.51007$); O1143, dense barium crown, ($n_D = 1.57422$); O1151, high-dispersion crown, ($n_D = 1.52002$); O451, light flint, ($n_D = 1.57524$); O469, dense flint, ($n_D = 1.64985$); O500, dense flint, ($n_D = 1.75130$); S163, extra dense flint ($n_D = 1.88995$).

TABLE 387.—Effect of Composition on Index of Refraction



DERIVATION OF PARTIAL DISPERSIONS OF GLASS FROM $n_F - n_C$

(F. E. Wright, Journ. Amer. Ceramic Soc., 3, 783, 1920; Journ. Opt. Soc. Amer., 4, 148, 195, 1920; 5, 389, 1921.)

The optical constants of a glass are generally stated as the index of refraction n_D , and the partial dispersions between the A ($.768\mu$), C ($.856$), D ($.589$), F ($.486$) and G' ($.434\mu$) lines and its ν value, $(n_0 - 1)/(n_F - n_C)$. The reciprocal of ν is called the average dispersive value. The following table is computed from $n_Y - n_X = a(n_F - n_C) - b$. The mean indices of refraction of two sets of glasses from which a and b were derived are:

| n_A | n_C | n_D | n_F | $n_{G'}$ | $n_C - n_A$ | $n_D - n_C$ | $n_F - n_D$ | $n_{G'} - n_F$ |
|----------|----------|----------|----------|----------|---------------|-------------|-------------|----------------|
| 1.539909 | 1.543168 | 1.545958 | 1.552616 | 1.557994 | $a = .288036$ | .272167 | .727833 | .658443 |
| 1.588807 | 1.593565 | 1.597767 | 1.608201 | 1.616995 | $b = .000529$ | .000219 | -.000219 | -.000843 |

| $n_F - n_C$ | $n_C - n_A$ | $n_D - n_C$ | $n_F - n_D$ | $n_{G'} - n_F$ | $n_F - n_C$ | $n_C - n_A$ | $n_D - n_C$ | $n_F - n_D$ | $n_{G'} - n_F$ |
|-------------|-------------|-------------|-------------|----------------|-------------|-------------|-------------|-------------|----------------|
| .0050 | .00197 | .00158 | .00342 | .00245 | .0150 | .00486 | .00430 | .01070 | .00903 |
| 55 | 212 | 172 | 378 | 278 | 2 | 492 | 436 | 1084 | 917 |
| .0060 | 226 | 185 | 415 | 311 | 4 | 498 | 441 | 1099 | 930 |
| 65 | 241 | 199 | 451 | 344 | 6 | 504 | 446 | 1114 | 943 |
| .0070 | 255 | 212 | 488 | 377 | 8 | 509 | 452 | 1128 | 956 |
| 75 | 270 | 226 | 524 | 410 | .0160 | .00515 | .00457 | .01143 | .00969 |
| .0080 | 284 | 240 | 560 | 442 | 2 | 521 | 463 | 1157 | 982 |
| 85 | 298 | 253 | 597 | 475 | 4 | 527 | 468 | 1172 | 996 |
| .0090 | 313 | 267 | 633 | 508 | 6 | 533 | 474 | 1186 | 1009 |
| .0100 | .00342 | .00294 | .00706 | .00574 | 8 | 538 | 479 | 1201 | 1022 |
| 2 | 348 | 300 | 720 | 587 | .0170 | .00544 | .00485 | .01215 | .01035 |
| 4 | 353 | 305 | 735 | 600 | 2 | 550 | 490 | 1230 | 1048 |
| 6 | 359 | 310 | 750 | 614 | 4 | 556 | 495 | 1245 | 1061 |
| 8 | 365 | 316 | 764 | 627 | 6 | 561 | 501 | 1259 | 1075 |
| .0110 | .00371 | .00321 | .00779 | .00640 | 8 | 567 | 506 | 1274 | 1088 |
| 2 | 377 | 327 | 793 | 653 | .0180 | .00573 | .00512 | .01288 | .01101 |
| 4 | 382 | 332 | 808 | 666 | .0185 | 587 | 525 | 1325 | 1134 |
| 6 | 388 | 338 | 822 | 679 | .0190 | 602 | 539 | 1361 | 1167 |
| 8 | 394 | 343 | 837 | 693 | 5 | 616 | 553 | 1397 | 1200 |
| .0120 | .00400 | .00349 | .00851 | .00706 | .0200 | 631 | 566 | 1434 | 1233 |
| 2 | 405 | 354 | 866 | 719 | 5 | 645 | 580 | 1470 | 1266 |
| 4 | 411 | 359 | 881 | 732 | .0210 | 660 | 593 | 1507 | 1298 |
| 6 | 417 | 365 | 895 | 745 | 5 | 674 | 607 | 1543 | 1331 |
| 8 | 423 | 370 | 910 | 759 | .0220 | 689 | 621 | 1579 | 1364 |
| .0130 | .00429 | .00376 | .00924 | .00772 | 5 | 703 | 634 | 1616 | 1397 |
| 2 | 434 | 381 | 939 | 785 | .0230 | 717 | 648 | 1652 | 1430 |
| 4 | 440 | 387 | 953 | 798 | 5 | 732 | 661 | 1689 | 1463 |
| 6 | 446 | 392 | 968 | 811 | .0240 | 746 | 675 | 1725 | 1496 |
| 8 | 452 | 397 | 983 | 824 | 5 | 761 | 689 | 1761 | 1529 |
| .0140 | .00457 | .00403 | .00997 | .00838 | .0250 | 775 | 702 | 1798 | 1562 |
| 2 | 463 | 408 | 1012 | 851 | 5 | 790 | 716 | 1834 | 1595 |
| 4 | 469 | 414 | 1026 | 864 | .0260 | 804 | 730 | 1870 | 1628 |
| 6 | 475 | 419 | 1041 | 877 | 5 | 819 | 743 | 1907 | 1661 |
| 8 | 481 | 425 | 1055 | 890 | .0270 | .00833 | .00757 | .01943 | .01693 |

TABLE 389.—Index of Refraction of Glasses (American)

Indices of refraction of optical glass made at the Bureau of Standards. Correct probably to 0.00001. The composition given refers to the raw material which went into the melts and does not therefore refer to the composition of the finished glass.

| Melt | 123 | 241 | 135 | 116 | 188 | 151 | 163 | 76 |
|--------------------------------|-----------------|---------------------|---------------|---------------------|--------------|---------------------|---------------|--------------|
| Wave-length | Ordinary crown. | Borosilicate crown. | Barium flint. | Light barium crown. | Light flint. | Dense barium crown. | Medium flint. | Dense flint. |
| Hg 4040.8 | 1.53189 | 1.53817 | 1.58851 | 1.59137 | 1.60507 | 1.63675 | 1.65788 | 1.69005 |
| Hg 4078.1 | 1.53147 | 1.53775 | 1.58791 | 1.59084 | 1.60430 | 1.63619 | 1.65692 | 1.68894 |
| H 4340.7 | 1.52818 | 1.53468 | 1.58327 | 1.58693 | 1.59860 | 1.63189 | 1.64973 | 1.68079 |
| Hg 4358.6 | 1.52798 | 1.53450 | 1.58299 | 1.58674 | 1.59826 | 1.63163 | 1.64931 | 1.68030 |
| H 4861.5 | 1.52326 | 1.53005 | 1.57646 | 1.58121 | 1.59020 | 1.62548 | 1.63941 | 1.66911 |
| Hg 4916.4 | 1.52283 | 1.52967 | 1.57587 | 1.58071 | 1.58958 | 1.62492 | 1.63884 | 1.66814 |
| Hg 5461.0 | 1.51929 | 1.52633 | 1.57105 | 1.57657 | 1.58380 | 1.62033 | 1.63143 | 1.66016 |
| Hg 5769.6 | 1.51771 | 1.52484 | 1.56894 | 1.57473 | 1.58128 | 1.61829 | 1.62834 | 1.65671 |
| Hg 5790.5 | 1.51760 | 1.52475 | 1.56881 | 1.57460 | 1.58112 | 1.61817 | 1.62815 | 1.65650 |
| Na 5893.2 | 1.51714 | 1.52430 | 1.56819 | 1.57406 | 1.58038 | 1.61756 | 1.62725 | 1.65548 |
| Hg 6234.6 | 1.51573 | 1.52297 | 1.56634 | 1.57242 | 1.57818 | 1.61576 | 1.62458 | 1.65250 |
| H 6563.0 | 1.51458 | 1.52188 | 1.56482 | 1.57107 | 1.57638 | 1.61427 | 1.62241 | 1.65007 |
| Li 6708.2 | 1.51412 | 1.52145 | 1.56423 | 1.57054 | 1.57567 | 1.61369 | 1.62157 | 1.64913 |
| K 7682.0 | 1.51160 | 1.51908 | 1.56100 | 1.56762 | 1.57183 | 1.61047 | 1.61701 | 1.64405 |
| (Percentage composition) | | | | | | | | |
| SiO ₂ | 67.0 | 61.2 | 53.7 | 48.0 | 53.9 | 37.0 | 45.6 | 39.0 |
| Na ₂ O | 12.0 | 9.4 | 1.7 | 2.0 | — | — | 3.4 | 3.0 |
| K ₂ O | 5.0 | 8.3 | 8.3 | 6.1 | 7.6 | 2.7 | 4.1 | 4.0 |
| B ₂ O ₃ | 3.5 | 11.0 | 2.7 | 4.0 | — | 5.0 | — | — |
| BaO | 10.0 | 0.1 | 14.3 | 29.5 | — | 47.0 | — | — |
| ZnO | 1.5 | — | 2.5 | 10.0 | — | 7.7 | — | — |
| As ₂ O ₃ | 0.4 | 0.4 | — | 1.4 | 0.3 | — | — | — |
| C ₂ O | — | 1.0 | — | — | 2.0 | — | 3.0 | 4.0 |
| PbO | — | — | 10.7 | — | 35.2 | — | 44.0 | 49.0 |
| SnO ₂ | — | — | — | — | — | — | — | 1.0 |

TABLE 390.—Dispersion of Glasses of Table 389

| Melt. | 123 | 241 | 135 | 116 | 188 | 151 | 163 | 76 |
|----------------|---------|---------|---------|---------|---------|---------|---------|---------|
| n_D | 1.51714 | 1.52430 | 1.56819 | 1.57406 | 1.58038 | 1.61756 | 1.62725 | 1.65548 |
| $n_F - n_C$ | 0.00868 | 0.00820 | 0.01164 | 0.01014 | 0.01391 | 0.01121 | 0.01700 | 0.01904 |
| $n_D - 1 = v$ | 59.6 | 63.9 | 48.8 | 56.6 | 41.7 | 55.1 | 36.9 | 34.4 |
| $n_F - n_C$ | 0.00612 | 0.00578 | 0.00827 | 0.00715 | 0.00901 | 0.00792 | 0.01216 | 0.01363 |
| $n_F - n_{C'}$ | 0.00492 | 0.00460 | 0.00681 | 0.00577 | 0.00831 | 0.00641 | 0.01032 | 0.01168 |
| $n_D - n_{C'}$ | 0.00256 | 0.00242 | 0.00337 | 0.00290 | 0.00400 | 0.00320 | 0.00484 | 0.00541 |

TABLE 391.—Index of Refraction of Glasses Made by Schott and Gen. Jena

The following constants are for glasses made by Schott and Gen. Jena: n_A , n_C , n_D , n_F , n_G are the indices of refraction in air for $A=0.7682\mu$, $C=0.6563\mu$, $D=0.5893$, $F=0.4861$, $G'=0.4341$, $v=(n_D-1)/(n_F-n_C)$. Ultra-violet indices: Simon, Wied. Ann. 53, 1894. Infrared: Rubens, Wied. Ann. 45, 1892. Table is revised from Landolt, Börnstein and Meyerhoffer, Kayser, Handbuch der Spectroscopie, and Schott and Gen's list No. 751, 1909. See also Hovestadt's "Jena Glass."

| Catalogue Type = | O 546 | O 381 | O 184 | O 102 | O 165 | S 57 |
|--------------------------------|----------------|--------------------------|-----------------------|-----------------------|-----------------------|--------------------------|
| Designation = | Zinc-Crown. | Higher Dispersion Crown. | Light Silicate Flint. | Heavy Silicate Flint. | Heavy Silicate Flint. | Heaviest Silicate Flint. |
| Melting Number = | 1092 | 1151 | 451 | 469 | 500 | 163 |
| v = | 60.7 | 51.3 | 41.1 | 33.7 | 27.6 | 22.2 |
| Kind of Light and Wave-length. | Cd 0.2763μ | 1.56759 | — | — | — | — |
| | Cd .2837 | 1.56372 | — | — | — | — |
| | Cd .2950 | 1.55723 | 1.57093 | — | — | — |
| | Cd .3403 | 1.54369 | 1.55262 | 1.71968 | 1.85487 | — |
| | Cd .3610 | 1.53897 | 1.54664 | 1.70536 | 1.83263 | — |
| | H .4340 μ | 1.52788 | 1.53312 | 1.59355 | 1.72800 | 1.94493 |
| | H .4861 | 1.52299 | 1.52715 | 1.58515 | 1.72091 | 1.91890 |
| | Na .5893 | 1.51698 | 1.52022 | 1.57524 | 1.71530 | 1.88995 |
| | H .6563 | 1.51446 | 1.51712 | 1.57119 | 1.71438 | 1.87893 |
| | K .7682 | 1.51143 | 1.51368 | 1.56669 | 1.73530 | 1.86702 |
| | .800 μ | 1.5103 | 1.5131 | 1.5659 | 1.7339 | 1.8650 |
| | 1.200 | 1.5048 | 1.5069 | 1.5627 | 1.7215 | 1.8431 |
| | 1.600 | 1.5008 | 1.5024 | 1.5585 | 1.7151 | 1.8366 |
| | 2.000 | 1.4967 | 1.4973 | 1.5487 | 1.7104 | 1.8316 |
| | 2.400 | — | — | 1.5440 | — | 1.8286 |

Percentage composition of the above glasses:

O 546, SiO_2 , 65.4; K_2O , 15.0; Na_2O , 5.0; BaO , 9.6; ZnO , 2.0; Mn_2O_3 , 0.1; As_2O_3 , 0.4; B_2O_3 , 2.5.

O 381, SiO_2 , 68.7; PbO , 13.3; Na_2O , 15.7; ZnO , 2.0; Mn_2O_3 , 0.1; As_2O_3 , 0.2.

O 184, SiO_2 , 53.7; PbO , 36.0; K_2O , 8.3; Na_2O , 1.0; Mn_2O_3 , 0.06; As_2O_3 , 0.3.

O 102, SiO_2 , 40.0; PbO , 52.6; K_2O , 6.5; Na_2O , 0.5; Mn_2O_3 , 0.09; As_2O_3 , 0.3.

O 165, SiO_2 , 29.26; PbO , 67.5; K_2O , 3.0; Mn_2O_3 , 0.04; As_2O_3 , 0.2.

S 57, SiO_2 , 21.9; PbO , 78.0; As_2O_3 , 0.1.

TABLE 392.— n_D , Dispersion and Density of Jena Glasses

| No. and Type of Jena Glass | n_D for D | $n_F - n_C$ | $v = \frac{n_D - 1}{n_F - n_C}$ | n_D | n_A | $n_F - n_D$ | $n_{H'} - n_F$ | Specific Weight. |
|-----------------------------|-------------|-------------|---------------------------------|--------|--------|-------------|----------------|------------------|
| O 225 Light phosphate crown | 1.5159 | .00737 | 70.0 | .00485 | .00515 | .00407 | 2.58 | |
| O 802 Boro-silicate crown | 1.4997 | .0765 | 64.0 | .0504 | .0534 | .0423 | 2.38 | |
| UV 3199 Ultra-violet crown | 1.5535 | .0781 | 64.4 | .0514 | .0546 | .0432 | 2.41 | |
| O 227 Barium-silicate crown | 1.5339 | .0909 | 59.4 | .0582 | .0630 | .0514 | 2.73 | |
| O 114 Soft-silicate crown | 1.5151 | .0910 | 59.6 | .0577 | .0642 | .0521 | 2.55 | |
| O 608 High-dispersion crown | 1.5149 | .0943 | 54.6 | .0595 | .0666 | .0543 | 2.60 | |
| UV 3248 Ultra-violet flint | 1.5332 | .0904 | 55.4 | .0641 | .0680 | .0553 | 2.75 | |
| O 381 High-dispersion crown | 1.5202 | .1026 | 51.3 | .0644 | .0727 | .0596 | 2.70 | |
| O 602 Baryt light flint | 1.5676 | .1072 | 57.0 | .0675 | .0759 | .0618 | 3.12 | |
| S 389 Borate flint | 1.5686 | .1102 | 51.6 | .0712 | .0775 | .0624 | 2.83 | |
| O 720 Extra light flint | 1.5308 | .1142 | 47.3 | .0711 | .0810 | .0669 | 2.87 | |
| O 154 Ordinary light flint | 1.5710 | .1327 | 43.0 | .0819 | .0943 | .0791 | 3.16 | |
| O 184 " " " " | 1.5900 | .1438 | 41.1 | .0882 | .1022 | .0861 | 3.28 | |
| O 748 Baryt flint | 1.6235 | .1599 | 39.1 | .0965 | .1142 | .0955 | 3.67 | |
| O 102 Heavy flint | 1.6489 | .1919 | 33.8 | .1152 | .1372 | .1180 | 3.87 | |
| O 41 " " " " | 1.7174 | .2434 | 29.5 | .1430 | .1740 | .1521 | 4.49 | |
| O 165 " " " " | 1.7541 | .2743 | 27.5 | .1607 | .1974 | .1730 | 4.78 | |
| S 386 Heavy flint | 1.6170 | .4289 | 21.4 | .2451 | .3109 | .2808 | 6.61 | |
| S 57 Heaviest flint | 1.6626 | .4882 | 14.7 | .2767 | .3547 | .3252 | 6.33 | |

TABLE 393.—Change of Indices of Refraction for 1° C in Units of the Fifth Decimal Place.

| No. and Designation. | Mean Temp. | C | D | F | G' | $-\frac{\Delta n}{n}$ 100 |
|-----------------------------------|------------|--------|--------|--------|--------|---------------------------|
| S 57 Heavy silicate flint . . . | 58.80 | 1.204 | 1.447 | 2.090 | 2.810 | 0.0166 |
| O 154 Light silicate flint . . . | 58.4 | 0.225 | 0.261 | 0.334 | 0.407 | 0.0078 |
| O 327 Baryt flint light . . . | 58.3 | -0.008 | 0.014 | 0.080 | 0.137 | 0.0079 |
| O 225 Light phosphate crown . . . | 58.1 | -0.202 | -0.190 | -0.158 | -0.142 | 0.0049 |

Pulfrich, Wied. Ann. 45, p. 609, 1892.

TABLE 394.—Index of Refraction of Rock Salt in Air

| $\lambda(\mu)$. | n . | Observer. | $\lambda(\mu)$. | n . | Observer. | $\lambda(\mu)$. | n . | Observer. |
|------------------|----------|-----------|------------------|----------|-----------|------------------|----------|-----------|
| 0.185409 | 1.89348 | M | 0.88396 | 1.534011 | L | 5.8932 | 1.516014 | P |
| .204470 | 1.70964 | " | .972298 | 1.532532 | " | " | 1.515553 | L |
| .291368 | 1.61325 | " | .98220 | 1.532435 | P | 6.4825 | 1.513628 | P |
| .358702 | 1.57932 | " | 1.036758 | 1.531762 | L | " | 1.513467 | L |
| .441587 | 1.55962 | " | 1.1786 | 1.530372 | P | 7.0718 | 1.511062 | P |
| .486149 | 1.55338 | " | " | 1.530374 | L | 7.6611 | 1.508318 | " |
| " | 1.553406 | L | 1.555137 | 1.528211 | " | 7.9558 | 1.506804 | " |
| " | 1.553399 | P | 1.7680 | 1.527440 | P | 8.8398 | 1.502035 | " |
| .58902 | 1.544340 | L | " | 1.527441 | L | 10.0184 | 1.494722 | " |
| .58932 | 1.544313 | P | 2.073516 | 1.520554 | " | 11.7864 | 1.481816 | " |
| 650304 | 1.540672 | P | 2.35728 | 1.525863 | P | 12.9650 | 1.471720 | " |
| " | 1.540702 | L | " | 1.525849 | L | 14.1436 | 1.460547 | " |
| .706548 | 1.538633 | P | 2.9466 | 1.524534 | P | 14.7330 | 1.454494 | " |
| .706529 | 1.536712 | P | 3.5359 | 1.523173 | " | 15.3223 | 1.447494 | " |
| .76821 | 1.53666 | M | 4.1252 | 1.521648 | P | 15.9116 | 1.441032 | " |
| .78576 | 1.536138 | P | " | 1.521625 | L | 20.57 | 1.3735 | RN |
| .88396 | 1.534011 | P | 5.0092 | 1.518978 | P | 22.3 | 1.340 | " |

$$n^2 = a^2 + \frac{M_1}{\lambda^2 - \lambda_1^2} + \frac{M_2}{\lambda^2 - \lambda_2^2} - k\lambda^2 - h\lambda^4 \text{ or } b^2 + \frac{M_1}{\lambda^2 - \lambda_1^2} + \frac{M_2}{\lambda^2 - \lambda_2^2} - \frac{M_3}{\lambda_3^2 - \lambda^2}$$

where $a^2 = 2.330165$ $\lambda_2^2 = 0.02547414$ $b^2 = 3.680137$
 $M_1 = 0.01278685$ $k = 0.0009285837$ $M_3 = 12059.95$
 $\lambda_1^2 = 0.0148500$ $h = 0.000000286086$ $\lambda_3^2 = 3600.$ (P)
 $M_2 = 0.005343924$

TABLE 395.—Change of Index of Refraction for 1° C in Units of the 5th Decimal Place

| | | | | | | | | | | | |
|-------------|--------|----|-------------|--------|----|--------|--------|----|------------|-------|---|
| 0.202 μ | +3.134 | Mi | 0.441 μ | —3.425 | Mi | C line | —3.749 | Pl | 0.76 μ | —3.73 | L |
| .210 | +1.570 | " | .508 | —3.517 | " | D " | —3.739 | " | 1.368 | —3.88 | L |
| .224 | —0.187 | " | .643 | —3.636 | " | F " | —3.648 | " | 1.88 | —3.85 | L |
| .298 | —2.727 | " | | | | G' " | —3.585 | " | 4.3 | —3.82 | L |

L. Annals of the Astrophysical Observatory of the Smithsonian Institution, Vol. 1, 1900.

M. Martens, Ann. d. Phys. 6, 1901, 8, 1902.

Mi Micheli, Ann. d. Phys. 7, 1902.

P. Paschen, Wied. Ann. 26, 1908.

Pl. Pulfrich, Wied. Ann. 45, 1892.

RN Rubens and Nichols, Wied. Ann. 60, 1897.

TABLE 396.—Index of Refraction of Swilite (Potassium Chloride) in Air

| $\lambda(\mu)$. | n . | Observer. | $\lambda(\mu)$. | n . | Observer. | $\lambda(\mu)$. | n . | Observer. |
|------------------|----------|-----------|------------------|----------|-----------|------------------|----------|-----------|
| 0.185409 | 1.82710 | M | 1.1786 | 1.478311 | P | 8.2505 | 1.462726 | P |
| .200090 | 1.71870 | " | " | 1.47824 | W | " | 1.46276 | P |
| .21946 | 1.64745 | " | 1.7680 | 1.475800 | P | 8.8398 | 1.460858 | P |
| .257317 | 1.58125 | " | " | 1.47580 | W | " | 1.46092 | W |
| .281640 | 1.55836 | " | 2.35728 | 1.474751 | P | 10.0184 | 1.45672 | P |
| .308227 | 1.54136 | " | 2.9466 | 1.473834 | " | " | 1.45673 | W |
| .358702 | 1.52115 | " | " | 1.47394 | W | 11.786 | 1.44919 | P |
| .394415 | 1.51219 | " | 3.5359 | 1.473049 | P | " | 1.44941 | W |
| .407832 | 1.50044 | " | " | 1.47304 | W | 12.965 | 1.44346 | P |
| .508606 | 1.49620 | " | 4.7146 | 1.471122 | P | " | 1.44385 | W |
| .58933 | 1.49044 | P | " | 1.47129 | W | 14.144 | 1.43722 | P |
| .67082 | 1.48660 | M | 5.3939 | 1.470013 | P | 15.912 | 1.42617 | " |
| .78576 | 1.483282 | P | " | 1.47001 | W | 17.680 | 1.41403 | " |
| .88398 | 1.481422 | P | 5.8932 | 1.468804 | P | 20.60 | 1.3882 | RN |
| .98220 | 1.480084 | " | " | 1.46880 | W | 22.5 | 1.369 | " |

$$n^2 = a^2 + \frac{M_1}{\lambda^2 - \lambda_1^2} + \frac{M_2}{\lambda^2 - \lambda_2^2} - k\lambda^2 - h\lambda^4 \text{ or } b^2 + \frac{M_1}{\lambda^2 - \lambda_1^2} + \frac{M_2}{\lambda^2 - \lambda_2^2} + \frac{M_3}{\lambda_3^2 - \lambda^2}$$

$a^2 = 2.174967$ $\lambda_2^2 = 0.0255550$ $b^2 = 3.866619$
 $M_1 = 0.008344206$ $k = 0.000513495$ $M_3 = 5569.715$
 $\lambda_1^2 = 0.0119082$ $h = 0.000000167587$ $\lambda_3^2 = 3292.47$ (P)
 $M_2 = 0.00698382$

W. Weller, see Paschen's article. Other references as under Table 395, above.

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TABLE 397.—Index of Refraction of Fluorite in Air

| λ (μ) | n | Observer | λ (μ) | n | Observer | λ (μ) | n | Observer |
|---------------------|---------|----------|---------------------|---------|----------|---------------------|---------|----------|
| 0.1856 | 1.50040 | S | 1.4733 | 1.42641 | P | 4.1252 | 1.40855 | P |
| .19881 | 1.49029 | " | 1.5715 | 1.42596 | " | 4.4199 | 1.40559 | " |
| .21441 | 1.48162 | " | 1.6206 | 1.42582 | " | 4.7146 | 1.40238 | " |
| .22645 | 1.47762 | " | 1.7680 | 1.42507 | " | 5.0002 | 1.39890 | " |
| .25713 | 1.46476 | " | 1.9153 | 1.42437 | " | 5.3030 | 1.39529 | " |
| .32525 | 1.44987 | " | 1.9944 | 1.42413 | " | 5.5935 | 1.39142 | " |
| .34555 | 1.44097 | " | 2.0626 | 1.42359 | " | 5.8932 | 1.38719 | " |
| .39681 | 1.44214 | " | 2.1608 | 1.42308 | " | 6.1825 | 1.3819 | " |
| .48007 | 1.43713 | P | 2.2100 | 1.42288 | " | 7.0718 | 1.36805 | " |
| .58930 | 1.43393 | P | 2.3573 | 1.42199 | " | 7.6612 | 1.35680 | " |
| .65618 | 1.43257 | S | 2.5537 | 1.42088 | " | 8.2505 | 1.34444 | " |
| .68671 | 1.43200 | " | 2.6519 | 1.42016 | " | 8.8308 | 1.33079 | " |
| .71836 | 1.43157 | " | 2.7502 | 1.41971 | " | 9.4291 | 1.31612 | " |
| .76040 | 1.43101 | " | 2.9466 | 1.41826 | " | 51.2 | 3.47 | RA |
| .8840 | 1.42982 | P | 3.1430 | 1.41707 | " | 61.1 | 2.66 | " |
| 1.1786 | 1.42787 | " | 3.2413 | 1.41612 | " | ∞ | 2.63 | S |
| 1.3756 | 1.42690 | " | 3.5359 | 1.41379 | " | | | |
| 1.4733 | 1.42641 | " | 3.8306 | 1.41120 | " | | | |

References under Table 331.

$$n^2 = a^2 + \frac{M_1}{\lambda^2 - \lambda_1^2} - c\lambda^2 - f\lambda^4 \text{ or } = b^2 + \frac{M_2}{\lambda^2 - \lambda_2^2} + \frac{M_3}{\lambda^2 - \lambda_3^2}$$

where $a^2 = 2.03882$ $f = 0.000002916$ $M_3 = 511.465$
 $M_1 = 0.0062183$ $b^2 = 6.09651$ $\lambda_2^2 = 1260.56$
 $\lambda_1^2 = 0.007706$ $M_2 = 0.0061386$ $\lambda_3 = 0.0940\mu$
 $c = 0.0031999$ $\lambda_2^2 = 0.00884$ $\lambda_3 = 35.5\mu$ (P)

TABLE 398.—Change of Index of Refraction for 1° C in Units of the 5th Decimal Place
C line, —1.220; D, —1.206; F, —1.170; G, —1.142. (P)TABLE 399.—Index of Refraction of Iceland Spar (CaCO_3) in Air

| λ (μ) | n_o | n_e | Observer | λ (μ) | n_o | n_e | Observer | λ (μ) | n_o | n_e | Observer |
|---------------------|--------|--------|----------|---------------------|--------|--------|----------|---------------------|--------|--------|----------|
| 0.198 | — | 1.5780 | M | 0.508 | 1.6653 | 1.4896 | M | 0.991 | 1.6438 | 1.4802 | C |
| .200 | 1.9028 | 1.5765 | " | .533 | 1.6628 | 1.4884 | " | 1.229 | 1.6393 | 1.4787 | " |
| .208 | 1.8673 | 1.5654 | " | .589 | 1.6584 | 1.4864 | " | 1.307 | 1.6379 | 1.4783 | " |
| .226 | 1.8130 | 1.5492 | " | .643 | 1.6550 | 1.4849 | " | 1.497 | 1.6346 | 1.4774 | " |
| .298 | 1.7230 | 1.5151 | C | .656 | 1.6544 | 1.4846 | " | 1.682 | 1.6313 | — | " |
| .340 | 1.7008 | 1.5056 | M | .670 | 1.6537 | 1.4843 | " | 1.749 | — | 1.4764 | " |
| .361 | 1.6932 | 1.5022 | C | .760 | 1.6500 | 1.4826 | " | 1.849 | 1.6280 | — | " |
| .410 | 1.6802 | 1.4964 | — | .768 | 1.6497 | 1.4826 | M | 1.908 | — | 1.4757 | " |
| .431 | 1.6755 | 1.4943 | M | .801 | 1.6487 | 1.4822 | C | 2.172 | 1.6210 | — | " |
| .486 | 1.6678 | 1.4907 | " | .905 | 1.6458 | 1.4810 | " | 2.324 | — | 1.4739 | " |

C. Carvalho, J. de Phys. (3), 9, 1900.

M. Martens, Ann. der Phys. (4) 6, 1901, 8, 1902.

P. Paschen, Wied. Ann. 56, 1895.

Pl. Pulfrich, Wied. Ann. 45, 1892.

RA. Rubens-Ashkinass, Wied. Ann. 67, 1899.

S. Starke, Wied. Ann. 60, 1897.

TABLE 400.—Index of Refraction of Nitroso-dimethyl-aniline (Wood)

| λ | n | λ | n | λ | n | λ | n | λ | n |
|-----------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|
| 0.497 | 2.140 | 0.525 | 1.945 | 0.584 | 1.815 | 0.636 | 1.647 | 0.713 | 1.718 |
| .500 | 2.114 | .536 | 1.909 | .602 | 1.796 | .647 | 1.758 | .730 | 1.713 |
| .506 | 2.074 | .546 | 1.879 | .611 | 1.783 | .659 | 1.750 | .749 | 1.709 |
| .508 | 2.025 | .557 | 1.857 | .620 | 1.778 | .669 | 1.743 | .763 | 1.697 |
| .516 | 1.985 | .569 | 1.834 | .627 | 1.769 | .696 | 1.723 | | |

Nitroso-dimethyl-aniline has enormous dispersion in yellow and green, metallic absorption in violet. See Wood. Phil. Mag 1903.

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TABLE 401.—Index of Refraction of Quartz (SiO_2), 18°C

| Wave length | Index Ordinary Ray | Index Extraordinary Ray | Fused | Wave length | Index Ordinary Ray | Index Extraordinary Ray | Fused |
|-------------|--------------------|-------------------------|---------|-------------|--------------------|-------------------------|---------|
| μ | | | | μ | | | |
| 0.185 | 1.67582 | 1.68999 | 1.5745 | 0.656 | 1.54189 | 1.55091 | 1.45640 |
| .193 | .65997 | .67343 | 1.5603 | .686 | .54099 | .54998 | |
| .198 | .65090 | .66397 | 1.55202 | .760 | .53917 | .54811 | |
| .206 | .64038 | .65300 | | 1.160 | .5329 | | |
| .214 | .63041 | .64264 | 1.53388 | .969 | .5216 | | |
| .219 | .62494 | .63698 | 1.52911 | 2.327 | .5156 | | |
| .231 | .61399 | .62560 | 1.5194 | .84 | .5039 | | |
| .257 | .59622 | .60712 | 1.5037 | 3.18 | .4944 | | |
| .274 | .58752 | .59811 | 1.49623 | .63 | .4799 | Rubens | |
| .340 | .56748 | .57738 | 1.4788 | .96 | .4679 | | |
| .396 | .55815 | .56771 | | 4.20 | .4569 | | |
| .410 | .55650 | .56600 | | 5.0 | .417 | | |
| .486 | .54968 | .55896 | | 6.45 | .274 | | |
| 0.589 | 1.54424 | 1.55334 | 1.45845 | 7.0 | 1.167 | | |

Except Rubens' values,—means from various authorities

TABLE 402.—Index of Refraction for Various Alums*

| R | Density. | Temp. C.° | Index of refraction for the Fraunhofer lines. | | | | | | | |
|---|----------|-----------|---|---------|---------|---------|---------|---------|---------|---------|
| | | | a | B | c | D | E | b | F | G |
| Aluminium Alums. $\text{RAl}(\text{SO}_4)_2 + 12\text{H}_2\text{O}.\dagger$ | | | | | | | | | | |
| Na | 1.667 | 17-28 | 1.43492 | 1.43563 | 1.43653 | 1.43884 | 1.44185 | 1.44231 | 1.44412 | 1.44804 |
| $\text{NH}_3(\text{CH}_3)$ | 1.568 | 7-17 | .45013 | .45062 | .45177 | .45410 | .45691 | .45749 | .45941 | .46363 |
| K | 1.735 | 14-15 | .45220 | .45303 | .45398 | .45645 | .45934 | .45996 | .46181 | .46609 |
| Rb | 1.852 | 7-21 | .45232 | .45328 | .45417 | .45660 | .45955 | .45999 | .46192 | .46618 |
| Cs | 1.961 | 15-25 | .45437 | .45517 | .45618 | .45856 | .46141 | .46203 | .46386 | .46821 |
| NH_4 | 1.631 | 15-20 | .45500 | .45599 | .45693 | .45939 | .46234 | .46288 | .46481 | .46923 |
| Tl | 2.329 | 10-23 | .49226 | .49317 | .49443 | .49748 | .50128 | .50209 | .50463 | .51076 |
| Chrome Alums. $\text{RCr}(\text{SO}_4)_2 + 12\text{H}_2\text{O}.\dagger$ | | | | | | | | | | |
| Cs | 2.043 | 6-12 | 1.47627 | 1.47732 | 1.47836 | 1.48100 | 1.48434 | 1.48491 | 1.48723 | 1.49280 |
| K | 1.817 | 6-17 | .47642 | .47738 | .47865 | .48137 | .48459 | .48513 | .48753 | .49309 |
| Rb | 1.946 | 12-17 | .47660 | .47756 | .47868 | .48151 | .48486 | .48522 | .48775 | .49323 |
| NH_4 | 1.719 | 7-18 | .47911 | .48014 | .48125 | .48418 | .48744 | .48794 | .49040 | .49594 |
| Tl | 2.386 | 9-25 | .51692 | .51798 | .51923 | .52280 | .52704 | .52787 | .53082 | .53808 |
| Iron Alums. $\text{RFe}(\text{SO}_4)_2 + 12\text{H}_2\text{O}.\dagger$ | | | | | | | | | | |
| K | 1.806 | 7-11 | 1.47630 | 1.47706 | 1.47837 | 1.48169 | 1.48580 | 1.48670 | 1.48939 | 1.49605 |
| Rb | 1.916 | 7-20 | .47700 | .47770 | .47894 | .48234 | .48654 | .48712 | .49003 | .49700 |
| Cs | 2.061 | 20-24 | .47825 | .47921 | .48042 | .48378 | .48797 | .48867 | .49136 | .49838 |
| NH_4 | 1.713 | 7-20 | .47927 | .48029 | .48150 | .48482 | .48921 | .48993 | .49286 | .49980 |
| Tl | 2.385 | 15-17 | .51674 | .51790 | .51943 | .52365 | .52859 | .52946 | .53284 | .54112 |

* According to the experiments of Soret (Arch. d. Sc. Phys. Nat. Genève, 1884, 1888, and Comptes Rendus, 1885).
† R stands for the different bases given in the first column.

For other alums see reference on Landolt-Börnstein-Roth Tabellen.

INDEX OF REFRACTION

Selected Monorefringent or Isotropic Minerals

The values are for the sodium D line unless otherwise stated and are arranged in the order of increasing indices. Selected by Dr. Edgar T. Wherry from a private compilation of Dr. E. S. Larsen of the U. S. Geological Survey.

| Mineral. | Formula. | Index of refraction, $\lambda = 0.589\mu$. |
|-----------------------|---|---|
| Villiaumite..... | NaF | 1.328 |
| Cryolithionite..... | $3\text{NaF} \cdot 3\text{LiF} \cdot 2\text{AlF}_3$ | 1.339 |
| Opal..... | $\text{SiO}_2 \cdot n\text{H}_2\text{O}$ | 1.406-1.440 |
| Fluorite..... | CaF_2 | 1.434 |
| Alum..... | $\text{K}_2\text{O} \cdot \text{Al}_2\text{O}_3 \cdot 4\text{SO}_3 \cdot 24\text{H}_2\text{O}$ | 1.450 |
| Sodalite..... | $3\text{Na}_2\text{O} \cdot 3\text{Al}_2\text{O}_3 \cdot 6\text{SiO}_2 \cdot 2\text{NaCl}$ | 1.483 |
| Cristobalite..... | SiO_2 | 1.486 |
| Analcite..... | $\text{Na}_2\text{O} \cdot \text{Al}_2\text{O}_3 \cdot 4\text{SiO}_2 \cdot 2\text{H}_2\text{O}$ | 1.487 |
| Sylvite..... | KCl | 1.490 |
| Noselite..... | $5\text{Na}_2\text{O} \cdot 3\text{Al}_2\text{O}_3 \cdot 6\text{SiO}_2 \cdot 2\text{SO}_3$ | 1.495 |
| Hauynite..... | Like preceding + CaO | 1.460 |
| Lazurite..... | $4\text{Na}_2\text{O} \cdot 3\text{Al}_2\text{O}_3 \cdot 6\text{SiO}_2 \cdot \text{Na}_2\text{S}_6$ | 1.500 ± |
| Leucite..... | $\text{K}_2\text{O} \cdot \text{Al}_2\text{O}_3 \cdot 4\text{SiO}_2$ | 1.500 |
| Pollucite..... | $2\text{Cs}_2\text{O} \cdot 2\text{Al}_2\text{O}_3 \cdot 9\text{SiO}_2 \cdot \text{H}_2\text{O}$ | 1.525 |
| Halite..... | NaCl | 1.544 |
| Bauxite..... | $\text{Al}_2\text{O}_3 \cdot n\text{H}_2\text{O}$ | 1.570 ± |
| Pharmacosiderite..... | $3\text{Fe}_2\text{O}_3 \cdot 2\text{As}_2\text{O}_5 \cdot 3\text{K}_2\text{O} \cdot 5\text{H}_2\text{O}$ | 1.676 |
| Spinel..... | $\text{MgO} \cdot \text{Al}_2\text{O}_3$ | 1.723 ± |
| Berzelite..... | $3(\text{Ca}, \text{Mg}, \text{Mn})\text{O} \cdot \text{As}_2\text{O}_5$ | 1.727 |
| Periclase..... | MgO | 1.736 |
| Grossularite..... | $3\text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot 3\text{SiO}_2$ | 1.736 |
| Helvite..... | $3(\text{Mn}, \text{Fe})\text{O} \cdot 3\text{BeO} \cdot 3\text{SiO}_2 \cdot \text{MnS}$ | 1.739 |
| Pyrope..... | $3\text{MgO} \cdot \text{Al}_2\text{O}_3 \cdot 3\text{SiO}_2$ | 1.745 |
| Arsenolite..... | As_2O_3 | 1.755 |
| Hessonite..... | $3\text{CaO} \cdot (\text{Al}, \text{Fe})_2\text{O}_3 \cdot 3\text{SiO}_2$ | 1.763 |
| Pleonaste..... | $(\text{Mg}, \text{Fe})\text{O} \cdot \text{Al}_2\text{O}_3$ | 1.770 ± |
| Almandine..... | $3\text{FeO} \cdot \text{Al}_2\text{O}_3 \cdot 3\text{SiO}_2$ | 1.778 |
| Hercynite..... | $\text{FeO} \cdot \text{Al}_2\text{O}_3$ | 1.800 ± |
| Gahnite..... | $\text{ZnO} \cdot \text{Al}_2\text{O}_3$ | 1.800 ± |
| Spessartite..... | $3\text{MnO} \cdot \text{Al}_2\text{O}_3 \cdot 3\text{SiO}_2$ | 1.811 |
| Lime..... | CaO | 1.830 |
| Uvarovite..... | $3\text{CaO} \cdot \text{Cr}_2\text{O}_3 \cdot 3\text{SiO}_2$ | 1.838 |
| Andradite..... | $3\text{CaO} \cdot \text{Fe}_2\text{O}_3 \cdot 3\text{SiO}_2$ | 1.857 |
| Microlite..... | $6\text{CaO} \cdot 3\text{Ta}_2\text{O}_5 \cdot \text{C}_6\text{H}_5\text{F}_3$ | 1.925 |
| Nantokite..... | CuCl | 1.930 |
| Pyrochlore..... | Contains CaO, Ce_2O_3 , TiO_2 , etc. | 1.960-2.000 |
| Schorlomite..... | $3\text{CaO} \cdot (\text{Fe}, \text{Ti})_2\text{O}_3 \cdot 3(\text{Si}, \text{Ti})\text{O}_2$ | 1.980 |
| Percylite..... | $\text{PbO} \cdot \text{CuCl}_2 \cdot \text{H}_2\text{O}$ | 2.050 |
| Picotite..... | $(\text{Mg}, \text{Fe})\text{O} \cdot (\text{Al}, \text{Cr})_2\text{O}_3$ | 2.050 ± |
| Eulytite..... | $2\text{Bi}_2\text{O}_3 \cdot 3\text{SiO}_2$ | 2.050 |
| Cerargyrite..... | AgCl | 2.061 |
| Mosesite..... | Contains Hg, NH_4 , Cl, etc. | 2.065 |
| Chromite..... | $\text{FeO} \cdot \text{Cr}_2\text{O}_3$ | 2.070 |
| Senarmontite..... | Sb_2O_3 | 2.087 |
| Embolite..... | $\text{Ag}(\text{Br}, \text{Cl})$ | 2.150 ± |
| Manganosite..... | MnO | 2.160 |
| Bunsenite..... | NiO | 2.18 (Li light) |
| Lewisite..... | $5\text{CaO} \cdot 2\text{TiO}_2 \cdot 3\text{Sb}_2\text{O}_5$ | 2.200 |
| Miersite..... | $\text{Cu}_2\text{I} \cdot \text{AgI}$ | 2.200 |
| Bromyrite..... | AgBr | 2.253 |
| Dysanalite..... | Contains CaO, FeO, TiO_2 , etc. | 2.330 |
| Marshite..... | CuI | 2.346 |
| Franklinite..... | $(\text{Zn}, \text{Fe}, \text{Mn})\text{O} \cdot (\text{Fe}, \text{Mn})_2\text{O}_3$ | 2.360 (Li light) |
| Sphalerite..... | $(\text{Zn}, \text{Fe})\text{S}$ | 2.370-2.470 |
| Perovskite..... | $\text{CaO} \cdot \text{TiO}_2$ | 2.380 |
| Diamond..... | C | 2.419 |
| Egiesonite..... | $\text{HgO} \cdot 2\text{HgCl}$ | 2.490 (Li light) |
| Hauerite..... | MnS_2 | 2.600 (Li light) |
| Aiabandite..... | MnS | 2.700 (Li light) |
| Cnrite..... | Cu_2O | 2.849 |

INDEX OF REFRACTION

Miscellaneous Monorefringent or Isotropic Solids

| Substance. | Spectrum line. | Index of refraction. | Authority. |
|----------------------------|----------------|----------------------|----------------------|
| Albite glass..... | D | 1.4890 | Larsen, 1909 |
| Amber..... | D | 1.546 | Mühlheim |
| Ammonium chloride..... | D | 1.6422 | Grailich |
| Anorthite glass..... | D | 1.5755 | Larsen, 1909 |
| Asphalt..... | D | 1.635 | E. L. Nichols |
| | | 1.621 | " " |
| Bell metal..... | 0.670 μ | 1.0052 | Beer |
| Boric Acid, melted..... | C | 1.4623 | Bedson and Williams |
| " " "..... | D | 1.4637 | " " " |
| " " "..... | F | 1.4604 | " " " |
| Borax, melted..... | C | 1.4624 | " " " |
| " " "..... | D | 1.4624 | " " " |
| " " "..... | D | 1.4630 | " " " |
| " " "..... | F | 1.4702 | " " " |
| Camphor..... | D | 1.532 | Kohlrausch |
| " " "..... | D | 1.5462 | Mühlheim |
| Canada balsam..... | D | 1.530 | Mean |
| Ebonite..... | red | 1.66 | Ayrton, Perry |
| Fuchsin..... | A | 2.03 | Mean |
| " " "..... | B | 2.19 | " " |
| " " "..... | C | 2.33 | " " |
| " " "..... | G | 1.97 | " " |
| " " "..... | H | 1.32 | " " |
| Gelatin, Nelson no. 1..... | D | 1.530 | Jones, 1911 |
| " various..... | D | 1.516-1.534 | " " |
| Gum Arabic..... | red | 1.480 | Jamin |
| " " "..... | red | 1.514 | Wollaston |
| Obsidian..... | D | 1.482-1.496 | Various |
| Phosphorus..... | D | 2.1442 | Gladstone, Dale |
| Pitch..... | red | 1.531 | Wollaston |
| Potassium bromide..... | D | 1.5593 | Topsøe, Christiansen |
| " chlorstannate..... | D | 1.6574 | " " |
| " iodide..... | D | 1.6666 | " " |
| Resins: Aloes..... | red | 1.619 | Jamin |
| Canada balsam..... | red | 1.528 | Wollaston |
| Colophony..... | red | 1.548 | Jamin |
| Copal..... | red | 1.528 | " " |
| Mastic..... | red | 1.535 | Wollaston |
| Peru balsam..... | D | 1.593 | Eaden Powell |
| Selenium..... | A | 2.61 | Wood |
| " " "..... | B | 2.68 | " " |
| " " "..... | C | 2.73 | " " |
| " " "..... | D | 2.93 | " " |
| Sodium chlorate..... | D | 1.5150 | Dussaud |
| Strontium nitrate..... | D | 1.5667 | Fock |

INDEX OF REFRACTION

Selected Uniaxial Minerals

The values are arranged in the order of increasing indices for the ordinary ray and are for the sodium D line unless otherwise indicated. Selected by Dr. Edgar T. Wherry from a private compilation of Dr. Esper S. Larsen of the U. S. Geological Survey.

| Mineral. | Formula. | Index of refraction. | |
|---------------------------------|--|----------------------|--------------------|
| | | Ordinary ray. | Extraordinary ray. |
| (a) UNIAXIAL POSITIVE MINERALS. | | | |
| Ice..... | H ₂ O | 1.309 | 1.313 |
| Sellaite..... | MgF ₂ | 1.378 | 1.390 |
| Chrysocolla..... | CuO.SiO ₂ .2H ₂ O | 1.460 = | 1.570 = |
| Laubanite..... | 2CaO.Al ₂ O ₃ .5SiO ₂ .6H ₂ O | 1.475 | 1.486 |
| Chabazite..... | (Ca, Na ₂)O.Al ₂ O ₃ .4SiO ₂ .6H ₂ O | 1.480 = | 1.482 = |
| Douglasite..... | 2KCl.FeCl ₂ .2H ₂ O | 1.488 | 1.500 |
| Hydronephelite..... | 2Na ₂ O.3Al ₂ O ₃ .6SiO ₂ .7H ₂ O | 1.490 | 1.502 |
| Apophyllite..... | K ₂ O.8CaO.16SiO ₂ .16H ₂ O | 1.535 = | 1.537 = |
| Quartz..... | SiO ₂ | 1.544 | 1.553 |
| Coquimbite..... | Fe ₂ O ₃ .3SO ₃ .9H ₂ O | 1.550 | 1.556 |
| Brucite..... | MgO.H ₂ O | 1.559 | 1.580 |
| Alunite..... | K ₂ O.3Al ₂ O ₃ .4SO ₃ .6H ₂ O | 1.572 | 1.592 |
| Penninite..... | 5(Mg, Fe)O.Al ₂ O ₃ .3SiO ₂ .4H ₂ O | 1.576 | 1.579 |
| Cacoxenite..... | 2Fe ₂ O ₃ .P ₂ O ₅ .12H ₂ O | 1.582 | 1.645 |
| Eudialite..... | 6Na ₂ O.6(Ca, Fe)O.20(Si, Zr)O ₂ .NaCl | 1.606 | 1.611 |
| Diopside..... | CuO.SiO ₂ .H ₂ O | 1.654 | 1.707 |
| Phenacite..... | 2BeO.SiO ₂ | 1.654 | 1.670 |
| Parisite..... | 2CeOF.CaO.3CO ₂ | 1.676 | 1.757 |
| Willemite..... | 2ZnO.SiO ₂ | 1.694 | 1.723 |
| Vesuvianite..... | 2(Ca, Mn, Fe)O.(Al, Fe)(OH, F)O.2SiO ₂ | 1.716 = | 1.718 = |
| Xenotime..... | Y ₂ O ₃ .P ₂ O ₅ | 1.721 | 1.816 |
| Connellite..... | 20CuO.SO ₃ .2CuCl ₂ .20H ₂ O | 1.724 | 1.746 |
| Benitoite..... | BaO.TiO ₂ .3SiO ₂ | 1.757 | 1.804 |
| Ganomallite..... | 6PbO.4(Ca, Mn)O.6SiO ₂ .H ₂ O | 1.910 | 1.945 |
| Scheelite..... | CaO.WO ₃ | 1.918 | 1.934 |
| Zircon..... | ZrO ₂ .SiO ₂ | 1.923 = | 1.968 = |
| Powellite..... | CaO.MoO ₃ | 1.967 | 1.978 |
| Calomel..... | HgCl | 1.973 | 2.050 |
| Cassiterite..... | SnO ₂ | 1.997 | 2.093 |
| Zincite..... | ZnO | 2.008 | 2.029 |
| Phosgenite..... | PbO.PbCl ₂ .CO ₂ | 2.114 | 2.140 |
| Penfieldite..... | PbO.2PbCl ₂ | 2.130 | 2.210 |
| Iodyrite..... | AgI | 2.210 | 2.220 |
| Tapiolite..... | FeO.(Ta, Nb) ₂ O ₅ | 2.270 | 2.420 (Li light) |
| Wurtzite..... | ZnS | 2.356 | 2.378 |
| Derbylite..... | 6FeO.Sb ₂ O ₃ .5TiO ₂ | 2.450 | 2.510 (Li light) |
| Greenockite..... | CdS | 2.506 | 2.529 |
| Rutile..... | TiO ₂ | 2.616 | 2.903 |
| Moissanite..... | CSi | 2.654 | 2.697 |
| Cinnabarite..... | HgS | 2.854 | 3.201 |
| (b) UNIAXIAL NEGATIVE MINERALS. | | | |
| Chiolite..... | 2NaF.AlF ₃ | 1.349 | 1.342 |
| Hanksite..... | 11Na ₂ O.9SO ₃ .2CO ₂ .KCl | 1.481 | 1.461 |
| Thaumasite..... | 3CaO.CO ₂ .SiO ₂ .SO ₃ .15H ₂ O | 1.507 | 1.468 |
| Hydrocalcite..... | 6MgO.Al ₂ O ₃ .CO ₂ .15H ₂ O | 1.512 | 1.498 |
| Cancrinite..... | 4Na ₂ O.CaO.4Al ₂ O ₃ .2CO ₂ .9SiO ₂ .3H ₂ O | 1.524 | 1.496 |
| Milarite..... | K ₂ O.4CaO.2Al ₂ O ₃ .24SiO ₂ .H ₂ O | 1.532 | 1.529 |
| Kaliophyllite..... | K ₂ O.Al ₂ O ₃ .2SiO ₂ | 1.537 | 1.533 |
| Mellite..... | Al ₂ O ₃ .C ₁₂ O ₇ .18H ₂ O | 1.539 | 1.511 |
| Marielite..... | "Ma" = 3Na ₂ O.3Al ₂ O ₃ .18SiO ₂ .2NaCl | 1.539 | 1.537 |
| Nephelite..... | Na ₂ O.Al ₂ O ₃ .2SiO ₂ | 1.542 | 1.538 |

INDEX OF REFRACTION

TABLE 405 (Continued).—Selected Uniaxial Minerals

| Mineral. | Formula. | Index of refraction. | |
|---|--|----------------------|--------------------|
| | | Ordinary ray. | Extraordinary ray. |
| (b) UNIAxIAL NEGATIVE MINERALS (continued). | | | |
| Wernerite..... | $\text{Me}_3\text{Mg}_4 \pm$ | 1.578 | 1.551 |
| Beryl..... | $3\text{BeO} \cdot \text{Al}_2\text{O}_3 \cdot 6\text{SiO}_2$ | 1.581 \pm | 1.575 \pm |
| Torbernite..... | $\text{CuO} \cdot 2\text{UO}_2 \cdot \text{P}_2\text{O}_5 \cdot 8\text{H}_2\text{O}$ | 1.592 | 1.582 |
| Meionite..... | "Me" = $4\text{CaO} \cdot 3\text{Al}_2\text{O}_3 \cdot 6\text{SiO}_2$ | 1.597 | 1.560 |
| Mellite..... | Contains Na_2O , CaO , Al_2O_3 , SiO_2 , etc. | 1.634 | 1.620 |
| Apatite..... | $9\text{CaO} \cdot 3\text{P}_2\text{O}_5 \cdot \text{Ca}(\text{F}, \text{Cl})_2$ | 1.634 | 1.631 |
| Calcite..... | $\text{CaO} \cdot \text{CO}_2$ | 1.658 | 1.486 |
| Gehlenite..... | $2\text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot \text{SiO}_2$ | 1.660 | 1.658 |
| Tourmaline..... | Contains Na_2O , FeO , Al_2O_3 , B_2O_3 , SiO_2 , etc. | 1.660 \pm | 1.638 \pm |
| Dolomite..... | $\text{CaO} \cdot \text{MgO} \cdot 2\text{CO}_2$ | 1.682 | 1.593 |
| Magnesite..... | $\text{MgO} \cdot \text{CO}_2$ | 1.700 | 1.509 |
| Pyrochroite..... | $\text{MnO} \cdot \text{H}_2\text{O}$ | 1.723 | 1.681 |
| Corundum..... | Al_2O_3 | 1.768 | 1.760 |
| Smithsonite..... | $\text{ZnO} \cdot \text{CO}_2$ | 1.818 | 1.618 |
| Rhodochrosite..... | $\text{MnO} \cdot \text{CO}_2$ | 1.818 | 1.595 |
| Jacobsite..... | $\text{K}_2\text{O} \cdot 3\text{Fe}_2\text{O}_3 \cdot 4\text{SO}_3 \cdot 6\text{H}_2\text{O}$ | 1.820 | 1.715 |
| Siderite..... | $\text{FeO} \cdot \text{CO}_2$ | 1.875 | 1.635 |
| Pyromorphite..... | $9\text{PbO} \cdot 3\text{F}_2\text{O}_3 \cdot \text{PbCl}_2$ | 2.050 | 2.042 |
| Barysilite..... | $3\text{PbO} \cdot 2\text{SiO}_2$ | 2.070 | 2.050 |
| Mimetite..... | $9\text{PbO} \cdot 3\text{As}_2\text{O}_5 \cdot \text{PbCl}_2$ | 2.135 | 2.118 |
| Matlockite..... | $\text{PbO} \cdot \text{PbCl}_2$ | 2.150 | 2.040 |
| Stolzite..... | $\text{PbO} \cdot \text{WO}_3$ | 2.260 | 2.182 |
| Geikielite..... | $(\text{Mg}, \text{Fe})\text{O} \cdot \text{TiO}_2$ | 2.310 | 1.950 |
| Vanadinite..... | $9\text{PbO} \cdot 3\text{V}_2\text{O}_5 \cdot \text{PbCl}_2$ | 2.354 | 2.290 |
| Wulfenite..... | $\text{PbO} \cdot \text{MoO}_3$ | 2.402 | 2.304 (Li light) |
| Octahedrite..... | TiO_2 | 2.554 | 2.493 |
| Massicotite..... | PbO | 2.665 | 2.535 (Li light) |
| Proustite..... | $3\text{Ag}_2\text{S} \cdot \text{As}_2\text{S}_3$ | 2.970 | 2.711 |
| Pyrazurite..... | $3\text{Ag}_2\text{S} \cdot \text{Sb}_2\text{S}_3$ | 3.084 | 2.881 " " |
| Hematite..... | Fe_2O_3 | 3.220 | 2.940 " " |

TABLE 406.—Miscellaneous Uniaxial Crystals

| Crystal. | Spectrum line. | Index of refraction. | | Authority. |
|---|----------------|----------------------|--------------------|------------|
| | | Ordinary ray. | Extraordinary ray. | |
| Ammonium arseniate $\text{NH}_4\text{H}_2\text{AsO}_4$ | D | 1.5766 | 1.5217 | T. and C.* |
| Benzil $(\text{C}_6\text{H}_5\text{CO})_2$ | D | 1.6588 | 1.6784 | Mean |
| Corundum, Al_2O_3 , sapphire, ruby..... | D | 1.769 | 1.760 | Osann |
| Ice at -8°C | D | 1.308 | 1.313 | Meyer |
| " " "..... | Li | 1.297 | 1.304 | " |
| Ivory..... | D | 1.530 | 1.541 | Kohlrausch |
| Potassium arseniate KH_2AsO_4 | F | 1.5702 | 1.5252 | T. and C. |
| " " "..... | D | 1.5674 | 1.5179 | " " " |
| " " "..... | C | 1.5632 | 1.5246 | " " " |
| Sodium arseniate $\text{Na}_3\text{AsO}_4 \cdot 12\text{H}_2\text{O}$ | D | 1.457 | 1.466 | Mean |
| " nitrate NaNO_3 | D | 1.586 | 1.336 | " |
| " phosphate $\text{Na}_3\text{PO}_4 \cdot 12\text{H}_2\text{O}$ | D | 1.447 | 1.453 | " |
| Nickel sulphate $\text{NiSO}_4 \cdot 6\text{H}_2\text{O}$ | F | 1.5173 | 1.4930 | T. and C. |
| " " "..... | D | 1.5109 | 1.4873 | " " " |
| " " "..... | C | 1.5078 | 1.4844 | " " " |
| Strychnine sulphate..... | D | 1.614 | 1.599 | Martin |

*Topsöe and Christiansen.

TABLE 407

INDEX OF REFRACTION

Selected Biaxial Minerals

The values are arranged in the order of increasing β index of refraction and are for the sodium D line except where noted. Selected by Dr. Edgar T. Wherry from private compilation of Dr. Esper S. Larsen of the U. S. Geological Survey.

| Mineral. | Formula. | Index of refraction. | | |
|--------------------------------|---|----------------------|-----------|------------|
| | | n_α | n_β | n_γ |
| (a) BIAxIAL POSITIVE MINERALS. | | | | |
| Stercorite..... | $\text{Na}_2\text{O} \cdot (\text{NH}_4)_2\text{O} \cdot \text{P}_2\text{O}_5 \cdot 9\text{H}_2\text{O}$ | 1.439 | 1.441 | 1.460 |
| Aluminite..... | $\text{Al}_2\text{O}_3 \cdot \text{SO}_3 \cdot 9\text{H}_2\text{O}$ | 1.459 | 1.464 | 1.470 |
| Tridymite..... | SiO_2 | 1.469 | 1.470 | 1.473 |
| Thenardite..... | $\text{Na}_2\text{O} \cdot \text{SO}_3$ | 1.464 | 1.474 | 1.485 |
| Carnallite..... | $\text{KCl} \cdot \text{MgCl}_2 \cdot 6\text{H}_2\text{O}$ | 1.466 | 1.475 | 1.494 |
| Alunogenite..... | $\text{Al}_2\text{O}_3 \cdot 3\text{SO}_3 \cdot 16\text{H}_2\text{O}$ | 1.474 | 1.476 | 1.483 |
| Melanterite..... | $\text{FeO} \cdot \text{SO}_3 \cdot 7\text{H}_2\text{O}$ | 1.471 | 1.478 | 1.486 |
| Natroliite..... | $\text{Na}_2\text{O} \cdot \text{Al}_2\text{O}_3 \cdot 3\text{SiO}_2 \cdot 2\text{H}_2\text{O}$ | 1.480 | 1.482 | 1.493 |
| Arcanite..... | $\text{K}_2\text{O} \cdot \text{SO}_3$ | 1.494 | 1.495 | 1.497 |
| Struvite..... | $(\text{NH}_4)_2\text{O} \cdot 2\text{MgO} \cdot \text{P}_2\text{O}_5 \cdot 12\text{H}_2\text{O}$ | 1.495 | 1.496 | 1.504 |
| Heulandite..... | $\text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot 6\text{SiO}_2 \cdot 3\text{H}_2\text{O}$ | 1.498 | 1.499 | 1.505 |
| Thomsonite..... | $(\text{Na}_2, \text{Ca})\text{O} \cdot \text{Al}_2\text{O}_3 \cdot 2\text{SiO}_2 \cdot 3\text{H}_2\text{O}$ | 1.497 | 1.503 | 1.525 |
| Harmotomite..... | $(\text{K}_2, \text{Ba})\text{O} \cdot \text{Al}_2\text{O}_3 \cdot 5\text{SiO}_2 \cdot 5\text{H}_2\text{O}$ | 1.503 | 1.505 | 1.508 |
| Petalite..... | $\text{Li}_2\text{O} \cdot \text{Al}_2\text{O}_3 \cdot 8\text{SiO}_2$ | 1.504 | 1.510 | 1.516 |
| Monetite..... | $2\text{CaO} \cdot \text{P}_2\text{O}_5 \cdot \text{H}_2\text{O}$ | 1.515 | 1.518 | 1.525 |
| Newberryite..... | $2\text{MgO} \cdot \text{P}_2\text{O}_5 \cdot 7\text{H}_2\text{O}$ | 1.514 | 1.519 | 1.533 |
| Gypsum..... | $\text{CaO} \cdot \text{SO}_3 \cdot 2\text{H}_2\text{O}$ | 1.520 | 1.523 | 1.530 |
| Muscagnite..... | $(\text{NH}_4)_2\text{O} \cdot \text{SO}_3$ | 1.521 | 1.523 | 1.533 |
| Albite..... | "Ab" = $\text{Na}_2\text{O} \cdot \text{Al}_2\text{O}_3 \cdot 6\text{SiO}_2$ | 1.525 | 1.529 | 1.536 |
| Hydromagnesite..... | $4\text{MgO} \cdot 3\text{CO}_2 \cdot 4\text{H}_2\text{O}$ | 1.527 | 1.530 | 1.540 |
| Wavellite..... | $3\text{Al}_2\text{O}_3 \cdot 2\text{P}_2\text{O}_5 \cdot 12(\text{H}_2\text{O}, 2\text{HF})$ | 1.525 | 1.534 | 1.552 |
| Kieserite..... | $\text{MgO} \cdot \text{SO}_3 \cdot \text{H}_2\text{O}$ | 1.523 | 1.535 | 1.586 |
| Copiapite..... | $2\text{Fe}_2\text{O}_3 \cdot 5\text{SO}_3 \cdot 18\text{H}_2\text{O}$ | 1.530 | 1.543 | 1.595 |
| Whewellite..... | $\text{CaO} \cdot \text{C}_2\text{O}_3 \cdot \text{H}_2\text{O}$ | 1.491 | 1.555 | 1.650 |
| Variscite..... | $\text{Al}_2\text{O}_3 \cdot \text{P}_2\text{O}_5 \cdot 4\text{H}_2\text{O}$ | 1.551 | 1.558 | 1.582 |
| Labradorite..... | Ab_2An_3 | 1.559 | 1.563 | 1.568 |
| Gibbsite..... | $\text{Al}_2\text{O}_3 \cdot 3\text{H}_2\text{O}$ | 1.566 | 1.566 | 1.587 |
| Wagnerite..... | $3\text{MgO} \cdot \text{P}_2\text{O}_5 \cdot \text{MgF}_2$ | 1.569 | 1.570 | 1.582 |
| Anhydrite..... | $\text{CaO} \cdot \text{SO}_3$ | 1.571 | 1.576 | 1.614 |
| Colemanite..... | $2\text{CaO} \cdot 3\text{B}_2\text{O}_3 \cdot 5\text{H}_2\text{O}$ | 1.586 | 1.592 | 1.614 |
| Fremontite..... | $\text{Na}_2\text{O} \cdot \text{Al}_2\text{O}_3 \cdot \text{P}_2\text{O}_5 \cdot (\text{H}_2\text{O}, 2\text{HF})$ | 1.594 | 1.603 | 1.615 |
| Vivianite..... | $3\text{FeO} \cdot \text{P}_2\text{O}_5 \cdot 8\text{H}_2\text{O}$ | 1.579 | 1.603 | 1.633 |
| Pectolite..... | $\text{Na}_2\text{O} \cdot 4\text{CaO} \cdot 6\text{SiO}_2 \cdot \text{H}_2\text{O}$ | 1.595 | 1.606 | 1.634 |
| Calamine..... | $2\text{ZnO} \cdot \text{SiO}_2 \cdot \text{H}_2\text{O}$ | 1.614 | 1.617 | 1.636 |
| Chondrodite..... | $4\text{MgO} \cdot 2\text{SiO}_2 \cdot \text{Mg}(\text{F}, \text{OH})_2$ | 1.609 | 1.616 | 1.630 |
| Turquois..... | $\text{CuO} \cdot 3\text{Al}_2\text{O}_3 \cdot 2\text{P}_2\text{O}_5 \cdot 9\text{H}_2\text{O}$ | 1.610 | 1.620 | 1.650 |
| Topaz..... | $2\text{AlOF} \cdot \text{SiO}_2$ | 1.619 | 1.620 | 1.627 |
| Celestine..... | $\text{SrO} \cdot \text{SO}_3$ | 1.622 | 1.624 | 1.631 |
| Prehnite..... | $2\text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot 3\text{SiO}_2 \cdot \text{H}_2\text{O}$ | 1.616 | 1.626 | 1.640 |
| Barite..... | $\text{BaO} \cdot \text{SO}_3$ | 1.636 | 1.637 | 1.648 |
| Anthophyllite..... | $\text{MgO} \cdot \text{SiO}_2$ | 1.633 | 1.642 | 1.657 |
| Sillimanite..... | $\text{Al}_2\text{O}_3 \cdot \text{SiO}_2$ | 1.638 | 1.642 | 1.653 |
| Forsterite..... | $2\text{MgO} \cdot \text{SiO}_2$ | 1.635 | 1.651 | 1.670 |
| Enstatite..... | $\text{MgO} \cdot \text{SiO}_2$ | 1.650 | 1.653 | 1.658 |
| Euclase..... | $2\text{BeO} \cdot \text{Al}_2\text{O}_3 \cdot 2\text{SiO}_2 \cdot \text{H}_2\text{O}$ | 1.652 | 1.655 | 1.671 |
| Triplite..... | $3\text{MnO} \cdot \text{P}_2\text{O}_5 \cdot \text{MnF}_2$ | 1.650 | 1.660 | 1.672 |
| Spodumenite..... | $\text{Li}_2\text{O} \cdot \text{Al}_2\text{O}_3 \cdot 4\text{SiO}_2$ | 1.660 | 1.666 | 1.676 |
| Diopside..... | $\text{CaO} \cdot \text{MgO} \cdot 2\text{SiO}_2$ | 1.664 | 1.671 | 1.694 |
| Olivine..... | $2(\text{Mg}, \text{Fe})\text{O} \cdot \text{SiO}_2$ | 1.662 | 1.680 | 1.699 |
| Triphylite..... | $\text{Li}_2\text{O} \cdot 2(\text{Fe}, \text{Mn})\text{O} \cdot \text{P}_2\text{O}_5$ | 1.688 | 1.688 | 1.692 |

INDEX OF REFRACTION

Selected Biaxial Minerals

| Mineral. | Formula. | Index of refraction. | | |
|--|--|----------------------|-----------|------------|
| | | n_α | n_β | n_γ |
| (a) BIAxIAL POSITIVE MINERALS (continued). | | | | |
| Zoisite..... | $4\text{CaO} \cdot 3\text{Al}_2\text{O}_3 \cdot 6\text{SiO}_2 \cdot \text{H}_2\text{O}$ | 1.700 | 1.702 | 1.706 |
| Strengite..... | $\text{Fe}_2\text{O}_3 \cdot \text{P}_2\text{O}_5 \cdot 4\text{H}_2\text{O}$ | 1.710 | 1.710 | 1.745 |
| Diasporite..... | $\text{Al}_2\text{O}_3 \cdot \text{H}_2\text{O}$ | 1.702 | 1.722 | 1.750 |
| Staurolite..... | $2\text{FeO} \cdot 5\text{Al}_2\text{O}_3 \cdot 4\text{SiO}_2 \cdot \text{H}_2\text{O}$ | 1.736 | 1.741 | 1.746 |
| Chrysoberyl..... | $\text{BeO} \cdot \text{Al}_2\text{O}_3$ | 1.747 | 1.748 | 1.757 |
| Azurite..... | $3\text{CuO} \cdot 2\text{CO}_2 \cdot \text{H}_2\text{O}$ | 1.730 | 1.758 | 1.838 |
| Scorodite..... | $\text{Fe}_2\text{O}_3 \cdot \text{As}_2\text{O}_5 \cdot 4\text{H}_2\text{O}$ | 1.705 | 1.774 | 1.797 |
| Olivinite..... | $4\text{CuO} \cdot \text{As}_2\text{O}_5 \cdot \text{H}_2\text{O}$ | 1.772 | 1.810 | 1.863 |
| Anglesite..... | $\text{PbO} \cdot \text{SO}_3$ | 1.877 | 1.882 | 1.894 |
| Titanite..... | $\text{CaO} \cdot \text{TiO}_2 \cdot \text{SiO}_2$ | 1.900 | 1.907 | 2.034 |
| Claudetite..... | As_2O_3 | 1.871 | 1.920 | 2.010 |
| Sulfur..... | S | 1.950 | 2.043 | 2.240 |
| Cotunnite..... | PbCl_2 | 2.200 | 2.217 | 2.260 |
| Huebnerite..... | $\text{MnO} \cdot \text{WO}_3$ | 2.170 | 2.220 | 2.320 |
| Manganite..... | $\text{Mn}_2\text{O}_3 \cdot \text{H}_2\text{O}$ | 2.240 | 2.240 | 2.530 (Li) |
| Raspite..... | $\text{PbO} \cdot \text{WO}_3$ | 2.270 | 2.270 | 2.300 |
| Mendipite..... | $2\text{PbO} \cdot \text{PbCl}_2$ | 2.240 | 2.270 | 2.310 |
| Tantalite..... | $(\text{Fe}, \text{Mn})\text{O} \cdot \text{Ta}_2\text{O}_5$ | 2.260 | 2.320 | 2.430 (Li) |
| Wolframite..... | $(\text{Fe}, \text{Mn})\text{O} \cdot \text{WO}_3$ | 2.310 | 2.360 | 2.460 (Li) |
| Crocoite..... | $\text{PbO} \cdot \text{CrO}_3$ | 2.310 | 2.370 | 2.660 (Li) |
| Pseudobrookite..... | $2\text{Fe}_2\text{O}_3 \cdot 3\text{TiO}_2$ | 2.380 | 2.390 | 2.420 (Li) |
| Stibiotantalite..... | $\text{Sb}_2\text{O}_5 \cdot \text{Ta}_2\text{O}_5$ | 2.374 | 2.404 | 2.457 |
| Montroydite..... | HgO | 2.370 | 2.500 | 2.650 (Li) |
| Brookite..... | TiO_2 | 2.583 | 2.586 | 2.741 |
| Lithargite..... | PbO | 2.510 | 2.610 | 2.710 |
| (b) BIAxIAL NEGATIVE MINERALS. | | | | |
| Mirabilite..... | $\text{Na}_2\text{O} \cdot \text{SO}_3 \cdot 10\text{H}_2\text{O}$ | 1.394 | 1.396 | 1.398 |
| Thomsonolite..... | $\text{NaF} \cdot \text{CaF}_2 \cdot \text{AlF}_3 \cdot \text{H}_2\text{O}$ | 1.407 | 1.414 | 1.415 |
| Natron..... | $\text{Na}_2\text{O} \cdot \text{CO}_2 \cdot 10\text{H}_2\text{O}$ | 1.405 | 1.425 | 1.440 |
| Kalinite..... | $\text{K}_2\text{O} \cdot \text{Al}_2\text{O}_3 \cdot 4\text{SO}_3 \cdot 24\text{H}_2\text{O}$ | 1.430 | 1.452 | 1.458 |
| Epsomite..... | $\text{MgO} \cdot \text{SO}_3 \cdot 7\text{H}_2\text{O}$ | 1.433 | 1.455 | 1.461 |
| Sassolite..... | $\text{B}_2\text{O}_3 \cdot \text{H}_2\text{O}$ | 1.340 | 1.450 | 1.450 |
| Borax..... | $\text{Na}_2\text{O} \cdot 2\text{B}_2\text{O}_3 \cdot 10\text{H}_2\text{O}$ | 1.447 | 1.470 | 1.472 |
| Goslarite..... | $\text{ZnO} \cdot \text{SO}_3 \cdot 7\text{H}_2\text{O}$ | 1.457 | 1.480 | 1.484 |
| Pickeringite..... | $\text{MgO} \cdot \text{Al}_2\text{O}_3 \cdot 4\text{SO}_3 \cdot 22\text{H}_2\text{O}$ | 1.476 | 1.480 | 1.483 |
| Bloedite..... | $\text{Na}_2\text{O} \cdot \text{MgO} \cdot 2\text{SO}_3 \cdot 4\text{H}_2\text{O}$ | 1.486 | 1.488 | 1.489 |
| Trona..... | $3\text{Na}_2\text{O} \cdot 4\text{CO}_2 \cdot 5\text{H}_2\text{O}$ | 1.410 | 1.492 | 1.542 |
| Thermonatrite..... | $\text{Na}_2\text{O} \cdot \text{CO}_2 \cdot \text{H}_2\text{O}$ | 1.420 | 1.495 | 1.518 |
| Stilbite..... | $(\text{Ca}, \text{Na})\text{O} \cdot \text{Al}_2\text{O}_3 \cdot 6\text{SiO}_2 \cdot 5\text{H}_2\text{O}$ | 1.494 | 1.498 | 1.500 |
| Niter..... | $\text{K}_2\text{O} \cdot \text{Na}_2\text{O}$ | 1.334 | 1.505 | 1.506 |
| Kainite..... | $\text{MgO} \cdot \text{SO}_3 \cdot \text{KCl} \cdot 3\text{H}_2\text{O}$ | 1.494 | 1.505 | 1.516 |
| Gaylussite..... | $\text{Na}_2\text{O} \cdot \text{CaO} \cdot 2\text{CO}_2 \cdot 5\text{H}_2\text{O}$ | 1.444 | 1.516 | 1.523 |
| Scolecite..... | $\text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot 3\text{SiO}_2 \cdot 3\text{H}_2\text{O}$ | 1.512 | 1.521 | 1.519 |
| Laumontite..... | $\text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot 4\text{SiO}_2 \cdot 4\text{H}_2\text{O}$ | 1.513 | 1.521 | 1.525 |
| Orthoclase..... | $\text{K}_2\text{O} \cdot \text{Al}_2\text{O}_3 \cdot 6\text{SiO}_2$ | 1.518 | 1.521 | 1.520 |
| Microcline..... | Same as preceding | 1.522 | 1.526 | 1.530 |
| Anorthoclase..... | $(\text{Na}, \text{K})\text{O} \cdot \text{Al}_2\text{O}_3 \cdot 6\text{SiO}_2$ | 1.523 | 1.529 | 1.531 |
| Glauberite..... | $\text{Na}_2\text{O} \cdot \text{CaO} \cdot 2\text{SO}_3$ | 1.515 | 1.532 | 1.536 |
| Cordierite..... | $4(\text{Mg}, \text{Fe})\text{O} \cdot 4\text{Al}_2\text{O}_3 \cdot 10\text{SiO}_2 \cdot \text{H}_2\text{O}$ | 1.534 | 1.538 | 1.540 |
| Chalcantithite..... | $\text{CuO} \cdot \text{SO}_3 \cdot 5\text{H}_2\text{O}$ | 1.516 | 1.539 | 1.546 |
| Oligoclase..... | Ab_4An | 1.539 | 1.543 | 1.547 |

INDEX OF REFRACTION

Selected Biaxial Minerals

| Mineral. | Formula. | Index of refraction. | | |
|--|--|----------------------|-----------|------------|
| | | n_a | n_β | n_γ |
| (b) BIAxIAL NEGATIVE CRYSTALS (continued). | | | | |
| Beryllonite..... | $\text{Na}_2\text{O} \cdot 2\text{BeO} \cdot \text{P}_2\text{O}_5$ | 1.552 | 1.558 | 1.561 |
| Kaolinite..... | $\text{Al}_2\text{O}_3 \cdot 2\text{SiO}_2 \cdot 2\text{H}_2\text{O}$ | 1.561 | 1.563 | 1.565 |
| Biotite..... | $\text{K}_2\text{O} \cdot 4(\text{Mg}, \text{Fe})\text{O} \cdot 2\text{Al}_2\text{O}_3 \cdot 6\text{SiO}_2 \cdot \text{H}_2\text{O}$ | 1.541 | 1.574 | 1.574 |
| Autunite..... | $\text{CaO} \cdot 2\text{UO}_3 \cdot \text{P}_2\text{O}_5 \cdot 8\text{H}_2\text{O}$ | 1.553 | 1.575 | 1.577 |
| Anorthite..... | "An" = $\text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot 2\text{SiO}_2$ | 1.576 | 1.584 | 1.588 |
| Lanthanite..... | $\text{La}_2\text{O}_3 \cdot 3\text{CO}_2 \cdot 9\text{H}_2\text{O}$ | 1.520 | 1.587 | 1.613 |
| Pyrophyllite..... | $\text{Al}_2\text{O}_3 \cdot 4\text{SiO}_2 \cdot \text{H}_2\text{O}$ | 1.552 | 1.588 | 1.600 |
| Talc..... | $3\text{MgO} \cdot 4\text{SiO}_2 \cdot \text{H}_2\text{O}$ | 1.539 | 1.589 | 1.589 |
| Hopeite..... | $3\text{ZnO} \cdot \text{P}_2\text{O}_5 \cdot 4\text{H}_2\text{O}$ | 1.572 | 1.590 | 1.590 |
| Muscovite..... | $\text{K}_2\text{O} \cdot 3\text{Al}_2\text{O}_3 \cdot 6\text{SiO}_2 \cdot 2\text{H}_2\text{O}$ | 1.561 | 1.590 | 1.591 |
| Amblygonite..... | $\text{Al}_2\text{O}_3 \cdot \text{P}_2\text{O}_5 \cdot 2\text{LiF}$ | 1.570 | 1.593 | 1.597 |
| Lepidolite..... | $\text{Al}_2\text{O}_3 \cdot 3\text{SiO}_2 \cdot 2(\text{K}, \text{Li})\text{F}$ | 1.560 | 1.598 | 1.605 |
| Phlogopite..... | $\text{K}_2\text{O} \cdot 6\text{MgO} \cdot \text{Al}_2\text{O}_3 \cdot 6\text{SiO}_2 \cdot 2\text{H}_2\text{O}$ | 1.562 | 1.606 | 1.606 |
| Tremolite..... | $\text{CaO} \cdot 3\text{MgO} \cdot 4\text{SiO}_2$ | 1.609 | 1.623 | 1.635 |
| Actinolite..... | $\text{CaO} \cdot 3(\text{Mg}, \text{Fe})\text{O} \cdot 4\text{SiO}_2$ | 1.611 | 1.627 | 1.636 |
| Wollastonite..... | $\text{CaO} \cdot \text{SiO}_2$ | 1.616 | 1.629 | 1.631 |
| Lazulite..... | $(\text{Fe}, \text{Mg})\text{O} \cdot \text{Al}_2\text{O}_3 \cdot \text{P}_2\text{O}_5 \cdot \text{H}_2\text{O}$ | 1.603 | 1.632 | 1.639 |
| Danburite..... | $\text{CaO} \cdot \text{B}_2\text{O}_3 \cdot 2\text{SiO}_2$ | 1.632 | 1.634 | 1.636 |
| Glaucophanite..... | $\text{Na}_2\text{O} \cdot 2\text{FeO} \cdot \text{Al}_2\text{O}_3 \cdot 6\text{SiO}_2$ | 1.621 | 1.638 | 1.638 |
| Andalusite..... | $\text{Al}_2\text{O}_3 \cdot \text{SiO}_2$ | 1.632 | 1.638 | 1.643 |
| Hornblende..... | Contains Na_2O , MgO , FeO , SiO_2 , etc. | 1.629 | 1.642 | 1.653 |
| Datolite..... | $2\text{CaO} \cdot 2\text{SiO}_2 \cdot \text{B}_2\text{O}_3 \cdot \text{H}_2\text{O}$ | 1.625 | 1.653 | 1.669 |
| Erythrite..... | $3\text{CoO} \cdot \text{As}_2\text{O}_5 \cdot 8\text{H}_2\text{O}$ | 1.626 | 1.661 | 1.699 |
| Monticellite..... | $\text{CaO} \cdot \text{MgO} \cdot \text{SiO}_2$ | 1.651 | 1.662 | 1.668 |
| Strontianite..... | $\text{SrO} \cdot \text{CO}_2$ | 1.520 | 1.667 | 1.667 |
| Witherite..... | $\text{BaO} \cdot \text{CO}_2$ | 1.529 | 1.676 | 1.677 |
| Aragonite..... | $\text{CaO} \cdot \text{CO}_2$ | 1.531 | 1.682 | 1.686 |
| Axinite..... | $6(\text{Ca}, \text{Mn})\text{O} \cdot 2\text{Al}_2\text{O}_3 \cdot \text{B}_2\text{O}_3 \cdot 8\text{SiO}_2 \cdot \text{H}_2\text{O}$ | 1.678 | 1.685 | 1.688 |
| Dumortierite..... | $8\text{Al}_2\text{O}_3 \cdot \text{B}_2\text{O}_3 \cdot 6\text{SiO}_2 \cdot \text{H}_2\text{O}$ | 1.678 | 1.686 | 1.689 |
| Cyanite..... | $\text{Al}_2\text{O}_3 \cdot \text{SiO}_2$ | 1.712 | 1.720 | 1.728 |
| Epidote..... | $4\text{CaO} \cdot 3(\text{Al}, \text{Fe})_2\text{O}_3 \cdot 6\text{SiO}_2 \cdot \text{H}_2\text{O}$ | 1.729 | 1.754 | 1.768 |
| Atacamite..... | $3\text{CuO} \cdot \text{CuCl}_2 \cdot 3\text{H}_2\text{O}$ | 1.831 | 1.861 | 1.880 |
| Fayalite..... | $2\text{FeO} \cdot \text{SiO}_2$ | 1.824 | 1.864 | 1.874 |
| Caledonite..... | $2(\text{Pb}, \text{Cu})\text{O} \cdot \text{SO}_3 \cdot \text{H}_2\text{O}$ | 1.818 | 1.866 | 1.909 |
| Malachite..... | $2\text{CuO} \cdot \text{CO}_2 \cdot \text{H}_2\text{O}$ | 1.655 | 1.875 | 1.909 |
| Lanarkite..... | $2\text{PbO} \cdot \text{SO}_3$ | 1.930 | 1.990 | 2.020 |
| Leadhillite..... | $4\text{PbO} \cdot \text{SO}_3 \cdot 2\text{CO}_2 \cdot \text{H}_2\text{O}$ | 1.870 | 2.000 | 2.010 |
| Cerussite..... | $\text{PbO} \cdot \text{CO}_2$ | 1.804 | 2.076 | 2.078 |
| Laurionite..... | $\text{PbCl}_2 \cdot \text{PbO} \cdot \text{H}_2\text{O}$ | 2.077 | 2.116 | 2.158 |
| Matlockite..... | $\text{PbO} \cdot \text{PbCl}_2$ | 2.040 | 2.150 | 2.150 |
| Baddeleyite..... | ZrO_2 | 2.130 | 2.190 | 2.200 |
| Lepidocrocite..... | $\text{Fe}_2\text{O}_3 \cdot \text{H}_2\text{O}$ | 1.930 | 2.210 | 2.510 |
| Limonite..... | $2\text{Fe}_2\text{O}_3 \cdot 3\text{H}_2\text{O}$ in part | 2.170 | 2.290 | 2.310 |
| Goethite..... | $\text{Fe}_2\text{O}_3 \cdot \text{H}_2\text{O}$ | 2.210 | 2.350 | 2.350 (Li) |
| Valentinite..... | Sb_2O_3 | 2.180 | 2.350 | 2.350 |
| Turgite..... | $2\text{Fe}_2\text{O}_3 \cdot \text{H}_2\text{O}$ in part | 2.450 | 2.550 | 2.550 (Li) |
| Realgar..... | As_2S_3 | 2.460 | 2.500 | 2.610 (Li) |
| Terlinguaite..... | Hg_2OCl | 2.350 | 2.640 | 2.670 (Li) |
| Hutchinsonite..... | $(\text{Ti}, \text{Ag})_2\text{S} \cdot \text{PbS} \cdot 2\text{As}_2\text{S}_3$ | 3.078 | 3.176 | 3.188 |
| Stibnite..... | Sb_2S_3 | 3.194 | 4.303 | 4.460 |

TABLES 408 AND 409

INDEX OF REFRACTION

TABLE 408.—Miscellaneous Biaxial Crystals

| Crystal. | Spectrum line. | Index of refraction. | | | Authority. |
|---|-------------------|----------------------|-----------|------------|------------|
| | | n_a | n_β | n_γ | |
| Ammonium oxalate, $(\text{NH}_4)_2\text{C}_2\text{O}_4 \cdot \text{H}_2\text{O}$. . . | D | 1.4381 | 1.5475 | 1.5950 | Brio |
| Ammonium acid tartrate, $(\text{NH}_4)\text{H}(\text{C}_4\text{H}_4\text{O}_6)$. . . | D | 1.5188 | 1.5614 | 1.5910 | T. and C.* |
| Ammonium tartrate, $(\text{NH}_4)_2\text{C}_4\text{H}_4\text{O}_6$. . . | D | — | 1.581 | — | Cloisaux |
| Antipyrin, $\text{C}_{11}\text{H}_{12}\text{N}_2\text{O}$. . . | D | 1.5697 | 1.6935 | 1.7324 | Lieweh |
| Citric acid, $\text{C}_6\text{H}_8\text{O}_7 \cdot \text{H}_2\text{O}$. . . | D | 1.4932 | 1.4977 | 1.5089 | Schrauf |
| Cocain, $\text{C}_8\text{H}_9\text{NO}_3 \cdot \text{H}_2\text{O}$. . . | D | 1.5390 | 1.5435 | — | Grallich |
| Magnesium carbonate, $\text{MgCO}_3 \cdot 3\text{H}_2\text{O}$. . . | D | 1.495 | 1.501 | 1.526 | Genth |
| " sulphate, $\text{MgSO}_4 \cdot 7\text{H}_2\text{O}$. . . | D | 1.432 | 1.455 | 1.461 | Means |
| " " " " " " " " " " " " " " " " | D | 1.4990 | 1.5266 | 1.5326 | Borel |
| Potassium bichromate, $\text{K}_2\text{Cr}_2\text{O}_7$. . . | H, | 1.4307 | 1.4532 | 1.4584 | |
| " chromate, K_2CrO_4 . . . | D | 1.7202 | 1.7380 | 1.8197 | Dufet |
| " " " " " " " " " " " " " " " " | D | — | 1.7254 | — | T. and C. |
| " nitrate, KNO_3 . . . | red | 1.6873 | 1.722 | 1.7305 | Mallard |
| " sulphate, K_2SO_4 . . . | F | 1.3349 | 1.5056 | 1.5661 | Schrauf |
| " " " " " " " " " " " " " " " " | D | 1.4976 | 1.4992 | 1.5029 | T. and C. |
| " " " " " " " " " " " " " " " " | D | 1.4932 | 1.4946 | 1.4980 | " " " |
| " " " " " " " " " " " " " " " " | C | 1.4911 | 1.4928 | 1.4959 | " " " |
| Racemic acid, $\text{C}_8\text{H}_8\text{O}_6 \cdot \text{H}_2\text{O}$. . . | yellow | — | 1.526 | — | Groth |
| Resorcin, $\text{C}_6\text{H}_4\text{O}$. . . | D | — | 1.555 | — | " |
| Sodium bichromate, $\text{Na}_2\text{Cr}_2\text{O}_7 \cdot 2\text{H}_2\text{O}$. . . | D | 1.6610 | 1.6904 | 1.7510 | Dufet |
| " acid tartrate, $\text{NaH}(\text{C}_4\text{H}_4\text{O}_6) \cdot 2\text{H}_2\text{O}$. . . | red | — | 1.5332 | — | Brio |
| Sugar (cane), $\text{C}_{12}\text{H}_{22}\text{O}_{11}$. . . | TI | 1.5422 | 1.5685 | 1.5734 | Calderon |
| " " " " " " " " " " " " " " " " | D | 1.5397 | 1.5667 | 1.5716 | " |
| " " " " " " " " " " " " " " " " | Li | 1.5379 | 1.5639 | 1.5693 | " |
| Tartaric acid, $\text{C}_4\text{H}_4\text{O}_6$ (right-) . . . | D | 1.4953 | 1.5353 | 1.6046 | Means |
| Zinc sulphate, $\text{ZnSO}_4 \cdot 7\text{H}_2\text{O}$. . . | F | 1.4620 | 1.4860 | 1.4897 | T. and C. |
| " " " " " " " " " " " " " " " " | D | 1.4568 | 1.4801 | 1.4836 | " " " |
| " " " " " " " " " " " " " " " " | C | 1.4544 | 1.4776 | 1.4812 | " " " |

* Topsöe and Christiansen.

TABLE 409.—Miscellaneous Liquids (see also Table 410), Liquefied Gases, Oils,
Fats and Waxes

| Substance. | Temp. ° C | Index for D 0.580μ. | Refer- ence. | Substance. | Temp. ° C | Index for D 0.580μ. | Refer- ence. |
|-------------------------------------|--------------|------------------------|-----------------|--------------------|--------------|------------------------|-----------------|
| Liquefied gases: | | | | Oils: | | | |
| Br ₂ | 15 | 1.050 | a | Lavender..... | 20 | 1.464-1.466 | e |
| Cl ₂ | 11 | 1.307 | b | Linseed..... | 15 | 1.4820-1.4852 | e |
| CO ₂ | 15 | 1.195 | b | Maize..... | 15.5 | 1.4757-1.4768 | d |
| C ₂ N ₂ | 18 | 1.325 | b | Mustard seed..... | 15.5 | 1.4750-1.4762 | d |
| C ₂ H ₄ | 6 | 1.130 | b | Neat's foot..... | 15 | 1.4695-1.4708 | e |
| H ₂ S..... | 18.5 | 1.384 | b | Olive..... | 15.5 | 1.4703-1.4718 | d |
| N ₂ | -160 | 1.205 | c | Palm..... | 60 | 1.4510 | d |
| NH ₃ | 16.5 | 1.325 | b | Peanut..... | 15.5 | 1.4723-1.4731 | d |
| NO..... | -90 | 1.330 | c | Peppermint..... | 20 | 1.464-1.468 | e |
| N ₂ O..... | 15 | 1.194 | b | Poppy..... | 15.5 | 1.4770 | d |
| O ₂ | -181 | 1.221 | c | Portpoise..... | 25 | 1.4677 | e |
| SO ₂ | 15. | 1.350 | b | Rape (Colza)..... | 15.5 | 1.4748-1.4752 | d |
| HCl..... | 10.5 | 1.252 | b | Sad..... | 25 | 1.4741 | e |
| HBr..... | 10 | 1.325 | b | Sesame..... | 15.5 | 1.4742 | d |
| HI..... | 10.5 | 1.466 | b | Soja bean..... | 15.5 | 1.4760-1.4775 | e |
| Oils: | | | | Sperm..... | 15.5 | 1.4665-1.4672 | e |
| Almond..... | 15.5 | 1.4728-1.4753 | d | Sunflower..... | 15.5 | 1.4739 | d |
| Castor..... | 15 | 1.4700-1.4803 | e | Tung..... | 10 | 1.593 | e |
| Citronella..... | 20 | 1.47-1.48 | e | Whale..... | 40 | 1.4649 | e |
| Clove..... | 20 | 1.5301-1.5360 | e | Fats and Waxes: | | | |
| Cocconut..... | 15.5 | 1.4587 | d | Beef tallow..... | 40 | 1.4552-1.4587 | e |
| Cod liver..... | 15 | 1.4790-1.4833 | e | Beeswax..... | 75 | 1.4398-1.4451 | e |
| Cotton seed..... | 15.5 | 1.4737-1.4757 | d | Carnauba wax..... | 84 | 1.4520-1.4541 | e |
| Croton..... | 27 | 1.4757-1.4768 | e | Cocoa butter..... | 40 | 1.4560-1.4518 | e |
| Eucalyptus..... | 20 | 1.460-1.467 | e | Lard..... | 40 | 1.4584-1.4601 | e |
| Lard..... | 15.5 | 1.4702-1.4720 | d | Mutton tallow..... | 60 | 1.4510 | e |

References: (a) Martens; (b) Bleekrode, *Pr. Roy. Soc.* 37, 330, 1884; (c) Liveing, *Dewar, Phil. Mag.*, 1802-3; (d) Tolman, *Munson, Bull.* 77, B. of C. Dept. Agriculture, 1005; (e) Seeker, *Van Nostrand's Chemical Annual*. For the oils of reference d, the average temperature coefficient is 0.000365 per ° C.

INDEX OF REFRACTION

Indices of Refraction of Liquids Relative to Air

| Substance. | Density. | Temp. °C | Indices of refraction. | | | | | Author- ity. |
|---|----------|-------------|------------------------|--------------|-------------|-------------|-------------|-----------------|
| | | | 0.397μ H | 0.434μ G' | 0.486μ F | 0.589μ D | 0.656μ C | |
| Acetaldehyde, CH ₃ CHO. | 0.780 | 20 | — | 1.3394 | 1.3350 | 1.3316 | 1.3288 | 1a |
| Acetone, CH ₃ COCH ₃ . | 0.791 | 20 | — | 1.3678 | 1.3639 | 1.3593 | 1.3573 | Means |
| Aniline, C ₆ H ₅ .NH ₂ . | 1.022 | 20 | — | 1.6204 | 1.6041 | 1.5863 | 1.5793 | " |
| Alcohol, methyl, CH ₃ .OH. | 0.794 | 20 | 1.3309 | 1.3362 | 1.3331 | 1.3290 | 1.3277 | rb |
| ethyl C ₂ H ₅ .OH. | 0.808 | 0 | — | 1.3773 | 1.3730 | 1.3695 | 1.3677 | Means |
| " " dn/dt. | 0.800 | 20 | — | 1.3700 | 1.3660 | 1.3618 | 1.3605 | 2 |
| " " " " " " " " | — | 20 | — | —0.0004 | —0.0004 | —0.0004 | —0.0004 | 1 |
| " n-propyl C ₃ H ₇ .OH. | 0.804 | 20 | — | 1.3938 | 1.3901 | 1.3854 | 1.3834 | Means |
| Benzene, C ₆ H ₆ . | 0.880 | 20 | — | 1.5236 | 1.5132 | 1.5012 | 1.4905 | " |
| " C ₆ H ₆ dn/dt. | — | 20 | — | —0.0007 | —0.0006 | —0.0006 | —0.0006 | 3 |
| Bromnaphthalene, C ₁₀ H ₇ Br. | 1.487 | 20 | 1.7289 | 1.7041 | 1.6810 | 1.6582 | 1.6495 | 4 |
| Carbon disulphide, CS ₂ . | 1.293 | 0 | 1.7175 | 1.6920 | 1.6688 | 1.6433 | 1.6330 | rd |
| " " " " " " " " | 1.263 | 20 | 1.6994 | 1.6748 | 1.6523 | 1.6276 | 1.6182 | 1c |
| " tetrachloride, CCl ₄ . | 1.591 | 20 | — | 1.4720 | 1.4676 | 1.4607 | 1.4579 | Means |
| Chinolin, C ₉ H ₇ N. | 1.090 | 20 | — | 1.6670 | 1.6470 | 1.6245 | 1.6161 | 1c |
| Chloral, CCl ₃ .CHO. | 1.512 | 20 | — | 1.4670 | 1.4624 | 1.4557 | 1.4530 | 1c |
| Chloroform, CHCl ₃ . | 1.480 | 20 | 1.463 | 1.458 | 1.4530 | 1.4407 | 1.4443 | Means |
| Decane, C ₁₀ H ₂₂ . | 0.728 | 14.9 | — | 1.4200 | 1.4160 | 1.4108 | 1.4088 | Means |
| Ether, ethyl, C ₂ H ₅ .O.C ₂ H ₅ . | 0.715 | 20 | — | 1.3607 | 1.3576 | 1.3538 | 1.3515 | " |
| " " dn/dt. | — | 20 | — | —0.0006 | —0.0006 | —0.0006 | —0.0006 | 1 |
| Ethyl nitrate, C ₂ H ₅ .O.NO ₃ . | 1.100 | 20 | — | 1.395 | 1.392 | 1.3853 | 1.3830 | 1a |
| Formic acid, H.CO ₂ H. | 1.210 | 20 | — | 1.3804 | 1.3764 | 1.3714 | 1.3693 | 5 |
| Glycerine, C ₃ H ₅ O ₃ . | 1.260 | 20 | — | 1.4828 | 1.4784 | 1.4730 | 1.4706 | 1c |
| Hexane, CH ₃ (CH ₂) ₄ .CH ₃ . | 0.660 | 20 | — | 1.3836 | 1.3799 | 1.3754 | 1.3734 | 1c |
| Hexylene, CH ₃ (CH ₂) ₄ .CH ₂ .CH ₂ . | 0.679 | 23.3 | — | 1.4059 | 1.4007 | 1.3945 | 1.3920 | Means |
| Methylene iodide CH ₂ I ₂ . | 3.318 | 20 | 1.8027 | — | 1.7902 | 1.7417 | 1.7320 | 1f |
| " " dn/dt. | — | 20 | — | — | —0.0007 | —0.0007 | —0.0006 | 1c |
| Naphthalene, C ₁₀ H ₈ . | 0.662 | 98.4 | — | — | 1.6031 | 1.5823 | 1.5746 | 1c |
| Nicotine, C ₁₀ H ₁₄ N ₂ . | 1.012 | 22.4 | — | 1.5430 | — | 1.5239 | 1.5198 | 6 |
| Octane, CH ₃ (CH ₂) ₆ .CH ₃ . | 0.707 | 15.1 | — | 1.4097 | 1.4046 | 1.4007 | 1.3987 | 7 |
| Oil, almond. | 0.92 | 0 | — | — | 1.4847 | 1.4782 | 1.4755 | 8 |
| anise seed. | 0.99 | 15.1 | 1.6084 | — | 1.5743 | 1.5572 | 1.5508 | 5 |
| " " " " " " " " | 0.99 | 21.4 | — | — | 1.5647 | 1.5475 | 1.5410 | 7 |
| bitter almond. | 1.06 | 20 | — | 1.5775 | 1.5623 | — | 1.5391 | 5 |
| cassia. | — | 10 | 1.7039 | — | 1.6389 | 1.6104 | 1.6007 | 7 |
| " " " " " " " " | — | 22.5 | 1.6985 | — | 1.6314 | 1.6026 | 1.5930 | 8 |
| cinnamon. | 1.05 | 23.5 | — | — | 1.6508 | 1.6188 | 1.6077 | 6 |
| olive. | 0.92 | 0 | — | — | 1.4825 | 1.4763 | 1.4738 | 6 |
| rock. | — | 0 | — | — | 1.4644 | 1.4573 | 1.4545 | 9 |
| turpentine. | 0.87 | 10.6 | 1.4939 | — | 1.4817 | 1.4744 | 1.4715 | 8 |
| " " " " " " " " | 0.87 | 20.7 | 1.4913 | — | 1.4793 | 1.4721 | 1.4692 | 1c |
| Pentane, CH ₃ (CH ₂) ₃ .CH ₃ . | 0.625 | 15.7 | — | 1.3645 | 1.3610 | 1.3581 | 1.3570 | 1g |
| Phenol, C ₆ H ₅ .OH. | 1.060 | 40.6 | — | 1.5684 | 1.5558 | 1.5425 | 1.5369 | 1h |
| " " " " " " " " | 1.021 | 82.7 | — | — | 1.5336 | — | 1.5174 | 1h |
| Styrene, C ₆ H ₅ .CH=CH ₂ . | 0.910 | 16.6 | — | 1.5816 | 1.5659 | 1.5485 | 1.5410 | 10 |
| Thymol, C ₁₀ H ₁₄ O. | 0.982 | — | — | — | 1.5386 | — | 1.5228 | Means |
| Toluene, CH ₃ .C ₆ H ₅ . | 0.86 | 20 | — | 1.5170 | 1.5070 | 1.4955 | 1.4911 | " |
| Water, H ₂ O. | — | 20 | 1.3435 | 1.3404 | 1.3372 | 1.3330 | 1.3312 | " |
| " " " " " " " " | — | 0 | 1.3444 | 1.3413 | 1.3380 | 1.3338 | 1.3310 | " |
| " " " " " " " " | — | 40 | 1.3411 | 1.3380 | 1.3340 | 1.3307 | 1.3290 | " |
| " " " " " " " " | — | 80 | 1.3332 | 1.3302 | 1.3270 | 1.3230 | 1.3213 | " |

References: 1, Landolt and Börnstein (a, Landolt; b, Korten; c, Brühl; d, Haagen; e, Landolt, Jahn; f, Nasini, Bernheimer; g, Eisenlohr; h, Eykman; i, Auwers, Eisenlohr); 2, Korten; 3, Walter; 4, Kettler; 5, Landolt; 6, Olds; 7, Baden Powell; 8, Willigen; 9, Fraunhofer; 10, Brühl.

INDEX OF REFRACTION

Indices of Refraction for Solutions of Salts and Acids Relative to Air

| Substance. | Density. | Temp. C. | Indices of refraction for spectrum lines. | | | | | Authority. | | | |
|---|-----------------|--------------------|---|--------------------|--------------------|-------------------------------------|----------------|--------------------|--------------------|--------------------|--------------------|
| | | | C | D | F | H _γ | H | | | | |
| (a) SOLUTIONS IN WATER. | | | | | | | | | | | |
| Ammonium chloride | 1.067 | 27°.05 | 1.37703 | 1.37936 | 1.38473 | — | 1.39336 | Willigen. | | | |
| “ “ | .025 | 29.75 | .34850 | .35050 | .35515 | — | .36243 | “ | | | |
| Calcium chloride | .398 | 25.05 | .44000 | .44279 | .44938 | — | .46001 | “ | | | |
| “ “ | .215 | 22.9 | .39411 | .39652 | .40206 | — | .41078 | “ | | | |
| “ “ | .143 | 25.8 | .37152 | .37369 | .37876 | — | .38666 | “ | | | |
| Hydrochloric acid | 1.166 | 20.75 | 1.40817 | 1.41109 | 1.41774 | — | 1.42816 | “ | | | |
| Nitric acid | .359 | 18.75 | .39893 | .40181 | .40857 | — | .41961 | “ | | | |
| Potash (caustic) . . | .416 | 11.0 | .40052 | .40281 | .40808 | — | .41637 | Fraunhofer. | | | |
| Potassium chloride . | normal solution | | .34087 | .34278 | .34719 | 1.35049 | — | Bender. | | | |
| “ “ | double normal | | .34982 | .35179 | .35645 | .35994 | — | “ | | | |
| “ “ | triple normal | | .35831 | .36029 | .36512 | .36890 | — | “ | | | |
| Soda (caustic) . . . | 1.376 | 21.6 | 1.41071 | 1.41334 | 1.41936 | — | 1.42872 | Willigen | | | |
| Sodium chloride . . | .189 | 18.07 | .37562 | .37789 | .38322 | 1.38746 | — | Schutt. | | | |
| “ “ | .109 | 18.07 | .35751 | .35959 | .36442 | .36823 | — | “ | | | |
| “ “ | .035 | 18.07 | .34000 | .34191 | .34628 | .34969 | — | “ | | | |
| Sodium nitrate . . . | 1.358 | 22.8 | 1.38283 | 1.38535 | 1.39134 | — | 1.40121 | Willigen. | | | |
| Sulphuric acid . . . | .811 | 18.3 | .43444 | .43669 | .44168 | — | .44883 | “ | | | |
| “ “ | .632 | 18.3 | .42227 | .42466 | .42967 | — | .43694 | “ | | | |
| “ “ | .221 | 18.3 | .36793 | .37009 | .37468 | — | .38158 | “ | | | |
| “ “ | .028 | 18.3 | .33663 | .33862 | .34285 | — | .34938 | “ | | | |
| Zinc chloride | 1.359 | 26.6 | 1.39977 | 1.40222 | 1.40797 | — | 1.41738 | “ | | | |
| “ “ | .209 | 26.4 | .37292 | .37515 | .38026 | — | .38845 | “ | | | |
| (b) SOLUTIONS IN ETHYL ALCOHOL. | | | | | | | | | | | |
| Ethyl alcohol | 0.789 | 25.5 | 1.35791 | 1.35971 | 1.36395 | — | 1.37094 | Willigen. | | | |
| “ “ | .932 | 27.6 | .35372 | .35556 | .35986 | — | .36662 | “ | | | |
| Fuchsin (nearly saturated) | — | 16.0 | .3918 | .398 | .361 | — | .3759 | Kundt. | | | |
| Cyanin (saturated) . . | — | 16.0 | .3831 | — | .3705 | — | .3821 | “ | | | |
| NOTE. — Cyanin in chloroform also acts anomalously; for example, Sieben gives for a 4.5 per cent. solution $\mu_A = 1.4593$, $\mu_B = 1.4695$, $\mu_F(\text{green}) = 1.4514$, $\mu_G(\text{blue}) = 1.4554$. For a 9.9 per cent. solution he gives $\mu_A = 1.4902$, $\mu_F(\text{green}) = 1.4497$, $\mu_G(\text{blue}) = 1.4597$. | | | | | | | | | | | |
| (c) SOLUTIONS OF POTASSIUM PERMANGANATE IN WATER.* | | | | | | | | | | | |
| Wave-length in cms. $\times 10^6$. | Spectrum line. | Index for 1 % sol. | Index for 2 % sol. | Index for 3 % sol. | Index for 4 % sol. | Wave-length in cms. $\times 10^6$. | Spectrum line. | Index for 1 % sol. | Index for 2 % sol. | Index for 3 % sol. | Index for 4 % sol. |
| 68.7 | B | 1.3328 | 1.3342 | — | 1.3382 | 51.6 | — | 1.3368 | 1.3385 | — | — |
| 65.6 | C | .3335 | .3348 | 1.3365 | .3391 | 50.0 | — | .3374 | .3383 | 1.3386 | 1.3404 |
| 61.7 | — | .3343 | .3365 | .3381 | .3410 | 48.6 | F | .3377 | — | — | .3408 |
| 59.4 | — | .3354 | .3373 | .3393 | .3426 | 48.0 | — | .3381 | .3395 | .3398 | .3413 |
| 58.9 | D | .3353 | .3372 | — | .3425 | 46.4 | — | .3397 | .3402 | .3414 | .3423 |
| 56.8 | — | .3362 | .3387 | .3412 | .3445 | 44.7 | — | .3407 | .3421 | .3426 | .3439 |
| 55.3 | — | .3366 | .3395 | .3417 | .3438 | 43.4 | — | .3417 | — | — | .3452 |
| 52.7 | E | .3363 | — | — | — | 42.3 | — | .3431 | .3442 | .3457 | .3468 |
| 52.2 | — | .3362 | .3377 | .3388 | — | — | — | — | — | — | — |

* According to Christiansen.

INDEX OF REFRACTION

Indices of Refraction of Gases and Vapors

A formula was given by Biot and Arago expressing the dependence of the index of refraction of a gas on pressure and temperature. More recent experiments confirm their conclusions. The formula is $n_t - 1 = \frac{n_0 - 1}{1 + \alpha t} \frac{p}{p_0}$, where n_t is the index of refraction for temperature t , n_0 for temperature zero, α the coefficient of expansion of the gas with temperature, and p the pressure of the gas in millimeters of mercury. For air see Table 413.

(a) Indices of refraction.

| Spectrum line. | $10^3 (n-1)$ Air. | Spectrum line. | $10^3 (n-1)$ Air. | Wave-length. | $(n-1) \cdot 10^3$. | | | |
|----------------|-------------------|----------------|-------------------|----------------|----------------------|-------|-----------------|-------|
| | | | | | Air. | O. | N. | H. |
| A | .2905 | M | .2903 | μ .4861 | .2951 | .2734 | .3012 | .1406 |
| B | .2911 | N | .3003 | .5461 | .2936 | .2717 | .2998 | .1397 |
| C | .2914 | O | .3015 | .5790 | .2930 | .2710 | — | .1393 |
| D | .2922 | P | .3023 | .6563 | .2910 | .2698 | .2982 | .1387 |
| E | .2933 | Q | .3031 | .4300 | .2971 | .2743 | CO ₂ | .1418 |
| F | .2943 | R | .3043 | .5462 | .2937 | .2704 | .4506 | .1397 |
| G | .2962 | S | .3053 | .6709 | .2918 | .2683 | .4471 | .1385 |
| H | .2978 | T | .3064 | 6.709 | .2881 | .2643 | .4804 | .1361 |
| K | .2980 | U | .3075 | 8.678 | .2888 | .2650 | .4579 | .1361 |
| L | .2987 | | | | | | | |

First 4, Cuthbertsons; the rest, Koch, 1909.

(b) The following are compiled mostly from a table published by Brühl (Zeits. für Phys. Chem. vol. 7, pp. 25-27). The numbers are from the results of experiments by Biot and Arago, Dulong, Jamin, Ketteler, Lorenz, Mascart, Chappius, Rayleigh, and Rivièrè and Prytz. When the number given rests on the authority of one observer the name of that observer is given. The values are for 0° Centigrade and 760 mm pressure.

| Substance. | Kind of light. | Indices of refraction and authority. | Substance. | Kind of light. | Indices of refraction and authority. |
|-----------------|----------------|--------------------------------------|------------------|----------------|--------------------------------------|
| Acetone . . . | D | 1.001079-1.001100 | Hydrogen . . | white | 1.000138-1.000143 |
| Ammonia . . | white | 1.000381-1.000385 | " . . . | D | 1.000132 Burton. |
| " . . . | D | 1.000373-1.000379 | Hydrogen sul- { | D | 1.000644 Dulong. |
| Argon . . . | D | 1.000281 Rayleigh. | phide . . . } | D | 1.000623 Mascart. |
| Benzene . . . | D | 1.001700-1.001823 | Methane . . . | white | 1.000443 Dulong. |
| Bromine . . . | D | 1.001132 Mascart. | " . . . | D | 1.000444 Mascart. |
| Carbon dioxide | white | 1.000449-1.000450 | Methyl alcohol. | D | 1.000549-1.000623 |
| " . . . | D | 1.000448-1.000454 | Methyl ether . | D | 1.000891 Mascart. |
| Carbon disul- { | white | 1.001500 Dulong. | Nitric oxide . . | white | 1.000303 Dulong. |
| phide . . . } | D | 1.001478-1.001485 | " " . . . | D | 1.000297 Mascart. |
| Carbon mon- { | white | 1.000340 Dulong. | Nitrogen . . . | white | 1.000295-1.000300 |
| oxide . . . } | white | 1.000335 Mascart. | " . . . | D | 1.000296-1.000298 |
| Chlorine . . . | white | 1.000772 Dulong. | Nitrous oxide . | white | 1.000503-1.000507 |
| " . . . | D | 1.000773 Mascart. | " " . . . | D | 1.000516 Mascart. |
| Chloroform . . | D | 1.001436-1.001464 | Oxygen . . . | white | 1.000272-1.000280 |
| Cyanogen . . . | white | 1.000834 Dulong. | " . . . | D | 1.000271-1.000272 |
| " . . . | D | 1.000784-1.000825 | Pentane . . . | D | 1.001711 Mascart. |
| Ethyl alcohol . | D | 1.000871-1.000885 | Sulphur dioxide | white | 1.000665 Dulong. |
| Ethyl ether . . | D | 1.001521-1.001544 | " " . . . | D | 1.000686 Ketteler. |
| Helium . . . | D | 1.000036 Ramsay. | Water . . . | white | 1.000261 Jamin. |
| Hydrochloric { | white | 1.000449 Mascart. | " . . . | D | 1.000249-1.000259 |
| acid . . . } | D | 1.000447 " | | | |

INDEX OF REFRACTION

TABLE 413.—Index of Refraction of Air (15°C, 76 cm)

Corrections for reducing wave lengths and frequencies in air (15° C, 76 cm) to vacuo.

The indices were computed from the Cauchy formula $(n-1)10^7 = 2726.43 + 12.288/(\lambda^2 \times 10^{-8}) + 0.3555/(\lambda^4 \times 10^{-16})$. For 0° C and 76 cm the constants of the equation become 2875.66, 13.412 and 0.3777 respectively, and for 30° C and 76 cm, 2580.72, 12.250 and 0.2576. Sellmeier's formula for but one absorption band closely fits the observations: $n^2 = 1 + 0.00057378\lambda^2/(\lambda^2 - 505260)$. If $n-1$ were strictly proportional to the density, then $(n-1)/\rho$ would equal $1 + a/\rho$ where a should be 0.00367. The following values of a were found to hold:

| | | | | | | | |
|-----------|------------|------------|------------|------------|------------|------------|------------|
| λ | 0.85 μ | 0.75 μ | 0.65 μ | 0.55 μ | 0.45 μ | 0.35 μ | 0.25 μ |
| a | 0.003672 | 0.003674 | 0.003678 | 0.003685 | 0.003700 | 0.003738 | 0.003872 |

The indices are for dry air (0.05 \pm % CO₂). Corrections to reduce to dry air the indices for moist air may be made for any wave-length by Lorenz's formula, $+0.00041(m/760)$, where m is the vapor pressure in mm. The corresponding frequencies in waves per cm and the corrections to reduce wave-lengths and frequencies in air at 15° C and 76 cm pressure to vacuo are given. E.g., a light wave of 5000 Angstroms in dry air at 15° C, 76 cm becomes 5001.391 Å in vacuo; a frequency of 20,000 waves per cm correspondingly becomes 19994.44. Meggers and Peters, Bul. Bureau of Standards, 14, p. 731, 1918.

| Wave-length, λ Ang- stroms. | Dry air ($n-1$) $\times 10^7$ 15° C 76 cm | Vacuo correction for λ in air ($n\lambda - \lambda$). Add. | Fre- quency waves per cm $\frac{1}{\lambda}$ in air. | Vacuo correction for $\frac{1}{\lambda}$ in air $(\frac{1}{n\lambda} - \frac{1}{\lambda})$. Subtract. | Wave-length, λ Ang- stroms. | Dry air ($n-1$) $\times 10^7$ 15° C 76 cm | Vacuo correction for λ in air ($n\lambda - \lambda$). Add. | Fre- quency waves per cm $\frac{1}{\lambda}$ in air. | Vacuo correction for $\frac{1}{\lambda}$ in air $(\frac{1}{n\lambda} - \frac{1}{\lambda})$. Subtract. |
|--|---|--|---|--|--|---|--|---|--|
| 2000 | 3256 | 0.651 | 50,000 | 16.27 | 5500 | 2771 | 1.524 | 18,181 | 5.04 |
| 2100 | 3188 | 0.670 | 47,610 | 15.18 | 5600 | 2769 | 1.551 | 17,857 | 4.94 |
| 2200 | 3132 | 0.689 | 45,454 | 14.23 | 5700 | 2768 | 1.578 | 17,543 | 4.85 |
| 2300 | 3086 | 0.710 | 43,478 | 13.41 | 5800 | 2766 | 1.604 | 17,241 | 4.77 |
| 2400 | 3047 | 0.731 | 41,666 | 12.69 | 5900 | 2765 | 1.631 | 16,949 | 4.68 |
| 2500 | 3014 | 0.754 | 40,000 | 12.05 | 6000 | 2763 | 1.658 | 16,666 | 4.60 |
| 2600 | 2986 | 0.776 | 38,461 | 11.48 | 6100 | 2762 | 1.685 | 16,303 | 4.53 |
| 2700 | 2962 | 0.800 | 37,037 | 10.97 | 6200 | 2761 | 1.712 | 16,129 | 4.45 |
| 2800 | 2941 | 0.824 | 35,714 | 10.50 | 6300 | 2760 | 1.739 | 15,873 | 4.38 |
| 2900 | 2923 | 0.848 | 34,482 | 10.08 | 6400 | 2759 | 1.766 | 15,625 | 4.31 |
| 3000 | 2907 | 0.872 | 33,333 | 9.60 | 6500 | 2758 | 1.792 | 15,384 | 4.24 |
| 3100 | 2893 | 0.897 | 32,258 | 9.33 | 6600 | 2757 | 1.810 | 15,151 | 4.18 |
| 3200 | 2880 | 0.922 | 31,250 | 9.00 | 6700 | 2756 | 1.846 | 14,925 | 4.11 |
| 3300 | 2866 | 0.947 | 30,303 | 8.69 | 6800 | 2755 | 1.873 | 14,705 | 4.05 |
| 3400 | 2859 | 0.972 | 29,411 | 8.41 | 6900 | 2754 | 1.900 | 14,492 | 3.99 |
| 3500 | 2850 | 0.998 | 28,571 | 8.14 | 7000 | 2753 | 1.927 | 14,285 | 3.93 |
| 3600 | 2842 | 1.023 | 27,777 | 7.89 | 7100 | 2752 | 1.954 | 14,084 | 3.88 |
| 3700 | 2835 | 1.049 | 27,027 | 7.66 | 7200 | 2751 | 1.981 | 13,888 | 3.82 |
| 3800 | 2829 | 1.075 | 26,315 | 7.44 | 7300 | 2751 | 2.008 | 13,698 | 3.77 |
| 3900 | 2823 | 1.101 | 25,641 | 7.24 | 7400 | 2750 | 2.035 | 13,513 | 3.72 |
| 4000 | 2817 | 1.127 | 25,000 | 7.04 | 7500 | 2749 | 2.062 | 13,333 | 3.66 |
| 4100 | 2812 | 1.153 | 24,300 | 6.86 | 7600 | 2749 | 2.089 | 13,157 | 3.62 |
| 4200 | 2808 | 1.179 | 23,809 | 6.68 | 7700 | 2748 | 2.116 | 12,987 | 3.57 |
| 4300 | 2803 | 1.205 | 23,255 | 6.52 | 7800 | 2748 | 2.143 | 12,820 | 3.52 |
| 4400 | 2799 | 1.232 | 22,727 | 6.36 | 7900 | 2747 | 2.170 | 12,658 | 3.48 |
| 4500 | 2796 | 1.258 | 22,222 | 6.21 | 8000 | 2746 | 2.197 | 12,500 | 3.43 |
| 4600 | 2792 | 1.284 | 21,739 | 6.07 | 8100 | 2746 | 2.224 | 12,345 | 3.39 |
| 4700 | 2789 | 1.311 | 21,276 | 5.93 | | | | | |
| 4800 | 2786 | 1.338 | 20,833 | 5.80 | 8250 | 2745 | 2.265 | 12,121 | 3.33 |
| 4900 | 2784 | 1.364 | 20,406 | 5.68 | 8500 | 2744 | 2.332 | 11,764 | 3.23 |
| | | | | | 8750 | 2743 | 2.400 | 11,428 | 3.13 |
| 5000 | 2781 | 1.391 | 20,000 | 5.56 | 9000 | 2742 | 2.468 | 11,111 | 3.05 |
| 5100 | 2779 | 1.417 | 19,607 | 5.45 | 9250 | 2741 | 2.536 | 10,810 | 2.96 |
| 5200 | 2777 | 1.444 | 19,230 | 5.34 | 9500 | 2740 | 2.604 | 10,526 | 2.88 |
| 5300 | 2775 | 1.471 | 18,867 | 5.23 | 9750 | 2740 | 2.671 | 10,256 | 2.81 |
| 5400 | 2773 | 1.497 | 18,518 | 5.13 | 10000 | 2739 | 2.739 | 10,000 | 2.74 |

MEDIA FOR DETERMINATIONS OF REFRACTIVE INDICES WITH THE MICROSCOPE

TABLE 414.—Liquids, n_D (0.589 μ) = 1.74 to 1.87

In 100 parts of methylene iodide at 20° C the number of parts of the various substances indicated in the following table form saturated solutions having the refractive indices specified. When ready for use the liquids can be mixed to give intermediate refractions. Commercial iodoform (CHI₃) powder is not suitable, but crystals from a solution of the powder in ether may be used, or the crystalized product may be bought. A fragment of tin in the liquids containing the SnI₄ will prevent discoloration.

| CHI ₃ . | SnI ₄ . | AsI ₃ . | SbI ₃ . | S. | n_{Da} at 20°. |
|--------------------|--------------------|--------------------|--------------------|----|------------------|
| | 25 | | 12 | | 1.764 |
| | 25 | | 12 | | 1.783 |
| | 30 | | | 6 | 1.806 |
| | 27 | 13 | 7 | | 1.820 |
| 40 | 27 | 16 | | | 1.826 |
| | 31 | 14 | 8 | 10 | 1.842 |
| 35 | 31 | 16 | 8 | 10 | 1.853 |
| | | | | | 1.868 |

TABLE 415.—Resinlike Substances, n_D (0.589 μ) = 1.68 to 2.10

Piperine, an inexpensive alkaloid, comes in very pure straw-colored crystals. Melted it dissolves the tri-iodides of Sb and As very freely. The solutions are fluid at slightly above 100° and when cold, resinlike. Three parts antimony iodide to one part of arsenic iodide with varying proportions of piperine are easier to manipulate than one containing either iodide alone. In preparing, the constituents, in powder of about 1 mm grain, should be weighed out and then fused *over*, not *in*, a low flame. Three-inch test tubes are suitable.

| Per cent Iodides. | 00. | 10. | 20. | 30. | 40. | 50. | 60. | 70. | 80. |
|---------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Index of refraction | 1.683 | 1.700 | 1.725 | 1.756 | 1.794 | 1.840 | 1.897 | 1.968 | 2.050 |

TABLE 416.—Permanent Standard Resinous Media, n_D (0.589 μ) = 1.546 to 1.682

Any proportions of piperine and rosin form a homogeneous fusion which cools to a transparent resinous mass. On account of the strong dispersion of piperine the refractive indices of minerals apparently matched with those of mixtures rich in this constituent are 0.005 to 0.01 too low. To correct this error a screen made of a thin film of 7 per cent antimony iodide and 93 per cent piperine should be used over the eye-piece. Any amber-colored rosin in lumps is suitable.

| Per cent Rosin. | 00. | 10. | 20. | 30. | 40. | 50. | 60. | 70. | 80. | 90. | 100. |
|---------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Index of refraction | 1.683 | 1.670 | 1.657 | 1.643 | 1.631 | 1.618 | 1.604 | 1.590 | 1.575 | 1.560 | 1.544 |

All taken from Merwin, Journ. Washington Acad. Sci. 3, 35, 1913.

TABLE 417.—Substances, n_D = 1.39 to 1.75

| n | n | n | n |
|------------------|--------------------|--------------------|----------------------------------|
| n-Heptane 1.39 | p-Xylene 1.50 | o-Toluidine 1.57 | α -Chloronaphthalene 1.63 |
| Octylene 1.41 | Chlorobenzene 1.53 | o-Bromophenol 1.58 | α -Bromonaphthalene 1.66 |
| Cyclohexane 1.44 | Eugenol 1.54 | Bromoform 1.59 | α -Iodonaphthalene 1.69 |
| d-Limonene 1.47 | Nitrobenzene 1.55 | Quinaldine 1.61 | Methylene iodide 1.75 |
| | Anethole 1.56 | Iodobenzene 1.62 | |

According to Fresnel, the amount of light reflected by the surface of a transparent medium $= \frac{1}{2} (A + B) = \frac{1}{2} \left\{ \frac{\sin^2(i - r)}{\sin^2(i + r)} + \frac{\tan^2(i - r)}{\tan^2(i + r)} \right\}$; A is the amount polarized in the plane of incidence; B is that polarized perpendicular to this; i and r are the angles of incidence and refraction.

TABLE 418.—Light reflected when $i=0^\circ$ or Incident Light is Normal to Surface $(n-1)^2/(n+1)^2$

| n . | $\frac{1}{2} (A+B)$. | n . | $\frac{1}{2} (A+B)$. | n . | $\frac{1}{2} (A+B)$. | n . | $\frac{1}{2} (A+B)$. |
|-------|-----------------------|-------|-----------------------|-------|-----------------------|----------|-----------------------|
| 1.00 | 0.00 | 1.4 | 2.78 | 2.0 | 11.11 | 5. | 44.44 |
| 1.02 | 0.01 | 1.5 | 4.00 | 2.25 | 14.06 | 5.83 | 50.00 |
| 1.05 | 0.06 | 1.6 | 5.33 | 2.5 | 18.37 | 10. | 66.67 |
| 1.1 | 0.23 | 1.7 | 6.72 | 2.75 | 22.89 | 100. | 96.08 |
| 1.2 | 0.83 | 1.8 | 8.16 | 3. | 25.00 | ∞ | 100.00 |
| 1.3 | 1.70 | 1.9 | 9.63 | 4. | 36.00 | | |

TABLE 419.—Light reflected when n is near Unity or equals $1+dn$

| i . | A . | B . | $\frac{1}{2} (A+B)$. | $\frac{A-B}{A+B}$ * | |
|-----------|----------|----------|-----------------------|---------------------|---|
| 0° | 1.000 | 1.000 | 1.000 | 0.0 | The values for A and B are strictly $(dn^2/4) \sec^4 i$ and $(dn^2/4) (1 - \tan^2 i)$; In columns 2, 3, and 4 $dn^2/4$ is omitted. |
| 5 | 1.015 | .985 | 1.000 | 1.5 | |
| 10 | 1.063 | .939 | 1.001 | 6.2 | |
| 15 | 1.149 | .862 | 1.005 | 14.3 | |
| 20 | 1.282 | .752 | 1.017 | 26.0 | |
| 25 | 1.482 | .612 | 1.047 | 41.5 | |
| 30 | 1.778 | .444 | 1.111 | 60.0 | |
| 35 | 2.221 | .260 | 1.240 | 79.1 | |
| 40 | 2.904 | .088 | 1.496 | 94.5 | |
| 45 | 4.000 | .000 | 2.000 | 100.0 | |
| 50 | 5.857 | .176 | 3.016 | 94.5 | |
| 55 | 9.239 | 1.081 | 5.160 | 79.1 | |
| 60 | 16.000 | 4.000 | 10.000 | 60.0 | |
| 65 | 31.346 | 12.952 | 22.149 | 41.5 | |
| 70 | 73.979 | 42.884 | 57.981 | 26.0 | |
| 75 | 222.85 | 167.16 | 195.00 | 14.3 | |
| 80 | 1099.85 | 971.21 | 1035.53 | 6.2 | |
| 85 | 17330.64 | 16808.08 | 17069.36 | 1.5 | |
| 90 | ∞ | ∞ | ∞ | 0.0 | |

TABLE 420.—Light reflected when $n = 1.55$

| i . | r . | A . | B . | dA .† | dB .† | $\frac{1}{2} (A+B)$. | $\frac{A-B}{A+B}$ * |
|-------|---------|--------|--------|---------|---------|-----------------------|---------------------|
| 0 | 0 | 0.00 | 4.65 | 0.130 | 0.130 | 4.65 | 0.0 |
| 5 | 3 13.4 | 4.70 | 4.61 | .131 | .129 | 4.65 | 1.0 |
| 10 | 6 25.9 | 4.84 | 4.47 | .135 | .126 | 4.66 | 4.0 |
| 15 | 9 36.7 | 5.09 | 4.24 | .141 | .121 | 4.66 | 9.1 |
| 20 | 12 44.8 | 5.45 | 3.92 | .150 | .114 | 4.68 | 16.4 |
| 25 | 15 49.3 | 5.95 | 3.50 | .161 | .105 | 4.73 | 25.9 |
| 30 | 18 49.1 | 6.64 | 3.00 | .175 | .094 | 4.82 | 37.8 |
| 35 | 21 43.1 | 7.55 | 2.40 | .191 | .081 | 4.98 | 51.7 |
| 40 | 24 30.0 | 8.77 | 1.75 | .210 | .066 | 5.26 | 66.7 |
| 45 | 27 8.5 | 10.38 | 1.08 | .233 | .049 | 5.73 | 81.2 |
| 50 | 29 37.1 | 12.54 | 0.46 | .263 | .027 | 6.50 | 92.9 |
| 55 | 31 54.2 | 15.43 | 0.05 | .303 | .007 | 7.74 | 99.3 |
| 60 | 33 58.1 | 19.35 | 0.12 | .342 | -.013 | 9.73 | 98.8 |
| 65 | 35 47.0 | 24.69 | 1.13 | .375 | -.032 | 12.91 | 91.2 |
| 70 | 37 19.1 | 31.99 | 4.00 | .400 | -.050 | 18.00 | 77.7 |
| 75 | 38 52.9 | 42.00 | 10.38 | .410 | -.060 | 26.19 | 61.8 |
| 80 | 39 26.8 | 55.74 | 23.34 | .370 | -.069 | 39.54 | 41.0 |
| 82 30 | 39 45.9 | 64.41 | 34.04 | .320 | -.067 | 49.22 | 30.8 |
| 85 0 | 39 59.6 | 74.52 | 49.03 | .250 | -.061 | 61.77 | 20.6 |
| 86 0 | 40 3.6 | 79.02 | 56.62 | .209 | -.055 | 67.82 | 16.5 |
| 87 0 | 40 6.7 | 83.80 | 65.32 | .163 | -.046 | 74.56 | 12.4 |
| 88 0 | 40 8.9 | 88.88 | 75.31 | .118 | -.036 | 82.10 | 8.3 |
| 89 0 | 40 10.2 | 94.28 | 86.79 | .063 | -.022 | 90.54 | 4.1 |
| 90 0 | 40 10.7 | 100.00 | 100.00 | .000 | -.000 | 100.00 | 0.0 |

Angle of total polarization $= 57^\circ 10'$, $A = 16.99$.

* This column gives the degree of polarization. † Columns 5 and 6 furnish a means of determining A and B for other values of n . They represent the change in these quantities for a change of n of 0.01.

Taken from E. C. Pickering's "Applications of Fresnel's Formula for the Reflection of Light."

OPTICAL CONSTANTS OF METALS

Two constants are required to characterize a metal optically, the refractive index, n , and the absorption index, k , the latter of which has the following significance: the amplitude of a wave after travelling one wave-length, λ^1 measured in the metal, is reduced in the ratio¹ $1 : e^{-2\pi k}$ or for any distance d , $1 : e^{-\frac{2\pi dk}{\lambda^1}}$; for the same wave-length measured in air this ratio becomes $1 : e^{-\frac{2\pi dnk}{\lambda^1}}$. nk is sometimes called the extinction coefficient. Plane polarized light reflected from a polished metal surface is in general elliptically polarized because of the relative change in phase between the two rectangular components vibrating in and perpendicular to the plane of incidence. For a certain angle, ϕ (principal incidence) the change is 90° and if the plane polarized incident beam has a certain azimuth $\bar{\psi}$ (Principal azimuth) circularly polarized light results. Approximately, (Drude, *Annalen der Physik*, 36, p. 546, 1889).

$$k = \tan 2\bar{\psi} (1 - \cot^2 \phi) \text{ and } n = \frac{\sin \phi \tan \phi}{(1 + k^2)^{\frac{1}{2}}} (1 + \frac{1}{2} \cot^2 \phi).$$

For rougher approximations the factor in parentheses may be omitted. R = computed percentage reflection.

(The points have been so selected that a smooth curve drawn through them very closely indicates the characteristics of the metal.)

| Metal. | λ | ϕ | $\bar{\psi}$ | Computed. | | | | Authority. |
|----------|-----------|---------|--------------|-----------|-------|------|-----|--------------|
| | | | | n | k | nk | R | |
| | μ | | | | | | % | |
| Cobalt | 0.231 | 64° 31' | 29° 39' | 1.10 | 1.30 | 1.43 | 32. | Minor. |
| | .275 | 70 22 | 29 59 | 1.41 | 1.52 | 2.14 | 46. | " |
| | .500 | 77 5 | 31 53 | 1.93 | 1.93 | 3.72 | 66. | " |
| | .650 | 79 0 | 31 25 | 2.35 | 1.87 | 4.40 | 69. | Ingersoll. |
| | 1.00 | 81 45 | 29 6 | 3.63 | 1.58 | 5.73 | 73. | " |
| | 1.50 | 83 21 | 26 18 | 5.22 | 1.29 | 6.73 | 75. | " |
| Copper | 2.25 | 83 48 | 26 5 | 5.65 | 1.27 | 7.18 | 76. | " |
| | .231 | 65 57 | 26 14 | 1.39 | 1.05 | 1.45 | 29. | Minor. |
| | .347 | 65 6 | 28 16 | 1.19 | 1.23 | 1.47 | 32. | " |
| | .500 | 70 44 | 33 46 | 1.10 | 2.13 | 2.34 | 56. | " |
| | .650 | 74 16 | 41 30 | 0.44 | 7.4 | 3.26 | 86. | Ingersoll. |
| | .870 | 78 40 | 42 30 | 0.35 | 11.0 | 3.85 | 91. | " |
| | 1.75 | 84 4 | 42 30 | 0.83 | 11.4 | 9.46 | 96. | " |
| | 2.25 | 85 13 | 42 30 | 1.03 | 11.4 | 11.7 | 97. | " |
| | 4.00 | 87 20 | 42 30 | 1.87 | 11.4 | 21.3 | | Först.-Fréd. |
| | 5.50 | 88 00 | 41 50 | 3.16 | 9.0 | 28.4 | | " |
| Gold | 1.00 | 81 45 | 44 00 | 0.24 | 28.0 | 6.7 | | " |
| | 2.00 | 85 30 | 43 56 | 0.47 | 26.7 | 12.5 | | " |
| | 3.00 | 87 05 | 43 50 | 0.80 | 24.5 | 19.6 | | " |
| | 5.00 | 88 15 | 43 25 | 1.81 | 18.1 | 33. | | " |
| | 1.00 | 82 10 | 29 15 | 3.85 | 1.60 | 6.2 | | " |
| Iridium | 2.00 | 83 10 | 29 40 | 4.30 | 1.66 | 7.1 | | " |
| | 3.00 | 81 40 | 30 40 | 3.33 | 1.79 | 6.0 | | " |
| | 5.00 | 79 00 | 32 20 | 2.27 | 2.03 | 4.6 | | " |
| | 0.420 | 72 20 | 31 42 | 1.41 | 1.79 | 2.53 | 54. | Tool. |
| Nickel | 0.589 | 76 1 | 31 41 | 1.79 | 1.86 | 3.33 | 62. | Drude. |
| | 0.750 | 78 45 | 32 6 | 2.19 | 1.99 | 4.36 | 70. | Ingersoll. |
| | 1.00 | 80 33 | 32 2 | 2.63 | 2.00 | 5.26 | 74. | " |
| Platinum | 2.25 | 81 21 | 33 30 | 3.95 | 2.33 | 9.20 | 85. | " |
| | 1.00 | 75 30 | 37 00 | 1.14 | 3.25 | 3.7 | | Först.-Fréd. |
| | 2.00 | 74 30 | 39 50 | 0.70 | 5.06 | 3.5 | | " |
| | 3.00 | 73 50 | 41 00 | 0.52 | 6.52 | 3.4 | | " |
| Silver | 5.00 | 72 00 | 42 10 | 0.34 | 9.01 | 3.1 | | " |
| | 0.226 | 62 41 | 22 16 | 1.41 | 0.75 | 1.11 | 18. | Minor. |
| | .293 | 63 14 | 18 56 | 1.57 | 0.62 | 0.97 | 17. | " |
| | .316 | 52 28 | 15 38 | 1.13 | 0.38 | 0.43 | 4. | " |
| | .332 | 52 1 | 37 2 | 0.41 | 1.61 | 0.65 | 32. | " |
| | .395 | 66 36 | 43 6 | 0.16 | 12.32 | 1.91 | 87. | " |
| | .500 | 72 31 | 43 29 | 0.17 | 17.1 | 2.94 | 93. | " |
| | .589 | 75 35 | 43 47 | 0.18 | 20.6 | 3.64 | 95. | " |
| | .750 | 79 26 | 44 6 | 0.17 | 30.7 | 5.16 | 97. | Ingersoll. |
| | 1.00 | 82 0 | 44 2 | 0.24 | 29.0 | 6.96 | 98. | " |
| Steel | 1.50 | 84 42 | 43 48 | 0.45 | 23.7 | 10.7 | 98. | " |
| | 2.25 | 86 18 | 43 34 | 0.77 | 10.9 | 15.4 | 99. | " |
| | 3.00 | 87 10 | 42 40 | 1.65 | 12.2 | 20.1 | | Först.-Fréd. |
| | 4.50 | 88 20 | 41 10 | 4.49 | 7.42 | 33.3 | | " |
| | 0.226 | 66 51 | 28 17 | 1.30 | 1.26 | 1.64 | 35. | Minor. |
| | .257 | 68 35 | 28 45 | 1.38 | 1.35 | 1.86 | 40. | " |
| | .325 | 69 57 | 30 9 | 1.37 | 1.53 | 2.09 | 45. | " |
| | .500 | 75 47 | 29 2 | 2.09 | 1.50 | 3.14 | 57. | " |
| | .650 | 77 48 | 27 9 | 2.70 | 1.33 | 3.59 | 59. | Ingersoll. |
| | 1.50 | 81 48 | 28 51 | 3.71 | 1.55 | 5.75 | 73. | " |
| | 2.25 | 83 22 | 30 36 | 4.14 | 1.79 | 7.41 | 80. | " |

Drude, *Annalen der Physik und Chemie*, 39, p. 481, 1890; 42, p. 186, 1891; 64, p. 159, 1898. Minor, *Annalen der Physik*, 10, p. 581, 1903. Tool, *Physical Review*, 31, p. 1, 1910. Ingersoll, *Astrophysical Journal*, 32, p. 265, 1910; Försterling and Fredericksz, *Annalen der Physik*, 40, p. 201, 1913.

TABLE 422.—Optical Constants of Metals (Additional Data)

| Metal. | λ . | n. | k. | R. | Ref. | Metal. | λ . | n. | k. | R. | Ref. |
|------------|-------------|------|------|----|------|------------|-------------|------|------|----|------|
| | μ | | | | | | μ | | | | |
| Al.* | 0.589 | 1.44 | 5.32 | 83 | 1 | Rh.* | 0.579 | 1.54 | 4.67 | 78 | 3 |
| Sb.* | .589 | 3.04 | 4.94 | 70 | 1 | Se.† | .400 | 2.94 | 2.31 | 44 | 5 |
| Bi.†† | white | 2.26 | — | — | 2 | | .490 | 3.12 | 1.49 | 35 | 5 |
| Cd.* | .589 | 1.13 | 5.01 | 85 | 1 | | .589 | 2.93 | 0.45 | 25 | 5 |
| Cr.* | .579 | 2.97 | 4.85 | 70 | 3 | | .760 | 2.60 | 0.06 | 20 | 5 |
| Cb.* | .579 | 1.80 | 2.11 | 41 | 3 | Si.* | .589 | 4.18 | 0.09 | 38 | 6 |
| Au.† | .257 | 0.92 | 1.14 | 28 | 4 | | 1.25 | 3.67 | 0.08 | 33 | 6 |
| | .441 | 1.18 | 1.85 | 42 | 4 | | 2.25 | 3.53 | 0.08 | 31 | 6 |
| | .589 | 0.47 | 2.83 | 82 | 4 | Na. (liq.) | .589 | .004 | 2.61 | 99 | 1 |
| I. crys. | .589 | 3.34 | 0.57 | 30 | 4 | Ta.* | .579 | 2.05 | 2.31 | 44 | 3 |
| Ir.* | .579 | 2.13 | 4.87 | 75 | 3 | Sn.* | .589 | 1.48 | 5.25 | 82 | 1 |
| Fe.§ | .257 | 1.01 | 0.88 | 16 | 4 | W.* | .579 | 2.76 | 2.71 | 49 | 3 |
| | .441 | 1.28 | 1.37 | 28 | 4 | V.* | .579 | 3.03 | 3.51 | 58 | 3 |
| | .589 | 1.51 | 1.63 | 33 | 4 | Zn.* | .257 | 0.55 | 0.61 | 20 | 4 |
| Pb.* | .589 | 2.01 | 3.48 | 62 | 1 | | .441 | 0.93 | 3.19 | 73 | 4 |
| Mg.* | .589 | 0.37 | 4.42 | 93 | 1 | | .589 | 1.93 | 4.66 | 74 | 4 |
| Mn.* | .579 | 2.49 | 3.89 | 64 | 3 | | .668 | 2.62 | 5.08 | 73 | 4 |
| Hg. (liq.) | .326 | 0.68 | 2.26 | 66 | 4 | | | | | | |
| | .441 | 1.01 | 3.42 | 74 | 4 | | | | | | |
| | .589 | 1.62 | 4.41 | 75 | 4 | | | | | | |
| | .668 | 1.72 | 4.70 | 77 | 4 | | | | | | |
| Fd.* | .579 | 1.62 | 3.41 | 65 | 3 | | | | | | |
| Pt.† | .257 | 1.17 | 1.65 | 37 | 4 | | | | | | |
| | .441 | 1.94 | 3.16 | 58 | 4 | | | | | | |
| | .589 | 2.63 | 3.54 | 59 | 4 | | | | | | |
| | .668 | 2.91 | 3.66 | 59 | 4 | | | | | | |
| Ni.* | .275 | 1.09 | 1.16 | 24 | 4 | | | | | | |
| | .441 | 1.16 | 1.23 | 25 | 4 | | | | | | |
| | .589 | 1.30 | 1.97 | 43 | 4 | | | | | | |

λ = wave-length, n = refraction index.
k = absorption index, R = reflection.
(1) Drude, see Table 421; (2) Kundt, prism used, Ann. der Physik und Chemie, 34, p. 477, 36, p. 824, 1889; (3) v. Wartenberg, Verh. deutsch. Physik. Ges. 12, p. 105, 1910; (4) Meier, Annales der Physik, 10, p. 581, 1903; (5) Wood, Phil. Mag. (6), 3, 607, 1902; (6) Ingersoll, see Table 421.
* solid, † electrolytic, ‡ prism, § deposited as film in vacuo.

TABLE 423.—Reflecting Power of Metals (See page 379)

| Wave-length | Al. | Sb. | Cd. | Co. | Graphite. | Ir. | Mg. | Mo. | Pd. | Rh. | Si. | Ta. | Te. | Sn. | W. | Va. | Zn. |
|-------------|------------|-----|-----|-----|-----------|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|-----|-----|
| μ | Per cents. | | | | | | | | | | | | | | | | |
| .5 | — | — | — | — | 22 | — | 72 | 46 | — | 76 | 34 | 38 | — | — | 49 | 57 | — |
| .6 | — | 53 | — | — | 24 | — | 73 | 48 | — | 77 | 32 | 45 | 49 | — | 51 | 58 | — |
| .8 | — | 54 | — | — | 25 | — | 74 | 52 | — | 81 | 29 | 64 | 48 | — | 56 | 60 | — |
| 1.0 | 71 | 55 | 72 | 67 | 27 | 78 | 74 | 58 | 72 | 84 | 28 | 78 | 50 | 54 | 62 | 61 | 80 |
| 2.0 | 82 | 60 | 87 | 72 | 35 | 87 | 77 | 82 | 81 | 91 | 28 | 90 | 52 | 61 | 85 | 69 | 92 |
| 4.0 | 92 | 68 | 96 | 81 | 43 | 94 | 84 | 90 | 88 | 92 | 28 | 93 | 57 | 72 | 93 | 79 | 97 |
| 7.0 | 96 | 71 | 98 | 93 | 54 | 95 | 91 | 93 | 94 | 94 | 28 | 94 | 68 | 81 | 95 | 88 | 98 |
| 10.0 | 98 | 72 | 98 | 97 | 59 | 96 | — | 94 | 97 | 95 | 28 | — | — | 84 | 96 | — | 98 |
| 12.0 | 98 | — | 99 | 97 | — | 96 | — | 95 | 97 | — | — | 95 | — | 85 | 96 | — | 99 |

Coblentz, Bulletin Bureau of Standards, 2, p. 457, 1906, 7, p. 197, 1911. The surfaces of some of the samples were not perfect so that the corresponding values have less weight. The methods for polishing the various metals are described in the original articles. The following more recent values are given by Coblentz and Emerson, Bul. Bur. Stds. 14, p. 207, 1917; Stellite, an exceedingly hard and untarnishable alloy of Co, Cr, Mo, Mn, and Fe (C, Si, S, P) was obtained from the Haynes Stellite Co, Kokomo, Indiana.

| | | | | | | | | | | | |
|----------------------|-----|-----|-----|-----|-----|------|------|------|------|------|------|
| Wave-length, μ , | .15 | .20 | .30 | .50 | .75 | 1.00 | 2.00 | 3.00 | 4.00 | 5.00 | 9.00 |
| Tungsten, | — | — | — | .50 | .53 | .576 | .900 | .943 | .948 | .953 | — |
| Stellite, | .32 | .42 | .50 | .64 | .67 | .689 | .747 | .792 | .825 | .848 | .880 |

SMITHSONIAN TABLES.

TABLE 424.—Reflecting Power of Metals

Perpendicular Incidence and Reflection (See also Tables 426-428)

The numbers give the per cents of the incident radiation reflected.

| Wave-length, μ . | Silver-backed Glass. | Mercury-backed Glass. | Mach's Magnesium. $60Al + 31Mg$. | Brandes-Schünnemann Alloy. $32Cu + 34Sn + 29Ni + 5Fe$. | Ross's Speculum Metal. $68.2Cu + 31.8Sn$. | Nickel. <i>Electrolytically Deposited.</i> | Copper. <i>Electrolytically Deposited.</i> | Steel. <i>Untempered.</i> | Copper. <i>Commercially Pure.</i> | Platinum. <i>Electrolytically Deposited.</i> | Gold. <i>Electrolytically Deposited.</i> | Brass. <i>(Trommsdorff).</i> | Silver. <i>Chemically Deposited.</i> |
|----------------------|----------------------|-----------------------|--------------------------------------|--|---|---|---|------------------------------|--------------------------------------|---|---|---------------------------------|---|
| .251 | - | - | 67.0 | 35.8 | 29.9 | 37.8 | - | 32.9 | 25.9 | 33.8 | 38.8 | - | 34.1 |
| .288 | - | - | 70.6 | 37.1 | 37.7 | 42.7 | - | 35.0 | 24.3 | 38.8 | 34.0 | - | 21.2 |
| .305 | - | - | 72.2 | 37.2 | 41.7 | 44.2 | - | 37.2 | 25.3 | 39.8 | 31.8 | - | 9.1 |
| .316 | - | - | - | - | - | - | - | - | - | - | - | - | 4.2 |
| .326 | - | - | 75.5 | 39.3 | - | 45.2 | - | 40.3 | 24.9 | 41.4 | 28.6 | - | 14.6 |
| .338 | - | - | - | - | - | 46.5 | - | - | - | - | - | - | 55.5 |
| .357 | - | - | 81.2 | 43.3 | 51.0 | 48.8 | - | 45.0 | 27.3 | 43.4 | 27.9 | - | 74.5 |
| .385 | - | - | 83.9 | 44.3 | 53.1 | 49.6 | - | 47.8 | 28.6 | 45.4 | 27.1 | - | 81.4 |
| .420 | - | - | 83.3 | 47.2 | 56.4 | 56.6 | - | 51.9 | 32.7 | 51.8 | 29.3 | - | 86.6 |
| .450 | 85.7 | 72.8 | 83.4 | 49.2 | 60.0 | 59.4 | 48.8 | 54.4 | 37.0 | 54.7 | 33.1 | - | 90.5 |
| .500 | 86.6 | 70.9 | 83.3 | 49.3 | 63.2 | 60.8 | 53.3 | 54.8 | 43.7 | 58.4 | 47.0 | - | 91.3 |
| .550 | 88.2 | 71.2 | 82.7 | 48.3 | 64.0 | 62.6 | 59.5 | 54.9 | 47.7 | 61.1 | 74.0 | - | 92.7 |
| .600 | 88.1 | 69.9 | 83.0 | 47.5 | 64.3 | 64.9 | 53.5 | 55.4 | 71.8 | 64.2 | 84.4 | - | 92.6 |
| .650 | 89.1 | 71.5 | 82.7 | 51.5 | 65.4 | 66.6 | 59.0 | 56.4 | 80.0 | 66.5 | 88.9 | - | 94.7 |
| .700 | 89.6 | 72.8 | 83.3 | 54.9 | 66.8 | 68.8 | 90.7 | 57.6 | 83.1 | 69.0 | 92.3 | - | 95.4 |
| .800 | - | - | 84.3 | 63.1 | - | 69.6 | - | 58.0 | 88.6 | 70.3 | 94.9 | - | 96.8 |
| 1.0 | - | - | 84.1 | 69.8 | 70.5 | 72.0 | - | 63.1 | 90.1 | 72.9 | - | - | 97.0 |
| 1.5 | - | - | 85.1 | 79.1 | 75.0 | 78.6 | - | 70.8 | 93.8 | 77.7 | 97.3 | - | 98.2 |
| 2.0 | - | - | 86.7 | 82.3 | 80.4 | 83.5 | - | 76.7 | 95.5 | 80.6 | 96.8 | 91.0 | 97.8 |
| 3.0 | - | - | 87.4 | 85.4 | 86.2 | 88.7 | - | 83.0 | 97.1 | 88.8 | - | 93.7 | 98.1 |
| 4.0 | - | - | 88.7 | 87.1 | 88.5 | 91.1 | - | 87.8 | 97.3 | 91.5 | 96.9 | 95.7 | 98.5 |
| 5.0 | - | - | 89.0 | 87.3 | 89.1 | 94.4 | - | 89.0 | 97.9 | 93.5 | 97.0 | 95.9 | 98.1 |
| 7.0 | - | - | 90.0 | 88.6 | 90.1 | 94.3 | - | 92.9 | 98.3 | 95.5 | 98.3 | 97.0 | 98.5 |
| 9.0 | - | - | 90.6 | 90.3 | 92.2 | 95.6 | - | 92.9 | 98.4 | 95.4 | 98.0 | 97.8 | 98.7 |
| 11.0 | - | - | 90.7 | 90.2 | 92.9 | 95.9 | - | 94.0 | 98.4 | 95.6 | 98.3 | 96.6 | 98.8 |
| 14.0 | - | - | 92.2 | 90.3 | 93.6 | 97.2 | - | 96.0 | 97.9 | 96.4 | 97.9 | - | 98.3 |

Based upon the work of Hagen and Rubens, Ann. der Phys. (1) 352, 1900; (8) 1, 1902; (11) 873, 1905.
Taken partly from Landolt-Börnstein-Meyerhoffer's Physikalisch-chemische Tabellen.

TABLE 425.—Percentage Diffuse Reflection from Miscellaneous Substances

| Wave-length μ | Lamp-blacks. | | | | | Pt. black electrol. | Green leaves. | Lead oxide. | Al. oxide. | Zinc oxide. | White Paper. | Lead carbonate. | Asphalt. | Black velvet. | Black felt. | Red brick. |
|----------------------|--------------|-------|------------------|------------|----------|------------------------|---------------|-------------|------------|-------------|--------------|--------------------|----------|---------------|-------------|------------|
| | Paint. | Rosin | Sperm candle. | Acetylene. | Camphor. | | | | | | | | | | | |
| *.60 | 3.2 | - | - | - | - | - | 25. | 52. | 84. | 82. | - | 89. | 15. | 1.8 | 14. | 30. |
| *.95 | 3.4 | 1.3 | 1.1 | 0.6 | 1.3 | 1.1 | - | - | 88. | 86. | 75. | 93. | - | - | 21. | - |
| 4.4 | 3.2 | 1.3 | .9 | .8 | 1.2 | 1.4 | - | 51. | 21. | 8. | 18. | 29. | - | 3.7 | - | - |
| 8.8 | 3.8 | - | 1.3 | 1.2 | 1.6 | 2.1 | - | 26. | 2. | 3. | 5. | 11. | - | 2.7 | - | 12. |
| 24.0 | 4.4 | 3.0 | 4.0 | 2.1 | 5.7 | 4.2 | - | 10. | 6. | 5. | - | 7. | - | - | - | - |

*Not monochromatic (max.) means from Coblentz, J. Franklin Inst. 1912. Bulletin Bureau of Standards, 9, p. 283, 1912, contains many other materials.

TABLE 426.—Percentage Reflection from Metals, Violet End of Spectrum

(Coblentz, Stair, Bur. Standards Journ. Res., 2, 343, 1929.)

| Wave length in μ | .05 | .10 | .15 | .20 | .25 | .30 | .35 | .40 | .50 | .60 |
|------------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|
| Ni electroplated | .. | .. | .. | .. | 40 | 44 | 51 | 53 | 56 | (60) |
| " vac. fused | .. | .. | .. | .. | 48 | 42 | 45 | 52 | 62 | 64 |
| Ag (min. 7%, 33 μ)..... | .. | .. | .. | .. | 30 | 16 | 71 | 88 | 92 | (94) |
| Stellite (Co, Cr, Mo)..... | .. | .. | .. | .. | 46 | 49 | 55 | 60 | 64 | (68) |
| Stainless steel, 13% Cr.... | .. | .. | .. | .. | 40 | 47 | 52 | 56 | 59 | (60) |
| Cobalt | .. | .. | .. | .. | 43 | 46 | 52 | 58 | 62 | (67) |
| Speculum | .. | .. | .. | .. | 31 | 41 | 50 | 56 | 60 | (62) |
| Beryllium (98.7%) | 46 | 53 | 67 | 79 | 84 | 87 | .. | .. | .. | .. |
| Chromium on steel..... | 69 | 63 | 65 | 71 | 78 | 82 | 86 | 88 | .. | .. |

TABLE 427.—Ultra-violet Reflecting Power of Some Metals

(Coblentz, Stair, Bur. Standards Journ. Res., 4, 189, 1930.)

| | 0.250 μ | .300 | .350 | .400 | .450 | .500 | .550 | .600 |
|---------------------------|-------------|------|------|------|------|------|------|------|
| Aluminum, cast, polished. | .43 | .45 | .54 | .62 | .68 | .72 | .73 | .74 |
| " rolled | .21 | .28 | .34 | .41 | .46 | .50 | .53 | .56 |
| Rhodium | .30 | .37 | .44 | .50 | .53 | .57 | .58 | .59 |
| Tin, polished | .33 | .38 | .45 | .52 | .60 | .67 | .72 | .73 |
| Duralumin | .24 | .31 | .44 | .46 | .46 | .46 | .46 | .46 |
| " tarnished to | .20 | .26 | .32 | | | | | |

TABLE 428.—Infra-red Reflectivity of Tungsten (Temperature Variation)

Three tungsten mirrors were used, — a polished Coolidge X-ray target and two polished flattened wires mounted in evacuated soft-glass bulbs with terminals for heating electrically. Weniger and Pfund, J. Franklin Inst.

| Wave-length in μ . | Absolute reflectivity at room temperature in per cent. | Per cent increase in reflectivity in going from room temperature to | | | |
|------------------------|--|---|----------|----------|----------|
| | | 1377° K. | 1628° K. | 1853° K. | 2056° K. |
| 0.67 | 51 | +6.0 | +7.4 | +8.7 | +9.8 |
| 0.80 | 55 | — | — | — | +8.2 |
| 1.27 | 70 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.00 | 83 | -6.6 | -8.2 | -9.6 | -11.0 |
| 2.00 | 85 | -7.5 | -9.3 | -10.9 | -12.3 |
| 2.00 | 92 | -7.7 | -9.4 | -11.1 | -12.5 |
| 4.00 | 93 | — | — | — | — |

See also Weniger and Pfund, Phys. Rev. 15, p. 427, 1919.

TABLE 429.—Percentage Reflecting Power of Dry Powdered Pigments

Taken from "The Physical Basis of Color Technology," Luckiesh, J. Franklin Inst., 1917. The total reflecting power depends on the distribution of energy in the illuminant and is given in the last three columns for noon sun, blue sky, and for a 7.9 lumens/watt tungsten filament.

| Spectrum color. | Violet. | Blue. | | | Green. | | | Yellow. | | Orange. | | | Red. | | | Noon sun. | Sky light. | Tungsten lamp. |
|-------------------------|---------|-------|------|------|--------|------|------|---------|------|---------|------|------|------|------|----|-----------|------------|----------------|
| Wave-length in μ | 0.44 | 0.46 | 0.48 | 0.50 | 0.52 | 0.54 | 0.56 | 0.58 | 0.60 | 0.62 | 0.64 | 0.66 | 0.68 | 0.70 | | | | |
| American vermilion.... | 8 | 6 | 5 | 5 | 6 | 6 | 9 | 11 | 24 | 39 | 53 | 61 | 66 | 65 | 14 | 12 | 12 | |
| Venetian red..... | 5 | 5 | 5 | 5 | 5 | 6 | 7 | 12 | 10 | 24 | 28 | 30 | 32 | 32 | 11 | 10 | 13 | |
| Tuscan red..... | 7 | 7 | 7 | 8 | 8 | 8 | 8 | 12 | 16 | 18 | 20 | 22 | 23 | 24 | 11 | 10 | 12 | |
| Indian red..... | 8 | 7 | 7 | 7 | 7 | 7 | 7 | 11 | 15 | 18 | 20 | 22 | 23 | 24 | 10 | 9 | 11 | |
| Burnt sienna..... | 4 | 4 | 4 | 4 | 5 | 6 | 9 | 14 | 18 | 20 | 21 | 23 | 24 | 25 | 11 | 9 | 13 | |
| Raw sienna..... | 12 | 13 | 13 | 13 | 18 | 26 | 35 | 43 | 46 | 46 | 45 | 44 | 45 | 43 | 33 | 30 | 37 | |
| Golden ochre..... | 22 | 22 | 23 | 27 | 40 | 53 | 63 | 71 | 75 | 74 | 73 | 73 | 73 | 72 | 58 | 55 | 63 | |
| Chrome yellow ochre... | 8 | 9 | 7 | 7 | 10 | 19 | 30 | 46 | 60 | 62 | 66 | 82 | 83 | 80 | 33 | 29 | 40 | |
| Yellow ochre..... | 20 | 20 | 21 | 24 | 32 | 42 | 53 | 63 | 64 | 61 | 60 | 59 | 59 | 59 | 49 | 46 | 53 | |
| Chrome yellow medium. | 5 | 5 | 6 | 8 | 18 | 48 | 66 | 75 | 78 | 79 | 81 | 81 | 81 | 81 | 54 | 50 | 63 | |
| Chrome yellow light.... | 13 | 13 | 18 | 30 | 56 | 82 | 88 | 89 | 90 | 89 | 88 | 87 | 85 | 84 | 76 | 70 | 82 | |
| Chrome green light.... | 10 | 10 | 14 | 23 | 26 | 23 | 20 | 17 | 14 | 11 | 9 | 8 | 7 | 6 | 10 | 19 | 18 | |
| Chrome green medium.. | 7 | 7 | 10 | 21 | 21 | 17 | 13 | 11 | 9 | 7 | 6 | 6 | 6 | 5 | 14 | 14 | 12 | |
| Cobalt blue..... | 59 | 58 | 49 | 35 | 23 | 15 | 11 | 10 | 10 | 10 | 11 | 15 | 20 | 25 | 16 | 18 | 13 | |
| Ultramarine blue..... | 67 | 54 | 38 | 21 | 10 | 6 | 4 | 3 | 3 | 4 | 5 | 7 | 10 | 17 | 7 | 10 | 6 | |

TABLE 430.—Infra-red Diffuse Percentage Reflecting Powers of Dry Pigments

| Wave-length in μ | Co_2O_3 | CuO | Cr_2O_3 | PbO | Fe_2O_3 | Y_2O_3 | PbCrO_4 | Al_2O_3 | ThO_2 | ZnO | MgO | CaO | ZrO_2 | PbCO_3 | MgCO_3 | White lead paint | Zn oxide paint |
|----------------------|-------------------------|--------------|-------------------------|--------------|-------------------------|------------------------|------------------|-------------------------|----------------|--------------|--------------|--------------|----------------|-----------------|-----------------|------------------|----------------|
| 0.60 * | 3 | — | 27 | 52 | 26 | 74 | 70 | 84 | 86 | 82 | 86 | 85 | 86 | 88 | 85 | 76 | 68 |
| 0.95 * | 4 | 24 | 45 | — | 41 | — | 41 | 88 | — | 86 | — | — | 84 | 93 | 89 | 79 | 72 |
| 4.4 | 14 | 15 | 33 | 51 | 30 | 34 | 21 | 21 | 47 | 8 | 16 | 22 | 23 | 29 | 11 | — | — |
| 8.8 | 13 | — | 33 | 26 | 4 | 11 | 5 | 20 | 7 | 3 | 2 | 4 | 5 | 10 | 4 | — | — |
| 24.0 | 6 | 4 | 8 | 10 | 9 | 10 | 7 | 6 | 10 | 5 | 9 | 6 | 5 | 7 | 9 | — | — |

* Non-monochromatic means from Coblentz, Bul. Bureau Standards 9, p. 283, 1912.

For the REFLECTING (and transmissive) power of ROUGHENED SURFACES at various angles of incidence, see Gorton, Physical Review, 7, p. 66, 1916. A surface of plate glass, ground uniformly with the finest emery and then silvered, used at an angle of 75° , reflected 90 per cent at 4μ , approached 100 for longer waves, only 10 at 1μ , less than 5 in the visible red and approached 0 for shorter waves. Similar results were obtained with a plate of rock salt for transmitted energy when roughened merely by breathing on it. In both cases the finer the surface, the more suddenly it cuts off the short waves.

TABLE 431.—Reflectivity of Snow, Sand, Etc.

(Hulburt, Journ. Opt. Soc. Amer., 17, 23, 1928.)

| | Maine sand * | Fla. sand † | Crushed quartz | Snow | Plaster of paris | White paper | Sodium carbonate ‡ | Sodium chloride | White cotton cloth § |
|-----------------------|--------------|-------------|----------------|------|------------------|-------------|--------------------|-----------------|----------------------|
| 0.3 to 0.4μ | 8 | 15 | 40 | 35 | 40 | 8 | 14 | 38 | 26 |
| 0.4 to 0.8μ | 25 | 40 | 50 | 40 | 53 | 30 | 28 | 49 | 42 |
| 0.8 to 2.6μ | 33 | 50 | 53 | 15 | 60 | 30 | 35 | 54 | 40 |
| 2.6 to 7μ | 31 | 30 | 28 | 18 | 63 | 15 | 18 | 55 | 20 |
| 7μ | 48 | .. | .. | 26 | .. | .. | .. | .. | .. |

* Yellow white grains of many kinds.

† Very white.

‡ Anhydrous.

§ Handkerchief.

TABLE 432.—Reflecting Power of Powders (White Light)

Various pure chemicals, very finely powdered and surface formed by pressing down with glass plate. White (noon sunlight) light. Reflection in per cent. Nutting, Jones, Elliott, Tr. Ill. Eng. Soc. 9, 593, 1914.

| | | | | | |
|------------------------|------|--------------------------|------|----------------------|------|
| Aluminum oxide..... | 83.6 | Magnesium carbonate..... | 86.6 | Sodium chloride..... | 78.1 |
| Barium sulphate..... | 81.1 | " " (block)..... | 97.5 | Sodium sulphate..... | 77.9 |
| Borax..... | 81.6 | Magnesium oxide..... | 85.7 | Starch..... | 80.3 |
| Boric acid..... | 83.2 | Rochelle salt..... | 79.3 | Sugar..... | 87.8 |
| Calcium carbonate..... | 83.8 | Salicylic acid..... | 81.1 | Tartaric acid..... | 79.1 |
| Citric acid..... | 81.5 | Sodium carbonate..... | 81.8 | | |

TABLE 433.—Variation of Reflecting Power of Surfaces with Angle

Illumination at normal incidence, $1\frac{1}{4}$ watt tungsten lamp, reflection at angles indicated with normal. Ill. Eng. Soc., Glare Committee, Tr. Ill. Eng. Soc. 11, p. 92, 1916.

| Angle of observation. | 0° | 1° | 3° | 5° | 10° | 15° | 30° | 45° | 60° |
|--|---------|------|------|------|------|------|------|------|------|
| Magnesium carbonate block..... | 0.88 | — | — | 0.88 | 0.88 | 0.87 | 0.83 | 0.72 | 0.68 |
| Magnesium oxide..... | 0.80 | — | — | 0.80 | 0.80 | 0.80 | 0.77 | 0.75 | 0.66 |
| Matt photographic paper..... | 0.78 | — | — | 0.78 | 0.78 | 0.78 | 0.78 | 0.76 | 0.72 |
| White blotter..... | 0.76 | — | — | 0.76 | 0.76 | 0.76 | 0.73 | 0.70 | 0.67 |
| Pot opal, ground..... | 0.69 | 0.69 | 0.69 | 0.69 | 0.69 | 0.69 | 0.68 | 0.66 | 0.64 |
| Flashed opal, not ground..... | 11.3 | 11.3 | 11.3 | 0.31 | 0.22 | 0.21 | 0.20 | 0.20 | 0.18 |
| Glass, fine ground..... | 0.29 | 0.29 | 0.29 | 0.29 | 0.27 | 0.20 | 0.14 | 0.13 | 0.12 |
| Glass, coarse ground..... | 0.23 | 0.22 | 0.21 | 0.20 | 0.19 | 0.16 | 0.11 | 0.11 | 0.12 |
| Matt varnish on foil..... | 0.83 | — | 0.78 | 0.72 | 0.62 | 0.49 | 0.28 | 0.21 | 0.16 |
| Mirror with ground face..... | 4.9 | — | — | 4.55 | 3.86 | 3.03 | 0.78 | 0.42 | 0.35 |
| The following figures, taken from Fowle, Smithsonian Misc. Col. 58, No. 8, indicate the amount of energy scattered on each side of the directly reflected beam from a silvered mirror; the energy at the center of the reflected beam was taken as 100,000, and the angle of incidence was about 3°. | | | | | | | | | |
| Angle of reflection, 3° ±..... | 0' | 8' | 10' | 15' | 20' | 30' | 45' | 60' | 100' |
| Energy..... | 100,000 | 600 | 244 | 146 | 107 | 66 | 33 | 22 | 11 |
| Wave-length of max. energy of Nernst lamp used as source about 2μ. | | | | | | | | | |

THE REFLECTING POWER OF BUILDING MATERIALS

Filter I (1.78μ), Chance's blue-green contrast filter No. 6, 3.3 mm thick, with their orange contrast filter No. 4, 2.7 mm thick. Filter II (0.84μ), 2 cm water-cell, Chance's orange contrast filter No. 4, and cobalt-blue glass, 1.8 mm thick. Filter III (0.61μ), 1 cm $K_2Cr_2O_7$ sol. (72 g/l) and 1 cm cell $CuSO_4$ sol. (57 g of hydrated salt/l). Filter IV (0.50μ), 2 cm cell $CuSO_4$ sol. sat. at $14.2^\circ C$. Gold film: radiation from "pointalight" through a thin gold film can be used in place of sunlight (compare with computed values). (Beckett, Proc. Phys. Soc., 43, 227, 1931.)

| Description | I (1.78μ) | II (0.84μ) | III (0.61μ) | IV (0.50μ) | Gold film | Com- puted |
|-----------------------------------|--------------------|---------------------|----------------------|---------------------|--------------|---------------|
| Magnesium carbonate..... | 0.63 | 0.99 | 0.98 | 0.96 | 0.96 | |
| CLAY TILES | | | | | | |
| Dutch: light red..... | 0.68 | 0.66 | 0.56 | 0.21 | 0.57 | 0.52 |
| Machine-made: red..... | .72 | .42 | .34 | .11 | .38 | .38 |
| " red..... | .55 | .38 | .31 | .11 | .34 | .33 |
| " lighter red..... | .52 | .40 | .32 | .13 | .34 | .33 |
| " dark purple..... | .22 | .22 | .19 | .13 | .19 | .18 |
| Hand-made: red..... | .60 | .47 | .37 | .12 | .40 | .39 |
| " red-brown..... | .55 | .33 | .28 | .13 | .31 | .31 |
| CONCRETE TILES | | | | | | |
| Uncolored..... | 0.37 | 0.38 | 0.36 | 0.27 | 0.35 | 0.33 |
| Brown..... | .13 | .17 | .15 | .09 | .15 | .13 |
| Brown: very rough..... | .08 | .13 | .13 | .10 | .12 | .11 |
| Black..... | .06 | .09 | .09 | .09 | .09 | .08 |
| SLATES | | | | | | |
| Dark gray: smooth..... | 0.09 | 0.11 | 0.11 | 0.11 | 0.11 | 0.10 |
| " fairly rough..... | .10 | .11 | .10 | .09 | .10 | .10 |
| " rough..... | .09 | .10 | .11 | .11 | .10 | .10 |
| Greenish gray: rough..... | .16 | .11 | .12 | .13 | .12 | .13 |
| Mauve..... | .14 | .16 | .13 | .10 | .14 | .13 |
| Blue-gray..... | .20 | .16 | .13 | .12 | .13 | .15 |
| Silver-gray (Norwegian)..... | .22 | .21 | .21 | .19 | .21 | .20 |
| OTHER ROOFING MATERIALS | | | | | | |
| Asbestos cement: white..... | 0.35 | 0.42 | 0.41 | 0.36 | 0.41 | 0.39 |
| " red..... | .33 | .33 | .29 | .14 | .31 | .26 |
| Enamelled steel: white..... | .35 | .53 | .53 | .57 | .52 | .52 |
| " green..... | .26 | .34 | .17 | .13 | .24 | .25 |
| " red..... | .24 | .26 | .18 | .08 | .19 | .19 |
| " blue..... | .23 | .27 | .17 | .18 | .20 | .23 |
| Galvanized iron: new..... | .58 | .30 | .34 | .34 | .35 | .35 |
| " very dirty..... | .10 | .09 | .09 | .09 | .09 | .09 |
| " whitewashed..... | .63 | .79 | .79 | .76 | .78 | .74 |
| Special roofing sheet: brown..... | .20 | .15 | .12 | .07 | .13 | .13 |
| " green..... | .13 | .20 | .12 | .12 | .14 | .15 |
| Bituminous felt..... | .10 | .12 | .11 | .11 | .12 | .11 |
| Aluminized felt..... | .67 | .60 | .61 | .57 | .62 | .60 |
| Weathered asphalt..... | .12 | .12 | .11 | .09 | .11 | .11 |
| Roofing lead: old..... | .46 | .20 | .19 | .15 | .21 | .23 |
| BRICKS | | | | | | |
| Gault: cream..... | 0.74 | 0.69 | 0.64 | 0.43 | 0.64 | 0.61 |
| Stock: light fawn..... | .56 | .47 | .38 | .19 | .44 | .39 |
| Fletton: light portion..... | .67 | .61 | .57 | .35 | .58 | .52 |
| " dark portion..... | .54 | .46 | .37 | .15 | .41 | .37 |
| Wire cut: red..... | .56 | .48 | .41 | .15 | .44 | .39 |
| Sand-lime: red..... | .41 | .37 | .30 | .11 | .32 | .30 |
| Mottled purple..... | .33 | .26 | .22 | .15 | .23 | .23 |
| Stafford: blue..... | .21 | .12 | .11 | .08 | .11 | .12 |
| Lime-clay (French)..... | .57 | .63 | .52 | .29 | .54 | .49 |

For classification of various light and radiation filters with bibliography, plots, and discussions, see Gibson, Spectral Filters, Journ. Opt. Soc. Amer., 13, 267-280, 1926.

Filters for the reproduction of sunlight and daylight and the determination of color temperatures, see Davis, Gibson, Bur. Standards Misc. Publ. 114, 1931.

TABLE 435.—Light Filters, Narrow Spectrum Regions

(Jones, Journ. Opt. Soc. Amer., 16, 250, 1928. Filters from the following components: Distilled H_2O ; Aq. sol. $CuSO_4 \cdot 5H_2O$; $NiSO_4 \cdot 7H_2O$; Glasses, Corning G 986A, G 586, G 986A; dyed gelatin, Wratten filters 88A, 25, 61, 49.)

| Filter and Absorbent | Concentration thickness | Wave lengths limits | Max. | Transmission at max. |
|-----------------------------------|-------------------------|---------------------|------|----------------------|
| 88A | | .720- 1.400 | ... | .80 |
| 88A, H_2O | 2 cm | .720- 1.380 | .800 | .72 |
| 88A, G 986A | .32 cm | .720- 1.020 | .770 | .35 |
| 25, $CuSO_4 \cdot 5H_2O$ | 5%, 2 cm | .590- .600 | .630 | .26 |
| 61, " | 5%, 2 cm | .490- .600 | .530 | .52 |
| 49, " | 5%, 2 cm | .380- .500 | .460 | .26 |
| G 586, " | .32 cm; 10%, 2 cm | .330- .430 | .380 | .69 |
| G 986, $NiSO_4 \cdot 7H_2O$ | .32 cm; 50%, 1 cm | .260- .360 | .310 | .50 |

TABLE 436.—Absorbing Power of Various Materials—Infra-red.

(Cartwright, Phys. Rev., 35, 415, 1930.)

The absorptive power is an integrated effect over the entire far infra-red. Litharge, powdered glass, white lead, copper sulphide, celestite, and red phosphorus were the best absorbers beyond 50μ . A very thin coat of the absorbing material in most cases was an inefficient absorber of the extreme infra-red waves. A very poor absorbing material in most cases such as copper or platinum will absorb if the surface is sufficiently rough.

For radiometers, the absorbing material is better when mixed with turpentine and alcohol and painted on the vanes. For thermocouples, the absorbing material is better if it is mixed with lacquer. 60-fold sensitiveness and better steadiness comes from evacuation.

The high absorption of glass in the near infra-red suggests its use as a source of radiation. Two Pt wires separated by 4 mm and covered with glass were heated by an electric current; the hot portion of the glass between the wires served as a source of extreme infra-red radiation. A convenient method of filtering out the near infra-red is to grind the windows with emery so that the pits are about 4μ deep. The apparatus may be adjusted with visible light by covering the rough surface with turpentine.

| Substance | Radiation absorbed for | | | Substance | Radiation absorbed for | | |
|--------------------------------------|------------------------|-------------------|-------|---|------------------------|-------------------|-------|
| | $\lambda < 5\mu$ | $\lambda > 50\mu$ | I/V | | $\lambda < 5\mu$ | $\lambda > 50\mu$ | I/V |
| Litharge | 10.8 | 4.3 | .40 | Silver sulphide | 12.8 | 4.4 | .34 |
| Ground glass | 11.9 | 4.7 | .40 | Copper sulphate crystals from solution. | 15.0 | 4.1 | .27 |
| Powdered glass | 11.7 | 5.0 | .43 | Wellsbach mantle material | 8.9 | 3.1 | .35 |
| White lead 2 Pb | | | | Platinum black | 18.2 | 4.4 | .24 |
| $CO_3 \cdot Pb(OH)_2$.. | 14.9 | 4.9 | .33 | Tartaric acid and sugar | 16.0 | 3.9 | .24 |
| White lead in lacquer | 14.3 | 4.4 | .31 | Talc | 12.5 | 3.8 | .30 |
| Red phosphorus | 18.3 | 5.0 | .27 | Water glass | 12.1 | 3.7 | .31 |
| Red phosphorus from a match box..... | 17.7 | 5.1 | .29 | Tellurium, powdered. | 19.2 | 3.3 | .17 |
| Celestite, powdered | | | | India ink | 18.8 | 3.8 | .20 |
| $SrSO_4$ | 14.7 | 4.6 | .31 | Lacquer | 8.6 | 3.0 | .35 |
| Brucite, powdered | | | | Castor oil | 8.8 | 2.8 | .32 |
| $Mg(OH)_2$ | 11.4 | 4.2 | .37 | Glycerine | 11.2 | 3.1 | .28 |
| Anglesite, powdered | | | | Turpentine | 8.1 | 0.2 | .02 |
| $PbSO_4$ | 14.2 | 4.2 | .30 | Clean receiver | 2.9 | 0.2 | .07 |
| Copper sulphide | 17.1 | 5.2 | .30 | | | | |
| Copper oxide | 13.8 | 4.4 | .32 | | | | |

TRANSMISSIBILITY OF RADIATION BY DYES

Percentage transmissions of aqueous solutions taken from The Physical Basis of Color-Technology, Luckiesh, J. Franklin Inst. 184, 1917.

| Spectrum color → | Violet. | | | Blue. | | | Green. | | | Yellow. | | Orange. | | | Red. | | |
|----------------------------|---------|-----|-----|-------|-----|-----|--------|-----|-----|---------|-----|---------|-----|-----|------|--|--|
| Wave-length in μ → | .44 | .46 | .48 | .50 | .52 | .54 | .56 | .58 | .60 | .62 | .64 | .66 | .68 | .70 | | | |
| Carmen ruby opt. | — | — | — | — | — | — | — | — | — | 4 | 18 | 37 | 30 | 60 | | | |
| Amido naphthol red. | — | — | — | — | — | — | — | — | 4 | 38 | 75 | 92 | 96 | 96 | | | |
| Coccine. | — | — | — | — | — | — | — | 4 | 56 | 66 | 68 | 98 | 96 | 98 | | | |
| Erythrosine. | 6 | — | — | — | — | — | 1 | 53 | 90 | 95 | 96 | 96 | 96 | 96 | | | |
| Hematoxyline. | 1 | 3 | 7 | 13 | 14 | 12 | 13 | 25 | 44 | 54 | 63 | 73 | 78 | 82 | | | |
| Alizarinered. | 1 | 1 | 2 | 3 | 4 | 6 | 11 | 22 | 30 | 54 | 65 | 72 | 77 | 79 | | | |
| Acid rosolic (pure). | 4 | 3 | 1 | — | — | — | 2 | 38 | 78 | 88 | 90 | 91 | 92 | 92 | | | |
| Rapid filter red. | — | — | — | — | — | 1 | 10 | 47 | 86 | 95 | 96 | 96 | 96 | 96 | | | |
| Aniline red fast extra A. | — | — | — | — | — | 2 | 12 | 34 | 55 | 72 | 84 | 88 | 90 | 92 | | | |
| Pinatype red fast. | — | — | — | — | — | — | — | — | 11 | 35 | 55 | 65 | 68 | 69 | | | |
| Eosine. | — | — | — | — | — | — | 1 | 54 | 87 | 93 | 92 | 92 | 92 | 92 | | | |
| Rose bengal. | 80 | 70 | 34 | 6 | 1 | — | 14 | 82 | 96 | 97 | 98 | 98 | 98 | 98 | | | |
| Cobalt nitrate. | 69 | 51 | 40 | 31 | 32 | 48 | 07 | 82 | 87 | 90 | 90 | 90 | 90 | 90 | | | |
| Tartrazine. | — | — | — | — | 7 | 52 | 75 | 86 | 91 | 95 | 96 | 97 | 98 | 98 | | | |
| Chrysoidin. | — | — | — | — | — | — | — | — | 2 | 23 | 50 | 71 | 70 | 79 | | | |
| Aurantia. | — | — | — | — | — | 3 | 23 | 53 | 82 | 92 | 96 | 96 | 96 | 96 | | | |
| Aniline yellow phosphine. | — | — | — | 2 | 20 | 43 | 60 | 60 | 67 | 75 | 81 | 85 | 86 | 87 | | | |
| Fluorescein. | 15 | 1 | — | 48 | 91 | 97 | 98 | 98 | 98 | 98 | 98 | 98 | 98 | 98 | | | |
| Aniline yellow fast S. | — | — | 1 | 7 | 43 | 84 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | | | |
| Methyl orange indicator. | — | — | — | — | — | — | 1 | 31 | 70 | 79 | 80 | 81 | 81 | 81 | | | |
| Uranine. | 15 | 1 | — | 1 | 58 | 96 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | | | |
| Uranine naphthaline. | — | — | — | 4 | 53 | 77 | 82 | 83 | 84 | 85 | 86 | 86 | 87 | 87 | | | |
| Orange B naphthol. | — | — | — | — | — | 1 | 43 | 88 | 95 | 96 | 97 | 97 | 97 | 97 | | | |
| Safranin. | — | — | — | — | — | — | — | — | 3 | 27 | 64 | 85 | 93 | 93 | | | |
| Martius gelb. | — | — | — | 1 | 43 | 84 | 91 | 94 | 95 | 95 | 95 | 95 | 95 | 95 | | | |
| Naphthol yellow. | — | — | 1 | 18 | 74 | 91 | 96 | 97 | 98 | 98 | 98 | 98 | 98 | 98 | | | |
| Potassium bichromate, sat. | — | — | — | — | — | 10 | 60 | 84 | 88 | 89 | 89 | 89 | 89 | 88 | | | |
| Cobalt chromate. | 17 | 36 | 62 | 82 | 88 | 90 | 92 | 93 | 95 | 96 | 96 | 96 | 96 | 95 | | | |
| Naphthol green. | 2 | 4 | 7 | 21 | 30 | 36 | 29 | 16 | 7 | 2 | 1 | — | — | — | | | |
| Brilliant green. | 4 | 39 | 60 | 52 | 23 | 4 | — | — | — | — | — | 2 | 23 | 64 | | | |
| Filter blue green. | 35 | 49 | 64 | 70 | 60 | 37 | 13 | 2 | — | — | — | — | — | — | | | |
| Malachite green. | — | 12 | 20 | 8 | 1 | — | — | — | — | — | — | — | — | 12 | 50 | | |
| Sauregrün. | 3 | 29 | 57 | 57 | 39 | 19 | 4 | 1 | — | — | — | — | — | 4 | 30 | | |
| Methylengrün. | 28 | 31 | 32 | 26 | 17 | 7 | 2 | 1 | — | — | — | — | — | 3 | 28 | | |
| Aniline green naphthol B. | 2 | 6 | 14 | 24 | 34 | 40 | 32 | 14 | 4 | 1 | — | — | — | — | | | |
| Neptune green. | — | 40 | 63 | 41 | 13 | 1 | — | — | — | — | — | — | — | 5 | | | |
| Cuprie chloride. | 77 | 84 | 89 | 92 | 92 | 89 | 80 | 67 | 52 | 36 | 19 | 6 | 2 | — | | | |
| Turnbull's blue. | 58 | 60 | 56 | 51 | 38 | 28 | 18 | 9 | 5 | 3 | 1 | — | — | — | | | |
| Victoria blau. | 52 | 23 | 9 | 1 | — | — | — | — | 1 | 4 | 21 | 49 | 73 | — | | | |
| Prussian blue (soluble). | 66 | 71 | 76 | 69 | 60 | 46 | 32 | 20 | 12 | 7 | 5 | 3 | 3 | — | | | |
| Wasser blau. | 80 | 75 | 51 | 26 | 7 | 1 | — | — | 1 | 2 | 6 | 18 | 37 | 60 | | | |
| Resorcin blue. | 25 | 18 | 6 | 2 | 1 | — | — | — | 1 | 2 | 14 | 41 | 64 | 72 | | | |
| Toluidin blau. | 66 | 31 | 13 | 3 | 1 | — | — | — | — | — | 1 | 4 | 16 | 40 | | | |
| Patent blue. | 83 | 91 | 84 | 76 | 65 | 46 | 24 | 8 | 2 | — | — | 6 | 42 | 78 | | | |
| Dianil blue. | 77 | 69 | 59 | 48 | 35 | 24 | 15 | 9 | 5 | 5 | 7 | 14 | 29 | 53 | | | |
| Filter blue. | 84 | 79 | 66 | 44 | 27 | 17 | 14 | 19 | 36 | 56 | 74 | 81 | 88 | 92 | | | |
| Aniline blue, methyl. | 92 | 88 | 78 | 52 | 27 | 9 | 3 | 2 | 2 | 4 | 8 | 16 | 25 | 45 | | | |
| Magenta. | 21 | 8 | 2 | 1 | — | — | 1 | 22 | 73 | 93 | 97 | 97 | 97 | 97 | | | |
| Gentiana violet. | 89 | 83 | 64 | 44 | 26 | 10 | 15 | 10 | 13 | 42 | 75 | 92 | 93 | 94 | | | |
| Rosazeine. | 50 | 28 | 2 | — | — | — | — | 6 | 55 | 90 | 98 | 98 | 98 | 98 | | | |
| Iodine (dense). | — | — | — | — | — | — | — | — | — | — | 1 | 93 | 11 | 23 | | | |
| Rhodamine B. | 81 | 71 | 45 | 13 | 2 | — | — | 23 | 83 | 96 | 96 | 96 | 95 | 94 | | | |
| Acid violet. | 84 | 76 | 68 | 50 | 33 | 26 | 27 | 34 | 40 | 70 | 84 | 96 | 96 | 96 | | | |
| Cyanine in alcohol. | 7 | 1 | — | — | — | — | — | — | — | — | — | 1 | 13 | 23 | | | |
| Xylene red. | 39 | 23 | 1 | — | — | — | — | 1 | 27 | 79 | 97 | 97 | 97 | 96 | | | |
| Methyl violet B. | 25 | 4 | — | — | — | — | — | — | — | — | 3 | 26 | 63 | 89 | | | |

For the infra-red transmission (to 12μ) and reflection powers of a number of aniline dyes, see Johnson and Spence, Phys. Rev. 5, p. 349, 1915.

Scientific Paper 440 of the Bureau of Standards, 1922, gives spectrum transmission curves (0.24 to 1.36μ) for the following dyes: Naphthol Yellow S, Orange 1, Amaranth, Erythrosine, Indigo Disulpho Acid, Ponceau 3R, and Light Green S F Yellowish.

TABLE 438.—Transmissibility of Radiation by Jena Glasses

Coefficients, α , in the formula $I_t = I_0\alpha^t$, where I_0 is the Intensity before, and I_t after, transmission through the thickness t . Deduced from observations by Müller, Vogel, and Rubens as quoted in Hovestadt's Jena Glass (English translation).

| Unit $t=1$ dm. | Coefficient of transmission, α . | | | | | | | | | |
|---|---|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| | .375 μ | 390 μ | 400 μ | 434 μ | 436 μ | 455 μ | 477 μ | 503 μ | 580 μ | 677 μ |
| O 340, Ord. light flint | .388 | .456 | .614 | .569 | .680 | .834 | .880 | .880 | .878 | .939 |
| O 102, H ^v vy silicate flint | — | .025 | .403 | .502 | .566 | .663 | .700 | .782 | .828 | .794 |
| O 93, Ord. " " | — | — | — | — | .714 | .807 | .899 | .871 | .903 | .943 |
| O 203, " " crown | .583 | .583 | .695 | .667 | .806 | .822 | .860 | .872 | .872 | .903 |
| O 598, (Crown) | — | — | — | — | .797 | .770 | .771 | .776 | .818 | .860 |

| Unit $t=1$ cm. | 0.7 μ | 0.95 μ | 1.1 μ | 1.4 μ | 1.7 μ | 2.0 μ | 2.3 μ | 2.5 μ | 2.7 μ | 2.9 μ | 3.1 μ |
|------------------------------|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| | 0.7 μ | 0.95 μ | 1.1 μ | 1.4 μ | 1.7 μ | 2.0 μ | 2.3 μ | 2.5 μ | 2.7 μ | 2.9 μ | 3.1 μ |
| S 204, Borate crown | 1.00 | .99 | .94 | .90 | .85 | .81 | .69 | .43 | .29 | .18 | — |
| S 179, Med. phosp. cr. | — | .98 | .95 | .90 | .84 | .67 | .49 | .87 | .18 | — | — |
| O 1143, Dense, bor. sil. cr. | .98 | — | .97 | — | .95 | .93 | .90 | .84 | .71 | .47 | .27 |
| O 1092, Crown | .99 | .96 | .95 | .99 | .99 | .91 | .82 | .71 | .60 | .48 | .29 |
| O 1151, " " | .98 | — | .99 | .99 | .98 | .94 | .90 | .79 | .75 | .45 | .32 |
| O 451, Light flint | 1.00 | — | .99 | — | .98 | .95 | .92 | .84 | .78 | .54 | .34 |
| O 469, Heavy " " | 1.00 | — | .98 | — | .99 | .98 | .98 | .97 | .90 | .66 | .50 |
| O 500, " " | 1.00 | — | 1.00 | — | 1.00 | — | 1.00 | .99 | .92 | .74 | .53 |
| S 163, " " | 1.00 | — | .98 | — | .99 | — | .99 | — | .94 | .78 | .60 |

TABLE 439.—Transmissibility of Radiation by Jena Colored Glasses

Taken from Catalog 4213, 1931, Schott and Gen, (41 glasses). R is reflection factor yellow light for two surfaces. Values of transmission are for 1 mm thickness. Ordinary figures refer to wave lengths in μ , .281 to .775, black-faced to infra-red.

| Glass durability | Density R | .281 .850 | .302 .950 | .334 1.15 | .366 1.30 | .436 1.60 | .480 2.00 | .546 2.20 | .578 2.40 | .644 2.60 | .700 2.80 | .775 3.00 |
|------------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| U G 1 2/3 | 2.77 .911 | .00 .22 | .17 .11 | .69 .05 | .85 .04 | .00 .03 | .00 .04 | .00 .06 | .00 .11 | .00 .15 | .01 .19 | .34 .17 |
| B G 1 3 | 2.50 .915 | .04 .97 | .40 .93 | .93 .76 | .97 .58 | .86 .40 | .44 .50 | .04 .59 | .05 .69 | .01 .74 | .51 .75 | .94 .55 |
| B G 4 5 | 2.41 .921 | .00 .12 | .00 .11 | .04 .13 | .74 .12 | .87 .14 | .53 .21 | .01 .45 | .01 .59 | .00 .63 | .07 .45 | .13 .40 |
| B G 10 1/2 | 2.60 .916 | .00 .31 | .00 .25 | .14 .26 | .64 .31 | .93 .47 | .95 .55 | .94 .56 | .88 .58 | .75 .55 | .62 .47 | .42 .46 |
| V G 1 2 | 2.93 .905 | .00 .05 | .00 .09 | .00 .18 | .00 .27 | .02 .47 | .47 .65 | .77 .71 | .56 .76 | .12 .77 | .06 .69 | .04 .55 |
| G G 2 3 | 2.58 .916 | .00 1.00 | .00 1.00 | .00 1.00 | .64 1.00 | .99 1.00 | 1.00 .99 | 1.00 .99 | 1.00 .98 | 1.00 .94 | 1.00 .84 | 1.00 .70 |
| G G 4 2 | 2.73 .913 | .00 .99 | .00 .99 | .03 .99 | .01 .99 | .67 .99 | .92 .99 | .97 .99 | .96 .98 | .94 .94 | .96 .85 | .99 .64 |
| G G 11 2 | 2.54 .913 | .00 .97 | .00 .96 | .00 .96 | .00 .99 | .01 .96 | .24 .97 | .99 .97 | .99 .95 | .99 .91 | .99 .82 | .98 .66 |
| R G 2 2 | 2.74 .913 | .00 .98 | .00 .98 | .00 .98 | .00 .98 | .00 .98 | .00 .98 | .00 .97 | .00 .95 | .92 .92 | .98 .81 | .98 .65 |
| R G 5 2 | 2.74 .913 | .00 .98 | .00 .98 | .00 .99 | .00 .99 | .00 .99 | .00 .99 | .00 .98 | .00 .97 | .02 .92 | .96 .79 | .98 .58 |
| N G 5 1 | 2.42 .919 | .00 .61 | .00 .59 | .00 .61 | .29 .65 | .59 .73 | .63 .78 | .66 .78 | .68 .76 | .70 .69 | .70 .58 | .65 .40 |

U G 1 dark purple (u. v., extreme red). B G 1 blue (u. v., extreme red). B G 4 blue (i. r.). B G 10, light blue green, i. r. absorption. V G 1 yellow-green. G G 2 colorless, u. v. absorption. G G 4 almost colorless, strong u. v. absorption. G G 11 dark yellow for contrast filters. R G 2 pure red. R G 5 dark red. N G 5 light neutral.

TABLE 440.—Transmissibility of Radiation by Jena Ultra-violet Glasses

| No. and Type of Glass. | Thickness. | 0.397 μ | 0.383 μ | 0.361 μ | 0.346 μ | 0.325 μ | 0.309 μ | 0.280 μ |
|------------------------|------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| UV 3199 Ultra-violet | 1 mm | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.56 |
| " " | 2 mm | 0.99 | 0.99 | 0.99 | 0.97 | 0.90 | 0.57 | |
| " " | 1 dm | 0.95 | 0.95 | 0.89 | 0.70 | 0.36 | | |
| UV 3248 | 1 mm | 1.00 | 1.00 | 1.00 | 1.00 | 0.98 | 0.91 | 0.35 |
| " " | 2 mm | 0.98 | 0.98 | 0.98 | 0.92 | 0.78 | 0.38 | |
| " " | 1 dm | 0.96 | 0.87 | 0.79 | 0.45 | 0.08 | | |

TABLE 441.—Transmissibility of Radiation by American Glasses

The following data giving the percentage transmission are selected from Coblenz, Emerson and Long, Bull. Bureau Standards, 14, 653, 1918.

| Glass or substance, manufacturer | Thickness, mm. | Wave lengths in μ | | | | | | | | | |
|--|----------------|-----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| | | 0.5 | 1.0 | 1.5 | 2.0 | 2.5 | 3.0 | 3.5 | 4.0 | 4.5 | 5.0 |
| Purple fluorite | 4.98 | — | — | — | 47 | 48 | 48 | 57 | 60 | 62 | 62 |
| Gold film on Crookes' glass | — | 22 | 3 | 2 | 1 | 1 | 1 | 0 | 0 | 0 | 0 |
| " " " crown glass | — | 34 | 8 | 3 | 2 | 1 | 1 | 0 | 0 | 0 | 0 |
| Molybdenite | .007 | 0 | 41 | 43 | 44 | 46 | 46 | 47 | 48 | 48 | 48 |
| Cr ₂ (SO ₄) ₃ ·18 H ₂ O | .24 | 0 | 83 | 63 | 37 | 11 | 0 | 0 | 0 | 0 | 0 |
| Chrome alum, 10 g to 100 g H ₂ O | 10 | — | 73 | 0 | 0 | — | — | — | — | — | — |
| CoCl ₂ , 10 g to 100 g H ₂ O | 10 | — | 50 | 0 | 0 | — | — | — | — | — | — |
| GLASSES: | | | | | | | | | | | |
| Copper ruby, flashed | 1.95 | — | 50 | 64 | 72 | 76 | 40 | 33 | 36 | 7 | 0 |
| G24, Corning, red, No. 243 | 5.90 | — | 60 | 70 | 72 | 65 | 2 | 1 | 0 | 0 | 0 |
| Schott's red, No. 2745 | 3.18 | — | 83 | 89 | 89 | 75 | 10 | 10 | 0 | 0 | 0 |
| G34, Corning, orange, No. 349 | 3.55 | — | 50 | 62 | 67 | 68 | 15 | 3 | 1 | 0 | 0 |
| Pyrex, Corning, No. 774 | 1.55 | 90 | 90 | 90 | 91 | 87 | 35 | 13 | 7 | 2 | 0 |
| Noviol, B, Corning, yellow | 2.88 | 80 | 75 | 60 | 82 | 75 | 23 | 4 | 4 | 0 | 0 |
| Novieweld 3, Corning, dark-yellow | 2.2 | 12 | 1 | 2 | 6 | 13 | 6 | 7 | 7 | 1 | 0 |
| Schott's 43111, green | 3.43 | 50 | 4 | 53 | 79 | 83 | 25 | 9 | 0 | 0 | 0 |
| G1710N, green, Corning | 5.11 | — | 1 | 23 | 53 | 68 | 20 | 9 | 8 | 0 | 0 |
| G174J, Corning, heat absorbing | 2.6 | — | 2 | 4 | 12 | 19 | 11 | 4 | 6 | 0 | 0 |
| G124JA, Corning | 1.5 | 52 | 0 | 1 | 5 | 10 | 3 | 5 | 6 | 0 | 0 |
| Cobalt blue | 2.43 | — | 74 | 43 | 63 | 79 | 36 | 27 | 28 | 0 | 0 |
| Schott's F3086, blue | 2.58 | — | 0 | 1 | 2 | 31 | 11 | 5 | 4 | 0 | 0 |
| G4013, Corning, blue | 6.36 | — | 0 | 15 | 50 | 61 | 11 | 1 | 2 | 0 | 0 |
| G584, Corning, blue, blue-green, No. 428 | 3.70 | — | 0 | 24 | 60 | 75 | 45 | 20 | 20 | 1 | 0 |
| G1711Z, Corning, pale-blue-green | 3.23 | — | 23 | 60 | 74 | 78 | 45 | 13 | 12 | 1 | 0 |
| Amethyst, G172BW ₆ , Corning | 2.11 | 55 | 91 | 91 | 91 | 88 | 42 | 20 | 25 | 7 | 0 |
| G172BW ₅ , Corning, red-purple | 4.43 | — | 0 | 0 | 2 | 5 | 6 | 8 | 12 | 2 | 0 |
| Crookes' A, A. O. Co. | 1.96 | 90 | 92 | 91 | 90 | 83 | 38 | 23 | 27 | 5 | 0 |
| Crookes' sage green 30, A. O. Co. | 1.98 | 50 | 0 | 0 | 4 | 11 | 8 | 8 | 11 | 3 | 0 |
| Lab. 58, A. O. Co. | 2.04 | 72 | 86 | 91 | 91 | 89 | 51 | 35 | 38 | 7 | 0 |
| Fieuzal B, A. O. Co. | 2.04 | 59 | 76 | 80 | 82 | 81 | 30 | 20 | 25 | 2 | 0 |
| Akopos green, J. K. O. Co. | 1.58 | 76 | 91 | 91 | 91 | 90 | 70 | 52 | 51 | 10 | 0 |

Manufacturers: Corning Glass Works, Corning, N. Y.; A. O. Co., American Optical Co., South-bridge, Mass.; J. K. O. Co., Julius King Optical Co., New York City. For other glasses see original reference. See also succeeding table, which contains data for many of the same glasses. For Corning Filters: Journ. Opt. Soc. Amer. 17, 40, 1928; Coblenz, Stair, Bur. Standards, Tech. Pap. 369, 1928; Sci. Pap., 113, 1929. Corning, Heat Transmitting, no. 254, 1 mm. transmits over 30%, 0.8 to 4 μ ; Sextant red, 2 mm. over 30% 0.8 to 4.2 μ ; Red Corex A, G986A, 3 mm., U. V. freely, visible to 0.4 μ , i.r. with max. at 0.7 and 2.6 μ .

TABLE 442.—Transmission of the Radiations from a Gas-filled Tungsten Lamp, the Sun, a Magnetite Arc, and from a Quartz Mercury Vapor Lamp (no Globe) through Various Substances, especially Colored Glasses.

| Color. | Trade name. | Source.* | Thick- ness in mm | Transmission, per cent. | | | |
|-----------------------|--------------------|----------|-------------------------|----------------------------------|------------------------------|-------------------------|--------------------------|
| | | | | Gas- filled tung- sten. | Quartz mercury vapor.† | Magne- tite arc.‡ | Solar radia- tion. |
| Greenish-yellow..... | Fieuzal, B | A. O. C. | 2.04 | 71.6 | 26.9 | 46.0 | 63 |
| " "..... | Fieuzal, 63 | F. H. E. | 1.80 | 75.5 | 34.3 | 55.0 | 72 |
| " "..... | Fieuzal, 64 | F. H. E. | 1.65 | 50.7 | 22.0 | — | — |
| " "..... | Euphos | B. S. | 3.27 | 78.0 | 25.0 | — | — |
| " "..... | Euphos, B | B. & L. | 3.12 | 78.8 | 24.7 | 53.0 | 64 |
| " "..... | Akopos green | J. K. | 1.58 | 84.6 | 20.5 | 50.0 | 74 |
| " "..... | Hallauer, 65 | B. S. | 2.36 | 70.3 | 17.7 | — | — |
| " "..... | Hallauer, 64 | F. H. E. | 1.35 | 58.7 | 25.9 | — | 55 |
| Smoky green..... | G 124, IP | C. G. W. | 2.81 | 0.4 | 0.2 | — | — |
| Yellow-green..... | Noviweid, 30% | C. G. W. | 2.14 | 5.1 | 7.8 | — | 9 |
| " "..... | Noviweid, shade 3 | C. G. W. | 2.20 | 3.4 | 4.2 | 2.7 | — |
| " "..... | Noviweid, shade 4‡ | C. G. W. | 2.20 | 1.6 | 1.2 | 0.8 | — |
| " "..... | Noviweid, shade 6 | C. G. W. | 2.17 | 0.9 | 0.4 | 0.2 | 0.9 |
| " "..... | Noviweid, shade 7 | C. G. W. | 2.17 | 0.8 | 0.2 | — | — |
| Amber..... | Saniweid, dark | J. K. | 3.12 | 51.6 | 15.2 | — | — |
| " "..... | G 34 | C. G. W. | 1.32 | 78.1 | 10.6 | 43.0 | 50 |
| Orange..... | Noviol, shade A | C. G. W. | 3.57 | 56.9 | 17.0 | — | 47 |
| Yellow..... | Noviol, shade B | C. G. W. | 2.00 | — | — | — | 81 |
| " "..... | Noviol, shade C | C. G. W. | 2.88 | 74.1 | 32.2 | 56.0 | 75 |
| " "..... | Noviol, shade C | C. G. W. | 2.00 | — | — | — | 72 |
| Sage green..... | Ferrous No. 30 | A. O. C. | 1.95 | 5.3 | 17.5 | — | 17 |
| Yellow-green..... | No. 61 | A. O. C. | 2.10 | 82.7 | 28.6 | — | 72 |
| Blue-green..... | Lab. No. 59 | A. O. C. | 1.93 | 3.7 | 17.3 | 11.5 | — |
| " "..... | G 124 JA | C. G. W. | 1.53 | 5.3 | 21.5 | 12.5 | 19 |
| Black..... | Smoke, C | B. & L. | 2.26 | 65.3 | 31.2 | 52.0 | 60 |
| " "..... | Smoke, D | B. & L. | 2.45 | 50.9 | 16.0 | 39.0 | 43 |
| Neutral tint..... | Crookes, A | A. O. C. | 1.97 | 85.3 | 46.1 | — | 89 |
| " "..... | Crookes, B | A. O. C. | 2.00 | 75.7 | 32.0 | 64.0 | 69 |
| Gold plate..... | Pfund | A. O. C. | — | 2.6 | 7.2 | 1.2 | 12 |
| " " (darker)..... | Pfund | A. O. C. | — | — | 1.3 | — | — |
| Colorless..... | Lab. No. 58 | A. O. C. | 1.58 | 83.3 | 40.0 | 65 | 83 |
| " "..... | Lab. No. 57 | A. O. C. | 2.00 | — | 51.9 | — | — |
| Amethyst..... | Shade C | A. O. C. | 2.11 | 82.8 | 44.3 | — | 79 |
| Purple..... | Electric smoke | A. O. C. | 1.89 | 36.6 | 2.2 | — | 11 |
| " "..... | G 55 A 62 | C. G. W. | 2.85 | 17.4 | 17.0 | — | 16 |
| Blue..... | Shade D | B. & L. | 2.09 | 37.6 | 20.7 | 39 | — |
| Blue, dark..... | G 53 | C. G. W. | 2.51 | 2.9 | 3.9 | — | — |
| Blue-green..... | G 17r-IZ | C. G. W. | 3.21 | 46.6 | 41.7 | — | — |
| Blue-green, pale..... | G 584 | C. G. W. | 3.75 | 24.9 | 25.2 | — | — |
| Red-purple..... | G 172 BW 5 | C. G. W. | 4.93 | 72.4 | 20.5 | — | — |
| Blue-purple..... | G 585 | C. G. W. | 3.13 | 35.8 | 34.0 | — | 41 |
| Red..... | Selenium | C. G. W. | 2.09 | 67.8 | 7.9 | 43 | 48 |
| " "..... | Schotts | B. S. | 3.22 | 60.4 | — | — | 46 |
| " "..... | Flashed | B. S. | — | — | 4.8 | — | — |
| Colorless..... | Window | B. S. | 1.85 | — | 50.5 | — | 82 |
| " "..... | Crown | B. S. | 1.56 | — | 61.9 | — | 92 |
| Brown..... | Mica | B. S. | 1.30 | — | 35.4 | — | — |
| Colorless..... | Mica | B. S. | 0.99 | — | 43.1 | — | — |
| Clear..... | Water | B. S. | 10.0 | 34.2 | ‡54.0 | — | — |

* A. O. C., Amer. Optical Co., Southbridge, Mass.; C. G. W., Corning Glass Works, Corning, N. Y.; B. & L., Bausch & Lomb, Rochester, N. Y.; J. K., Julius King Optical Co., New York City; F. H. E., F. H. Edmonds, optician, Washington, D. C.; B. S., Bureau of Standards; scrap material, source unknown.

† Infra-red radiation absorbed by quartz cell containing 1 cm layer of water. Taken from Coblenz-Emerson & Long, Bul. Bureau Standards, 14, 653, 1918.

‡ Transmission of 1 cm cell having glass windows.

TABLE 443.—Ultra-violet Transparency (302 mμ)

Bur. Standards Res. Pap. no. 113, 3, 629, 1929, gives data for vitaglass, sunlit, helioglass uviol-Jena, neuglass, Corning Corex-D, quartz, cellophane, tracing cloth. For various fabrics, see Res. Pap. no. 6. For depth of penetration of various wave lengths (u. v., i. r.) see Spectral Characteristics of Light Sources and Window Materials, Trans. Illum. Eng. Soc., 23, 251, 1928. Average per cent transmission of some glasses at 302 mμ when new and after 10 hr. exposure, distance 15 m. to 110 v tungsten u. v. quartz Hg lamp and sun 5 to 12 m. Qualities vary from sample to sample of glasses.

| | Quartz glass | Corex-D | Neuglass | Uviol | Helio | Sunlit | Vitaglass |
|-----------------|--------------|---------|----------|-------|-------|--------|-----------|
| New..... | 92 | 61 | 63 | 67 | 64 | 71 | 58 |
| After lamp..... | 92 | 59 | 50 | 48 | 45 | 41 | 33 |
| After sun..... | 92 | 60 | 57 | 53 | 53 | 51 | 42 |

TABLE 444(a).—Ultra-Violet Transparency Atmospheric Components

$$I = I_0 10^{-\alpha d}, d \text{ in cm } 0^\circ\text{C}, 760 \text{ mm}$$

| Oxygen | Oxygen | Ozone | Ozone |
|--------------------------------|--------------------------------|--------------------|---------------------------------|
| 0.1900 μ $\alpha = 0.0014$ | 0.186 μ $\alpha = 0.0089$ | 0.2378 μ 100.5 | 0.230 μ 50 0.290 μ 16.6 |
| .1920 .0007 | .193 .0015 | .2482 141 | .240 95 .300 4.6 |
| .1929 .0022 | | .2537 148.8 | .250 120 .310 1.23 |
| .1947 .0007 | O ₂ , air, Kreusler | .2652 123 | .260 120 .320 .35 |
| .1950 .0021 | | .2804 45.6 | .270 91 .330 .093 |
| .1955 .00075 | Air | .2967 6.9 | .280 46 .340 .024 |
| .1962 .0020 | 0.186 μ $\alpha = 0.0019$ | .3125 .96 | |
| .1970 .0007 | | .3341 .07 | Fabry, Buisson, 1913 |
| .2000 .00043 | Water | | Nitrogen |
| .2050 .0003 | 0.1875 μ $\alpha = 0.0055$ | Lauchil, 1929 | 0.186 = 0.000478 |
| .2100 .0002 | .1900 .0026 | | Kreusler, 1901 |
| | .1950 .0012 | | |
| | .2000 .0007 | | |
| Granath, Phys. Rev., 1929 | | | |

Air at sea-level (Washington), 400 m practically no absorption $\lambda > .3\mu$; $< .28\mu$ about that due to molecular scattering. Air transmission reduced by 1/100: 22 km at .28 μ ; 5 at 25 μ ; 0.57 at .22 μ ; 20 km at .205 μ . (Dawson, Granath, Hulburt, Phys. Rev., 33, 1073, 1929.)

(b).—Atmospheric Transparency for Ultra-Violet

(Zenith sun, Fabry, Buisson, C. R. 175, 156, 1922; Astrophys. Journ., 54, 297, 1921; joined to Abbot's, Annals Astrophys. Obs. Smithsonian Inst., 2, 112, 1908, via Forsythe-Christison, Gen. Elec. Rev., 662, 1929.)

| | | | | | | | | | | | | |
|--------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Wave length, μ | .29 | .30 | .31 | .32 | .33 | .34 | .35 | .37 | .39 | .41 | .43 | .45 |
| % transmitted..... | 0 | .9 | 9. | 20. | 27. | 33. | 38. | 46. | 51. | 56. | 60. | 64. |

TABLE 445.—Penetration Ultra-Violet Light into Sea Water

(Hulburt, 1928.)

The transparency of sea water declines rapidly with decreasing wave length (λ) in the u. v., becoming quite small below 3000 Å. λ 3400 to 3000 Å, CaSO_4 gives $\frac{1}{2}$ the absorption, H_2O $\frac{1}{4}$; 3000 to 2500 Å, MgCl_2 , CaSO_4 , H_2O each about $\frac{1}{2}$. $I = I_0 10^{-\alpha x}$, x in cm.

| | m μ | 254 | 266 | 280 | 303 | 313 | 366 | 436 | 546 | 578 | 612m μ |
|-----------------|---------|------|------|------|------|------|-------|--------|--------|--------|------------|
| distilled water | a..... | .030 | .021 | .015 | .005 | .002 | .001 | .00005 | .00015 | .00028 | .0010 |
| tap water | "..... | .045 | .032 | .020 | .007 | .003 | .001 | .. | .. | .. | .. |
| sea water | "..... | .067 | .057 | .039 | .017 | .009 | .0013 | .00010 | .00015 | .0003 | .0010 |

TRANSPARENCY OF THE VARIOUS SUBSTANCES OF TABLES 394 TO 402

Alum: Ordinary alum (crystal) absorbs the infra-red.

Metallic reflection at 9.05μ and 30 to 40μ .

Rock-salt: Rubens and Trowbridge (Wied. Ann. 65, 1898) give the following transparencies for a 1 cm. thick plate in %:

| λ | 9 | 10 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20.7 | 23.7 μ |
|-----------|------|------|------|------|------|------|------|------|------|-----|------|------------|
| % | 99.5 | 99.5 | 99.3 | 97.6 | 93.1 | 84.6 | 66.1 | 51.6 | 27.5 | 9.6 | 0.6 | 0. |

Pfänger (Phys. Zt. 5, 1904) gives the following for the ultra-violet, same thickness: 280μ , 95.5%; 231, 86%; 210, 77%; 186, 70%.

Metallic reflection at 0.110 μ , 0.156, 51.2, and 87μ .

Sylvite: Transparency of a 1 cm. thick plate (Trowbridge, Wied. Ann. 60, 1897).

| λ | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20.7 | 23.7 μ |
|-----------|------|------|------|------|------|------|------|------|-----|-----|-----|------|------------|
| % | 100. | 98.8 | 99.0 | 99.5 | 99.5 | 97.5 | 95.4 | 93.6 | 92. | 86. | 76. | 58. | 15. |

Metallic reflection at 0.114 μ , 0.161, 61.1, 100μ .

Fluorite: Very transparent for the ultra-violet nearly to 0.1μ .

Rubens and Trowbridge give the following for a 1 cm. plate (Wied. Ann. 60, 1897):

| λ | 8 μ | 9 | 10 | 11 | 12 μ |
|-----------|---------|------|------|-----|----------|
| % | 84.4 | 54.3 | 16.4 | 1.0 | 0 |

Metallic reflection at 24μ , 31.6, 40μ .

Iceland Spar: Merritt (Wied. Ann. 55, 1895) gives the following values of k in the formula $i = i_0 e^{-kd}$ (d in cm.):

For the ordinary ray:

| λ | 1.02 | 1.45 | 1.72 | 2.07 | 2.11 | 2.30 | 2.44 | 2.53 | 2.60 | 2.65 | 2.74 μ |
|-----------|------|------|------|------|------|------|------|------|------|------|------------|
| k | 0.0 | 0.0 | 0.03 | 0.13 | 0.74 | 1.92 | 3.00 | 1.92 | 1.21 | 1.74 | 2.36 |

| λ | 2.83 | 2.90 | 2.95 | 3.04 | 3.30 | 3.47 | 3.62 | 3.80 | 3.98 | 4.35 | 4.52 | 4.83 μ |
|-----------|------|------|------|------|------|------|------|------|----------|------|------|------------|
| k | 1.32 | 0.70 | 1.80 | 4.71 | 22.7 | 19.4 | 9.6 | 18.6 | ∞ | 6.6 | 14.3 | 6.1 |

For the extraordinary ray:

| λ | 2.49 | 2.87 | 3.00 | 3.28 | 3.38 | 3.59 | 3.76 | 3.90 | 4.02 | 4.41 | 4.67 μ |
|-----------|------|------|------|------|------|------|------|------|------|------|------------|
| k | 0.14 | 0.08 | 0.43 | 1.32 | 0.89 | 1.79 | 2.04 | 1.17 | 0.89 | 1.07 | 2.40 |

| λ | 4.91 | 5.04 | 5.34 | 5.50 μ |
|-----------|------|------|------|------------|
| k | 1.25 | 2.13 | 4.41 | 12.8 |

Quartz: Very transparent to the ultra-violet; Pfänger gets the following transmission values for a plate 1 cm. thick: at 0.222μ , 94.2%; 0.214, 92; 0.203, 83.6; 0.186, 67.2%.

Merritt (Wied. Ann. 55, 1895) gives the following values for k (see formula under Iceland Spar):

For the ordinary ray:

| λ | 2.72 | 2.83 | 2.95 | 3.07 | 3.17 | 3.38 | 3.67 | 3.82 | 3.96 | 4.12 | 4.50 μ |
|-----------|------|------|------|------|------|------|------|------|------|------|------------|
| k | 0.20 | 0.47 | 0.57 | 0.31 | 0.20 | 0.15 | 1.26 | 1.61 | 2.04 | 3.41 | 7.30 |

For the extraordinary ray:

| λ | 2.74 | 2.89 | 3.00 | 3.08 | 3.26 | 3.43 | 3.52 | 3.59 | 3.64 | 3.74 | 3.91 | 4.19 | 4.36 μ |
|-----------|------|------|------|------|------|------|------|------|------|------|------|------|------------|
| k | 0.0 | 0.11 | 0.33 | 0.26 | 0.11 | 0.51 | 0.76 | 1.88 | 1.83 | 1.62 | 2.22 | 3.35 | 8.0 |

For $\lambda > 7\mu$, becomes opaque, metallic reflection at 8.50μ , 9.02, 20.75-24.4 μ , then transparent again.

The above are taken from Kayser's "Handbuch der Spectroscopie," vol. iii.

TABLE 447.—Color Screens

The following light-filters are quoted from Landolt's "Das optische Drehungsvermögen, etc." 1898. Although only the potassium salt does not keep well it is perhaps safer to use freshly prepared solutions.

| Color. | Thick- ness. mm. | Water solutions of | Grammes of substance in 100 c.cm. | Optical cen- tre of band. μ | Transmission. |
|--------|------------------------|--|---|---------------------------------------|---|
| Red | 20 | Crystal-violet, 5BO | 0.005 | 0.6659 | { begins about 0.718 μ . ends sharp at 0.639 μ . |
| " | 20 | Potassium monochromate | 10. | | |
| Yellow | 20 | Nickel-sulphate, NiSO ₄ .7aq. | 30. | 0.5919 | 0.614-0.574 μ . |
| " | 15 | Potassium monochromate | 10. | | |
| " | 15 | Potassium permanganate | 0.025 | | |
| Green | 20 | Copper chloride, CuCl ₂ .2aq. | 60. | 0.5330 | 0.540-0.505 μ |
| " | 20 | Potassium monochromate | 10. | | |
| Bright | 20 | Double-green, SF | 0.02 | 0.4885 | { 0.526-0.494 and 0.494-0.458 μ |
| blue | 20 | Copper-sulphate, CuSO ₄ .5aq. | 15. | | |
| Dark | 20 | Crystal-violet, 5BO | 0.005 | 0.4482 | 0.478-0.410 μ |
| blue | 20 | Copper sulphate, CuSO ₄ .5aq. | 15. | | |

TABLE 448.—Color Screens

The following list is condensed from Wood's Physical Optics :

Methyl violet, 4R (Berlin Anilin Fabrik) very dilute, and nitroso-dimethyl-aniline transmits 0.365 μ .

Methyl violet + chinin-sulphate (separate solutions), the violet solution made strong enough to blot out 0.4359 μ , transmits 0.4047 and 0.4048, also faintly 0.3984.

Cobalt glass + aesculin solution transmits 0.4359 μ .

Guinea green B extra (Berlin) + chinin sulphate transmits 0.4916 μ .

Neptune green (Bayer, Elberfeld) + chrysoidine. Dilute the latter enough to just transmit 0.579 μ and 0.5461; then add the Neptune green until the yellow lines disappear.

Chrysoidine + eosine transmits 0.5790 μ . The former should be dilute and the eosine added until the green line disappears.

Silver chemically deposited on a quartz plate is practically opaque except to the ultra-violet region 0.3160-0.3260 where 90% of the energy passes through. The film should be of such thickness that a window backed by a brilliantly lighted sky is barely visible.

In the following those marked with a * are transparent to a more or less degree to the ultra-violet.

* Cobalt chloride: solution in water, — absorbs 0.50-0.53 μ ; addition of CaCl₂ widens the band to 0.47-0.50. It is exceedingly transparent to the ultra-violet down to 0.20. If dissolved in methyl alcohol + water, absorbs 0.50-0.53 and everything below 0.35. In methyl alcohol alone 0.485-0.555 and below 0.40 μ .

Copper chloride: in ethyl alcohol absorbs above 0.585 and below 0.535; in alcohol + 50% water, above 0.595 and below 0.37 μ .

Neodymium salts are useful combined with other media, sharpening the edges of the absorption bands. In solution with bichromate of potash, transmits 0.535-0.565 and above 0.60 μ , the bands very sharp (a useful screen for photographing with a visually corrected objective).

Praseodymium salts: three strong bands at 0.482, .468, .444. In strong solutions they fuse into a sharp band at 0.435-0.485 μ . Absorption below 0.34.

Picric acid absorbs 0.36-0.42 μ , depending on the concentration.

Potassium chromate absorbs 0.40-0.35, 0.30-0.24, transmits 0.23 μ .

* Potassium permanganate: absorbs 0.555-0.50, transmits all the ultra-violet.

Chromium chloride: absorbs above 0.57, between 0.50 and .39, and below 0.33 μ . These limits vary with the concentration.

Aesculin: absorbs below 0.363 μ , very useful for removing the ultra-violet.

* Nitroso-dimethyl-aniline: very dilute aqueous solution absorbs 0.49-0.37 and transmits all the ultra-violet.

Very dense cobalt glass + dense ruby glass or a strong potassium bichromate solution cuts off everything below 0.70 and transmits freely the red.

Iodine: saturated solution in CS₂ is opaque to the visible and transparent to the infra-red.

INFRA-RED TRANSMISSION AND ABSORPTION

TABLE 452.—Per Cent Transmission, Gases, 6.7 to 32.8 μ

(Strong, Phys. Rev., 37, 1565, 1931, restrahlung.)

Length of cell, 4 inches.

| Material | Pressure | 6.7 μ | 8.7 μ | 20.75 μ | 22.9 μ | 27.3 μ | 29.4 μ | 32.8 μ |
|--|----------|-----------|-----------|-------------|------------|------------|------------|------------|
| NH ₃ | 760mm | 24 | 26 | 79 | 93 | 83 | 82 | 62 |
| C ₂ H ₂ | 760 | 95 | 92 | 99 | 101 | 101 | 100 | 98 |
| H ₂ S..... | 760 | 97 | 98 | 98 | 97 | 92 | 90 | 83 |
| SO ₂ | 760 | 98 | 5 | 7 | 58 | 100 | 100 | 96 |
| C ₆ H ₆ | 96 | 65 | 97 | 102 | 99 | 100 | 98 | 95 |
| CCl ₄ | 114 | 95 | 99 | 97 | 99 | 99 | 99 | 91 |
| CS ₂ | 361 | 30 | 98 | 100 | 86 | 98 | 99 | 96 |
| CHCl ₃ | 200 | 93 | 90 | 99 | 98 | 98 | 97 | 97 |
| (C ₂ H ₅) ₂ O..... | 526 | 17 | 6 | 61 | 45 | 69 | 71 | 61 |

TABLE 453.—Per Cent Transmission, Solids, 6.7 to 32.8 μ

| Material | Description | 6.7 μ | 8.7 μ | 20.75 μ | 22.9 μ | 27.3 μ | 29.4 μ | 32.8 μ |
|-----------------|-----------------------------------|-----------|-----------|-------------|------------|------------|------------|------------|
| Lacquer film | $\pm .55\mu$ thickness | 96 | 93 | 97 | 98 | 99 | 99 | 100 |
| Mica | 10 μ thickness | 83 | 22 | 19 | 00 | 35 | 42 | 44 |
| Soot on lacquer | Opaque to visible | 25 | 22 | 67 | 53 | 60 | 67 | 60 |
| Quartz, fused | 10 μ thickness | 86 | 02 | 01 | 03 | 51 | 55 | 68 |
| Glass | 3 μ thickness | 93 | 07 | 12 | 14 | 48 | 51 | 56 |
| Cellophane | 25 μ thickness | 33 | 04 | 04 | 01 | 20 | 25 | 26 |
| MgO | Deposit from burning Mg ribbon | 88 | 86 | 04 | 02 | 90 | 93 | 87 |
| ZnO | Deposit from Zn arc | 99 | 80 | 15 | 05 | 93 | 79 | 80 |

TABLE 454.—Per Cent Reflection, Solids, 22.9 and 32.8 μ

| Description of reflector | 22.9 μ | 32.8 μ |
|--|--------------------|------------|
| Deposit of MgO from burning Mg ribbon..... | 0 | 0 |
| Reflection β -MgO..... | 80 | 33 |
| Mica..... | 32 | .. |
| Paraffin..... | 04 | .. |
| Pencil mark on paper..... | 09 | .. |
| Silver covered with | Soot coating..... | 43 |
| | MgO coating..... | 48 |
| | ZnO coating..... | 08 |
| | Optical black..... | 01 |
| Gold foil blackened with bismuth..... | 31 | .. |
| KBr + 1.5 μ CaF ₂ deposited by evaporation..... | > 19 | .. |
| KI + 1.5 μ CaF ₂ deposited by evaporation..... | 10 | .. |
| | 13 | .. |

TABLE 455.—Per Cent Transmission, Various Substances, 20 to 130 μ

(Barnes, Phys. Rev., 39, 562, 1932, which see for special technique used for analysis in this region.)

| | | 20 μ | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 | 120 | 130 μ |
|-------------------|----------|----------|-----|-----|----|----|----|----|----|-----|-----|------|-----------|
| Fused quartz.... | 0.2 mm | 0 | 0 | 2 | 20 | 35 | 51 | 53 | 52 | .. | .. | .. | .. |
| "..... | 1.0 " | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 6 | 18 | 30 | 22 | 27 |
| Crystal " | 1.0 " | 0 | 1 | 7 | 42 | 57 | 62 | 59 | 72 | 71 | 78 | 70 | 72 |
| Sulphur, rhombic | 0.9 " | 30 | 40 | 10 | 6 | 39 | 37 | 52 | 58 | 51 | 56 | 58 | 38 |
| Paraffin..... | 2.0 " | 19 | 35 | 42 | 51 | 58 | 64 | 65 | 75 | 85 | 79 | 76 | 70 |
| Mica..... | 6 μ | 6 | 18 | 50 | 53 | 46 | 57 | 50 | 21 | 27 | 50 | (55) | (55) |
| Cellophane..... | 40 μ | 0 | 16 | 22 | 23 | 24 | 24 | 23 | 29 | 30 | 30 | 42 | 42 |
| Celluloid..... | 1 μ | 92 | 93 | 95 | 96 | 96 | 97 | 97 | 98 | 98 | 99 | 99 | 99 |
| Black paper..... | 0.1 mm | .. | .. | .. | 2 | 5 | 13 | 19 | 22 | 23 | 26 | 28 | 30 |
| Camphor soot..... | * | 60 | 76 | 79 | 80 | 81 | 82 | 84 | 85 | 86 | 87 | 89 | 90 |
| Pfund Bi black.. | * | 30 | 40 | 44 | 48 | 50 | 40 | 45 | 58 | 60 | 57 | 60 | 63 |
| Lampblack, | | | | | | | | | | | | | |
| water glass.... | 0.8† | 0 | (1) | (3) | 7 | 12 | 21 | 20 | 26 | 30 | 25 | 30 | 30 |

* On celluloid 1 μ thick. † For Rubens, Hoffmann, lampblack-water-glass mixture see Berliner Ber. 424, 1922. For Pfund's Bi Black see Rev. Sci. Instr., 1, 397, 1930. A considerable number of bands appear in some of the curves from which the above values were read.

FAR INFRA-RED, 20 TO 150 μ

(John Strong, Phys. Rev., 38, 1818, 1931.)

TABLE 456.—Restrahlung bands

| Number of reflections | Crystal mirrors | Filter (3 mm paraffin in each case) | Wave length in μ | Frequency in \sim /cm |
|-----------------------|-----------------|---|-------------------------|----------------------------|
| 4 | Quartz | 1 cm KCl | 20.7 | 483 |
| 3 | Fluorite | 5 mm KCl | 23 | 435 |
| 1 | Metal | | | |
| 2 | Fluorite | 3 mm KBr | 27.3 | 366 |
| 4 | Calcite | | 29.4 | 340 |
| 3 | Fluorite | 0.4 mm quartz | 32.8 | 305 |
| 1 | Metal | 1.2 mm KBr | | |
| 3 | Aragonite | 0.4 mm quartz | 41 * † | 244 |
| 1 | Metal | | | |
| 4 | NaCl | 2 mm quartz | 52 | 192 |
| 4 | KCl | " | 63 | 159 |
| 4 | KBr | " | 83 | 120 |
| 4 | KI | " | 94 | 106 |
| 4 | TlBr | " | 117 | 85 |
| 4 | TlI | " | 152 | 66 |

* The use of a paraffin window about 3 mm thick stops the short wave length restrahlung of quartz at 8.7 μ and of calcite at 6.7 μ .

† Weak reflection at 41 μ .

TABLE 457.—Reflecting Power

| | $\lambda = 20\mu$ \sim /cm = 500 | 25 400 | 33 $\frac{1}{3}$ 300 | 50 200 | 66 $\frac{2}{3}$ 150 | 100 100 | 150 μ 66 $\frac{2}{3}$ | |
|------------------------------|---------------------------------------|-----------|-------------------------|-----------|-------------------------|------------|-------------------------------|-----|
| Rough brass | 67 | 70 | 78 | 83 | 92 | 96 | 100 | (1) |
| " " | 24 | 33 | 42 | 58 | 68 | 81 | 99 | (2) |
| " " | 12 | 14 | 17 | 21 | 25 | 40 | 82 | (3) |
| Galena | 31 | 30 | 21 | 51 | 73 | 76 | 76 | (4) |
| Zincite | 50 | 35 | 18 | 21 | 18 | 20 | 15 | (5) |
| β magnesia, fused..... | 80 | 60 | 34 | 30 | 30 | 30 | 30 | ... |
| Stibnite | 21 | 20 | 4 | 39 | 48 | 52 | 39 | (6) |
| Sphalerite | 10 | 15 | 29 | 20 | 19 | 18 | 17 | (6) |
| Corundum | (30) | 41 | 26 | 31 | 29 | 24 | 22 | (6) |
| Cuprite | 45 | 47 | 47 | 42 | 41 | 42 | 46 | ... |

(1) Ground with No. 60 carborundum. (2) Ditto No. 220. (3) Ditto No. 400. (4) Surface || to cleavage plane, highly polished. (5) Natural crystal. (6) Qualitative only.

TABLE 458.—Transmission

| | $\lambda = 20\mu$ \sim /cm = 500 | 25 400 | 33 $\frac{1}{3}$ 300 | 50 200 | 66 $\frac{2}{3}$ 150 | 100 100 | 150 μ 66 $\frac{2}{3}$ | |
|----------------------------------|---------------------------------------|-----------|-------------------------|-----------|-------------------------|------------|-------------------------------|-----|
| KBr | .. | 61 | 46 | 3 | .. | .. | .. | (7) |
| KI | .. | 83 | 76 | 12 | .. | .. | .. | (7) |
| Amorphous SiO ₂ | 3 | 27 | 64 | 63 | 62 | 70 | 87 | ... |
| CCl ₄ liquid..... | (57) | 63 | 50 | 74 | 74 | (72) | .. | ... |
| KCl | 97 | 97 | 96 | 93 | 80 | 98 | .. | (8) |

(7) No corrections for reflections. (8) Evaporated on lacquer film.

REFLECTION AND ABSORPTION OF LONG-WAVE RADIATIONS

TABLE 459.—Long-wave Absorption by Gases

Unless otherwise noted, gases were contained in a 20 cm long tube. Rubens, Wartenberg, Verh. d. Phys. Ges. 13, p. 796, 1911.

| Gas. | Pressure, cm | Percentage absorption. | | | | | | Gas. | Pressure, cm | Percentage absorption. | | | | | |
|---------------------|--------------|------------------------|------|------|------------------|-----------------|-------------------------------------|------|--------------|------------------------|------|------------------|-----------------|--|--|
| | | 23μ | 52μ | 110μ | Long λ, Hg lamp. | | 23μ | | | 52μ | 110μ | Long λ, Hg lamp. | | | |
| | | | | | | Fil-tered, 314μ | | | | | | | Fil-tered, 314μ | | |
| H ₂ ... | 76 | 100 | 100 | 100 | 100 | 100 | NH ₃ ... | 76 | 83.1 | 0.5 | 99.2 | 43.3 | 66.7 | | |
| Cl ₂ ... | 76 | 100 | 99.6 | 99.5 | 98.5 | 97.6 | CH ₄ ... | 76 | 91 | 94.3 | 99.2 | 100 | 100 | | |
| Br ₂ ... | 20 | 100 | 100 | 100 | 100 | 100 | C ₂ H ₂ ... | 76 | 99.5 | 87.4 | 97.3 | 97.9 | 100 | | |
| SO ₂ ... | 76 | 22.6 | 76.9 | 12.7 | 6 | 4.8 | C ₂ H ₄ ... | 76 | 99 | 96.4 | 92.8 | 100 | 100 | | |
| CO ₂ ... | 76 | 100 | 100 | 100 | 100 | 100 | CS ₂ ... | 26 | 97.8 | 100 | 100 | 99.5 | 100 | | |
| CO... | 76 | 100 | 100 | 94.1 | 92.1 | 91.6 | C ₂ H ₆ O... | 6 | 85.4 | 5.4 | 58 | 52.4 | 49.0 | | |
| H ₂ S... | 76 | 99.6 | 11.6 | 5.4 | 10.3 | 21.4 | C ₂ H ₁₀ O... | 51 | 20.8 | 46 | 34 | 21.8 | 10.7 | | |
| N ₂ O... | 76 | 100 | 96.8 | 98.4 | 93.3 | 90.8 | C ₂ H ₁₂ ... | 46 | 66† | 44.5 | 88.8 | 87 | 84.2 | | |
| NO... | 76 | — | 94 | 99 | 87.3 | 85.5 | CH ₃ Cl... | 14 | 98 | 100 | 100 | 95.4 | 94.7 | | |
| (CN) ₂ | 76 | 100 | 97.8 | 100 | 99.3 | — | H ₂ O*... | 76 | 39.6 | 0.7 | 19.6 | 33.6 | 49.2 | | |

* Steam 100° C passed through tube 40 cm long, 150° C; 0.06 cm ppt. H₂O.

† Pentane vapor, pressure 36 cm.

TABLE 460.—Properties with Wave-lengths 108 ± μ

Rubens and Woods, Verh. d. Phys. Ges. 13, p. 88, 1911.

With quartz, 1.7 cm thick: 60 to 80μ, absorption very great; 63μ, 90%; 82μ, 97.5; 97μ, 83.

| (a) PERCENTAGE REFLECTION. | | | | | | | | | | |
|--------------------------------------|----------------------------------|------------------------------------|---------------------------------|--|--------------------------------|--------------------------------------|-----------|--------|--------|----------|
| Wave-length. | Iceland spar. | Marble. | Rock salt. | Sylvite | KBr | KI | Fluorite. | Glass. | Water. | Alcohol. |
| $\lambda = 82\mu^*$. | — | — | 25.8 | 36.0 | 82.6 | 20.6 | 19.7 | — | 0.6 | — |
| $\lambda = 108\mu^\dagger$. | 47.1 | 43.8 | 20.3 | 19.3 | 31.1 | 35.5 | 20.2 | 19.2 | 11.6 | 1.6 |
| * Restrahlung from KBr. | | | | | | \dagger Isolated with quartz lens. | | | | |
| (b) PERCENTAGE TRANSPARENCY. | | | | | | | | | | |
| Uncorrected for reflections. | | | | | | | | | | |
| Solid. | Thickness. | Transparency. | Liquid. | Thickness. | Thickness precipitable liquid. | Transparency. | | | | |
| Paraffin..... | 3.03 | 57.0 | Benzene..... | 1.00 | — | 56.8 | | | | |
| Mica..... | 0.055 | 16.6 | Ethyl alcohol..... | 0.158 | — | 7.9 | | | | |
| Hard rubber..... | 0.40 | 39.0 | Ethyl ether..... | 0.158 | — | 37.1 | | | | |
| Quartz axis..... | 2.00 | 62.6 | Water..... | 0.029 | — | 25.8 | | | | |
| Quartz, amorph..... | 3.85 | 0 | Water..... | 0.044 | — | 13.6 | | | | |
| Rock salt..... | 0.21 | 21.5 | Vapors: | | | | | | | |
| Fluorite..... | 0.59 | 5.3 | Alcohol..... | 2.00 | 0.023 | 88 | | | | |
| Diamond..... | 1.26 | 45.3 | Ether..... | 2.00 | 0.350 | 33.5 | | | | |
| Quartz \perp axis..... | 2.00 | 81.3 | Benzene..... | 2.00 | 0.003 | 100 | | | | |
| " "..... | 4.03 | 66.4 | Water..... | 4.00 | 0.21 | 19.6 | | | | |
| " "..... | 7.26 | 49.8 | CO ₂ | 2.00 | — | 100 | | | | |
| " "..... | 11.74 | 35.5 | | | | | | | | |
| " "..... | 14.66 | 29.0 | | | | | | | | |
| (c) TRANSPARENCY OF BLACK ABSORBERS. | | | | | | | | | | |
| Method and wave-length. | Black silk paper, .025 mm thick. | Opaque black paper, 0.11 mm thick. | Black card-board, 0.4 mm thick. | Candle lamp-black, 10 cm ² = 1.8 mg | | | | | | |
| Spectrometer | 2 μ | 0 | 0 | 0.5 | | | | | | |
| | 4 | 0.9 | 0 | 8.6 | | | | | | |
| | 6 | 1.7 | 0 | 16.0 | | | | | | |
| | 12 | 8.2 | 1.4 | 37.6 | | | | | | |
| Fluorite "reststrahlen" | 26 | 24.2 | 3.2 | 76.7 | | | | | | |
| Rock salt "reststrahlen" | 52 | 40.0 | 15.1 | 91.3 | | | | | | |
| Quartz lens isolation | 108 | 61.5 | 33.5 | 91.5 | | | | | | |

TABLES 461-462

ROTATION OF PLANE OF POLARIZED LIGHT

TABLE 461.—Tartaric Acid; Camphor; Santonin; Santonic Acid; Cane Sugar

A few examples are here given showing the effect of wavelength on the rotation of the plane of polarization. The rotations are for a thickness of one decimeter of the solution. The examples are quoted from Landolt & Börnstein's "Phys. Chem. Tab." The following symbols are used:—

ρ = number grams of the active substance in 100 grams of the solution.

c = " " solvent " " cubic centimeter "

q = " " active " " cubic centimeter "

Right-handed rotation is marked +, left-handed —.

| Line of spectrum | Wave length according to Angstrom in $\text{cm} \times 10^6$ | Tartaric acid,* $\text{C}_4\text{H}_6\text{O}_6$, dissolved in water. $q = 50$ to 95, temp. = 24°C | Camphor,* $\text{C}_{10}\text{H}_{16}\text{O}$, dissolved in alcohol. $q = 50$ to 95, temp. = 22.9°C | Santonin,† $\text{C}_{15}\text{H}_{10}\text{O}_3$, dissolved in chloroform. $q = 75$ to 96.5, temp. = 20°C | | | |
|------------------|--|---|---|---|--|--|-------------------------------|
| B | 68.67 | | | | | | |
| C | 65.62 | $+2^\circ.748 + 0.09446 q$ | $38^\circ.549 - 0.0852 q$ | $-140^\circ.1 + 0.2085 q$ | | | |
| D | 58.92 | $+1.950 + .13030 q$ | $51.045 - .0904 q$ | $-149.3 + .1555 q$ | | | |
| E | 52.69 | $+1.53 + .17514 q$ | $74.331 - .1343 q$ | $-202.7 + .3086 q$ | | | |
| b ₁ | 51.83 | | | $-285.6 + .5820 q$ | | | |
| b ₂ | 51.72 | $-.832 + .10147 q$ | $70.348 - .1451 q$ | $-302.38 + .6557 q$ | | | |
| F | 48.61 | $-3.598 + .23077 q$ | $99.601 - .1912 q$ | $-365.55 + .8284 q$ | | | |
| e | 43.83 | $-9.657 + .31437 q$ | $149.606 - .2346 q$ | $-534.98 + 1.5240 q$ | | | |
| | | Santonin,† $\text{C}_{15}\text{H}_{10}\text{O}_3$, dissolved in alcohol. $c = 1.782$ temp. = 20°C | Santonin,† $\text{C}_{15}\text{H}_{10}\text{O}_3$, dissolved in alcohol. $c = 4.046$ temp. = 20°C | Santonin,† $\text{C}_{15}\text{H}_{10}\text{O}_3$, dissolved in chloroform. $c = 3.1-30.5$ temp. = 20°C | Santonin,† $\text{C}_{15}\text{H}_{10}\text{O}_3$, dissolved in chloroform. $c = 27.192$ temp. = 20°C | Cane sugar,† $\text{C}_{12}\text{H}_{22}\text{O}_{11}$, dissolved in water. $\rho = 10$ to 30 | |
| B | 68.67 | -110.4° | 442° | 484° | -49° | | |
| C | 65.62 | -118.8 | 504 | 549 | -57 | | |
| D | 58.92 | -161.0 | 693 | 754 | -74 | | |
| E | 52.69 | -222.6 | 991 | 1088 | -105 | | |
| b ₁ | 51.83 | -237.1 | 1053 | 1148 | -112 | | |
| b ₂ | 51.72 | — | — | — | — | | |
| F | 48.61 | -261.7 | 1323 | 1444 | -137 | | |
| e | 43.83 | -380.0 | 2011 | 2201 | -197 | | |
| G | 43.97 | — | — | — | — | | |
| g | 42.26 | — | 2381 | 2610 | -230 | | See Supplementary table below |

* Arndtsen, Ann. Chim. Phys. (3) 54, 1858. † Narini, R. Acc. dei Lincei, (3) 13, 1882.

† Stefan, Sitzb. d. Wien. Akad. 52, 1865.

Supplementary to Table 461

Values obtained at the Bureau of Standards for the rotation of sucrose are given below.

| Light Source | Rot. λ | $[\alpha]_{\lambda}^{20}$ | Light Source | Rot. λ | $[\alpha]_{\lambda}^{20}$ |
|--------------|-----------------------|---------------------------|--------------|-----------------------|---------------------------|
| | Rot. $\lambda = 5461$ | | | Rot. $\lambda = 5461$ | |
| Li 6708 | .644 | 50.45 | Cd 4678 | 1.493 | 109.9 |
| Cd 6438 | .711 | 55.70 | Hg 4358 | 1.644 | 128.8 |
| Na 5892.5 | .84922 | 66.520 | Ag 4208 | 1.786 | 139.9 |
| Hg 5780 | .8854 | 69.36 | Hg 4047 | 1.95 | 152.8 |
| Hg 5461 | 1.0000 | 78.342 | | | |
| Ag 5209 | 1.108 | 86.80 | | | |
| Cd 5086 | 1.167 | 91.43 | | | |
| Cd 4800 | 1.323 | 103.05 | | | |

The above values are for a near normal solution, i.e. approximately 26 g of sucrose per 100 cc.

TABLE 462.—Sodium Chlorate; Quartz

| Sodium chlorate (Guye, C. R. 108, 1880) | | | | Quartz (Soret & Sarasin, Arch. de Gen. 1882, or C. R. 95, 1882)* | | | | | |
|---|-------------|---------|-----------------|--|-------------|-----------------|------------------|-------------|-----------------|
| Spectrum line | Wave length | Temp. C | Rotation per mm | Spectrum line | Wave length | Rotation per mm | Spectrum line | Wave length | Rotation per mm |
| a | 7164A | 15°.0 | 2°.068 | A | 7604 | 12°.668 | Cd ₉ | 3609 | 63°.628 |
| B | 6870 | 17.4 | 2.318 | a | 7164 | 14.304 | N | 3582 | 64.459 |
| C | 6563 | 20.6 | 2.599 | B | 6870 | 15.746 | Cd ₁₀ | 3405 | 69.454 |
| D | 5892 | 18.3 | 3.104 | | | | O | 3441 | 70.587 |
| E | 5270 | 16.0 | 3.841 | C | 6563 | 17.318 | | | |
| F | 4861 | 11.9 | 4.587 | D ₁ | 5896 | 21.684 | Cd ₁₁ | 3401 | 72.448 |
| G' | 4340 | 10.1 | 5.331 | D ₂ | 5890 | 21.727 | P | 3360 | 74.571 |
| G | 4308 | 14.5 | 6.005 | | | | Q | 3286 | 78.579 |
| H | 4101 | 13.3 | 6.754 | E | 5270 | 27.543 | Cd ₁₂ | 3247 | 80.459 |
| L | 3820 | 14.0 | 7.654 | F | 4862 | 32.773 | | | |
| M | 3728 | 10.7 | 8.100 | G | 4308 | 42.604 | R | 3180 | 84.972 |
| N | 3581 | 12.9 | 8.861 | | | | Cd ₁₇ | 2747 | 121.052 |
| P | 3361 | 12.1 | 9.801 | h | 4102 | 47.481 | Cd ₁₈ | 2571 | 143.266 |
| Q | 3287 | 11.9 | 10.787 | H | 3969 | 51.193 | Cd ₂₃ | 2312 | 190.426 |
| R | 3180 | 13.1 | 11.921 | K | 3934 | 52.155 | | | |
| T | 3021 | 12.8 | 12.424 | | | | Cd ₂₄ | 2264 | 201.824 |
| Cd ₁₇ | 2747 | 12.2 | 13.426 | L | 3820 | 55.625 | Cd ₂₅ | 2193 | 220.731 |
| Cd ₁₈ | 2571 | 11.6 | 14.965 | M | 3728 | 58.894 | Cd ₂₆ | 2143 | 235.972 |

* The paper is quoted from a paper by Ketteler in Wied. Ann. vol. 21, p. 444.

ELECTRICAL EQUIVALENTS

Abbreviations: int., international; e.m.u., electromagnetic units; e.s.u., electrostatic units; c.g.s., centimeter-gram-second units. (Taken from Circular 60 of U. S. Bureau of Standards, 1916, Electric Units and Standards, but made consistent with Birge's values, p. 77 et seq.)

RESISTANCE:

- 1 international ohm =
 1.00051 absolute ohms
 1.0001 int. ohms (France, before 1911)
 1.00016 Board of Trade units (England, 1903)
 1.01358 B. A. units
 1.00283 "legal ohms" of 1884
 1.06300 Siemens units

- 1 absolute ohm =
 0.99949 int. ohms
 1 "practical" e.m.u.
 10^9 c.g.s. e.m.u.
 1.11262×10^{-12} c.g.s. e.s.u.

CURRENT:

- 1 international ampere =
 0.99995 absolute ampere
 1.00084 int. amperes (U. S. before 1911)
 1.00130 int. amperes (England, before 1906)
 1.00106 int. amperes (England, 1906-08)
 1.00010 int. amperes (England, 1909-10)
 1.00032 int. amperes (Germany, before 1911)
 1.0002 int. amperes (France, before 1911)

- 1 absolute ampere =
 1.00005 int. amperes
 1 "practical" e.m.u.
 0.1 c.g.s. e.m.u.
 2.99796×10^9 c.g.s. e.s.u.

ELECTROMOTIVE FORCE:

- 1 international volt =
 1.00046 absolute volts
 1.00084 int. volts (U. S. before 1911)
 1.00130 int. volts (England, before 1906)
 1.00106 int. volts (England, 1906-08)
 1.00010 int. volts (England, 1909-10)
 1.00032 int. volts (Germany, before 1911)
 1.00032 int. volts (France, before 1911)
 1 absolute volt =
 0.99954 int. volt
 1 "practical" e.m.u.
 10^8 c.g.s. e.m.u.
 0.00333560 c.g.s. e.s.u.

QUANTITY OF ELECTRICITY:

(Same as current equivalents.)

- 1 international coulomb =
 1/3600 ampere-hour
 1/96494 faraday

CAPACITY:

- 1 international farad =
 0.99949 absolute farad
 1 absolute farad =
 1.00051 int. farads
 1 "practical" e.m.u.
 10^{-9} c.g.s. e.m.u.
 8.98776×10^{11} c.g.s. e.s.u.

INDUCTANCE:

- 1 international henry =
 1.00051 absolute henries
 1 absolute henry =
 0.99949 int. henry
 1 "practical" e.m.u.
 10^9 e.m.u.
 1.11262×10^{-12} c.g.s. e.s.u.

ENERGY AND POWER:

(standard gravity = 980.665 cm/sec./sec.)

- 1 international joule =
 1.00041 absolute joules
 1 absolute joule =
 0.99959 int. joule
 10^7 ergs
 0.737500 standard foot-pound
 0.101972 standard kilogram-meter
 0.277778×10^{-6} kilowatt-hour

RESISTIVITY:

- 1 ohm-cm = 0.393700 ohm-inch
 = 10,000 ohm (meter, mm²)
 = 12,732.4 ohm (meter, mm)
 = 393.700 microhm-inch
 = 1,000,000 microhm-cm
 = 6,015,290 ohm (mil, foot)

- 1 ohm (meter, gram) = 5710.0 ohm (mile, pound)

MAGNETIC QUANTITIES:

- 1 int. gilbert = 0.99995 absolute gilbert
 1 absolute gilbert = 1.00005 int. gilberts
 1 int. maxwell = 1.00046 absolute maxwells
 1 absolute maxwell = 0.99954 int. maxwell
 1 gilbert = 0.7958 ampere-turn
 1 gilbert per cm = 0.7958 ampere-turn per cm
 = 2.021 ampere-turns per inch
 1 maxwell = 1 line
 = 10^{-8} volt-second
 1 maxwell per cm² = 6.452 maxwells per in.²

COMPOSITION AND ELECTROMOTIVE FORCE OF VOLTAIC CELLS

The electromotive forces given in this table approximately represent what may be expected from cell in good working order, but, with the exception of the standard cells, all of them are subject to considerable variation.

| (a) Double Fluid Cells | | | | | |
|------------------------|---------------|--|-----------------------------------|---|-----------------|
| Name of cell | Negative pole | Solution | Positive pole | Solution | E.m.f. in volts |
| Bunsen | Amalg. Zn | 1, H ₂ SO ₄ ; 12, H ₂ O | C | Fuming HNO ₃ | 1.94 |
| " | " " | " | " | HNO ₃ ; dens. 1.38 | 1.86 |
| Chromate | " " | 12, K ₂ Cr ₂ O ₇ ; 25, H ₂ SO ₄ ; 100, H ₂ O | " | 1, H ₂ SO ₄ ; 12, H ₂ O | 2.00 |
| " | " " | 1, H ₂ SO ₄ ; 12, H ₂ O | " | 12, K ₂ Cr ₂ O ₇ ; 100, H ₂ O | 2.03 |
| Daniell | " " | 1, H ₂ SO ₄ ; 4, H ₂ O | Cu | Sat. sol. CuSO ₄ ; 5, H ₂ O | 1.06 |
| " | " " | 1, H ₂ SO ₄ ; 12, H ₂ O | " | " | 1.09 |
| " | " " | 5% sol. ZnSO ₄ ; 6H ₂ O | " | " | 1.08 |
| " | " " | 1 NaCl; 4 parts H ₂ O | " | " | 1.05 |
| Grove | " " | 1 H ₂ SO ₄ ; 12 H ₂ O | Pt | Fuming HNO ₃ | 1.93 |
| " | " " | Sol. ZnSO ₄ | " | HNO ₃ ; dens. 1.33 | 1.66 |
| " | " " | H ₂ SO ₄ sol.; dens. 1.136 | " | Concent. HNO ₃ | 1.93 |
| " | " " | H ₂ SO ₄ ; dens. 1.136 | " | HNO ₃ ; dens. 1.33 | 1.79 |
| " | " " | H ₂ SO ₄ sol.; dens. 1.14 | " | HNO ₃ ; dens. 1.19 | 1.66 |
| " | " " | H ₂ SO ₄ sol.; dens. 1.06 | " | " " " | 1.61 |
| " | " " | NaCl sol. | " | " " 1.33 | 1.88 |
| Partz | " " | Sol. MgSO ₄ | " | Sol. K ₂ Cr ₂ O ₇ | 2.06 |
| (b) Single Fluid Cells | | | | | |
| Leclanche | Amalg. Zn | Sol. NH ₄ Cl | Carbon* | | 1.46 |
| Chaperon | " " | Sol. KOH | Copper** | | .98 |
| Edison-Lelande | " " | " | " | | .70 |
| AgCl | Zn | 23% sol. NH ₄ Cl | Silver*** | | 1.02 |
| Law | " | 15% " " " | Carbon | | 1.37 |
| Dry cell | " | 1 pt. ZnO, 1 pt. NH ₄ Cl, 3 pts. plaster of paris, 2 pts. ZnCl ₂ , and water to make a paste | " | | 1.3 |
| Poggendorff | Amalg. Zn | Sol. K ₂ Cr ₂ O ₇ | " | | 1.08 |
| " | " " | 12 K ₂ Cr ₂ O ₇ ; 25 H ₂ SO ₄ ; 100, H ₂ O | " | | 2.01 |
| Regnault | " " | 1 H ₂ SO ₄ ; 12 H ₂ O; 1 CaSO ₄ | Cd | | .34 |
| Volta couple | Zn | H ₂ O | Cu | | .98 |
| (c) Secondary Cells | | | | | |
| Pb accumulator | Pb | H ₂ SO ₄ sol. of density 1.1 | PbO ₂ | | 2.21 |
| Regnier (1) | Cu | CuSO ₄ ; H ₂ SO ₄ | " | | 1.68 |
| " (2) | Amalg. Zn | ZnSO ₄ sol. | " | | to .85 |
| Main | " " | H ₂ SO ₄ ; dens. about 1.1 | in H ₂ SO ₃ | | 2.36 |
| Edison | Fe | KOH 20% sol. | A nickel oxide | | 2.50 |

* Depolarizer: Manganese peroxide with powdered carbon. ** Depolarizer: CuO. *** Depolarizer: Silver chloride.

† F. Streintz gives the following value of the temperature variation $\frac{dE}{dt}$ at different stages of charge:

| E. M. F. | 1.9223 | 1.9828 | 2.0031 | 2.0084 | 2.0105 | 2.0779 | 2.2070 |
|-------------------------|--------|--------|--------|--------|--------|--------|--------|
| dE/dt × 10 ⁶ | 140 | 228 | 335 | 285 | 255 | 130 | 73 |

Dolezalek gives the following relation between E. M. F. and acid concentration:

| Per cent H ₂ SO ₄ | 64.5 | 52.2 | 35.3 | 21.4 | 5.2 |
|---|------|------|------|------|------|
| E. M. F., °C | 2.37 | 2.25 | 2.10 | 2.00 | 1.80 |

CONTACT DIFFERENCE OF POTENTIAL IN VOLTS

Solids with Liquids and Liquids with Liquids in Air *

Temperature of substances during experiment about 16° C

| | C | Cu | Fe | Pb | Pt | Sn | Zn | Amalg. Zn | Brass | Dis- tilled water |
|--|--------------------|----------------------|--------|----------------------|----------------------|--------|------------------------|--------------|--------|-------------------------|
| H ₂ O | { .01 to .17 | { .269 to .100 | .148 | .171 | { .285 to .345 | .177 | { -.105 to +.156 | .100 | .231 | ... |
| Alum. sat.sol. . | ... | — .127 | — .653 | — .139 | .246 | — .225 | — .536 | ... | .014 | ... |
| CuSO ₄ sol. | | | | | | | | | | |
| sp.gr. 1.087.. | ... | .103 | ... | ... | ... | ... | ... | ... | ... | ... |
| CuSO ₄ sat.sol. | ... | .070 | ... | ... | ... | ... | ... | ... | ... | ... |
| Sea salt sol. | | | | | | | | | | |
| 1.18 at 20° C | ... | — .475 | — .605 | ... | — .856 | — .334 | — .565 | ... | — .435 | ... |
| NH ₄ Cl, sat.sol. | ... | — .396 | — .652 | — .189 | .059 | — .364 | — .637 | ... | — .348 | — |
| ZnSO ₄ sol. 1.125 | | | | | | | | | | |
| at 4° C..... | ... | ... | ... | ... | ... | ... | — .238 | ... | ... | ... |
| ZnSO ₄ sat.sol.. | ... | ... | ... | ... | ... | ... | — .430 | — .284 | ... | — .200 |
| One part H ₂ O + 3, sat. ZnSO ₄ | ... | ... | ... | ... | ... | ... | — .444 | ... | ... | ... |
| Strong H ₂ SO ₄ in water: | | | | | | | | | | |
| 1 to 20 by wt.. | ... | ... | ... | ... | ... | ... | — .344 | ... | ... | ... |
| 1 to 10 by vol. { about | ... | ... | ... | ... | ... | ... | ... | — .358 | ... | ... |
| 1 to 5 by wt.. | ... | ... | ... | ... | ... | ... | ... | .429 | ... | ... |
| 5 to 1 by wt.. { | { .01 to 3.0 | ... | ... | — .120 | ... | — .25 | ... | ... | — .016 | ... |
| Con. H ₂ SO ₄ .. | { .55 to .85 | 1.113 | ... | { .72 to 1.252 | { 1.3 to 1.6 | ... | ... | .848 | ... | 1.298 |
| Con. HNO ₃ .. | ... | ... | ... | ... | .672 | ... | ... | ... | ... | ... |

Mercurous sulphate paste, Hg, + .475. Sat. CuSO₄ sol., H₂O, — .043; sat. ZnSO₄ sol., + .095; 1 pt. H₂O, 3 pt. ZnSO₄ + .102.

Concentrated H₂SO₄, H₂O, + 1.298; sat. alum. sol., + 1.456; CuSO₄ sat. + 1.269; ZnSO₄ sat. sol., + 1.699.

* Everett, Units and physical constants: Table of Ayrton and Perry's results, prepared by Ayrton.

DIFFERENCE OF POTENTIAL BETWEEN METALS IN SOLUTIONS OF SALTS

The following numbers are given by G. Magnanini * for the difference of potential in hundredths of a volt between zinc in a normal solution of sulphuric acid and the metals named at the head of the different columns when placed in the solution named in the first column. The solutions were contained in a U-tube, and the sign of the difference of potential is such that the current will flow from the more positive to the less positive through the external circuit.

| Strength of the solution in gram molecules per liter. | | Zinc.† | Cadmium.† | Lead. | Tin. | Copper. | Silver. |
|---|---|--|-----------|-------|-------|---------|---------|
| No. of molecules. | Salt. | Difference of potential in centivolts. | | | | | |
| 0.5 | H ₂ SO ₄ | 0.0 | 36.6 | 51.3 | 51.3 | 100.7 | 121.3 |
| 1.0 | NaOH | —32.1 | 19.5 | 31.8 | 0.2 | 80.2 | 95.8 |
| 1.0 | KOH | —42.5 | 15.5 | 32.0 | —1.2 | 77.0 | 104.0 |
| 0.5 | Na ₂ SO ₄ | 1.4 | 35.6 | 50.8 | 51.4 | 101.3 | 120.9 |
| 1.0 | Na ₂ S ₂ O ₃ | —5.9 | 24.1 | 45.3 | 45.7 | 38.8 | 64.8 |
| 1.0 | KNO ₃ | 11.8‡ | 31.9 | 42.6 | 31.1 | 81.2 | 105.7 |
| 1.0 | NaNO ₃ | 11.5 | 32.3 | 51.0 | 40.9 | 95.7 | 114.8 |
| 0.5 | K ₂ CrO ₄ | 23.9‡ | 42.8 | 41.2 | 40.9 | 94.6 | 121.0 |
| 0.5 | K ₂ Cr ₂ O ₇ | 72.8 | 61.1 | 78.4 | 68.1 | 123.6 | 132.4 |
| 0.5 | K ₂ SO ₄ | 1.8 | 34.7 | 51.0 | 40.9 | 95.7 | 114.8 |
| 0.5 | (NH ₄) ₂ SO ₄ | —0.5 | 37.1 | 53.2 | 57.6‡ | 101.5 | 125.7 |
| 0.25 | K ₄ FeC ₆ N ₆ | —6.1 | 33.6 | 50.7 | 41.2 | —‡ | 87.8 |
| 0.167 | K ₆ Fe ₂ (CN) ₁₂ | 41.0§ | 80.8 | 81.2 | 130.9 | 110.7 | 124.9 |
| 1.0 | KCNS | —1.2 | 32.5 | 52.8 | 52.7 | 52.5 | 72.5 |
| 1.0 | NaNO ₃ | 4.5 | 35.2 | 50.2 | 49.0 | 103.6 | 104.6? |
| 0.5 | Sr(NO ₃) ₂ | 14.8 | 38.3 | 50.6 | 48.7 | 103.0 | 119.3 |
| 0.125 | Ba(NO ₃) ₂ | 21.9 | 39.3 | 51.7 | 52.8 | 109.6 | 121.5 |
| 1.0 | KNO ₃ | —‡ | 35.6 | 47.5 | 49.9 | 104.8 | 115.0 |
| 0.2 | KClO ₄ | 15–10‡ | 39.9 | 53.8 | 57.7 | 105.3 | 120.9 |
| 0.167 | KBrO ₃ | 13–20‡ | 40.7 | 51.3 | 50.9 | 111.3 | 120.8 |
| 1.0 | NH ₄ Cl | 2.9 | 32.4 | 51.3 | 50.9 | 81.2 | 101.7 |
| 1.0 | KF | 2.8 | 22.5 | 41.1 | 50.8 | 61.3 | 61.5 |
| 1.0 | NaCl | — | 31.9 | 51.2 | 50.3 | 80.9 | 101.3 |
| 1.0 | KBr | 2.3 | 31.7 | 47.2 | 52.5 | 73.6 | 82.4 |
| 1.0 | KCl | — | 32.1 | 51.6 | 52.6 | 81.6 | 107.6 |
| 0.5 | Na ₂ SO ₃ | —8.2 | 28.7 | 41.0 | 31.0 | 68.7 | 103.7 |
| — | NaOBr | 18.4 | 41.6 | 73.1 | 70.6‡ | 89.9 | 99.7 |
| 1.0 | C ₄ H ₆ O ₆ | 5.5 | 39.7 | 61.3 | 54.4§ | 104.6 | 123.4 |
| 0.5 | C ₄ H ₆ O ₆ | 4.1 | 41.3 | 61.6 | 57.6 | 110.9 | 125.7 |
| 0.5 | C ₄ H ₄ KNaO ₆ | —7.9 | 31.5 | 51.5 | 42–47 | 100.8 | 119.7 |

* "Rend. della R. Acc. di Roma," 1890.

† Amalgamated.

‡ Not constant.

§ After some time.

|| A quantity of bromine was used corresponding to NaOH = 1.

THERMOELECTRIC POWER

The thermoelectric power of a circuit of two metals is the electromotive force produced by one degree C difference of temperature between the junctions. The thermoelectric power varies with the temperature, thus: thermoelectric power $= Q = dE/dt = A + Bt$, where A is the thermoelectric power at 0°C , B is a constant, and t is the mean temperature of the junctions. The neutral point is the temperature at which $dE/dt = 0$, and its value is $-A/B$. When a current is caused to flow in a circuit of two metals originally at a uniform temperature, heat is liberated at one of the junctions and absorbed at the other. The rate of production or liberation of heat at each junction, or Peltier effect, is given in calories per second, by multiplying the current by the coefficient of the Peltier effect. This coefficient in calories per coulomb $= QT/\mathcal{T}$, in which Q is in volts per degree C, T is the absolute temperature of the junction, and $\mathcal{T} = 4.19$. Heat is also liberated or absorbed in each of the metals as the current flows through portions of varying temperature. The rate of production or liberation of heat in each metal, or the Thomson effect, is given in calories per second by multiplying the current by the coefficient of the Thomson effect. This coefficient, in calories per coulomb $= BT\theta/\mathcal{T}$, in which B is in volts per degree C, T is the mean absolute temperature of the junctions, and θ is the difference of temperature of the junctions. (BT) is Sir W. Thomson's "Specific Heat of Electricity." The algebraic signs are so chosen in the following table that when A is positive, the current flows in the metal considered from the hot junction to the cold. When B is positive, Q increases (algebraically) with the temperature. The values of A , B , and thermoelectric power in the following table are with respect to lead as the other metal of the thermoelectric circuit. The thermoelectric power of a couple composed of two metals, 1 and 2, is given by subtracting the value for 2 from that for 1; when this difference is positive, the current flows from the hot junction to the cold in 1. In the following table, A is given in microvolts per degree, B in microvolts per degree per degree, and the neutral point in degrees.

The table has been compiled from the results of Becquerel, Matthiessen and Tait; in reducing the results, the electromotive force of the Grove and Daniell cells has been taken as 1.95 and 1.07 volts. The value for constantan was reduced from results given in Landolt-Börnstein's tables. The thermoelectric powers of antimony and bismuth alloys are given by Becquerel in the reference given below.

| Substance. | A Microvolts. | B Microvolts. | Thermoelectric power at mean temp. of junctions (microvolts). | | Neutral point $-\frac{A}{B}$ | Author- ity. |
|----------------------------------|--------------------|--------------------|---|--------------------|------------------------------------|-----------------|
| | | | 20°C | 50°C | | |
| Aluminum..... | -0.76 | +0.0039 | -0.68 | -0.56 | +195 | T |
| Antimony, comm'l pressed wire... | — | — | +6.0 | — | — | M |
| “ axial..... | — | — | +22.6 | — | — | “ |
| “ equatorial..... | — | — | +26.4 | — | — | “ |
| Argentan..... | -11.94 | -0.0506 | -12.05 | -14.47 | -236 | T |
| “..... | — | — | — | -12.7 | — | B |
| Arsenic..... | — | — | -13.56 | — | — | M |
| Bismuth, comm'l pressed wire... | — | — | -97.0 | — | — | “ |
| “ pure..... | — | — | -89.0 | — | — | “ |
| “ crystal, axial..... | — | — | -65.0 | — | — | “ |
| “ equatorial..... | — | — | -45.0 | — | — | “ |
| Cadmium..... | +2.63 | +0.0424 | +3.48 | +4.75 | -62 | T |
| “ fused..... | — | — | — | +2.45 | — | B |
| Calcium..... | — | — | — | +8.9 | — | S' |
| Cobalt..... | — | — | -22 | — | — | M |
| Constantan..... | — | — | — | -19.3 | — | — |
| Copper..... | +1.34 | +0.0094 | +1.52 | +1.81 | -143 | T |
| “ commercial..... | — | — | +0.10 | — | — | M |
| “ galvanoplastic..... | — | — | +3.8 | — | — | “ |
| Gallium..... | — | — | -0.2 | — | — | S |
| Gold..... | +2.80 | +0.0101 | +3.0 | +3.30 | [-277] | T |
| Iron..... | +17.15 | -0.0482 | +10.2 | +14.74 | +356 | T |
| “ pianoforte wire..... | — | — | +17.5 | — | — | M |
| “ commercial..... | — | — | — | +12.10 | — | B |
| “..... | — | — | — | +0.10 | — | “ |
| Lead..... | — | 0.0000 | -0.00 | 0.00 | — | — |
| Magnesium..... | +2.22 | -0.0094 | +2.03 | +1.75 | +236 | T |
| Molybdenum..... | — | — | +5.9 | — | — | S |
| Mercury..... | — | — | -0.413 | -3.30 | — | MB |
| Nickel..... | — | — | — | -15.50 | — | B |
| “ (-18° to 175°)..... | -21.8 | -0.0506 | -22.8 | -24.33 | [-431] | T |
| “ (250°-300°)..... | -83.57 | +0.2384 | — | — | — | “ |
| “ (above 340°)..... | -3.04 | -0.0506 | — | — | — | “ |

TABLE 467 (continued).—Thermoelectric Power

| Substance. | A Microvolts. | B Microvolts. | Thermoelectric power at mean temp. of junctions (microvolts). | | Neutral point $-\frac{A}{B}$ | Autho- rity. |
|-----------------------------|------------------|------------------|---|-------|------------------------------------|-----------------|
| | | | 20° C | 50° C | | |
| Palladium | -6.18 | -0.0355 | -6.9 | -7.96 | -174 | T |
| Phosphorus (red) | - | - | +29.9 | - | - | M |
| Platinum | - | - | +0.9 | - | - | " |
| " (hardened) | +2.57 | -0.0074 | +2.42 | +2.20 | 347 | T |
| " (malleable) | -0.60 | -0.0109 | -818 | -1.15 | -55 | " |
| " wire | - | - | - | +0.94 | - | B |
| " another specimen . . . | - | - | - | -2.14 | - | " |
| Platinum-iridium alloys: | | | | | | |
| 85% Pt + 15% Ir | +7.90 | +0.0062 | +8.03 | +8.21 | [-1274] | T |
| 90% Pt + 10% Ir | +5.90 | -0.0133 | +5.63 | +5.23 | 444 | " |
| 95% Pt + 5% Ir | +6.15 | +0.0055 | +6.26 | +6.42 | [-1118] | " |
| Selenium | - | - | +807. | - | - | M |
| Silver | +2.12 | +0.0147 | +2.41 | +2.86 | -144 | T |
| " (pure hard) | - | - | +3.00 | - | - | M |
| " wire | - | - | - | +2.18 | - | B |
| Steel | +11.27 | -0.0325 | +10.62 | +9.65 | 347 | T |
| Tantalum | - | - | -2.6 | - | - | - |
| Tellurium β | - | - | +500. | - | - | H |
| " α | - | - | +160. | - | - | H |
| Thallium | - | - | +0.8 | - | - | - |
| Tin (commercial) | - | - | - | +0.33 | - | H |
| " | - | - | +0.1 | - | - | M |
| " | -0.43 | +0.0055 | -0.33 | -0.16 | 78 | T |
| Tungsten | - | - | -2.0 | - | - | - |
| Zinc | +2.32 | +0.0238 | +2.79 | +3.51 | -98 | T |
| " pure pressed | - | - | +3.7 | - | - | M |

B Ed. Becquerel, "Ann. de Chim. et de Phys." [4] vol. 8. S. Bureau of Standards.

M Matthiesen, "Pogg. Ann." vol. 103, reduced by Fleming Jenkin.

T Tait, "Trans. R. S. E." vol. 27, reduced by Mascart.

H Haken, Ann. der Phys. 32, p. 291, 1910. (Electrical conductivity of $\text{Te}\beta = 0.04$, $\text{Te}\alpha$ 1.7 c. m. units.) Swisher, 1917.

TABLE 468.—Thermoelectric Power of Alloys

The thermoelectric powers of a number of alloys are given in this table, the authority being Ed. Becquerel. They are relative to lead, and for a mean temperature of 50° C. In reducing the results from copper as a reference metal, the thermoelectric power of lead to copper was taken as -1.9.

| Substance. | Relative quantity. | Thermoelec- tric power in microvolts. | Substance. | Relative quantity. | Thermoelec- tric power in microvolts. | Substance. | Relative quantity. | Thermoelec- tric power in microvolts. |
|------------|--------------------|---|------------|--------------------|---|------------------|--------------------|---|
| Antimony | 806 | 227 | Antimony | 2 | 43 | Bismuth | 4 | -51.4 |
| Cadmium | 696 | | Zinc | 1 | | Antimony | 1 | |
| Antimony | 4 | 146 | Tin | 1 | | Bismuth | 8 | -63.2 |
| Cadmium | 2 | | Antimony | 12 | 35 | Antimony | 1 | |
| Zinc | 1 | 137 | Cadmium | 10 | | Bismuth | 10 | -68.2 |
| Antimony | 806 | | Zinc | 3 | 10.2 | Antimony | 1 | |
| Cadmium | 696 | 95 | Antimony | 10 | | Bismuth | 12 | -66.9 |
| Bismuth | 121 | | Tellurium | 1 | 8.8 | Antimony | 1 | |
| Antimony | 806 | 8.1 | Antimony | 10 | | Bismuth | 2 | 60 |
| Zinc | 406 | | Bismuth | 1 | 2.5 | Tin | 1 | |
| Antimony | 806 | 76 | Antimony | 4 | 1.4 | Bismuth | 10 | -24.5 |
| Zinc | 406 | | Iron | 1 | -0.4 | Selenium | 1 | |
| Bismuth | 121 | 46 | Antimony | 8 | | Bismuth | 12 | -31.1 |
| Antimony | 4 | | Magnesium | 1 | -43.8 | Zinc | 1 | |
| Cadmium | 2 | 46 | Antimony | 8 | -33.4 | Bismuth | 12 | -46.0 |
| Lead | 1 | | Lead | 1 | | Arsenic | 1 | |
| Zinc | 1 | 46 | Bismuth | - | -33.4 | Bismuth | 1 | 68.1 |
| Antimony | 4 | | Bismuth | 2 | | Bismuth sulphide | 1 | |
| Cadmium | 2 | 46 | Antimony | 1 | | | | |
| Zinc | 1 | | | | | | | |
| Tin | 1 | | | | | | | |

TABLE 469.—Thermal Electromotive Force of Metals and Alloys versus Platinum (millivolts)

One junction is supposed to be at 0° C; + indicates that the current flows from the 0° junction into the platinum. The rhodium and iridium were rolled, the other metals drawn.*

| Temperature, ° C. | Au. | Ag. | 90%Pt+ 10%Pd. | 10%Pt+ 90%Pd. | Pd. | 90%Pt+ 10%Rh. | 90%Pt+ 10%Ru. | Ir. | Rh. |
|-------------------|-------|-------|------------------|------------------|-------|------------------|------------------|-------|-------|
| —185 | —0.15 | —0.16 | —0.11 | +0.24 | +0.77 | — | —0.53 | —0.28 | —0.24 |
| —80 | —0.31 | —0.30 | —0.09 | +0.15 | +0.39 | — | —0.39 | —0.32 | —0.31 |
| +100 | +0.74 | +0.72 | +0.26 | —0.19 | —0.56 | — | +0.73 | +0.65 | +0.65 |
| +200 | +1.8 | +1.7 | +0.62 | —0.31 | —1.20 | — | +1.6 | +1.5 | +1.5 |
| +300 | +3.0 | +3.0 | +1.0 | —0.37 | —2.0 | +2.3 | +2.6 | +2.5 | +2.6 |
| +400 | +4.5 | +4.5 | +1.5 | —0.35 | —2.8 | +3.2 | +3.6 | +3.6 | +3.7 |
| +500 | +6.1 | +6.2 | +1.9 | —0.18 | —3.8 | +4.1 | +4.6 | +4.8 | +5.1 |
| +600 | +7.9 | +8.2 | +2.4 | +0.12 | —4.9 | +5.1 | +5.7 | +6.1 | +6.5 |
| +700 | +9.9 | +10.6 | +2.9 | +0.61 | —6.3 | +6.2 | +6.9 | +7.6 | +8.1 |
| +800 | +12.0 | +13.2 | +3.4 | +1.2 | —7.9 | +7.2 | +8.0 | +9.1 | +9.9 |
| +900 | +14.3 | +16.0 | +3.8 | +2.1 | —9.6 | +8.3 | +9.2 | +10.8 | +11.7 |
| +1000 | +16.8 | — | +4.3 | +3.1 | —11.5 | +9.5 | +10.4 | +12.6 | +13.7 |
| +1100 | — | — | +4.8 | +4.2 | —13.5 | +10.6 | +11.6 | +14.5 | +15.8 |
| +(1300) | — | — | — | — | — | +13.1 | +14.2 | +18.6 | +20.4 |
| +(1500) | — | — | — | — | — | +15.6 | +16.9 | +23.1 | +25.6 |

* Holborn and Day.

TABLE 470.—Thermal Electromotive Force of Platinum-Rhodium Alloys versus Platinum

Temperature versus Electromotive Force in Millivolts

| Temp. °C | Per Cent Rhodium | | | | | | | |
|----------|------------------|-------|-------|-------|-------|-------|-------|---------|
| | 0.5 | 1.0 | 5.0 | 10.0 | 20.0 | 40.0 | 80.0 | 100.0 * |
| 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 100 | +0.10 | +0.18 | +0.54 | +0.64 | +0.63 | +0.65 | +0.62 | +0.70 |
| 200 | .20 | .37 | 1.16 | 1.43 | 1.44 | 1.52 | 1.49 | 1.61 |
| 300 | .29 | .57 | 1.82 | 2.32 | 2.40 | 2.55 | 2.55 | 2.68 |
| 400 | .39 | .76 | 2.49 | 3.25 | 3.47 | 3.70 | 3.77 | 3.91 |
| 500 | .48 | .94 | 3.17 | 4.22 | 4.63 | 4.97 | 5.12 | 5.28 |
| 600 | .58 | 1.12 | 3.86 | 5.22 | 5.87 | 6.36 | 6.60 | 6.77 |
| 700 | .67 | 1.30 | 4.55 | 6.26 | 7.20 | 7.85 | 8.20 | 8.40 |
| 800 | .76 | 1.48 | 5.25 | 7.33 | 8.59 | 9.45 | 9.92 | 10.16 |
| 900 | .85 | 1.66 | 5.96 | 8.43 | 10.06 | 11.16 | 11.76 | 12.04 |
| 1000 | .94 | 1.84 | 6.68 | 9.57 | 11.58 | 12.98 | 13.73 | 14.05 |
| 1100 | 1.03 | 2.02 | 7.42 | 10.74 | 13.17 | 14.90 | 15.81 | 16.18 |
| 1200 | 1.13 | 2.20 | 8.16 | 11.93 | 14.84 | 16.91 | 17.99 | 18.42 |

* Bur. Standards Journ. Res., 3, 1029, 1929.

TABLE 471.—Thermal Electromotive Force of Aluminum versus Platinum *
Temperature versus Electromotive Force

| °C | Intern. mv | °C | Intern. mv | °C | Intern. mv |
|-----|------------|-----|------------|-----|------------|
| 0 | 0.000 | 240 | 1.374 | 480 | 3.703 |
| 20 | +0.062 | 260 | 1.538 | 500 | 3.931 |
| 40 | 0.135 | 280 | 1.708 | 520 | 4.164 |
| 60 | 0.218 | 300 | 1.884 | 540 | 4.403 |
| 80 | 0.312 | 320 | 2.065 | 560 | 4.647 |
| 100 | 0.416 | 340 | 2.252 | 580 | 4.896 |
| 120 | 0.529 | 360 | 2.444 | 600 | 5.150 |
| 140 | 0.651 | 380 | 2.641 | 620 | 5.409 |
| 160 | 0.781 | 400 | 2.843 | 640 | 5.673 |
| 180 | 0.919 | 420 | 3.050 | 660 | 5.942 |
| 200 | 1.064 | 440 | 3.262 | | |
| 220 | 1.216 | 460 | 3.480 | | |

* Bur. Standards Circ. 346, 1927.

TABLE 472.—Thermal Electromotive Force of Zinc versus Platinum
Temperature versus Electromotive Force

| °C | Intern. mv | °C | Intern. mv | °C | Intern. mv |
|-----|------------|-----|------------|-----|------------|
| 0 | 0.000 | 150 | 1.276 | 300 | 3.417 |
| 25 | +0.153 | 175 | 1.572 | 325 | 3.853 |
| 50 | 0.331 | 200 | 1.894 | 350 | 4.310 |
| 75 | 0.533 | 225 | 2.240 | 375 | 4.786 |
| 100 | 0.758 | 250 | 2.610 | 400 | 5.290 |
| 125 | 1.005 | 275 | 3.002 | 415 | 5.604 |

TABLE 473.—Thermal Electromotive Force of Cadmium versus Platinum
Temperature versus Electromotive Force

| °C | Intern. mv | °C | Intern. mv | °C | Intern. mv |
|-----|------------|-----|------------|-----|------------|
| 0 | 0.000 | 125 | 1.211 | 250 | 3.255 |
| 25 | +0.171 | 150 | 1.559 | 275 | 3.740 |
| 50 | 0.378 | 175 | 1.940 | 300 | 4.238 |
| 75 | 0.620 | 200 | 2.351 | 315 | 4.539 |
| 100 | 0.898 | 225 | 2.790 | | |

TABLE 474.—Thermal Electromotive Force of Nickel versus Platinum *
Temperature versus Electromotive Force

| °C | Intern. mv | °C | Intern. mv | °C | Intern. mv |
|-----|------------|-----|------------|------|------------|
| 0 | 0.000 | 400 | 5.450 | 800 | 9.350 |
| 25 | -0.350 | 425 | 5.580 | 825 | 9.675 |
| 50 | 0.710 | 450 | 5.745 | 850 | 10.010 |
| 75 | 1.090 | 475 | 5.960 | 875 | 10.350 |
| 100 | 1.485 | 500 | 6.165 | 900 | 10.695 |
| 125 | 1.880 | 525 | 6.360 | 925 | 11.045 |
| 150 | 2.285 | 550 | 6.585 | 950 | 11.400 |
| 175 | 2.695 | 575 | 6.800 | 975 | 11.765 |
| 200 | 3.105 | 600 | 7.040 | 1000 | 12.130 |
| 225 | 3.505 | 625 | 7.290 | 1025 | 12.500 |
| 250 | 3.890 | 650 | 7.550 | 1050 | 12.875 |
| 275 | 4.255 | 675 | 7.825 | 1075 | 13.250 |
| 300 | 4.590 | 700 | 8.105 | 1100 | 13.625 |
| 325 | 4.880 | 725 | 8.415 | | |
| 350 | 5.110 | 750 | 8.720 | | |
| 375 | 5.290 | 775 | 9.030 | | |

* Bur. Standards Journ. Res., 5, 1291, 1930.

TABLE 475.—Thermoelectric Properties at Low Temperatures

(Borelius, Keesom, Johansson, Linde, Com. Phys. Lab. Leiden, no. 206, 1930.)

Thermoelectric Force in Microvolts per °K. against Silver Alloy

| °C | Cu | Ag | Au | Pd | Pt | Fe | Pb |
|------|-------|-------|-------|--------|-------|-------|-------|
| -255 | +0.07 | -0.10 | -1.20 | +0.75 | +1.54 | +0.05 | -1.06 |
| -240 | 0.45 | +0.37 | -0.05 | 2.10 | 3.60 | 1.40 | -1.19 |
| -220 | 0.90 | 0.30 | +0.24 | 3.40 | 5.24 | 4.80 | -1.25 |
| -200 | 0.89 | 0.31 | 0.30 | 3.48 | 5.40 | 8.45 | -1.29 |
| -180 | 0.72 | 0.25 | 0.30 | 2.14 | 4.36 | 11.5 | -1.33 |
| -160 | 0.61 | 0.22 | 0.33 | 0.54 | 3.02 | 14.0 | -1.42 |
| -140 | 0.52 | 0.21 | 0.37 | -1.06 | 1.72 | 15.8 | -1.54 |
| -120 | 0.47 | 0.20 | 0.40 | -2.52 | 0.50 | 16.9 | -1.67 |
| -100 | 0.44 | 0.20 | 0.44 | -3.92 | -0.70 | 17.5 | -1.79 |
| -80 | 0.45 | 0.20 | 0.47 | -5.27 | -1.76 | 17.5 | -1.92 |
| -60 | 0.47 | 0.20 | 0.51 | -6.52 | -2.80 | 17.3 | -2.05 |
| -40 | 0.49 | 0.20 | 0.55 | -7.80 | -3.80 | 16.9 | -2.17 |
| -20 | 0.51 | 0.20 | 0.58 | -9.05 | -4.72 | 16.2 | -2.29 |
| 0 | 0.53 | 0.21 | 0.62 | -10.32 | -5.62 | 15.8 | -2.42 |
| +20 | 0.56 | 0.22 | 0.65 | -11.6 | -6.56 | 15.3 | -2.54 |

TABLE 476.—Thomson Effect in Microvolts per Degree

| °K. | Cu | Ag | Au | Pd | Pt | Fe | Ni | Co | Pb |
|-----|-------|-------|-------|-------|-------|------|-------|-------|-------|
| 20 | +0.59 | +1.40 | +2.83 | +1.9 | +3.2 | +1.3 | ... | ... | |
| 25 | 1.04 | 1.23 | 2.09 | 2.6 | 3.6 | 2.7 | ... | ... | |
| 30 | 1.22 | 0.85 | 1.58 | 3.1 | 3.9 | 4.1 | -4.5 | -0.2 | 0.00 |
| 40 | 1.03 | 0.24 | 0.88 | 3.2 | 3.8 | 6.7 | -5.4 | -0.3 | -0.04 |
| 50 | 0.67 | -0.02 | 0.45 | 2.5 | 2.7 | 9.0 | -5.0 | -0.8 | -0.06 |
| 60 | 0.18 | -0.17 | 0.19 | 1.0 | 1.0 | 10.8 | -4.5 | -2.0 | -0.09 |
| 70 | -0.29 | -0.24 | 0.07 | -1.5 | -1.1 | 11.9 | -4.1 | -3.7 | -0.12 |
| 80 | -0.46 | -0.25 | 0.05 | -4.6 | -3.3 | 12.6 | -4.0 | -5.5 | -0.15 |
| 90 | -0.48 | -0.17 | 0.17 | -6.6 | -5.1 | 12.9 | -4.0 | -7.0 | -0.18 |
| 100 | -0.45 | -0.03 | 0.32 | -7.8 | -6.5 | 13.0 | -4.5 | -8.4 | -0.20 |
| 110 | -0.37 | +0.12 | 0.45 | -8.7 | -7.5 | 13.0 | -5.3 | -9.8 | -0.23 |
| 120 | -0.26 | 0.25 | 0.56 | -9.3 | -8.0 | 12.8 | -6.4 | -11.1 | -0.26 |
| 130 | -0.13 | 0.35 | 0.66 | -9.7 | -8.2 | 12.2 | -7.4 | -12.4 | -0.29 |
| 140 | +0.02 | 0.44 | 0.75 | -10.1 | -8.2 | 11.0 | -8.3 | -13.5 | -0.32 |
| 150 | 0.17 | 0.52 | 0.83 | -10.3 | -8.3 | 8.9 | -9.0 | -14.6 | -0.34 |
| 160 | 0.31 | 0.59 | 0.91 | -10.6 | -8.4 | 6.1 | -9.7 | -15.7 | -0.37 |
| 170 | 0.46 | 0.66 | 0.99 | -10.9 | -8.5 | 2.6 | -10.3 | -16.7 | -0.40 |
| 180 | 0.59 | 0.72 | 1.06 | -11.2 | -8.7 | -0.2 | -10.9 | -17.6 | -0.42 |
| 200 | 0.79 | 0.84 | 1.19 | -12.1 | -9.1 | -3.5 | -12.1 | -19.6 | -0.46 |
| 220 | 0.96 | 0.96 | 1.31 | -13.3 | -9.8 | -4.5 | -13.3 | -21.5 | -0.49 |
| 240 | 1.10 | 1.08 | 1.43 | -14.6 | -10.6 | -4.8 | -14.5 | -23.4 | -0.52 |
| 260 | 1.24 | 1.20 | 1.54 | -15.8 | -11.4 | -5.2 | -15.7 | -25.4 | -0.54 |
| 280 | 1.38 | 1.32 | 1.66 | -17.0 | -12.3 | -5.6 | | | -0.55 |
| 300 | +1.52 | +1.44 | +1.77 | -18.2 | -13.2 | -5.9 | | | -0.57 |

TABLE 477.—Peltier Effect

The coefficient of Peltier effect may be calculated from the constants A and B of Table 467, as there shown. With Q (see Table 467) in microvolts per °C and T = absolute temperature (K), the coefficient of Peltier effect= $\frac{QT}{42}$ cal. per coulomb= $0.00086 QT$ cal. per ampere-hour= $QT/1000$ millivolts (=millijoules per coulomb). Experimental results, expressed in slightly different units, are here given. The figures are for the heat production at a junction of copper and the metal named, in calories per ampere-hour. The current flowing from copper to the metal named, a positive sign indicates a warming of the junction. The temperature not being stated by either author, and Le Roux not giving the algebraic signs, these results are not of great value.

| Calories per ampere-hour. | | | | | | | | | | | |
|---------------------------|-------|-----------------|-----------|-------|------|----------------|-------|------|------|------|------|
| | Sb. ‡ | Sb. commercial. | Bi. pure. | Bi. § | Cd. | German Silver. | Fe. | Ni. | Pt. | Ag. | Zn. |
| Jahn* | - | - | - | - | -.62 | - | -3.61 | 4.36 | 0.32 | -.41 | -.58 |
| Le Roux† | 13.02 | 4.8 | 19.1 | 25.8 | 0.46 | 2.47 | 2.5 | - | - | - | .39 |

* "Wied. Ann." vol. 34, p. 767.

† "Ann. de Chim. et de Phys." (4) vol. 10, p. 201.

‡ Becquerel's antimony is 866 parts Sb + 406 parts Zn + 121 parts Bi.

§ Becquerel's bismuth is 10 parts Bi + 1 part Sb.

TABLE 478.—Peltier Effect, Fe-Constantan, Ni-Cu, 0° — 560°C

| Temperature. | 0° | 20° | 130° | 240° | 320° | 560° | g. cal. $\times 10^{-3}$ per coulomb. |
|---------------------|------|------|------|------|------|------|--|
| Fe-Constantan . . . | 3.1 | 3.6 | 4.5 | 6.2 | 8.2 | 12.5 | |
| Ni-Cu | 1.92 | 2.15 | 2.45 | 2.06 | 1.91 | 2.38 | |

TABLE 479.—Peltier Electromotive Force in Millivolts

| Metal against Copper. | Sb. | Fe. | Cd. | Zn. | Ag. | An. | Pb. | Sn. | Al. | Pt. | Pd. | Ni. | Bi. |
|-----------------------|-------|-------|------|------|------|------|-------|-------|------|-------|-------|-------|-------|
| Le Roux . | -5.54 | -2.93 | -.53 | -.45 | - | - | - | - | - | - | - | - | +22.3 |
| Jahn . . . | - | -3.68 | -.72 | -.68 | -.48 | - | - | - | - | +3.37 | - | +5.07 | - |
| Edlund . . | - | -2.96 | -.16 | -.01 | +.03 | +3.3 | +5.50 | +5.56 | +7.0 | +1.02 | +2.17 | - | +17.7 |
| Caswell . . | - | - | - | - | +.03 | - | - | - | +7.0 | +8.5 | - | +6.0 | +16.1 |

Le Roux, 1867; Jahn, 1888; Edlund, 1870-71; Caswell, Phys. Rev. 33, p. 381, 1911.

TABLE 480.—Thermoelectric Power; Pressure Effects

The following values of the thermoelectric powers under various pressures are taken from Bridgman, *Pr. Am. Acad. Arts and Sc.* 53, p. 269, 1918. A positive emf means that the current at the hot junction flows from the uncompressed to the compressed metal. The cold junction is always at 0° C. The last two columns give the constants in the equation $E = \text{thermoelectric force against lead (0° to 100° C)} = (At + Bt^2) \times 10^{-6}$ volts, at atmospheric pressure, a positive emf meaning that the current flows from lead to the metal under consideration at the hot junction.

| Metal. | Thermo-electric force, volts $\times 10^9$ | | | | | | | | | | Formula coefficients. | |
|--------------|--|--------|---------|---------|---------|---------|---------|---------|---------|---------|------------------------|--|
| | Pressure, kg/cm ² | | | | | | | | | | | |
| | 2000 | | 4000 | | 8000 | | 12,000 | | | | | |
| | Temperature, ° C | | | | | | | | | | | |
| | 50° | 100° | 50° | 100° | 50° | 100° | 20° | 50° | 100° | A | B | |
| Bi † | 53,000 | 85,000 | 110,000 | 185,000 | 255,000 | 425,000 | 185,000 | 452,000 | 710,000 | -74.42 | + .0160 | |
| Zn † | 6,200 | 14,100 | 13,000 | 28,500 | 26,100 | 58,100 | 14,400 | 38,500 | 87,400 | +3.047 | -.00495 | |
| Tl † | 4,930 | 10,870 | 9,380 | 20,200 | 17,170 | 37,630 | 8,780 | 23,750 | 52,400 | +1.659 | -.00134 ¹ | |
| Cd † | 2,040 | 7,120 | 4,620 | 14,380 | 10,060 | 28,740 | 6,680 | 10,180 | 45,500 | +12.002 | + .1610 | |
| Constantan † | 2,850 | 5,050 | 5,800 | 11,810 | 11,530 | 23,700 | 6,750 | 17,200 | 35,470 | -34.76 | -.0307 | |
| Pd * | 2,100 | 4,380 | 4,400 | 8,800 | 8,630 | 17,600 | 5,000 | 12,070 | 20,520 | -5.496 | -.01760 | |
| Pt * | 1,810 | 3,600 | 3,600 | 7,310 | 7,370 | 14,350 | 3,880 | 11,030 | 21,570 | -3.002 | -.01334 | |
| W † | 1,100 | 2,530 | 2,360 | 4,090 | 4,060 | 10,120 | 2,700 | 7,050 | 15,140 | +1.594 | + .01705 | |
| Ni * | 700 | 1,680 | 1,500 | 3,400 | 3,230 | 7,100 | 1,880 | 5,140 | 11,440 | -17.61 | -.0178 | |
| Ag * | 810 | 1,870 | 1,720 | 3,720 | 3,350 | 7,100 | +1,000 | 4,950 | 10,500 | +2.556 | + .00432 | |
| § Fe † | 300 | 1,670 | 590 | 3,250 | 5,300 | 5,820 | -900 | 220 | 7,680 | +16.18 | -.00890 ² | |
| Pb † | 460 | 1,050 | 920 | 2,120 | 1,860 | 4,210 | +880 | 281 | 6,310 | — | — | |
| Au * | 456 | 1,052 | 905 | 2,051 | 1,791 | 3,071 | +900 | 2,627 | 5,760 | +2.800 | + .00467 ³ | |
| Cu † | +292 | 584 | +580 | 1,216 | 1,124 | 2,420 | +506 | 1,616 | 3,546 | +2.777 | + .00483 | |
| § Al † | -70 | 101 | -91 | 294 | 32 | 929 | -68 | 312 | 1,962 | -0.416 | + .00008 ⁴ | |
| § Mo † | +93 | 140 | +187 | 278 | 375 | 555 | +146 | 562 | 833 | +5.892 | + .02167 ⁵ | |
| § Sn † | +38 | +87 | +58 | +165 | +70 | +292 | -182 | +10 | +390 | -0.230 | -.00667 | |
| Manganin † | -123 | -232 | -242 | -452 | -480 | -804 | -308 | -710 | -1,314 | +1.366 | + .000414 ⁶ | |
| Mg † | -84 | -167 | -181 | -362 | -395 | -701 | -250 | -648 | -1,296 | -0.095 | + .00004 | |
| Co † | -156 | -348 | -316 | -692 | -630 | -1,360 | -352 | -937 | -2,061 | -17.32 | -.0390 | |

* Identical wire of Table 485. † Another wire of same sample. ‡ Different sample.
§ Results too irregular for interpolation for values at other temperature and pressures; see original article.
(1) $-.0556^{\mu}$; (2) $-.0486^{\mu}$, annealed ingot iron; (3) $-.05166^{\mu}$; (4) $-.041^{\mu}$; (5) $-.0425^{\mu}$; (6) $-.04112^{\mu}$.

* Identical wire of Table 485. † Another wire of same sample. ‡ Different sample.

§ Results too irregular for interpolation for values at other temperature and pressures; see original article.

(1) -0.056⁶; (2) -0.86⁶, annealed ingot iron; (3) -0.0166⁶; (4) -0.041⁶; (5) -0.0425⁶; (6) -0.0412⁶.

TABLE 481.—Peltier and Thomson Heats; Pressure Effects

The following data indicate the magnitude of the effect of pressure on the Peltier and Thomson heats. They refer to the same samples as for the last table. The Peltier heat is considered positive if heat is absorbed by the positive current from the surroundings on flowing from uncompressed to compressed metal. A positive d^2E/dt^2 means a larger Thomson heat in the compressed metal, and the Thomson heat is itself considered positive if heat is absorbed by the positive current in flowing from cold to hot metal. Same reference and notes as for preceding table.

| Metal. | Peltier heat, 10 ⁸ × Joules/coulomb. | | | | | | Thomson heat, 10 ⁸ × Joules/coulomb/° C | | | | | |
|--------------|--|-------|------|--------|-------|------|---|------|------|--------|------|------|
| | Pressure kg/cm ² | | | | | | Pressure kg/cm ² | | | | | |
| | 6000 | | | 12,000 | | | 6000 | | | 12,000 | | |
| | Temperature ° C | | | | | | Temperature ° C | | | | | |
| | 0° | 50° | 100° | 0° | 50° | 100° | 0° | 50° | 100° | 0° | 50° | 100° |
| § Bi† | +1070 | +1210 | — | +2580 | +2810 | — | +1150 | +650 | — | -520 | -405 | — |
| Zn† | +98 | +140 | +100 | +100 | +278 | +412 | +41 | +48 | +56 | +63 | +133 | +220 |
| Tl† | +66 | +95 | +121 | +112 | +171 | +220 | +38 | +28 | +26 | +79 | +63 | +50 |
| Cd† | +19 | +71 | +118 | +81 | +148 | +221 | +100 | +74 | +63 | +105 | +92 | +93 |
| Constantan † | +40 | +57 | +70 | +90 | +114 | +140 | +5 | +6 | +6 | +13 | +14 | +17 |
| Pd * | +35 | +43 | +52 | +68 | +86 | +103 | +3 | +4 | +4 | +9 | +9 | +8 |
| Pt * | +23 | +37 | +35 | +45 | +76 | +65 | +40 | -6 | -18 | +96 | +17 | +59 |
| W † | +17 | +25 | +32 | +36 | +40 | +65 | +8 | +7 | +6 | +9 | +14 | +20 |
| Ni * | +11 | +17 | +23 | +24 | +37 | +50 | +9 | +7 | +8 | +16 | +15 | +10 |
| Ag * | +13 | +17 | +23 | +25 | +34 | +44 | +4 | +5 | +6 | +7 | +8 | +10 |
| § Fe† | -11 | -18 | -15 | -38 | +38 | +36 | +79 | +58 | -121 | -347 | +120 | -194 |
| Pb† | +7 | +10 | +16 | +14 | +20 | +30 | +2 | +6 | +10 | +6 | +8 | +20 |
| Au * | +6 | +10 | +11 | +13 | +18 | +25 | +4 | +4 | +5 | +6 | +6 | +7 |
| Cu† | +4 | +6 | +8 | +8 | +11 | +16 | +1 | +1 | +1 | +6 | +3 | +8 |
| Al† | -2 | +2 | +8 | +3 | +7 | +17 | +6 | +9 | +11 | +21 | +10 | +20 |
| Mo† | -1 | +2 | +0 | +2 | +4 | +1 | -1 | -5 | -1 | +2 | -11 | -2 |
| § Sn† | -1 | +1 | +1 | -5 | +2 | +2 | +6 | +0 | -1 | +20 | +2 | -5 |
| Manganin † | -2 | -2 | -2 | -4 | -4 | -4 | +1 | +1 | +0 | +2 | +1 | +1 |
| Mg† | -16 | -18 | -21 | -35 | -42 | -48 | 0 | 0 | 0 | 0 | 0 | 0 |
| § Co† | -23 | -33 | -44 | -46 | -67 | -90 | -14 | -11 | -10 | -20 | -24 | -28 |

* † ‡ § Same significance as in preceding table.

TABLE 482

THE TRIBO-ELECTRIC SERIES

In the following table it is so arranged that any material in the list becomes positively electrified when rubbed by one lower in the list. The phenomenon depends upon surface conditions and circumstances may alter the relative positions in the list.

| | | |
|--------------------------------|------------------------------|---------------------------------|
| 1 Asbestos (sheet). | 13 Silk. | 24 Amber. |
| 2 Rabbit's fur, hair, (Hlg). | 14 Al, Mn, Zn, Cd, Cr, felt, | 25 Slate, chrome-alum. |
| 3 Glass (combn. tubing). | hand, wash-leather. | 26 Shellac, resin, sealing-wax. |
| 4 Vitreous silica, opossum's | 15 Filter paper. | 27 Ebonite. |
| fur. | 16 Vulcanized fiber. | 28 Co, Ni, Sn, Cu, As, Bi, |
| 5 Glass (fusen.). | 17 Cotton. | Sb, Ag, Pd, C, Te, Eu- |
| 6 Mica. | 18 Magnalium. | reka, straw, copper sul- |
| 7 Wool. | 19 K-alum, rock-salt, satin | phate, brass. |
| 8 Glass (pol.), quartz (pol.), | spar. | 29 Para rubber, iron alum. |
| glazed porcelain. | 20 Woods, Fe. | 30 Guttapercha. |
| 9 Glass (broken edge), | 21 Unglazed porcelain, sal- | 31 Sulphur. |
| ivory. | ammoniac. | 32 Pt, Ag, Au. |
| 10 Calcite. | 22 K-bichromate, paraffin, | 33 Celluloid. |
| 11 Cat's fur. | tinned-Fe. | 34 Indiarubber. |
| 12 Ca, Mg, Pb, fluor spar. | 23 Cork, ebony. | |
| borax. | | |

Shaw, Pr. Roy. Soc. 94, p. 16, 1917; the original article shows the alterations in the series sequence due to varied conditions.

TABLE 483

AUXILIARY TABLE FOR COMPUTING WIRE RESISTANCES

For computing resistance in ohms per meter from resistivity, ρ , in microns per cm. cube (see Table 484, etc.). *e. g.* to compute for No. 23 copper wire when $\rho = 1.724$: 1 meter = $0.0387 + .0271 + .0008 + .0002 = 0.0668$ ohms; for No. 11 lead wire when $\rho = 20.4$: 1 meter = $0.0479 + .0010 = 0.0489$ ohms. The following relation allows computation for wires of other gage numbers: resistance in ohms per meter of No. $N = 2(\mu - 3)$ within 1%: *e. g.* resistance of meter of No. 18 = $2 \times$ No. 15.

| Gage No. | Diam. in mm. | Section mm ² . | ρ in micro-ohms per cm. cube. | | | | | | | | | |
|----------|--------------|---------------------------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. | 10. |
| | | | Resistance of wire 1 meter long in ohms. | | | | | | | | | |
| 0000 | 11.7 | 107.2 | .04933 | .03187 | .02280 | .01373 | .00466 | .00560 | .00653 | .00746 | .00840 | .00933 |
| 00 | 9.27 | 67.43 | .03148 | .02297 | .01445 | .00593 | .00742 | .00890 | .0104 | .0119 | .0133 | .0148 |
| 1 | 7.35 | 42.41 | .02236 | .01472 | .00707 | .00943 | .0118 | .0141 | .0165 | .0189 | .0212 | .0236 |
| 3 | 5.83 | 26.67 | .01375 | .00750 | .00912 | .01150 | .01387 | .01625 | .01862 | .02100 | .02337 | .02575 |
| 5 | 4.62 | 16.77 | .00596 | .00719 | .00799 | .00923 | .00998 | .01122 | .01246 | .01370 | .01494 | .01618 |
| 7 | 3.66 | 10.55 | .00408 | .00490 | .00584 | .00679 | .00774 | .00869 | .00964 | .01059 | .01154 | .01249 |
| 9 | 2.91 | 6.634 | .00251 | .00301 | .00352 | .00403 | .00454 | .00505 | .00556 | .00607 | .00658 | .00709 |
| 11 | 2.30 | 4.172 | .00240 | .00279 | .00319 | .00359 | .00399 | .00439 | .00479 | .00519 | .00559 | .00599 |
| 13 | 1.83 | 2.624 | .00381 | .00476 | .00571 | .00666 | .00761 | .00856 | .00951 | .01046 | .01141 | .01236 |
| 15 | 1.45 | 1.650 | .00606 | .00721 | .00836 | .00951 | .01066 | .01181 | .01296 | .01411 | .01526 | .01641 |
| 17 | 1.15 | 1.038 | .00963 | .01133 | .01303 | .01473 | .01643 | .01813 | .01983 | .02153 | .02323 | .02493 |
| 19 | .912 | .6527 | .0153 | .0186 | .0219 | .0252 | .0285 | .0318 | .0351 | .0384 | .0417 | .0450 |
| 21 | .723 | .4105 | .0244 | .0297 | .0350 | .0403 | .0456 | .0509 | .0562 | .0615 | .0668 | .0721 |
| 23 | .573 | .2582 | .0387 | .0475 | .0563 | .0651 | .0739 | .0827 | .0915 | .1003 | .1091 | .1179 |
| 25 | .455 | .1624 | .0616 | .0752 | .0888 | .1024 | .1160 | .1296 | .1432 | .1568 | .1704 | .1840 |
| 27 | .361 | .1021 | .0979 | .1199 | .1419 | .1639 | .1859 | .2079 | .2299 | .2519 | .2739 | .2959 |
| 29 | .286 | .0642 | .1557 | .1877 | .2197 | .2517 | .2837 | .3157 | .3477 | .3797 | .4117 | .4437 |
| 31 | .227 | .0474 | .2476 | .2952 | .3428 | .3904 | .4380 | .4856 | .5332 | .5808 | .6284 | .6760 |
| 33 | .180 | .0254 | .3937 | .4784 | .5631 | .6478 | .7325 | .8172 | .9019 | .9866 | .1071 | .1186 |
| 35 | .143 | .0160 | .6262 | .7752 | .9242 | .1073 | .1224 | .1375 | .1526 | .1677 | .1828 | .1979 |
| 37 | .113 | .0100 | .9950 | .1220 | .1450 | .1680 | .1910 | .2140 | .2370 | .2600 | .2830 | .3060 |
| 39 | .090 | .0063 | 1.583 | .1966 | .2399 | .2832 | .3265 | .3698 | .4131 | .4564 | .4997 | .5430 |
| 40 | .080 | .0050 | 1.996 | .2492 | .2985 | .3478 | .3971 | .4464 | .4957 | .5450 | .5943 | .6436 |

RESISTIVITY OF METALS AND SOME ALLOYS

The resistivities are the values of ρ in the equation $R = \rho l/s$, where R is the resistance in microhms of a length l cm of uniform cross section s cm². The temperature coefficient is a_s in the formula $R_t = R_s[1 + a_s(t - t_s)]$. The information of column 2 does not necessarily apply to the temperature coefficient. See also next table for temperature coefficients α° to 100°C , also page 413 for values on metals of high purity.

| Substance | Remarks | Temperature °C | Microhm- cm | Refer- ence | Temperature coefficient | | |
|--------------------|---------------------|-------------------|----------------|----------------|-------------------------|-----------|----------------|
| | | | | | t_s | a_s | Refer- ence |
| Advance..... | see constantan | — | — | — | — | — | — |
| Aluminum..... | see p. 421 | 20 | 2.828 | 1 | 18° | — | — |
| "..... | " | -189 | .64 | 3 | 25 | + .0039 | 2 |
| "..... | " | -100 | 1.53 | 3 | 100 | + .0034 | 4 |
| "..... | " | 0 | 2.62 | 3 | 500 | + .0040 | 4 |
| "..... | " | +100 | 3.86 | 3 | — | + .0050 | 4 |
| "..... | " | 400 | 8.0 | 3 | — | — | — |
| Antimony..... | — | — | 39.1 | 30 | 20 | + .0036 | 5 |
| "..... | — | -190 | 10.5 | 6 | — | — | — |
| "..... | liquid | +860 | 120 | 7 | — | — | — |
| Arsenic..... | — | — | 35 | 8 | — | — | — |
| Beryllium..... | — | 20 | 10.1 | 31 | — | — | — |
| Bismuth..... | — | 18 | 119.0 | 9 | 20 | + .004 | 5 |
| "..... | — | 100 | 160.2 | 9 | — | — | — |
| Brass..... | — | 20 | 7 | 5 | 20 | + .002 | 5 |
| Cadmium..... | drawn | -160 | 2.72 | 10 | 20 | + .0038 | 5 |
| "..... | " | 18 | 7.54 | 9 | — | — | — |
| "..... | " | 100 | 9.82 | 9 | — | — | — |
| "..... | liquid | 318 | 34.1 | 11 | — | — | — |
| Cæsium..... | — | -187 | 5.25 | 12 | — | — | — |
| "..... | — | — | 19 | 11 | — | — | — |
| "..... | solid } liquid } | 27 | 22.2 | 13 | — | — | — |
| Calcium..... | 99.57 pure | 30 | 36.6 | 13 | — | — | — |
| Calido..... | see constantan | 20 | 4.59 | 14 | — | + .0036 | 14 |
| Chromium..... | — | 0 | 2.6 | 15 | — | — | — |
| Climax..... | — | 20 | 87 | 5 | 20 | + .0007 | 5 |
| Cobalt..... | 99.8 pure | 20 | 9.7 | 16 | — | — | — |
| Constantan..... | 60% Cu, 40% Ni | 20 | 49 | 5 | 12 | + .000008 | 4 |
| "..... | — | — | — | — | 25 | + .000002 | 4 |
| "..... | — | — | — | — | 100 | + .000033 | 4 |
| "..... | — | — | — | — | 200 | + .000020 | 4 |
| "..... | — | — | — | — | 500 | + .000027 | 4 |
| Copper..... | annealed | 20 | 1.724 | 1 | 20 | + .00393 | 5 |
| "..... | hard-drawn | 20 | 1.77 | 1 | " | + .00382 | 5 |
| "..... | electrolytic | -206 | .144 | 17 | 100 | + .0038 | 4 |
| "..... | " | +205 | 2.92 | 17 | 400 | + .0042 | 4 |
| "..... | pure | 400 | 4.10 | 3 | 1000 | + .0062 | 4 |
| "..... | very pure, ann'd | 20 | 1.692 | 18 | — | — | — |
| Eureka..... | see constantan | — | — | — | — | — | — |
| Excello..... | — | 20 | 92 | 5 | 20 | + .00016 | 5 |
| Gallium..... | — | 0 | 53 | 12 | — | — | — |
| German silver..... | 18% Ni | 20 | 33 | 5 | 20 | + .0004 | 5 |
| Germanium..... | — | 0 | 89000. | 32 | — | — | — |
| Gold..... | 99.9 pure | -183 | .68 | 17 | 20 | + .0034 | 5 |
| "..... | — | 0 | 2.22 | 11 | 100 ann'd | + .0025 | 4 |
| "..... | pure, drawn | 20 | 2.44 | 9 | 500 | + .0035 | 4 |
| "..... | 99.9 pure | 194.5 | 3.77 | 17 | 1000 | + .0049 | 4 |
| Ia Ia..... | see constantan | — | — | — | — | — | — |
| Ideal..... | " | — | — | — | — | — | — |
| Indium..... | — | 0 | 8.37 | 19 | — | — | — |
| Iridium..... | — | -186 | 1.92 | 20 | — | — | — |
| "..... | — | 0 | 6.10 | 20 | — | — | — |
| "..... | — | +100 | 8.3 | 20 | — | — | — |

Arranged in Order of Increasing Resistivity (ohm-cm³×10⁻⁶, 20°C)

| | | | | | | | |
|----|-------|----|-------|----|--------|----------|----------------------|
| Ag | 1.468 | Mn | 5. ± | Pd | 10.21 | Ga | 53 |
| Cu | 1.59 | Mo | (5.3) | Pt | 10.96 | Os | 56 |
| Au | 2.22 | Zn | 5.75 | Rb | 13 | Hg | 94.07 |
| Al | 2.6 | Ir | 6.10 | Sn | 13 | Bi | 110 |
| Cr | 2.6 | K | 6.1 | Ta | 14.6 | Graphite | 8 × 10 ² |
| Ti | 3.2 | Ni | 6.93 | Tl | 17.6 | Carbon | 3 × 10 ³ |
| Na | 4.3 | Cd | 7.04 | Cs | 19 | Te | 2 × 10 ⁵ |
| Ca | 4.3 | In | 8.37 | Pb | 20.4 | P | 10 ¹² |
| Mg | 4.35 | Li | 8.55 | Sr | (23.5) | B | 8 × 10 ¹² |
| Rh | 4.69 | Fe | 8.8 | As | 35 | Se | 10 ¹³ |
| W | 5 | Co | 9 | Sb | 39 | S | 10 ¹⁷ |

RESISTIVITY OF METALS AND SOME ALLOYS

| Substance | Remarks | Temperature °C | Microhm- cm | Refer- ence | Temperature coefficient | | |
|-------------|--------------------|-------------------|----------------|----------------|-------------------------|-----------|----------------|
| | | | | | t_s | a_s | Refer- ence |
| Iron | 99.98% pure | 20 | 10 | 5 | 20 | +0.0050 | 5 |
| " | pure, soft | -205.3 | .652 | 17 | 0 | + .0062 | 21 |
| " | " | - 78 | 5.32 | 17 | 25 | + .0052 | 4 |
| " | " | 0 | 8.85 | 17 | 100 | + .0068 | 4 |
| " | " | + 98.5 | 17.8 | 17 | 500 | + .0147 | 4 |
| " | " | 106.1 | 21.5 | 17 | 1000 | + .0050 | 4 |
| " | " | 400 | 43.3 | 3 | — | — | — |
| " | electrolytic | 0 | 10.0 | 34 | — | — | — |
| " | " | 100 | 14.41 | 34 | — | — | — |
| steel | E. B. B. | 20 | 10.4 | 5 | 20 see col. 2 | + .005 | 5 |
| " | B. B. | 20 | 11.9 | 5 | " " " " | + .004 | 5 |
| " | Siemens-Martin | 20 | 18 | 5 | " " " " | + .003 | 5 |
| " | manganese | 20 | 70 | 5 | " " " " | + .001 | 5 |
| " | 35% Ni, "invar." | 20 | 81 | 22 | — | — | — |
| " | piano wire | 0 | 11.8 | 23 | 0 see col. 2 | + .0032 | 23 |
| " | temp. glass, hard | 0 | 45.7 | 23 | " see col. 2 | + .0016 | 23 |
| " | " , yellow | 0 | 27 | 23 | — | — | — |
| " | " , blue | 0 | 20.5 | 23 | 0 see col. 2 | + .0033 | 23 |
| " | " , soft | 0 | 15.9 | 23 | — | — | — |
| Lead | " | 20 | 22 | 5 | 20 | + .0030 | 5 |
| " | cold pressed | -183 | 6.02 | 17 | 18 | + .0043 | 2 |
| " | " | - 78 | 14.1 | 17 | — | — | — |
| " | " | 0 | 10.8 | 33 | — | — | — |
| " | " | + 90.4 | 28 | 17 | — | — | — |
| " | " | 106.1 | 36.9 | 17 | — | — | — |
| " | " | 318 | 94 | 24 | — | — | — |
| Lithium | solid | -187 | 1.34 | 12 | — | — | — |
| " | " | 0 | 8.55 | 12 | — | — | — |
| " | " | 99.3 | 12.7 | 12 | — | — | — |
| " | liquid | 230 | 45.2 | 25 | — | — | — |
| Magnesium | " | 20 | 4.6 | 5 | 20 | + .004 | 5 |
| " | free from Zn | -183 | 1.00 | 17 | 0 | + .0038 | 24 |
| " | " | - 78 | 2.97 | 17 | 25 | + .0050 | 4 |
| " | " | 0 | 4.35 | 17 | 100 | + .0045 | 4 |
| " | " | + 98.5 | 5.99 | 17 | 500 | + .0036 | 4 |
| " | pure | 400 | 11.9 | 3 | 600 | + .0100 | 4 |
| Manganese | " | — | 5.0 ± | 15 | — | — | — |
| Manganin | 84 Cu, 12 Mn, 4 Ni | 20 | 44 | 5 | 12 | + .000006 | 4 |
| " | " | — | — | — | 25 | .000000 | 4 |
| " | " | — | — | — | 100 | — .000042 | 4 |
| " | " | — | — | — | 250 | — .000052 | 4 |
| " | " | — | — | — | 475 | — .000000 | 4 |
| " | " | — | — | — | 500 | — .00011 | 4 |
| Mercury | " | 20 | 95.783 | 5 | 20 | + .00089 | 5 |
| " | solid | -183.5 | 6.97 | 17 | 0 | + .00088 | 26 |
| " | " | -102.0 | 15.04 | 17 | — | — | — |
| " | " | - 50.3 | 21.3 | 17 | $R_t = R(1 +$ | — | — |
| " | " | - 39.2 | 25.5 | 17 | .00089t + | — | — |
| " | liquid | - 36.1 | 80.6 | 17 | .000001t ²) | — | — |
| " | " | 0 | 94.07 | 17 | — | — | — |
| " | " | 50 | 98.50 | 27 | — | — | — |
| " | " | 100 | 103.25 | 24 | — | — | — |
| " | " | 200 | 114.27 | 24 | — | — | — |
| " | " | 350 | 135.5 | 24 | — | — | — |
| Molybdenum | very pure | 0 | 5.14 | 35 | 25 | + .0033 | 4 |
| " | " | — | — | — | 100 | + .0034 | 4 |
| " | " | — | — | — | 1000 | + .0048 | 4 |
| Monel metal | " | 20 | 42 | 5 | 20 | + .0020 | 5 |
| Nichrome | " | 20 | 100 | 5 | 20 | + .0004 | 5 |
| Nickel | " | 20 | 7.8 | 5 | 20 | + .006 | 5 |
| " | very pure | 20 | 7.236 | 31 | — | — | — |
| " | pure | -182.5 | 1.44 | 28 | 0 | + .0062 | 24 |
| " | " | - 78.2 | 4.31 | 28 | 25 | + .0043 | 4 |
| " | " | 0 | 6.03 | 28 | 100 | + .0043 | 4 |
| " | " | 94.9 | 11.1 | 28 | 500 | + .0030 | 4 |
| " | " | — | — | — | 1000 | + .0037 | 4 |

RESISTIVITY OF METALS AND SOME ALLOYS

| Substance | Remarks | Temperature, °C | Microhm cm | Reference | Temperature coefficient | | |
|-----------------|--------------|--------------------|---------------|-----------|-------------------------|----------|-----------|
| | | | | | t_0 | a_0 | Reference |
| Osmium..... | — | 20 | 9.5 | 36 | — | — | — |
| Palladium..... | — | 20 | 11 | 5 | 20 | +0.0033 | 5 |
| "..... | very pure | -183 | 2.78 | 17 | 0 | +0.0035 | 21 |
| "..... | " " | -78 | 7.17 | 17 | — | — | — |
| "..... | " " | 0 | 10.21 | 17 | — | — | — |
| Platinum..... | — | 98.5 | 13.79 | 17 | — | — | — |
| "..... | wire | 0 | 9.83 | 31 | 20 | +0.003 | 5 |
| "..... | " | -203.1 | 2.44 | 17 | 0 | +0.0037 | 21 |
| "..... | " | -97.5 | 6.87 | 17 | — | — | — |
| "..... | " | 0 | 10.06 | 17 | — | — | — |
| "..... | " | 100 | 14.85 | 17 | — | — | — |
| "..... | " | 400 | 26 | 3 | — | — | — |
| Potassium..... | — | -75 | 4 | 13 | 0 | +0.0057 | 33 |
| "..... | — | 0 | 6.1 | 13 | — | — | — |
| "..... | — | 55 | 8.4 | 13 | — | — | — |
| Rhodium..... | — | -186 | 7.0 | 20 | — | — | — |
| "..... | — | -78.3 | 3.09 | 20 | — | — | — |
| "..... | — | 0 | 5.11 | 33 | 0 | +0.0043 | 33 |
| "..... | — | 100 | 6.60 | 20 | — | — | — |
| Rubidium..... | solid | -190 | 2.5 | 13 | — | — | — |
| "..... | " | 0 | 11.6 | 13 | — | — | — |
| "..... | liquid | 35 | 13.4 | 13 | — | — | — |
| Silicium..... | — | 40 | 19.6 | 13 | — | — | — |
| Silver..... | 99.98 pure | 20 | 58 ± | — | — | — | — |
| "..... | electrolytic | 18 | 1.629 | 2 | 20 | +0.0038 | 5 |
| "..... | " | -183 | 1.300 | 17 | 25 | +0.0030 | 4 |
| "..... | " | -78 | 1.021 | 17 | 100 | +0.0036 | 4 |
| "..... | " | 0 | 1.468 | 17 | 500 | +0.0044 | 4 |
| "..... | " | 98.15 | 2.062 | 17 | — | — | — |
| "..... | " | 102.1 | 2.608 | 17 | — | — | — |
| "..... | " | 400 | 3.77 | 17 | — | — | — |
| Sodium..... | solid | -180 | 1.0 | 3 | — | — | — |
| "..... | " | -75 | 2.8 | 13 | — | — | — |
| "..... | " | 0 | 4.3 | 13 | 0 | +0.0054 | 3 |
| "..... | " | 55 | 5.4 | 13 | — | — | — |
| "..... | liquid | 116 | 10.2 | 13 | — | — | — |
| Strontium..... | — | 20 | 24.8 | 8 | — | — | — |
| Tantalum..... | — | 20 | 15.5 | 5 | 20 | +0.0031 | 5 |
| Tellurium*..... | — | 10.6 | 200.000 | 8 | — | — | — |
| Thallium..... | pure | -183 | 4.08 | 17 | — | — | — |
| "..... | " | -78 | 11.8 | 17 | — | — | — |
| "..... | " | 0 | 17.60 | 17 | — | — | — |
| "..... | " | 98.5 | 24.7 | 17 | — | — | — |
| Therlo..... | — | 20 | 47 | 5 | 20 | +0.00001 | 5 |
| Tin..... | — | 20 | 11.5 | 5 | 20 | +0.0042 | 5 |
| "..... | — | -184 | 3.40 | 17 | — | — | — |
| "..... | — | -78 | 8.8 | 17 | — | — | — |
| "..... | — | 0 | 13 | 17 | — | — | — |
| "..... | — | 91.45 | 18.2 | 17 | — | — | — |
| Titanium..... | — | — | 3.2 | 15 | — | — | — |
| Tungsten..... | — | 20 | 5.51 | 29 | 18 | +0.0045 | 2 |
| "..... | 1000°K | 727 | 25.3 | 29 | 500 | +0.0057 | 4 |
| "..... | 1500°K | 1227 | 41.4 | 29 | 1000 | +0.0089 | 4 |
| "..... | 2000°K | 1727 | 59.4 | 29 | — | — | — |
| "..... | 3000°K | 2727 | 98.9 | 29 | — | — | — |
| "..... | 3500°K | 3227 | 118 | 29 | — | — | — |
| Zinc..... | trace Fe | -183 | 1.62 | 17 | 20 | +0.0037 | 5 |
| "..... | " " | -78 | 3.34 | 17 | — | — | — |
| "..... | " " | 0 | 5.75 | 17 | — | — | — |
| "..... | " " | 92.45 | 8 | 17 | — | — | — |
| "..... | " " | 191.5 | 10.37 | 17 | — | — | — |
| "..... | liquid | 440 | 37.2 | 7 | — | — | — |

References to Table 484: (1) See page 421. (2) Jäger, Diesselhorst, *Wiss. Abh. D. Phys. Tech. Reich.* 3, p. 269, 1900. (3) Nicolai, 1907. (4) Somerville, *Phys. Rev.* 31, p. 261, 1910; 33, p. 77, 1911. (5) Circular 74, Bureau of Standards, 1918. (6) Eucken, Gehlhoff. (7) De la Rive. (8) Matthiessen. (9) Jäger, Diesselhorst. (10) Lees, 1908. (11) Mean. (12) Guntz, Broniewski. (13) Hackspill. (14) Swisher, 1917. (15) Shukow. (16) Reichardt, 1901. (17) Dewar, Fleming, Dickson, 1898. (18) Wolff, Dellinger, 1910. (19) Erhardt, 1881. (20) Broniewski, Hackspill, 1911. (21) Dewar, Fleming, 1893, 1896. (22) Circular 58, Bureau of Standards, 1916. (23) Strouhal, Barus, 1883. (24) Vincentini, Onofei, 1890. (25) Bernini, 1905. (26) Glazebrook, *Phil. Mag.* 20, p. 343, 1885. (27) Grimaldi, 1888. (28) Fleming, 1900. (29) Langmuir, *Gen. Elec. Rev.* 19, 1916. (30) Eucken-Gehlhoff, 1912. (31) Wenner-Lindberg, I. C. T., 1929. (32) Bidwell, 1922. (33) Mean. (34) Gumlich. (35) Worthing, I. C. T., 1929. (36) Blau, 1905.

* See note to Table 467.

TABLE 485.—Resistance of Metals under Pressure (Bridgman)

The average temperature coefficients are per °C between 0° and 100° C. The instantaneous pressure coefficients are the values of the derivative $(1/r)\{dr/dp\}_t$, where r is the observed resistance at the pressure p and temperature t . The average coefficient is the total change of resistance between 0 and 12,000 kg/cm² divided by 12,000 and the resistance at atmospheric pressure and the temperature in question. Table taken from Proc. Nat. Acad. 3, p. 11, 1917. For coefficients at intermediate temperatures and pressures, see more detailed account in Proc. Amer. Acad. 52, p. 573, 1917. Sn, Cd, Zn, Kahlbaum's "K" grade; Ti, Bi, electrolytic, high purity; Pb, Ag, Au, Cu, Fe, Pt, of exceptional purity. Al better than ordinary, others only of high grade commercial purity.

| | Average temperature coefficient 0° to 100° C | | Pressure coefficients. | | | | | |
|---------|--|-----------------|----------------------------|-----------|-------------|-------------|--|-------------|
| | | | Instantaneous coefficient. | | | | Average coefficient 0 to 12,000 kg. cm ² | |
| | | | At 0° C | | At 100° C | | | |
| | At 0 kg | At 12,000 kg | 0 kg | 12,000 kg | 0 kg | 12,000 kg | At 0° | At 100° |
| In..... | + .00406 | + .00383 | — .041226 | — .041016 | — .041510 † | — .041072 † | — .041021 | — .041131 † |
| Sn..... | .00447 | .00411 | .041044 | .040036 | .041062 | .040973 | .040920 | .040951 |
| Tl..... | .00517 | .00499 | .041310 | .041180 | .041456 | .041200 | .041151 | .041226 |
| Cd..... | .00424 | .00418 | .041063 | .040837 | .041106 | .040887 | .040894 | .040927 |
| Pb..... | .00421 | .00412 | .041442 | .041220 | .041483 | .041237 | .041212 | .041253 |
| Zn..... | .00416 | .00420 | .040540 | .040425 | .040524 | .040407 | .040470 | .040454 |
| Al..... | .00434 | .00435 | .040116 | .040365 | .040397 | .040373 | .040382 | .040377 |
| Ag..... | .004974 | .004060 | .040358 | .040321 | .040355 | .040331 | .040333 | .040330 |
| Au..... | .003968 | .003964 | .040312 | .040286 | .040304 | .040292 | .040287 | .040292 |
| Cu..... | .004293 | .004303 | .040201 | .040179 | .040184 | .040175 | .040183 | .040177 |
| Ni..... | .004873 | .004855 | .040158 | .040142 | .040163 | .040156 | .040147 | .040158 |
| Co..... | .003657 | .003676 | .040094 | .040081 | .040076 | .040070 | .040057 | .040073 |
| Fe..... | .006206 | .006184 | .040241 | .040218 | .040247 | .040230 | .040246 | .040235 |
| Pd..... | .003178 | .003185 | .040198 | .040190 | .040189 | .040187 | .040190 | .040186 |
| Pt..... | .003868 | .003873 | .040198 | .040181 | .040190 | .040182 | .040187 | .040184 |
| Mo..... | .004336 | .004340 | .040133 | .040126 | .040130 | .040125 | .040120 | .040126 |
| Ta..... | .002973 | .002967 | .040149 | .040130 | .040153 | .040147 | .040143 | .040140 |
| W..... | .003219 | .003216 | .040128 | .040121 | .040130 | .040123 | .040123 | .040126 |
| Mg..... | .00390 * | — | .04055 | — | — | — | .04055 | — |
| Sb..... | .00473 | .00403 | + .041220 | + .041064 | + .040768 | + .040723 | + .041220 | + .040768 |
| Bi..... | + .00438 | + .00395 | + .04154 | + .040213 | + .04152 § | + .041895 § | + .042228 | + .041980 § |
| Te..... | — .0063 † | — | — .03129 | — | — | — | — | — |

* 0° to 20°.

† 0° to 24°.

‡ Extrapolated from 50°.

§ Extrapolated from 75°.

Additional data from P. Nat. Acad. Sc., 6, 505, 1920. Data are 10,000 × mean pressure coefficient, 0 — 12,000 kg, and 10,000 × instantaneous pressure coefficient at 0 kg. l = liquid; s = solid.

| | | | | | | | | |
|-------------|---------|--------|------------|---------|--------|--------------|----------|--------|
| Li, s, 0° | + .0772 | + .068 | Ca, 0° | + .106 | + .129 | Ti, 0° | ± .001 ? | |
| Li, l, 240° | + .093 | + .093 | Sr, 0° | + .080 | + .502 | Zr, 0° | — .0040 | — .004 |
| Na, s, 0° | — .345 | — .663 | Hg, s, 0° | — .236b | | Bi, l, 275° | — .101c | — .123 |
| Na, l, 200° | — .436 | — .922 | Hg, l, 25° | — .219 | — .334 | W, 0° | — .0135 | — .014 |
| K, s, 25° | — .604 | — 1.86 | Ga, s, 0° | — .0247 | | La, 0° | — .0331 | — .039 |
| K, l, 165° | — .809a | — 1.68 | Ga, l, 30° | — .0531 | — .064 | P, black, 0° | — .81 | — 2.00 |

a, 0 — 9,000 kg; b, 7,640 — 12,000 kg; c, 0 — 7,000 kg. The Ga, Na, K, Mg, Hg, Bi, W, P, of exceptional purity.

TABLE 486.—Resistance of Mercury and Manganin under Pressure

Mercury, pure and free from air and with proper precautions, makes a reliable secondary electric-resistance pressure gauge. For construction and manipulation see "The Measurement of High Hydrostatic Pressure; a Secondary Mercury Resistance Gauge," Bridgman, Pr. Am. Acad. 44, p. 221, 1919.

| Pressure, kg/cm ² | — | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 4000 | 5000 | 6000 | 6500 |
|------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| $R(p, -75^\circ)$ | 0.0186 | 0.0955 | 0.8030 | 0.8818 | 0.8714 | 0.8582 | 0.8478 | 0.8268 | 0.8076 | 0.7806 | 0.7807 |
| $R(p, 25^\circ)$ | 1.0000 | 0.8536 | 0.6824 | 0.9535 | 0.9394 | 0.9258 | 0.8882 | 0.8652 | 0.8438 | 0.8335 | |
| *..... | 1.0000 | 0.9854 | 0.9710 | 0.9588 | 0.9462 | 0.9342 | 0.9228 | 0.9010 | 0.8806 | 0.8616 | 0.8527 |
| $R(p, 125^\circ)$ | 1.0070 | 1.0770 | 1.0580 | 1.0400 | 1.0230 | 1.0070 | 0.9908 | 0.9614 | 0.9342 | 0.9086 | 0.8966 |

* This line gives the Specific Mass Resistance at 25°, the other lines the specific volume resistance.

The use of mercury as above has the advantage of being perfectly reproducible so that at any time a pressure can be measured without recourse to a fundamental standard. However, at 0° C mercury freezes at 7500 kg/cm². Manganin is suitable over a much wider range. Over a temperature range 0 to 50° C the pressure resistance relation is linear within 1/10 per cent of the change of resistance up to 13,000 kg/cm². The coefficient varies slightly with the sample. Bridgman's samples (German) had values of $(\Delta R/pR_0) \times 10^8$ from 2295 to 2325. These are + instead of —, as with most of the above metals. See "The Measurement of Hydrostatic Pressure up to 20,000 Kilograms per Square Centimeter," Bridgman, Pr. Am. Acad. 47, p. 321, 1911.

EFFECT OF TENSION ON THE RESISTANCE OF METALS

(Bridgman, Proc. Amer. Acad. Arts and Sci., 57, 41, 1922.)

Generally hydrostatic pressure decreases the electrical resistance of metals. A few are abnormal (see Table 485)—Bi, Li, Ca, Sr, Sb. Unit stress, kg/cm². The tension coefficient of specific resistance is obtained by subtracting $(1 + 2\sigma)/E$ from the coefficient of observed resistance.

| | Li | Ca | Sr | Sb | Bi | Mang. | Therlo | Co |
|---|-----|------|-------|------|-------|-------|--------|-------|
| Recip. Young's mod. $\times 10^6$ | 20 | 4.75 | 7.5 | 1.25 | 4.2 | 0.72 | 0.69 | 0.5 |
| Poisson ratio.... | .42 | .30 | .36 | .30? | .37 | .33 | .33 | .30 |
| Tens. coef. spec. resist. $\times 10^6$... | +11 | + .8 | -21.2 | +3.0 | -3.65 | - .60 | - .73 | + .19 |

Supplementary Values to Table 484

Resistance temperature coefficient for a number of metals and alloys of high purity due to J. R. Caldwell (1931).

| Metal | $(R_{100}-R_0)/100R_0$ | Alloy | $(R_{100}-R_0)/100R_0$ |
|----------|------------------------|-------------|------------------------|
| Ni | 0.00667 | 95 Pt— 5 Rh | 0.00215 |
| Zn | .00419 | 90 Pt—10 Rh | 0.00169 |
| Cd | .00423 | 80 Pt—20 Rh | 0.00140 |
| Pt | .003925 | 60 Pt—40 Rh | 0.00144 |
| Rh | .00436 | 40 Pt—60 Rh | 0.00194 |
| | | 20 Pt—80 Rh | 0.00260 |

Note to Table 491, p. 417: Superconductivity. Apparent only below about 10° K. (-263° C). The following metals are known to show it below the indicated temperatures. A low current density is necessary.

| | | | | | |
|-----------------|---------|----------------|---------|----------------|---------|
| Titanium | 1°75 K. | Indium | 3°37 K. | Thallium | 2°37 K. |
| Gallium | 1.05 | Tin | 3.7 | Lead | 7.2 |
| Niobium | 8.2 | Tantalum | 4.4 | Thorium | 1.5 |
| Molybdenum | 1.? | Mercury | 4.22 | Some alloys | |

Zn, Cd, Ge, Al, Pt, Na, Li do not show it.

McLennan, Nature, 130, Dec. 10, 1932. Hill, Rev. Scientific Instr., 4, 3, 1933.

CONDUCTIVITY AND RESISTIVITY OF MISCELLANEOUS ALLOYS

TEMPERATURE COEFFICIENTS

Conductivity in mhos or $\frac{1}{\text{ohms per cm}^3} = \gamma_t = \gamma_0(1 - at + bt^2)$ and resistivity in microhms -cm
 $= \rho_t = \rho_0(1 + at - bt^2)$.

| Metals and alloys | Composition by weight | $\frac{\gamma_0}{10^4}$ | $a \times 10^6$ | ρ_0 | Author-ity |
|----------------------------------|--|-------------------------|-------------------|----------|------------|
| Gold-copper-silver.. | 58.3 Au + 26.5 Cu + 15.2 Ag | 7.58 | 574* | 13.2 | 1 |
| " " " | 66.5 Au + 15.4 Cu + 18.1 Ag | 6.83 | 529† | 14.6 | 1 |
| " " " | 7.4 Au + 78.3 Cu + 14.3 Ag | 28.06 | 1830‡ | 3.6 | 1 |
| Invar..... | | 1.33 | 2000 | 75 | 10 |
| Welding iron..... | 0.05% Cu | 6.25 | 6000 | 18 | 9 |
| Woods metal..... | 56Bi, 17Cd, 14Pb, 13Sn | 1.93 | 2900 | 52 | 11 |
| Brass..... | Various..... | 12.2-15.6 | $1-2 \times 10^3$ | 6.4-8.4 | 2 |
| " hard drawn..... | 70.2 Cu + 29.8Zn | 12.16 | — | 8.2 | 3 |
| " annealed..... | " | 14.35 | — | 7.0 | 3 |
| German silver..... | Various..... | 3-5 | — | 20-33 | 2 |
| " " | 60.16 Cu + 25.37 Zn + 14.03 Ni + .30 Fe with trace of cobalt and manganese | 3.33 | 360 | 30 | 4 |
| Aluminum bronze... | | 7.5-8.5 | 600 | 12-13 | 2 |
| Phosphor bronze... | | 10-20 | — | 5-10 | 2 |
| Silicium bronze... | | 41 | — | 2.4 | 5 |
| Manganese-copper... | 30 Mn + 70 Cu..... | 1.00 | 40 | 100 | 4 |
| Nickel-manganese- copper..... | 3 Ni + 24 Mn + 73 Cu..... | 2.10 | —30 | 48 | 4 |
| Nickelin..... | 18.46 Ni + 61.63 Cu + 19.67 Zn + 0.24 Fe + 0.19 Co + 0.18 Mn | 3.01 | 300 | 33 | 4 |
| Patent nickel..... | 25.1 Ni + 74.41 Cu + 0.42 Fe + 0.23 Zn + 0.13 Mn + trace of cobalt | 2.92 | 190 | 34 | 4 |
| Rheotan..... | 53.28 Cu + 25.31 Ni + 16.89 Zn + 4.46 Fe + 0.37 Mn | 1.90 | 410 | 53 | 4 |
| Rheotan..... | 53 Cu, 25Ni, 17Zn, 5Fe..... | 2.24 | 280 | 45 | 12 |
| Copper-manganese- iron..... | 91 Cu + 7.1 Mn + 1.9 Fe.... | 4.98 | 120 | 20 | 6 |
| Copper-manganese- iron..... | 70.6 Cu + 23.2 Mn + 6.2 Fe. | 1.30 | 22 | 77 | 6 |
| Copper-manganese- iron..... | 69.7 Cu + 29.9 Ni + 0.3 Fe.. | 2.60 | 120 | 38 | 7 |
| Therlo..... | 85 Cu, 13Mn, 2Al..... | 2.24 | 10 | 46.5 | 10 |
| Manganin..... | 84 Cu + 12 Mn + 4 Ni..... | 2.3 | 6 | 44 | 2 |
| Constantan..... | 60 Cu + 40 Ni..... | 2.04 | 8 | 49 | 8 |

¹ Matthiessen.

² Various.

³ W. Siemens.

⁴ Feussner and Lindeck.

⁵ Van der Ven.

⁶ Blood.

⁷ Feussner.

⁸ Jaeger-Diesselhorst.

⁹ LeChatelier.

¹⁰ I.C.T.

¹¹ Weber.

¹² Niccolai.

*, †, ‡, $b \times 10^9 = 924, 93, 7280$.

CONDUCTING POWER OF ALLOYS

This table shows the conducting power of alloys and the variation of the conducting power with temperature.* The values of C_0 were obtained from the original results by assuming silver = $\frac{10^6}{1.585}$ mhos. The conductivity is taken as $C_t = C_0(1 - \alpha t + \beta t^2)$, and the range of temperature was from 0° to 100° C.

The table is arranged in three groups to show (1) that certain metals when melted together produce a solution which has a conductivity equal to the mean of the conductivities of the components, (2) the behavior of those metals alloyed with others, and (3) the behavior of the other metals alloyed together.

It is pointed out that, with a few exceptions, the percentage variation between 0° and 100° can be calculated from the formula $P' = P_c \frac{l}{\bar{p}}$, where l is the observed and \bar{p} the calculated conducting power of the mixture at 100° C and P_c is the calculated mean variation of the metals mixed.

| Alloys. | Weight % | Volume % | $\frac{C_0}{10^4}$ | $\alpha \times 10^6$ | $\delta \times 10^9$ | Variation per 100° C. | |
|-------------------------------------|-----------------|----------|--------------------|----------------------|----------------------|-----------------------|-------------|
| | of first named. | | | | | Observed. | Calculated. |
| GROUP 1. | | | | | | | |
| Sn ₆ Pb | 77.04 | 83.96 | 7.57 | 3890 | 8670 | 30.18 | 29.67 |
| Sn ₄ Cd | 82.41 | 83.10 | 9.18 | 4080 | 11870 | 28.89 | 30.03 |
| SnZn | 78.06 | 77.71 | 10.56 | 3880 | 8720 | 30.12 | 30.16 |
| PbSn | 64.13 | 53.41 | 6.40 | 3780 | 8420 | 29.41 | 29.10 |
| ZnCd ₂ | 24.76 | 26.06 | 16.16 | 3780 | 8000 | 29.86 | 29.67 |
| SnCd ₄ | 23.05 | 23.50 | 13.67 | 3850 | 9410 | 29.08 | 30.25 |
| CdPb ₆ | 7.37 | 10.57 | 5.78 | 3500 | 7270 | 27.74 | 27.60 |
| GROUP 2. | | | | | | | |
| Lead-silver (Pb ₂₀ Ag) . | 95.05 | 94.64 | 5.60 | 3630 | 7960 | 28.24 | 19.96 |
| Lead-silver (PbAg) . | 48.97 | 46.90 | 8.03 | 1960 | 3100 | 16.53 | 7.73 |
| Lead-silver (PbAg ₂) . | 32.44 | 30.64 | 13.80 | 1990 | 2600 | 17.36 | 10.42 |
| Tin-gold (Sn ₁₂ Au) . . | 77.94 | 90.32 | 5.20 | 3080 | 6640 | 24.20 | 14.83 |
| “ “ (Sn ₅ Au) | 59.54 | 79.54 | 3.03 | 2920 | 6300 | 22.90 | 5.95 |
| Tin-copper | 92.24 | 93.57 | 7.59 | 3680 | 8130 | 28.71 | 19.76 |
| “ “ † | 80.58 | 83.60 | 8.05 | 3330 | 6840 | 26.24 | 14.57 |
| “ “ † | 12.49 | 14.91 | 5.57 | 547 | 294 | 5.18 | 3.99 |
| “ “ † | 10.30 | 12.35 | 6.41 | 666 | 1185 | 5.48 | 4.46 |
| “ “ † | 9.67 | 11.61 | 7.64 | 691 | 304 | 6.60 | 5.22 |
| “ “ † | 4.96 | 6.02 | 12.44 | 995 | 795 | 9.25 | 7.83 |
| “ “ † | 1.15 | 1.41 | 39.41 | 2670 | 5070 | 21.74 | 20.53 |
| Tin-silver | 91.30 | 96.52 | 7.81 | 3820 | 8190 | 30.00 | 23.31 |
| “ “ | 53.85 | 75.51 | 8.65 | 3770 | 8550 | 29.18 | 11.89 |
| Zinc-copper † | 36.70 | 42.06 | 13.75 | 1370 | 1340 | 12.40 | 11.29 |
| “ “ † | 25.00 | 29.45 | 13.70 | 1270 | 1240 | 11.49 | 10.08 |
| “ “ † | 16.53 | 23.61 | 13.44 | 1880 | 1800 | 12.80 | 12.30 |
| “ “ † | 8.89 | 10.88 | 29.61 | 2040 | 3030 | 17.41 | 17.42 |
| “ “ † | 4.06 | 5.03 | 38.09 | 2470 | 4100 | 20.61 | 20.62 |

NOTE. — Barus, in the "Am. Jour. of Sci." vol. 36, has pointed out that the temperature variation of platinum alloys containing less than 10% of the other metal can be nearly expressed by an equation $y = \frac{n}{x} - m$, where y is the temperature coefficient and x the specific resistance, m and n being constants. If α be the temperature coefficient at 0° C and s the corresponding specific resistance, $s(\alpha + m) = n$.

For platinum alloys Barus's experiments gave $m = -.000194$ and $n = .0378$.

For steel $m = -.000303$ and $n = .0620$.

Matthiessen's experiments reduced by Barus gave for

Gold alloys $m = -.000045$, $n = .00721$.

Silver " $m = -.000112$, $n = .00538$.

Copper " $m = -.000386$, $n = .00055$.

* From the experiments of Matthiessen and Vogt, "Phil. Trans. R. S." v. 154.

† Hard-drawn.

TABLE 489 (continued).—Conducting Power of Alloys

| GROUP 3. | | | | | | | |
|------------------------|-----------------|----------|--------------------------|-----------------|-----------------|-----------------------|-------------|
| Alloys. | Weight % | Volume % | C_0 10 ⁴ | $a \times 10^6$ | $b \times 10^9$ | Variation per 100° C. | |
| | of first named. | | | | | Observed. | Calculated. |
| Gold-copper † . . . | 99.23 | 98.36 | 35.42 | 2650 | 4650 | 21.87 | 23.22 |
| “ “ † . . . | 90.55 | 81.66 | 10.16 | 749 | 81 | 7.41 | 7.53 |
| Gold-silver † . . . | 87.95 | 79.86 | 13.46 | 1090 | 793 | 10.09 | 9.65 |
| “ “ * . . . | 87.95 | 79.86 | 13.61 | 1140 | 1160 | 10.21 | 9.59 |
| “ “ † . . . | 64.80 | 52.08 | 9.48 | 673 | 246 | 6.49 | 6.58 |
| “ “ * . . . | 64.80 | 52.08 | 9.51 | 721 | 495 | 6.71 | 6.42 |
| “ “ † . . . | 31.33 | 19.86 | 13.69 | 885 | 531 | 8.23 | 8.62 |
| “ “ * . . . | 31.33 | 19.86 | 13.73 | 908 | 641 | 8.44 | 8.31 |
| Gold-copper † . . . | 34.83 | 19.17 | 12.94 | 864 | 570 | 8.07 | 8.18 |
| “ “ † . . . | 1.52 | 0.71 | 53.02 | 3320 | 7300 | 25.90 | 25.86 |
| Platinum-silver † . . | 33.33 | 19.65 | 4.22 | 330 | 208 | 3.10 | 3.21 |
| “ “ † . . . | 9.81 | 5.05 | 11.38 | 774 | 656 | 7.08 | 7.25 |
| “ “ † . . . | 5.00 | 2.51 | 19.96 | 1240 | 1150 | 11.29 | 11.88 |
| Palladium-silver † . . | 25.00 | 23.28 | 5.38 | 324 | 154 | 3.40 | 4.21 |
| Copper-silver † . . . | 98.08 | 98.35 | 56.49 | 3450 | 7990 | 26.50 | 27.30 |
| “ “ † . . . | 94.40 | 95.17 | 51.93 | 3250 | 6940 | 25.57 | 25.41 |
| “ “ † . . . | 76.74 | 77.64 | 44.06 | 3030 | 6070 | 24.29 | 21.92 |
| “ “ † . . . | 42.75 | 46.67 | 47.29 | 2870 | 5280 | 22.75 | 24.00 |
| “ “ † . . . | 7.14 | 8.25 | 50.65 | 2750 | 4360 | 23.17 | 25.57 |
| “ “ † . . . | 1.31 | 1.53 | 50.30 | 4120 | 8740 | 26.51 | 29.77 |
| Iron-gold † | 13.59 | 27.93 | 1.73 | 3490 | 7010 | 27.92 | 14.70 |
| “ “ † | 9.80 | 21.18 | 1.26 | 2970 | 1220 | 17.55 | 11.20 |
| “ “ † | 4.76 | 10.96 | 1.46 | 487 | 103 | 3.84 | 13.40 |
| Iron-copper † . . . | 0.40 | 0.46 | 24.51 | 1550 | 2090 | 13.44 | 14.03 |
| Phosphorus-copper † . | 2.50 | — | 4.62 | 476 | 145 | — | — |
| “ “ † . | 0.95 | — | 14.91 | 1320 | 1640 | — | — |
| Arsenic-copper † . . | 5.40 | — | 3.97 | 516 | 989 | — | — |
| “ “ † . . | 2.80 | — | 8.12 | 736 | 446 | — | — |
| “ “ † . . | trace | — | 38.52 | 2640 | 4830 | — | — |

* Annealed.

† Hard-drawn.

TABLE 490.—Allowable Carrying Capacity of Rubber-covered Copper Wires

(For inside wiring — Nat. Board Fire Underwriters' Rules.)

| B + S Gage | 18 | 16 | 14 | 12 | 10 | 8 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | 00 | 0000 |
|------------|----|----|----|----|----|----|----|----|----|----|----|-----|-----|-----|------|
| Amperes | 3 | 6 | 12 | 17 | 24 | 33 | 46 | 54 | 65 | 76 | 90 | 107 | 127 | 150 | 210 |

500,000 circ. mills, 390 amp.; 1,000,000 c. m., 650 amp.; 2,000,000 c. m., 1,050 amp. For insulated al. wire, capacity = 84% of cu. Preece gives as formula for fusion of bare wires $I = ad^2$, where d = diam. in inches, a for cu. is 10,244; al., 7585; pt., 5172; German silver, 5230; platinoid, 4750; Fe, 3148; Pb., 1379; alloy 2 pts. Pb., 1 of Sn., 1318.

RESISTIVITIES AT HIGH AND LOW TEMPERATURES*

The electrical resistivity (ρ , ohms per cm. cube) of good conductors depends greatly on chemical purity. Slight contamination even with metals of lower ρ may greatly increase ρ . Solid solutions of good conductors generally have higher ρ than components. Reverse is true of bad conductors. In solid state allotropic and crystalline forms greatly modify ρ . For liquid metals this last cause of variability disappears. The ρ temperature coefficients of pure metals is of the same order as the coefficients of expansion of gases. For temperature resistance (t, ρ) plot at low temperatures the graph is convex towards the axis of t and probably approaches tangency to it. However for extremely low temperatures Onnes finds very sudden and great drops in ρ . e.g. for Mercury, $\rho_{3.6K} < 4 \times 10^{-10} \rho_0$ and for Sn, $\rho_{3.8K} < 10^{-10} \rho_0$. The t, ρ graph for an alloy may be nearly parallel to the t axis, cf. constantan; for poor conductors ρ may decrease with increasing t . At the melting-points there are three types of behavior of good conductors: those about doubling ρ and then possessing nearly linear t, ρ graphs (Al., Cu., Sn., Au., Ag., Pb.); those where ρ suddenly increases and then the ρ temp. coefficient is only approximately constant; (Hg., Na., K.); those about doubling ρ then having a ρ slowly changing to a ρ temp. coef. (Zn., Cd.); those where ρ suddenly decreases and thereafter steadily increases (Sb., Bi.). The values from different authorities do not necessarily fit because of different samples of metals. The Shimank values (given to tenths of %) are for material of theoretical purity and are determined by the α rule (see his paper, also Nernst, Ann. d. Phys. 36, p. 403, 1911 for temperature resistance thermometry). The Shimank and Pirani values are originally given as ratios to ρ_0 . (Ann. d. Phys. 45, p. 706, 1914, 46, p. 176, 1915.) Resistivities are in micro-ohms per cm. cube unless stated. Italicized figures indicate liquid state.

| Gold. | | | Copper. | | | Silver. | | | Zinc. | | |
|---------------------|----------|-------------------------|---------------------|----------|-------------------------|---------------------|----------|-------------------------|---------------------|----------|-------------------------|
| $^{\circ}\text{C.}$ | ρ_t | $\frac{\rho_t}{\rho_0}$ | $^{\circ}\text{C.}$ | ρ_t | $\frac{\rho_t}{\rho_0}$ | $^{\circ}\text{C.}$ | ρ_t | $\frac{\rho_t}{\rho_0}$ | $^{\circ}\text{C.}$ | ρ_t | $\frac{\rho_t}{\rho_0}$ |
| -252.8 | 0.018 | .0081 | -258.6 | 0.014 | .0091 | -258.6 | 0.009 | .0057 | -252.9 | .0511 | .0089 |
| -200. | .601 | .267 | -252.8 | .016 | .0103 | -252.8 | .014 | .0090 | -200. | 1.39 | .242 |
| -192.5 | .520 | .231 | -251.1 | .028 | .0178 | -189.5 | .334 | .222 | -191.1 | 1.23 | .214 |
| -150. | .907 | .444 | -206.6 | .103 | .1035 | -200. | .357 | .237 | -150. | 2.00 | .348 |
| -100. | 1.400 | .623 | -192.9 | .249 | .1580 | -150. | .638 | .424 | -100. | 2.90 | .504 |
| -77.6 | 1.564 | .696 | -150. | .507 | .359 | -100. | .916 | .608 | -77.8 | 3.97 | .691 |
| -50. | 1.813 | .806 | -100. | .904 | .573 | -76.8 | 1.040 | .690 | -50. | 4.04 | .703 |
| 0. | 2.247 | 1.00 | -50. | 1.240 | .786 | -50. | 1.212 | .805 | 0. | 5.75 | 1.00 |
| 100. | 2.97 | 1.32 | 0. | 1.578 | 1.00 | 0. | 1.506 | 1.00 | 100. | 7.95 | 1.38 |
| 200. | 3.83 | 1.70 | 100. | 2.28 | 1.44 | 100. | 2.15 | 1.43 | 200. | 13.25 | 2.30 |
| 500. | 6.62 | 2.94 | 200. | 2.66 | 1.88 | 200. | 2.80 | 1.86 | 500. | 17.00 | 2.96 |
| 750. | 9.35 | 4.16 | 500. | 5.08 | 3.22 | 400. | 3.46 | 2.30 | 427. | 37.30 | 6.40 |
| 1000. | 12.54 | 5.58 | 750. | 7.03 | 4.40 | 750. | 6.65 | 4.42 | 450. | 57.05 | 6.40 |
| 1063. | 13.50 | 6.01 | 1000. | 9.42 | 5.97 | 960. | 8.4 | 5.58 | 500. | 56.60 | 6.36 |
| 1063. | 30.52 | 13.7 | 1083. | 10.20 | 6.47 | 960. | 16.6 | 11.0 | 600. | 55.90 | 6.25 |
| 1200. | 32.8 | 14.6 | 1083. | 21.30 | 13.5 | 1000. | 17.01 | 11.3 | 700. | 55.60 | 6.10 |
| 1400. | 35.6 | 15.8 | 1200. | 22.30 | 14.1 | 1200. | 19.30 | 12.9 | 800. | 55.60 | 6.10 |
| 1500. | 37.0 | 16.5 | 1400. | 23.80 | 15.1 | 1400. | 21.72 | 14.4 | 850. | 55.74 | 6.21 |
| | | | 1500. | 24.62 | 15.6 | 1500. | 23.0 | 15.3 | | | |
| Mercury. | | | Potassium. | | | Sodium. | | | Iron. | | |
| $^{\circ}\text{C.}$ | ρ_t | $\frac{\rho_t}{\rho_0}$ | $^{\circ}\text{C.}$ | ρ_t | $\frac{\rho_t}{\rho_0}$ | $^{\circ}\text{C.}$ | ρ_t | $\frac{\rho_t}{\rho_0}$ | $^{\circ}\text{C.}$ | ρ_t | $\frac{\rho_t}{\rho_0}$ |
| -200. | 5.38 | .057 | -200. | 1.720 | .246 | -200. | 0.605 | .137 | -252.7 | 0.011 | .0010 |
| -150. | 10.30 | .109 | -150. | 2.654 | .379 | -150. | 1.455 | .330 | -200. | 2.27 | .212 |
| -100. | 15.42 | .164 | -100. | 3.724 | .532 | -100. | 2.380 | .541 | -192.5 | .844 | .079 |
| -50. | 21.4 | .227 | -50. | 5.134 | .732 | -50. | 3.365 | .764 | -100. | 5.92 | .554 |
| -30. | 07.7 | .075 | 0. | 7.060 | 1.00 | 0. | 4.40 | 1.000 | -75.1 | 6.43 | .602 |
| 0. | 04.1 | 1.000 | 20. | 7.116 | 1.016 | 20. | 4.873 | 1.107 | -50. | 8.15 | .763 |
| 50. | 05.3 | 1.045 | 60. | 8.760 | 1.256 | 93.5 | 6.290 | 1.434 | 0. | 10.68 | 1.00 |
| 100. | 103.1 | 1.096 | 65. | 15.40 | 1.914 | 100. | 0.220 | 2.005 | 100. | 16.61 | 1.554 |
| 200. | 114.0 | 1.212 | 100. | 15.31 | 2.187 | 120. | 0.724 | 2.200 | 200. | 24.50 | 2.293 |
| 300. | 127.0 | 1.350 | 120. | 16.70 | 2.380 | 140. | 10.34 | 2.349 | 400. | 43.24 | 4.052 |
| Manganin. | | | German Silver. | | | Constantan. | | | 90 % Pt. 10 % Rh. | | |
| $^{\circ}\text{C.}$ | ρ_t | $\frac{\rho_t}{\rho_0}$ | $^{\circ}\text{C.}$ | ρ_t | $\frac{\rho_t}{\rho_0}$ | $^{\circ}\text{C.}$ | ρ_t | $\frac{\rho_t}{\rho_0}$ | $^{\circ}\text{C.}$ | ρ_t | $\frac{\rho_t}{\rho_0}$ |
| -200. | 37.8 | .974 | -200. | 27.9 | .930 | -200. | 42.4 | .961 | -200. | 14.49 | .685 |
| -150. | 38.2 | .985 | -150. | 28.7 | .957 | -150. | 43.0 | .975 | -150. | 16.29 | .770 |
| -100. | 38.5 | .992 | -100. | 29.3 | .977 | -100. | 43.5 | .986 | -100. | 18.05 | .854 |
| -50. | 38.7 | .997 | -50. | 29.7 | .990 | -50. | 43.9 | .995 | -50. | 19.66 | .930 |
| 0. | 38.8 | 1.000 | 0. | 30.0 | 1.000 | 0. | 44.1 | 1.000 | 0. | 21.14 | 1.000 |
| 100. | 38.9 | 1.003 | 100. | 33.1 | 1.103 | 100. | 44.6 | 1.012 | 100. | 24.20 | 1.145 |
| 400. | 38.3 | .987 | | | | 400. | 44.8 | 1.016 | | | |

Au. below 0° , Nicolai, Lincei Rend. (5), 16, p. 757, 906, 1007; above, Northrup, Jour. Franklin Inst. 177, p. 85, 1914. Cu. below, Nicolai, l. c. above, Northrup, ditto, 177, p. 1, 1914. Ag. below, Nicolai, l. c. above, Northrup, ditto, 178, p. 85, 1914. Zn. below, Dewar, Fleming, Phil. Mag. 36, p. 271, 1893; above, Northrup, 175, p. 153, 1913. Hg. below, Dewar, Fleming, Proc. Roy. Soc. 66, p. 76, 1900; above, Northrup, see Cd. K. below, Gunz, Broniewski, C. R. 147, p. 1474, 1908, 148, p. 204, 1909. Above, Northrup, Tr. Am. Electroch. Soc. p. 185, 1911. Na. below, means, above, see K. Fe., Manganin, Constantan. Nicolai, l. c. German Silver, 90% Pt. 90% Rh., Dewar and Fleming—Phil. Mag. 36, p. 271, 1893. * See also page 413.

TABLE 491 (continued).—Resistivities at High and Low Temperatures
(Ohms per cm cube unless stated otherwise.)

| Platinum. | | | Lead. | | | Bismuth. | | | Cadmium. | | |
|-----------|----------|-------------------------|--------|----------|-------------------------|----------|----------|-------------------------|----------|----------|-------------------------|
| °C. | ρ_t | $\frac{\rho_t}{\rho_0}$ | °C. | ρ_t | $\frac{\rho_t}{\rho_0}$ | °C. | ρ_t | $\frac{\rho_t}{\rho_0}$ | °C. | ρ_t | $\frac{\rho_t}{\rho_0}$ |
| -265. | 0.10 | .0092 | -252.9 | 0.59 | .0298 | -200. | 34.8 | .314 | -252.9 | 0.17 | .0218 |
| -253. | .15 | .014 | -203. | 4.42 | .223 | -150. | 55.3 | .499 | -200. | 1.66 | .214 |
| -233. | .54 | .049 | -192.8 | 5.22 | .264 | -100. | 75.6 | .683 | -190.2 | 2.00 | .258 |
| -153. | 4.18 | .378 | -103. | 11.8 | .598 | -50. | 94.3 | .852 | -183.1 | 2.22 | .286 |
| -73. | 7.82 | .708 | -75.8 | 13.95 | .705 | 0. | 110.7 | 1.00 | -139.2 | 3.60 | .464 |
| 0. | 11.05 | 1.00 | -53. | 15.7 | .792 | 17. | 120.0 | 1.083 | -100. | 4.80 | .619 |
| 100. | 14.1 | 1.28 | 0. | 19.8 | 1.00 | 100. | 156.5 | 1.413 | 0. | 7.75 | 1.00 |
| 200. | 17.9 | 1.62 | 100. | 27.8 | 1.403 | 200. | 214.5 | 1.937 | 300. | 16.50 | 2.13 |
| 400. | 25.4 | 2.30 | 200. | 38.0 | 1.919 | 259. | 267.0 | 2.411 | 325. | 33.76 | 4.35 |
| 800. | 40.3 | 3.65 | 319. | 50.0 | 2.52 | 263. | 127.5 | 1.150 | 350. | 53.60 | 4.35 |
| 1000. | 47.0 | 4.25 | 333. | 95.0 | 4.80 | 300. | 128.9 | 1.164 | 400. | 33.70 | 4.35 |
| 1200. | 52.7 | 4.77 | 400. | 95.3 | 4.90 | 500. | 130.9 | 1.203 | 500. | 53.12 | 4.40 |
| 1400. | 58.0 | 5.25 | 600. | 107.2 | 5.41 | 700. | 150.8 | 1.361 | 700. | 53.78 | 4.62 |
| 1600. | 63.0 | 5.70 | 800. | 110.2 | 5.80 | 750. | 153.5 | 1.386 | | | |

| Tin. | | | Carbon, Graphite.* | | Fused silica. | | Alundum cement. | |
|-------|----------|-------------------------|--------------------|---------------------------|---------------|----------------------|-----------------|--------------------------|
| °C. | ρ_t | $\frac{\rho_t}{\rho_0}$ | °C. | ρ in ohms, cm. cube. | °C. | ρ = megohms cm. | °C. | ρ in ohms cm. cube. |
| -200. | 2.60 | .199 | | | 15. | >200,000,000. | 20. | >9 × 10 ⁶ |
| -100. | 7.57 | .580 | 0. | Carbon 0.0035 | 230. | 20,000,000. | 800. | 30500. |
| 0. | 13.05 | 1.00 | 500. | .0027 | 300. | 200,000. | 900. | 13'000. |
| 200. | 20.30 | 1.55 | 1000. | .0021 | 350. | 30,000. | 1000. | 7'000. |
| 225. | 22.00 | 1.69 | 1500. | .0015 | 450. | 800. | 1100. | 6500. |
| 235. | 47.00 | 3.65 | 2000. | .0011 | 700. | 30. | 1200. | 2300. |
| 750. | 61.22 | 4.69 | 2500. | .0009 | 850. | about 20. | 1600. | 190. |

ρ_t , low, Nerst, l. c. high, Pirrari, Ber. Deutsch. Phys. Ges. 12, p. 305, Pb. low, Schimank, Nerst, l. c. high, Northrup, see Zn. Bi. low, means, high, Northrup, see Zn. Cd. low, Euchen, Gehlhoff, Verh. Deutsch. Phys. Ges. 14, p. 169, 1912, high, Northrup, see Zn. Sn. low, Dewar, Fleming, high, Northrup, see Zn. Carbon, graphite, Metallurg. Ch. Eng. 13, p. 23, 1915. Silica, Campbell, Nat. Phys. Lab. 11, p. 207, 1914. Alundum, Metallurg. Ch. Eng. 12, p. 125, 1914.

* Diamond 1030° C, $\rho > 10^7$; 1380°, 7.5×10^4 , v. Wartenberg, 1912.

TABLE 492.—Volume and Surface Resistivity of Solid Dielectrics

The resistance between two conductors insulated by a solid dielectric depends both upon the surface resistance and the volume resistance of the insulator. The volume resistivity, ρ , is the resistance between two opposite faces of a centimeter cube. The surface resistivity, σ , is the resistance between two opposite edges of a centimeter square of the surface. The surface resistivity usually varies through a wide range with the humidity. (Curtis, Bul. Bur. Standards, 11, 359, 1915, which see for discussion and data for many additional materials.)

| Material. | σ ; megohms 50% humidity. | σ ; megohms 70% humidity. | σ ; megohms 50% humidity. | ρ Megohms-cm. |
|------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|-----------------------|
| Amber | 6×10^8 | 2×10^8 | 1×10^5 | 5×10^{10} |
| Beeswax, yellow | 6×10^8 | 6×10^8 | 5×10^8 | 2×10^9 |
| Celluloid | 5×10^4 | 2×10^4 | 2×10^3 | 2×10^4 |
| Fiber, red | 2×10^4 | 3×10^3 | 2×10^2 | 5×10^3 |
| Glass, plate | 5×10^4 | 6×10 | 2×10 | 2×10^7 |
| " Kavalier | 4×10^6 | 4×10^3 | 1×10^3 | 8×10^9 |
| Hard rubber, new | 3×10^9 | 1×10^8 | 2×10^3 | 1×10^{12} |
| Ivory | 5×10^3 | 1×10^3 | 3×10 | 2×10^2 |
| Khotinsk cement | 7×10^8 | 3×10^8 | 5×10^5 | 2×10^9 |
| Marble, Italian | 3×10^3 | 2×10^2 | 2×10 | 1×10^5 |
| Mica, colorless | 2×10^7 | 4×10^7 | 8×10^3 | 2×10^{11} |
| Paraffin (parowax) | 9×10^9 | 7×10^9 | 6×10^9 | 1×10^{10} |
| Porcelain, unglazed | 6×10^8 | 7×10^3 | 5×10 | 3×10^8 |
| Quartz, fused | 3×10^8 | 2×10^3 | 2×10^2 | 5×10^{12} |
| Rosin | 6×10^8 | 3×10^8 | 2×10^8 | 5×10^{10} |
| Sealing wax | 2×10^9 | 6×10^8 | 9×10^7 | 8×10^9 |
| Shellac | 6×10^7 | 3×10^6 | 7×10^3 | 1×10^{10} |
| Slate | 9×10 | 3×10 | 1×10 | 1×10^2 |
| Sulphur | 7×10^9 | 4×10^9 | 1×10^8 | 1×10^{11} |
| Wood, parafined mahogany | 4×10^6 | 5×10^5 | 7×10^3 | 4×10^7 |

TABLE 493.—Variation of Electrical Resistance of Glass and Porcelain with Temperature

The following table gives the values of a , b , and c in the equation

$$\log R = a + bt + ct^2,$$

where R is the specific resistance expressed in ohms, that is, the resistance in ohms per centimeter of a rod one square centimeter in cross section.*

| No. | Kind of glass. | Density. | a | b | c | Range of temp. Centigrade. |
|-----|--|----------|--------|--------|-----------|----------------------------|
| 1 | Test-tube glass | — | 13.86 | —0.44 | .000065 | 0°–250° |
| 2 | “ “ “ | 2.458 | 14.24 | —0.55 | .0001 | 37–131 |
| 3 | Bohemian glass | 2.43 | 16.21 | —0.43 | .0000394 | 60–174 |
| 4 | Lime glass (Japanese manufacture) . | 2.55 | 13.14 | —0.31 | —0.000021 | 10–85 |
| 5 | “ “ “ “ | 2.499 | 14.002 | —0.25 | —0.00006 | 35–95 |
| 6 | Soda-lime glass (French flask) . | 2.533 | 14.58 | —0.49 | .000075 | 45–120 |
| 7 | Potash-soda lime glass | 2.58 | 16.34 | —0.425 | .0000364 | 66–193 |
| 8 | Arsenic enamel flint glass | 3.07 | 18.17 | —0.55 | .000088 | 105–135 |
| 9 | Flint glass (Thomson's electrometer jar) | 3.172 | 18.021 | —0.36 | —0.000091 | 100–200 |
| 10 | Porcelain (white evaporating dish) . | — | 15.65 | —0.42 | .00005 | 68–290 |

COMPOSITION OF SOME OF THE ABOVE SPECIMENS OF GLASS.

| Number of specimen = | 3 | 4 | 5 | 7 | 8 | 9 |
|-----------------------------|------------|------------|-------|-------|------|-------|
| Silica | 61.3 | 57.2 | 70.05 | 75.65 | 54.2 | 55.18 |
| Potash | 22.9 | 21.1 | 1.44 | 7.92 | 10.5 | 13.28 |
| Soda | Lime, etc. | Lime, etc. | 14.32 | 6.92 | 7.0 | — |
| Lead oxide | by diff. | by diff. | 2.70 | — | 23.9 | 31.01 |
| Lime | 15.8 | 16.7 | 10.33 | 8.48 | 0.3 | 0.35 |
| Magnesia | — | — | — | 0.36 | 0.2 | 0.06 |
| Arsenic oxide | — | — | — | — | 3.5 | — |
| Alumina, iron oxide, etc. . | — | — | 1.45 | 0.70 | 0.4 | 0.67 |

* T. Gray, "Phil. Mag." 1880, and "Proc. Roy. Soc." 1882.

TABLE 494.—Temperature Resistance Coefficients of Glass, Porcelain and Quartz dr/dt

| Temperature. | 450° | 500° | 575° | 600° | 700° | 750° | 800° | 900° | 1000° |
|---------------------|------|------|------|------|-------|------|-------|-------|-------|
| Glass | —32. | —6. | —1.5 | —8 | —0.17 | —0.1 | —0.06 | — | — |
| Porcelain | — | — | —16. | —9.8 | —2.8 | —1.6 | —0.70 | —0.30 | —0.12 |
| Quartz | — | — | — | — | — | —10. | —6.40 | —2.60 | —1.00 |

Somerville, Physical Review, 31, p. 261, 1910.

TABLE 495
TABULAR COMPARISON OF WIRE GAGES

| Gage No. | American wire gage (B. & S.) mils.† | American wire gage (B. & S.) mm.† | Steel wire gage* mils. | Steel wire gage* mm. | Stubs' steel wire gage mils. | (British) standard wire gage mils. | Birmingham wire gage (Stubs') mils. | Gage No. |
|----------|-------------------------------------|-----------------------------------|------------------------|----------------------|------------------------------|------------------------------------|-------------------------------------|----------|
| 7-0 | | | 490.0 | 12.4 | | 500. | | 7-0 |
| 6-0 | | | 461.5 | 11.7 | | 464. | | 6-0 |
| 5-0 | | | 430.5 | 10.9 | | 432. | | 5-0 |
| 4-0 | 460. | 11.7 | 393.8 | 10.0 | | 400. | 454. | 4-0 |
| 3-0 | 410. | 10.4 | 362.5 | 9.2 | | 372. | 425. | 3-0 |
| 2-0 | 365. | 9.3 | 331.0 | 8.4 | | 348. | 380. | 2-0 |
| 0 | 325. | 8.3 | 306.5 | 7.8 | | 324. | 340. | 0 |
| 1 | 289. | 7.3 | 283.0 | 7.2 | 227. | 300. | 300. | 1 |
| 2 | 258. | 6.5 | 262.5 | 6.7 | 219. | 276. | 284. | 2 |
| 3 | 229. | 5.8 | 243.7 | 6.2 | 212. | 252. | 259. | 3 |
| 4 | 204. | 5.2 | 225.3 | 5.7 | 207. | 232. | 238. | 4 |
| 5 | 182. | 4.6 | 207.0 | 5.3 | 204. | 212. | 220. | 5 |
| 6 | 162. | 4.1 | 192.0 | 4.9 | 201. | 192. | 203. | 6 |
| 7 | 144. | 3.7 | 177.0 | 4.5 | 199. | 176. | 180. | 7 |
| 8 | 128. | 3.3 | 162.0 | 4.1 | 197. | 160. | 165. | 8 |
| 9 | 114. | 2.91 | 148.3 | 3.77 | 194. | 144. | 148. | 9 |
| 10 | 102. | 2.59 | 135.0 | 3.43 | 191. | 128. | 134. | 10 |
| 11 | 91. | 2.30 | 120.5 | 3.06 | 188. | 116. | 120. | 11 |
| 12 | 81. | 2.05 | 105.5 | 2.68 | 185. | 104. | 109. | 12 |
| 13 | 72. | 1.83 | 91.5 | 2.32 | 182. | 92. | 95. | 13 |
| 14 | 64. | 1.63 | 80.0 | 2.03 | 180. | 80. | 83. | 14 |
| 15 | 57. | 1.45 | 72.0 | 1.83 | 178. | 72. | 72. | 15 |
| 16 | 51. | 1.29 | 62.5 | 1.59 | 175. | 64. | 65. | 16 |
| 17 | 45. | 1.15 | 54.0 | 1.37 | 172. | 56. | 58. | 17 |
| 18 | 40. | 1.02 | 47.5 | 1.21 | 168. | 48. | 49. | 18 |
| 19 | 36. | 0.91 | 41.0 | 1.04 | 164. | 40. | 42. | 19 |
| 20 | 32. | .81 | 34.8 | 0.88 | 161. | 36. | 35. | 20 |
| 21 | 28.5 | .72 | 31.7 | .81 | 157. | 32. | 32. | 21 |
| 22 | 25.3 | .62 | 28.6 | .73 | 155. | 28. | 28. | 22 |
| 23 | 22.6 | .57 | 25.8 | .66 | 153. | 24. | 25. | 23 |
| 24 | 20.1 | .51 | 23.0 | .58 | 151. | 22. | 22. | 24 |
| 25 | 17.9 | .45 | 20.4 | .52 | 148. | 20. | 20. | 25 |
| 26 | 15.9 | .40 | 18.1 | .46 | 146. | 18. | 18. | 26 |
| 27 | 14.2 | .36 | 17.3 | .439 | 143. | 16.4 | 16. | 27 |
| 28 | 12.6 | .32 | 16.2 | .411 | 139. | 14.8 | 14. | 28 |
| 29 | 11.3 | .29 | 15.0 | .381 | 134. | 13.6 | 13. | 29 |
| 30 | 10.0 | .25 | 14.0 | .356 | 127. | 12.4 | 12. | 30 |
| 31 | 8.9 | .227 | 13.2 | .335 | 120. | 11.6 | 10. | 31 |
| 32 | 8.0 | .202 | 12.8 | .325 | 115. | 10.8 | 9. | 32 |
| 33 | 7.1 | .180 | 11.8 | .300 | 112. | 10.0 | 8. | 33 |
| 34 | 6.3 | .160 | 10.4 | .264 | 110. | 9.2 | 7. | 34 |
| 35 | 5.6 | .143 | 9.5 | .241 | 108. | 8.4 | 5. | 35 |
| 36 | 5.0 | .127 | 9.0 | .229 | 106. | 7.6 | 4. | 36 |
| 37 | 4.5 | .113 | 8.5 | .216 | 103. | 6.8 | | 37 |
| 38 | 4.0 | .101 | 8.0 | .203 | 101. | 6.0 | | 38 |
| 39 | 3.5 | .090 | 7.5 | .191 | 99. | 5.2 | | 39 |
| 40 | 3.1 | .080 | 7.0 | .178 | 97. | 4.8 | | 40 |
| 41 | | | 6.6 | .168 | 95. | 4.4 | | 41 |
| 42 | | | 6.2 | .157 | 92. | 4.0 | | 42 |
| 43 | | | 6.0 | .152 | 88. | 3.6 | | 43 |
| 44 | | | 5.8 | .147 | 85. | 3.2 | | 44 |
| 45 | | | 5.5 | .140 | 81. | 2.8 | | 45 |
| 46 | | | 5.2 | .132 | 79. | 2.4 | | 46 |
| 47 | | | 5.0 | .127 | 77. | 2.0 | | 47 |
| 48 | | | 4.8 | .122 | 75. | 1.6 | | 48 |
| 49 | | | 4.6 | .117 | 72. | 1.2 | | 49 |
| 50 | | | 4.4 | .112 | 69. | 1.0 | | 50 |

* The Steel Wire Gage is the same gage which has been known by the various names: "Washburn and Moen," "Roeb-ling," "American Steel and Wire Co.'s." Its abbreviation should be written "Std. W. G.," to distinguish it from "S. W. G.," the usual abbreviation for the (British) Standard Wire Gage.

† The American Wire Gage sizes have been rounded off to the usual limits of commercial accuracy. They are given to four significant figures in Tables 499 to 502. They can be calculated with any desired accuracy, being based upon a simple mathematical law. The diameter of No. 0000 is defined as 0.4600 inch and of No. 36 as 0.0050 inch. The

ratio of any diameter to the diameter of the next greater number $\sqrt[39]{\frac{.4600}{.0050}} = 1.1229322$.

Taken from Circular No. 31. Copper Wire Tables, U.S. Bureau of Standards which contains more complete tables.

SMITHSONIAN TABLES.

Introduction to Wire Tables; Mass and Volume Resistivity of Copper and Aluminum

The following wire tables are abridged from those prepared by the Bureau of Standards at the request and with the cooperation of the Standards Committee of the American Institute of Electrical Engineers (Circular No. 31 of the Bureau of Standards). The standard of copper resistance used is "The International Annealed Copper Standard" as adopted Sept. 5, 1913, by the International Electrotechnical Commission and represents the average commercial high-conductivity copper for the purpose of electric conductors. This standard corresponds to a conductivity of 58×10^{-5} c.g.s. units, and a density of 8.89, at 20° C.

In the various units of mass resistivity and volume resistivity this may be stated as

| |
|-------------------------------------|
| 0.15328 ohm (meter, gram) at 20° C. |
| 875.20 ohms (mile, pound) at 20° C. |
| 1.7241 microhm-cm at 20° C. |
| 0.67879 microhm-inch at 20° C. |
| 10.371 ohms (mil, foot) at 20° C. |

The temperature coefficient for this particular resistivity is $\alpha_{20} = 0.00393$, or $\alpha_0 = 0.00427$. The temperature coefficient of copper is proportional to the conductivity, so that where the conductivity is known the temperature coefficient may be calculated, and vice-versa. Thus the next table shows the temperature coefficients of copper having various percentages of the standard conductivity. A consequence of this relation is that the change of resistivity per degree is constant, independent of the sample of copper and independent of the temperature of reference. This resistivity-temperature constant, for volume resistivity and Centigrade degrees, is 0.00681 microhm cm, and for mass resistivity is 0.000597 ohm (meter, gram).

The density of 8.89 grams per cubic centimeter at 20° C, is equivalent to 0.32117 pounds per cubic inch.

The values in the following tables are for annealed copper of standard resistivity. The user of the tables must apply the proper correction for copper of other resistivity. Hard-drawn copper may be taken as about 2.7 per cent higher resistivity than annealed copper.

The following is a fair average of the chemical content of commercial high conductivity copper:

| | | | |
|----------------|--------|---------------|--------|
| Copper | 99.91% | Sulphur | 0.002% |
| Silver | .03 | Iron | .002 |
| Oxygen | .052 | Nickel | Trace |
| Arsenic | .002 | Lead | " |
| Antimony | .002 | Zinc | " |

The following values are consistent with the data above:

| | |
|--|-------------------------|
| Conductivity at 0° C, in c.g.s. electromagnetic units..... | 62.969×10^{-5} |
| Resistivity at 0° C, in microhm-cms..... | 1.5881 |
| Density at 0° C | 8.90 |
| Coefficient of linear expansion per degree C..... | 0.000017 |
| "Constant mass" temperature coefficient of resistance at 0° C. | 0.00427 |

The aluminum tables are based on a figure for the conductivity published by the U. S. Bureau of Standards, which is the result of many thousands of determinations by the Aluminum Company of America. A volume resistivity of 2.828 microhm-cm and a density of 2.70 may be considered to be good average values for commercial hard-drawn aluminum. These values give:

| | |
|---|------------------------|
| Conductivity at 0° C in c.g.s. electromagnetic units..... | 38.36×10^{-6} |
| Mass resistivity, in ohms (meter, gram) at 20° C..... | 0.0764 |
| " " " (mile, pound) at 20° C..... | 436. |
| Mass per cent conductivity relative to copper..... | 200.7% |
| Volume resistivity, in microhm-cm at 20° C..... | 2.828 |
| " " in microhm-inch at 20° C..... | 1.113 |
| Volume per cent conductivity relative to copper..... | 61.0% |
| Density, in grams per cubic centimeter..... | 2.70 |
| Density, in pounds per cubic inch..... | 0.0975 |

The average chemical content of commercial aluminum wire is

| | |
|----------------|--------|
| Aluminum | 99.57% |
| Silicon | 0.29 |
| Iron | 0.14 |

COPPER WIRE

TABLE 497.—Temperature Coefficients of Copper for Different Initial Temperatures (Centigrade) and Different Conductivities

| Ohms (meter, gram) at 20° C. | Per cent conductivity. | α_0 | α_{15} | α_{20} | α_{25} | α_{30} | α_{50} |
|------------------------------------|---------------------------|----------------------|----------------------|---------------------------|----------------------|----------------------|----------------------|
| 0.161 34 .159 66 | 95% 96% | 0.001 03 0.001 08 | 0.003 80 0.003 85 | 0.003 73 0.003 77 | 0.003 67 0.003 70 | 0.003 60 0.003 64 | 0.003 36 0.003 39 |
| .158 02 .157 53 | 97% 97.3% | .004 13 .004 14 | .003 80 .003 90 | .003 81 .003 82 | .003 74 .003 75 | .003 67 .003 68 | .003 42 .003 43 |
| .156 40 .154 82 | 98% 99% | .004 17 .004 22 | .003 93 .003 97 | .003 85 .003 89 | .003 78 .003 82 | .003 71 .003 74 | .003 45 .003 48 |
| .153 28 .151 70 | 100% 101% | .004 27 .004 31 | .004 01 .004 05 | .003 93 .003 97 | .003 85 .003 89 | .003 78 .003 82 | .003 52 .003 55 |

NOTE.—The fundamental relation between resistance and temperature is the following:

$$R_t = R_{t_1}(1 + \alpha_{t_1}[t - t_1]),$$

where α_{t_1} is the "temperature coefficient," and t_1 is the "initial temperature" or "temperature of reference."

The values of α in the above table exhibit the fact that the temperature coefficient of copper is proportional to the conductivity. The table was calculated by means of the following formula, which holds for any per cent conductivity, n , within commercial ranges, and for centigrade temperatures. (n is considered to be expressed decimally: e.g., if per cent conductivity = 99 per cent, $n = 0.99$.)

$$\alpha_{t_1} = \frac{1}{\frac{1}{n(0.00393)} + (t_1 - 20)}.$$

TABLE 498.—Reduction of Observations to Standard Temperature (Copper)

| Temper- ature C. | Corrections to reduce Resistivity to 20° C. | | | | Factors to reduce Resistance to 20° C. | | | Temper- ature C. |
|---------------------|---|-----------------|-----------------------|-------------------|--|---------------------------------------|--|---------------------|
| | Ohm (meter, gram). | Microhm- cm. | Ohm (mile, pound). | Microhm- inch. | For 96 per cent con- ductivity. | For 98 per cent con- ductivity. | For 100 per cent con- ductivity. | |
| 0 | +0.011 94 | +0.1361 | + 68.20 | +0.053 58 | 1.0816 | 1.0834 | 1.0853 | 0 |
| 5 | + .008 96 | + .1021 | + 51.15 | + .049 18 | 1.0600 | 1.0613 | 1.0626 | 5 |
| 10 | + .005 97 | + .0681 | + 34.10 | + .026 79 | 1.0302 | 1.0401 | 1.0499 | 10 |
| 11 | + .005 37 | + .0612 | + 30.69 | + .024 11 | 1.0352 | 1.0359 | 1.0367 | 11 |
| 12 | + .004 78 | + .0544 | + 27.28 | + .021 43 | 1.0311 | 1.0318 | 1.0325 | 12 |
| 13 | + .004 18 | + .0476 | + 23.87 | + .018 75 | 1.0271 | 1.0277 | 1.0283 | 13 |
| 14 | + .003 58 | + .0408 | + 20.46 | + .016 07 | 1.0232 | 1.0237 | 1.0242 | 14 |
| 15 | + .002 99 | + .0340 | + 17.05 | + .013 40 | 1.0192 | 1.0192 | 1.0200 | 15 |
| 16 | + .002 39 | + .0272 | + 13.64 | + .010 72 | 1.0153 | 1.0156 | 1.0160 | 16 |
| 17 | + .001 79 | + .0204 | + 10.23 | + .008 04 | 1.0114 | 1.0117 | 1.0119 | 17 |
| 18 | + .001 19 | + .0136 | + 6.82 | + .005 36 | 1.0076 | 1.0078 | 1.0079 | 18 |
| 19 | + .000 60 | + .0068 | + 3.41 | + .002 68 | 1.0038 | 1.0039 | 1.0039 | 19 |
| 20 | 0 | 0 | 0 | 0 | 1.0000 | 1.0000 | 1.0000 | 20 |
| 21 | — .000 60 | — .0068 | — 3.41 | — .002 68 | 0.9962 | 0.9962 | 0.9961 | 21 |
| 22 | — .001 19 | — .0136 | — 6.82 | — .005 36 | .9925 | .9924 | .9922 | 22 |
| 23 | — .001 79 | — .0204 | — 10.23 | — .008 04 | .9888 | .9886 | .9883 | 23 |
| 24 | — .002 39 | — .0272 | — 13.64 | — .010 72 | .9851 | .9848 | .9845 | 24 |
| 25 | — .002 99 | — .0340 | — 17.05 | — .013 40 | .9815 | .9811 | .9807 | 25 |
| 26 | — .003 58 | — .0408 | — 20.46 | — .016 07 | .9779 | .9774 | .9770 | 26 |
| 27 | — .004 18 | — .0476 | — 23.87 | — .018 75 | .9743 | .9737 | .9732 | 27 |
| 28 | — .004 78 | — .0544 | — 27.28 | — .021 43 | .9707 | .9701 | .9695 | 28 |
| 29 | — .005 37 | — .0612 | — 30.69 | — .024 11 | .9672 | .9665 | .9658 | 29 |
| 30 | — .005 97 | — .0681 | — 34.10 | — .026 79 | .9636 | .9629 | .9622 | 30 |
| 35 | — .008 96 | — .1021 | — 51.15 | — .049 18 | .9464 | .9454 | .9443 | 35 |
| 40 | — .011 94 | — .1361 | — 68.20 | — .053 58 | .9298 | .9285 | .9271 | 40 |
| 45 | — .014 93 | — .1701 | — 85.25 | — .066 08 | .9138 | .9122 | .9105 | 45 |
| 50 | — .017 92 | — .2042 | — 102.30 | — .080 37 | .8983 | .8964 | .8945 | 50 |
| 55 | — .020 90 | — .2382 | — 119.35 | — .093 76 | .8833 | .8812 | .8791 | 55 |
| 60 | — .023 89 | — .2722 | — 136.40 | — .107 16 | .8680 | .8665 | .8642 | 60 |
| 65 | — .026 87 | — .3062 | — 153.45 | — .120 56 | .8549 | .8523 | .8497 | 65 |
| 70 | — .029 86 | — .3403 | — 170.50 | — .133 95 | .8413 | .8385 | .8358 | 70 |
| 75 | — .032 85 | — .3743 | — 187.55 | — .147 34 | .8281 | .8252 | .8223 | 75 |

WIRE TABLE, STANDARD ANNEALED COPPER

American Wire Gage (B. & S.). English Units

| Gage No. | Diameter in Mils. at 20° C. | Cross-Section at 20° C. | | Ohms per 1000 Feet.* | | | |
|----------|-----------------------------|-------------------------|----------------|----------------------|---------------------|----------------------|----------------------|
| | | Circular Mils. | Square Inches. | 0° C (= 32° F.) | 20° C (= 68° F.) | 50° C (= 122° F.) | 75° C (= 167° F.) |
| 0000 | 460.0 | 211 600. | .01662 | .0045 16 | .0049 01 | .0054 79 | .0059 61 |
| 000 | 409.6 | 167 800. | .1318 | .050 95 | .061 80 | .069 09 | .075 16 |
| 00 | 364.8 | 133 100. | .1045 | .071 81 | .077 93 | .087 12 | .094 78 |
| 0 | 324.9 | 105 500. | .082 89 | .090 55 | .098 27 | .1099 | .1195 |
| 1 | 289.3 | 83 600. | .065 73 | .1142 | .1239 | .1385 | .1507 |
| 2 | 257.6 | 66 370. | .052 13 | .1440 | .1563 | .1747 | .1900 |
| 3 | 229.4 | 52 640. | .041 34 | .1816 | .1970 | .2203 | .2396 |
| 4 | 204.3 | 41 740. | .032 78 | .2289 | .2485 | .2778 | .3022 |
| 5 | 181.9 | 33 100. | .026 00 | .2887 | .3133 | .3502 | .3810 |
| 6 | 162.0 | 26 250. | .020 62 | .3640 | .3951 | .4416 | .4805 |
| 7 | 144.3 | 20 820. | .016 35 | .4590 | .4982 | .5509 | .6050 |
| 8 | 128.5 | 16 510. | .012 97 | .5788 | .6282 | .7023 | .7640 |
| 9 | 114.4 | 13 090. | .010 28 | .7299 | .7921 | .8855 | .9633 |
| 10 | 101.9 | 10 380. | .008 155 | .9203 | .9989 | 1.117 | 1.215 |
| 11 | 90.74 | 8234. | .006 467 | 1.161 | 1.260 | 1.408 | 1.532 |
| 12 | 80.81 | 6530. | .005 129 | 1.463 | 1.588 | 1.775 | 1.931 |
| 13 | 71.96 | 5178. | .004 067 | 1.845 | 2.003 | 2.239 | 2.436 |
| 14 | 64.08 | 4107. | .003 225 | 2.327 | 2.525 | 2.823 | 3.071 |
| 15 | 57.07 | 3257. | .002 558 | 2.934 | 3.184 | 3.560 | 3.873 |
| 16 | 50.82 | 2583. | .002 028 | 3.700 | 4.016 | 4.489 | 4.884 |
| 17 | 45.26 | 2048. | .001 609 | 4.666 | 5.064 | 5.660 | 6.158 |
| 18 | 40.30 | 1624. | .001 276 | 5.883 | 6.385 | 7.138 | 7.765 |
| 19 | 35.89 | 1288. | .001 012 | 7.418 | 8.051 | 9.001 | 9.792 |
| 20 | 31.96 | 1022. | .000 802 3 | 9.355 | 10.15 | 11.35 | 12.35 |
| 21 | 28.45 | 810.1 | .000 636 3 | 11.80 | 12.80 | 14.31 | 15.57 |
| 22 | 25.35 | 642.4 | .000 504 6 | 14.87 | 16.14 | 18.05 | 19.63 |
| 23 | 22.57 | 509.5 | .000 400 2 | 18.76 | 20.36 | 22.76 | 24.76 |
| 24 | 20.10 | 404.0 | .000 317 3 | 23.65 | 25.67 | 28.70 | 31.22 |
| 25 | 17.90 | 320.4 | .000 251 7 | 29.82 | 32.37 | 36.18 | 39.36 |
| 26 | 15.94 | 254.1 | .000 199 6 | 37.61 | 40.81 | 45.63 | 49.64 |
| 27 | 14.20 | 201.5 | .000 158 3 | 47.42 | 51.47 | 57.53 | 62.59 |
| 28 | 12.64 | 159.8 | .000 125 5 | 59.80 | 64.90 | 72.55 | 78.93 |
| 29 | 11.26 | 126.7 | .000 099 53 | 75.40 | 81 83 | 91.48 | 99.52 |
| 30 | 10.03 | 100.5 | .000 078 94 | 95.08 | 103.2 | 115.4 | 125.5 |
| 31 | 8.928 | 79.70 | .000 062 60 | 119.9 | 130.1 | 145.5 | 158.2 |
| 32 | 7.950 | 63.21 | .000 049 64 | 151.2 | 164.1 | 183.4 | 199.5 |
| 33 | 7.080 | 50.13 | .000 039 37 | 190.6 | 206.9 | 231.3 | 251.6 |
| 34 | 6.305 | 39.75 | .000 031 22 | 240.4 | 260.9 | 291.7 | 317.3 |
| 35 | 5.615 | 31.52 | .000 024 76 | 303.1 | 329.0 | 367.8 | 400.1 |
| 36 | 5.000 | 25.00 | .000 019 64 | 382.2 | 414.8 | 463.7 | 504.5 |
| 37 | 4.453 | 19.83 | .000 015 57 | 482.0 | 523.1 | 584.8 | 636.2 |
| 38 | 3.965 | 15.72 | .000 012 35 | 607.8 | 659.6 | 737.4 | 802.2 |
| 39 | 3.531 | 12.47 | .000 009 793 | 766.4 | 831.8 | 929.8 | 1012. |
| 40 | 3.145 | 9.888 | .000 007 766 | 966.5 | 1049. | 1173. | 1276. |

* Resistance at the stated temperatures of a wire whose length is 1000 feet at 20° C.

WIRE TABLE, STANDARD ANNEALED COPPER

American Wire Gage (B. & S.). English Units

| Gage No. | Diameter in Mils. at 20° C. | Pounds per 1000 Feet. | Feet per Pound. | Feet per Ohm.* | | | |
|----------|-----------------------------|-----------------------|-----------------|--------------------|---------------------|----------------------|----------------------|
| | | | | 0° C. (=32° F.) | 20° C. (=68° F.) | 50° C. (=122° F.) | 75° C. (=167° F.) |
| 0000 | 460.0 | 640.5 | 1.561 | 22 140. | 20 400. | 18 250. | 16 780. |
| 000 | 409.6 | 507.9 | 1.968 | 17 560. | 16 180. | 14 470. | 13 300. |
| 00 | 364.8 | 402.8 | 2.482 | 13 930. | 12 830. | 11 480. | 10 550. |
| 0 | 324.9 | 319.5 | 3.130 | 11 040. | 10 180. | 9 103. | 8 367. |
| 1 | 289.3 | 253.3 | 3.947 | 8758. | 8070. | 7219. | 6636. |
| 2 | 257.6 | 200.9 | 4.977 | 6946. | 6400. | 5725. | 5202. |
| 3 | 229.4 | 159.3 | 6.276 | 5508. | 5075. | 4540. | 4173. |
| 4 | 204.3 | 126.4 | 7.914 | 4368. | 4025. | 3600. | 3309. |
| 5 | 181.9 | 100.2 | 9.980 | 3464. | 3192. | 2855. | 2625. |
| 6 | 162.0 | 79.46 | 12.58 | 2747. | 2531. | 2264. | 2081. |
| 7 | 144.3 | 63.02 | 15.87 | 2179. | 2007. | 1796. | 1651. |
| 8 | 128.5 | 49.98 | 20.01 | 1728. | 1592. | 1424. | 1309. |
| 9 | 114.4 | 39.63 | 25.23 | 1370. | 1262. | 1129. | 1038. |
| 10 | 101.9 | 31.43 | 31.82 | 1087. | 1001. | 895.6 | 823.2 |
| 11 | 90.74 | 24.92 | 40.12 | 861.7 | 794.0 | 710.2 | 652.8 |
| 12 | 80.81 | 19.77 | 50.59 | 683.3 | 629.6 | 563.2 | 517.7 |
| 13 | 71.96 | 15.68 | 63.80 | 541.9 | 499.3 | 446.7 | 410.6 |
| 14 | 64.08 | 12.43 | 80.44 | 429.8 | 396.0 | 354.2 | 325.6 |
| 15 | 57.07 | 9.858 | 101.4 | 340.8 | 314.0 | 280.9 | 258.2 |
| 16 | 50.82 | 7.818 | 127.9 | 270.3 | 249.0 | 222.8 | 204.8 |
| 17 | 45.26 | 6.200 | 161.3 | 214.3 | 197.5 | 176.7 | 162.4 |
| 18 | 40.30 | 4.917 | 203.4 | 170.0 | 156.6 | 140.1 | 128.8 |
| 19 | 35.89 | 3.899 | 256.5 | 134.8 | 124.2 | 111.1 | 102.1 |
| 20 | 31.96 | 3.092 | 323.4 | 106.9 | 98.50 | 88.11 | 80.99 |
| 21 | 28.46 | 2.452 | 407.8 | 84.78 | 78.11 | 69.87 | 64.23 |
| 22 | 25.35 | 1.945 | 514.2 | 67.23 | 61.95 | 55.41 | 50.94 |
| 23 | 22.57 | 1.542 | 648.4 | 53.32 | 49.13 | 43.94 | 40.39 |
| 24 | 20.10 | 1.223 | 817.7 | 42.28 | 38.96 | 34.85 | 32.03 |
| 25 | 17.90 | 0.9699 | 1031. | 33.53 | 30.90 | 27.64 | 25.40 |
| 26 | 15.94 | .7692 | 1300. | 26.59 | 24.50 | 21.92 | 20.15 |
| 27 | 14.20 | .6100 | 1639. | 21.09 | 19.43 | 17.38 | 15.98 |
| 28 | 12.64 | .4837 | 2067. | 16.72 | 15.41 | 13.78 | 12.67 |
| 29 | 11.26 | .3836 | 2607. | 13.26 | 12.22 | 10.93 | 10.05 |
| 30 | 10.03 | .3042 | 3287. | 10.52 | 9.691 | 8.669 | 7.968 |
| 31 | 8.928 | .2413 | 4145. | 8.341 | 7.685 | 6.875 | 6.319 |
| 32 | 7.950 | .1913 | 5227. | 6.614 | 6.095 | 5.452 | 5.011 |
| 33 | 7.080 | .1517 | 6591. | 5.245 | 4.833 | 4.323 | 3.974 |
| 34 | 6.395 | .1203 | 8310. | 4.160 | 3.833 | 3.429 | 3.152 |
| 35 | 5.615 | .095 42 | 10 480. | 3.299 | 3.040 | 2.719 | 2.499 |
| 36 | 5.000 | .075 68 | 13 210. | 2.616 | 2.411 | 2.156 | 1.982 |
| 37 | 4.453 | .060 01 | 16 660. | 2.075 | 1.912 | 1.710 | 1.572 |
| 38 | 3.965 | .047 59 | 21 010. | 1.645 | 1.516 | 1.356 | 1.247 |
| 39 | 3.531 | .037 74 | 26 500. | 1.305 | 1.202 | 1.075 | 0.9886 |
| 40 | 3.145 | .029 93 | 33 410. | 1.035 | 0.9534 | 0.8529 | .7840 |

* Length at 20° C of a wire whose resistance is 1 ohm at the stated temperatures.

WIRE TABLE, STANDARD ANNEALED COPPER

American Wire Gage (B. & S.). English Units

| Gage No. | Diameter in Mils. at 20° C. | Ohms per Pound. | | | Pounds per Ohm. |
|----------|-----------------------------|---------------------|----------------------|-----------------------|----------------------|
| | | 0° C. (= 32° F.) | 20° C. (= 68° F.) | 50° C. (= 122° F.) | 20° C. (= 68° F.) |
| 0000 | 460.0 | 0.000 070 51 | 0.000 076 52 | 0.000 085 54 | 13 070. |
| 000 | 409.6 | .000 1121 | .000 1217 | .000 1360 | 8219. |
| 00 | 364.8 | .000 1783 | .000 1935 | .000 2163 | 5169. |
| 0 | 324.9 | .000 2835 | .000 3076 | .000 3439 | 3251. |
| 1 | 289.3 | .000 4507 | .000 4891 | .000 5408 | 2044. |
| 2 | 257.6 | .000 7166 | .000 7778 | .000 8695 | 1286. |
| 3 | 229.4 | .001 140 | .001 237 | .001 383 | 808.6 |
| 4 | 204.3 | .001 812 | .001 966 | .002 198 | 508.5 |
| 5 | 181.9 | .002 881 | .003 127 | .003 495 | 319.8 |
| 6 | 162.0 | .004 581 | .004 972 | .005 558 | 201.1 |
| 7 | 144.3 | .007 284 | .007 905 | .008 838 | 126.5 |
| 8 | 128.5 | .011 58 | .012 57 | .014 05 | 79.55 |
| 9 | 114.4 | .018 42 | .019 99 | .022 34 | 50.03 |
| 10 | 101.9 | .029 28 | .031 78 | .035 53 | 31.47 |
| 11 | 90.74 | .046 56 | .050 53 | .056 49 | 19.79 |
| 12 | 80.81 | .074 04 | .080 35 | .089 83 | 12.45 |
| 13 | 71.96 | .1177 | .1278 | .1428 | 7.827 |
| 14 | 64.68 | .1872 | .2032 | .2271 | 4.922 |
| 15 | 57.07 | .2976 | .3230 | .3611 | 3.096 |
| 16 | 50.82 | .4733 | .5136 | .5742 | 1.947 |
| 17 | 45.26 | .7525 | .8167 | .9130 | 1.224 |
| 18 | 40.30 | 1.197 | 1.299 | 1.452 | 0.7700 |
| 19 | 35.89 | 1.903 | 2.065 | 2.308 | .4843 |
| 20 | 31.96 | 3.025 | 3.283 | 3.670 | .3046 |
| 21 | 28.46 | 4.810 | 5.221 | 5.836 | .1915 |
| 22 | 25.35 | 7.649 | 8.301 | 9.280 | .1205 |
| 23 | 22.57 | 12.16 | 13.20 | 14.76 | .075 76 |
| 24 | 20.10 | 19.34 | 20.99 | 23.46 | .047 65 |
| 25 | 17.90 | 30.75 | 33.37 | 37.31 | .029 97 |
| 26 | 15.94 | 48.89 | 53.06 | 59.32 | .018 85 |
| 27 | 14.20 | 77.74 | 84.37 | 94.32 | .011 85 |
| 28 | 12.64 | 123.6 | 134.2 | 150.0 | .007 454 |
| 29 | 11.26 | 196.6 | 213.3 | 238.5 | .004 688 |
| 30 | 10.03 | 312.5 | 339.2 | 379.2 | .002 948 |
| 31 | 8.928 | 497.0 | 539.3 | 602.9 | .001 854 |
| 32 | 7.950 | 790.2 | 857.6 | 958.7 | .001 166 |
| 33 | 7.080 | 1256. | 1364. | 1524. | .000 7333 |
| 34 | 6.305 | 1998. | 2168. | 2424. | .000 4612 |
| 35 | 5.615 | 3177. | 3448. | 3854. | .000 2901 |
| 36 | 5.000 | 5051. | 5482. | 6128. | .000 1824 |
| 37 | 4.453 | 8032. | 8717. | 9744. | .000 1147 |
| 38 | 3.965 | 12 770. | 13 860. | 15 490. | .000 072 15 |
| 39 | 3.531 | 20 310. | 22 040. | 24 640. | .000 045 38 |
| 40 | 3.145 | 32 290. | 35 040. | 39 170. | .000 028 54 |

WIRE TABLE, STANDARD ANNEALED COPPER

American Wire Gage (B. & S.). Metric Units

| Gage No. | Diameter in mm at 20° C. | Cross Section in mm ² at 20° C. | Ohms per Kilometer.* | | | |
|----------|--------------------------|--|----------------------|--------|--------|--------|
| | | | 0° C. | 20° C. | 50° C. | 75° C. |
| 0000 | 11.68 | 107.2 | 0.1482 | 0.1668 | 0.1798 | 0.1936 |
| 000 | 10.40 | 85.03 | .1868 | .2028 | .2267 | .2466 |
| 00 | 9.266 | 67.43 | .2356 | .2557 | .2858 | .3110 |
| 0 | 8.252 | 53.48 | .2971 | .3224 | .3604 | .3921 |
| 1 | 7.348 | 42.41 | .3746 | .4066 | .4545 | .4944 |
| 2 | 6.544 | 33.63 | .4724 | .5127 | .5731 | .6235 |
| 3 | 5.827 | 26.67 | .5956 | .6465 | .7227 | .7862 |
| 4 | 5.189 | 21.15 | .7511 | .8152 | .9113 | .9914 |
| 5 | 4.621 | 16.77 | .9471 | 1.028 | 1.149 | 1.250 |
| 6 | 4.115 | 13.30 | 1.194 | 1.296 | 1.449 | 1.576 |
| 7 | 3.665 | 10.55 | 1.506 | 1.634 | 1.827 | 1.988 |
| 8 | 3.264 | 8.366 | 1.899 | 2.061 | 2.304 | 2.506 |
| 9 | 2.906 | 6.634 | 2.395 | 2.599 | 2.905 | 3.161 |
| 10 | 2.588 | 5.261 | 3.020 | 3.277 | 3.663 | 3.985 |
| 11 | 2.305 | 4.172 | 3.807 | 4.132 | 4.619 | 5.025 |
| 12 | 2.053 | 3.309 | 4.801 | 5.211 | 5.825 | 6.337 |
| 13 | 1.828 | 2.624 | 6.054 | 6.571 | 7.345 | 7.991 |
| 14 | 1.628 | 2.081 | 7.634 | 8.285 | 9.262 | 10.08 |
| 15 | 1.450 | 1.650 | 9.627 | 10.45 | 11.68 | 12.71 |
| 16 | 1.291 | 1.309 | 12.14 | 13.17 | 14.73 | 16.02 |
| 17 | 1.150 | 1.038 | 15.31 | 16.61 | 18.57 | 20.20 |
| 18 | 1.024 | 0.8231 | 19.30 | 20.95 | 23.42 | 25.48 |
| 19 | 0.9116 | .6527 | 24.34 | 26.42 | 29.53 | 32.12 |
| 20 | .8118 | .5176 | 30.69 | 33.31 | 37.24 | 40.51 |
| 21 | .7230 | .4105 | 38.70 | 42.00 | 46.95 | 51.08 |
| 22 | .6438 | .3255 | 48.80 | 52.96 | 59.21 | 64.41 |
| 23 | .5733 | .2582 | 61.54 | 66.79 | 74.66 | 81.22 |
| 24 | .5106 | .2047 | 77.60 | 84.21 | 94.14 | 102.4 |
| 25 | .4547 | .1624 | 97.85 | 106.2 | 118.7 | 129.1 |
| 26 | .4049 | .1288 | 123.4 | 133.9 | 149.7 | 162.9 |
| 27 | .3606 | .1021 | 155.6 | 168.9 | 188.8 | 205.4 |
| 28 | .3211 | .08098 | 196.2 | 212.0 | 238.0 | 258.9 |
| 29 | .2859 | .06422 | 247.4 | 268.5 | 300.1 | 326.5 |
| 30 | .2546 | .05093 | 311.9 | 338.6 | 378.5 | 411.7 |
| 31 | .2268 | .04039 | 393.4 | 426.9 | 477.2 | 510.2 |
| 32 | .2019 | .03203 | 496.0 | 538.3 | 601.8 | 654.7 |
| 33 | .1798 | .02540 | 625.5 | 678.8 | 758.8 | 825.5 |
| 34 | .1601 | .02014 | 788.7 | 856.0 | 956.9 | 1041. |
| 35 | .1426 | .01597 | 994.5 | 1079. | 1207. | 1313. |
| 36 | .1270 | .01267 | 1254. | 1361. | 1522. | 1655. |
| 37 | .1131 | .01005 | 1581. | 1716. | 1919. | 2087. |
| 38 | .1007 | .007967 | 1994. | 2164. | 2419. | 2632. |
| 39 | .08969 | .006318 | 2514. | 2729. | 3051. | 3319. |
| 40 | .07987 | .005010 | 3171. | 3441. | 3847. | 4185. |

*Resistance at the stated temperatures of a wire whose length is 1 kilometer at 20° C.

WIRE TABLE, STANDARD ANNEALED COPPER

American Wire Gage (B. & S.), Metric Units

| Gage No. | Diameter in mm at 20° C. | Kilograms per Kilometer. | Meters per Gram. | Meters per Ohm.* | | | |
|----------|--------------------------|--------------------------|------------------|------------------|--------|--------|--------|
| | | | | 0° C. | 20° C. | 50° C. | 75° C. |
| 0000 | 11.68 | 953.2 | 0.001 049 | 6749. | 6219. | 5563. | 5113. |
| 000 | 10.40 | 755.9 | .001 323 | 5352. | 4932. | 4412. | 4055. |
| 00 | 9.266 | 599.5 | .001 668 | 4245. | 3911. | 3499. | 3216. |
| 0 | 8.252 | 475.4 | .002 103 | 3366. | 3102. | 2774. | 2550. |
| 1 | 7.348 | 377.0 | .002 652 | 2669. | 2460. | 2200. | 2022. |
| 2 | 6.544 | 299.0 | .003 345 | 2117. | 1951. | 1745. | 1604. |
| 3 | 5.827 | 237.1 | .004 217 | 1679. | 1547. | 1384. | 1272. |
| 4 | 5.189 | 188.0 | .005 318 | 1331. | 1227. | 1097. | 1009. |
| 5 | 4.621 | 149.1 | .006 706 | 1056. | 972.9 | 870.2 | 799.9 |
| 6 | 4.115 | 118.2 | .008 457 | 837.3 | 771.5 | 690.1 | 634.4 |
| 7 | 3.665 | 93.78 | .010 66 | 664.0 | 611.8 | 547.3 | 503.1 |
| 8 | 3.264 | 74.37 | .013 45 | 526.6 | 485.2 | 434.0 | 399.0 |
| 9 | 2.906 | 58.98 | .016 96 | 417.6 | 384.8 | 344.2 | 316.4 |
| 10 | 2.588 | 46.77 | .021 38 | 331.2 | 305.1 | 273.0 | 250.9 |
| 11 | 2.305 | 37.09 | .026 96 | 262.6 | 242.0 | 216.5 | 199.0 |
| 12 | 2.053 | 29.42 | .034 00 | 208.3 | 191.9 | 171.7 | 157.8 |
| 13 | 1.828 | 23.33 | .042 87 | 165.2 | 152.2 | 136.1 | 125.1 |
| 14 | 1.628 | 18.50 | .054 06 | 131.0 | 120.7 | 108.0 | 99.24 |
| 15 | 1.450 | 14.67 | .068 16 | 103.9 | 95.71 | 85.62 | 78.70 |
| 16 | 1.291 | 11.63 | .085 95 | 82.38 | 75.90 | 67.90 | 62.41 |
| 17 | 1.150 | 9.226 | .1084 | 65.33 | 60.20 | 53.85 | 49.50 |
| 18 | 1.024 | 7.317 | .1367 | 51.81 | 47.74 | 42.70 | 39.25 |
| 19 | 0.9116 | 5.803 | .1723 | 41.09 | 37.86 | 33.86 | 31.13 |
| 20 | .8118 | 4.602 | .2173 | 32.58 | 30.02 | 26.86 | 24.69 |
| 21 | .7230 | 3.649 | .2740 | 25.84 | 23.81 | 21.30 | 19.58 |
| 22 | .6438 | 2.894 | .3455 | 20.49 | 18.88 | 16.89 | 15.53 |
| 23 | .5733 | 2.295 | .4357 | 16.25 | 14.97 | 13.39 | 12.31 |
| 24 | .5106 | 1.820 | .5494 | 12.89 | 11.87 | 10.62 | 9.764 |
| 25 | .4547 | 1.443 | .6928 | 10.22 | 9.417 | 8.424 | 7.743 |
| 26 | .4049 | 1.145 | .8736 | 8.105 | 7.468 | 6.680 | 6.141 |
| 27 | .3606 | 0.9078 | 1.102 | 6.428 | 5.922 | 5.298 | 4.870 |
| 28 | .3211 | .7199 | 1.389 | 5.097 | 4.697 | 4.201 | 3.862 |
| 29 | .2859 | .5709 | 1.752 | 4.042 | 3.725 | 3.332 | 3.063 |
| 30 | .2546 | .4527 | 2.209 | 3.206 | 2.954 | 2.642 | 2.429 |
| 31 | .2268 | .3590 | 2.785 | 2.542 | 2.342 | 2.095 | 1.926 |
| 32 | .2019 | .2847 | 3.512 | 2.016 | 1.858 | 1.662 | 1.527 |
| 33 | .1798 | .2258 | 4.429 | 1.599 | 1.473 | 1.318 | 1.211 |
| 34 | .1601 | .1791 | 5.584 | 1.268 | 1.168 | 1.045 | 0.9606 |
| 35 | .1426 | .1420 | 7.042 | 1.006 | 0.9265 | 0.8288 | .7618 |
| 36 | .1270 | .1126 | 8.879 | 0.7974 | .7347 | .6572 | .6041 |
| 37 | .1131 | .089 31 | 11.20 | .6324 | .5827 | .5212 | .4791 |
| 38 | .1007 | .070 83 | 14.12 | .5015 | .4621 | .4133 | .3799 |
| 39 | .089 69 | .056 17 | 17.80 | .3977 | .3664 | .3278 | .3013 |
| 40 | .079 87 | .044 54 | 22.45 | .3154 | .2906 | .2600 | .2390 |

* Length at 20° C. of a wire whose resistance is 1 ohm at the stated temperatures.

WIRE TABLE, STANDARD ANNEALED COPPER

American Wire Gage (B. & S.). Metric Units

| Gage No. | Diameter in mm at 20° C. | Ohms per Kilogram. | | | Grams per Ohm. |
|----------|--------------------------|--------------------|-------------|-------------|----------------|
| | | 0° C. | 20° C. | 50° C. | |
| 0000 | 11.68 | 0.000 155 4 | 0.000 168 7 | 0.000 188 6 | 5 928 000. |
| 000 | 10.40 | .000 247 2 | .000 268 2 | .000 299 9 | 3 728 000. |
| 00 | 9.266 | .000 393 0 | .000 426 5 | .000 476 8 | 2 344 000. |
| 0 | 8.252 | .000 624 9 | .000 678 2 | .000 758 2 | 1 474 000. |
| 1 | 7.348 | .000 993 6 | .001 078 | .001 206 | 927 300. |
| 2 | 6.544 | .001 580 | .001 715 | .001 917 | 583 200. |
| 3 | 5.827 | .002 512 | .002 726 | .003 048 | 366 800. |
| 4 | 5.189 | .003 995 | .004 335 | .004 846 | 230 700. |
| 5 | 4.621 | .006 352 | .006 893 | .007 706 | 145 100. |
| 6 | 4.115 | .010 10 | .010 96 | .012 25 | 91 230. |
| 7 | 3.605 | .016 06 | .017 43 | .019 48 | 57 380. |
| 8 | 3.264 | .025 53 | .027 71 | .030 98 | 36 080. |
| 9 | 2.906 | .040 60 | .044 06 | .049 26 | 22 690. |
| 10 | 2.588 | .064 56 | .070 07 | .078 33 | 14 270. |
| 11 | 2.305 | .1026 | .1114 | .1245 | 8976. |
| 12 | 2.053 | .1632 | .1771 | .1980 | 5645 |
| 13 | 1.828 | .2595 | .2817 | .3149 | 3559. |
| 14 | 1.628 | .4127 | .4479 | .5007 | 2233. |
| 15 | 1.450 | .6562 | .7122 | .7961 | 1404. |
| 16 | 1.291 | 1.043 | 1.132 | 1.266 | 883.1 |
| 17 | 1.150 | 1.659 | 1.801 | 2.013 | 555.4 |
| 18 | 1.024 | 2.638 | 2.863 | 3.201 | 349.3 |
| 19 | 0.9116 | 4.194 | 4.552 | 5.089 | 219.7 |
| 20 | .8118 | 6.670 | 7.238 | 8.092 | 138.2 |
| 21 | .7230 | 10.60 | 11.51 | 12.87 | 86.88 |
| 22 | .6438 | 16.86 | 18.30 | 20.46 | 54.64 |
| 23 | .5733 | 26.81 | 29.10 | 32.53 | 34.36 |
| 24 | .5106 | 42.63 | 46.27 | 51.73 | 21.61 |
| 25 | .4547 | 67.79 | 73.57 | 82.25 | 13.59 |
| 26 | .4049 | 107.8 | 117.0 | 130.8 | 8.548 |
| 27 | .3606 | 171.4 | 186.0 | 207.9 | 5.376 |
| 28 | .3211 | 272.5 | 295.8 | 330.6 | 3.381 |
| 29 | .2859 | 433.3 | 470.3 | 525.7 | 2.126 |
| 30 | .2546 | 689.0 | 747.8 | 836.0 | 1.337 |
| 31 | .2268 | 1090. | 1189. | 1329. | 0.8410 |
| 32 | .2019 | 1742. | 1891. | 2114. | .5289 |
| 33 | .1798 | 2770. | 3006. | 3361. | .3326 |
| 34 | .1601 | 4404. | 4780. | 5344. | .2092 |
| 35 | .1426 | 7003. | 7601. | 8497. | .1316 |
| 36 | .1270 | 11140. | 12090. | 13510. | .082 74 |
| 37 | .1131 | 17710. | 19220. | 21480. | .052 04 |
| 38 | .1007 | 28150. | 30560. | 34100. | .032 73 |
| 39 | .089 69 | 44770. | 48590. | 54310. | .020 58 |
| 40 | .079 87 | 71180. | 77260. | 86360. | .012 94 |

WIRE TABLE, ALUMINUM

Hard-Drawn Aluminum Wire at 20° C (68° F.)

American Wire Gage (B. & S.). English Units

| Gage No. | Diameter in Mils. | Cross Section. | | Ohms per 1000 Feet. | Pounds per 1000 Feet. | Pounds per Ohm. | Feet per Ohm. |
|----------|-------------------|----------------|----------------|---------------------|-----------------------|-----------------|---------------|
| | | Circular Mils. | Square Inches. | | | | |
| 0000 | 460. | 212 000. | 0.166 | 0.0804 | 195. | 2420. | 12 400. |
| 000 | 410. | 168 000. | .132 | .101 | 154. | 1520. | 9860. |
| 00 | 365. | 133 000. | .105 | .128 | 122. | 957. | 7820. |
| 0 | 325. | 106 000. | .0829 | .161 | 97.0 | 602. | 6200. |
| 1 | 289. | 83 700. | .0657 | .203 | 76.9 | 379. | 4920. |
| 2 | 258. | 66 400. | .0521 | .256 | 61.0 | 238. | 3900. |
| 3 | 229. | 52 600. | .0413 | .323 | 48.4 | 150. | 3090. |
| 4 | 204. | 41 700. | .0328 | .408 | 38.4 | 94.2 | 2450. |
| 5 | 182. | 33 100. | .0260 | .514 | 30.4 | 59.2 | 1950. |
| 6 | 162. | 26 300. | .0206 | .648 | 24.1 | 37.2 | 1540. |
| 7 | 144. | 20 800. | .0164 | .817 | 19.1 | 23.4 | 1220. |
| 8 | 128. | 16 500. | .0130 | 1.03 | 15.2 | 14.7 | 970. |
| 9 | 114. | 13 100. | .0103 | 1.30 | 12.0 | 9.26 | 770. |
| 10 | 102. | 10 400. | .008 15 | 1.64 | 9.55 | 5.83 | 610. |
| 11 | 91. | 8230. | .006 47 | 2.07 | 7.57 | 3.66 | 484. |
| 12 | 81. | 6530. | .005 13 | 2.61 | 6.00 | 2.30 | 384. |
| 13 | 72. | 5180. | .004 07 | 3.29 | 4.76 | 1.45 | 304. |
| 14 | 64. | 4110. | .003 23 | 4.14 | 3.78 | 0.911 | 241. |
| 15 | 57. | 3260. | .002 56 | 5.22 | 2.99 | .573 | 191. |
| 16 | 51. | 2580. | .002 03 | 6.59 | 2.37 | .360 | 152. |
| 17 | 45. | 2050. | .001 61 | 8.31 | 1.88 | .227 | 120. |
| 18 | 40. | 1620. | .001 28 | 10.5 | 1.49 | .143 | 95.5 |
| 19 | 36. | 1290. | .001 01 | 13.2 | 1.18 | .0897 | 75.7 |
| 20 | 32. | 1020. | .000 802 | 16.7 | 0.939 | .0564 | 60.0 |
| 21 | 28.5 | 810. | .000 636 | 21.0 | .745 | .0355 | 47.6 |
| 22 | 25.3 | 642. | .000 505 | 26.5 | .591 | .0223 | 37.8 |
| 23 | 22.6 | 509. | .000 400 | 33.4 | .468 | .0140 | 29.9 |
| 24 | 20.1 | 404. | .000 317 | 42.1 | .371 | .008 82 | 23.7 |
| 25 | 17.9 | 320. | .000 252 | 53.1 | .295 | .005 55 | 18.8 |
| 26 | 15.9 | 254. | .000 200 | 67.0 | .234 | .003 49 | 14.9 |
| 27 | 14.2 | 202. | .000 158 | 84.4 | .185 | .002 19 | 11.8 |
| 28 | 12.6 | 160. | .000 126 | 106. | .147 | .001 38 | 9.39 |
| 29 | 11.3 | 127. | .000 099 5 | 134. | .117 | .000 868 | 7.45 |
| 30 | 10.0 | 101. | .000 078 9 | 169. | .0924 | .000 546 | 5.91 |
| 31 | 8.9 | 79.7 | .000 062 6 | 213. | .0733 | .000 343 | 4.68 |
| 32 | 8.0 | 63.2 | .000 049 6 | 269. | .0581 | .000 216 | 3.72 |
| 33 | 7.1 | 50.1 | .000 039 4 | 339. | .0461 | .000 136 | 2.95 |
| 34 | 6.3 | 39.8 | .000 031 2 | 428. | .0365 | .000 085 4 | 2.34 |
| 35 | 5.6 | 31.5 | .000 024 8 | 540. | .0290 | .000 053 7 | 1.85 |
| 36 | 5.0 | 25.0 | .000 019 6 | 681. | .0230 | .000 033 8 | 1.47 |
| 37 | 4.5 | 19.8 | .000 015 6 | 858. | .0182 | .000 021 2 | 1.17 |
| 38 | 4.0 | 15.7 | .000 012 3 | 1080. | .0145 | .000 013 4 | 0.924 |
| 39 | 3.5 | 12.5 | .000 009 79 | 1360. | .0115 | .000 008 40 | .733 |
| 40 | 3.1 | 9.9 | .000 007 77 | 1720. | .0091 | .000 005 28 | .581 |

WIRE TABLE, ALUMINUM

Hard-Drawn Aluminum Wire at 20° C (68° F.)

American Wire Gage (B. & S.). Metric Units

| Gage No. | Diameter in mm. | Cross Section in mm. ² | Ohms per Kilometer. | Kilograms per Kilometer. | Grams per Ohm. | Meters per Ohm. |
|----------|-----------------|-----------------------------------|---------------------|--------------------------|----------------|-----------------|
| 0000 | 11.7 | 107. | 0.264 | 289. | 1 100 000. | 3790. |
| 000 | 10.4 | 85.0 | .333 | 230. | 690 000. | 3010. |
| 00 | 9.3 | 67.4 | .419 | 182. | 434 000. | 2380. |
| 0 | 8.3 | 53.5 | .529 | 144. | 273 000. | 1890. |
| 1 | 7.3 | 42.4 | .667 | 114. | 172 000. | 1500. |
| 2 | 6.5 | 33.6 | .841 | 90.8 | 108 000. | 1190. |
| 3 | 5.8 | 26.7 | 1.06 | 72.0 | 67 900. | 943. |
| 4 | 5.2 | 21.2 | 1.34 | 57.1 | 42 700. | 748. |
| 5 | 4.6 | 16.8 | 1.69 | 45.3 | 26 900. | 593. |
| 6 | 4.1 | 13.3 | 2.13 | 35.9 | 16 900. | 470. |
| 7 | 3.7 | 10.5 | 2.68 | 28.5 | 10 600. | 373. |
| 8 | 3.3 | 8.37 | 3.38 | 22.6 | 6680. | 296. |
| 9 | 2.91 | 6.63 | 4.26 | 17.9 | 4200. | 235. |
| 10 | 2.59 | 5.26 | 5.38 | 14.2 | 2640. | 186. |
| 11 | 2.30 | 4.17 | 6.78 | 11.3 | 1660. | 148. |
| 12 | 2.05 | 3.31 | 8.55 | 8.93 | 1050. | 117. |
| 13 | 1.83 | 2.62 | 10.8 | 7.08 | 657. | 92.8 |
| 14 | 1.63 | 2.08 | 13.6 | 5.62 | 413. | 73.6 |
| 15 | 1.45 | 1.65 | 17.1 | 4.46 | 260. | 58.4 |
| 16 | 1.29 | 1.31 | 21.6 | 3.53 | 164. | 46.3 |
| 17 | 1.15 | 1.04 | 27.3 | 2.80 | 103. | 36.7 |
| 18 | 1.02 | 0.823 | 34.4 | 2.22 | 64.7 | 29.1 |
| 19 | 0.91 | .653 | 43.3 | 1.76 | 40.7 | 23.1 |
| 20 | .81 | .518 | 54.6 | 1.40 | 25.6 | 18.3 |
| 21 | .72 | .411 | 68.9 | 1.11 | 16.1 | 14.5 |
| 22 | .64 | .326 | 86.9 | 0.879 | 10.1 | 11.5 |
| 23 | .57 | .258 | 110. | .697 | 6.36 | 9.13 |
| 24 | .51 | .205 | 138. | .553 | 4.00 | 7.24 |
| 25 | .45 | .162 | 174. | .438 | 2.52 | 5.74 |
| 26 | .40 | .129 | 220. | .348 | 1.58 | 4.55 |
| 27 | .36 | .102 | 277. | .276 | 0.995 | 3.61 |
| 28 | .32 | .0810 | 349. | .219 | .626 | 2.86 |
| 29 | .29 | .0642 | 440. | .173 | .394 | 2.27 |
| 30 | .25 | .0509 | 555. | .138 | .248 | 1.80 |
| 31 | .227 | .0404 | 700. | .109 | .156 | 1.43 |
| 32 | .202 | .0320 | 883. | .0865 | .0979 | 1.13 |
| 33 | .180 | .0254 | 1110. | .0686 | .0616 | 0.899 |
| 34 | .160 | .0201 | 1400. | .0544 | .0387 | .712 |
| 35 | .143 | .0160 | 1770. | .0431 | .0244 | .565 |
| 36 | .127 | .0127 | 2230. | .0342 | .0153 | .448 |
| 37 | .113 | .0100 | 2820. | .0271 | .00963 | .355 |
| 38 | .101 | .0080 | 3550. | .0215 | .00606 | .262 |
| 39 | .090 | .0063 | 4480. | .0171 | .00381 | .223 |
| 40 | .080 | .0050 | 5640. | .0135 | .00240 | .177 |

ELECTROCHEMICAL EQUIVALENTS

Every gram-ion involved in an electrolytic change requires the same number of coulombs or ampere-hours of electricity per unit change of valency. This constant is 96,494 coulombs or 26.804 ampere-hours per gram-hour (a faraday) corresponding to an electrochemical equivalent for silver of 0.00111803 gram sec.⁻¹ amp.⁻¹. It is to be noted that the *change of valence* of the element from its state before to that after the electrolytic action should be considered. The valence of a free, uncombined element is to be considered as 0. The same current will electrolyze "chemically equivalent" quantities per unit time. The valence is then included in the "chemically equivalent" quantity.

| Ele- ment | Change of valency | Mg per coulomb | Coulombs per mg | Grams per amp. hour | Ele- ment | Change of valency | Mg per coulomb | Coulombs per mg | Grams per amp. hour |
|--------------|----------------------|----------------------|-----------------------|---------------------------|--------------|----------------------|----------------------|-----------------------|---------------------------|
| Al | 3 | 0.09317 | 10.731 | 0.3354 | Ni | 1 | 0.6082 | 1.6442 | 2.1895 |
| Cl | 1 | .36746 | 2.7213 | 1.3229 | " | 2 | .3041 | 3.2884 | 1.0948 |
| " | 3 | .12249 | 8.1649 | .4410 | " | 3 | .20273 | 4.9326 | .7298 |
| " | 5 | .07349 | 13.606 | .2646 | O | 2 | .082909 | 12.0611 | .298500 |
| " | 7 | .05249 | 19.049 | .18891 | " | 4 | .041454 | 24.1222 | .149250 |
| Cu | 1 | .6588 | 1.5179 | 2.3717 | Pt | 2 | 1.01165 | .98848 | 3.6419 |
| " | 2 | .3294 | 3.0358 | 1.1858 | " | 4 | .50582 | 1.97696 | 1.8210 |
| Au | 1 | 2.044 | .4893 | 7.357 | " | 6 | .33722 | 2.9654 | 1.2140 |
| " | 3 | .6813 | 1.468 | 2.452 | K | 1 | .4052 | 2.467 | 1.4587 |
| H | 1 | .0104442 | 95.747 | .0375991 | Ag | 1 | 1.111803 | .894430 | 4.02491 |
| Pb | 1 | 2.1475 | .46565 | 7.7310 | Na | 1 | .23833 | 4.1958 | .85799 |
| " | 2 | 1.07375 | .93130 | 3.8655 | Sn | 2 | .61505 | 1.6259 | 2.2142 |
| " | 4 | .53688 | 1.8626 | 1.9328 | " | 4 | .30752 | 3.2518 | 1.1071 |
| Hg | 1 | 2.0790 | .48100 | 7.4844 | Zn | 2 | .33875 | 2.9520 | 1.21950 |
| " | 2 | 1.0395 | .96200 | 3.7422 | | | | | |

The electrochemical equivalent for silver is 0.00111803 g sec.⁻¹ amp.⁻¹.

For other elements the electrochemical equivalent = (atomic weight divided by change of valency) times 1/96494 g/sec./amp. or g/coulomb.

NOTE.—The change of valency for O₂ is usually 2, etc.

TABLE 504.—Conductivity of Electrolytic Solutions

This subject has occupied the attention of a considerable number of eminent workers in molecular physics, and a few results are here tabulated. It has seemed better to confine the examples to the work of one experimenter, and the tables are quoted from a paper by F. Kohlrausch,* who has been one of the most reliable and successful workers in this field.

The study of electrolytic conductivity, especially in the case of very dilute solutions, has furnished material for generalizations, which may to some extent help in the formation of a sound theory of the mechanism of such conduction. If the solutions are made such that per unit volume of the solvent medium there are contained amounts of the salt proportional to its electrochemical equivalent, some simple relations become apparent. The solutions used by Kohlrausch were therefore made by taking numbers of grams of the pure salts proportional to their electrochemical equivalent, and using a liter of water as the standard of quantity of the solvent. Taking the electrochemical equivalent number as the chemical equivalent or atomic weight divided by the valence, and using this number of grams to the liter of water, we get what is called the normal or gram molecule per liter solution. In the table, m is used to represent the number of gram molecules to the liter of water in the solution for which the conductivities are tabulated. The conductivities were obtained by measuring the resistance of a cell filled with the solution by means of a Wheatstone bridge alternating current and telephone arrangement. The results are for 18° C., and relative to mercury at 0° C., the cell having been standardized by filling with mercury and measuring the resistance. They are supposed to be accurate to within one per cent of the true value.

The tabular numbers were obtained from the measurements in the following manner:—

Let K_{18} = conductivity of the solution at 18° C relative to mercury at 0° C.

K_{18}^w = conductivity of the solvent water at 18° C relative to mercury at 0° C.

Then $K_{18} - K_{18}^w = k_{18}$ = conductivity of the electrolyte in the solution measured.

$\frac{k_{18}}{m} = \mu$ = conductivity of the electrolyte in the solution per molecule, or the "specific molecular conductivity."

Value of k_{18} for a few Electrolytes

This short table illustrates the apparent law that the conductivity in very dilute solutions is proportional to the amount of salt dissolved.

| m | KCl | NaCl | AgNO ₃ | KC ₂ H ₃ O ₂ | K ₂ SO ₄ | MgSO ₄ |
|---------|-------|-------|-------------------|---|--------------------------------|-------------------|
| 0.00001 | 1.216 | 1.024 | 1.080 | 0.939 | 1.275 | 1.056 |
| 0.00002 | 2.434 | 2.056 | 2.146 | 1.886 | 2.532 | 2.104 |
| 0.00006 | 7.272 | 6.162 | 6.462 | 5.610 | 7.524 | 6.216 |
| 0.0001 | 12.09 | 10.29 | 10.78 | 9.34 | 12.49 | 10.34 |

TABLE 505.—Electro-Chemical Equivalents and Normal Solutions

The following table of the electro-chemical equivalent numbers and the densities of approximately normal solutions of the salts quoted in Table 506 may be convenient. They represent grams per cubic centimeter of the solution at the temperature given.

| Salt dissolved. | Grams per liter. | m | Temp. C. | Density. | Salt dissolved. | Grams per liter. | m | Temp. C. | Density. |
|---|------------------|--------|----------|----------|---|------------------|--------|----------|----------|
| KCl . . . | 74.59 | 1.0 | 15.2 | 1.0457 | $\frac{1}{2}$ K ₂ SO ₄ . | 87.16 | 1.0 | 18.9 | 1.0658 |
| NH ₄ Cl . . . | 53.55 | 1.0009 | 18.6 | 1.0152 | $\frac{1}{2}$ Na ₂ SO ₄ . | 71.09 | 1.0003 | 18.6 | 1.0602 |
| NaCl . . . | 58.50 | 1.0 | 18.4 | 1.0391 | $\frac{1}{2}$ Li ₂ SO ₄ . | 55.09 | 1.0007 | 18.6 | 1.0445 |
| LiCl . . . | 42.48 | 1.0 | 18.4 | 1.0227 | $\frac{1}{2}$ MgSO ₄ . | 60.17 | 1.0023 | 18.6 | 1.0573 |
| $\frac{1}{2}$ BaCl ₂ . . . | 104.0 | 1.0 | 18.6 | 1.0888 | $\frac{1}{2}$ ZnSO ₄ . | 80.58 | 1.0 | 5.3 | 1.0794 |
| $\frac{1}{2}$ ZnCl ₂ . . . | 68.0 | 1.012 | 15.0 | 1.0592 | $\frac{1}{2}$ CuSO ₄ . | 79.9 | 1.001 | 18.2 | 1.0776 |
| KI . . . | 165.9 | 1.0 | 18.6 | 1.1183 | $\frac{1}{2}$ K ₂ CO ₃ . | 69.17 | 1.0006 | 18.3 | 1.0576 |
| KNO ₃ . . . | 101.17 | 1.0 | 18.6 | 1.0601 | $\frac{1}{2}$ Na ₂ CO ₃ . | 53.04 | 1.0 | 17.9 | 1.0517 |
| NaNO ₃ . . . | 85.08 | 1.0 | 18.7 | 1.0542 | KOH . . . | 56.27 | 1.0025 | 18.8 | 1.0477 |
| AgNO ₃ . . . | 169.9 | 1.0 | — | — | HCl . . . | 36.51 | 1.0041 | 18.6 | 1.0161 |
| $\frac{1}{2}$ Ba(NO ₃) ₂ . . . | 65.28 | 0.5 | — | — | HNO ₃ . . . | 63.13 | 1.0014 | 18.6 | 1.0318 |
| KClO ₃ . . . | 61.29 | 0.5 | 18.3 | 1.0367 | $\frac{1}{2}$ H ₂ SO ₄ . | 49.06 | 1.0006 | 18.9 | 1.0300 |
| KC ₂ H ₃ O ₂ . . . | 98.18 | 1.0005 | 18.6 | 1.0467 | | | | | |

* "Wied. Ann." vol. 26, pp. 161-226, 1885.

SPECIFIC MOLECULAR CONDUCTIVITY OF SOLUTIONS
MERCURY = 10^8

| Salt dissolved. | $m = 10$ | 5 | 3 | 1 | 0.5 | 0.1 | .05 | .03 | .01 |
|-------------------------------|----------|------|------|------|------|------|-------|-------|------|
| $\frac{1}{2}K_2SO_4$. . . | — | — | — | — | 672 | 736 | 897 | 959 | 1098 |
| KCl | — | — | 827 | 919 | 958 | 1047 | 1083 | 1107 | 1147 |
| KI | — | 770 | 900 | 968 | 997 | 1069 | 1102 | 1123 | 1161 |
| NH_4Cl | — | 752 | 825 | 907 | 948 | 1035 | 1078 | 1101 | 1142 |
| KNO_3 | — | — | 572 | 752 | 839 | 983 | 1037 | 1067 | 1122 |
| $\frac{1}{2}BaCl_2$ | — | — | 487 | 658 | 725 | 861 | 904 | 939 | 1006 |
| $KClO_3$ | — | — | — | — | 799 | 927 | (976) | 1006 | 1053 |
| $\frac{1}{2}BaN_2O_6$. . . | — | — | — | — | 531 | 755 | 828 | (870) | 951 |
| $\frac{1}{2}CuSO_4$ | — | — | 150 | 241 | 288 | 424 | 479 | 537 | 675 |
| $AgNO_3$ | — | 351 | 448 | 635 | 728 | 886 | 936 | (966) | 1017 |
| $\frac{1}{2}ZnSO_4$ | — | 82 | 146 | 249 | 302 | 431 | 500 | 556 | 685 |
| $\frac{1}{2}MgSO_4$ | — | 82 | 151 | 270 | 330 | 474 | 532 | 587 | 715 |
| $\frac{1}{2}Na_2SO_4$ | — | — | — | 475 | 559 | 734 | 784 | 828 | 906 |
| $\frac{1}{2}ZnCl_2$ | 60 | 180 | 280 | 514 | 601 | 768 | 817 | 851 | 915 |
| NaCl | — | 398 | 528 | 695 | 757 | 865 | 897 | (920) | 962 |
| $NaNO_3$ | — | — | 430 | 617 | 694 | 817 | 855 | 877 | 907 |
| $KC_2H_3O_2$ | 30 | 240 | 381 | 594 | 671 | 784 | 820 | 841 | 879 |
| $\frac{1}{2}Na_2CO_3$ | — | — | 254 | 427 | 510 | 682 | 751 | 799 | 899 |
| $\frac{1}{2}H_2SO_4$ | 660 | 1270 | 1560 | 1820 | 1899 | 2084 | 2343 | 2515 | 2855 |
| C_2H_4O | 0.5 | 2.6 | 5.2 | 12 | 19 | 43 | 62 | 79 | 132 |
| HCl | 600 | 1420 | 2010 | 2780 | 3017 | 3244 | 3330 | 3369 | 3416 |
| HNO_3 | 610 | 1470 | 2070 | 2770 | 2991 | 3225 | 3289 | 3328 | 3395 |
| $\frac{1}{2}H_3PO_4$ | 148 | 160 | 170 | 200 | 250 | 430 | 540 | 620 | 790 |
| KOH | 423 | 990 | 1314 | 1718 | 1841 | 1986 | 2045 | 2078 | 2124 |
| NH_3 | 0.5 | 2.4 | 3.3 | 8.4 | 12 | 31 | 43 | 50 | 92 |

| Salt dissolved. | .006 | .002 | .001 | .0006 | .0002 | .0001 | .00006 | .00002 | .00001 |
|-------------------------------|------|------|------|-------|-------|-------|--------|--------|--------|
| $\frac{1}{2}K_2SO_4$ | 1130 | 1181 | 1207 | 1220 | 1241 | 1249 | 1254 | 1266 | 1275 |
| KCl | 1162 | 1185 | 1193 | 1199 | 1209 | 1209 | 1212 | 1217 | 1216 |
| KI | 1176 | 1197 | 1203 | 1209 | 1214 | 1216 | 1216 | 1216 | 1207 |
| NH_4Cl | 1157 | 1180 | 1190 | 1197 | 1204 | 1209 | 1215 | 1209 | 1205 |
| KNO_3 | 1140 | 1173 | 1180 | 1190 | 1199 | 1207 | 1220 | 1198 | 1215 |
| $\frac{1}{2}BaCl_2$ | 1031 | 1074 | 1092 | 1102 | 1118 | 1126 | 1133 | 1144 | 1142 |
| $KClO_3$ | 1068 | 1091 | 1101 | 1109 | 1119 | 1122 | 1126 | 1135 | 1141 |
| $\frac{1}{2}BaN_2O_6$ | 982 | 1033 | 1054 | 1066 | 1084 | 1096 | 1100 | 1114 | 1114 |
| $\frac{1}{2}CuSO_4$ | 740 | 873 | 950 | 987 | 1039 | 1062 | 1074 | 1084 | 1086 |
| $AgNO_3$ | 1033 | 1057 | 1068 | 1069 | 1077 | 1078 | 1077 | 1073 | 1080 |
| $\frac{1}{2}ZnSO_4$ | 744 | 861 | 919 | 953 | 1001 | 1023 | 1032 | 1047 | 1060 |
| $\frac{1}{2}MgSO_4$ | 773 | 881 | 935 | 967 | 1015 | 1034 | 1036 | 1052 | 1056 |
| $\frac{1}{2}Na_2SO_4$ | 933 | 980 | 998 | 1009 | 1026 | 1034 | 1038 | 1056 | 1054 |
| $\frac{1}{2}ZnCl_2$ | 939 | 979 | 994 | 1004 | 1020 | 1029 | 1031 | 1035 | 1036 |
| NaCl | 976 | 998 | 1008 | 1014 | 1018 | 1029 | 1027 | 1028 | 1024 |
| $NaNO_3$ | 921 | 942 | 952 | 956 | 966 | 975 | 970 | 972 | 975 |
| $KC_2H_3O_2$ | 891 | 913 | 919 | 923 | 933 | 934 | 935 | 943 | 939 |
| $\frac{1}{2}Na_2CO_3$ | 956 | 1010 | 1037 | 1046 | 988 | 874 | 790 | 715 | 697* |
| $\frac{1}{2}H_2SO_4$ | 3001 | 3240 | 3316 | 3342 | 3280 | 3118 | 2927 | 2077 | 1413* |
| C_2H_4O | 170 | 283 | 380 | 470 | 796 | 995 | 1133 | 1328 | 1304* |
| HCl | 3438 | 3455 | 3455 | 3440 | 3340 | 3170 | 2968 | 2057 | 1254* |
| HNO_3 | 3421 | 3448 | 3427 | 3108 | 3285 | 3088 | 2863 | 1904 | 1144* |
| $\frac{1}{2}H_3PO_4$ | 858 | 945 | 968 | 977 | 920 | 837 | 746 | 497 | 402* |
| KOH | 2141 | 2140 | 2110 | 2074 | 1892 | 1689 | 1474 | 845 | 747* |
| NH_3 | 116 | 190 | 260 | 330 | 500 | 610 | 690 | 700 | 560* |

* Acids and alkaline salts show peculiar irregularities.

SPECIFIC MOLECULAR CONDUCTIVITY OF SOLUTIONS

TABLE 507.—Limiting Values of μ

This table shows limiting values of $\mu = \frac{k}{m} \cdot 10^8$ for infinite dilution for neutral salts, calculated from Table 305.

| Salt. | μ | Salt. | μ | Salt. | μ | Salt. | μ |
|--------------------------------------|-------|--|-------|--|-------|---------------------------------------|-------|
| $\frac{1}{2}\text{K}_2\text{SO}_4$. | 1280 | $\frac{1}{2}\text{BaCl}_2$. | 1150 | $\frac{1}{2}\text{MgSO}_4$. | 1080 | $\frac{1}{2}\text{H}_2\text{SO}_4$. | 3700 |
| KCl . . . | 1220 | $\frac{1}{2}\text{KClO}_3$. | 1150 | $\frac{1}{2}\text{Na}_2\text{SO}_4$. | 1060 | HCl . . . | 3500 |
| KI . . . | 1220 | $\frac{1}{2}\text{BaNO}_3\text{O}_6$. | 1120 | $\frac{1}{2}\text{ZnCl}_2$. . | 1040 | HNO_3 . . | 3500 |
| NH_4Cl . . | 1210 | $\frac{1}{2}\text{CuSO}_4$. | 1100 | NaCl . . . | 1030 | $\frac{1}{3}\text{H}_3\text{PO}_4$. | 1100 |
| KNO_3 . . | 1210 | AgNO_3 . | 1090 | NaNO_3 . . | 980 | KOH . . . | 2200 |
| — | — | $\frac{1}{2}\text{ZnSO}_4$. | 1080 | $\text{K}_2\text{C}_2\text{H}_3\text{O}_2$ | 940 | $\frac{1}{2}\text{Na}_2\text{CO}_3$. | 1400 |

If the quantities in Table 507 be represented by curves, it appears that the values of the specific molecular conductivities tend toward a limiting value as the solution is made more and more dilute. Although these values are of the same order of magnitude, they are not equal, but depend on the nature of both the ions forming the electrolyte.

When the numbers in Table 508 are multiplied by Hittorf's constant, or 0.00011, quantities ranging between 0.14 and 0.10 are obtained which represent the velocities in millimetres per second of the ions when the electromotive force gradient is one volt per millimetre.

Specific molecular conductivities in general become less as the concentration is increased, which may be due to mutual interference. The decrease is not the same for different salts, but becomes much more rapid in salts of high valence.

Salts having acid or alkaline reactions show marked differences. They have small specific molecular conductivity in very dilute solutions, but as the concentration is increased the conductivity rises, reaches a maximum and again falls off. Kohlrausch does not believe that this can be explained by impurities. H_3PO_4 in dilute solution seems to approach a monobasic acid, while H_2SO_4 shows two maxima, and like H_3PO_4 approaches in very weak solution to a monobasic acid.

Kohlrausch concludes that the law of independent migration of the ions in media like water is sustained.

TABLE 508.—Temperature Coefficients

The temperature coefficient in general diminishes with dilution, and for very dilute solutions appears to approach a common value. The following table gives the temperature coefficient for solutions containing 0.01 gram molecule of the salt.

| Salt. | Temp. Coeff. | Salt. | Temp. Coeff. | Salt. | Temp. Coeff. | Salt. | Temp. Coeff. |
|--------------------------------|--------------|---------------------------------------|--------------|---------------------------------------|--------------|--|--------------|
| KCl . . . | 0.0221 | KI . . . | 0.0219 | $\frac{1}{2}\text{K}_2\text{SO}_4$. | 0.0223 | $\frac{1}{2}\text{K}_2\text{CO}_3$. . | 0.0249 |
| NH_4Cl . . | 0.0226 | KNO_3 . . | 0.0216 | $\frac{1}{2}\text{Na}_2\text{SO}_4$. | 0.0240 | $\frac{1}{2}\text{Na}_2\text{CO}_3$. . | 0.0265 |
| NaCl . . . | 0.0238 | NaNO_3 . . | 0.0226 | $\frac{1}{2}\text{Li}_2\text{SO}_4$. | 0.0242 | KOH . . . | 0.0194 |
| LiCl . . . | 0.0232 | AgNO_3 . . | 0.0221 | $\frac{1}{2}\text{MgSO}_4$. | 0.0236 | HCl . . . | 0.0159 |
| $\frac{1}{2}\text{BaCl}_2$. . | 0.0234 | $\frac{1}{2}\text{Ba}(\text{NO}_3)_2$ | 0.0224 | $\frac{1}{2}\text{ZnSO}_4$. | 0.0234 | HNO_3 . . . | 0.0162 |
| $\frac{1}{2}\text{ZnCl}_2$. . | 0.0239 | KClO_3 . . | 0.0219 | $\frac{1}{2}\text{CuSO}_4$. | 0.0229 | $\frac{1}{2}\text{H}_2\text{SO}_4$. . | 0.0125 |
| $\frac{1}{2}\text{MgCl}_2$. | 0.0241 | $\text{KC}_2\text{H}_3\text{O}_2$. | 0.0229 | — | — | $\frac{1}{2}\text{H}_2\text{SO}_4$ for $m = .001$ } | 0.0159 |

THE EQUIVALENT CONDUCTIVITY OF SALTS, ACIDS AND BASES IN AQUEOUS SOLUTIONS

In the following table the equivalent conductance is expressed in reciprocal ohms. The concentration is expressed in milli-equivalents of solute per liter of solution at the temperature to which the conductance refers. (In the cases of potassium hydrogen sulphate and phosphoric acid the concentration is expressed in milli-formula-weights of solute, KHSO_4 or H_3PO_4 , per liter of solution, and the values are correspondingly the modal, or "formal," conductances.) Except in the cases of the strong acids the conductance of the water was subtracted, and for sodium acetate, ammonium acetate and ammonium chloride the values have been corrected for the hydrolysis of the salts. The atomic weights used were those of the International Commission for 1905, referred to oxygen as 16.00. Temperatures are on the hydrogen gas scale.

Concentration in $\frac{\text{gram equivalents}}{1000 \text{ liter}}$

Equivalent conductance in $\frac{\text{reciprocal ohms per centimeter cube}}{\text{gram equivalents per cubic centimeter}}$

| Substance. | Concentration. | Equivalent conductance at the following °C temperatures. | | | | | | | | | |
|--------------------|----------------|--|---------|---------|---------|-------|-------|-------|-------|------|--------|
| | | 18° | 25° | 50° | 75° | 100° | 128° | 156° | 218° | 281° | 306° |
| Potassium chloride | 0 | 130.1 | (152.1) | (232.5) | (321.5) | 414 | (519) | 625 | 825 | 1005 | 1120 |
| " | 2 | 126.3 | 146.4 | — | — | 393 | — | 588 | 779 | 930 | 1008 |
| " | 10 | 122.4 | 141.5 | 215.2 | 295.2 | 377 | 470 | 560 | 741 | 874 | 910 |
| " | 80 | 113.5 | — | — | — | 342 | — | 498 | 638 | 723 | 720 |
| " | 100 | 112.0 | 129.0 | 194.5 | 264.6 | 336 | 415 | 490 | — | — | — |
| Sodium chloride | 0 | 109.0 | — | — | — | 362 | — | 555 | 760 | 970 | 1080 |
| " | 2 | 105.6 | — | — | — | 349 | — | 534 | 722 | 895 | 955 |
| " | 10 | 102.0 | — | — | — | 336 | — | 511 | 685 | 820 | 860 |
| " | 80 | 93.5 | — | — | — | 301 | — | 450 | 500 | 674 | 680 |
| " | 100 | 92.0 | — | — | — | 296 | — | 442 | — | — | — |
| Silver nitrate | 0 | 115.8 | — | — | — | 367 | — | 570 | 780 | 965 | 1065 |
| " | 2 | 112.2 | — | — | — | 353 | — | 539 | 727 | 877 | 935 |
| " | 10 | 108.0 | — | — | — | 337 | — | 507 | 673 | 790 | 818 |
| " | 20 | 105.1 | — | — | — | 326 | — | 488 | 639 | — | — |
| " | 40 | 101.3 | — | — | — | 312 | — | 462 | 599 | 680 | 680 |
| " | 80 | 96.5 | — | — | — | 294 | — | 432 | 552 | 614 | 604 |
| " | 100 | 94.6 | — | — | — | 289 | — | — | — | — | — |
| Sodium acetate | 0 | 78.1 | — | — | — | 285 | — | 450 | 660 | — | 924 |
| " | 2 | 74.5 | — | — | — | 268 | — | 421 | 578 | — | 801 |
| " | 10 | 71.2 | — | — | — | 253 | — | 396 | 542 | — | 702 |
| " | 80 | 63.4 | — | — | — | 221 | — | 340 | 452 | — | — |
| Magnesium sulphate | 0 | 114.1 | — | — | — | 426 | — | 690 | 1080 | — | — |
| " | 2 | 94.3 | — | — | — | 302 | — | 377 | 260 | — | — |
| " | 10 | 76.1 | — | — | — | 234 | — | 241 | 143 | — | — |
| " | 20 | 67.5 | — | — | — | 190 | — | 195 | 110 | — | — |
| " | 40 | 59.3 | — | — | — | 160 | — | 158 | 88 | — | — |
| " | 80 | 52.0 | — | — | — | 136 | — | 133 | 75 | — | — |
| " | 100 | 49.8 | — | — | — | 130 | — | 126 | — | — | — |
| " | 200 | 43.1 | — | — | — | 110 | — | 109 | — | — | — |
| Ammonium chloride | 0 | 131.1 | 152.0 | — | — | (415) | — | (628) | (841) | — | (1176) |
| " | 2 | 126.5 | 146.5 | — | — | 399 | — | 601 | 801 | — | 1031 |
| " | 10 | 122.5 | 141.7 | — | — | 382 | — | 573 | 758 | — | 925 |
| " | 30 | 118.1 | — | — | — | — | — | — | — | — | 828 |
| Ammonium acetate | 0 | (90.8) | — | — | — | (338) | — | (523) | — | — | — |
| " | 10 | 91.7 | — | — | — | 300 | — | 456 | — | — | — |
| " | 25 | 88.2 | — | — | — | 286 | — | 426 | — | — | — |

From the investigations of Noyes, Melcher, Cooper, Eastman and Kato; Journal of the American Chemical Society, 30, p. 335, 1908.

SMITHSONIAN TABLES.

THE EQUIVALENT CONDUCTIVITY OF SALTS, ACIDS AND BASES IN AQUEOUS SOLUTIONS

| Substance. | Concentration. | Equivalent conductance at the following °C temperatures. | | | | | | | | | |
|-----------------------------|----------------|--|-------|-------|-------|-------|--------|-------|--------|------|--------|
| | | 18° | 25° | 50° | 75° | 100° | 128° | 156° | 218° | 281° | 306° |
| Barium nitrate. | 0 | 116.9 | — | — | — | 385 | — | 600 | 840 | 1120 | 1300 |
| " " | 2 | 109.7 | — | — | — | 352 | — | 536 | 715 | 828 | 824 |
| " " | 10 | 101.0 | — | — | — | 322 | — | 481 | 618 | 658 | 615 |
| " " | 40 | 88.7 | — | — | — | 280 | — | 412 | 507 | 503 | 448 |
| " " | 80 | 81.6 | — | — | — | 258 | — | 372 | 449 | 430 | — |
| " " | 100 | 79.1 | — | — | — | 249 | — | — | — | — | — |
| Potassium sulphate | 0 | 132.8 | — | — | — | 455 | — | 715 | 1065 | 1460 | 1725 |
| " " | 2 | 124.8 | — | — | — | 402 | — | 605 | 806 | 893 | 867 |
| " " | 10 | 115.7 | — | — | — | 365 | — | 537 | 672 | 687 | 637 |
| " " | 40 | 104.2 | — | — | — | 320 | — | 455 | 545 | 519 | 466 |
| " " | 80 | 97.2 | — | — | — | 294 | — | 415 | 482 | 448 | 396 |
| " " | 100 | 95.0 | — | — | — | 286 | — | — | — | — | — |
| Hydrochloric acid | 0 | 379.0 | — | — | — | 850 | — | 1085 | 1265 | 1380 | 1424 |
| " " | 2 | 373.6 | — | — | — | 826 | — | 1048 | 1217 | 1332 | 1337 |
| " " | 10 | 368.1 | — | — | — | 807 | — | 1016 | 1168 | 1226 | 1162 |
| " " | 80 | 353.0 | — | — | — | 762 | — | 946 | 1044 | 1046 | 862 |
| " " | 100 | 350.6 | — | — | — | 754 | — | 929 | 1006 | — | — |
| Nitric acid | 0 | 377.0 | 421.0 | 570 | 706 | 826 | 945 | 1047 | (1230) | — | (1380) |
| " " | 2 | 371.2 | 413.7 | 559 | 690 | 806 | 919 | 1012 | 1166 | — | 1156 |
| " " | 10 | 365.0 | 406.0 | 548 | 676 | 786 | 893 | 978 | — | — | — |
| " " | 50 | 353.7 | 393.3 | 528 | 649 | 750 | 845 | 917 | — | — | 454* |
| " " | 100 | 346.4 | 385.0 | 516 | 632 | 728 | 817 | 880 | — | — | (2030) |
| Sulphuric acid | 0 | 383.0 | (429) | (591) | (740) | 891 | (1041) | 1176 | 1505 | — | (2030) |
| " " | 2 | 353.9 | 390.8 | 501 | 561 | 571 | 551 | 536 | 563 | — | 637 |
| " " | 10 | 309.0 | 337.0 | 406 | 435 | 446 | 460 | 481 | 533 | — | — |
| " " | 50 | 253.5 | 273.0 | 323 | 350 | 384 | 417 | 448 | 502 | — | — |
| " " | 100 | 233.3 | 251.2 | 300 | 336 | 369 | 404 | 435 | 483 | — | 474* |
| Potassium hydrogen sulphate | 2 | 455.3 | 506.0 | 601.0 | 754 | 784 | 773 | 754 | — | — | — |
| " " | 50 | 295.5 | 318.3 | 374.4 | 403 | 422 | 446 | 477 | — | — | — |
| " " | 100 | 263.7 | 283.1 | 329.1 | 354 | 375 | 402 | 435 | — | — | — |
| Phosphoric acid | 0 | 338.3 | 376 | 510 | 631 | 730 | 839 | 930 | — | — | — |
| " " | 2 | 283.1 | 311.9 | 401 | 464 | 498 | 508 | 489 | — | — | — |
| " " | 10 | 203.0 | 222.0 | 273 | 300 | 308 | 298 | 274 | — | — | — |
| " " | 50 | 122.7 | 132.6 | 157.8 | 168.6 | 168 | 158 | 142 | — | — | — |
| " " | 100 | 96.5 | 104.0 | 122.7 | 129.9 | 128 | 120 | 108 | — | — | — |
| Acetic acid | 0 | (347.0) | — | — | — | (773) | — | (980) | (1165) | — | (1268) |
| " " | 10 | 14.50 | — | — | — | 25.1 | — | 22.2 | 14.7 | — | — |
| " " | 30 | 8.50 | — | — | — | 14.7 | — | 13.0 | 8.65 | — | — |
| " " | 80 | 5.22 | — | — | — | 9.05 | — | 8.00 | 5.34 | — | — |
| " " | 100 | 4.67 | — | — | — | 8.10 | — | — | 4.82 | — | 1.57 |
| Sodium hydroxide | 0 | 216.5 | — | — | — | 594 | — | 835 | 1060 | — | — |
| " " | 2 | 212.1 | — | — | — | 582 | — | 814 | — | — | — |
| " " | 20 | 205.8 | — | — | — | 559 | — | 771 | 930 | — | — |
| " " | 50 | 200.6 | — | — | — | 540 | — | 738 | 873 | — | — |
| Barium hydroxide | 0 | 222 | 256 | 389 | (520) | 645 | (760) | 847 | — | — | — |
| " " | 2 | 215 | — | 359 | 4 | 591 | — | — | — | — | — |
| " " | 10 | 207 | 235 | 342 | 449 | 548 | 664 | 722 | — | — | — |
| " " | 50 | 191.1 | 215.1 | 308 | 399 | 478 | 549 | 593 | — | — | — |
| " " | 100 | 180.1 | 204.2 | 291 | 373 | 443 | 503 | 531 | — | — | — |
| Ammonium hydroxide | 0 | (238) | (271) | (404) | (526) | (647) | (764) | (908) | (1141) | — | (1406) |
| " " | 10 | 9.66 | — | — | — | 23.2 | — | 22.3 | 15.6 | — | — |
| " " | 30 | 5.66 | — | — | — | 13.6 | — | 13.0 | — | — | — |
| " " | 100 | 3.10 | 3.62 | 5.35 | 6.70 | 7.47 | — | 7.17 | 4.82 | — | 1.33 |

* These values are at the concentration 80.0.

THE EQUIVALENT CONDUCTIVITY OF SOME ADDITIONAL SALTS IN AQUEOUS SOLUTION

Conditions similar to those of the preceding table except that the atomic weights for 1908 were used.

| Substance. | Concentration. | Equivalent conductance at the following $^{\circ}\text{C}$ temperature. | | | | | | | |
|--------------------------|----------------|---|--------------|--------------|--------------|--------------|---------------|---------------|---------------|
| | | 0° | 18° | 25° | 50° | 75° | 100° | 128° | 156° |
| Potassium nitrate . . . | 0 | 80.8 | 126.3 | 145.1 | 219 | 299 | 384 | 485 | 580 |
| " " . . . | 2 | 78.6 | 122.5 | 140.7 | 212.7 | 289.9 | 370.3 | 460.7 | 551 |
| " " . . . | 12.5 | 75.3 | 117.2 | 134.9 | 202.9 | 276.4 | 351.5 | 435.4 | 520.4 |
| " " . . . | 50 | 70.7 | 109.7 | 126.3 | 189.5 | 257.4 | 326.1 | 402.9 | 476.1 |
| " " . . . | 100 | 67.2 | 104.5 | 120.3 | 180.2 | 244.1 | 308.5 | 379.5 | 447.3 |
| Potassium oxalate . . . | 0 | 79.4 | 127.6 | 147.5 | 230 | 322 | 419 | 538 | 653 |
| " " . . . | 2 | 74.9 | 119.9 | 139.2 | 215.9 | 300.2 | 389.3 | 489.1 | 587 |
| " " . . . | 12.5 | 69.3 | 111.1 | 129.2 | 199.1 | 275.1 | 354.1 | 438.8 | 524.3 |
| " " . . . | 50 | 63 | 101 | 116.5 | 178.6 | 244.9 | 312.2 | 383.8 | 449.5 |
| " " . . . | 100 | 59.3 | 94.6 | 109.5 | 167 | 227.5 | 288.9 | 353.2 | 409.7 |
| " " . . . | 200 | 55.8 | 88.4 | 102.3 | 155 | 210.9 | 265.1 | 321.9 | 372.1 |
| Calcium nitrate . . . | 0 | 70.4 | 112.7 | 130.6 | 202 | 282 | 369 | 474 | 575 |
| " " . . . | 2 | 66.5 | 107.1 | 123.7 | 191.9 | 266.7 | 346.5 | 438.4 | 529.8 |
| " " . . . | 12.5 | 61.6 | 98.6 | 114.5 | 176.2 | 244 | 314.6 | 394.5 | 473.7 |
| " " . . . | 50 | 55.6 | 88.6 | 102.6 | 157.2 | 216.2 | 276.8 | 343 | 405.1 |
| " " . . . | 100 | 51.9 | 82.6 | 95.8 | 146.1 | 199.9 | 255.5 | 315.1 | 369.1 |
| " " . . . | 200 | 48.3 | 76.7 | 88.8 | 135.4 | 184.7 | 234.4 | 288 | 334.7 |
| Potassium ferrocyanide . | 0 | 98.4 | 159.6 | 185.5 | 288 | 403 | 527 | | |
| " " . . . | 0.5 | 91.6 | - | 171.1 | | | | | |
| " " . . . | 2 | 84.8 | 137 | 158.9 | 243.8 | 335.2 | 427.6 | | |
| " " . . . | 12.5 | 71 | 113.4 | 131.6 | 200.3 | 271 | 340 | | |
| " " . . . | 50 | 58.2 | 93.7 | 108.6 | 163.3 | 219.5 | 272.4 | | |
| " " . . . | 100 | 53 | 84.9 | 98.4 | 148.1 | 198.1 | 245 | | |
| " " . . . | 200 | 48.8 | 77.8 | 90.1 | 135.7 | 180.6 | 222.3 | | |
| " " . . . | 400 | 45.4 | 72.1 | 83.3 | 124.8 | 165.7 | 203.1 | | |
| Barium ferrocyanide . | 0 | 91 | 150 | 176 | 277 | 393 | 521 | | |
| " " . . . | 2 | 46.9 | 75 | 86.2 | 127.5 | 166.2 | 202.3 | | |
| " " . . . | 12.5 | 30.4 | 48.8 | 56.5 | 83.1 | 107 | 129.8 | | |
| Calcium ferrocyanide . | 0 | 88 | 146 | 171 | 271 | 386 | 512 | | |
| " " . . . | 2 | 47.1 | 75.5 | 86.2 | 130 | | | | |
| " " . . . | 12.5 | 31.2 | 49.9 | 57.4 | | | | | |
| " " . . . | 50 | 24.1 | 38.5 | 44.4 | 64.6 | 81.9 | | | |
| " " . . . | 100 | 21.9 | 35.1 | 40.2 | 58.4 | 73.7 | 84.3 | | |
| " " . . . | 200 | 20.6 | 32.9 | 37.8 | 55 | 68.7 | 77.5 | | |
| " " . . . | 400 | 20.2 | 32.2 | 37.1 | 54 | 67.5 | 76.2 | | |
| Potassium citrate . . . | 0 | 76.4 | 124.6 | 144.5 | 228 | 320 | 420 | | |
| " " . . . | 0.5 | - | 120.1 | 139.4 | | | | | |
| " " . . . | 2 | 71 | 115.4 | 134.5 | 210.1 | 293.8 | 381.2 | | |
| " " . . . | 5 | 67.6 | 109.9 | 128.2 | 198.7 | 276.5 | 357.2 | | |
| " " . . . | 12.5 | 62.9 | 101.8 | 118.7 | 183.6 | 254.2 | 326 | | |
| " " . . . | 50 | 54.4 | 87.8 | 102.1 | 157.5 | 215.5 | 273 | | |
| " " . . . | 100 | 50.2 | 80.8 | 93.9 | 143.7 | 196.5 | 247.5 | | |
| " " . . . | 300 | 43.5 | 69.8 | 81 | 123.5 | 167 | 209.5 | | |
| Lanthanum nitrate . . . | 0 | 75.4 | 122.7 | 142.6 | 223 | 313 | 413 | 531 | 651 |
| " " . . . | 2 | 68.9 | 110.8 | 128.9 | 200.5 | 279.8 | 363.5 | 457.5 | 549 |
| " " . . . | 12.5 | 61.4 | 98.5 | 114.4 | 176.7 | 243.4 | 311.2 | 383.4 | 447.8 |
| " " . . . | 50 | 54 | 86.1 | 99.7 | 152.5 | 207.6 | 261.4 | 315.8 | 357.7 |
| " " . . . | 100 | 49.9 | 79.4 | 91.8 | 139.5 | 189.1 | 236.7 | 282.5 | 316.3 |
| " " . . . | 200 | 46 | 72.1 | 83.5 | 126.4 | 170.2 | 210.8 | 249.6 | 276.2 |

From the investigations of Noyes and Johnston, Journal of the American Chemical Society, 31, p. 287, 1909.

TABLES 511 AND 512

TABLE 511.—The Equivalent Conductivity of the Separate Ions

| Ion. | 0° | 18° | 25° | 50° | 75° | 100° | 128° | 156° |
|--|------|-----------------|------|-----|-----|------|------|------|
| K | 40.4 | 64.6 | 74.5 | 115 | 159 | 206 | 263 | 317 |
| Na | 26 | 43.5 | 50.9 | 82 | 116 | 155 | 203 | 249 |
| NH ₄ | 40.2 | 64.5 | 74.5 | 115 | 159 | 207 | 264 | 319 |
| Ag | 32.9 | 54.3 | 63.5 | 101 | 143 | 188 | 245 | 299 |
| $\frac{1}{2}$ Ba | 33 | 55 ² | 65 | 104 | 149 | 200 | 262 | 322 |
| $\frac{1}{2}$ Ca | 30 | 51 ² | 60 | 98 | 142 | 191 | 252 | 312 |
| $\frac{1}{3}$ La | 35 | 61 | 72 | 119 | 173 | 235 | 312 | 388 |
| Cl | 41.1 | 65.5 | 75.5 | 116 | 160 | 207 | 264 | 318 |
| NO ₃ | 40.4 | 61.7 | 70.6 | 104 | 140 | 178 | 222 | 263 |
| C ₂ H ₃ O ₂ | 20.3 | 34.6 | 40.8 | 67 | 96 | 130 | 171 | 211 |
| $\frac{1}{2}$ SO ₄ | 41 | 68 ² | 79 | 125 | 177 | 234 | 303 | 370 |
| $\frac{1}{2}$ C ₂ O ₄ | 39 | 63 ² | 73 | 115 | 163 | 213 | 275 | 336 |
| $\frac{1}{3}$ C ₆ H ₅ O ₇ | 36 | 60 | 70 | 113 | 161 | 214 | | |
| $\frac{1}{4}$ Fe(CN) ₆ | 58 | 95 | 111 | 173 | 244 | 321 | | |
| H | 240 | 314 | 350 | 465 | 565 | 644 | 722 | 777 |
| OH | 105 | 172 | 192 | 284 | 360 | 439 | 525 | 592 |

From Johnson, Journ. Amer. Chem. Soc., 31, p. 1010, 1909.

TABLE 512.—Hydrolysis of Ammonium Acetate and Ionization of Water

| Temperature. | Percentage hydrolysis. | Ionization constant of water. | Hydrogen-ion concentration in pure water. Equivalents per liter. |
|--------------|------------------------|-----------------------------------|--|
| <i>t</i> | 100h | K _w × 10 ¹⁴ | C _H × 10 ⁷ |
| 0 | — | 0.089 | 0.30 |
| 18 | (0.35) | 0.46 | 0.68 |
| 25 | — | 0.82 | 0.91 |
| 100 | 4.8 | 48. | 6.9 |
| 156 | 18.6 | 223. | 14.9 |
| 218 | 52.7 | 461. | 21.5 |
| 306 | 91.5 | 168. | 13.0 |

Noyes, Kato, Kanolt, Sosman, No. 63 Publ. Carnegie Inst., Washington.

SMITHSONIAN TABLES.

DIELECTRIC STRENGTH

TABLE 513.—Steady Potential Difference in Volts required to produce a Spark in Air with Ball Electrodes

| Spark length. cm. | $R = 0$ Points. | $R = 0.25$ cm. | $R = 0.5$ cm. | $R = 1$ cm. | $R = 2$ cm. | $R = 3$ cm. | $R = \infty$ Plates. |
|----------------------|--------------------|-------------------|------------------|-------------|-------------|-------------|-------------------------|
| 0.02 | — | — | 1560 | 1530 | | | |
| 0.04 | — | — | 2460 | 2430 | 2340 | | |
| 0.06 | — | — | 3300 | 3240 | 3060 | | |
| 0.08 | — | — | 4050 | 3990 | 3810 | | |
| 0.1 | 3720 | 5010 | 4740 | 4560 | 4560 | 4500 | 4350 |
| 0.2 | 4680 | 8610 | 8490 | 8490 | 8370 | 7770 | 7590 |
| 0.3 | 5310 | 11140 | 11460 | 11340 | 11190 | 10560 | 10650 |
| 0.4 | 5970 | 14040 | 14310 | 14340 | 14250 | 13140 | 13560 |
| 0.5 | 6300 | 15990 | 16950 | 17220 | 16650 | 16470 | 16320 |
| 0.6 | 6840 | 17130 | 19740 | 20070 | 20070 | 19380 | 19110 |
| 0.8 | 8070 | 18960 | 23790 | 24780 | 25830 | 26220 | 24960 |
| 1.0 | 8670 | 20670 | 26190 | 27810 | 29850 | 32760 | 30840 |
| 1.5 | 9960 | 22770 | 29970 | 37260 | | | |
| 2.0 | 10140 | 24570 | 33060 | 45480 | | | |
| 3.0 | 11250 | 28380 | | | | | |
| 4.0 | 12210 | 29580 | | | | | |
| 5.0 | 13050 | | | | | | |

Based on the results of Baille, Bichat-Blondot, Freyburg, Liebig, Macfarlane, Orgler, Paschen, Quincke, de la Rue, Wolff. For spark lengths from 1 to 200 wave-lengths of sodium light, see Earhart, Phys. Rev. 15, p. 163; Hobbs, Phil. Mag. 10, p. 607, 1905.

TABLE 514.—Alternating Current Potential required to produce a Spark in Air with various Ball Electrodes

The potentials given are the maxima of the alternating waves used. Frequency, 33 cycles per second.

| Spark length. cm. | $R = 1$ cm. | $R = 1.92$ | $R = 5$ | $R = 7.5$ | $R = 10$ | $R = 15$ |
|----------------------|-------------|------------|---------|-----------|----------|----------|
| 0.08 | 3770 | | | | | |
| .10 | 4400 | 4380 | 4330 | 4290 | 4245 | 4230 |
| .15 | 5990 | 5940 | 5830 | 5790 | 5800 | 5780 |
| .20 | 7510 | 7440 | 7340 | 7250 | 7320 | 7330 |
| .25 | 9045 | 8970 | 8850 | 8710 | 8760 | 8760 |
| 0.30 | 10480 | 10400 | 10270 | 10130 | 10180 | 10150 |
| .35 | 11980 | 11890 | 11670 | 11570 | 11610 | 11590 |
| .40 | 13360 | 13300 | 13100 | 12930 | 12980 | 12970 |
| .45 | 14770 | 14700 | 14400 | 14290 | 14330 | 14320 |
| .50 | 16140 | 16070 | 15890 | 15640 | 15690 | 15690 |
| 0.6 | 18700 | 18730 | 18550 | 18300 | 18350 | 18400 |
| .7 | 21350 | 21380 | 21140 | 20980 | 20990 | 21000 |
| .8 | 23820 | 24070 | 23740 | 23490 | 23540 | 23550 |
| 0.9 | 26190 | 26640 | 26400 | 26130 | 26110 | 26090 |
| 1.0 | 28380 | 29170 | 28950 | 28770 | 28680 | 28610 |
| 1.2 | 32400 | 34100 | 33790 | 33660 | 33640 | 33620 |
| 1.4 | 35850 | 38850 | 38850 | 38580 | 38620 | 38580 |
| 1.6 | 38750 | 43400 | 43570 | 43250 | 43520 | |
| 1.8 | 40900 | — | 48300 | 47900 | | |
| 2.0 | 42950 | — | — | 52400 | | |

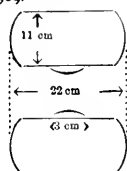
Based upon the results of Kawalski, Phil. Mag. 18, p. 699, 1909.

TABLES 515 AND 516 DIELECTRIC STRENGTH

TABLE 515.—Potential Necessary to produce a Spark in Air between more widely Separated Electrodes

| Spark length, cm. | Dull points. Alter- nating current. | Steady potentials. | | | | Spark length, cm. | Dull points. Alter- nating current. | Steady potentials. | |
|-------------------|--|--------------------|-----------|-----------------|---------|-------------------|--|--------------------|-----------|
| | | Ball electrodes. | | Cup electrodes. | | | | Ball electrodes. | |
| | | R=1 cm. | R=2.5 cm. | Projection. | | | | R=1 cm. | R=2.5 cm. |
| | | | | 4.5 mm. | 1.5 mm. | | | | |
| 0.3 | - | - | - | - | 11280 | 6.0 | 61000 | - | 86830 |
| 0.5 | - | 17610 | 17620 | - | 17420 | 7.0 | - | 52000 | - |
| 0.7 | - | - | 23050 | - | 22950 | 8.0 | 67000 | 52400 | 90200 |
| 1.0 | 12000 | 30240 | 31390 | 31400 | 31260 | 10.0 | 73000 | 74300 | 91930 |
| 1.2 | - | 33800 | 36810 | - | 36700 | 12.0 | 82600 | - | 93300 |
| 1.5 | - | 37930 | 44310 | - | 44510 | 14.0 | 92000 | - | 94400 |
| 2.0 | 29200 | 42320 | 50000 | 56500 | 56530 | 15.0 | - | - | 94700 |
| 2.5 | - | 45000 | 65180 | - | 68720 | 16.0 | 101000 | - | 101000 |
| 3.0 | 40000 | 46710 | 71200 | 80400 | 81140 | 20.0 | 119000 | | |
| 3.5 | - | - | 75300 | - | 92400 | 25.0 | 140600 | | |
| 4.0 | 48500 | 49100 | 78600 | 101700 | 103800 | 30.0 | 165700 | | |
| 4.5 | - | - | 81540 | - | 114600 | 35.0 | 190900 | | |
| 5.0 | 56500 | 50310 | 83800 | - | 126500 | | | | |
| 5.5 | - | - | - | - | 135700 | | | | |

This table for longer spark lengths contains the results of Voege, Ann. der Phys. 14, 1904, using alternating current and "dull point" electrodes, and the results with steady potential found in the recent very careful work of C. Müller, Ann. d. Phys. 28, p. 585, 1909.



The specially constructed electrodes for the columns headed "cup electrodes" had the form of a projecting knob 3 cm in diameter and having a height of 4.5 mm and 1.5 mm respectively, attached to the plane face of the electrodes. These electrodes give a very satisfactory linear relation between the spark lengths and the voltage throughout the range studied.

TABLE 516.—Effect of the Pressure of the Gas on the Dielectric Strength

Voltages are given for different spark lengths l .

| Pressure, cm Hg | $l=0.04$ | $l=0.06$ | $l=0.08$ | $l=0.10$ | $l=0.20$ | $l=0.30$ | $l=0.40$ | $l=0.50$ |
|-----------------|----------|----------|----------|----------|----------|----------|----------|----------|
| 2 | — | — | — | — | 744 | 939 | 1110 | 1266 |
| 4 | — | 483 | 567 | 648 | 1015 | 1350 | 1645 | 1915 |
| 6 | — | 582 | 690 | 795 | 1290 | 1740 | 2140 | 2505 |
| 10 | — | 771 | 933 | 1090 | 1840 | 2450 | 3015 | 3580 |
| 15 | — | 1060 | 1280 | 1490 | 2460 | 3300 | 4080 | 4850 |
| 25 | 1110 | 1420 | 1725 | 2040 | 3500 | 4800 | 6000 | 7120 |
| 35 | 1375 | 1820 | 2220 | 2615 | 4505 | 6270 | 7870 | 9340 |
| 45 | 1640 | 2150 | 2660 | 3120 | 5475 | 7650 | 9620 | 11420 |
| 55 | 1820 | 2420 | 3025 | 3610 | 6375 | 8950 | 11290 | 13455 |
| 65 | 2040 | 2720 | 3400 | 4060 | 7245 | 10210 | 12950 | 15470 |
| 75 | 2255 | 3035 | 3805 | 4565 | 8200 | 11570 | 14650 | 17450 |

This table is based upon the results of Orgler, 1899. See this paper for work on other gases (or Landolt-Börnstein-Meyerhoffer).

For long spark lengths in various gases see Voege, Electrotechn. Z. 28, 1907. For dielectric strength of air and CO₂ in cylindrical air condensers, see Wien, Ann. d. Phys. 29, p. 679, 1909.

TABLES 517 AND 518

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TABLE 517.—Dielectric Strength of Materials

Potential necessary for puncture expressed in kilovolts per centimeter thickness of the dielectric.

| Substance. | Kilovolts per cm. | Substance. | Kilovolts per cm. | Substance. | Kilovolts per cm. |
|-------------------|-------------------|-------------------|-------------------|--------------------|-------------------|
| Ebonite | 300-1100 | Oils: Thickness | | Papers: | |
| Empire cloth . . | 80-300 | Castor | 0.2 mm 190 | Beeswaxed . . . | 770 |
| " paper | 450 | " | 1.0 " 130 | Blotting | 150 |
| Fibre | 20 | Cottonseed . . . | 70 | Manilla | 25 |
| Fuller board . . | 200-300 | Lard | 0.2 " 140 | Paraffined . . . | 500 |
| Glass | 300-1500 | " | 1.0 " 40 | Varnished | 100-250 |
| Granite (fused) . | 90 | Linseed, raw . . | 0.2 " 185 | Paraffine: | |
| Guttapercha . . | 80-200 | " | 1.0 " 90 | Melted | 75 |
| Impregnated jute | 20 | " boiled | 0.2 " 190 | " Melt point. | |
| Leatheroid . . . | 30-60 | " | 1.0 " 80 | Solid 43° | 350 |
| Linen, varnished | 100-200 | Lubricating . . | 50 | " 47° | 400 |
| Liquid air . . . | 40-90 | Neatsfoot . . . | 0.2 " 200 | " 52° | 230 |
| Mica: Thickness. | | " | 1.0 " 90 | " 70° | 450 |
| Madras 0.1 mm . | 1600 | Olive | 0.2 " 170 | Presspaper . . . | 45-75 |
| " 1.0 " | 300 | " | 1.0 " 75 | Rubber | 160-500 |
| Bengal 0.1 " . | 2200 | Paraffin | 0.2 " 215 | Vaseline | 90-130 |
| " 1.0 " | 700 | " | 1.0 " 160 | Thickness. | |
| Canada 0.1 " . | 1500 | Sperm, mineral . | 0.2 " 180 | Xylene 0.2 mm . | 140 |
| " 1.0 " | 500 | " | 1.0 " 85 | " 1.0 " | 80 |
| South America . | 1500 | " natural | 0.2 " 195 | | |
| Micanite | 400 | " | 1.0 " 90 | | |
| | | Turpentine . . . | 0.2 " 160 | | |
| | | " | 1.0 " 110 | | |

TABLE 518.—Potentials in Volts to Produce a Spark in Kerosene

| Spark length. mm. | Electrodes Balls of Diam. <i>d</i> . | | | |
|----------------------|--------------------------------------|-------|-------|-------|
| | 0.5 cm. | 1 cm. | 2 cm. | 3 cm. |
| 0.1 | 3800 | 3400 | 2750 | 2200 |
| .2 | 7500 | 6450 | 4800 | 3500 |
| .3 | 10250 | 9450 | 7450 | 4600 |
| .4 | 11750 | 10750 | 9100 | 5600 |
| .5 | 13050 | 12400 | 11000 | 6900 |
| .6 | 14000 | 13550 | 12250 | 8250 |
| .8 | 15500 | 15100 | 13850 | 10450 |
| 1.0 | 16750 | 16400 | 15250 | 12350 |

Determinations of the dielectric strength of the same substance by different observers do not agree well For a discussion of the sources of error see Mościcki, *Electrotechn. Z.* 25, 1904.

For more detailed information on the dependence of the sparking distance in oils as a function of the nature of the electrodes, see Edmondson, *Phys. Review* 6, p. 65, 1898.

TABLE 519.—Dielectric Constant (Specific Inductive Capacity) of Gases

Atmospheric Pressure

Wave lengths of the measuring current greater than 10000 cm

| Gas | °C | Dielectric constant | | Ref. | Gas | °C | Dielectric constant | | Ref. |
|-------------------------------|-----|---------------------|----------|------|--------------------------|-----|---------------------|----------|------|
| | | Vacuum = 1 | Air = 1 | | | | Vacuum = 1 | Air = 1 | |
| Air | 0 | 1.000588 | 1.000000 | (1) | HCl | 100 | 1.00258 | 1.00199 | (2) |
| NH ₃ | 20 | 1.00718 | 1.00659 | (2) | H ₂ | 0 | 1.000264 | .999676 | (1) |
| CS ₂ | 0 | 1.00290 | 1.00231 | (3) | CH ₄ | 0 | 1.000948 | 1.000360 | (2) |
| " | 100 | 1.00239 | 1.00180 | (2) | N ₂ O | 0 | 1.00108 | 1.00050 | (1) |
| CO ₂ | 0 | 1.000966 | 1.000377 | (1) | SO ₂ | 0 | 1.00993 | 1.00934 | (2) |
| CO | 0 | 1.000692 | 1.000104 | (1) | H ₂ O, 4 atm. | 145 | 1.00705 | 1.00646 | (2) |
| C ₂ H ₄ | 0 | 1.00138 | 1.00079 | (1) | | | | | |

(1) Mean. (2) Bädcker, 1901. (3) Klemenčič, 1885.

TABLE 520.—Variation of the Dielectric Constant with the Temperature

If $\epsilon\theta$ = the dielectric constant at the temperature $\theta^\circ\text{C}$ of the above table, ϵ_t at the temperature $t^\circ\text{C}$, and α and β are quantities in the following table, then $\epsilon_t = \epsilon\theta - \alpha(t - \theta) + \beta(t - \theta)^2$.

| | | | |
|---------------------------|--------------------------------|-------------------------------|---------------------------------|
| Ammonia, | $\alpha = 5.45 \times 10^{-5}$ | $\beta = 2.59 \times 10^{-7}$ | Range, 15-110°C 0-110 145 |
| Sulphur dioxide | 6.19×10^{-5} | 1.86×10^{-7} | |
| Water vapor. | 1.4×10^{-4} | | |

The dielectric constant of air at 76 cm and varying temperature may be calculated since $D - 1$ is approximately proportional to the density.

TABLE 521.—Variation of the Dielectric Constant of Gases with the Pressure

| | °C | Pressure atm. | | | | °C | Pressure atm. | | |
|-----|----|---------------|--------|-----|------------------|----|---------------|--------|-----|
| Air | 19 | 20 | 1.0108 | (1) | Air | 11 | 120 | 1.0579 | (2) |
| " | " | 40 | 1.0218 | (1) | " | " | 140 | 1.0674 | (2) |
| " | " | 60 | 1.0330 | (1) | " | " | 160 | 1.0760 | (2) |
| " | " | 80 | 1.0439 | (1) | " | " | 180 | 1.0845 | (2) |
| " | " | 100 | 1.0548 | (1) | CO ₂ | 15 | 10 | 1.008 | (3) |
| " | 11 | 20 | 1.0101 | (2) | " | " | 20 | 1.020 | (3) |
| " | " | 40 | 1.0196 | (2) | " | " | 40 | 1.060 | (3) |
| " | " | 60 | 1.0294 | (2) | N ₂ O | 15 | 10 | 1.010 | (3) |
| " | " | 80 | 1.0387 | (2) | " | " | 20 | 1.025 | (3) |
| " | " | 100 | 1.0482 | (2) | " | " | 40 | 1.070 | (3) |

(1) Tangl, 1907. (2) Occhialini, 1905. (3) Linde, 1895.

TABLE 522.—Dielectric Constant of Liquids (ϵ). Pressure Effect

(Danforth, Phys. Rev., 38, 1224, 1931.)

| | P atm. | 30°C | | 75°C | | | P atm. | 0°C | | 30°C | | |
|--|-----------|-------|---------|-------|---------|--|-----------|------|---------|-------|-------|-------|
| | | ε | Density | ε | Density | | | ε | Density | | | |
| C ₂ H ₅ OH..... | 1 | 1.82 | 0.613 | | | Ethyl alcohol | 1000 | 27.8 | 0.806 | 23.2 | 0.781 | |
| Pentane | 1000 | 1.96 | .701 | 1.92 | | | 8000 | 29.4 | .864 | 25.3 | .844 | |
| | 4000 | 2.12 | .796 | 2.11 | | | 12000 | 35.3 | 1.031 | 31.7 | 1.019 | |
| | 8000 | 2.24 | .865 | 2.22 | | C ₄ H ₉ OH..... | 1 | 21.1 | .819 | 17.3 | .806 | |
| | 12000 | 2.33 | .907 | 2.31 | | i-butyl alcohol | 1000 | 22.9 | .877 | 18.7 | .856 | |
| CS ₂ | 1 | 2.61 | 1.241 | | | | 8000 | 26.8 | 1.031 | 22.8 | 1.018 | |
| Carbon bisulphide | 1000 | 2.82 | 1.332 | 2.69 | 1.29 | | 12000 | 28.2 | 1.080 | 23.9 | 1.069 | |
| | 4000 | 3.11 | 1.487 | 3.02 | 1.46 | C ₃ H ₈ O ₃ | 1 | 49.9 | 1.272 | 42.8 | 1.254 | |
| | 8000 | 3.33 | 1.601 | 3.28 | 1.58 | Glycerine | 1000 | 51.9 | 1.305 | 44.8 | 1.287 | |
| | 12000 | 3.52 | 1.689 | 3.45 | 1.66 | | 4000 | 56.4 | 1.367 | 49.1 | 1.349 | |
| (C ₂ H ₅) ₂ O..... | 1 | 4.15 | .720 | | | | 8000 | 61.1 | 1.429 | 53.8 | 1.410 | |
| Ether | 1000 | 4.88 | .801 | 4.08 | .74 | Anomalous dispersion 247000 cycles | | | | | | |
| | 4000 | 6.05 | .911 | 5.17 | .87 | Isobutyl-alcohol: 0°C | | | | | | |
| | 8000 | 6.93 | .988 | 6.00 | .94 | P:..... | 1 | 2900 | 5810 | 9680 | 10830 | 12130 |
| | 12000 | 7.68 | 1.047 | 6.94 | 1.00 | ε:..... | 21.1 | 24.4 | 25.9 | 27.4 | 27.2 | 26.4 |
| C ₆ H ₅ Br..... | 1 | 5.22 | 1.465 | 4.87 | 1.40 | Glycerine..P | 1 | 1940 | 4290 | 6330 | 8490 | |
| Bromo-benzene | 500 | 5.36 | 1.525 | 5.05 | 1.46 | 0°C..... | ε | 49.9 | 53.4 | 55.6 | 52.2 | 40.1 |
| | 1000 | 5.47 | 1.558 | 5.16 | 1.50 | Eugenol....P | 1 | 2960 | 5081 | 5680 | 6300 | |
| | 4000 | 5.88 | 1.705 | 5.62 | 1.65 | 30°C..... | ε | 9.42 | 10.79 | 11.09 | 10.57 | 6.05 |
| | 8000 | | | 5.95 | 1.76 | | | | | | | |
| C ₆ H ₅ Cl..... | 1 | 5.41 | 1.004 | 4.90 | .96 | | | | | | | |
| Chloro-benzene | 500 | 5.59 | 1.038 | 5.12 | 1.00 | | | | | | | |
| | 1000 | 5.75 | 1.065 | 5.28 | 1.03 | | | | | | | |
| | 4000 | 6.33 | 1.152 | 5.88 | 1.13 | | | | | | | |
| | 8000 | | | 6.29 | 1.20 | | | | | | | |
| C ₆ H ₁₃ OH.... | 1 | 12.90 | .812 | 8.55 | .78 | | | | | | | |
| Hexyl alcohol | 1000 | 13.54 | .861 | 9.32 | .84 | | | | | | | |
| | 4000 | 15.06 | .937 | 10.42 | .92 | | | | | | | |
| | 8000 | | | 11.15 | .99 | | | | | | | |

TABLE 523.—Dielectric Constant of Liquids

A wave length greater than 10000 centimeters is denoted by ∞ .

| Substance | Temp. °C. | Wave-length, cm. | Dielectric constant. | Author- ity. | Substance. | Temp. °C. | Wave-length, cm. | Dielectric constant. | Author- ity. |
|--------------|--------------|---------------------|-------------------------|-----------------|------------------|--------------|---------------------|-------------------------|-----------------|
| Alcohol: | | | | | Alcohol: | | | | |
| Amyl . . . | frozen | ∞ | 2.4 | 1 | Methyl . . . | -50 | ∞ | 45.3 | 1 |
| " . . . | -100 | " | 30.1 | 1 | " . . . | 0 | " | 35.0 | 1 |
| " . . . | -50 | " | 23.0 | 1 | " . . . | +20 | " | 31.2 | 1 |
| " . . . | 0 | " | 17.4 | 1 | " . . . | 17 | 75 | 33.2 | 2 |
| " . . . | +20 | " | 16.0 | 1 | Propyl . . . | -120 | " | 46.2 | 1 |
| " . . . | 18 | 200 | 10.8 | 2 | " . . . | -60 | " | 33.7 | 1 |
| " . . . | 18 | 73 | 4.7 | 2 | " . . . | 0 | " | 24.8 | 1 |
| Ethyl . . . | frozen | ∞ | 2.7 | 1 | " . . . | +20 | " | 22.2 | 1 |
| " . . . | -120 | " | 54.6 | 1 | " . . . | 15 | 75 | 12.3 | 2 |
| " . . . | -80 | " | 44.3 | 1 | Acetone . . . | -80 | ∞ | 33.8 | 5 |
| " . . . | -40 | " | 35.3 | 1 | " . . . | 0 | " | 26.6 | 5 |
| " . . . | 0 | " | 28.4 | 1 | " . . . | 15 | 1200 | 21.85 | 6 |
| " . . . | +20 | " | 25.8 | 1 | " . . . | 17 | 73 | 20.7 | 7 |
| " . . . | 17 | 200 | 24.4 | 2 | Acetic acid . . | 18 | ∞ | 9.7 | 8 |
| " . . . | " | 75 | 23.0 | 2 | " . . . | 15 | 1200 | 10.3 | 6 |
| " . . . | " | 53 | 20.6 | 3 | " . . . | 17 | 200 | 7.07 | 2 |
| " . . . | " | 4 | 8.8 | 3 | " . . . | 19 | 75 | 6.29 | 2 |
| " . . . | " | 0.4 | 5.0 | 4 | Amyl acetate . . | 19 | ∞ | 4.81 | 9 |
| Methyl . . . | frozen | ∞ | 3.07 | 1 | Amylene . . . | 16 | " | 2.20 | 10 |
| " . . . | -100 | " | 58.0 | 1 | | | | | |

DIELECTRIC CONSTANT OF LIQUIDS

A wave length greater than 10000 centimeters is designated by ∞.

| Substance. | Temp. °C. | Wave- length cm. | Di- el. const. | Author- ity. | Substance. | Temp. °C. | Wave- length cm. | Di- el. const. | Author- ity. |
|---|---------------|------------------------|----------------------|-----------------|---------------------------|-----------------|------------------------|----------------------|-----------------|
| Aniline | 18 | ∞ | 7.316 | 11 | Nitrobenzol | (frozen) -10 | ∞ | 9.9 | 1 |
| Benzol (benzene) | 18 | | 2.288 | | " | -5 | " | 42.0 | " |
| " | 19 | 73 | 2.26 | 2 | " | 0 | " | 41.0 | " |
| Bromine | 23 | 84 | 3.18 | 12 | " | +15 | " | 37.8 | " |
| Carbon bisulphide | 20 | ∞ | 2.626 | 13 | " | 30 | " | 35.1 | " |
| " | 17 | 73 | 2.64 | 2 | " | 18 | " | 36.45 | 11 |
| Chloroform | 18 | ∞ | 5.2 | 11 | " | 17 | 73 | 34.0 | 2 |
| " | 17 | 73 | 4.95 | 2 | Octane | 17 | ∞ | 1.949 | 16 |
| Decane | 14 | ∞ | 1.97 | 10 | Oils : | | | | |
| Decylene | 17 | " | 2.24 | " | Almond | 20 | ∞ | 2.83 | 18 |
| Ethyl ether | -80 | ∞ | 7.05 | 5 | Castor | 11 | " | 4.67 | 19 |
| " | -40 | " | 5.67 | " | Colza | 20 | " | 3.11 | 20 |
| " | 0 | " | 4.68 | " | Cottonseed | 14 | " | 3.10 | 21 |
| " | 18 | " | 4.368 | 11 | Lemon | 21 | " | 2.25 | 22 |
| " | 20 | " | 4.30 | 13 | Linseed | 13 | " | 3.35 | 21 |
| " | 60 | " | 3.65 | " | Neatsfoot | - | " | 3.02 | 20 |
| " | 100 | " | 3.12 | " | Olive | 20 | " | 3.11 | 23 |
| " | 140 | " | 2.66 | " | Peanut | 11.4 | " | 3.03 | 21 |
| " | 180 | " | 2.12 | " | Petroleum | - | 2000 | 2.13 | 24 |
| " | Crit. temp | " | | | Petroleum ether | 20 | ∞ | 1.92 | 20 |
| " | 192 | " | 1.53 | " | Rape seed | 16 | " | 2.85 | 21 |
| " | 18 | 83 | 4.35 | 14 | Sesame | 13.4 | " | 3.02 | " |
| Formic acid | +2 | 73 | 19.0 | 2 | Sperm | 20 | " | 3.17 | 20 |
| " | (frozen) | | | | Turpentine | 20 | " | 2.23 | " |
| " | 15 | 1200 | 62.0 | 6 | Vaseline | - | " | 2.17 | 25 |
| " | 16 | 73 | 58.5 | 2 | Phenol | 48 | 73 | 9.68 | 2 |
| Glycerine | 15 | 1200 | 56.2 | 6 | Toluene | -83 | ∞ | 2.51 | 5 |
| " | 15 | 200 | 39.1 | 2 | " | +16 | " | 2.33 | " |
| " | 15 | 75 | 25.4 | " | " | 19 | 73 | 2.31 | 2 |
| " | - | 8.5 | 4.4 | 15 | Meta-xylene | 18 | ∞ | 2.37 ⁶ | 11 |
| " | - | 0.4 | 2.6 | 4 | " | 17 | 73 | 2.37 | 2 |
| Hexane | 17 | ∞ | 1.880 | 16 | | | | | |
| Hydrogen perox- } ide 46 % in H ₂ O } | 18 | 75 | 84.7 | 17 | Water | 18 | ∞ | 81.07 | 11 |
| | | | | | for temp. coeff. | 17 | 200 | 86.6 | 2 |
| | | | | | see Table 524. | 17 | 74 | 81.7 | " |
| | | | | | | 17 | 38 | 83.6 | " |

- 1 Abegg-Seitz, 1899.
- 2 Drude, 1896.
- 3 Marx, 1898.
- 4 Lampa, 1896.
- 5 Abegg, 1897.
- 6 Thwing, 1894.
- 7 Drude, 1898.
- 8 Francke, 1893.
- 9 Löwe, 1898.

- 10 Landolt-Jahn, 1892.
- 11 Turner, 1900.
- 12 Schlundt.
- 13 Tangl, 1903.
- 14 Coolidge, 1899.
- 15 v. Lang, 1896.
- 16 Nernst, 1894.
- 17 Calvert, 1900.

- 18 Hasenöhl, 1896.
- 19 Arons-Rubens, 1892.
- 20 Hopkinson, 1881.
- 21 Salvioni, 1888.
- 22 Tomaszewski, 1888.
- 23 Heinke, 1896.
- 24 Marx.
- 25 Fuchs.

DIELECTRIC CONSTANT OF LIQUIDS

TABLE 524.—Temperature Coefficients of the Formula:

$$D_{\theta} = D_i[1 - \alpha(t - \theta) + \beta(t - \theta)^2]$$

| Substance. | α | β | Temp. range, °C. | Authority. |
|---------------------|----------|------------|---------------------|---------------|
| Amyl acetate . . . | 0.0024 | — | — | Löwe. |
| Aniline | 0.00351 | — | — | Ratz. |
| Benzene | 0.00106 | 0.0000087 | 10-40 | Hasenöhrl. |
| Carbon bisulphide . | 0.000966 | — | — | Ratz. |
| “ “ | 0.000922 | 0.00000060 | 20-181 | Tangl. |
| Chloroform | 0.00410 | 0.000015 | 22-181 | “ |
| Ethyl ether | 0.00459 | — | — | Ratz. |
| Methyl alcohol . . | 0.0057 | — | — | Drude. |
| Oils: Almond . . . | 0.00163 | 0.000026 | — | Hasenöhrl. |
| Castor | 0.01067 | — | — | Heinke, 1896. |
| Olive | 0.00364 | — | — | “ “ |
| Paraffine | 0.000738 | 0.0000072 | — | Hasenöhrl. |
| Toluene | 0.000921 | — | 0-13 | Ratz. |
| “ “ | 0.000977 | 0.00000046 | 20-181 | Tangl. |
| Water | 0.004474 | — | 5-20 | Heerwagen. |
| “ “ | 0.004583 | 0.0000117 | 0-76 | Drude. |
| “ “ | 0.00436 | — | 4-25 | Coolidge. |
| Meta-xylene . . . | 0.000817 | — | 20-181 | Tangl. |

(See Table 520 for the signification of the letters.)

TABLE 525.—Dielectric Constant of Liquefied Gases

A wave-length greater than 10000 centimeters is designated by ∞ .

| Substance. | Temp. °C. | Wave- length cm. | Diel. constant. | Authority. | Substance. | Temp. °C. | Wave- length cm. | Diel. constant | Authority. |
|------------------|--------------|---------------------|--------------------|------------|----------------------|--------------|---------------------|-------------------|------------|
| Air | -191 | ∞ | 1.432 | 1 | Nitrous oxide | | | | |
| “ “ | “ | 75 | 1.47-1.50 | 2 | “ “ N ₂ O | -88 | ∞ | 1.938 | 8 |
| Ammonia | -34 | 75 | 21-23 | 3 | “ “ . | -5 | “ | 1.630 | 5 |
| “ “ | 14 | 130 | 16.2 | 4 | “ “ . | +5 | “ | 1.578 | “ |
| Carbon dioxide . | -5 | ∞ | 1.608 | 5 | “ “ . | +15 | “ | 1.520 | “ |
| “ “ | 0 | “ | 1.583 | “ | Oxygen | -182 | “ | 1.491 | 9 |
| “ “ | +10 | “ | 1.540 | “ | “ “ . | “ | “ | 1.465 | 8 |
| “ “ | +15 | “ | 1.526 | “ | Sulphur dioxide . | 14.5 | 120 | 13.75 | 4 |
| Chlorine | -60 | “ | 2.150 | “ | “ “ . | 20 | ∞ | 14.0 | 6 |
| “ “ | -20 | “ | 2.030 | “ | “ “ . | 40 | “ | 12.5 | “ |
| “ “ | 0 | “ | 1.970 | “ | “ “ . | 60 | “ | 10.8 | “ |
| “ “ | +10 | “ | 1.940 | “ | “ “ . | 80 | “ | 9.2 | “ |
| “ “ | 0 | “ | 2.08 | 6 | “ “ . | 100 | “ | 7.8 | “ |
| “ “ | +14 | 100 | 1.88 | 4 | “ “ . | 120 | “ | 6.4 | “ |
| Cyanogen | 23 | 84 | 2.52 | 7 | “ “ . | 140 | “ | 4.8 | “ |
| Hydrocyanic acid | 21 | “ | about 95 | “ | Critical | 154.2 | “ | 2.1 | “ |
| Hydrogen sulph. | 10 | ∞ | 5.93 | 6 | | | | | |
| “ “ | 50 | “ | 4.92 | “ | | | | | |
| “ “ | 90 | “ | 3.76 | “ | | | | | |

1 v. Pirani, 1903.

2 Bahn-Kiebitz, 1904.

3 Goodwin-Thompson, 1899.

4 Coolidge, 1899.

5 Linde, 1895.

6 Eversheim, 1904.

7 Schlundt, 1901.

8 Hasenöhrl, 1900.

9 Fleming-Dewar, 1896.

TABLES 526 AND 527
DIELECTRIC CONSTANT

TABLE 526.—Standard Solutions for the Calibration of Apparatus for the Measuring of Dielectric Constant

| Turner. | | Drude. | | | | Nernst. | |
|-----------------------------|---|---|--------------|----------------------|--------------------|---|----------------------|
| Substance. | Diel. const. at 18°. $\lambda = \infty$. | Acetone in benzene at 19°. $\lambda = 75$ cm. | | | | Ethyl alcohol in water at 19.5°. $\lambda = \infty$. | |
| | | Per cent by weight. | Density 16°. | Dielectric constant. | Temp. coefficient. | Per cent by weight. | Dielectric constant. |
| Benzene | 2.288 | 0 | 0.885 | 2.26 | 0.1% | 100 | 26.0 |
| Meta-xylene | 2.376 | 20 | 0.866 | 5.10 | 0.3 | 90 | 29.3 |
| Ethyl ether | 4.367 | 40 | 0.847 | 8.43 | 0.4 | 80 | 33.5 |
| Aniline | 7.298 | 60 | 0.830 | 12.1 | 0.5 | 70 | 38.0 |
| Ethyl chloride | 10.90 | 80 | 0.813 | 16.2 | 0.5 | 60 | 43.1 |
| O-nitro toluene . . . | 27.71 | 100 | 0.797 | 20.5 | 0.6 | | |
| Nitrobenzene | 36.45 | | | | | | |
| Water (conduct. 10^{-6}) | 81.07 | | | | | | |
| | | Water in acetone at 19°. $\lambda = 75$ cm. | | | | | |
| | | 0 | 0.797 | 20.5 | 0.6% | | |
| | | 20 | 0.856 | 31.5 | 0.5 | | |
| | | 40 | 0.903 | 43.5 | 0.5 | | |
| | | 60 | 0.940 | 57.0 | 0.5 | | |
| | | 80 | 0.973 | 70.6 | 0.5 | | |
| | | 100 | 0.999 | 80.9 | 0.4 | | |

TABLE 527.—Dielectric Constant of Solids

| Substance. | Condition. | Wave-length, cm. | Dielectric constant. | Author-ity. | Substance. | Condition. | Wave-length, cm. | Dielectric constant. | Author-ity. |
|------------------------|------------|------------------|----------------------|-------------|-------------------------------|----------------|------------------|----------------------|-------------|
| Asphalt | — | ∞ | 2.68 | 1 | Iodine (cryst.) . . . | Temp. 23 | 75 | 4.00 | 2 |
| Barium sulphate . . . | — | 75 | 10.2 | 2 | Lead chloride (powder) | — | " | 42 | 2 |
| Caoutchouc | — | ∞ | 2.22 | 3 | " nitrate | — | " | 16 | 2 |
| Diamond | — | " | 16.5 | 1 | " sulphate | — | " | 28 | 2 |
| " | — | 75 | 5.50 | 2 | " molybdenate . . . | — | " | 24 | 2 |
| Ebonite | — | ∞ | 2.72 | 4 | Marble (Carrara) | — | " | 8.3 | 2 |
| " | — | " | 2.86 | 5 | Mica | — | ∞ | 5.66-5.97 | 5 |
| " | — | 1000 | 2.55 | 6 | " | — | " | 5.80-6.62 | 15 |
| Glass * | Density. | | | | Madras, brown . . . | — | " | 2.5-3.4 | 16 |
| Flint (extra heavy) . | 4.5 | ∞ | 9.90 | 7 | " green | — | " | 3.9-5.5 | 16 |
| Flint (very light) . . | 2.87 | " | 6.61 | 7 | " ruby | — | " | 4.4 | 16 |
| Hard crown | 2.48 | " | 6.96 | 7 | Bengal, yellow . . . | — | " | 2.8 | 16 |
| Mirror | — | " | 6.44-7.46 | 5 | " white | — | " | 4.2 | 16 |
| " | — | " | 5.37-5.90 | 8 | " ruby | — | " | 4.2-4.7 | 16 |
| " | — | 600 | 5.42-6.20 | 8 | Canadian amber . . . | — | " | 3.0 | 16 |
| Lead (Powell) | 3.0-3.5 | ∞ | 5.4-8.0 | 9 | South America Ozokerite (raw) | — | " | 5.9 | 16 |
| Jena | — | " | 5.5-8.1 | 10 | Paper (telephone) | — | " | 2.21 | 1 |
| Boron | — | " | 7.8-8.5 | 10 | " (cable) | — | " | 2.0 | 17 |
| Barium Borosilicate . | — | " | 6.4-7.7 | 1 | Paraffine | Melting point. | " | 2.46 | 18 |
| Gutta percha | — | " | 3.3-4.9 | 11 | " | 44-46 | " | 2.32 | 19 |
| Ice | Temp. —5 | 1200 | 2.85 | 12 | " | 54-56 | " | 2.10 | 20 |
| " | —18 | 5000 | 3.16 | 13 | " | 74-76 | " | 2.16 | 20 |
| " | —190 | 75 | 1.76-1.88 | 14 | | | | | |

References on p. 447.

* For the effect of temperature, see Gray-Dobbie, Pr. Roy. Soc. 63, 1898; 67, 1900.
" " " " wave-length, see K. F. Löwe, Wied. Ann. 66, 1893.

DIELECTRIC CONSTANT

TABLE 527 (continued).—Dielectric Constant of Solids

| Substance. | Condi- tion. | Wave- length, cm. | Diel. constant. | Author- ity. | Substance. | Condi- tion. | Wave- length, cm. | Diel. constant. | Author- ity. |
|-----------------|-----------------|-------------------------|--------------------|-----------------|--------------|---------------------------|-------------------------|--------------------|-----------------|
| Paraffine . . . | 47.°6 | 61 | 2.16 | 21 | Sulphur | | | | |
| " . . . | 50.°2 | 61 | 2.25 | 21 | Amorphous | — | ∞ | 3.98 | 1 |
| Phosphorus: | | | | | " | — | 75 | 3.80 | 2 |
| Yellow . . . | — | 75 | 3.60 | 2 | Cast, fresh | — | ∞ | 4.22 | 1 |
| Solid . . . | — | 80 | 4.1 | 22 | " " | — | " | 4.05 | 18 |
| Liquid . . . | — | 80 | 3.85 | 22 | " " | — | 75 | 3.95 | 2 |
| Porcelain: | | | | | Cast, old | — | ∞ | 3.60 | 18 |
| Hard | | | | | " " | — | 75 | 3.90 | 2 |
| (Royal B'l'n) | — | ∞ | 5.73 | 15 | Liquid . . . | near melting- point | ∞ | 3.42 | 1 |
| Seger " " | — | " | 6.61 | 15 | " " | | | | |
| Figure " " | — | " | 6.84 | 15 | Strontium | | | | |
| Selenium . . . | — | " | 7.44 | 1 | sulphate | — | 75 | 11.3 | 2 |
| " . . . | — | 75 | 6.60 | 2 | Thallium | | | | |
| " . . . | — | ∞ | 6.13 | 23 | carbonate | — | 75 | 17 | 2 |
| " . . . | — | 1000 | 6.14 | 23 | " nitrate | — | 75 | 16.5 | 2 |
| Shellac . . . | — | ∞ | 3.10 | 4 | Wood | | | | |
| " . . . | — | " | 2.95-3.73 | 24 | Red beech . | fibres | ∞ | 4.83-2.51 | — |
| " . . . | — | " | 3.07 | 25 | " " | ⊥ " | " | 7.73-3.63 | — |
| Amber . . . | — | — | 2.86 | 18 | Oak . . . | " | " | 4.22-2.46 | — |
| | | | | | " . . . | ⊥ " | " | 6.84-3.64 | — |

1 v. Pirani, 1903.
2 Schmidt, 1903.
3 Gordon, 1879.
4 Winklemann, 1889.
5 Elsas, 1891.
6 Ferry, 1897.
7 Hopkinson, 1891.
8 Arons-Rubens, 1891.
9 Gray-Dobbie, 1898.

10 Löwe, 1898.
11 (submarine-data).
12 Thwing, 1894.
13 Abegg, 1897.
14 Behn-Kiebitz, 1904.
15 Starke, 1897.
16 E. Wilson.
17 Campbell, 1906.

18 Fallinger, 1902.
19 Boltzmann, 1875.
20 Zietkowski, 1900.
21 Hormell, 1902.
22 Schlundt, 1904.
23 Vonwiller-Mason, 1907.
24 Wüllner, 1887.
25 Donle.

TABLE 528.—Dielectric Constant of Crystals

D_a, D_β, D_γ are the dielectric constants along the brachy, macro and vertical axes respectively.

| Substance. | Wave- length, cm. | Diel. const. | | Author- ity. | Substance. | Wave- length, cm. | Diel. const. | | | Author- ity. |
|----------------------------------|-------------------------|--------------|-------|-----------------|--------------------------------------|-------------------------|----------------|----------------|----------------|-----------------|
| | | ⊥ Axis. | Axis. | | | | D _a | D _β | D _γ | |
| UNIAXIAL: | | | | | RHOMBIC: | | | | | |
| Apatite . . . | 75 | 9.50 | 7.40 | 1 | Aragonite . . . | ∞ | 9.14 | — | 7.13 | 4 |
| Beryl . . . | ∞ | 7.85 | 7.44 | 2 | " . . . | 75 | 9.80 | 7.68 | 6.55 | 1 |
| " . . . | — | 7.10 | 6.05 | 3 | Barite . . . | ∞ | 6.97 | 10.09 | 7.00 | 4 |
| " . . . | 75 | 6.05 | 5.52 | 1 | " . . . | 75 | 7.65 | 12.20 | 7.70 | 1 |
| Calcite . . . | ∞ | 8.49 | 7.56 | 4 | Celestite . . . | 75 | 7.70 | 18.5 | 8.30 | 1 |
| " . . . | " | 8.78 | 8.29 | 5 | Cerussite . . . | 75 | 25.4 | 23.2 | 19.2 | 1 |
| Dolomite . . . | 75 | 7.80 | 6.80 | 1 | MgSO ₄ +7H ₂ O | ∞ | 5.26 | 6.05 | 8.28 | 7 |
| Iceland spar . . . | 75 | 8.50 | 8.00 | 1 | K ₂ SO ₄ . . . | " | 6.09 | 5.08 | 4.48 | 7 |
| Quartz . . . | ∞ | 4.69 | 5.06 | 4 | Rochelle salt* | " | 6.70 | 6.92 | 8.89 | 7 |
| " . . . | " | 4.38 | 4.46 | 6 | Sulphur . . . | " | 3.81 | 3.97 | 4.77 | 8 |
| " . . . | 1000 | 4.27 | 4.34 | 6 | " . . . | " | 3.65 | 3.85 | 4.66 | 7 |
| Ruby (Siam) . . . | — | 13.3 | 11.3 | 4 | " . . . | 75 | 3.62 | 3.85 | 4.66 | 1 |
| Rutile (TiO ₂) . . . | 75 | 89 | 1.73 | 1 | Topaz . . . | 75 | 6.65 | 6.70 | 6.30 | 1 |
| Tourmaline . . . | ∞ | 7.13 | 6.54 | 4 | " colorless . | — | 6.25 | 6.54 | 6.44 | 4 |
| " . . . | 75 | 6.75 | 5.65 | 1 | | | | | | |
| Zircon . . . | 75 | 12.8 | 12.6 | 1 | | | | | | |

1 Schmidt, 1903.
2 Starke, 1897.
3 Curie, 1889.

4 Fallinger, 1902, 1919.
5 v. Pirani, 1903.
6 Ferry, 1897.

7 Borel, 1893.
8 Boltzmann, 1875.

* See page 448.

ELECTROSTRICTION. PIEZO-ELECTRICITY

Electrostriction is a phenomenon observed when an isotropic dielectric is placed in an electrostatic field (F), the form and volume of the dielectric altering. Similar effects occur in anisotropic materials but are obscured by piezo-electric effects. Piezo-electricity occurs when a crystal dielectric is mechanically strained becoming electrically polarized. The magnitude and direction of the polarization (P) depends on the crystal used, the amount of strain and its direction relative to the axes of the crystal. Pyro-electricity is of the nature of a temperature-coefficient dp/dt . For fuller discussion and more extensive data see I.C.T., 6, 207, 1918 (Cody).

TABLE 529.—Electrostriction (Means)

| | Glass | Paraffin | Ebonite | Rubber (vulcanized) | |
|-----------------|----------------------|----------------------|-----------------------|------------------------|--------------------------------|
| $\Delta l/lE^2$ | $.4 \times 10^{-12}$ | 90×10^{-12} | 600×10^{-12} | 6000×10^{-12} | $\text{cm}^2/\text{c.g.s.e}^2$ |

These values divided by 1.11×10^{-5} for values in $\text{cm}^2/\text{volt}^2$.

TABLE 530.—Piezo-electricity

| | | | |
|--|------------|---|----------------------|
| Rochelle salt, $\text{KNaC}_4\text{H}_4\text{O}_6 \cdot 4\text{H}_2\text{O}$ | $d_{13} =$ | $17 \times 10^{-8} (\text{es}/\text{cm}^2)/(\text{dyne}/\text{cm}^2)$ | -70°C |
| " | | 8100 | +20 |
| " | | 1100 | +30 |
| " | | 400 | +40 |
| Benzil, $\text{C}_{14}\text{H}_{10}\text{O}_2$ | $d_{11} =$ | 24 | " |
| $\text{LiNa}_3(\text{MoO}_4)_2 \cdot 6\text{H}_2\text{O}$ | $d_{33} =$ | 14 | " |
| Rb. tartrate, $\text{Rb}_2\text{C}_4\text{H}_4\text{O}_6$ | $d_{11} =$ | 8 | " |
| Tartaric acid, $\text{C}_4\text{H}_6\text{O}_6$ | $d_{14} =$ | -24 | " |
| " | $d_{15} =$ | +28 | " |
| " | $d_{25} =$ | -36 | " |
| " | $d_{31} =$ | 2. | " |
| " | $d_{32} =$ | 6. | " |
| " | $d_{33} =$ | 6. | " |
| " | $d_{36} =$ | 4. | " |
| Tourmaline | $d_{33} =$ | 5.78 | " |
| " | $d_{15} =$ | 11.0 | " |
| " | $d_{22} =$ | 0.7 | " |
| " | $d_{31} =$ | 0.7 | " |
| Patchouli camphor, $\text{C}_{15}\text{H}_{20}\text{O}$ | $d_{11} =$ | .14 | " |
| Diamond, C | " | 0 | " |
| Quartz, SiO_2 | $d_{11} =$ | -6.9 | " |
| Sodium chlorate, NaClO_3 | $d_{11} =$ | -4.8 | " |
| Fenchoneoxene, $\text{C}_{10}\text{H}_{17}\text{NO}$ | $d_{33} =$ | -10.2 | " |

Addenda to Table 528, p. 447, Dielectric Constant of Rochelle Salt:

The polarization of the Rochelle salt dielectric in an electric field is somewhat analogous to the behavior of the magnetization of iron in a magnetic field, showing both saturation and hysteresis. The dielectric constant D depends on the initial and final fields and the hysteresis.

Initial field, 765 v/cm; Final field, 690 v/cm; Average D (23°C), 40

| | | |
|-----|------|-----|
| 765 | -153 | 205 |
| 765 | -765 | 157 |
| 0 | 880 | 86 |

The last value may be fair value for ordinary purposes. The electrodes were tinfoil attached with shellac. The field was applied perpendicular to the a axis. Like piezo-electric properties, the dielectric constant varies with different crystals. It depends on the temperature as follows: (field 0 to 880 v/cm)

-70°C , $D = 12$; -40° , 14; -20° , 48; 0° , 174; $+20^\circ$, 88; $+30^\circ$, 52.

(Data from Valesek, University of Minnesota, 1921.)

THE CALCULATION OF THE HIGH-FREQUENCY RESISTANCE OF CONDUCTORS

(By Dr. F. W. Grover, Consulting Physicist, Bur. Standards, 1931.)

The resistance of a conductor to high frequency alternating currents is not the same as it offers to direct or low frequency currents. The linkages of flux with the inner portions of the conductor are more numerous than with the outer portions. That is, the reactances of the inner filaments are greater than those of the outer filaments. Consequently, the current density decreases from the outside toward the center of the conductor.

This tendency of the current to crowd toward the outer portions of the cross section becomes more pronounced the higher the frequency, and at very high frequencies the current density is sensibly zero everywhere except in the surface layer of the conductor. This phenomenon is called the "skin effect." It causes an increase in the effective resistance of the conductor over its resistance to a direct current.

What is of interest in the calculation of the high frequency resistance is the *resistance ratio*, the quotient of the resistance at the given frequency by the direct current resistance. The resistance ratio depends upon the distribution of current density in the cross section, and this is a function of the frequency and the shape of the cross section. In general,

however, the resistance ratio is a function of the parameter $\frac{\sqrt{f}}{R_0}$, in which f is the frequency, and R_0 is the direct current resistance per unit length. In what follows R_0 will be taken as the direct current resistance per 1000 ft. of conductor.

The distribution of current in the cross section is affected by a neighboring conductor carrying high frequency currents. This *proximity effect* finds an explanation in that the value of the mutual inductance of any filament A of one conductor on a filament B of the other conductor depends upon the positions of A and B in their respective cross sections. The proximity effect may be very appreciable for conductors nearly in contact; falling off rapidly as their distance is increased, it is negligible for moderate ratios of distance apart to cross sectional dimensions. In such cases the resistance is sensibly the same as for an isolated conductor.

Beside the spacing factor of the conductors, the proximity effect depends upon the frequency, and in lesser degree upon the shape of the cross sections. Quantitatively, the proximity effect may be expressed by the *proximity factor*, which is the quotient of actual resistance of the conductor by the resistance which it would have if removed to a great distance from the disturbing conductor, both values of resistance being referred to the same frequency.

That is, if

R_0 = the direct current resistance

R_1 = the resistance of the conductor when isolated, frequency f

R_2 = the resistance in the presence of the disturbing conductor
at frequency f

then the proximity factor is $P = \frac{R_2}{R_1}$, and the resistance ratio $\frac{R_2}{R_0}$, in the presence of the

disturbing conductor, is obtained from the resistance ratio $\frac{R_1}{R_0}$ when isolated by the rela-

tion $\frac{R_2}{R_0} = P \frac{R_1}{R_0}$. Resistance ratio may be obtained in any case if the resistance ratio

when isolated is known, together with the value of the proximity factor.

Formulas for the high-frequency resistance ratio have been developed in only a few simple (but important) cases, and even then very complicated formulas result. For practical work tables are necessary for simplifying the calculations. The following tables cover the most important cases.

Formulas have been derived for the high-frequency resistance ratio of single-layer coils wound with round wire. Generally, these differ from one another and from measured values, because, simplifying assumptions are made which are not sufficiently realized in practice. No tables of values for coils such as are met in practical radio work are available. As a rough guide, the high-frequency resistance ratio for a single-layer coil is often from two to five times as great as the resistance ratio of the same wire stretched out straight and carrying current of the given frequency. The experimental work available indicates that this factor due to the coiling of the wire, that is, the total proximity effect of the turns of the coil, is largely dependent upon the frequency and the ratio of wire diameter to pitch of winding, and in lesser degree to the ratio of length to diameter.

(Calculated by Dr. F. W. Grover, Consulting Physicist, Bur. Standards, 1931.)

TABLE 532.—Resistance Ratio "*F*" for Isolated Round WiresResistance ratio *F* of isolated round wire, as a function of the square root of the frequency divided by the direct current resistance per 1000 ft. of conductor.

| $\sqrt{f/R_0}$ | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 |
|----------------|-------|-------|--------|--------|-------|-------|-------|-------|-------|-------|-------|
| <i>F</i> | 1.000 | 1.000 | 1.0005 | 1.0025 | 1.008 | 1.019 | 1.038 | 1.069 | 1.114 | 1.173 | 1.247 |
| $\sqrt{f/R_0}$ | 100 | 120 | 140 | 160 | 180 | 200 | 250 | 300 | 350 | 400 | 500 |
| <i>F</i> | 1.247 | 1.427 | 1.631 | 1.836 | 2.036 | 2.231 | 2.715 | 3.201 | 3.688 | 4.176 | 5.152 |

TABLE 533.—Values of Resistance Ratio for Isolated Tubular Conductors

t, thickness of wall of tube; *d*, outer diameter of tube.

| $\sqrt{\frac{f}{R_0}} \frac{t}{d} =$ | 0.01 | 0.02 | 0.03 | 0.04 | 0.05 | 0.06 | 0.07 | 0.08 | 0.09 | 0.10 |
|--------------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------------|
| 0 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 50 | 1.000 | 1.000 | 1.000 | 1.001 | 1.001 | 1.001 | 1.001 | 1.001 | 1.001 | 1.001 |
| 100 | 1.001 | 1.001 | 1.002 | 1.002 | 1.004 | 1.008 | 1.007 | 1.009 | | 1.014 |
| 150 | 1.001 | 1.003 | 1.006 | 1.011 | 1.017 | 1.024 | 1.033 | 1.044 | 1.056 | 1.070 |
| 200 | 1.002 | 1.008 | 1.019 | 1.034 | 1.053 | 1.076 | 1.104 | 1.134 | 1.167 | 1.204 |
| 250 | 1.005 | 1.020 | 1.046 | 1.081 | 1.125 | 1.176 | 1.233 | 1.296 | 1.365 | 1.440 |
| 300 | 1.011 | 1.042 | 1.095 | 1.163 | 1.25 | 1.34 | 1.44 | 1.55 | 1.65 | 1.75 |
| 350 | 1.020 | 1.076 | 1.167 | 1.285 | 1.42 | 1.56 | 1.70 | 1.83 | 1.97 | 2.09 |
| 400 | 1.032 | 1.127 | 1.27 | 1.44 | 1.66 | 1.81 | 1.99 | 2.13 | 2.28 | 2.42 |
| 450 | 1.051 | 1.198 | 1.41 | 1.63 | 1.87 | 2.08 | 2.28 | 2.44 | 2.60 | 2.74 |
| 500 | 1.079 | 1.30 | 1.57 | 1.86 | 2.14 | 2.34 | 2.56 | 2.73 | 2.88 | 3.03 |
| $\sqrt{\frac{f}{R_0}} \frac{t}{d} =$ | 0.10 | 0.12 | 0.15 | 0.20 | 0.25 | 0.30 | 0.35 | 0.40 | 0.45 | Solid 0.50 |
| 0 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 50 | 1.001 | 1.001 | 1.002 | 1.004 | 1.006 | 1.008 | 1.012 | 1.015 | 1.017 | 1.019 |
| 100 | 1.014 | 1.021 | 1.032 | 1.063 | 1.094 | 1.132 | 1.175 | 1.202 | 1.224 | 1.247 |
| 150 | 1.070 | 1.102 | 1.155 | 1.266 | 1.39 | 1.51 | 1.60 | 1.68 | 1.71 | 1.733 |
| 200 | 1.204 | 1.294 | 1.42 | 1.65 | 1.845 | 1.995 | 2.095 | 2.15 | 2.20 | 2.231 |
| 250 | 1.44 | 1.585 | 1.79 | 2.11 | 2.32 | 2.45 | 2.536 | 2.64 | 2.68 | 2.715 |
| 300 | 1.75 | 1.94 | 2.19 | 2.51 | 2.735 | 2.90 | 3.03 | 3.12 | 3.17 | 3.201 |
| 350 | 2.09 | 2.33 | 2.57 | 2.90 | 3.15 | 3.35 | 3.495 | 3.59 | 3.66 | 3.688 |
| 400 | 2.42 | 2.66 | 2.92 | 3.27 | 3.58 | 3.80 | 3.96 | 4.07 | 4.14 | 4.176 |
| 450 | 2.74 | 3.00 | 3.27 | 3.66 | 4.00 | 4.25 | 4.43 | 4.55 | 4.63 | 4.664 |
| 500 | 3.03 | 3.33 | 3.62 | 4.07 | 4.42 | 4.69 | 4.90 | 5.03 | 5.12 | 5.152 |

TABLE 534.—Coefficients in Formula for Proximity Factor of Equal Parallel Round Wires

The proximity factor of two equal parallel conductors may be calculated by the formula

$$P = 1 + [G \cdot d^2 / s^2] / [F(1 - H d^2 / s^2)]$$

in which the coefficient *F* is to be obtained from Table 532 for the given value of f/R_0 and the coefficients *G* and *H* are to be taken from the table below for the given value of f/R_0 . In the table below the values of *H* apply to currents in the same direction; in the case of currents in opposite directions *H'* is to be used. In the above formula *d* is the diameter of the wires and *s* their axial spacing. The proximity factor for two equal parallel tubular conductors does not differ much from the value for two solid wires with the same axial spacing and a value of f/R_0 one-half the value for two solid wires of the same diameter, except for conductors very close together.

| $\sqrt{f/R_0}$ | <i>G</i> | <i>H</i> | <i>H'</i> | $\sqrt{f/R_0}$ | <i>G</i> | <i>H</i> | <i>H'</i> |
|----------------|----------|----------|-----------|----------------|----------|----------|-----------|
| 0 | 0 | +0.0417 | +0.0417 | 200 | 0.8491 | -0.1904 | 0.5530 |
| 25 | 0.0036 | .0395 | .0443 | 250 | 1.0959 | — .2017 | .5932 |
| 50 | .0519 | + .0109 | .0798 | 300 | 1.340 | — .2093 | .6200 |
| 75 | .1903 | — .0659 | .1838 | 350 | 1.585 | — .2149 | .6389 |
| 100 | .3562 | — .1379 | .3112 | 400 | 1.830 | — .2191 | .6530 |
| 125 | .4914 | — .1685 | .4114 | 450 | 2.073 | — .2224 | .6639 |
| 150 | .6096 | — .1776 | .4787 | 500 | 2.319 | — .2231 | .6722 |
| 175 | .7277 | — .1839 | .5228 | | | | |

TABLE 535.—Ratio of Alternating to Direct Current Resistances for Copper Wires

This table gives the ratio of the resistance of straight copper wires with alternating currents of different frequencies to the value of the resistance with direct currents.

| Diameter of wire in millimeters. | Frequency $f =$ | | | | | |
|----------------------------------|-----------------|--------|-------|--------|---------|-----------|
| | 60 | 100 | 1000 | 10,000 | 100,000 | 1,000,000 |
| 0.05 | — | — | — | — | — | *1.001 |
| 0.1 | — | — | — | — | *1.001 | 1.008 |
| 0.25 | — | — | — | — | 1.003 | 1.247 |
| 0.5 | — | — | — | *1.001 | 1.047 | 2.240 |
| 1.0 | — | — | — | 1.008 | 1.503 | 4.19 |
| 2.0 | — | — | 1.001 | 1.120 | 2.756 | 8.10 |
| 3. | — | — | 1.006 | 1.437 | 4.00 | 12.0 |
| 4. | — | — | 1.021 | 1.842 | 5.24 | 17.4 |
| 5. | — | *1.001 | 1.047 | 2.240 | 6.49 | 19.7 |
| 7.5 | 1.001 | 1.002 | 1.210 | 3.22 | 7.50 | 29.7 |
| 10. | 1.003 | 1.008 | 1.503 | 4.19 | 12.7 | 39.1 |
| 15. | 1.016 | 1.038 | 2.136 | 6.14 | 18.8 | — |
| 20. | 1.044 | 1.120 | 2.756 | 8.10 | 25.2 | — |
| 25. | 1.105 | 1.247 | 3.38 | 10.1 | 28.3 | — |
| 40. | 1.474 | 1.842 | 5.24 | 17.4 | — | — |
| 100. | 3.31 | 4.19 | 13.7 | 39.1 | — | — |

Values between 1.000 and 1.001 are indicated by *1.001.

The values are for wires having an assumed conductivity of 1.60 microhm-cms; for copper wires at room temperatures the values are slightly less than as given in table.

The change of resistance of wire other than copper (iron wires excepted) may be calculated from the above table by taking it as proportional to $d\sqrt{f}/\rho$ where d = diameter, f the frequency and ρ the resistivity.

If a given wire be wound into a solenoid, its resistance, at a given frequency, will be greater than the values in the table, which apply to straight wires only. The resistance in this case is a complicated function of the pitch and radius of the winding, the frequency, and the diameter of the wire, and is found by experiment to be sometimes as much as twice the value for a straight wire.

TABLE 536.—Maximum Diameter of Wires for High-frequency Resistance Ratio of 1.01

| Frequency $\div 10^6 \dots$ | 0.1 | 0.2 | 0.4 | 0.6 | 0.8 | 1.0 | 1.2 | 1.5 | 2.0 | 3.0 |
|-----------------------------|--------------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| Wave-length, meters | 3000 | 1500 | 750 | 500 | 375 | 300 | 250 | 200 | 150 | 100 |
| Material. | Diameter in centimeters. | | | | | | | | | |
| Copper..... | 0.0356 | 0.0251 | 0.0177 | 0.0145 | 0.0125 | 0.0112 | 0.0102 | 0.0092 | 0.0079 | 0.0065 |
| Silver..... | 0.0345 | 0.0244 | 0.0172 | 0.0141 | 0.0122 | 0.0109 | 0.0099 | 0.0089 | 0.0077 | 0.0063 |
| Gold..... | 0.0420 | 0.0297 | 0.0210 | 0.0172 | 0.0149 | 0.0133 | 0.0121 | 0.0108 | 0.0094 | 0.0077 |
| Platinum..... | 0.1120 | 0.0793 | 0.0560 | 0.0457 | 0.0396 | 0.0354 | 0.0323 | 0.0290 | 0.0250 | 0.0205 |
| Mercury..... | 0.264 | 0.187 | 0.132 | 0.1080 | 0.0936 | 0.0836 | 0.0763 | 0.0683 | 0.0591 | 0.0483 |
| Manganin..... | 0.1784 | 0.1261 | 0.0892 | 0.0729 | 0.0631 | 0.0564 | 0.0515 | 0.0461 | 0.0399 | 0.0325 |
| Constantan..... | 0.1892 | 0.1337 | 0.0946 | 0.0772 | 0.0664 | 0.0598 | 0.0540 | 0.0488 | 0.0423 | 0.0345 |
| German silver..... | 0.1942 | 0.1372 | 0.0970 | 0.0792 | 0.0692 | 0.0614 | 0.0560 | 0.0500 | 0.0434 | 0.0354 |
| Graphite..... | 0.765 | 0.541 | 0.383 | 0.312 | 0.271 | 0.242 | 0.221 | 0.197 | 0.171 | 0.140 |
| Carbon..... | 1.60 | 1.13 | 0.801 | 0.654 | 0.566 | 0.506 | 0.462 | 0.414 | 0.358 | 0.292 |
| Iron $\mu = 1000 \dots$ | 0.00263 | 0.00186 | 0.00131 | 0.00108 | 0.00094 | 0.00083 | 0.00076 | 0.00068 | 0.00059 | 0.00048 |
| $\mu = 500 \dots$ | 0.00373 | 0.00264 | 0.00187 | 0.00152 | 0.00132 | 0.00118 | 0.00108 | 0.00096 | 0.00084 | 0.00068 |
| $\mu = 100 \dots$ | 0.00838 | 0.00590 | 0.00418 | 0.00340 | 0.00295 | 0.00264 | 0.00241 | 0.00215 | 0.00186 | 0.00152 |

Bureau of Standards Circular 74, Radio Instruments and Measurements, 1918.

TABLES 537 AND 538

WIRELESS TELEGRAPHY

TABLE 537.—Radiation Resistances for Various Wave-Lengths and Antenna Heights

The radiation theory of Hertz shows that the radiated energy of an oscillator may be represented by $E = \text{constant} (h^2/\lambda^2) I^2$, where h is the length of the oscillator, λ , the wave-length and I the current at its center. For a flat-top antenna $E = 1600 (h^2/\lambda^2) I^2$ watts; $1600 h^2/\lambda^2$ is called the radiation resistance.

(h = height to center of capacity of conducting system.)

| h = Wave- Length λ | 40 Ft. | 60 Ft. | 80 Ft. | 100 Ft. | 120 Ft. | 160 Ft. | 200 Ft. | 300 Ft. | 450 Ft. | 600 Ft. | 1200 Ft. |
|----------------------------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| <i>m</i> | <i>ohm</i> | <i>ohm</i> | <i>ohm</i> | <i>ohm</i> | <i>ohm</i> | <i>ohm</i> | <i>ohm</i> | <i>ohm</i> | <i>ohm</i> | <i>ohm</i> | <i>ohm</i> |
| 200 | 6.0 | 13.4 | 24.0 | 37.0 | 54.0 | 95.0 | | | | | |
| 300 | 2.7 | 6.0 | 10.6 | 16.5 | 23.8 | 42.4 | | | | | |
| 400 | 1.5 | 3.4 | 6.0 | 9.3 | 13.4 | 23.8 | | | | | |
| 600 | 0.66 | 1.5 | 2.7 | 4.1 | 6.0 | 10.6 | 16.4 | 37.4 | 84.0 | 149.0 | |
| 800 | 0.37 | 0.84 | 1.5 | 2.3 | 3.4 | 6.0 | 9.2 | 21.0 | 47.0 | 84.0 | |
| 1000 | 0.24 | 0.54 | 0.95 | 1.5 | 2.1 | 3.8 | 6.0 | 13.5 | 30.0 | 54.0 | 215.0 |
| 1200 | 0.17 | 0.37 | 0.66 | 1.03 | 1.5 | 2.6 | 4.1 | 9.3 | 21.0 | 37.0 | 149.0 |
| 1500 | 0.11 | 0.24 | 0.42 | 0.66 | 0.95 | 1.7 | 2.6 | 6.0 | 13.4 | 24.0 | 95.0 |
| 2000 | | 0.13 | 0.24 | 0.37 | 0.54 | 0.95 | 1.5 | 3.4 | 7.5 | 13.4 | 54.0 |
| 2500 | | | 0.15 | 0.24 | 0.34 | 0.61 | 0.95 | 2.2 | 4.8 | 8.6 | 34.0 |
| 3000 | | | 0.11 | 0.17 | 0.24 | 0.42 | 0.66 | 1.5 | 3.4 | 6.0 | 24.0 |
| 4000 | | | 0.06 | 0.09 | 0.13 | 0.24 | 0.37 | 0.84 | 1.9 | 3.4 | 13.4 |
| 5000 | | | | | | | 0.24 | 0.53 | 1.20 | 2.2 | 8.6 |
| 6000 | | | | | | | 0.16 | 0.37 | 0.84 | 1.5 | 6.0 |
| 7000 | | | | | | | 0.12 | 0.27 | 0.61 | 1.1 | 4.4 |

Austin, Jour. Wash. Acad. of Sci. 1, p. 190, 1911.

TABLE 538.—The Dielectric Properties of Nonconductors

Phillips Thomas, J. Franklin Inst. 176, 283, 1913.

| Results of tests at unit area and unit thickness of dielectric. | | | | |
|---|------------------------|------------------------|------------------------|--------------------|
| At 1000 cycles. | Mica. | Paper. | Celluloid. | Ice. |
| Max. breakdown volts per cm. | 1.06×10^6 | 0.71×10^6 | 1.05×10^6 | $.011 \times 10^6$ |
| Specific induct. capacity | 4.00 | 4.90 | 13.26 | 86.40 |
| Max. absorbable energy, watt-sec/cm ³ | 0.198 | 0.108 | 0.640 | .00040 |
| 90°-angle of lead | 0° 57' | 2° 10' | 3° 40' | 13° 39' |
| Equiv. resistance ohms/cm ³ $\times 10^{11}$ | 3.91 | 9.84 | 48.3 | 1400 |
| Conductivity per cm. cube $\times 10^{-10}$ | 2.56 | 1.02 | 0.207 | .00722 |
| Percent change in cap. per cycle $\times 10^4$ | 2.18 | 14.31 | 30.7 | 70.0 |
| Percent change in resistance per cycle | 0.258 | 0.146 | 0.106 | 0.127 |
| At 15 cycles. | | | | |
| Specific inductive capacity | 4.09 | 5.77 | 18.60 | 429.0 |
| Max. absorbable energy, watt-sec/cm ³ | 0.203 | 0.126 | 0.90 | 0.002 |
| Percent change in capacity per cycle | 0.00 | 0.306 | 1.74 | 1.59 |
| On direct current. | | | | |
| Conductivity per cm ³ | 2.42×10^{-11} | 2.27×10^{-14} | 71.5×10^{-14} | 163.10^{-11} |

TABLE 539 POWER FACTOR AND DIELECTRIC CONSTANT

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(See also Table 540 on page 454.)

From the range of the values given, an approximate figure can be taken for a particular material and its relative position with respect to other materials seen. Data of this kind are much effected by the condition and past treatment of the samples, and by the conditions of the tests.

The power factor and dielectric constant of dry air may be taken as zero and 1.00. Fused quartz has the lowest power factor among the solid insulating materials, and is used for supporting the insulated plates of standard air condensers.

TABLE 539.—Values for Power Factor in Per Cent for Several Electrical Insulating Materials at Radio-Frequencies

| Material | Frequency kc | Measurements reported by— | | | | |
|-------------------------------------|-----------------|---------------------------|-----------|------|------------------------|-------------------------|
| | | 1 | 2 | 3 | 4 | 5 |
| Amber..... | 187.5 | 0.459 | | | | |
| | 300 | .476 | | | | |
| | 600 | .495 | | | | |
| | 1000 | .513 | | | | |
| Glass..... | 30 | | | | 0.35-2.98 ^b | |
| | 600 | 0.040-0.653 ^a | | | | |
| Cobalt glass..... | 500 | | 0.70 | | | |
| Flint glass..... | 500 | | .42 | | | |
| | 890 | | .40 | | | |
| Plate glass..... | 14 | | | 0.97 | | |
| | 100 | | | .77 | | 0.93 |
| | 500 | | .70 | .66 | | |
| | 635 | | | | | .82 |
| | 1000 | | | .62 | | |
| Pyrex glass..... | 14 | | | .88 | | |
| | 30 | | | | 0.56 and 0.26 | |
| | 100 | | | .74 | | .58 |
| | 420 | | | | | .50 |
| | 500 | | .42 | .67 | | |
| Photographic glass..... | 750 | | .68 | | | |
| | 100 | | | | | .95 |
| | 235 | | | | | .86 |
| Hard rubber..... | 1700 | | | | | .77 |
| | 135 | | | | | .68 |
| | 315 | | | | | .70 |
| | 600 | .62 | | | | |
| | 625 | | | | | .70 |
| | 710 | | .88 | | | |
| | 1000 | .68 | | | | |
| | 1085 | | | | | .74 |
| Marble ^e | 1126 | | 1.05 | | | |
| | 80-650 | | | | | 0.35-4.72 |
| Mica..... | 600 | .017 | | | | .007-.93 ^f |
| Laminated phenolic insulation | 190 | | 3.85-7.35 | | | 2.62- 8.0 |
| | 1000 | | 4.20-6.65 | | | 3.85- 5.6 |
| Moulded phenolic insulation | 190 | | | | | 1.64-10.9 |
| | 1000 | | | | | 1.56- 8.4 |
| Wood (oak)..... | 300 | | 3.68 | | | 13.8, 2.94 ^e |
| | 635 | | 3.85 | | | 10.1, 3.24 ^e |
| | 1060 | | 4.20 | | | |
| | 500 | | 3.33 | | | 3.63 |
| (maple)..... | 500 | | 6.48 | | | |
| (birch)..... | 870 | | | | | 3.76 |
| Paraffin..... | 14 | | | .042 | | |
| | 100 | | | .031 | | .017 |
| | 500 | | | .026 | | |
| | 1070 | | | | | .034 |

(1) Schott, Erich, Hochfrequenzverluste von Gläsern und einigen anderen Dielektrics, Jahrb. Drahtlosen Tele. u. Tele., 18, 82-122, August, 1921. (2) Hoch, E. T. Power losses in insulating materials. Bell System Tech. Journ., 1, No. 2, Nov., 1922. (3) MacLeod, H. J. Power losses in dielectrics. Phys. Rev., 21, 53-73, 1923. (4) Decker, William C., Power losses in commercial glasses, Electr. World, 89, 601-603, March 19, 1927. (5) Data from the Bureau of Standards.

^a Range of 27 samples. ^b Range of 9 samples. ^c Range of 10 samples. ^d Range of several samples. ^e After drying 48 hours at 80°C. ^f Range of a number of samples from different localities.

TABLE 540.—Values of Dielectric Constant for Several Electrical Insulating Materials at Radio-Frequencies

| Material | Frequency, kc | Measurements reported by— | | | |
|-------------------------------|------------------|---------------------------|---------|----------------------|-----------------------|
| | | 1 | 2 | 3 | 4 |
| Glass..... | 30 | ... | ... | 5.1-7.9 ^a | ... |
| Crown glass..... | 230 | 6.3 | ... | ... | ... |
| | 800 | 6.2 | ... | ... | ... |
| Flint glass..... | 500 | ... | 7.0 | ... | ... |
| | 890 | ... | 7.0 | ... | ... |
| Plate glass..... | 500 | ... | 6.8 | ... | 7.6 |
| Cobalt glass..... | 500 | ... | 7.3 | ... | ... |
| Pyrex glass..... | 30 | ... | ... | 4.8 | ... |
| | 500 | ... | 4.9 | ... | 5.8 |
| Photographic glass..... | 100 | ... | ... | ... | 7.5 |
| | 1700 | ... | ... | ... | 7.4 |
| Hard rubber..... | 135 | ... | ... | ... | 3.7 |
| | 210 | ... | 3.0 | ... | ... |
| | 1126 | ... | 3.0 | ... | 3.7 |
| Marble..... | 44 | 8.4 | ... | ... | ... |
| | 80-650 | ... | ... | ... | 9.2-11.7 ^c |
| | 1400 | 7.3 | ... | ... | ... |
| Mica..... | 100-1000 | ... | ... | ... | 5.8-8.7 |
| Laminated phenolic insulation | 190 | ... | 5.4-5.8 | ... | 5.0-7.4 |
| | 1000 | ... | 5.1-5.6 | ... | 4.7-7.0 |
| Moulded phenolic insulation | 190 | ... | ... | ... | 4.3-7.6 |
| | 1000 | ... | ... | ... | 4.9-7.0 |
| Wood (oak)..... | 300 | ... | 3.2 | ... | 6.7, 3.1 ^b |
| | 425 | ... | 3.3 | ... | ... |
| | 635 | ... | 3.3 | ... | 6.5, 3.0 ^b |
| | 1060 | ... | 3.3 | ... | ... |
| (maple)..... | 500 | ... | 4.4 | ... | 4.4 |
| (birch)..... | 500 | ... | 5.2 | ... | ... |
| (baywood)..... | 870 | ... | ... | ... | 3.8 |

(1) Bairsto, G. E., Conductivity and dielectric constant of dielectrics for high-frequency oscillations. Proc. Roy. Soc. London, A, 96, 363-382, Jan., 1920. (2) Hoch, E. T., Power losses in insulating materials. Bell System Tech. Journ., 1, No. 2, Nov., 1922. (3) Decker, William C., Power losses in commercial glasses. Electr. World, 89, 601-603, March 19, 1927. (4) Data from the Bureau of Standards.

^a Range of 9 samples of various chemical compositions reported. ^b After drying sample for 48 hours at 86°C. ^c Range of 19 samples of various kinds of marble.

TABLE 541.—Absorption Factors for Radio Propagation

For frequencies up to 1000 kc and transmission over sea water the semiempirical transmission formulas of Austin-Cohen, Austin, Fuller, and Espenschied, Anderson and Bailey take the form

$$F (\mu \text{ volts/meter}) = (377/\lambda)(hI/d) \sqrt{\theta/\sin \theta} \cdot e^{-\frac{\alpha d}{\lambda x}}$$

where the coefficient $377hI/\lambda d$ represents the simple Hertzian radiation field over a perfectly conducting plane surface, the factor $\sqrt{\theta/\sin \theta}$ corrects the formula for the curvature of the earth, and the factor $e^{-\alpha d/\lambda x}$ is the absorption factor, α the damping factor, and x is determined experimentally. d , the distance from the transmitter, and λ , the wave length, both are measured in kilometers. The following tabulation completes the information concerning these formulas. (See next page.)

TABLE 541 (continued).—Absorption Factors for Radio Propagation

| Name of formula | Damping factor | x | Nature of path | Distance km | Frequency kc | Remarks |
|---------------------|----------------|------|----------------|-------------|--------------|---------|
| Austin-Cohen..... | 0.0015 | 0.5 | Sea water | Up to 2000 | 80-1000 | |
| Austin revised..... | .0014 | .6 | Sea water | Up to 12000 | 12-1000 | |
| Fuller..... | .0045 | 1.4 | Sea water | 3900 | 25.4-100 | (a) |
| E, A, and B..... | .005 | 1.25 | Sea water | 5000 | 17-60 | (b) |

(a) Honolulu to San Francisco. (b) Omitted factor $\sqrt{\theta/\sin \theta}$, E, A, and B, Espenschied, Anderson and Bailey.

Bown and Gillet substituting their measured values of F , at 640 kc taken within 150 km of Washington, D. C., in the Austin-Cohen formula get

$\alpha = 0.028$ for dry sandy soil; 0.009 for moist soil; 0.0025 for $\frac{1}{2}$ salt water (Chesapeake Bay).

Austin concludes that for frequencies greater than 60 kc over land, absorption is considerably greater than over sea water. From 60 kc to 20 kc overland absorption decreases and approaches that over sea water. In these results the total field received in the day time is considered. In the following results the ground wave only is considered.

Over land especially at the higher frequencies there are so many variables that no simple complete formula is available for F . We may write $F_{xd} = a$ constant from the Hertzian formula and modify it by a factor A for absorption and quote some results, i.e.

$$F = (377h I/\lambda D)A$$

Smith, Rose, and Barfield calculated from Sommerfeld's theory and approximately checked at some broadcast frequencies the following results.

TABLE 542.—Transmission Path Over Sea Water Whose Conductivity Was Assumed = 1.1×10^{-11} e.m.u.

| Frequency, kc | 50 km | 100 km | 150 km |
|---------------|----------------------|--------|--------|
| 10000..... | Absorption factors 1 | 0.92 | 0.80 |
| 3000..... | 1 | 1 | 1 |

TABLE 543.—Transmission Path Over Land Whose Conductivity Was Assumed = 1.1×10^{-13} e.m.u.

| Frequency, kc | 1.5 km | 4 km | 5 km | Absorption factor at a distance of— | | | | 75 km | 100 km | 150 km |
|---------------|--------|------|------|-------------------------------------|-------|-------|-------|-------|--------|--------|
| | | | | 10 km | 15 km | 25 km | 50 km | | | |
| 300..... | | | | | | | 0.98 | | 0.93 | 0.82 |
| 1000..... | | | | | | 0.56 | .29 | 0.20 | .14 | .08 |
| 3000..... | | | 0.40 | 0.20 | 0.10 | | | | | |
| 10000..... | 0.10 | 0.03 | | | | | | | | |

Rolf calculates from Sommerfeld's theory the following:

TABLE 544.—Transmission Path Over Land Whose Inductivity $\epsilon = 15$ e.s.u. and Whose Conductivity $\delta = 10^{-13}$ e.m.u. (Good Conducting Ground)

| Frequency, kc | 2 km | Absorption factor at a distance of— | | | 100 km |
|---------------|------|-------------------------------------|-------|-------|--------|
| | | 5 km | 10 km | 40 km | |
| 300..... | | | | | 0.90 |
| 1000..... | | | 0.80 | | .25 |
| 3000..... | | | .30 | 0.04 | |
| 10000..... | 0.16 | 0.05 | .02 | | |

TABLE 545.—Transmission Path Over Ground With Inductivity $\epsilon = 15$ e.s.u. and Conductivity $\sigma = 10^{-15}$ e.m.u. (Bad Conducting Ground)

| Frequency, kc | 10 km | Absorption factor at a distance of— | | 100 km |
|---------------|-------|-------------------------------------|-------|--------|
| | | 20 km | 50 km | |
| 75..... | | | | 0.90 |
| 150..... | | | | .70 |
| 300..... | | | 0.50 | .10 |
| 500..... | 0.90 | 0.40 | .10 | |
| 1000..... | .40 | | | |

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KILOCYCLE-METER CONVERSION TABLE

Velocity of propagation, 299820 km/sec.

The number of kilocycles (kc) is the number of thousands of times the rapidly alternating current in the antenna repeats its direction of flow per sec. The smaller the wave length, the larger the frequency. To obtain approximate kc divide 300000 by the number of m (see next table). For accurate conversion the constant is 299820. The wave length is equal to the velocity divided by the frequency. The velocity of radio waves in space, according to the best available data, is 299820 km/sec. This table and the next are entirely reversible, i.e., 50 kc is 5996 m, and also 50 m is 5996 kc. The range of the table is easily extended by shifting the decimal point in opposite directions for each pair of values—e.g., 2230 kc or m is equivalent to 134.4 m or kc; whence 223 kc or m is equivalent to 1344 m or kc. (Taken from Bur. Standards, Misc. Publ., 67, 1925.)

| kc or m | m or kc | kc or m | m or kc | kc or m | m or kc | kc or m | m or kc | kc or m | m or kc |
|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| 1,010 | 296.9 | 1,410 | 212.6 | 1,810 | 165.6 | 2,210 | 135.7 | 2,610 | 114.9 |
| 1,020 | 293.9 | 1,420 | 211.1 | 1,820 | 164.7 | 2,220 | 135.1 | 2,620 | 114.4 |
| 1,030 | 291.1 | 1,430 | 209.7 | 1,830 | 163.8 | 2,230 | 134.4 | 2,630 | 114.0 |
| 1,040 | 288.3 | 1,440 | 208.2 | 1,840 | 162.9 | 2,240 | 133.8 | 2,640 | 113.6 |
| 1,050 | 285.5 | 1,450 | 206.8 | 1,850 | 162.1 | 2,250 | 133.3 | 2,650 | 113.1 |
| 1,060 | 282.8 | 1,460 | 205.4 | 1,860 | 161.2 | 2,260 | 132.7 | 2,660 | 112.7 |
| 1,070 | 280.2 | 1,470 | 204.0 | 1,870 | 160.3 | 2,270 | 132.1 | 2,670 | 112.3 |
| 1,080 | 277.6 | 1,480 | 202.6 | 1,880 | 159.5 | 2,280 | 131.5 | 2,680 | 111.9 |
| 1,090 | 275.1 | 1,490 | 201.2 | 1,890 | 158.6 | 2,290 | 130.9 | 2,690 | 111.5 |
| 1,100 | 272.6 | 1,500 | 199.9 | 1,900 | 157.8 | 2,300 | 130.4 | 2,700 | 111.0 |
| 1,110 | 270.1 | 1,510 | 198.6 | 1,910 | 157.0 | 2,310 | 129.8 | 2,710 | 110.6 |
| 1,120 | 267.7 | 1,520 | 197.2 | 1,920 | 156.2 | 2,320 | 129.2 | 2,720 | 110.2 |
| 1,130 | 265.3 | 1,530 | 196.0 | 1,930 | 155.3 | 2,330 | 128.7 | 2,730 | 109.8 |
| 1,140 | 263.0 | 1,540 | 194.7 | 1,940 | 154.5 | 2,340 | 128.1 | 2,740 | 109.4 |
| 1,150 | 260.7 | 1,550 | 193.4 | 1,950 | 153.8 | 2,350 | 127.6 | 2,750 | 109.0 |
| 1,160 | 258.5 | 1,560 | 192.2 | 1,960 | 153.0 | 2,360 | 127.0 | 2,760 | 108.6 |
| 1,170 | 256.3 | 1,570 | 191.0 | 1,970 | 152.2 | 2,370 | 126.5 | 2,770 | 108.2 |
| 1,180 | 254.1 | 1,580 | 189.8 | 1,980 | 151.4 | 2,380 | 126.0 | 2,780 | 107.8 |
| 1,190 | 252.0 | 1,590 | 188.6 | 1,990 | 150.7 | 2,390 | 125.4 | 2,790 | 107.5 |
| 1,200 | 249.9 | 1,600 | 187.4 | 2,000 | 149.9 | 2,400 | 124.9 | 2,800 | 107.1 |
| 1,210 | 247.8 | 1,610 | 186.2 | 2,010 | 149.2 | 2,410 | 124.4 | 2,810 | 106.7 |
| 1,220 | 245.8 | 1,620 | 185.1 | 2,020 | 148.4 | 2,420 | 123.9 | 2,820 | 106.3 |
| 1,230 | 243.8 | 1,630 | 183.9 | 2,030 | 147.7 | 2,430 | 123.4 | 2,830 | 105.9 |
| 1,240 | 241.8 | 1,640 | 182.8 | 2,040 | 147.0 | 2,440 | 122.9 | 2,840 | 105.6 |
| 1,250 | 239.9 | 1,650 | 181.7 | 2,050 | 146.3 | 2,450 | 122.4 | 2,850 | 105.2 |
| 1,260 | 238.0 | 1,660 | 180.6 | 2,060 | 145.5 | 2,460 | 121.9 | 2,860 | 104.8 |
| 1,270 | 236.1 | 1,670 | 179.5 | 2,070 | 144.8 | 2,470 | 121.4 | 2,870 | 104.5 |
| 1,280 | 234.2 | 1,680 | 178.5 | 2,080 | 144.1 | 2,480 | 120.9 | 2,880 | 104.1 |
| 1,290 | 232.4 | 1,690 | 177.4 | 2,090 | 143.5 | 2,490 | 120.4 | 2,890 | 103.7 |
| 1,300 | 230.6 | 1,700 | 176.4 | 2,100 | 142.8 | 2,500 | 119.9 | 2,900 | 103.4 |
| 1,310 | 228.9 | 1,710 | 175.3 | 2,110 | 142.1 | 2,510 | 119.5 | 2,910 | 103.0 |
| 1,320 | 227.1 | 1,720 | 174.3 | 2,120 | 141.4 | 2,520 | 119.0 | 2,920 | 102.7 |
| 1,330 | 225.4 | 1,730 | 173.3 | 2,130 | 140.8 | 2,530 | 118.5 | 2,930 | 102.3 |
| 1,340 | 223.7 | 1,740 | 172.3 | 2,140 | 140.1 | 2,540 | 118.0 | 2,940 | 102.0 |
| 1,350 | 222.1 | 1,750 | 171.3 | 2,150 | 139.5 | 2,550 | 117.6 | 2,950 | 101.6 |
| 1,360 | 220.4 | 1,760 | 170.4 | 2,160 | 138.8 | 2,560 | 117.1 | 2,960 | 101.3 |
| 1,370 | 218.8 | 1,770 | 169.4 | 2,170 | 138.1 | 2,570 | 116.7 | 2,970 | 100.9 |
| 1,380 | 217.3 | 1,780 | 168.4 | 2,180 | 137.5 | 2,580 | 116.2 | 2,980 | 100.6 |
| 1,390 | 215.7 | 1,790 | 167.5 | 2,190 | 136.9 | 2,590 | 115.8 | 2,990 | 100.3 |
| 1,400 | 214.2 | 1,800 | 166.6 | 2,200 | 136.3 | 2,600 | 115.3 | 3,000 | 99.94 |

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KILOCYCLE-METER CONVERSION TABLE

Velocity of propagation, 299820 km/sec.

| kc or m | m or kc | kc or m | m or kc | kc or m | m or kc | kc or m | m or kc | kc or m | m or kc |
|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| 3,010 | 99.61 | 3,510 | 85.42 | 4,010 | 74.77 | 4,510 | 66.48 | 5,010 | 59.84 |
| 3,020 | 99.28 | 3,520 | 85.18 | 4,020 | 74.58 | 4,520 | 66.33 | 5,020 | 59.73 |
| 3,030 | 98.95 | 3,530 | 84.94 | 4,030 | 74.40 | 4,530 | 66.19 | 5,030 | 59.61 |
| 3,040 | 98.62 | 3,540 | 84.70 | 4,040 | 74.21 | 4,540 | 66.04 | 5,040 | 59.49 |
| 3,050 | 98.30 | 3,550 | 84.46 | 4,050 | 74.03 | 4,550 | 65.89 | 5,050 | 59.37 |
| 3,060 | 97.98 | 3,560 | 84.22 | 4,060 | 73.85 | 4,560 | 65.75 | 5,060 | 59.25 |
| 3,070 | 97.66 | 3,570 | 83.98 | 4,070 | 73.67 | 4,570 | 65.61 | 5,070 | 59.13 |
| 3,080 | 97.34 | 3,580 | 83.75 | 4,080 | 73.49 | 4,580 | 65.46 | 5,080 | 59.02 |
| 3,090 | 97.03 | 3,590 | 83.52 | 4,090 | 73.31 | 4,590 | 65.32 | 5,090 | 58.90 |
| 3,100 | 96.72 | 3,600 | 83.28 | 4,100 | 73.13 | 4,600 | 65.18 | 5,100 | 58.79 |
| | | | | | | | | | |
| 3,010 | 96.41 | 3,610 | 83.05 | 4,110 | 72.95 | 4,610 | 65.04 | 5,110 | 58.67 |
| 3,120 | 96.10 | 3,620 | 82.82 | 4,120 | 72.77 | 4,620 | 64.90 | 5,120 | 58.56 |
| 3,130 | 95.79 | 3,630 | 82.60 | 4,130 | 72.60 | 4,630 | 64.76 | 5,130 | 58.44 |
| 3,140 | 95.48 | 3,640 | 82.37 | 4,140 | 72.42 | 4,640 | 64.62 | 5,140 | 58.33 |
| 3,150 | 95.18 | 3,650 | 82.14 | 4,150 | 72.25 | 4,650 | 64.48 | 5,150 | 58.22 |
| 3,160 | 94.88 | 3,660 | 81.92 | 4,160 | 72.07 | 4,660 | 64.34 | 5,160 | 58.10 |
| 3,170 | 94.58 | 3,670 | 81.70 | 4,170 | 71.90 | 4,670 | 64.20 | 5,170 | 57.99 |
| 3,180 | 94.28 | 3,680 | 81.47 | 4,180 | 71.73 | 4,680 | 64.06 | 5,180 | 57.88 |
| 3,190 | 93.99 | 3,690 | 81.25 | 4,190 | 71.56 | 4,690 | 63.93 | 5,190 | 57.77 |
| 3,200 | 93.69 | 3,700 | 81.03 | 4,200 | 71.39 | 4,700 | 63.79 | 5,200 | 57.66 |
| | | | | | | | | | |
| 3,210 | 93.40 | 3,710 | 80.81 | 4,210 | 71.22 | 4,710 | 63.66 | 5,210 | 57.55 |
| 3,220 | 93.11 | 3,720 | 80.60 | 4,220 | 71.05 | 4,720 | 63.52 | 5,220 | 57.44 |
| 3,230 | 92.82 | 3,730 | 80.38 | 4,230 | 70.88 | 4,730 | 63.39 | 5,230 | 57.33 |
| 3,240 | 92.54 | 3,740 | 80.17 | 4,240 | 70.71 | 4,740 | 63.25 | 5,240 | 57.22 |
| 3,250 | 92.25 | 3,750 | 79.95 | 4,250 | 70.55 | 4,750 | 63.12 | 5,250 | 57.11 |
| 3,260 | 91.97 | 3,760 | 79.74 | 4,260 | 70.38 | 4,760 | 62.99 | 5,260 | 57.00 |
| 3,270 | 91.69 | 3,770 | 79.53 | 4,270 | 70.22 | 4,770 | 62.86 | 5,270 | 56.89 |
| 3,280 | 91.41 | 3,780 | 79.32 | 4,280 | 70.05 | 4,780 | 62.72 | 5,280 | 56.78 |
| 3,290 | 91.13 | 3,790 | 79.11 | 4,290 | 69.89 | 4,790 | 62.59 | 5,290 | 56.68 |
| 3,300 | 90.86 | 3,800 | 78.90 | 4,300 | 69.73 | 4,800 | 62.46 | 5,300 | 56.57 |
| | | | | | | | | | |
| 3,310 | 90.58 | 3,810 | 78.69 | 4,310 | 69.56 | 4,810 | 62.33 | 5,310 | 56.46 |
| 3,320 | 90.31 | 3,820 | 78.49 | 4,320 | 69.40 | 4,820 | 62.20 | 5,320 | 56.36 |
| 3,330 | 90.04 | 3,830 | 78.28 | 4,330 | 69.24 | 4,830 | 62.07 | 5,330 | 56.25 |
| 3,340 | 89.77 | 3,840 | 78.08 | 4,340 | 69.08 | 4,840 | 61.95 | 5,340 | 56.15 |
| 3,350 | 89.50 | 3,850 | 77.88 | 4,350 | 68.92 | 4,850 | 61.82 | 5,350 | 56.04 |
| 3,360 | 89.23 | 3,860 | 77.67 | 4,360 | 68.77 | 4,860 | 61.69 | 5,360 | 55.94 |
| 3,370 | 88.97 | 3,870 | 77.47 | 4,370 | 68.61 | 4,870 | 61.56 | 5,370 | 55.83 |
| 3,380 | 88.70 | 3,880 | 77.27 | 4,380 | 68.45 | 4,880 | 61.44 | 5,380 | 55.73 |
| 3,390 | 88.44 | 3,890 | 77.07 | 4,390 | 68.30 | 4,890 | 61.31 | 5,390 | 55.63 |
| 3,400 | 88.18 | 3,900 | 76.88 | 4,400 | 68.14 | 4,900 | 61.19 | 5,400 | 55.52 |
| | | | | | | | | | |
| 3,410 | 87.92 | 3,910 | 76.68 | 4,410 | 67.99 | 4,910 | 61.06 | 5,410 | 55.42 |
| 3,420 | 87.67 | 3,920 | 76.48 | 4,420 | 67.83 | 4,920 | 60.94 | 5,420 | 55.32 |
| 3,430 | 87.41 | 3,930 | 76.29 | 4,430 | 67.68 | 4,930 | 60.82 | 5,430 | 55.22 |
| 3,440 | 87.16 | 3,940 | 76.10 | 4,440 | 67.53 | 4,940 | 60.69 | 5,440 | 55.11 |
| 3,450 | 86.90 | 3,950 | 75.90 | 4,450 | 67.38 | 4,950 | 60.57 | 5,450 | 55.01 |
| 3,460 | 86.65 | 3,960 | 75.71 | 4,460 | 67.22 | 4,960 | 60.45 | 5,460 | 54.91 |
| 3,470 | 86.40 | 3,970 | 75.52 | 4,470 | 67.07 | 4,970 | 60.33 | 5,470 | 54.81 |
| 3,480 | 86.16 | 3,980 | 75.33 | 4,480 | 66.92 | 4,980 | 60.20 | 5,480 | 54.71 |
| 3,490 | 85.91 | 3,990 | 75.14 | 4,490 | 66.78 | 4,990 | 60.08 | 5,490 | 54.61 |
| 3,500 | 85.66 | 4,000 | 74.96 | 4,500 | 66.63 | 5,000 | 59.96 | 5,500 | 54.51 |

WIRELESS TELEGRAPHY

KILOCYCLE-METER CONVERSION TABLE

Velocity of propagation, 299820 km/sec.

| kc or m | m or kc | kc or m | m or kc | kc or m | m or kc | kc or m | m or kc | kc or m | m or kc |
|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| 5,510 | 54.41 | 6,010 | 49.89 | 6,510 | 46.06 | 7,010 | 42.77 | 7,510 | 39.92 |
| 5,520 | 54.32 | 6,020 | 49.80 | 6,520 | 45.98 | 7,020 | 42.71 | 7,520 | 39.87 |
| 5,530 | 54.22 | 6,030 | 49.72 | 6,530 | 45.91 | 7,030 | 42.65 | 7,530 | 39.82 |
| 5,540 | 54.12 | 6,040 | 49.64 | 6,540 | 45.84 | 7,040 | 42.59 | 7,540 | 39.76 |
| 5,550 | 54.02 | 6,050 | 49.56 | 6,550 | 45.77 | 7,050 | 42.53 | 7,550 | 39.71 |
| 5,560 | 53.92 | 6,060 | 49.48 | 6,560 | 45.70 | 7,060 | 42.47 | 7,560 | 39.66 |
| 5,570 | 53.83 | 6,070 | 49.39 | 6,570 | 45.63 | 7,070 | 42.41 | 7,570 | 39.61 |
| 5,580 | 53.73 | 6,080 | 49.31 | 6,580 | 45.57 | 7,080 | 42.35 | 7,580 | 39.55 |
| 5,590 | 53.64 | 6,090 | 49.23 | 6,590 | 45.50 | 7,090 | 42.29 | 7,590 | 39.50 |
| 5,600 | 53.54 | 6,100 | 49.15 | 6,600 | 45.43 | 7,100 | 42.23 | 7,600 | 39.45 |
| 5,610 | 53.44 | 6,110 | 49.07 | 6,610 | 45.36 | 7,110 | 42.17 | 7,610 | 39.40 |
| 5,620 | 53.35 | 6,120 | 48.99 | 6,620 | 45.29 | 7,120 | 42.11 | 7,620 | 39.35 |
| 5,630 | 53.25 | 6,130 | 48.91 | 6,630 | 45.22 | 7,130 | 42.05 | 7,630 | 39.29 |
| 5,640 | 53.16 | 6,140 | 48.83 | 6,640 | 45.15 | 7,140 | 41.99 | 7,640 | 39.24 |
| 5,650 | 53.07 | 6,150 | 48.75 | 6,650 | 45.09 | 7,150 | 41.93 | 7,650 | 39.19 |
| 5,660 | 52.97 | 6,160 | 48.67 | 6,660 | 45.02 | 7,160 | 41.87 | 7,660 | 39.14 |
| 5,670 | 52.88 | 6,170 | 48.59 | 6,670 | 44.95 | 7,170 | 41.82 | 7,670 | 39.09 |
| 5,680 | 52.79 | 6,180 | 48.51 | 6,680 | 44.88 | 7,180 | 41.76 | 7,680 | 39.04 |
| 5,690 | 52.69 | 6,190 | 48.44 | 6,690 | 44.82 | 7,190 | 41.70 | 7,690 | 38.99 |
| 5,700 | 52.60 | 6,200 | 48.36 | 6,700 | 44.75 | 7,200 | 41.64 | 7,700 | 38.94 |
| 5,710 | 52.51 | 6,210 | 48.28 | 6,710 | 44.68 | 7,210 | 41.58 | 7,710 | 38.89 |
| 5,720 | 52.42 | 6,220 | 48.20 | 6,720 | 44.62 | 7,220 | 41.53 | 7,720 | 38.84 |
| 5,730 | 52.32 | 6,230 | 48.13 | 6,730 | 44.55 | 7,230 | 41.47 | 7,730 | 38.79 |
| 5,740 | 52.23 | 6,240 | 48.05 | 6,740 | 44.48 | 7,240 | 41.41 | 7,740 | 38.74 |
| 5,750 | 52.14 | 6,250 | 47.97 | 6,750 | 44.42 | 7,250 | 41.35 | 7,750 | 38.69 |
| 5,760 | 52.05 | 6,260 | 47.89 | 6,760 | 44.35 | 7,260 | 41.30 | 7,760 | 38.64 |
| 5,770 | 51.96 | 6,270 | 47.82 | 6,770 | 44.29 | 7,270 | 41.24 | 7,770 | 38.59 |
| 5,780 | 51.87 | 6,280 | 47.74 | 6,780 | 44.22 | 7,280 | 41.18 | 7,780 | 38.54 |
| 5,790 | 51.78 | 6,290 | 47.67 | 6,790 | 44.16 | 7,290 | 41.13 | 7,790 | 38.49 |
| 5,800 | 51.69 | 6,300 | 47.59 | 6,800 | 44.09 | 7,300 | 41.07 | 7,800 | 38.44 |
| 5,810 | 51.60 | 6,310 | 47.52 | 6,810 | 44.03 | 7,310 | 41.02 | 7,810 | 38.39 |
| 5,820 | 51.52 | 6,320 | 47.44 | 6,820 | 43.96 | 7,320 | 40.96 | 7,820 | 38.34 |
| 5,830 | 51.43 | 6,330 | 47.36 | 6,830 | 43.90 | 7,330 | 40.90 | 7,830 | 38.29 |
| 5,840 | 51.34 | 6,340 | 47.29 | 6,840 | 43.83 | 7,340 | 40.85 | 7,840 | 38.24 |
| 5,850 | 51.25 | 6,350 | 47.22 | 6,850 | 43.77 | 7,350 | 40.79 | 7,850 | 38.19 |
| 5,860 | 51.16 | 6,360 | 47.14 | 6,860 | 43.71 | 7,360 | 40.74 | 7,860 | 38.14 |
| 5,870 | 51.08 | 6,370 | 47.07 | 6,870 | 43.64 | 7,370 | 40.68 | 7,870 | 38.10 |
| 5,880 | 50.99 | 6,380 | 46.99 | 6,880 | 43.58 | 7,380 | 40.63 | 7,880 | 38.05 |
| 5,890 | 50.90 | 6,390 | 46.92 | 6,890 | 43.52 | 7,390 | 40.57 | 7,890 | 38.00 |
| 5,900 | 50.82 | 6,400 | 46.85 | 6,900 | 43.45 | 7,400 | 40.52 | 7,900 | 37.95 |
| 5,910 | 50.73 | 6,410 | 46.77 | 6,910 | 43.39 | 7,410 | 40.46 | 7,910 | 37.90 |
| 5,920 | 50.65 | 6,420 | 46.70 | 6,920 | 43.33 | 7,420 | 40.41 | 7,920 | 37.86 |
| 5,930 | 50.56 | 6,430 | 46.63 | 6,930 | 43.26 | 7,430 | 40.35 | 7,930 | 37.81 |
| 5,940 | 50.47 | 6,440 | 46.56 | 6,940 | 43.20 | 7,440 | 40.30 | 7,940 | 37.76 |
| 5,950 | 50.39 | 6,450 | 46.48 | 6,950 | 43.14 | 7,450 | 40.24 | 7,950 | 37.71 |
| 5,960 | 50.31 | 6,460 | 46.41 | 6,960 | 43.08 | 7,460 | 40.19 | 7,960 | 37.67 |
| 5,970 | 50.22 | 6,470 | 46.34 | 6,970 | 43.02 | 7,470 | 40.14 | 7,970 | 37.62 |
| 5,980 | 50.14 | 6,480 | 46.27 | 6,980 | 42.95 | 7,480 | 40.08 | 7,980 | 37.57 |
| 5,990 | 50.05 | 6,490 | 46.20 | 6,990 | 42.89 | 7,490 | 40.03 | 7,990 | 37.52 |
| 6,000 | 49.97 | 6,500 | 46.13 | 7,000 | 42.83 | 7,500 | 39.98 | 8,000 | 37.48 |

WIRELESS TELEGRAPHY

KILOCYCLE-METER CONVERSION TABLE

Velocity of propagation, 299820 km/sec.

| kc or m | m or kc | kc or m | m or kc | kc or m | m or kc | kc or m | m or kc | kc or m | m or kc |
|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| 8,010 | 37.43 | 8,410 | 35.65 | 8,810 | 34.03 | 9,210 | 32.55 | 9,610 | 31.20 |
| 8,020 | 37.38 | 8,420 | 35.61 | 8,820 | 33.99 | 9,220 | 32.52 | 9,620 | 31.17 |
| 8,030 | 37.34 | 8,430 | 35.57 | 8,830 | 33.95 | 9,230 | 32.48 | 9,630 | 31.13 |
| 8,040 | 37.29 | 8,440 | 35.52 | 8,840 | 33.92 | 9,240 | 32.45 | 9,640 | 31.10 |
| 8,050 | 37.24 | 8,450 | 35.48 | 8,850 | 33.88 | 9,250 | 32.41 | 9,650 | 31.07 |
| 8,060 | 37.20 | 8,460 | 35.44 | 8,860 | 33.84 | 9,260 | 32.38 | 9,660 | 31.04 |
| 8,070 | 37.15 | 8,470 | 35.40 | 8,870 | 33.80 | 9,270 | 32.34 | 9,670 | 31.01 |
| 8,080 | 37.11 | 8,480 | 35.36 | 8,880 | 33.76 | 9,280 | 32.31 | 9,680 | 30.97 |
| 8,090 | 37.06 | 8,490 | 35.31 | 8,890 | 33.73 | 9,290 | 32.27 | 9,690 | 30.94 |
| 8,100 | 37.01 | 8,500 | 35.27 | 8,900 | 33.69 | 9,300 | 32.24 | 9,700 | 30.91 |
| | | | | | | | | | |
| 8,110 | 36.97 | 8,510 | 35.23 | 8,910 | 33.65 | 9,310 | 32.20 | 9,710 | 30.88 |
| 8,120 | 36.92 | 8,520 | 35.19 | 8,920 | 33.61 | 9,320 | 32.17 | 9,720 | 30.85 |
| 8,130 | 36.88 | 8,530 | 35.15 | 8,930 | 33.57 | 9,330 | 32.14 | 9,730 | 30.81 |
| 8,140 | 36.83 | 8,540 | 35.11 | 8,940 | 33.54 | 9,340 | 32.10 | 9,740 | 30.78 |
| 8,150 | 36.79 | 8,550 | 35.07 | 8,950 | 33.50 | 9,350 | 32.07 | 9,750 | 30.75 |
| 8,160 | 36.74 | 8,560 | 35.03 | 8,960 | 33.46 | 9,360 | 32.03 | 9,760 | 30.72 |
| 8,170 | 36.70 | 8,570 | 34.98 | 8,970 | 33.42 | 9,370 | 32.00 | 9,770 | 30.69 |
| 8,180 | 36.65 | 8,580 | 34.94 | 8,980 | 33.39 | 9,380 | 31.96 | 9,780 | 30.66 |
| 8,190 | 36.61 | 8,590 | 34.90 | 8,990 | 33.35 | 9,390 | 31.93 | 9,790 | 30.63 |
| 8,200 | 36.56 | 8,600 | 34.86 | 9,000 | 33.31 | 9,400 | 31.90 | 9,800 | 30.59 |
| | | | | | | | | | |
| 8,210 | 36.52 | 8,610 | 34.82 | 9,010 | 33.28 | 9,410 | 31.86 | 9,810 | 30.56 |
| 8,220 | 36.47 | 8,620 | 34.78 | 9,020 | 33.24 | 9,420 | 31.83 | 9,820 | 30.53 |
| 8,230 | 36.43 | 8,630 | 34.74 | 9,030 | 33.20 | 9,430 | 31.79 | 9,830 | 30.50 |
| 8,240 | 36.39 | 8,640 | 34.70 | 9,040 | 33.17 | 9,440 | 31.76 | 9,840 | 30.47 |
| 8,250 | 36.34 | 8,650 | 34.66 | 9,050 | 33.13 | 9,450 | 31.73 | 9,850 | 30.44 |
| 8,260 | 36.30 | 8,660 | 34.62 | 9,060 | 33.09 | 9,460 | 31.69 | 9,860 | 30.41 |
| 8,270 | 36.25 | 8,670 | 34.58 | 9,070 | 33.06 | 9,470 | 31.66 | 9,870 | 30.38 |
| 8,280 | 36.21 | 8,680 | 34.54 | 9,080 | 33.02 | 9,480 | 31.63 | 9,880 | 30.35 |
| 8,290 | 36.17 | 8,690 | 34.50 | 9,090 | 32.98 | 9,490 | 31.59 | 9,890 | 30.32 |
| 8,300 | 36.12 | 8,700 | 34.46 | 9,100 | 32.95 | 9,500 | 31.56 | 9,900 | 30.28 |
| | | | | | | | | | |
| 8,310 | 36.08 | 8,710 | 34.42 | 9,110 | 32.91 | 9,510 | 31.53 | 9,910 | 30.25 |
| 8,320 | 36.04 | 8,720 | 34.38 | 9,120 | 32.88 | 9,520 | 31.49 | 9,920 | 30.22 |
| 8,330 | 35.99 | 8,730 | 34.34 | 9,130 | 32.84 | 9,530 | 31.46 | 9,930 | 30.19 |
| 8,340 | 35.95 | 8,740 | 34.30 | 9,140 | 32.80 | 9,540 | 31.43 | 9,940 | 30.16 |
| 8,350 | 35.91 | 8,750 | 34.27 | 9,150 | 32.77 | 9,550 | 31.39 | 9,950 | 30.13 |
| 8,360 | 35.86 | 8,760 | 34.23 | 9,160 | 32.73 | 9,560 | 31.36 | 9,960 | 30.10 |
| 8,370 | 35.82 | 8,770 | 34.19 | 9,170 | 32.70 | 9,570 | 31.33 | 9,970 | 30.07 |
| 8,380 | 35.78 | 8,780 | 34.15 | 9,180 | 32.66 | 9,580 | 31.30 | 9,980 | 30.04 |
| 8,390 | 35.74 | 8,790 | 34.11 | 9,190 | 32.62 | 9,590 | 31.26 | 9,990 | 30.01 |
| 8,400 | 35.69 | 8,800 | 34.07 | 9,200 | 32.59 | 9,600 | 31.23 | 10,000 | 29.98 |

WIRELESS TELEGRAPHY

Wave-Length in Meters, Frequency in periods per second, and Oscillation Constant LC in Microhenries and Microfarads

The relation between the free wave-length in meters, the frequency in cycles per second, and the capacity-inductance product in microfarads and microhenries are given for circuits between 1000 and 10,000 meters. For values between 100 and 1000 meters, multiply the columns for n by 10 and move the decimal point of the corresponding LC column two places to the left (dividing by 100); for values between 10,000 and 100,000, divide the n column by 10 and multiply the LC column by 100. The relation between wave-length and capacity-inductance may be relied upon throughout the table to within one part in 200.

Example 1: What is the natural wave-length of a circuit containing a capacity of 0.001 microfarad, and an inductance of 454 microhenries? The product of the inductance and capacity is $454 \times 0.001 = 0.454$. Find 0.454 under LC; opposite under meters is 1270 meters, the natural wave-length of the circuit.

Example 2: What capacity must be associated with an inductance of 880 microhenries in order to tune the circuit to 3500 meters? Find opposite 3500 meters the LC value 3.45; divide this by 880, and the quotient, 0.00397, is the desired capacity in microfarads.

Example 3: A condenser has the capacity of 0.004 microfarad. What inductance must be placed in series with this condenser in order that the circuit shall have a wave-length of 600 meters? From the table, the LC value corresponding to 600 meters is 0.101. Divide this by 0.004, the capacity of the condenser, and the desired inductance is 25.2 microhenries.

| Meters. | n | LC | Meters. | n | LC | Meters. | n | LC |
|---------|---------|-------|---------|---------|-------|---------|---------|-------|
| 1000 | 300,000 | 0.281 | 1300 | 230,800 | 0.476 | 1600 | 187,500 | 0.721 |
| 1010 | 297,000 | 0.287 | 1310 | 229,000 | 0.483 | 1610 | 186,300 | 0.730 |
| 1020 | 294,100 | 0.293 | 1320 | 227,300 | 0.490 | 1620 | 185,200 | 0.739 |
| 1030 | 291,300 | 0.299 | 1330 | 225,600 | 0.498 | 1630 | 184,100 | 0.748 |
| 1040 | 288,400 | 0.305 | 1340 | 223,900 | 0.505 | 1640 | 182,900 | 0.757 |
| 1050 | 285,700 | 0.310 | 1350 | 222,200 | 0.513 | 1650 | 181,800 | 0.766 |
| 1060 | 283,600 | 0.316 | 1360 | 220,600 | 0.521 | 1660 | 180,700 | 0.776 |
| 1070 | 280,400 | 0.322 | 1370 | 218,900 | 0.529 | 1670 | 179,600 | 0.785 |
| 1080 | 277,800 | 0.328 | 1380 | 217,400 | 0.536 | 1680 | 178,600 | 0.794 |
| 1090 | 275,200 | 0.335 | 1390 | 215,800 | 0.544 | 1690 | 177,500 | 0.804 |
| | | | | | | | | |
| 1100 | 272,700 | 0.341 | 1400 | 214,300 | 0.552 | 1700 | 176,500 | 0.813 |
| 1110 | 270,300 | 0.347 | 1410 | 212,800 | 0.559 | 1710 | 175,400 | 0.823 |
| 1120 | 267,900 | 0.353 | 1420 | 211,300 | 0.567 | 1720 | 174,400 | 0.833 |
| 1130 | 265,500 | 0.359 | 1430 | 209,800 | 0.576 | 1730 | 173,400 | 0.842 |
| 1140 | 263,100 | 0.366 | 1440 | 208,300 | 0.584 | 1740 | 172,400 | 0.852 |
| 1150 | 260,900 | 0.372 | 1450 | 206,900 | 0.592 | 1750 | 171,400 | 0.862 |
| 1160 | 258,600 | 0.379 | 1460 | 205,500 | 0.600 | 1760 | 170,500 | 0.872 |
| 1170 | 256,400 | 0.385 | 1470 | 204,100 | 0.608 | 1770 | 169,400 | 0.882 |
| 1180 | 254,200 | 0.392 | 1480 | 202,700 | 0.617 | 1780 | 168,500 | 0.892 |
| 1190 | 252,100 | 0.399 | 1490 | 201,300 | 0.625 | 1790 | 167,600 | 0.902 |
| | | | | | | | | |
| 1200 | 250,000 | 0.405 | 1500 | 200,000 | 0.633 | 1800 | 166,700 | 0.912 |
| 1210 | 247,900 | 0.412 | 1510 | 198,700 | 0.642 | 1810 | 165,700 | 0.923 |
| 1220 | 245,900 | 0.419 | 1520 | 197,400 | 0.650 | 1820 | 164,800 | 0.933 |
| 1230 | 243,900 | 0.426 | 1530 | 196,100 | 0.659 | 1830 | 163,900 | 0.943 |
| 1240 | 241,900 | 0.433 | 1540 | 194,800 | 0.668 | 1840 | 163,000 | 0.953 |
| 1250 | 240,000 | 0.440 | 1550 | 193,600 | 0.676 | 1850 | 162,200 | 0.963 |
| 1260 | 238,100 | 0.447 | 1560 | 192,300 | 0.685 | 1860 | 161,300 | 0.974 |
| 1270 | 236,200 | 0.454 | 1570 | 191,100 | 0.694 | 1870 | 160,400 | 0.985 |
| 1280 | 234,400 | 0.461 | 1580 | 189,900 | 0.703 | 1880 | 159,600 | 0.995 |
| 1290 | 232,600 | 0.468 | 1590 | 188,700 | 0.712 | 1890 | 158,700 | 1.006 |

Adapted from table prepared by Greenleaf W. Picard; copyright by Wireless Specialty Apparatus Company, New York. Computed on basis of 300,000 kilometers per second for the velocity of propagation of electromagnetic waves.

WIRELESS TELEGRAPHY

Wave-Length, Frequency and Oscillation Constant

| Meters. | n | LC | Meters. | n | LC | Meters. | n | LC |
|---------|---------|-------|---------|---------|------|---------|--------|------|
| 1900 | 157,900 | 1.016 | 2800 | 107,100 | 2.21 | 7000 | 42,860 | 13.8 |
| 1910 | 157,100 | 1.026 | 2820 | 106,400 | 2.24 | 7100 | 42,250 | 14.2 |
| 1920 | 156,300 | 1.037 | 2840 | 105,600 | 2.27 | 7200 | 41,670 | 14.6 |
| 1930 | 155,400 | 1.048 | 2860 | 104,900 | 2.30 | 7300 | 41,100 | 15.0 |
| 1940 | 154,600 | 1.059 | 2880 | 104,200 | 2.33 | 7400 | 40,540 | 15.4 |
| 1950 | 153,800 | 1.070 | 2900 | 103,400 | 2.37 | 7500 | 40,000 | 15.8 |
| 1960 | 153,100 | 1.081 | 2920 | 102,700 | 2.40 | 7600 | 39,470 | 16.3 |
| 1970 | 152,300 | 1.092 | 2940 | 102,000 | 2.43 | 7700 | 38,960 | 16.7 |
| 1980 | 151,500 | 1.103 | 2960 | 101,300 | 2.47 | 7800 | 38,460 | 17.1 |
| 1990 | 150,800 | 1.114 | 2980 | 100,700 | 2.50 | 7900 | 37,980 | 17.6 |
| 2000 | 150,000 | 1.126 | 3000 | 100,000 | 2.53 | 8000 | 37,500 | 18.0 |
| 2020 | 148,500 | 1.148 | 3100 | 96,770 | 2.70 | 8100 | 37,040 | 18.5 |
| 2040 | 147,100 | 1.171 | 3200 | 93,750 | 2.88 | 8200 | 36,590 | 18.9 |
| 2060 | 145,600 | 1.194 | 3300 | 90,910 | 3.07 | 8300 | 36,140 | 19.4 |
| 2080 | 144,200 | 1.218 | 3400 | 88,240 | 3.26 | 8400 | 35,710 | 19.9 |
| 2100 | 142,900 | 1.241 | 3500 | 85,910 | 3.45 | 8500 | 35,290 | 20.3 |
| 2120 | 141,500 | 1.265 | 3600 | 83,330 | 3.65 | 8600 | 34,880 | 20.8 |
| 2140 | 140,200 | 1.289 | 3700 | 81,080 | 3.85 | 8700 | 34,480 | 21.3 |
| 2160 | 138,900 | 1.313 | 3800 | 78,950 | 4.06 | 8800 | 34,090 | 21.8 |
| 2180 | 137,600 | 1.338 | 3900 | 76,920 | 4.28 | 8900 | 33,710 | 22.3 |
| 2200 | 136,400 | 1.362 | 4000 | 75,000 | 4.50 | 9000 | 33,330 | 22.8 |
| 2220 | 135,100 | 1.387 | 4100 | 73,170 | 4.73 | 9100 | 32,970 | 23.3 |
| 2240 | 133,900 | 1.412 | 4200 | 71,430 | 4.96 | 9200 | 32,610 | 23.8 |
| 2260 | 132,700 | 1.438 | 4300 | 69,770 | 5.20 | 9300 | 32,260 | 24.3 |
| 2280 | 131,600 | 1.463 | 4400 | 68,180 | 5.45 | 9400 | 31,910 | 24.9 |
| 2300 | 130,400 | 1.489 | 4500 | 66,670 | 5.70 | 9500 | 31,590 | 25.4 |
| 2320 | 129,300 | 1.515 | 4600 | 65,220 | 5.96 | 9600 | 31,250 | 25.9 |
| 2340 | 128,200 | 1.541 | 4700 | 63,830 | 6.22 | 9700 | 30,930 | 26.5 |
| 2360 | 127,100 | 1.568 | 4800 | 62,500 | 6.49 | 9800 | 30,610 | 27.0 |
| 2380 | 126,000 | 1.594 | 4900 | 61,220 | 6.76 | 9900 | 30,310 | 27.6 |
| 2400 | 125,000 | 1.621 | 5000 | 60,000 | 7.04 | 10000 | 30,000 | 28.1 |
| 2420 | 124,000 | 1.648 | 5100 | 58,820 | 7.32 | | | |
| 2440 | 123,000 | 1.676 | 5200 | 57,690 | 7.61 | | | |
| 2460 | 121,900 | 1.703 | 5300 | 56,600 | 7.91 | | | |
| 2480 | 121,000 | 1.731 | 5400 | 55,560 | 8.21 | | | |
| 2500 | 120,000 | 1.759 | 5500 | 54,550 | 8.51 | | | |
| 2520 | 119,000 | 1.787 | 5600 | 53,570 | 8.83 | | | |
| 2540 | 118,100 | 1.816 | 5700 | 52,630 | 9.15 | | | |
| 2560 | 117,200 | 1.845 | 5800 | 51,720 | 9.47 | | | |
| 2580 | 116,300 | 1.874 | 5900 | 50,850 | 9.81 | | | |
| 2600 | 115,400 | 1.903 | 6000 | 50,000 | 10.1 | | | |
| 2620 | 114,500 | 1.932 | 6100 | 49,180 | 10.5 | | | |
| 2640 | 113,600 | 1.962 | 6200 | 48,550 | 10.8 | | | |
| 2660 | 112,800 | 1.991 | 6300 | 47,620 | 11.1 | | | |
| 2680 | 111,900 | 2.02 | 6400 | 46,870 | 11.5 | | | |
| 2700 | 111,100 | 2.05 | 6500 | 46,150 | 11.9 | | | |
| 2720 | 110,300 | 2.08 | 6600 | 45,450 | 12.3 | | | |
| 2740 | 109,500 | 2.11 | 6700 | 44,780 | 12.6 | | | |
| 2760 | 108,700 | 2.14 | 6800 | 44,120 | 13.0 | | | |
| 2780 | 107,900 | 2.18 | 6900 | 43,480 | 13.4 | | | |
| 2800 | 107,100 | 2.21 | 7000 | 42,860 | 13.8 | | | |

SKIP-DISTANCE AND RANGE TABLE

For frequencies between 1500 and 30000 kc

(This table was prepared by the Naval Research Laboratory.)

| Frequency in kilocycles | Range of ground wave | Skip-distance | | | | Maximum reliable range | | | | |
|-------------------------------|-------------------------------|---------------|-------|--------|-------|------------------------|-------|--------------|-------|------------|
| | | Summer | | Winter | | Summer | | Winter | | Note |
| | | Day | Night | Day | Night | Day | Night | Day | Night | |
| 1500-1715 | 100 | | | | | 100 | 100 | 150 | 300 | b, g |
| 1715-2000 | 90 | | | | | 120 | 175 | 170 | 600 | b, c, h, d |
| 2000-2250 | 85 | | | | | 130 | 250 | 200 | 750 | b, c, i |
| 2250-2750 | 80 | | | | | 150 | 350 | 220 | 1500 | b, j |
| 2750-2850 | 70 | | | | | 170 | 500 | 300 | 2500 | c, k |
| 2850-3500 | 65 | | | | | 200 | 900 | 350 | 3000 | b, c, l |
| 3500-4000 | 60 | | | | | 250 | 1500 | 400 | 4500 | b, c, d, h |
| 4000-5500 | 55 | | | | | 300 | 4000 | 500 | 7000 | b, c, m |
| 5500-5700 | 50 | | | | | 400 | 4000 | 600 | 8000 | b |
| 5700-6000 | 50 | 50 | 50 | 50 | 60 | 450 | 5000 | 650 | 8000 | c |
| 6000-6150 | 50 | 60 | 70 | 60 | 90 | 500 | 5500 | 700 | 8000 | e |
| 6150-6675 | 45 | 70 | 115 | 80 | 175 | 550 | 6500 | 750 | 8000 | b |
| 6675-7000 | 45 | 80 | 185 | 100 | 290 | 650 | 7000 | 820 | 8000 | c |
| 7000-7300 | 45 | 90 | 220 | 115 | 360 | 700 | 7500 | 900 | 8000 | d |
| 7300-8200 | 40 | 140 | 290 | 175 | 465 | 750 | 8000 | 1100 | 8000 | c |
| 8200-8550 | 40 | 160 | 370 | 200 | 570 | 800 | 8000 | 1300 | 8000 | b |
| 8550-8900 | 40 | 170 | 420 | 230 | 630 | 900 | 8000 | 1460 | 8000 | b, c |
| 8900-9500 | 40 | 200 | 485 | 270 | 710 | 950 | 8000 | 1680 | 8000 | c |
| 9500-9600 | 40 | 220 | 530 | 280 | 740 | 1000 | 8000 | 1820 | 8000 | e |
| 9600-11000 | 35 | 260 | 625 | 325 | 860 | 1100 | 8000 | 2140 | 8000 | c |
| 11000-11400 | 35 | 300 | 750 | 380 | 1000 | 1200 | 8000 | 2460 | 8000 | b |
| 11400-11700 | 35 | 315 | 800 | 400 | 1080 | 1300 | 8000 | 2700 | | e |
| 11700-11900 | 35 | 335 | 835 | 420 | 1120 | 1500 | 8000 | 2800 | | c |
| 11900-12300 | 30 | 350 | 870 | 430 | 1170 | 1550 | 8000 | 3000 | | b |
| 12300-12825 | 30 | 370 | 940 | 460 | 1240 | 1600 | 8000 | 3200 | | c |
| 12825-13350 | 30 | 390 | 1000 | 485 | | 1700 | 8000 | 3440 | | b, c |
| 13350-14000 | 30 | 420 | 1075 | 510 | | 1800 | | 3660 | | c |
| 14000-14400 | 30 | 440 | 1150 | 545 | | 1950 | | 4060 | | d |
| 14400-15100 | 30 | 460 | 1230 | 580 | | 2200 | | 4360 | | c |
| 15100-15350 | 30 | 475 | 1300 | 610 | | 2300 | | 4640 | | e |
| 15350-16400 | 30 | 500 | 1370 | 640 | | 2500 | | 5060 | | c |
| 16400-17100 | 25 | 550 | | 700 | | 3000 | | 5600 | | b |
| 17100-17750 | 25 | 580 | | 740 | | 3500 | | 6200 | | b, c |
| 17750-17800 | 25 | 600 | | 755 | | 4000 | | 6450 | | e |
| 17800-21450 | 20 | 660 | | 835 | | 5000 | | 7000 | | c |
| 21450-21550 | 20 | 750 | | 1050 | | 6000 | | 7000 | | e |
| 21550-22300 | 20 | 780 | | 1090 | | 7000 | | 7000 | | b |
| 22300-23000 | 20 | 835 | | 1130 | | 7000 | | 7000 | | b, c |
| 23000-28000 | 15 | 900 | | 1200 | | un- known | | un- known | | f |
| 28000-30000 | 10 | 1000 | | 1400 | | un- known | | un- known | | d |

Skip-distance—Shortest distance beyond the ground wave at which communication is possible, or the point where the sky wave first comes to earth. On certain frequencies and at certain seasons communication is possible within the skip-distance due to echoes and around the world signals. Skip-distance variations are not so very large in the day time but they may be quite variable at night. It should be noted that the ground wave variations ranges are based upon overland data; the ranges over sea are considerably greater. Useful working ranges are, however, based entirely upon the sky wave.

The above table was obtained from the general average of a large number of observations. For the night ranges given it is assumed that the greater part of the path between the transmitting and receiving stations is in darkness.

As the distances given in this table are general averages many discrepancies may be found in practice due to seasonal changes, sun spot activities, geographical location, local weather conditions, etc.

(a) For approximate wave lengths use Table 547. (b) Mobile, ships and coastal stations, aircraft, railroad stock, etc. (c) Fixed, permanent stations handling point to point traffic. (d) Amateur. (e) Broadcast. (f) Not reserved. (g) 1601 experimental, 1600-1652-1664-1680-1704-1712, portable. (h) U. S. entirely amateur. (i) U. S. 2002-2300 experimental visual broadcasting. (j) 2308 experimental. (k) 2750-2950 experimental visual broadcasting. (l) 3088 experimental. (m) 4795 experimental.

MAGNETIC PROPERTIES

DEFINITIONS AND GENERAL DISCUSSION

Unit pole is a quantity of magnetism repelling another unit pole with a force of one dyne; 4π lines of force radiate from it. M , pole strength; $4\pi M$ lines of force radiate from pole of strength M .

H , field strength, = no. of lines of force crossing unit area in normal direction; unit = gauss = one line per unit area.

\mathbf{M} , magnetic moment, = MI , where l is length between poles of magnet.

I , intensity of magnetization or pole strength per unit area, = $\mathbf{M}/V = M/A$ where A is cross section of uniformly magnetized pole face, and V is the volume of the magnet. $4\pi M/A = 4\pi I$ = no. lines of force leaving unit area of pole.

J , specific intensity of magnetism, = I/ρ where ρ = density, g/cm³.

ϕ , magnetic flux, = $4\pi M + HA$ for magnet placed in field of strength H (axis parallel to field). Unit, the maxwell.

B , flux density (magnetic) induction, = $\phi/A = 4\pi I + H$; unit the gauss, maxwell per cm.

μ , magnetic permeability, = B/H . Strength of field in air-filled solenoid = $H = (4\pi/10) ni$ in gauss, i in amperes, n , number of turns per cm length. If iron filled, induction increased, i.e., no. of lines of force per unit area, B , passing through coil is greater than H ; $\mu = B/H$.

κ , susceptibility; permeability relates to effect of iron core on magnetic field strength of coil; if effect be considered on iron core, which becomes a magnet of pole strength M and intensity of magnetism I , then the ratio $I/H = (\mu - 1)/4\pi$ is the magnetic susceptibility per unit volume and is a measure of the magnetizing effect of a magnetic field on the material placed in the field. $\mu = 4\pi\kappa + 1$.

χ , specific susceptibility (per unit mass) = $\kappa/\rho = J/H$.

χ_A , atomic susceptibility, = $\chi \times$ (atomic weight); χ_M = molecular susceptibility.

J_A , J_M , similarly atomic and molecular intensity of magnetization.

Hysteresis is work done in taking a cm³ of the magnetic material through a magnetic cycle = $\oint H dI = (1/4\pi) \oint H dB$. Steinmetz's empirical formula gives a close approximation to the hysteresis loss; it is $aB^{1.6}$ where B is the max. induction and a is a constant (see Table 575). The retentivity (B_r) is the value of B when the magnetizing force is reduced to zero. The reversed field necessary to reduce the magnetism to zero is called the coercive force (H_c).

Ferromagnetic substances, μ very large, κ very large: Fe, Ni, Co, Heusler's alloy (Cu 62.5, Mn 23.5, Al 14. See Stephenson, Phys. Rev. 1910), magnetite and a few alloys of Mn. μ for Heusler's alloy, 90 to 100 for $B = 2200$; for Si steel steel 350 to 5300.

Paramagnetic substances, $\mu > 1$, very small but positive, $\kappa = 10^{-3}$ to 10^{-6} : oxygen, especially at low temperatures, salts of Fe, Ni, Mn, many metallic elements. (See Table 580.)

Diamagnetic substances, $\mu < 1$, κ negative. Most diamagnetic substance known is Bi, -14×10^{-6} . Volume susceptibility (see Table 580).

Paramagnetic substances show no retentivity or hysteresis effect. Susceptibility independent of field strength. The specific susceptibility for both para- and diamagnetic substances is independent of field strength.

For Hall effect (galvanomagnetic difference of potential), Ettinghausen effect (galvanomagnetic difference of temperature), Nernst effect (thermomagnetic difference of potential) and the Leduc effect (thermomagnetic difference of temperature), see Tables 593 and 594.

Magneto-strictive phenomena:

Joule effect: Mechanical change in length when specimen is subjected to a magnetic field. With increasing field strength, iron and some iron alloys show first a small increment $\Delta l/l = (7 \text{ to } 35) \times 10^{-7}$, then a decrement, and for $H = 1600$, $\Delta l/l$ may amount to $-(6 \text{ to } 8) \times 10^{-6}$. Cast cobalt with increasing field first decreases, $\Delta l/l = -8 \times 10^{-6}$, $H = 150$, then increases in length, $\Delta l/l = +5 \times 10^{-6}$, $H = 2000$; annealed cobalt steadily contracts, $\Delta l/l = -25 \times 10^{-6}$, $H = 2000$. Ni rapidly then slowly contracts, $\Delta l/l = -30 \times 10^{-6}$, $H = 100$; -35×10^{-6} , $H = 300$; -36×10^{-6} , $H = 2000$ (Williams, Phys. Rev. 34, 44, 1912). A transverse field generally gives a reciprocal effect.

Wiedemann effect: The lower end of a vertical wire, magnetized longitudinally, when a current is passed through it, if free, twists in a certain direction, depending upon circumstances (see Williams, Phys. Rev. 32, 281, 1911). A reciprocal effect is observed in that when a rod of soft iron, exposed to longitudinal magnetizing force, is twisted, its magnetism is reduced.

Villari effect; really a reciprocal Joule effect. The susceptibility of an iron wire is increased by stretching when the magnetism is below a certain value, but diminished when above that value.

TABLE 550.—Magnetic Properties of Various Types of Iron and SteelFrom tests made at the Bureau of Standards. B and H are measured in cgs units.

| Values of B | | 2000 | 4000 | 6000 | 8000 | 10,000 | 12,000 | 14,000 | 16,000 | 18,000 | 20,000 |
|---------------------------|-------|------|------|------|------|--------|--------|--------|--------|--------|--------|
| Annealed Norway iron | H | .81 | 1.15 | 1.60 | 2.18 | 3.06 | 4.45 | 7.25 | 23.5 | 116. | — |
| | μ | 2470 | 3480 | 3750 | 3670 | 3270 | 2700 | 1930 | 680 | 150 | — |
| Cast semi-steel | H | 2.00 | 2.90 | 4.30 | 6.46 | 9.82 | 15.1 | 24.9 | 50.5 | 135. | 325. |
| | μ | 1000 | 1380 | 1400 | 1240 | 1020 | 795 | 563 | 317 | 133 | 62. |
| Machinery steel | H | 5.0 | 8.8 | 13.1 | 18.6 | 25.8 | 35.8 | 50.5 | 76.0 | 142. | — |
| | μ | 400 | 455 | 460 | 430 | 390 | 340 | 280 | 210 | 127 | — |

TABLE 551.—Magnetic Properties of a Specimen of Very Pure Iron (.017% C)From tests at the Bureau of Standards. B and H are measured in cgs units.

| Values of B | | 2000 | 4000 | 6000 | 8000 | 10,000 | 12,000 | 14,000 | 16,000 | 18,000 | 20,000 |
|--------------------------------------|-------|------|------|------|------|--------|--------|--------|--------|--------|--------|
| Very pure iron } as received } | H | 3.30 | 4.48 | 6.35 | 9.10 | 13.0 | 18.9 | 28.8 | 47.0 | 103. | 240. |
| | μ | 606 | 893 | 945 | 880 | 770 | 635 | 486 | 340 | 175 | 83 |
| Annealed in vacuo } from 900° C } | H | .46 | .60 | .80 | 1.02 | 1.38 | 2.00 | 3.20 | 11.3 | 72.0 | 194. |
| | μ | 4350 | 6670 | 7500 | 7840 | 7250 | 6000 | 4380 | 1420 | 250 | 103 |

As received: H_{\max} 150
 B_{\max} 18,900
 B_r 7,650
 H_c 2.8

After annealing: H_{\max} 150
 B_{\max} 19,500
 H_c 0.53

TABLE 552.—Magnetic Properties of Electrical SheetsFrom tests at the Bureau of Standards. B and H are measured in cgs units.

| Values of B | | 2000 | 4000 | 6000 | 8000 | 10,000 | 12,000 | 14,000 | 16,000 | 18,000 | 20,000 |
|---|-------|------|------|------|------|--------|--------|--------|--------|--------|--------|
| Dynamo steel | H | 1.00 | 1.10 | 1.43 | 2.00 | 3.10 | 4.95 | 9.20 | 34.0 | 114. | — |
| | μ | 2000 | 3640 | 4200 | 4000 | 3220 | 2420 | 1520 | 470 | 158 | — |
| Ordinary trans- } former steel } | H | .60 | .87 | 1.10 | 1.48 | 2.28 | 3.85 | 10.9 | 43.0 | 149. | — |
| | μ | 3340 | 4600 | 5450 | 5400 | 4380 | 3120 | 1280 | 372 | 121 | — |
| High silicon trans- } former steel } | H | .60 | .70 | .90 | 1.28 | 1.99 | 3.60 | 9.80 | 47.4 | 165. | — |
| | μ | 4000 | 5720 | 6670 | 6250 | 5020 | 3340 | 1430 | 338 | 109 | — |

TABLE 553.—Magnetic Properties of Two Types of American Magnet Steel

From tests at the Bureau of Standards. B and H are measured in cgs units.

| Values of B | | 2000 | 4000 | 6000 | 8000 | 10,000 | 12,000 | 14,000 | 16,000 | 18,000 | 20,000 |
|-----------------|-------|------|------|------|------|--------|--------|--------|--------|--------|--------|
| Tungsten steel. | H | 35.0 | 53.3 | 63.3 | 72.5 | 83.4 | 100 | 200 | — | — | — |
| | μ | 57 | 75 | 95 | 111 | 120 | 110 | 70 | — | — | — |
| Chrome steel... | H | 34.5 | 49.0 | 63.5 | 88.4 | 143 | 270 | — | — | — | — |
| | μ | 58 | 82 | 95 | 91 | 70 | 45 | — | — | — | — |

Percentage composition: Tungsten steel, C 0.67 W 5.1 Mn 0.38 Si 0.26

Chrome steel, C 0.81 W 0.06 Cr 2.04 Si 0.25

Tungsten steel: H_{\max} 200 B_{\max} 14,000 Chrome steel: H_{\max} 200 B_{\max} 11,050 H_c 62.5 B_r 10,400 H_c 45.7 B_r 7,030TABLE 554.—Magnetic Properties of a Ferro-Cobalt Alloy, Fe_2Co (35% Cobalt)From tests at the Bureau of Standards. B and H are measured in cgs units.

| Values of B | | 2000 | 4000 | 6000 | 8000 | 10,000 | 12,000 | 14,000 | 16,000 | 18,000 | 20,000 |
|--------------------------|-------|------|------|------|------|--------|--------|--------|--------|--------|--------|
| As received..... | H | 3.10 | 4.28 | 5.50 | 7.17 | 9.65 | 13.4 | 19.1 | 27.3 | 40.0 | 65.0 |
| | μ | 645 | 935 | 1090 | 1115 | 1040 | 900 | 730 | 590 | 450 | 310 |
| Annealed at } 1000° C | H | 3.00 | 4.11 | 5.05 | 6.45 | 8.40 | 11.3 | 15.4 | 21.9 | 31.7 | 50.6 |
| | μ | 670 | 970 | 1190 | 1240 | 1190 | 1060 | 910 | 730 | 570 | 400 |
| Quenched from 1000° C | H | 10.8 | 13.8 | 19.1 | 28.7 | 43.4 | 65.8 | 104 | 163 | 262 | — |
| | μ | 185 | 290 | 314 | 270 | 230 | 182 | 135 | 98 | 60 | — |

As received

Annealed at 1000° C

Quenched from 1000° C

 B_{\max} { 15,000
15,000
15,000 H_{\max} { 22.9
18.3
130 B_r { 7750
7460
8240 H_c { 3.79
3.95
14.3

TABLE 555.—Magnetic Properties of a Ring Sample of Transformer Steel in Very Weak Fields

From tests made at the Bureau of Standards. B and H are measured in cgs units.

| | | | | | | | | | | |
|-----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Values of H | 0.001 | 0.002 | 0.004 | 0.006 | 0.008 | 0.010 | 0.012 | 0.014 | 0.018 | 0.020 |
| Values of B | 0.45 | 0.91 | 1.85 | 2.87 | 3.94 | 5.05 | 6.30 | 7.51 | 10.19 | 11.64 |
| Values of μ | 450 | 455 | 462 | 478 | 492 | 505 | 525 | 536 | 566 | 582 |

TABLE 556.—Magnetic Properties of Iron in Very Weak Fields

The effect of very small magnetizing forces has been studied by C. Baur and by Lord Rayleigh. The following short table is taken from Baur's paper, and is taken by him to indicate that the susceptibility is finite for zero values of H and for a finite range increases in simple proportion to H . He gives the formula $k = 15 + 100H$, or $I = 15H + 100H^2$. The experiments were made on an annealed ring of round bar 1.013 cms radius, the ring having a radius of 9.432 cms. Lord Rayleigh's results for an iron wire not annealed give $k = 6.4 + 5.1H$, or $I = 6.4H + 5.1H^2$. The forces were reduced as low as 0.00004 cgs, the relation of k to H remaining constant.

| First experiment. | | | Second experiment. | |
|-------------------|-------|--------|--------------------|-------|
| H | k | I | H | k |
| .01580 | 16.46 | 2.63 | .0130 | 15.50 |
| .03081 | 17.65 | 5.47 | .0847 | 18.38 |
| .07083 | 23.00 | 10.33 | .0046 | 20.49 |
| .13188 | 28.00 | 38.15 | .1864 | 25.07 |
| .23011 | 30.81 | 91.56 | .2903 | 32.40 |
| .38422 | 58.56 | 224.87 | .3397 | 35.20 |

COMPOSITION AND MAGNETIC

This table and Table 558 below are taken from a paper by Dr. Hopkinson * on the magnetic properties of iron and steel which is stated in the paper to have been 240. The maximum magnetization is not tabulated; but as stated in the by 4π. "Coercive force" is the magnetizing force required to reduce the magnetization to zero. The "demagnetizing" magnetization in the opposite direction to the "maximum induction" stated in the table. The "energy" which, however, was only found to agree roughly with the results of experiment.

| No. of Test. | Description of specimen. | Temper. | Chemical analysis. | | | | | |
|--------------|------------------------------|---------------------------------|--------------------|------------|----------|----------|-------------|-------------------|
| | | | Total Carbon. | Manganese. | Sulphur. | Silicon. | Phosphorus. | Other substances. |
| 1 | Wrought iron . . . | Annealed | — | — | — | — | — | — |
| 2 | Malleable cast iron . . . | " | — | — | — | — | — | — |
| 3 | Gray cast iron . . . | — | — | — | — | — | — | — |
| 4 | Bessemer steel . . . | — | 0.045 | 0.200 | 0.030 | None | 0.040 | — |
| 5 | Whitworth mild steel . . . | Annealed | 0.090 | 0.153 | 0.016 | " | 0.042 | — |
| 6 | " " . . . | " | 0.320 | 0.438 | 0.017 | 0.042 | 0.035 | — |
| 7 | " " . . . | { Oil-hard- ened | " | " | " | " | " | — |
| 8 | " " . . . | Annealed | 0.890 | 0.165 | 0.005 | 0.081 | 0.019 | — |
| 9 | " " . . . | { Oil-hard- ened | " | " | " | " | " | — |
| 10 | Hadfield's manganese steel { | — | 1.005 | 12.360 | 0.038 | 0.204 | 0.070 | — |
| 11 | Manganese steel . . . | As forged | 0.674 | 4.730 | 0.023 | 0.608 | 0.078 | — |
| 12 | " " . . . | Annealed | " | " | " | " | " | — |
| 13 | " " . . . | { Oil-hard- ened | " | " | " | " | " | — |
| 14 | " " . . . | As forged | 1.298 | 8.740 | 0.024 | 0.094 | 0.072 | — |
| 15 | " " . . . | Annealed | " | " | " | " | " | — |
| 16 | " " . . . | { Oil-hard- ened | " | " | " | " | " | — |
| 17 | Silicon steel . . . | As forged | 0.685 | 0.694 | " | 3.438 | 0.123 | — |
| 18 | " " . . . | Annealed | " | " | " | " | " | — |
| 19 | " " . . . | { Oil-hard- ened | " | " | " | " | " | — |
| 20 | Chrome steel . . . | As forged | 0.532 | 0.393 | 0.020 | 0.220 | 0.041 | 0.621 Cr. |
| 21 | " " . . . | Annealed | " | " | " | " | " | " |
| 22 | " " . . . | { Oil-hard- ened | " | " | " | " | " | " |
| 23 | " " . . . | As forged | 0.687 | 0.028 | " | 0.134 | 0.043 | 1.195 Cr. |
| 24 | " " . . . | Annealed | " | " | " | " | " | " |
| 25 | " " . . . | { Oil-hard- ened | " | " | " | " | " | " |
| 26 | Tungsten steel . . . | As forged | 1.357 | 0.036 | None. | 0.043 | 0.047 | 4.649 W. |
| 27 | " " . . . | Annealed | " | " | " | " | " | " |
| 28 | " " . . . | { Hardened in cold water | " | " | " | " | " | " |
| 29 | " " . . . | { Hardened in tepid water | " | " | " | " | " | " |
| 30 | " " (French) . . . | { Oil-hard- ened | 0.511 | 0.625 | None. | 0.021 | 0.028 | 3.444 W. |
| 31 | " " . . . | Very hard | 0.855 | 0.312 | — | 0.151 | 0.089 | 2.353 W. |
| 32 | Gray cast iron . . . | — | 3.455 | 0.173 | 0.042 | 2.044 | 0.151 | 2.064 C.† |
| 33 | Mottled cast iron . . . | — | 2.581 | 0.610 | 0.105 | 1.476 | 0.435 | 1.477 C.† |
| 34 | White " " . . . | — | 2.036 | 0.386 | 0.467 | 0.764 | 0.458 | — |
| 35 | Spiegeleisen . . . | — | 4.510 | 7.970 | Trace. | 0.502 | 0.128 | — |

* Phil. Trans. Roy. Soc. vol. 176.

† Graphitic carbon.

PROPERTIES OF IRON AND STEEL

The numbers in the columns headed "magnetic properties" give the results for the highest magnetizing force used, paper, it may be obtained by subtracting the magnetizing force (240) from the maximum induction and then dividing netizing force" is the magnetizing force which had to be applied in order to leave no residual magnetization after dissipated" was calculated from the formula:—Energy dissipated = coercive force \times maximum induction $\div \pi$

| No. of Test. | Description of specimen. | Temper. | Specific electrical resistance. | Magnetic properties. | | | | Energy dissipated per cycle. |
|--------------|------------------------------|---------------------------------|---------------------------------|----------------------|---------------------|-----------------|----------------------|------------------------------|
| | | | | Maximum induction. | Residual induction. | Coercive force. | Demagnetizing force. | |
| 1 | Wrought iron | Annealed | .01378 | 18251 | 7248 | 2.30 | — | 13356 |
| 2 | Malleable cast iron . . | " | .03254 | 12408 | 7479 | 8.80 | — | 34742 |
| 3 | Gray cast iron | — | .10560 | 10783 | 3928 | 3.80 | — | 13037 |
| 4 | Bessemer steel | — | .01050 | 18196 | 7860 | 2.96 | — | 17137 |
| 5 | Whitworth mild steel . . | Annealed | .01080 | 19840 | 7080 | 1.63 | — | 10289 |
| 6 | " " | " | .01446 | 18736 | 9840 | 6.73 | — | 40120 |
| 7 | " " | { Oil-hard- ened | .01390 | 18796 | 11040 | 11.00 | — | 65786 |
| 8 | " " | Annealed | .01559 | 16120 | 10740 | 8.26 | — | 42366 |
| 9 | " " | { Oil-hard- ened | .01695 | 16120 | 8736 | 19.38 | — | 99401 |
| 10 | Hadfield's manganese steel } | — | .06554 | 310 | — | — | — | — |
| 11 | Manganese steel | As forged | .05368 | 4623 | 2202 | 23.50 | 37.13 | 34567 |
| 12 | " " | Annealed | .03928 | 10578 | 5848 | 33.86 | 46.10 | 113963 |
| 13 | " " | { Oil-hard- ened | .05556 | 4769 | 2158 | 27.64 | 40.29 | 41941 |
| 14 | " " | As forged | .06993 | 747 | — | — | — | — |
| 15 | " " | Annealed | .06316 | 1985 | 540 | 24.50 | 50.39 | 15474 |
| 16 | " " | { Oil-hard- ened | .07066 | 733 | — | — | — | — |
| 17 | Silicon steel | As forged | .06163 | 15148 | 11073 | 9.49 | 12.60 | 45740 |
| 18 | " " | Annealed | .06185 | 14701 | 8149 | 7.80 | 10.74 | 36485 |
| 19 | " " | { Oil-hard- ened | .06195 | 14696 | 8084 | 12.75 | 17.14 | 59619 |
| 20 | Chrome steel | As forged | .02016 | 15778 | 9318 | 12.24 | 13.87 | 61439 |
| 21 | " " | Annealed | .01942 | 14848 | 7570 | 8.98 | 12.24 | 42425 |
| 22 | " " | { Oil-hard- ened | .02708 | 13960 | 8595 | 38.15 | 48.45 | 169455 |
| 23 | " " | As forged | .01791 | 14680 | 7568 | 18.40 | 22.03 | 85944 |
| 24 | " " | Annealed | .01849 | 13233 | 6489 | 15.40 | 19.79 | 64842 |
| 25 | " " | { Oil-hard- ened | .03035 | 12868 | 7891 | 40.80 | 56.70 | 167050 |
| 26 | Tungsten steel | As forged | .02249 | 15718 | 10144 | 15.71 | 17.75 | 78568 |
| 27 | " " | Annealed | .02250 | 16498 | 11008 | 15.30 | 16.93 | 80315 |
| 28 | " " | { Hardened in cold water | .02274 | — | — | — | — | — |
| 29 | " " | { Hardened in tepid water | .02249 | 15610 | 9482 | 30.10 | 34.70 | 149500 |
| 30 | " " (French) | { Oil-hard- ened | .03604 | 14480 | 8643 | 47.07 | 64.46 | 216864 |
| 31 | " " | Very hard | .04427 | 12133 | 6818 | 51.20 | 70.69 | 197660 |
| 32 | Gray cast iron | — | .11400 | 9148 | 3161 | 13.67 | 17.03 | 39789 |
| 33 | Mottled cast iron | — | .06286 | 10546 | 5108 | 12.24 | — | 41072 |
| 34 | White " " | — | .05661 | 9342 | 5554 | 12.24 | 20.40 | 36383 |
| 35 | Spiegeleisen | — | .10520 | 385 | 77 | — | — | — |

TABLE 558.—Permeability of Some of the Specimens in Table 557

This table gives the induction and the permeability for different values of the magnetizing force of some of the specimens in Table 557. The specimen numbers refer to the same table. The numbers in this table have been taken from the curves given by Dr. Hopkinson, and may therefore be slightly in error; they are the mean values for rising and falling magnetizations.

| Magnetizing force. <i>H</i> | Specimen 1 (iron). | | Specimen 8 (annealed steel). | | Specimen 9 (same as 8 tempered). | | Specimen 3 (cast iron). | |
|--------------------------------|--------------------|-------|------------------------------|-------|----------------------------------|-------|-------------------------|-------|
| | <i>B</i> | μ | <i>B</i> | μ | <i>B</i> | μ | <i>B</i> | μ |
| 1 | — | — | — | — | — | — | 265 | 265 |
| 2 | 200 | 100 | — | — | — | — | 700 | 350 |
| 3 | — | — | — | — | — | — | 1625 | 542 |
| 5 | 10050 | 2010 | 1525 | 300 | 750 | 150 | 3000 | 600 |
| 10 | 12550 | 1255 | 9000 | 900 | 1650 | 165 | 5000 | 500 |
| 20 | 14550 | 727 | 11500 | 575 | 5875 | 294 | 6000 | 300 |
| 30 | 15200 | 507 | 12050 | 422 | 9875 | 329 | 6500 | 217 |
| 40 | 15800 | 395 | 13300 | 332 | 11600 | 290 | 7100 | 177 |
| 50 | 16000 | 320 | 13800 | 276 | 12000 | 240 | 7350 | 149 |
| 70 | 16360 | 234 | 14350 | 205 | 13400 | 191 | 7900 | 113 |
| 100 | 16800 | 168 | 14900 | 149 | 14500 | 145 | 8500 | 85 |
| 150 | 17400 | 116 | 15700 | 105 | 15800 | 105 | 9500 | 63 |
| 200 | 17950 | 90 | 16100 | 80 | 16100 | 80 | 10190 | 51 |

Tables 559-563 give the results of some experiments by Du Bois,* on the magnetic properties of iron, nickel, and cobalt under strong magnetizing forces. The experiments were made on ovoids of the metals 18 centimeters long and 0.6 centimeters diameter. The specimens were as follows: (1) Soft Swedish iron carefully annealed and having a density 7.82. (2) Hard English cast steel yellow tempered at 230° C; density 7.78. (3) Hard drawn best nickel containing 99% Ni with some SiO₂ and traces of Fe and Cu; density 8.82. (4) Cast cobalt giving the following composition on analysis: Co = 93.1, Ni = 5.8, Fe = 0.8, Cu = 0.2, Si = 0.1, and C = 0.3. The specimen was very brittle and broke in the lathe, and hence contained a surfaced joint held together by clamps during the experiment. Referring to the columns, *H*, *B*, and μ have the same meaning as in the other tables, *S* is the magnetic moment per gram, and *I* the magnetic moment per cubic centimeter. *H* and *S* are taken from the curves published by Du Bois; the others have been calculated using the densities given.

TABLE 559.—Magnetic Properties of Soft Iron at 0° and 100° C

| Soft iron at 0° C. | | | | | Soft iron at 100° C. | | | | |
|--------------------|----------|----------|----------|-------|----------------------|----------|----------|----------|-------|
| <i>H</i> | <i>S</i> | <i>I</i> | <i>B</i> | μ | <i>H</i> | <i>S</i> | <i>I</i> | <i>B</i> | μ |
| 100 | 180.0 | 1408 | 17790 | 177.9 | 100 | 180.0 | 1402 | 17720 | 177.2 |
| 200 | 194.5 | 1521 | 19310 | 96.5 | 200 | 194.0 | 1511 | 19190 | 96.0 |
| 400 | 208.0 | 1627 | 20830 | 52.1 | 400 | 207.0 | 1613 | 20660 | 51.6 |
| 700 | 215.5 | 1685 | 21870 | 31.2 | 700 | 213.4 | 1663 | 21590 | 29.8 |
| 1000 | 218.0 | 1705 | 22420 | 22.4 | 1000 | 215.0 | 1674 | 22040 | 21.0 |
| 1200 | 218.5 | 1709 | 22670 | 18.9 | 1200 | 215.5 | 1679 | 22300 | 18.6 |

TABLE 560.—Magnetic Properties of Steel at 0° and 100° C

| Steel at 0° C. | | | | | Steel at 100° C. | | | | |
|----------------|----------|----------|----------|-------|------------------|----------|----------|----------|-------|
| <i>H</i> | <i>S</i> | <i>I</i> | <i>B</i> | μ | <i>H</i> | <i>S</i> | <i>I</i> | <i>B</i> | μ |
| 100 | 165.0 | 1283 | 16240 | 162.4 | 100 | 165.0 | 1278 | 16170 | 161.7 |
| 200 | 181.0 | 1408 | 17900 | 89.5 | 200 | 180.0 | 1395 | 17730 | 88.6 |
| 400 | 193.0 | 1500 | 19250 | 48.1 | 400 | 191.0 | 1480 | 19000 | 47.5 |
| 700 | 199.5 | 1552 | 20210 | 28.9 | 700 | 197.0 | 1527 | 19890 | 28.4 |
| 1000 | 203.5 | 1583 | 20900 | 20.9 | 1000 | 199.0 | 1543 | 20380 | 20.4 |
| 1200 | 205.0 | 1595 | 21240 | 17.7 | 1500 | 203.0 | 1573 | 21270 | 14.2 |
| 3750† | 212.0 | 1650 | 24470 | 6.5 | 3000 | 205.5 | 1593 | 23020 | 7.7 |
| | | | | | 5000 | 208.0 | 1612 | 25260 | 5.1 |

* "Phil. Mag." 5 series, vol. xxix.

† The results in this and the other tables for forces above 1200 were not obtained from the ovoids above referred to, but from a small piece of the metal provided with a polished mirror surface and placed, with its polished face normal to the lines of force, between the poles of a powerful electromagnet. The induction was then inferred from the rotation of the plane of a polarized ray of red light reflected normally from the surface. (See Kerr's "Constants," p. 480.)

MAGNETIC PROPERTIES OF METALS

TABLE 561.—Cobalt at 0° and 100° C

| <i>H</i> | <i>S</i> | <i>I</i> | <i>B</i> | μ |
|---|----------|----------|----------|-------|
| 200 | 106 | 8.48 | 10850 | 54.2 |
| 300 | 116 | 9.28 | 11960 | 39.9 |
| 500 | 127 | 10.16 | 13260 | 26.5 |
| 700 | 131 | 10.48 | 13870 | 19.8 |
| 1000 | 134 | 10.76 | 14520 | 14.5 |
| 1500 | 138 | 11.04 | 15380 | 10.3 |
| 2500 | 143 | 11.44 | 16870 | 6.7 |
| 4000 | 145 | 11.64 | 18630 | 4.7 |
| 6000 | 147 | 11.76 | 20780 | 3.5 |
| 9000 | 149 | 11.92 | 23980 | 2.6 |
| At 0° C this specimen gave the following results: | | | | |
| 7900 | 154 | 12.32 | 23380 | 3.0 |

TABLE 562.—Nickel at 0° and 100° C

| <i>H</i> | <i>S</i> | <i>I</i> | <i>B</i> | μ |
|---|----------|----------|----------|-------|
| 100 | 35.0 | 309 | 3980 | 39.8 |
| 200 | 43.0 | 380 | 4966 | 24.8 |
| 300 | 46.0 | 406 | 5399 | 18.0 |
| 500 | 50.0 | 441 | 6043 | 12.1 |
| 700 | 51.5 | 454 | 6409 | 9.1 |
| 1000 | 53.0 | 468 | 6875 | 6.9 |
| 1500 | 56.0 | 494 | 7707 | 5.1 |
| 2500 | 58.4 | 515 | 8973 | 3.6 |
| 4000 | 59.0 | 520 | 10540 | 2.6 |
| 6000 | 59.2 | 522 | 12501 | 2.1 |
| 9000 | 59.4 | 524 | 15585 | 1.7 |
| 12000 | 59.6 | 526 | 18666 | 1.5 |
| At 0° C this specimen gave the following results: | | | | |
| 12300 | 67.5 | 595 | 19782 | 1.6 |

TABLE 563.—Magnetite

The following results are given by Du Bois * for a specimen of magnetite.

| <i>H</i> | <i>I</i> | <i>B</i> | μ |
|----------|----------|----------|-------|
| 500 | 325 | 4580 | 9.16 |
| 1000 | 345 | 5340 | 5.34 |
| 2000 | 350 | 6400 | 3.20 |
| 12000 | 350 | 16400 | 1.37 |

Professor Ewing has investigated the effects of very intense fields on the induction in iron and other metals.† The results show that the intensity of magnetization does not increase much in iron after the field has reached an intensity of 1000 c. g. s. units, the increase of induction above this being almost the same as if the iron were not there, that is to say, dB/dH is practically unity. For hard steels, and particularly manganese steels, much higher forces are required to produce saturation. Hadfield's manganese steel seems to have nearly constant susceptibility up to a magnetizing force of 10,000. The following tables, taken from Ewing's papers, illustrate the effects of strong fields on iron and steel. The results for nickel and cobalt do not differ greatly from those given above.

TABLE 564.—Lowmoor Wrought Iron

| <i>H</i> | <i>I</i> | <i>B</i> | μ |
|----------|----------|----------|-------|
| 3080 | 1680 | 24130 | 7.83 |
| 6450 | 1740 | 28300 | 4.39 |
| 10450 | 1730 | 32250 | 3.09 |
| 13600 | 1720 | 35200 | 2.59 |
| 16390 | 1630 | 36810 | 2.25 |
| 18760 | 1680 | 39900 | 2.13 |
| 18980 | 1730 | 40730 | 2.15 |

TABLE 565.—Vicker's Tool Steel

| <i>H</i> | <i>I</i> | <i>B</i> | μ |
|----------|----------|----------|-------|
| 6210 | 1530 | 25480 | 4.10 |
| 9970 | 1570 | 29650 | 2.97 |
| 12120 | 1550 | 31620 | 2.60 |
| 14660 | 1580 | 34550 | 2.36 |
| 15530 | 1610 | 35820 | 2.31 |

TABLE 566.—Hadfield's Manganese Steel

| <i>H</i> | <i>I</i> | <i>B</i> | μ |
|----------|----------|----------|-------|
| 1930 | 55 | 2620 | 1.36 |
| 2380 | 84 | 3430 | 1.44 |
| 3350 | 84 | 4400 | 1.31 |
| 5920 | 111 | 7310 | 1.24 |
| 6620 | 187 | 8970 | 1.35 |
| 7890 | 191 | 10290 | 1.30 |
| 8390 | 263 | 11690 | 1.39 |
| 9810 | 396 | 14790 | 1.51 |

TABLE 567.—Saturation Values for Steels

| | | <i>H</i> | <i>I</i> | <i>B</i> | μ |
|---|---|----------|----------|----------|-------|
| 1 | Bessemer steel containing about 0.4 per cent carbon . . . | 17600 | 1770 | 39880 | 2.27 |
| 2 | Siemens-Marten steel containing about 0.5 per cent carbon . . . | 18000 | 1660 | 38860 | 2.16 |
| 3 | Crucible steel for making chisels, containing about 0.6 per cent carbon | 19470 | 1480 | 38010 | 1.95 |
| 4 | Finer quality of 3 containing about 0.8 per cent carbon . . . | 18330 | 1580 | 38190 | 2.08 |
| 5 | Crucible steel containing 1 per cent carbon | 19620 | 1440 | 37690 | 1.92 |
| 6 | Whitworth's fluid-compressed steel | 18700 | 1590 | 38710 | 2.07 |

* "Phil. Mag." 5 series, vol. xxix, 1899.

† "Phil. Trans. Roy. Soc." 1885 and 1899.

DEMAGNETIZING FACTORS FOR RODS

TABLE 568

H = true intensity o. magnetizing field, H' = intensity of applied field, I = intensity of magnetization, $H = H' - NI$.

Shuddemagen says: The demagnetizing factor is not a constant, falling for highest values of I to about $1/7$ the value when unsaturated; for values of B ($=H+4\pi I$) less than 10000, N is approximately constant; using a solenoid wound on an insulating tube, or a tube of split brass, the reversal method gives values for N which are considerably lower than those given by the step-by-step method; if the solenoid is wound on a thick brass tube, the two methods practically agree.

| Ratio of Length to Diameter. | Values of $N \times 10^4$. | | | | | | |
|------------------------------|-----------------------------|------------------------|------------------------------|------------------------|---|-----------|-----------|
| | Cylinder. | | | | | | |
| | Ellipsoid. | Uniform Magnetization. | Magnetometric Method (Mann). | Ballistic Step Method. | | | |
| | | | | Dubois. | Shuddemagen for Range of Practical Constancy. | | |
| | | | | | Diameter. | | |
| | | | | 0.158 cm. | 0.3175 cm. | 1.111 cm. | 1.905 cm. |
| 5 | 7015 | — | 6800 | | | | |
| 10 | 2549 | 630 | 2550 | 2160 | — | — | 1960 |
| 15 | 1350 | 280 | 1400 | 1206 | — | — | 1075 |
| 20 | 848 | 160 | 898 | 775 | — | — | 671 |
| 30 | 432 | 70 | 460 | 393 | 388 | 350 | 343 |
| 40 | 266 | 39 | 274 | 238 | 234 | 212 | 209 |
| 50 | 181 | 25 | 182 | 162 | 160 | 145 | 149 |
| 60 | 132 | 18 | 131 | 118 | 116 | 106 | 106 |
| 70 | 101 | 13 | 99 | 89 | 88 | | |
| 80 | 80 | 9.8 | 78 | 69 | 69 | 66 | 63 |
| 90 | 65 | 7.8 | 63 | 55 | 56 | | |
| 100 | 54 | 6.3 | 51.8 | 45 | 46 | 41 | 41 |
| 150 | 26 | 2.8 | 25.1 | 20 | 23 | 21 | 21 |
| 200 | 16 | 1.57 | 15.2 | 11 | 12.5 | 11 | 11 |
| 300 | 7.5 | 0.70 | 7.5 | 5.0 | | | |
| 400 | 4.5 | 0.39 | — | 2.8 | | | |

C. R. Mann, Physical Review, 3, p. 359; 1896.

H. DuBois, Wied. Ann. 7, p. 942; 1902.

C. L. B. Shuddemagen, Proc. Am. Acad. Arts and Sci. 43, p. 185, 1907 (Bibliography).

TABLE 569

Shuddemagen also gives the following, where B is determined by the step method and $H = H' - KB$.

| Ratio of Length to Diameter. | Values of $K \times 10^4$. | |
|------------------------------|-----------------------------|-------------------------|
| | Diameter 0.3175 cm. | Diameter 1.1 to 2.0 cm. |
| 15 | — | 85.2 |
| 20 | — | 53.3 |
| 25 | — | 36.6 |
| 30 | 30.9 | 27.3 |
| 40 | 18.6 | 16.6 |
| 50 | 12.7 | 11.6 |
| 60 | 9.25 | 8.45 |
| 80 | 5.5 | 5.05 |
| 100 | 3.66 | 3.26 |
| 150 | 1.83 | 1.67 |

TABLE 570.—Magnetic Properties of Iron and Steel

| | | Electro- lytic Iron. | Good Cast Steel. | Poor Cast Steel. | Steel. | Cast Iron. | Electrical Sheets. | |
|----------------------------------|----|----------------------------|------------------------|------------------------|------------------|------------------|--------------------|-------------------|
| | | | | | | | Ordinary. | Silicon Steel. |
| Chemical composition in per cent | C | 0.024 | 0.044 | 0.56 | 0.99 | 3.11 | 0.036 | 0.036 |
| | Si | 0.004 | 0.004 | 0.18 | 0.10 | 3.27 | 0.330 | 3.90 |
| | Mn | 0.008 | 0.40 | 0.29 | 0.40 | 0.56 | 0.260 | 0.090 |
| | P | 0.008 | 0.044 | 0.076 | 0.04 | 1.05 | 0.040 | 0.009 |
| | S | 0.001 | 0.027 | 0.035 | 0.07 | 0.06 | 0.068 | 0.006 |
| Coercive force | | 2.83 [0.36] | 1.51 [0.37] | 7.1 (44.3) | 16.7 (52.4) | 11.4 [4.6] | [1.30] | [0.77] |
| Residual B | | 11400 [10800] | 10600 [11000] | 10500 (10500) | 53000 (7500) | 5100 [5350] | [9400] | [9850] |
| Maximum permeability | | 1850 [14400] | 3550 [14800] | 700 (170) | 375 (110) | 240 [600] | [3270] | [6130] |
| B for H=150 | | 19200 [18900] | 18800 [19100] | 17400 (15400) | 16700 (11700) | 10400 [11000] | [18200] | [17550] |
| 4πI for saturation | | 21620 [21630] | 21420 [21420] | 20600 (20200) | 19800 (18000) | 16400 [16800] | [20500] | [19260] |

E. Gumlich, Zs. für Electrochemie, 15, p. 599; 1909

Brackets indicate annealing at 800° C in vacuum.

Parentheses indicate hardening by quenching from cherry-red.

TABLE 571.—Cast Iron in Intense Fields

| Soft Cast Iron. | | | | Hard Cast Iron. | | | |
|-----------------|-------|------|------|-----------------|-------|------|------|
| H | B | I | μ | H | B | I | μ |
| 114 | 9950 | 782 | 87.3 | 142 | 7860 | 614 | 55.4 |
| 172 | 10800 | 846 | 62.8 | 254 | 9700 | 752 | 38.2 |
| 433 | 13900 | 1070 | 32.1 | 339 | 10850 | 836 | 30.6 |
| 744 | 15750 | 1200 | 21.2 | 684 | 13050 | 983 | 19.1 |
| 1234 | 17300 | 1280 | 14.0 | 915 | 14050 | 1044 | 15.4 |
| 1820 | 18170 | 1300 | 10.0 | 1570 | 15900 | 1138 | 10.1 |
| 12700 | 31100 | 1465 | 2.5 | 2020 | 16800 | 1176 | 8.3 |
| 13550 | 32100 | 1475 | 2.4 | 10900 | 26540 | 1245 | 2.4 |
| 13800 | 32500 | 1488 | 2.4 | 13200 | 28600 | 1226 | 2.2 |
| 15100 | 33650 | 1472 | 2.2 | 14800 | 30200 | 1226 | 2.0 |

B. O. Peirce, Proc. Am. Acad. 44, 1909.

TABLE 572.—Corrections for Ring Specimens

In the case of ring specimens, the average magnetizing force is not the value at the mean radius, the ratio of the two being given in the table. The flux density consequently is not uniform, and the measured hysteresis is less than it would be for a uniform distribution. This ratio is also given for the case of constant permeability, the values being applicable for magnetizations in the neighborhood of the maximum permeability. For higher magnetizations the flux density is more uniform, for lower it is less, and the correction greater.

| Ratio of Radial Width to Diameter of Ring. | Ratio of Average H to H at Mean Radius. | | Ratio of Hysteresis for Uniform Distribution to Actual Hysteresis. | |
|--|--|----------------------------|---|----------------------------|
| | Rectangular Cross-section. | Circular Cross-section. | Rectangular Cross-section. | Circular Cross-section. |
| 1/2 | 1.0986 | 1.0718 | 1.112 | 1.084 |
| 1/3 | 1.0397 | 1.0294 | 1.045 | 1.033 |
| 1/4 | 1.0216 | 1.0162 | 1.024 | 1.018 |
| 1/5 | 1.0137 | 1.0102 | 1.015 | 1.011 |
| 1/6 | 1.0094 | 1.0070 | 1.010 | 1.008 |
| 1/7 | 1.0069 | 1.0052 | 1.008 | 1.006 |
| 1/8 | 1.0052 | 1.0040 | 1.006 | 1.004 |
| 1/10 | 1.0033 | 1.0025 | 1.003 | 1.002 |
| 1/19 | 1.0009 | 1.0007 | 1.001 | 1.001 |

M. G. Lloyd, Bull. Bur. Standards, 5, p. 435; 1908.

TABLE 573.—Energy Losses in Transformer Steels

Determined by the wattmeter method.

Loss per cycle per cc = $AB^2 + buB^u$, where B = flux density in gaussses and u = frequency in cycles per second. x shows the variation of hysteresis with B between 5000 and 10000 gaussses, and y the same for eddy currents.

| Designation. | Thick- ness. cm. | Ergs per Gramme per Cycle. | | | | x | y | a | Watts per Pound at 60 Cycles and 10000 Gausses. | | |
|----------------|------------------------|----------------------------|-----------------------------|------------------|-----------------------------|------|------|---------|---|------------------|--------|
| | | 10000 Gausses. | | 5000 Gausses. | | | | | Eddy Current Loss for Gage No. 29 † | Hyste- resis. | Total. |
| | | Hyste- resis. | Eddy Cur- rents at 60 | Hyste- resis. | Eddy Cur- rents at 60 | | | | | | |
| Unannealed | | | | | | | | | | | |
| A | 0.0399 | 1599 | 186 | 562 | 46 | 1.51 | 2.02 | 0.00490 | 0.41 | 4.35 | 4.76 |
| B | .0326 | 1156 | 134 | 384 | 36 | 1.59 | 1.89 | .00358 | 0.44 | 3.14 | 3.58 |
| C | .0422 | 1032 | 242 | 356 | 70 | 1.51 | 1.79 | .00319 | 0.47 | 2.81 | 3.28 |
| D | .0381 | 1009 | 184 | 353 | 48 | 1.52 | 1.94 | .00312 | 0.44 | 2.74 | 3.18 |
| Annealed | | | | | | | | | | | |
| E | .0476 | 735 | 236 | 246 | 58 | 1.58 | 2.02 | .00227 | 0.36 | 2.00 | 2.36 |
| F | .0280 | 666 | 100 | 220 | 27 | 1.60 | 1.88 | .00206 | 0.44 | 1.81 | 2.25 |
| G | .0394 | 563 | 210 | 193 | 54 | 1.54 | 1.96 | .00174 | 0.47 | 1.53 | 2.00 |
| H* | .0307 | 412 | 146 | 138.5 | 39 | 1.58 | 1.90 | .00127 | 0.54 | 1.12 | 1.66 |
| I | .0318 | 341 | 202 | 111.5 | 55 | 1.62 | 1.88 | .00105 | 0.70 | 0.93 | 1.63 |
| K* | .0282 | 394 | 124 | 130 | 32 | 1.61 | 1.90 | .00122 | 0.54 | 1.07 | 1.61 |
| L | .0346 | 381 | 184 | 125 | 50 | 1.61 | 1.88 | .00118 | 0.535 | 1.035 | 1.57 |
| B | .0338 | 354 | 200 | 116 | 57 | 1.61 | 1.81 | .00110 | 0.61 | 0.96 | 1.57 |
| M | .0335 | 372 | 178 | 127 | 46 | 1.55 | 1.95 | .00115 | 0.55 | 1.01 | 1.56 |
| N | .0340 | 321 | 210 | 105 | 56 | 1.62 | 1.90 | .00099 | 0.63 | 0.87 | 1.50 |
| P | .0437 | 334 | 184 | 107 | 50 | 1.64 | 1.88 | .00103 | 0.34 | 0.91 | 1.25 |
| Silicon steels | | | | | | | | | | | |
| Q† | .0361 | 303 | 54 | 98 | 15 | 1.63 | — | .00094 | 0.14 | 0.825 | 0.965 |
| R | .0315 | 288 | 42 | 93 | 11 | 1.64 | — | .00089 | 0.15 | 0.78 | 0.93 |
| S | .0452 | 278 | 72 | 90 | 18 | 1.63 | — | .00086 | 0.12 | 0.755 | 0.875 |
| T | .0338 | 250 | 60 | 78 | 13 | 1.68 | — | .00077 | 0.18 | 0.68 | 0.86 |
| U | .0346 | 270 | 42 | 86 | 12 | 1.66 | — | .00084 | 0.12 | 0.735 | 0.855 |
| V* | .0310 | 251.5 | 47 | 79 | 13 | 1.68 | — | .00078 | 0.17 | 0.685 | 0.855 |
| W* | .0305 | 197 | 43 | 62.3 | 12.4 | 1.67 | — | .00061 | 0.16 | 0.535 | 0.695 |
| X | .0430 | 200 | 65 | 64.2 | 16.6 | 1.65 | — | .00062 | 0.12 | 0.545 | 0.665 |

* German.

† English.

† In order to make a fair comparison, the eddy current loss has been computed for a thickness of 0.0357 cm (Gage No. 29), assuming the loss proportional to the thickness.

Lloyd and Fisher, Bull. Bur. Standards, 5, p. 453; 1909.

Note. — For formulæ and tables for the calculation of mutual and self inductance see Bulletin Bureau of Standards, vol. 8, p. 1-237, 1912.

TABLE 574.—Magnetic Properties of Permalloy

(Vensen, Nickel-Iron Alloys, Journ. Franklin Inst., 199, 340, 1925; Arnold, Elmen, Permalloy, loc. cit., 195, 621, 1923.)

| Alloy | Permeability | | Satura- tion 41 (gausses) | Hys- teresis $B = 10000$ Erg/C ³ /cycle | Reten- tivity gausses | Coer- cive force gilbert/ cm | Elec- trical resis- tance microhms per cm ² 20°C | Den- sity |
|-------------------------|-----------------------------|---------------|------------------------------------|--|-----------------------------|--|---|--------------|
| | Initial B/H $H = 0$ | B/H max. | | | | | | |
| Fe, 3 mm thick..... | 700 | 26,000 | 22,600 | 600 | 8,600 | 0.20 | 10 | 7.9 |
| 4% Si, .35 mm thick... | 440 | 15,500 | 20,000 | 500 | 5,200 | .15 | 55 | 7.6 |
| 50% Ni, .35 mm thick*.. | 3,000 | 70,000 | 15,500 | 220 | 7,300 | .05 | 46 | 8.3 |
| 78% Ni, .35 mm thick.. | 5,850 | 74,000 | 10,500 | 200 | 5,500 | .05 | 21 | 8.6 |

* Permalloy.

DISSIPATION OF ENERGY IN THE CYCLIC MAGNETIZATION OF VARIOUS SUBSTANCES

C. P. Steinmetz concludes from his experiments* that the dissipation of energy due to hysteresis in magnetic metals can be expressed by the formula $c = aB^{1.6}$, where c is the energy dissipated and a a constant. He also concludes that the dissipation is the same for the same range of induction, no matter what the absolute value of the terminal inductions may be. His experiments show this to be nearly true when the induction does not exceed ± 15000 c. g. s. units per sq. cm. It is possible that, if metallic induction only be taken, this may be true up to saturation; but it is not likely to be found to hold for total inductions much above the saturation value of the metal. The law of variation of dissipation with induction range in the cycle, stated in the above formula, is also subject to verification.†

Values of Constant α

The following table gives the values of the constant a as found by Steinmetz for a number of different specimens. The data are taken from his second paper.

| Number of specimen. | Kind of material. | Description of specimen. | Value of α . |
|---------------------|-------------------|---|---------------------|
| 1 | Iron . . | Norway iron | .00227 |
| 2 | " . . | Wrought bar | .00326 |
| 3 | " . . | Commercial ferrottype plate | .00548 |
| 4 | " . . | Annealed " | .00458 |
| 5 | " . . | Thin tin plate | .00286 |
| 6 | " . . | Medium thickness tin plate | .00425 |
| 7 | Steel . . | Soft galvanized wire | .00349 |
| 8 | " . . | Annealed cast steel | .00848 |
| 9 | " . . | Soft annealed cast steel | .00457 |
| 10 | " . . | Very soft annealed cast steel | .00318 |
| 11 | " . . | Same as 8 tempered in cold water | .02792 |
| 12 | " . . | Tool steel glass hard tempered in water | .07476 |
| 13 | " . . | " " tempered in oil | .02670 |
| 14 | " . . | " " annealed | .01899 |
| 15 | " . . | { Same as 12, 13, and 14, after having been subjected to an alternating m. m. f. of from 4000 to 6000 ampere turns for demagnetization } | .06130 |
| 16 | " . . | | .02700 |
| 17 | " . . | | .01445 |
| 18 | Cast iron . . | Gray cast iron | .01300 |
| 19 | " " . . | " " " containing $\frac{1}{2}\%$ aluminium | .01365 |
| 20 | " " . . | " " " " $\frac{1}{2}\%$ " | .01459 |
| 21 | Magnetite . . | { A square rod 6 sq. cms. section and 6.5 cms. long, from the Tilly Foster mines, Brewsters, Putnam County, New York, stated to be a very pure sample } | .02348 |
| 22 | Nickel . . | Soft wire | .0122 |
| 23 | " . . | { Annealed wire, calculated by Steinmetz from Ewing's experiments } | .0156 |
| 24 | " . . | Hardened, also from Ewing's experiments | .0385 |
| 25 | Cobalt . . | { Rod containing about 2% of iron, also calculated from Ewing's experiments by Steinmetz } | .0120 |
| | | { Consisted of thin needle-like chips obtained by milling grooves about 8 mm. wide across a pile of thin sheets clamped together. About 30% by volume of the specimen was iron. } | |
| 26 | Iron filings | { 1st experiment, continuous cyclic variation of m. m. f. 180 cycles per second } | .0457 |
| | | { 2d experiment, 114 cycles per second } | .0396 |
| | | { 3d " 79-91 cycles per second } | .0373 |

* "Trans. Am. Inst. Elect. Eng." January and September, 1892.

† See T. Gray, "Proc. Roy. Soc." vol. lvi.

TABLE 576.—Magnetism and Temperature, Critical Temperature

The magnetic moment of a magnet diminishes with increasing temperature. Different specimens vary widely. In the formula $Mt/M_0 = (1 - at)$ the value of a may range from .0003 to .001 (see Tables 559-560). The effect on the permeability with weak fields may at first be an increase. There is a critical temperature (Curie point) above which the permeability is very small (paramagnetic?). Diamagnetic susceptibility does not change with the temperature. Paramagnetic susceptibility decreases with increase in temperature. This and the succeeding two tables are taken from Dushman, "Theories of Magnetism," General Electric Review, 1916.

| Substance. | Critical temperature, Curie point. | Refer-ence. | Substance. | Critical temperature, Curie point. | Refer-ence. |
|---|------------------------------------|-------------|---------------------|------------------------------------|-------------|
| Iron, α form | 756° C | 1 | MnBi..... | 360 to 380° C | 4 |
| " β form | 920 | 1 | MnSb..... | 310 " 320 | 4 |
| " γ form | 1280 | 1 | MnAs..... | 45 " 50 | 4 |
| Magnetite (Fe ₃ O ₄) | 536 | 1 | MnP..... | 18 " 25 | 4 |
| " | 580 | 2 | Heusler alloy | 310 | 5 |
| " | 555 | 3 | Nickel | 340 | 1 |
| Cobalt-ferrite (Fe ₂ Co) | 520 | 3 | " | 376 | 6 |
| | | | Cobalt..... | 1075 | 6 |

References: (1) P. Curie; (2) see Williams, Electron Theory of Magnetism, quoted from Weiss; (3) du Bois, Tr. Far. Soc. 8, 211, 1912; (4) Hilpert, Tr. Far. Soc. 8, 207, 1912; (5) Gumaer; (6) Stiller, Phys. Rev. 33, 268, 1911.

TABLE 577.—Temperature Variation for Paramagnetic Substances

The relation deduced by Curie that $\chi = C/T$, where C is a constant and T the absolute temperature, holds for some paramagnetic substances over the ranges given in the following table. Many paramagnetic substances do not obey the law (Honda and Owen, Ann. d. Phys. 32, 1027, 1910; 37, 657, 1912). See the following table.

| Substance. | $C \times 10^6$ | Range ° C | Refer-ence. | Substance. | $C \times 10^6$ | Range ° C | Refer-ence. |
|----------------|-----------------|---------------|-------------|--------------------------|-----------------|-------------|-------------|
| Oxygen | 33,700 | 20° to 450° C | 1 | Gadolinium sulphate..... | 21,000 | -250° to 17 | 2 |
| Air..... | 7,830 | — | 1 | Ferrous sulphate..... | 11,000 | -259 " 17 | 2 |
| Palladium..... | 1,520 | 20 to 1370 | 1 | Ferric sulphate..... | 17,000 | -208 " 17 | 3 |
| Magnetite..... | 28,000 | 850 " 1360 | 1 | Manganese chloride..... | 30,000 | -258 " 17 | 3 |
| Cast iron..... | 38,500 | 850 " 1267 | 1 | | | | |

References: (1) P. Curie, London Electrician, 66, 500, 1912; see also Du Bois, Rap. du Cong. 2, 460, 1900; (2) Perrier, Onnes, Tables annuelles, 3, 288, 1914; (3) Oosterhuis, Onnes, l.c. 2, 389, 1913.

TABLE 578.—Temperature Effect on Susceptibility of Diamagnetic Elements

No effect:

| | | | |
|-------------------------|-----------------|------------------------|-----------------|
| B Cryst. 430 to 1200° | P white | Se — | Sb -170 to 50° |
| C Diamond, +170 to 200° | S Cryst.; ppt. | Br -170 to 18° | Cs and Au |
| C "Sugar" carbon | Zn -170 to 300° | Zr Cryst. -170 to 500° | Hg -39 to +350° |
| Si Cryst. | As — | Cd -170 to 300° | Pb 327 to 600° |

Increase with rise in Temperature:

| | | |
|-----------------------|-------------------------|-----------------|
| Be — | C Diamond, 200 to 1200° | I -170 to 114° |
| B Cryst. +170 to 400° | Ag — | Hg -170 to -30° |

Decrease with rise in Temperature:

| | | | |
|-------------------|-----------------|-----------------|-----------------|
| C Amorphous | Gd -179 to 30° | In -170 to 150° | Tl — |
| C Ceylon graphite | Ge -170 to 600° | Sb +50 to +631° | Pb -170 to 327° |
| Cu — | Zr 500 to 1200° | Te — | Bi -170 to 268° |
| Zn +300 to 700° | Cd 500 to 700° | I +114 to +200° | |

TABLE 579.—Temperature Effect on Susceptibility of Paramagnetic Elements

No effect:

| | | | |
|-----------------|----------------|-----------------|------|
| Li — | K -170 to 150° | Cr -170 to 500° | W — |
| Na -170 to 97° | Ca -170 to 18° | Mn -170 to 250° | Os — |
| Al 657 to 1100° | V -170 to 500° | Rb — | |

Increase with rise in Temperature:

| | | | |
|-----------------|------------------|------------------|----------------|
| Ti -40 to 1100° | Cr 500 to 1100° | Ru +550 to 1200° | Ba -170 to 18° |
| V 500 to 1100° | Mo -170 to 1200° | Rh — | Ir and Th |

Decrease with rise in Temperature:

| | | | |
|-----------------|-----------------|-----------------|-------------------|
| (O) — | Ti -180 to -40° | Ni 350 to 800° | Pd and Ta |
| As -170 to 657° | Mn 250 to 1015° | Co above 1150° | Pt and U |
| Mg — | (Fe) — | Cb -170 to 400° | Rare earth metals |

Tables 578 and 579 are due to Honda and Owen; for reference, see preceding table.

MAGNETIC SUSCEPTIBILITY

If \mathfrak{I} is the intensity of magnetization produced in a substance by a field strength \mathfrak{H} , then the magnetic susceptibility $\Pi = \mathfrak{I} / \mathfrak{H}$. This is generally referred to the unit mass; italicized figures refer to the unit volume. The susceptibility depends greatly upon the purity of the substance, especially its freedom from iron. The mass susceptibility of a solution containing p per cent by weight of a water-free substance is, if Π_0 is the susceptibility of water, $(p/100) \Pi + (1 - p/100) \Pi_0$.

| Substance. | $\mathfrak{H} \times 10^6$ | Temp. °C | Remarks | Substance. | $\mathfrak{H} \times 10^6$ | Temp. °C | Remarks |
|---|----------------------------|-------------|---------|--|----------------------------|-------------|---------|
| Ag | -0.19 | 18° | | K ₂ CO ₃ | -0.50 | 20° | Sol'n |
| AgCl | -0.28 | | | Li | +0.38 | | |
| Air, 1 Atm. | +0.024 | 15 | | Mo | +0.04 | 18 | |
| Al | +0.65 | 18 | | Mg | +0.55 | 18 | |
| Al ₂ K ₂ (SO ₄) ₄ 24H ₂ O | -1.0 | | Crys. | MgSO ₄ | -0.40 | | |
| A, 1 Atm. | -0.10 | 0 | | Mn | +11. | 18 | |
| As | -0.3 | 18 | | MnCl ₂ | +122. | 18 | Sol'n |
| Au | -0.15 | 18 | | MnSO ₄ | +100. | 18 | " |
| B | -0.71 | 18 | | N ₂ , 1 Atm. | 0.001 | 16 | |
| BaCl ₂ | -0.36 | 20 | | NH ₃ | -1.1 | | |
| Be | +0.79 | 15 | Powd. | Na | +0.51 | 18 | |
| Bi | -1.4 | 18 | | NaCl | -0.50 | 20 | |
| Br | -0.38 | 18 | | Na ₂ CO ₃ | -0.19 | 17 | Powd. |
| C, arc-carbon | -2.0 | 18 | | Na ₂ CO ₃ · 10 H ₂ O | -0.46 | 17 | " |
| C, diamond | -0.49 | 18 | | Nb | +1.3 | 18 | |
| CH ₄ , 1 Atm. | +0.001 | 16 | | NiCl ₂ | +40. | 18 | Sol'n |
| CO ₂ , 1 Atm. | +0.002 | 16 | | NiSO ₄ | +30. | 20 | " |
| CS ₂ | -0.77 | 18 | | O ₂ , 1 Atm. | +0.120 | 20 | |
| CaO | -0.27 | 16 | Powd. | Os | +0.04 | 20 | |
| CaCl ₂ | -0.40 | 19 | " | P, white | -0.90 | 20 | |
| CaCO ₃ , marble | -0.7 | | | P, red | -0.50 | 20 | |
| Cd | -0.17 | 18 | | Pb | -0.12 | 20 | |
| CeBr ₃ | +6.3 | 18 | | PbCl ₂ | -0.25 | 15 | Powd. |
| Cl ₂ , 1 Atm. | -0.59 | 16 | | Pd | +5.8 | 18 | |
| CoCl ₂ | +90. | 18 | Sol'n | PrCl ₃ | +13. | 18 | Sol'n |
| CoBr ₂ | +47. | 18 | " | Pt | +1.1 | 18 | |
| CoI ₂ | +33. | 18 | " | PtCl ₄ | 0.0 | 22 | Sol'n |
| CoSO ₄ | +57. | 19 | " | Rh | +1.1 | 18 | |
| Co(NO ₃) ₂ | +57. | 18 | " | S | -0.48 | 18 | |
| Cr | +3.7 | 18 | | SO ₂ , 1 Atm. | -0.30 | 16 | |
| CsCl | -0.28 | 17 | Powd. | Sb | -0.94 | 18 | |
| Cu | -0.09 | 18 | | Se | -0.32 | 18 | |
| CuCl ₂ | +12. | 20 | Sol'n | Si | -0.12 | 18 | Crys. |
| CuSO ₄ | +10. | 20 | Sol'n | SiO ₂ , Quartz | -0.44 | 20 | |
| CuS | +0.16 | 17 | Powd. | —Glass | -0.5± | | |
| FeCl ₃ | +90. | 18 | Sol'n | Sn | +0.03 | 20 | |
| FeCl ₂ | +90. | 18 | " | SrCl ₂ | -0.42 | 20 | Sol'n |
| FeSO ₄ | +82. | 20 | " | Ta | +0.93 | 18 | |
| Fe ₂ (NO ₃) ₆ | +50. | 18 | " | Te | -0.32 | 20 | |
| FeCn ₆ K ₄ | -0.44 | | Powd. | Th | +0.18 | 18 | |
| FeCn ₆ K ₃ | +9.1 | | " | Ti | +3.1 | 18 | |
| He, 1 Atm. | -0.002 | 0 | | Va | +1.5 | 18 | |
| H ₂ , 1 Atm. | 0.000 | 16 | | Wo | +0.33 | 20 | |
| H ₂ , 40 Atm. | 0.000 | 16 | | Zn | -0.15 | 18 | |
| H ₂ O | -0.79 | 20 | | ZnSO ₄ | -0.40 | | |
| HCl | -0.80 | 20 | | Zr | -0.45 | 18 | |
| H ₂ SO ₄ | +0.78 | 20 | | CH ₃ OH | -0.73 | | |
| HNO ₃ | -0.70 | 20 | | C ₂ H ₅ OH | -0.80 | | |
| Hg | -0.19 | 20 | | C ₃ H ₇ OH | -0.80 | | |
| I | -0.4 | 20 | | C ₂ H ₅ OC ₂ H ₅ | -0.60 | 20 | |
| In | 0.1± | 18 | | CHCl ₃ | -0.58 | | |
| Ir | +0.15 | 18 | | C ₆ H ₆ | -0.78 | | |
| K | +0.40 | 20 | | Ebonite | +1.1 | | |
| KCl | -0.50 | 20 | | Glycerine | -0.64 | 22 | |
| KBr | -0.40 | 20 | | Sugar | -0.57 | | |
| KI | -0.38 | 20 | | Paraffin | -0.58 | | |
| KOH | -0.35 | 22 | Sol'n | Petroleum | -0.91 | | |
| K ₂ SO ₄ | -0.42 | 20 | | Toluene | -0.77 | | |
| KMnO ₄ | +2.0 | | | Wood | -0.2-5 | | |
| KNO ₃ | -0.33 | 20 | | Xylene | -0.81 | | |

Values are mostly means taken of values given in Landolt-Börnstein's *Physikalisch-chemische Tabellen*. See especially Honda, *Annalen der Physik* (4), 32, 1910.

TABLE 581
MAGNETO-OPTIC ROTATION
GENERAL DISCUSSION

Faraday discovered that, when a piece of heavy glass is placed in magnetic field and a beam of plane polarized light passed through it in a direction parallel to the lines of magnetic force, the plane of polarization of the beam is rotated. This was subsequently found to be the case with a large number of substances, but the amount of the rotation was found to depend on the kind of matter and its physical condition, and on the strength of the magnetic field and the wave-length of the polarized light. Verdet's experiments agree fairly well with the formula—

$$\theta = cH \left(r - \lambda \frac{dr}{d\lambda} \right) \frac{r^2}{\lambda^2},$$

where c is a constant depending on the substance used, l the length of the path through the substance, H the intensity of the component of the magnetic field in the direction of the path of the beam, r the index of refraction, and λ the wave-length of the light in air. If H be different, at different parts of the path, H is to be taken as the integral of the variation of magnetic potential between the two ends of the medium. Calling this difference of potential τ , we may write $\theta = A\tau$, where A is constant for the same substance, kept under the same physical conditions, when the one kind of light is used. The constant A has been called "Verdet's constant,"* and a number of values of it are given in Tables 582-586. For variation with temperature the following formula is given by Bichat:—

$$R = R_0 (1 - 0.00104t + 0.000014t^2),$$

which has been used to reduce some of the results given in the table to the temperature corresponding to a given measured density. For change of wave-length the following approximate formula, given by Verdet and Becquerel, may be used:—

$$\frac{\theta_1}{\theta_2} = \frac{\mu_1^2(\mu_1^2 - 1)\lambda_2^2}{\mu_2^2(\mu_2^2 - 1)\lambda_1^2},$$

where μ is index of refraction and λ wave-length of light.

A large number of measurements of what has been called molecular rotation have been made, particularly for organic substances. These numbers are not given in the table, but numbers proportional to molecular rotation may be derived from Verdet's constant by multiplying in the ratio of the molecular weight to the density. The densities and chemical formulæ are given in the table. In the case of solutions, it has been usual to assume that the total rotation is simply the algebraic sum of the rotations which would be given by the solvent and dissolved substance, or substances, separately; and hence that determinations of the rotary power of the solvent medium and of the solution enable the rotary power of the dissolved substance to be calculated. Experiments by Quincke and others do not support this view, as very different results are obtained from different degrees of saturation and from different solvent media. No results thus calculated have been given in the table, but the qualitative result, as to the sign of the rotation produced by a salt, may be inferred from the table. For example, if a solution of a salt in water gives Verdet's constant less than 0.0130 at 20° C, Verdet's constant for the salt is negative.

The table has been for the most part compiled from the experiments of Verdet,† H. Becquerel,‡ Quincke,§ Koepsel,|| Arons,¶ Kundt,** Jahn,†† Schönrock,‡‡ Gordon,§§ Rayleigh and Sidgwick,||| Perkin,¶¶ Bichat.***

As a basis for calculation, Verdet's constant for carbon disulphide and the sodium line D has been taken as 0.0420 and for water as 0.0130 at 20° C.

* The constancy of this quantity has been verified through a wide range of variation of magnetic field by H. E. J. G. Du Bois (Wied. Ann. vol. 35, p. 137, 1888.
† "Ann. de Chim. et de Phys." [3] vol. 52, p. 129, 1858.
‡ "Ann. de Chim. et de Phys." [5] vol. 12; "C. R." vols. 90, p. 1407, 1880, and 100, p. 1374, 1885.
§ "Wied. Ann." vol. 24, p. 606, 1885.
|| "Wied. Ann." vol. 26, p. 456, 1885.
¶ "Wied. Ann." vol. 24, p. 161, 1885.
** "Wied. Ann." vols. 23, p. 228, 1884, and 27, p. 191, 1886.
†† "Wied. Ann." vol. 43, p. 280, 1891.
‡‡ "Zeits. für Phys. Chem." vol. 11, p. 753, 1893.
§§ "Proc. Roy. Soc." 36, p. 4, 1883.
||| "Phil. Trans. R. S." 176, p. 343, 1885.
¶¶ "Jour. Chem. Soc."
*** "Jour. de Phys." vols. 8, p. 204, 1879, and 9, p. 204 and p. 275, 1880.

MAGNETO-OPTIC ROTATION

Solids, Verdet's Constant

| Substance. | Formula. | Wave-length. | Verdet's Constant. Minutes. | Temp. C. | Authority |
|---|---|--------------|-----------------------------|----------|------------------------|
| | | μ | | | |
| Amber | | 0.589 | 0.0095 | 18-20° | Quincke. |
| Blende | ZnS | " | 0.2234 | 15 | Becquerel. |
| Diamond | C | " | 0.0127 | 15 | " |
| Lead borate | PbB ₂ O ₄ | " | 0.0600 | 15 | " |
| Selenium | Se | 0.687 | 0.4625 | 15 | " |
| Sodium borate | Na ₂ B ₄ O ₇ | 0.589 | 0.0170 | 15 | " |
| Ziqueline (Cuprite) | Cu ₂ O | 0.687 | 0.5908 | 15 | " |
| Fluorite | CaFl ₂ | 0.2534 | 0.05989 | 20 | Meyer, Ann. der |
| | | .3655 | .02526 | " | Physik, 30, 1909. |
| | | .4358 | .01717 | " | |
| | | .4916 | .01329 | " | |
| | | .589 | .00897 | " | |
| | | 1.00 | .00300 | " | |
| | | 2.50 | .00049 | " | |
| | | 3.00 | .00030 | " | |
| Glass, Jena: Medium phosphate em. | | 0.589 | 0.0161 | 18 | DuBois, Wied. Ann. |
| Heavy crown, O1143 | | " | 0.0220 | " | 51, 1894. |
| Light flint, O451 | | " | 0.0317 | " | |
| Heavy flint, O500 | | " | 0.0608 | " | |
| " " S163 | | " | 0.0888 | " | |
| Zeiss, Ultraviolet | | 0.313 | 0.0674 | 16 | Landau, Phys. ZS. |
| " | | 0.495 | .0369 | " | 9, 1908. |
| " | | 0.436 | .0311 | " | |
| Quartz, along axis, i.e., plate cut \perp to axis | SiO ₂ | 0.2194 | 0.1587 | 20 | Borel, Arch. sc. phys. |
| | | .2573 | .1079 | " | 16, 1903. |
| | | .3609 | .04617 | " | |
| | | .4800 | .02574 | " | |
| | | .5892 | .01664 | " | |
| | | .6439 | .01368 | " | |
| Rock salt | NaCl | 0.2599 | 0.2708 | 20 | Meyer, as above. |
| | | .3100 | .1561 | " | |
| | | .4046 | .0775 | " | |
| | | .4916 | .0483 | " | |
| | | .6708 | .0245 | " | |
| | | 1.00 | .01050 | " | |
| | | 2.00 | .00262 | " | |
| | | 4.00 | .00069 | " | |
| Sugar, cane: along axis IIA | C ₁₂ H ₂₂ O ₁₁ | 0.451 | 0.0122 | 20 | Voigt, Phys. ZS. 9, |
| | | .540 | .0076 | " | 1908. |
| | | .626 | .0066 | " | |
| axis IIA ¹ | - | 0.451 | 0.0129 | " | |
| | | .540 | .0084 | " | |
| | | .626 | .0075 | " | |
| Sylvite | KCl | 0.4358 | 0.0534 | 20 | Meyer, as above. |
| | | .5461 | .0316 | " | |
| | | .6708 | .02012 | " | |
| | | .90 | .01051 | " | |
| | | 1.20 | .00608 | " | |
| | | 2.00 | .00207 | " | |
| | | 4.00 | .00054 | " | |

TABLES 583 AND 584
MAGNETO-OPTIC ROTATION

TABLE 583.—Liquids, Verdet's Constant for $\lambda = 0.589\mu$

| Substance | Chemical formula | Density in grams per cm ³ | Verdet's constant in minutes | Temp. C | Authority |
|-----------------------------|---|--------------------------------------|------------------------------|---------|-------------|
| Acetone..... | C ₃ H ₆ O | 0.7947 | 0.0113 | 20° | Jahn |
| Acids: Formic..... | CH ₂ O ₂ | 1.2273 | .0105 | 15 | Perkin |
| Acetic..... | C ₂ H ₄ O ₂ | 1.0561 | .0105 | 21 | " |
| Hydrochloric..... | HCl | 1.2072 | .0224 | 15 | " |
| Hydrobromic..... | HBr | 1.7859 | .0343 | " | " |
| Hydroiodic..... | HI | 1.9473 | .0515 | " | " |
| Nitric..... | HNO ₃ | 1.5190 | .0070 | 13 | " |
| Alcohols: Methyl..... | CH ₃ OH | .7920 | .0093 | 20 | Jahn |
| Ethyl..... | C ₂ H ₅ OH | .7900 | .0112 | " | " |
| Benzene..... | C ₆ H ₆ | .8786 | .0297 | " | " |
| Bromides: Methyl..... | CH ₃ Br | 1.7331 | .0205 | 0 | Perkin |
| Ethyl..... | C ₂ H ₅ Br | 1.4486 | .0183 | 15 | " |
| Carbon bisulphide..... | CS ₂ | 1.26 | .0420 | 18 | Rayleigh |
| Chlorides: Carbon..... | CCl ₄ | 1.60 | .0321 | 15 | Becquerel |
| Chloroform..... | CHCl ₃ | 1.4823 | .0164 | 20 | Jahn |
| Ethyl..... | C ₂ H ₅ Cl | .9169 | .0138 | 6 | Perkin |
| Iodides: Methyl..... | CH ₃ I | 2.2832 | .0336 | 15 | " |
| Ethyl..... | C ₂ H ₅ I | 1.9417 | .0296 | " | " |
| Nitrates: Methyl..... | CH ₃ O.NO ₂ | 1.2157 | .0078 | " | " |
| Ethyl..... | C ₂ H ₅ O.NO ₂ | 1.1149 | .0091 | " | " |
| Paraffins: Pentane..... | C ₅ H ₁₂ | .6332 | .0118 | " | " |
| Hexane..... | C ₆ H ₁₄ | .6743 | .0125 | " | " |
| Toluene..... | C ₇ H ₈ | .8581 | .0269 | 28 | Schönrock |
| Water, = 0.2496 μ | H ₂ O | .. | .1042 | .. | See Meyer, |
| .275..... | .. | .. | .0776 | .. | Ann. der |
| .4046..... | .. | .. | .0293 | .. | Physik, 30, |
| .589..... | .. | .. | .0131 | .. | 1909 |
| 1.000..... | .. | .. | .00410 | .. | .. |
| 1.300..... | .. | .. | .00264 | .. | .. |
| Xylene..... | C ₈ H ₁₀ | .8746 | .0263 | 27 | Schönrock |

TABLE 584.—Solutions of Acids and Salts in Water. Verdet's Constant for $\lambda = 0.589\mu$

| Chemical formula | Density grams per cm ³ | Verdet's constant in minutes | Temp. C | * | Chemical formula | Density grams per cm ³ | Verdet's constant in minutes | Temp. C | * |
|---------------------------------------|-----------------------------------|------------------------------|---------|---|---|-----------------------------------|------------------------------|---------|---|
| HBr..... | 1.3775 | 0.0244 | 20° | P | Fe ₂ Cl ₆ | 1.6933 | -0.0206 | 15° | B |
| HCl..... | 1.1573 | .0204 | " | " | "..... | 1.5315 | — | .1140 | " |
| "..... | 1.0762 | .0168 | " | " | "..... | 1.1681 | — | .0015 | " |
| HI..... | 1.9057 | .0499 | " | " | "..... | 1.0864 | .0081 | " | " |
| "..... | 1.1760 | .0205 | " | " | "..... | 1.0232 | .0122 | " | " |
| HNO ₃ | 1.3560 | .0105 | " | " | HgCl ₂ | 1.0381 | .0137 | 16 | S |
| NH ₃ | .8918 | .0153 | 15 | " | NiCl ₂ | 1.4685 | .0270 | 15 | B |
| NH ₄ Br..... | 1.2805 | .0226 | " | " | "..... | 1.2432 | .0196 | " | " |
| BaBr ₂ | 1.5399 | .0215 | 20 | J | KCl..... | 1.6000 | .0163 | " | " |
| CdBr ₂ | 1.3291 | .0192 | " | " | NaCl..... | 1.0418 | .0144 | " | J |
| CaBr ₂ | 1.2491 | .0189 | " | " | SrCl ₂ | 1.1921 | .0162 | " | " |
| KBr..... | 1.1424 | .0163 | " | " | SnCl ₂ | 1.3280 | .0266 | " | V |
| "..... | 1.0876 | .0151 | " | " | ZnCl ₂ | 1.2851 | .0196 | " | " |
| NaBr..... | 1.1351 | .0165 | " | " | NH ₄ I..... | 1.5948 | .0396 | " | P |
| "..... | 1.0824 | .0152 | " | " | "..... | 1.2341 | .0235 | " | " |
| K ₂ CO ₃ | 1.1906 | .0140 | " | " | KI..... | 1.6743 | .0338 | " | B |
| Na ₂ CO ₃ | 1.1006 | .0140 | " | " | "..... | 1.1705 | .0182 | " | " |
| NH ₄ Cl..... | 1.0718 | .0178 | 15 | V | KNO ₃ | 1.0634 | .0130 | 20 | J |
| BaCl ₂ | 1.2897 | .0168 | 20 | J | NaNO ₃ | 1.1112 | .0131 | " | " |
| CdCl ₂ | 1.3179 | .0185 | " | " | U ₂ O ₃ N ₂ O ₈ | 2.0267 | .0053 | " | B |
| "..... | 1.1732 | .0160 | " | " | "..... | 1.1963 | .0115 | " | " |
| CaCl ₂ | 1.1504 | .0165 | " | " | BaSO ₄ | 1.1788 | .0134 | " | J |
| "..... | 1.0832 | .0152 | " | " | K ₂ SO ₄ | 1.0475 | .0133 | " | " |
| FeCl ₂ | 1.4331 | .0025 | 15 | B | Na ₂ SO ₄ | 1.0661 | .0135 | " | " |
| "..... | 1.1093 | .0118 | " | " | | | | | |

* P, Perkin; J, Jahn; V, Verdet; B, Becquerel; S, Schönrock; see p. 476 for references.

MAGNETO-OPTIC ROTATION

TABLE 585.—Gases, Verdet's Constant

| Substance. | Pressure. | Temp. | Verdet's constant in minutes. | Authority. |
|-----------------------------|-------------|----------|-------------------------------|------------|
| Atmospheric air | Atmospheric | Ordinary | 6.83×10^{-6} | Becquerel. |
| Carbon dioxide | " | " | 13.00 " | " |
| Carbon disulphide | 74 cms. | 70° C | 23.49 " | Bichat. |
| Ethylene | Atmospheric | Ordinary | 34.48 " | Becquerel. |
| Nitrogen | " | " | 6.92 " | " |
| Nitrous oxide | " | " | 16.90 " | " |
| Oxygen | " | " | 6.28 " | " |
| Sulphur dioxide | " | " | 31.39 " | " |
| " " | 246 cms. | 20° C | 38.40 " | Bichat. |

See also Siertsema, Ziting. Kon. Akad. Watt., Amsterdam, 7, 1899; 8, 1900.

Du Bois shows that in the case of substances like iron, nickel, and cobalt which have a variable magnetic susceptibility the expression in Verdet's equation, which is constant for substances of constant susceptibility, requires to be divided by the susceptibility to obtain a constant. For this expression he proposes the name "Kundt's constant." These experiments of Kundt and Du Bois show that it is not the difference of magnetic potential between the two ends of the medium, but the product of the length of the medium and the induction per unit area, which controls the amount of rotation of the beam.

TABLE 586.—Verdet's and Kundt's Constants

The following short table is quoted from Du Bois' paper. The quantities are stated in c. g. s. measure, circular measure (radians) being used in the expression of "Verdet's constant" and "Kundt's constant."

| Name of substance. | Magnetic susceptibility. | Verdet's constant. | | Wave-length of light in cms. | Kundt's constant. |
|-----------------------------|--------------------------|---------------------------|-------------|------------------------------|-------------------|
| | | Number. | Authority. | | |
| Cobalt | — | — | — | 6.44×10^{-5} | 3.99 |
| Nickel | — | — | — | " | 3.15 |
| Iron | — | — | — | 6.56 " | 2.63 |
| Oxygen : 1 atmo. | $+0.0126 \times 10^{-5}$ | 0.000179×10^{-5} | Becquerel. | 5.89 " | 0.014 |
| Sulphur dioxide | —0.0751 " | 0.302 " | " | " | —4.00 |
| Water | —0.0694 " | 0.377 " | Arons | " | —5.4 |
| Nitric acid | —0.0633 " | 0.356 " | Becquerel. | " | —5.6 |
| Alcohol | —0.0566 " | 0.330 " | De la Rive. | " | —5.8 |
| Ether | —0.0541 " | 0.315 " | " | " | —5.8 |
| Arsenic chloride | —0.0876 " | 1.222 " | Becquerel. | " | —14.9 |
| Carbon disulphide | —0.0716 " | 1.222 " | Rayleigh. | " | —17.1 |
| Faraday's glass | —0.0982 " | 1.738 " | Becquerel. | " | —17.7 |

TABLE 587.—Values of Kerr's Constant *

Du Bois has shown that the rotation of the major axis of vibration of radiations normally reflected from a magnet is algebraically equal to the normal component of magnetization multiplied into a constant K . He calls this constant K , Kerr's constant for the magnetized substance forming the magnet.

| Color of light. | Spectrum line. | Wave-length in cms. $\times 10^6$ | Kerr's constant in minutes per c. g. s. unit of magnetization. | | | |
|------------------|----------------|-----------------------------------|--|---------|---------|------------|
| | | | Cobalt. | Nickel. | Iron. | Magnetite. |
| Red | Li a | 67.7 | —0.0208 | —0.0173 | —0.0154 | +0.0096 |
| Red | — | 62.0 | —0.0198 | —0.0160 | —0.0138 | +0.0120 |
| Yellow | D | 58.9 | —0.0193 | —0.0154 | —0.0130 | +0.0133 |
| Green | b | 51.7 | —0.0179 | —0.0159 | —0.0111 | +0.0072 |
| Blue | F | 48.6 | —0.0180 | —0.0163 | —0.0101 | +0.0026 |
| Violet | G | 43.1 | —0.0182 | —0.0175 | —0.0089 | — |

* H. E. J. G. Du Bois, "Phil. Mag." vol. 29.

TABLE 588.—Dispersion of Kerr Effect

| Wave-length. | 0.5 μ | 1.0 μ | 1.5 μ | 2.0 μ | 2.5 μ |
|--------------|-----------|-----------|-----------|-----------|-----------|
| Steel . . . | —11'. | —16'. | —14'. | —11'. | —9'.0 |
| Cobalt . . . | —9.5 | —11.5 | —9.5 | —11. | —6.5 |
| Nickel . . . | —5.5 | —4.0 | 0 | +1.75 | +3.0 |

Field Intensity = 10,000 C. G. S. units. (Intensity of Magnetization = about 800 in steel, 700 to 800 in cobalt, about 400 in nickel). Ingersoll, Phil. Mag. 11, p. 41, 1906.

TABLE 589.—Dispersion of Kerr Effect

| Mirror. | Field (C. G. S.) | .41 μ | .44 μ | .48 μ | .52 μ | .56 μ | .60 μ | .64 μ | .66 μ |
|------------|------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| Iron . . | 21,500 | — .25 | — .26 | — .28 | — .31 | — .36 | — .42 | — .44 | — .45 |
| Cobalt . . | 20,000 | — .36 | — .35 | — .34 | — .35 | — .35 | — .35 | — .35 | — .36 |
| Nickel . . | 19,000 | — .16 | — .15 | — .13 | — .13 | — .14 | — .14 | — .14 | — .14 |
| Steel . . | 19,200 | — .27 | — .28 | — .31 | — .35 | — .38 | — .40 | — .44 | — .45 |
| Invar . . | 19,800 | — .22 | — .23 | — .24 | — .23 | — .23 | — .22 | — .23 | — .23 |
| Magnetite | 16,400 | — .07 | — .02 | + .04 | + .06 | + .08 | + .06 | + .04 | + .03 |

Foote, Phys. Rev. 34, p. 96, 1912.

See also Ingersoll, Phys. Rev. 35, p. 312, 1912, for "The Kerr Rotation for Transverse Magnetic Fields," and Snow, l. c. 2, p. 29, 1913, "Magneto-optical Parameters of Iron and Nickel."

RESISTANCE OF METALS. MAGNETIC EFFECTS

TABLE 590.—Temperature Variation of Resistance of Bismuth, Transverse Magnetic Field

| Proportional Values of Resistance. | | | | | | | | | |
|------------------------------------|-------|-------|-------|------|------|------|------|-------|-------|
| H | -192° | -135° | -100° | -37° | 0° | +18° | +60° | +100° | +183° |
| 0 | 0.40 | 0.60 | 0.70 | 0.88 | 1.00 | 1.08 | 1.25 | 1.42 | 1.79 |
| 2000 | 1.16 | 0.87 | 0.86 | 0.90 | 1.08 | 1.11 | 1.26 | 1.43 | 1.80 |
| 4000 | 2.32 | 1.35 | 1.20 | 1.10 | 1.18 | 1.21 | 1.31 | 1.46 | 1.82 |
| 6000 | 4.00 | 2.06 | 1.60 | 1.29 | 1.30 | 1.32 | 1.39 | 1.51 | 1.85 |
| 8000 | 5.90 | 2.88 | 2.00 | 1.50 | 1.43 | 1.42 | 1.46 | 1.57 | 1.87 |
| 10000 | 8.60 | 3.80 | 2.43 | 1.72 | 1.57 | 1.54 | 1.54 | 1.62 | 1.89 |
| 12000 | 10.8 | 4.76 | 2.93 | 1.94 | 1.71 | 1.67 | 1.62 | 1.67 | 1.92 |
| 14000 | 12.9 | 5.82 | 3.50 | 2.16 | 1.87 | 1.80 | 1.70 | 1.73 | 1.94 |
| 16000 | 15.2 | 6.95 | 4.11 | 2.38 | 2.02 | 1.93 | 1.79 | 1.80 | 1.96 |
| 18000 | 17.5 | 8.15 | 4.76 | 2.60 | 2.18 | 2.06 | 1.88 | 1.87 | 1.99 |
| 20000 | 19.8 | 9.50 | 5.40 | 2.81 | 2.33 | 2.20 | 1.97 | 1.95 | 2.03 |
| 25000 | 25.5 | 13.3 | 7.30 | 3.50 | 2.73 | 2.52 | 2.22 | 2.10 | 2.09 |
| 30000 | 30.7 | 18.2 | 9.8 | 4.20 | 3.17 | 2.86 | 2.46 | 2.28 | 2.17 |
| 35000 | 35.5 | 20.35 | 12.2 | 4.95 | 3.62 | 3.25 | 2.69 | 2.45 | 2.25 |

TABLE 591.—Increase of Resistance of Nickel due to a Transverse Magnetic Field, expressed as % of Resistance at 0° and H=0

| H | -190° | -75° | 0° | +18° | +100° | +182° |
|-------|-------|-------|-------|-------|-------|-------|
| 0 | +0 | 0 | 0 | 0 | 0 | 0 |
| 1000 | +0.20 | +0.23 | +0.07 | +0.07 | +0.06 | +0.04 |
| 2000 | +0.17 | +0.16 | +0.03 | +0.03 | +0.72 | -0.07 |
| 3000 | 0.00 | -0.05 | -0.34 | -0.36 | -0.14 | -0.60 |
| 4000 | -0.17 | -0.15 | -0.60 | -0.72 | -0.70 | -1.15 |
| 6000 | -0.19 | -0.20 | -0.70 | -0.83 | -1.02 | -1.53 |
| 8000 | -0.19 | -0.23 | -0.76 | -0.90 | -1.15 | -1.66 |
| 10000 | -0.18 | -0.27 | -0.82 | -0.95 | -1.23 | -1.76 |
| 12000 | -0.18 | -0.30 | -0.87 | -1.00 | -1.30 | -1.85 |
| 14000 | -0.18 | -0.32 | -0.91 | -1.04 | -1.37 | -1.95 |
| 16000 | -0.17 | -0.35 | -0.94 | -1.09 | -1.44 | -2.05 |
| 18000 | -0.17 | -0.38 | -0.98 | -1.13 | -1.51 | -2.15 |
| 20000 | -0.16 | -0.41 | -1.03 | -1.17 | -1.59 | -2.25 |
| 25000 | -0.14 | -0.49 | -1.12 | -1.29 | -1.76 | -2.50 |
| 30000 | -0.12 | -0.56 | -1.22 | -1.40 | -1.95 | -2.73 |
| 35000 | -0.10 | -0.63 | -1.32 | -1.50 | -2.13 | -2.98 |

F. C. Blake, Ann. der Physik, 28, p. 449; 1909.

TABLE 592.—Change of Resistance of Various Metals in a Transverse Magnetic Field. Room Temperature

| Metal. | Field Strength in Gauss. | Per cent Increase. | Authority. |
|--------------|---|--------------------|-------------------------------------|
| Nickel | 10000 | -1.2 | Williams, Phil. Mag. 9, 1905. |
| " | " | -1.4 | Barlow, Pr. Roy. Soc. 71, 1903. |
| " | 6000 | -1.0 | Dagostino, Atti Ac. Linc. 17, 1908. |
| " | 10000 | -1.4 | Grummach, Ann. der Phys. 22, 1906. |
| Cobalt | " | -0.53 | " |
| Cadmium | " | +0.03 | " |
| Zinc | " | +0.01 | " |
| Copper | " | +0.004 | " |
| Silver | " | +0.004 | " |
| Gold | " | +0.003 | " |
| Tin | " | +0.002 | " |
| Palladium | " | +0.001 | " |
| Platinum | " | +0.0005 | " |
| Lead | " | +0.0004 | " |
| Tantalum | " | +0.0003 | " |
| Magnesium | 6000 | +0.01 | Dagostino, l. c. |
| Manganin | " | +0.01 | " |
| Tellurium | ? | +0.02 to 0.34 | Goldhammer, Wied Ann. 31, 1887. |
| Antimony | ? | +0.02 to 0.16 | " |
| Iron | Different specimens show very diverse results, usually an increase in weak fields, a decrease in strong. Alloys behave similarly to iron. | | Grummach, l. c. |
| Nickel steel | | | Barlow, l. c. Williams, l. c. |
| | | | Williams, l. c. |

TABLE 593.—Transverse Galvanomagnetic and Thermomagnetic Effects

Effects are considered positive when, the magnetic field being directed away from the observer, and the primary current of heat or electricity directed from left to right, the upper edge of the specimen has the higher potential or higher temperature.

E = difference of potential produced; T = difference of temperature produced; I = primary current; $\frac{dt}{dx}$ = primary temperature gradient; B = breadth, and D = thickness, of specimen H = intensity of field. C. G. S. units.

Hall effect (Galvanomagnetic difference of Potential), $E = R \frac{HI}{D}$

Ettingshausen effect (" " " Temperature), $T = P \frac{HI}{D}$

Nernst effect (Thermomagnetic " " Potential), $E = QHB \frac{dt}{dx}$

Leduc effect (" " " Temperature), $T = SHB \frac{dt}{dx}$

| Substance. | Values of R . | $P \times 10^6$. | $Q \times 10^6$. | $S \times 10^6$. |
|-------------------------|---------------------|-------------------|-------------------|-------------------|
| Tellurium | +400 to 800 | +200 | +360000 | +400 |
| Antimony | +0.9 " 0.22 | +2 | +9000 to 18000 | +200 |
| Steel | +0.012 " 0.033 | -0.07 | -700 " 1700 | +69 |
| Heusler alloy | +0.010 " 0.026 | - | +1600 " 7000 | - |
| Iron | +0.007 " 0.011 | -0.06 | -1000 " 1500 | +39 |
| Cobalt | +0.0016 " 0.0046 | +0.01 | +1800 " 2240 | +13 |
| Zinc | - | - | -54 " 240 | +13 |
| Cadmium | +0.0055 | - | - | - |
| Iridium | +0.00040 | - | up to -5.0 | +5 |
| Lead | +0.00009 | - | -5.0 (?) | - |
| Tin | -0.00003 | - | -4.0 (?) | - |
| Platinum | -0.0002 | - | - | -2 |
| Copper | -0.00052 | - | -90 to 270 | -18 |
| German silver | -0.00054 | - | - | - |
| Gold | -0.00057 to 0.00071 | - | - | - |
| Constantine | -0.0009 | - | - | - |
| Manganese | -0.00093 | - | - | - |
| Palladium | -0.0007 to 0.0012 | - | +50 to 130 | -3 |
| Silver | -0.0008 " 0.0015 | - | -46 " 430 | -41 |
| Sodium | -0.0023 | - | - | - |
| Magnesium | -0.00094 to 0.0035 | - | - | - |
| Aluminum | -0.00036 " 0.0037 | - | - | - |
| Nickel | -0.0045 " 0.024 | +0.04 to 0.19 | +2000 " 9000 | -45 |
| Carbon | -0.017 | +5. | +100 | - |
| Bismuth | up to 16. | +3 to 40 | + up to 132000 | -200 |

TABLE 594.—Variation of Hall Constant with the Temperature

| Bismuth. ¹ | | | | | | Antimony. ² | | | | |
|-----------------------|--------|-------|------|--------|-------|------------------------|-------|-------|--------|-------|
| H | -182° | -90° | -23° | +11.5° | +100° | H | -186° | -79° | +21.5° | +58° |
| 1000 | 62.2 | 28.0 | 17.0 | 13.3 | 7.28 | 1750 | 0.263 | 0.249 | 0.217 | |
| 2000 | 55.0 | 25.0 | 16.0 | 12.7 | 7.17 | 3960 | 0.252 | 0.243 | 0.211 | |
| 3000 | 49.7 | 22.9 | 15.1 | 12.1 | 7.06 | 6160 | 0.245 | 0.235 | 0.209 | 0.203 |
| 4000 | 45.8 | 21.5 | 14.3 | 11.5 | 6.95 | | | | | |
| 5000 | 42.6 | 20.2 | 13.6 | 11.0 | 6.84 | | | | | |
| 6000 | 40.1 | 18.9 | 12.9 | 10.6 | 6.72 | | | | | |
| Bismuth. ³ | | | | | | | | | | |
| H | +14.5° | +104° | 125° | 189° | 212° | 239° | 259° | 269° | | 270° |
| 890 | 5.28 | 2.57 | 2.12 | 1.42 | 1.24 | 1.11 | 0.97 | 0.83 | | 0.77* |

¹ Barlow, Ann. der Phys. 12, 1903.³ Traubenberg, Ann. der Phys. 17, 1905.² Everdingen, Comm. Phys. Lab. Leiden, 58.

* Melting-point.

Both tables taken from Jahn, Jahrbuch der Radioaktivität und Elektronik, 5, p. 166; 1908, who has collected data of all observers and gives extensive bibliography.

TABLE 595

INTERNATIONAL ATOMIC WEIGHTS, ATOMIC NUMBERS AND VALENCIES

Quoted from the 1st Report of the Committee on Atomic Weights of the International Union of Chemistry (Journ. Amer. Chem. Soc., 3, 1637, 1931).

| Element | Symbol and atomic number | Relative atomic weight oxygen = 16 | Valencies | Element | Symbol and atomic number | Relative atomic weight oxygen = 16 | Valencies |
|---------------|--------------------------|------------------------------------|-----------|---------------|--------------------------|------------------------------------|-----------|
| Aluminum.... | Al 13 | 26.97 | 3 | Molybdenum... | Mo 42 | 96.0 | 4, 6 |
| Antimony.... | Sb 51 | 121.76 | 3, 5 | Neodymium... | Nd 60 | 144.27 | 3 |
| Argon..... | A 18 | 39.944 | 0 | Neon..... | Ne 10 | 20.183 | 0 |
| Arsenic..... | As 33 | 74.93 | 3, 5 | Nickel..... | Ni 28 | 58.69 | 2, 3 |
| Barium..... | Ba 56 | 137.36 | 2 | Nitrogen..... | N 7 | 14.008 | 3, 5 |
| Beryllium.... | Be 4 | 9.02 | 2 | Osmium..... | Os 76 | 190.8 | 6, 8 |
| Bismuth..... | Bi 83 | 209.00 | 3, 5 | Oxygen..... | O 8 | 16.0000 | 2 |
| Boron..... | B 5 | 10.82 | 3 | Palladium.... | Pd 46 | 106.7 | 2, 4 |
| Bromine..... | Br 35 | 79.916 | 1 | Phosphorus... | P 15 | 31.02 | 3, 5 |
| Cadmium..... | Cd 48 | 112.41 | 2 | Platinum..... | Pt 78 | 195.23 | 2, 4 |
| Calcium..... | Ca 20 | 40.08 | 2 | Potassium.... | K 19 | 39.10 | 1 |
| Carbon..... | C 6 | 12.000 | 4 | Praseodymium | Pr 59 | 140.92 | 3 |
| Cerium..... | Ce 58 | 140.13 | 3, 4 | Radium..... | Ra 88 | 225.97 | 2 |
| Cesium..... | Cs 55 | 132.81 | 1 | Radon..... | Rn 86 | 222 | 0 |
| Chlorine..... | Cl 17 | 35.457 | 1 | Rhenium..... | Re 75 | 186.31 | .. |
| Chromium.... | Cr 24 | 52.01 | 2, 3, 6 | Rhodium..... | Rh 45 | 102.91 | 3 |
| Cobalt..... | Co 27 | 58.94 | 2, 3 | Rubidium.... | Rb 37 | 85.44 | 1 |
| Columbium... | Cb 41 | 93.3 | 5 | Ruthenium... | Ru 44 | 101.7 | 6, 8 |
| Copper..... | Cu 29 | 63.57 | 1, 2 | Samarium.... | Sm 62 | 150.43 | 3 |
| Dysprosium... | Dy 66 | 162.46 | 3 | Scandium.... | Sc 21 | 45.10 | 3 |
| Erbium..... | Er 68 | 167.64 | 3 | Selenium..... | Se 34 | 79.2 | 2, 4, 6 |
| Europium.... | Eu 63 | 152.0 | 3 | Silicon..... | Si 14 | 28.06 | 4 |
| Fluorine..... | F 9 | 19.00 | 1 | Silver..... | Ag 47 | 107.880 | 1 |
| Gadolinium... | Gd 64 | 157.3 | 3 | Sodium..... | Na 11 | 22.997 | 1 |
| Gallium..... | Ga 31 | 69.72 | 3 | Strontium.... | Sr 38 | 87.63 | 2 |
| Germanium... | Ge 32 | 72.60 | 4 | Sulphur..... | S 16 | 32.06 | 2, 4, 6 |
| Gold..... | Au 79 | 197.2 | 1, 3 | Tantalum.... | Ta 73 | 181.4 | 5 |
| Hafnium..... | Hf 72 | 178.6 | .. | Tellurium.... | Te 52 | 127.5 | 2, 4, 6 |
| Helium..... | He 2 | 4.002 | 0 | Terbium..... | Tb 65 | 159.2 | 3 |
| Holmium..... | Ho 67 | 163.5 | 3 | Thallium.... | Tl 81 | 204.39 | 1, 3 |
| Hydrogen.... | H 1 | 1.0078 | 1 | Thorium..... | Th 90 | 232.12 | 4 |
| Indium..... | In 49 | 114.8 | 3 | Thulium..... | Tm 69 | 169.4 | 3 |
| Iodine..... | I 53 | 126.932 | 1 | Tin..... | Sn 50 | 118.70 | 2, 4 |
| Iridium..... | Ir 77 | 193.1 | 4 | Titanium.... | Ti 22 | 47.90 | 4 |
| Iron..... | Fe 26 | 55.84 | 2, 3 | Tungsten.... | W 74 | 184.0 | 6 |
| Krypton..... | Kr 36 | 82.9 | 0 | Uranium..... | U 92 | 238.14 | 4, 6 |
| Lanthanum... | La 57 | 138.90 | 3 | Vanadium.... | V 23 | 50.95 | 3, 5 |
| Lead..... | Pb 82 | 207.22 | 2, 4 | Xenon..... | Xe 54 | 130.2 | 0 |
| Lithium..... | Li 3 | 6.940 | 1 | Ytterbium... | Yb 70 | 173.5 | 3 |
| Lutecium.... | Lu 71 | 175.0 | 3 | Yttrium..... | Y 39 | 88.92 | 3 |
| Magnesium... | Mg 12 | 24.32 | 2 | Zinc..... | Zn 30 | 65.38 | 2 |
| Manganese... | Mn 25 | 54.93 | 2, 3, 7 | Zirconium.... | Zr 40 | 91.22 | 4 |
| Mercury..... | Hg 80 | 200.61 | 1, 2 | | | | |

ISOTOPES. PACKING FRACTIONS

(See Table 851)

This table contains several sets of values. Those followed directly by figures in parentheses, e.g., Sn, 118.72 (-7.13 ± 2), taken from Aston, Proc. Roy. Soc., 115A, 487, 1927, give first the atomic mass referred to oxygen ($O_{16} + O_{17}$) determined by the mass spectroscopy and often of greater probable accuracy than the corresponding atomic weight determination (see Birge, p. 81 ff.). The figures following in parentheses are "packing fractions". The protons and electrons are so closely packed that their electromagnetic fields interfere and a certain fraction of the combined mass is destroyed. The mass destroyed corresponds to energy released. The greater this is the more tightly are the charges cemented and the more stable the nucleus. The "fraction" measures the divergence from the "whole number" rule divided by the mass number, expressed in parts per 10,000. The numbers in braces are ordinary atomic weights from page 483. Numbers in brackets are % abundance. The other numbers are the nearest whole numbers to the mass of the corresponding isotope. Aston, Philos. Mag., 49, 1199, 1925. See page 486 for the radioactive isotopes.

| | | | | |
|----|----|----|--|-----------------------|
| H | 1 | 2 | 1.00778(77.8 \pm 1.5) | Abundance of 2, 1/800 |
| He | 2 | 1 | 4.00216(5.4 \pm 1) | |
| Li | 3 | 2 | 6.012(20.0 \pm 3), 7.012(17.0 \pm 3) | |
| Be | 4 | 1 | [9.02] (Aston) | |
| B | 5 | 2 | 10.0135(13.5 \pm 1.5), 11.0110(10.0 \pm 1.5) | |
| C | 6 | 2 | 12.0036(3.0 \pm 1), 13 (Birge, 1929) [Relative abundance, 400-1] | |
| N | 7 | 1 | 14.008(5.7 \pm 2), 15 (Naudé, 1929) [Relative abundance, 700-1] | |
| O | 8 | 2 | 16.0000, 17, 18, (Giauque, Johnston, 1929)[Abundance $O_{16}/O_{17} = 8600$, $O_{16}/O_{18} = 1100$] | |
| F | 9 | 1 | 19.000(0.0 \pm 1) | |
| Ne | 10 | 2 | 20.0004(0.2 \pm 1), 22.0048(2.2?) | |
| Na | 11 | 1 | [22.997] (Aston) | |
| Mg | 12 | 3 | 24, 25, 26 (Dempster) | |
| Al | 13 | 1 | [26.97] (Aston) | |
| Si | 14 | 3 | 28, 29, 30 (Aston) | |
| P | 15 | 1 | 30.9825(-5.6 \pm 1.5) | |
| S | 16 | 3 | 32, 97% of whole; 34, 33 (Aston) | |
| Cl | 17 | 2 | 34.983(-4.8 \pm 1.5), 36.980(-5.0 \pm 1.5) | |
| A | 18 | 2 | 39.971(-7.2 \pm 1), 35.976(-6.6 \pm 5), 1% of whole | |
| K | 19 | 2 | 39, 41 (Aston) | |
| Ca | 20 | 2? | 40, 44? (Dempster) | |
| Sc | 21 | 1 | [45.10] (Aston) | |
| Ti | 22 | 1 | [47.90] (Aston) | |
| V | 23 | 1 | [50.96] (Aston) | |
| Cr | 24 | 4 | [52.011] 52(-10)[82], 53[10], 50[5], 54[3], Aston, 1930 | |
| Mn | 25 | 1 | [54.93] (Aston) | |
| Fe | 26 | 2? | 56, 54? (Aston) | |
| Ni | 28 | 2 | 58, 60 (Aston) | |
| Zn | 30 | 4 | [65.380] (-9.0), 64[48], 66[26], 68[17], 65[2], 67[5], 69[1], 70[0.4] | |
| As | 33 | 1 | 74.934(-8.8 \pm 1.5) | |
| Se | 34 | 6 | 80, 78, 76, 82, 77, 74 (Aston) | |
| Br | 35 | 2 | 78.929(-9.0 \pm 1.5), 80.926(-8.6 \pm 1.5) | |
| Kr | 36 | 6 | 83.928(-8.5 \pm 2)[57], 85.929(-8.2 \pm 1.5)[17], 81.927(-8.8 \pm 1.5)[12] 82.927(-8.17 \pm 1.5)[12], 79.926(-9.4 \pm 2)[2], 77.926(-9.4 \pm 2)[1.4] | |
| Rb | 37 | 2 | 85, 87 (Aston) | |
| Sr | 38 | 2 | 88, 86 (Aston) | |
| Yt | 39 | 1 | [88.92] (Aston) | |
| Zr | 40 | 3 | [91.22] (Aston) | |
| Mo | 42 | 7 | 95.97(-5.5), 98(-5.5)[23], 96[18], 95[15], 92[14], 94[10], 100(-5.5)[10], 97[10] | |
| Ru | 44 | 7 | 102[30], 101[22], 104[17], 100[14], 99[12], 96[5], 98?, (Aston, 1931) | |
| In | 49 | 1 | [114.8] (Aston) | |
| Sn | 50 | 11 | 118.72(-7.3 \pm 2), 120[27.0], 118[21], 116[14.1], 124[6.2], 119[11.0], 117[0.8], 122[5.0], 121[3.0], 112[1.1], 114[.7], 115[0.4] (Probably all the same packing fraction.) | |
| Sb | 51 | 2 | 121, 123 (Aston) | |
| Te | 52 | 3 | 128, 130, 126 (Aston) | |
| I | 53 | 1 | 126.932(-5.13 \pm 2) | |
| Xe | 54 | 9 | 131.27(-5.3), 129[27.1], 132[26.4], 131[20.7], 134[10.3], 136[8.8], 130[4.2], 128[2.3] 126[.1], 124[.1] (Probably all the same packing fraction.) | |
| Cs | 55 | 1 | [132.81] (Aston) | |
| Pr | 59 | 1 | [140.92] (Aston) | |
| Nd | 60 | 3 | 142, 144, 146, (145) (Aston) | |
| Os | 76 | 6 | 190.31(-1.0 \pm 2.0), 192[42.6], 190[25.1], 189[17.3], 188[13.5], 186[1.0], 187[0.6] (Aston, 1931) | |
| Hg | 80 | 6 | 200.62(+.08), 202[29.27], 200[23.77], 199[16.4], 198[10], 201[13.7], 204[6.8], 196[.1] (All same packing fraction.) | |
| Tl | 81 | 8 | 207, 205, 211, 203, 201, 209, 213, 215, Goslin, Allison | |
| U | 92 | 8 | 238, 239, 240, 234, 237, 235, 233, 236, Goslin, Allison | |

Corrections (Nature 192, 477, Mar. 26, 1932.

Kr 83.7, Xe 131.3.

Calculation of atomic weights from mass spectra leads to the following: (O = 16): Ratio isotopes O_{16} :

$O_{18}/O_{17}::630:10.2$.

Li 6.923, Cs 132.91, B 10.806, Ge 72.65, Se 78.96, Te 128.03, W 183.96, Br 79.916, Re 186.22, Ru 101.1,

Os 190.31.

For isotopes of Pb (201 to 216), Bi (205 to 217, 219), Ra (226, 228, 230, 232), Th (229 to 236); Bishop, Lawrenz, Dollins, Allison, Goslin, Phys. Rev. 43, 1933.

TABLE 597.—Periodic System of the Elements

| O | I | II | III | IV | V | VI | VII | |
|-------------|------------------|-----------|-------------------------------|-----------------|-------------------------------|-----------------|-------------------------------|--|
| — | R ₂ O | RO | R ₂ O ₃ | RO ₂ | R ₂ O ₅ | RO ₃ | R ₂ O ₇ | RO ₄ and Oxides. |
| — | — | — | — | RH ₄ | RH ₃ | RH | RH | — and Hydrides. |
| He 4 | Li 7 | Gl 9 | B 11 | C 12 | N 14 | O 16 | F 19 | — |
| Ne 20 | Na 23 | Mg 24 | Al 27 | Si 28 | P 31 | S 32 | Cl 35 | — |
| A 40 | K 39 | Ca 40 | Sc 44 | Ti 48 | V 51 | Cr 52 | Mn 55 | Fe 56 Ni 59 Co 59 |
| — | Cu 64 | Zn 65 | Ga 70 | Ge 72 | As 75 | Se 79 | Br 80 | — |
| Kr 82 | Rb 85 | Sr 88 | Yt 89 | Zr 91 | Cb 94 | Mo 96 | — | Ru 102 Rh 103 Pd 107 |
| — | Ag 108 | Cd 112 | In 115 | Sn 119 | Sb 120 | Te 128 | I 127 | — |
| X 128 | Cs 133 | Ba 137 | La 139 | Ce 140 | Pr 141 | Nd 144 | — | — |
| — | Sa 150 | Eu 152 | Gd 157 | Tb 159 | Ds 162 | Er 163 | — | — |
| — | Tm 168 | Yb 174 | Lu 175 | — | Ta 181 | W 184 | — | Os 191 Ir 193 Pt 195 |
| — | Au 197 | Hg 201 | Tl 204 | Pb 207 | Bi 208 | Po 210 | — | — |
| Em (222) | — | Ra 226 | Ac (227) | Th 232 | Ux ₂ 234 | U 238 | — | — |

TABLE 598.—Atomic Numbers

| | | | | |
|---------------|--------------|---------------|-----------------|-----------------|
| 1 Hydrogen | 20 Calcium | 39 Yttrium | 58 Cerium | 76 Osmium |
| 2 Helium | 21 Scandium | 40 Zirconium | 59 Praseodymium | 77 Iridium |
| 3 Lithium | 22 Titanium | 41 Niobium † | 60 Neodymium | 78 Platinum |
| 4 Beryllium † | 23 Vanadium | 42 Molybdenum | 61 Illinium | 79 Gold |
| 5 Boron | 24 Chromium | 43 Massium | 62 Samarium | 80 Mercury |
| 6 Carbon | 25 Manganese | 44 Ruthenium | 63 Europium | 81 Thallium |
| 7 Nitrogen | 26 Iron | 45 Rhodium | 64 Gadolinium | 82 Lead |
| 8 Oxygen | 27 Cobalt | 46 Palladium | 65 Terbium | 83 Bismuth |
| 9 Fluorine | 28 Nickel | 47 Silver | 66 Dysprosium | 84 Polonium |
| 10 Neon | 29 Copper | 48 Cadmium | 67 Holmium | 85 Alabamine |
| 11 Sodium | 30 Zinc | 49 Indium | 68 Erbium | 86 Radon |
| 12 Magnesium | 31 Gallium | 50 Tin | 69 Thulium | 87 Virginium |
| 13 Aluminum | 32 Germanium | 51 Antimony | 70 Ytterbium | 88 Radium |
| 14 Silicon | 33 Arsenic | 52 Tellurium | 71 Lutecium | 89 Actinium |
| 15 Phosphorus | 34 Selenium | 53 Iodine | 72 Hafnium | 90 Thorium |
| 16 Sulphur | 35 Bromine | 54 Xenon | 73 Tantalum | 91 Protactinium |
| 17 Chlorine | 36 Krypton | 55 Cesium | 74 Tungsten * | 92 Uranium |
| 18 Argon | 37 Rubidium | 56 Barium | | |
| 19 Potassium | 38 Strontium | 57 Lanthanum | | |

* Bohemium

† Glucinium.

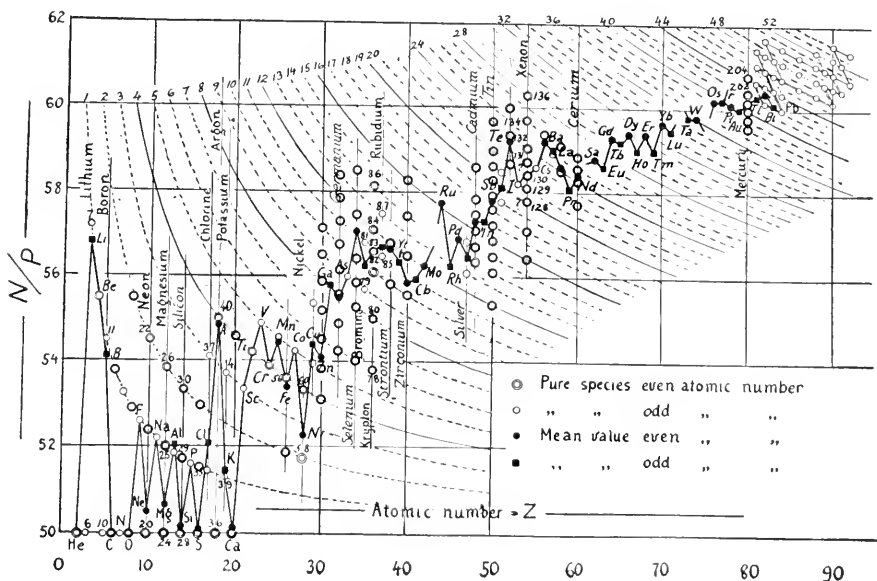
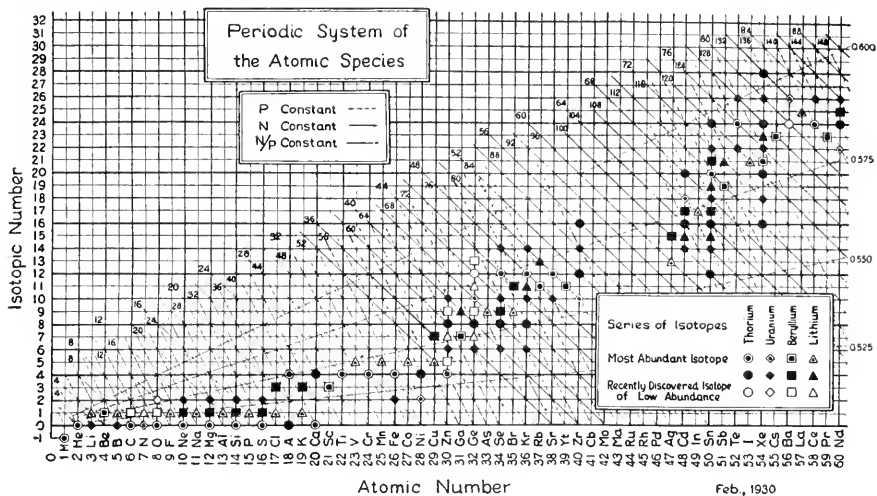
‡ Columbium.

ATOMIC STRUCTURE

(Harkins, Science, 70, 433, 463, 1929.)

If weight of proton (p) + electron (e) = 1, atomic wt. = no. of protons + electrons in atom. $(pe)_{\text{av}}$ = composition of complete atom, atomic weight (av). P , no. of protons in atom, = W . N = total number electrons in nucleus; $P - N = Z$ = atomic number. $2N - P$ = isotopic number; electronic number = no. electrons.

The structure of the loosely bound nonnuclear electrons decides various chemical and physical properties. The tightly bound nuclear atoms should produce periodic properties. Abundance of atomic species reveals nuclear stability (possibility of other factors). High stability shown by abundance of even electronic numbers. Species of odd electronic number are so rare that only four have been discovered. There is high stability for isotopic numbers divisible by 4, a secondary stability when by 2. When N and P even, Z odd, earth's crust 87.4%; meteorites, 95.4; when N even, P , Z odd, 10.8, 2.1; Z even, P , N odd, 1.8, 2.5; P even, N , Z odd, 0.0007, 0.0. Lower left-hand rectangle of lower figure constitutes 99.9% of all known material.



ELECTRON CONFIGURATIONS IN NORMAL ATOM

Individual electrons in an atom may be designated by two quantum numbers, "azimuthal" and "total". The first is expressed by s, p, d, etc.; the last numerically in specific cases, by n in general.

Designation of quantum numbers:

Azimuth quantum: literal, s; number, o; Bohr, k, 1; The total quantum number is equal to

| | | | |
|--------|---|---|---------------------------------------|
| p | 1 | 2 | or greater than 1 + 1, i.e., 1, 2, 3, |
| d | 2 | 3 | — for s electrons, 2, 3, 4,— for p |
| f | 3 | 4 | electrons, etc. |
| g | 4 | 5 | |
| h etc. | 5 | 6 | |

An electron is called, e.g., a 6p electron, 6 for the total quantum number, p implying an l value of 1. Note that 4p, 5s, 3d, etc., electrons are equivalent to Bohr's 4₂, 5₁, 3₃ electrons. The number of electrons for a given type in an atom may be expressed by an exponent, e.g., 3d⁵. For more detailed connection between configurations and spectroscopic terms see Hund's book. The lower-case letters n, l, s, j, m should be used for the quantum numbers of an electron, and the capitals L, S, J, M for the quantum numbers of a term (or level) of an atom, ionized or neutral. A specification of atomic structure would include all the inner electrons, e.g., for Fe in its normal state 1s²2s²2p⁶3s²3p⁶3d⁶4s². For short only those electrons "outside" an inert gas shell need be considered. A complete np⁶ group, and all the groups which are normally completed earlier in the periodic table, can be neglected. Thus the notation for the normal state of Fe becomes 3d⁶4s².

Examples of the notation for a level and the configuration from which it arises is 3d⁶ 4s² ⁵D₄, the normal state of the iron atom; 2s² 2p³ ⁴S_{1/2}, the low level of O II. The total quantum numbers may be omitted when they are the lowest which the particular sort of electron can have if not belonging to already completed shells. For example, 4s, 4p, 3d, 4f in spectra from K I to Zn I and Ca II to Ga II, etc., are the s, p, d, and f electrons of lowest quantum numbers not belonging to completed groups. The 3p⁶ group is completed and the 3s² and all the groups of smaller n have been previously completed, leaving 4s, 4p, 3d, 4f still to be added. These last can therefore be represented by s, p, d and f.

The normal state of Fe I would thus be designated as d⁶s² ⁵D₄, that of O II as s²p³ ⁴S_{1/2}. For Ge I, in which the electron groups 3d¹⁰ and 4s² may be regarded as completed, the electrons to be represented by the letters alone would be the 5s, 4p, 4d, and 4f electrons; and so on.

Odd terms arise when the sum of the l values for all electrons is odd, even terms from configurations for which the l sum is even. Since the l sum for completed groups is always even, only outer uncompleted groups need be considered. Even (odd) terms are those in which the number of p and f electrons together is even (odd). In the parts of the periodic table where s and d groups are being completed the lowest terms of all the atoms are even. Where p groups are being completed (and also in the rare earth f-group) the lowest terms are alternately odd and even. Except in the rare earth group the only spectra for which the normal state corresponds to an odd term are B I, N I, F I and C II, O II, Ne II etc. and the homologous spectra in later periods.

Permitted transitions are those in which the l of one electron changes by one unit, (and the l of another electron by 0 or 2 units, if two electrons change) so that all such transitions are between even and odd terms.

Electron Configurations¹

| Ele- ment | K | L | | M | | | N | | | | O | | | Nor- mal term | Atomic No. |
|--------------|------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------------------------------|---------------|
| | 1,0 | 2,0 | 2,1 | 3,0 | 3,1 | 3,2 | 4,0 | 4,1 | 4,2 | 4,3 | 5,0 | 5,1 | 5,2 | | |
| | 1s | 2s | 2p | 3s | 3p | 3d | 4s | 4p | 4d | 4f | 5s | 5p | 5d | | |
| H | 1 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | ² S _{1/2} | 1 |
| He | 2 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | ¹ S ₀ | 2 |
| Li | 2 | 1 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | ² S _{1/2} | 3 |
| Be | 2 | 2 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | ¹ S ₀ | 4 |
| B | 2 | 2 | 1 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | ² P _{1/2} | 5 |
| C | 2 | 2 | 2 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | ³ P ₀ | 6 |
| N | 2 | 2 | 3 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | ⁴ S _{3/2} | 7 |
| O | 2 | 2 | 4 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | ³ P ₂ | 8 |
| F | 2 | 2 | 5 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | ² P _{3/2} | 9 |
| Ne | 2 | 2 | 6 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | ¹ S ₀ | 10 |
| Na | Same as for neon | | | 1 | .. | .. | .. | .. | .. | .. | .. | .. | .. | ² S _{1/2} | 11 |
| Mg | " | | | 2 | .. | .. | .. | .. | .. | .. | .. | .. | .. | ¹ S ₀ | 12 |
| Al | " | | | 2 | 1 | .. | .. | .. | .. | .. | .. | .. | .. | ² P _{1/2} | 13 |
| Si | " | | | 2 | 2 | .. | .. | .. | .. | .. | .. | .. | .. | ³ P ₀ | 14 |
| P | " | | | 2 | 3 | .. | .. | .. | .. | .. | .. | .. | .. | ⁴ S _{3/2} | 15 |
| S | " | | | 2 | 4 | .. | .. | .. | .. | .. | .. | .. | .. | ³ P ₂ | 16 |
| Cl | " | | | 2 | 5 | .. | .. | .. | .. | .. | .. | .. | .. | ² P _{3/2} | 17 |
| A | " | | | 2 | 6 | .. | .. | .. | .. | .. | .. | .. | .. | ¹ S ₀ | 18 |

¹ Based by permission upon table by Ruark and Urey. Atoms, molecules, and quanta. 1930.

ELECTRON CONFIGURATIONS IN NORMAL ATOM

| Element | K | L | M | | | N | | | | O | | | P | | Normal term | No. Atomic |
|---------|-----------------------|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|--------------|------------|
| | | | 3.0 | 3.1 | 3.2 | 4.0 | 4.1 | 4.2 | 4.3 | 5.0 | 5.1 | 5.2 | 6.0 | 6.1 | | |
| | | | 3s | 3p | 3d | 4s | 4p | 4d | 4f | 5s | 5p | 5d | 6s | 6p | | |
| K | Same as for Argon | | | | | 1 | .. | .. | .. | .. | .. | .. | .. | .. | $2S_{1/2}$ | 19 |
| Ca | .. | .. | .. | .. | .. | 2 | .. | .. | .. | .. | .. | .. | .. | .. | $1S_0$ | 20 |
| Sc | .. | .. | 1 | 2 | .. | 2 | .. | .. | .. | .. | .. | .. | .. | .. | $2D_{3/2}$ | 21 |
| Ti | .. | .. | 2 | 2 | .. | 2 | .. | .. | .. | .. | .. | .. | .. | .. | $3F_2$ | 22 |
| V | .. | .. | 3 | 2 | .. | 2 | .. | .. | .. | .. | .. | .. | .. | .. | $4F_{3/2}$ | 23 |
| Cr | .. | .. | 5 | 1 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | $7S_3$ | 24 |
| Mn | .. | .. | 5 | 2 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | $6S_{5/2}$ | 25 |
| Fe | .. | .. | 6 | 2 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | $5D_4$ | 26 |
| Co | .. | .. | 7 | 2 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | $4F_{9/2}$ | 27 |
| Ni | .. | .. | 8 | 2 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | $3F_4$ | 28 |
| Cu | .. | .. | 10 | 1 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | $2S_{1/2}$ | 29 |
| Zn | .. | .. | 10 | 2 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | $1S_0$ | 30 |
| Ga | .. | .. | 10 | 2 | 1 | .. | .. | .. | .. | .. | .. | .. | .. | .. | $2P_{1/2}$ | 31 |
| Ge | .. | .. | 10 | 2 | 2 | .. | .. | .. | .. | .. | .. | .. | .. | .. | $3P_0$ | 32 |
| As | .. | .. | 10 | 2 | 3 | .. | .. | .. | .. | .. | .. | .. | .. | .. | $4S_{3/2}$ | 33 |
| Se | .. | .. | 10 | 2 | 4 | .. | .. | .. | .. | .. | .. | .. | .. | .. | $3P_2$ | 34 |
| Br | .. | .. | 10 | 2 | 5 | .. | .. | .. | .. | .. | .. | .. | .. | .. | $2P_{3/2}$ | 35 |
| Kr | .. | .. | 10 | 2 | 6 | .. | .. | .. | .. | .. | .. | .. | .. | .. | $1S_0$ | 36 |
| Rb | Same as for krypton | | | | | .. | .. | .. | .. | 1 | .. | .. | .. | .. | $2S_{1/2}$ | 37 |
| Sr | .. | .. | .. | .. | .. | .. | .. | .. | .. | 2 | .. | .. | .. | .. | $1S_0$ | 38 |
| Y | .. | .. | 1 | .. | .. | .. | .. | .. | .. | 2 | .. | .. | .. | .. | $2D_{3/2}$ | 39 |
| Zr | .. | .. | 2 | .. | .. | .. | .. | .. | .. | 2 | .. | .. | .. | .. | $3F_2$ | 40 |
| Cb | .. | .. | 4 | .. | .. | .. | .. | .. | .. | 1 | .. | .. | .. | .. | $6D_{1/2}$ | 41 |
| Mo | .. | .. | 5 | .. | .. | .. | .. | .. | .. | 1 | .. | .. | .. | .. | $7S_3$ | 42 |
| .. | .. | .. | (6) | .. | .. | .. | .. | .. | .. | (1) | .. | .. | .. | .. | $(6D_{3/2})$ | 43 |
| Ru | .. | .. | 7 | .. | .. | .. | .. | .. | .. | 1 | .. | .. | .. | .. | $5F_5$ | 44 |
| Rh | .. | .. | 8 | .. | .. | .. | .. | .. | .. | 1 | .. | .. | .. | .. | $4F_{9/2}$ | 45 |
| Pd | .. | .. | 10 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. | $1S_0$ | 46 |
| Ag | Same as for palladium | | | | | .. | .. | .. | .. | 1 | .. | .. | .. | .. | $2S_{1/2}$ | 47 |
| Cd | .. | .. | .. | .. | .. | .. | .. | .. | .. | 2 | .. | .. | .. | .. | $1S_0$ | 48 |
| In | .. | .. | .. | .. | .. | .. | .. | .. | .. | 2 | 1 | .. | .. | .. | $2P_{1/2}$ | 49 |
| Sn | .. | .. | .. | .. | .. | .. | .. | .. | .. | 2 | 2 | .. | .. | .. | $3P_0$ | 50 |
| Sb | .. | .. | .. | .. | .. | .. | .. | .. | .. | 2 | 3 | .. | .. | .. | $4S_{3/2}$ | 51 |
| Te | .. | .. | .. | .. | .. | .. | .. | .. | .. | 2 | 4 | .. | .. | .. | $3P_2$ | 52 |
| I | .. | .. | .. | .. | .. | .. | .. | .. | .. | 2 | 5 | .. | .. | .. | $2P_{3/2}$ | 53 |
| Xe | .. | .. | .. | .. | .. | .. | .. | .. | .. | 2 | 6 | .. | .. | .. | $1S_0$ | 54 |

ELECTRON CONFIGURATIONS IN NORMAL ATOM

| Element | K L M | N | | | | O | | | | P | | | Q | Normal term | Atomic No. |
|---------|---|-----|-----|-----|-----|-----------|-----|-----|-----|------------|-----|-----|-----|--------------|------------|
| | | 4,0 | 4,1 | 4,2 | 4,3 | 5,0 | 5,1 | 5,2 | 5,3 | 6,0 | 6,1 | 6,2 | 7,0 | | |
| | | 4s | 4p | 4d | 4f | 5s | 5p | 5d | 5f | 6s | 6p | 6d | 7s | | |
| Cs | Xenon configuration. | .. | .. | .. | .. | Shell | .. | .. | .. | 1 | .. | .. | .. | $^2S_{1/2}$ | 55 |
| Ba | Shells 1s to 4d contain 46 electrons. | .. | .. | .. | .. | 5s | .. | .. | .. | 2 | .. | .. | .. | 1S_0 | 56 |
| La | " | .. | .. | .. | .. | to | 1 | .. | .. | 2 | .. | .. | .. | $^2D_{3/2}$ | 57 |
| Ce | " | .. | .. | .. | 1 | 5p | 1 | .. | .. | 2 | .. | .. | .. | 3H_4 | 58 |
| Pr | " | .. | .. | .. | 2 | contain | 1 | .. | .. | 2 | .. | .. | .. | $^4K_{11/2}$ | 59 |
| Nd | " | .. | .. | .. | 3 | tain | 1 | .. | .. | 2 | .. | .. | .. | 3L_6 | 60 |
| Il | " | .. | .. | .. | 4 | 8 | 1 | .. | .. | 2 | .. | .. | .. | $^6L_{9/2}$ | 61 |
| Sa | " | .. | .. | .. | 5 | electrons | 1 | .. | .. | 2 | .. | .. | .. | 7K_4 | 62 |
| Eu | " | .. | .. | .. | 6 | trons | 1 | .. | .. | 2 | .. | .. | .. | $^8H_{13/2}$ | 63 |
| Gd | " | .. | .. | .. | 7 | .. | 1 | .. | .. | 2 | .. | .. | .. | 9D_2 | 64 |
| Tb | " | .. | .. | .. | 8 | .. | 1 | .. | .. | 2 | .. | .. | .. | $^8H_{17/2}$ | 65 |
| Dy | " | .. | .. | .. | 9 | .. | 1 | .. | .. | 2 | .. | .. | .. | $^7K_{10}$ | 66 |
| Ho | " | .. | .. | .. | 10 | .. | 1 | .. | .. | 2 | .. | .. | .. | $^6L_{19/2}$ | 67 |
| Er | " | .. | .. | .. | 11 | .. | 1 | .. | .. | 2 | .. | .. | .. | $^5L_{10}$ | 68 |
| Tu | " | .. | .. | .. | 12 | .. | 1 | .. | .. | 2 | .. | .. | .. | $^4K_{17/2}$ | 69 |
| Yb | " | .. | .. | .. | 13 | .. | 1 | .. | .. | 2 | .. | .. | .. | 3H_6 | 70 |
| Lu | " | .. | .. | .. | 14 | .. | 1 | .. | .. | 2 | .. | .. | .. | $^2D_{3/2}$ | 71 |
| Hf | Shells 1s to 5p contain 68 electrons | .. | .. | .. | .. | 2 | .. | .. | .. | 2 | .. | .. | .. | 3F_2 | 72 |
| Ta | " | .. | .. | .. | .. | 3 | .. | .. | .. | 2 | .. | .. | .. | $^4F_{3/2}$ | 73 |
| W | " | .. | .. | .. | .. | 4 | .. | .. | .. | 2 | .. | .. | .. | 5D_0 | 74 |
| Re | " | .. | .. | .. | .. | 5 | .. | .. | .. | 2 | .. | .. | .. | $^6S_{5/2}$ | 75 |
| Os | " | .. | .. | .. | .. | 6 | .. | .. | .. | 1 | .. | .. | .. | $^6D_{9/2}$ | .. |
| Ir | " | .. | .. | .. | .. | 6 | .. | .. | .. | 2 | .. | .. | .. | 5D_4 | 76 |
| Pt | " | .. | .. | .. | .. | 7 | .. | .. | .. | 1 | .. | .. | .. | 5F_5 | .. |
| Au | " | .. | .. | .. | .. | 7 | .. | .. | .. | 2 | .. | .. | .. | $^4F_{9/2}$ | 77 |
| Hg | " | .. | .. | .. | .. | 8 | .. | .. | .. | 1 | .. | .. | .. | $^4F_{9/2}$ | .. |
| Tl | " | .. | .. | .. | .. | 9 | .. | .. | .. | 1 | .. | .. | .. | 3D_3 | 78 |
| Pb | Shells 1s to 5d contain 78 electrons | .. | .. | .. | .. | .. | .. | .. | .. | 1 | .. | .. | .. | $^2S_{1/2}$ | 79 |
| Bi | " | .. | .. | .. | .. | .. | .. | .. | .. | 2 | .. | .. | .. | 1S_0 | 80 |
| Po | " | .. | .. | .. | .. | .. | .. | .. | .. | 2 | 1 | .. | .. | $^2P_{1/2}$ | 81 |
| — | " | .. | .. | .. | .. | .. | .. | .. | .. | 2 | 2 | .. | .. | 3P_0 | 82 |
| Rn | " | .. | .. | .. | .. | .. | .. | .. | .. | 2 | 3 | .. | .. | $^4S_{3/2}$ | 83 |
| — | " | .. | .. | .. | .. | .. | .. | .. | .. | 2 | 4 | .. | .. | 3P_2 | 84 |
| — | " | .. | .. | .. | .. | .. | .. | .. | .. | 2 | 5 | .. | .. | $^2P_{3/2}$ | 85 |
| — | " | .. | .. | .. | .. | .. | .. | .. | .. | 2 | 6 | .. | .. | 1S_0 | 86 |
| Ra | Radon configuration. Shells 1s to 5d contain 78 electrons | .. | .. | .. | .. | .. | .. | .. | .. | The shells | .. | .. | 1 | $^2S_{1/2}$ | 87 |
| Ac | " | .. | .. | .. | .. | .. | .. | .. | .. | 6s to 6p | 1 | 2 | 2 | 1S_0 | 88 |
| Th | " | .. | .. | .. | .. | 1 | .. | .. | .. | contain | 1 | 2 | 2 | $^2D_{3/2}$ | 89 |
| UN | " | .. | .. | .. | .. | .. | .. | .. | .. | 8 | 2 | 2 | 2 | 3H_4 | 90 |
| U | " | .. | .. | .. | .. | .. | .. | .. | .. | electrons | 1 | 2 | 2 | 3F_2 | .. |
| — | " | .. | .. | .. | .. | .. | .. | .. | .. | .. | 3 | 2 | 2 | $^4K_{11/2}$ | 91 |
| — | " | .. | .. | .. | .. | .. | .. | .. | .. | .. | 3 | 2 | 2 | $^4F_{3/2}$ | .. |
| — | " | .. | .. | .. | .. | 3 | .. | .. | .. | .. | 1 | 2 | 2 | 5L_6 | 92 |
| — | " | .. | .. | .. | .. | .. | .. | .. | .. | .. | 4 | 2 | 2 | 5D_0 | .. |

EFFECTIVE ATOMIC RADII

Goldschmidt, on the basis of reasonable though empirical assumptions, has calculated effective radii of atoms in various charged conditions; Pauling, on the basis of wave-mechanics, has presented theoretical values for most of the elements, the two series agreeing well in many cases. The latter values are printed in bold-faced type; the values considered nontypical are in parentheses; e.g., for silicon we have: Si^{+} 0.22—0.39 **0.41**, Si^0 (1.12—) 1.18, Si^{-4} (1.98); **2.71**, signifying silicon, carrying 4 + charges, has apparent radius between 0.22 and 0.41; but the lower values relate to compounds where the atoms appear to be deformed; so Goldschmidt gives 0.39 as most significant. Wave-mechanics yields **0.41**. Neutral, the radius ranges from 1.12, in abnormal compounds, to 1.18 in those typical; when carrying — charges, the value is 1.98, according to calculations deemed faulty, **2.71** according to theory. In applying the data to replacements, halides and oxides are usually ionized, and the values in the outer columns apply. Thus in fluorite the value for Ca^{+2} should be added to that for F^{-1} , giving between 2.32 and 2.42, or 2.37 as a mean; and the observed Ca-F distance in the crystal is 2.36 Angstrom units. In the remaining types of compounds the atoms appear to be largely neutral and the first column should be used. The units are Angstroms. Wherry, Amer. Mineralog., 14, 54, 1929.

| Atomic no.; element | Radius neutral atom Angstroms | Charge | Radius positively charged ion Angstroms | Atomic no.; element | Radius neutral atom Angstroms | Charge | Radius positively charged ion Angstroms |
|---------------------|-------------------------------|--------|---|---------------------|-------------------------------|--------|---|
| 1 H | | | | 42 Mo | 1.36 | 6 | 0.62 |
| 2 He | (0.93) | | | Mo | | 4 | 0.66 (—0.83) |
| 3 Li | (1.50—)1.56 | 1 | 0.60 —0.78(—0.82) | 44 Ru | 1.27—1.34 | 4 | 0.63 —0.65 |
| 4 Be | 1.05(—1.15) | 2 | 0.31 —0.34 | 45 Rh | 1.34—1.35 | 3 | 0.69 |
| 5 B | | 3 | 0.20 | 46 Pd | 1.37 | | |
| 6 C | (0.45—)0.77 | 4 | 0.15 | 47 Ag | (1.17—)1.44 | 1 | (0.70—)1.13— 1.26 |
| 7 N | (0.65—)0.71 | 5 | 0.11 | 48 Cd | (1.47—)1.39(—1.60) | 2 | (0.78—) 0.97 —1.03 |
| 8 O | 0.60(—0.65) | 6 | 0.09 | 49 In | 1.45—1.62 | 3 | 0.81 —0.92 |
| 9 F | 0.67 | 7 | 0.07 | 50 Sn | (1.27—)1.40 | 4 | (0.64—) 0.71 (—0.81) |
| 10 Ne | (1.12) | | | 51 Sb | (1.22—)1.34(—1.44) | 5 | 0.62 |
| 11 Na | (1.77—)1.86 | 1 | 0.95 —0.98(—1.09) | 52 Te | | 3 | 0.90 |
| 12 Mg | (1.42—)1.62 | 2 | 0.65 —0.78(—0.85) | Te | 1.33—1.43 | 6 | 0.56 |
| 13 Al | (1.16—)1.43 | 3 | 0.50 —0.57(—0.66) | 53 I | 1.36—1.40 | 4 | 0.81 —0.89 |
| 14 Si | (1.12—)1.18 | 4 | (0.22—)0.39— 0.41 | I | | 7 | 0.50 |
| 15 P | 0.93 | 5 | 0.34 | 54 Xe | (1.90) | 5 | 0.94 |
| 16 S | 1.02—1.04 | 6 | 0.29 —0.34 | 55 Cs | (2.37—)2.55 | 1 | 1.65 — 1.69 (—1.75) |
| 17 Cl | 1.05—1.07 | 7 | 0.26 | 56 Ba | 2.10 | 2 | 1.35 — 1.43 (—1.49) |
| 18 A | (1.54) | | | 57 La | | 3 | 1.15 —1.22 |
| 19 K | (2.07—)2.23 | 1 | 1.33(—1.84) | 58 Ce | 1.82—1.83 | 4 | 1.01 —1.02 |
| 20 Ca | (1.70—)1.97 | 2 | 0.99—1.06(—1.50) | | | | |
| 21 Sc | 1.51 | 3 | 0.81 —0.83 | 59 Pr | | 3 | 1.18 |
| 22 Ti | (1.40—)1.49(—1.53) | 4 | (0.58—)0.64— 0.68 | Pr | | 4 | 0.92 —1.00 |
| 23 V | 1.32(—1.43) | 5 | 0.59 | 60 Nd | | 3 | 1.16 |
| 24 Cr | (1.17—)1.25(—1.54) | 6 | 0.59 —0.61 | 62 Sm | | 3 | 1.15 |
| 25 Mn | (1.17—)1.29(—1.59) | 7 | 0.52 —0.65 | 63 Eu | | 3 | 1.13 |
| Mn | | 4 | 0.50 —0.52 | 64 Gd | | 3 | 1.13 |
| Mn | | 2 | 0.80 —0.91 | 65 Tb | | 3 | 1.11 |
| 26 Fe | (1.21—)1.26(—1.45) | 3 | (0.49—)0.67 | 66 Dy | | 3 | 1.09 |
| Fe | | 2 | 0.75 —0.83 | 67 Ho | | 3 | 1.07 |
| | | | | | | | 1.05 |
| 27 Co | 1.26(—1.39) | 3 | 0.29—0.47 | 68 Er | | 3 | 1.04 |
| Co | | 2 | 0.72 —0.82 | 69 Tm | | 3 | 1.04 |
| 28 Ni | 1.24(—1.39) | 3 | 0.35 | 70 Yb | | 3 | 1.00 |
| Ni | | 2 | 0.69 —0.78 | 72 Hf | 1.66 | | |
| 29 Cu | (1.22—)1.27(—1.37) | 2 | 0.70 | 73 Ta | 1.42—1.44 | | |
| Cu | | 1 | (0.58—) 0.96 | 74 W | 1.37 | 6 | 0.88 |
| 30 Zn | 1.31—1.34 | 2 | 0.74 —0.83 | 75 W | | 4 | 0.66 —0.68 |
| 31 Ga | (1.28—)1.33(—1.45) | 3 | 0.62 | 76 Os | 1.30—1.34 | 4 | 0.65 —0.67 |
| 32 Ge | 1.22 | 4 | 0.44 — 0.53 | 77 Ir | 1.35 | 4 | 0.64 —0.66 |
| 33 As | (1.04—)1.16(—1.26) | 5 | 0.47 | 78 Pt | 1.38(—1.43) | | |
| As | | 3 | 0.69 | 79 Au | 1.40—1.44 | 1 | 1.37 |
| 34 Se | 1.13—1.17 | 6 | 0.42 | 80 Hg | 1.46—1.49 | 2 | 1.10 —1.12 |
| 35 Br | 1.19 | 7 | 0.39 | 81 Tl | (1.71—)1.99(—2.25) | 3 | 0.95 —1.05 |
| 36 Kr | (1.69) | | | Tl | | 1 | 1.44—1.51 |
| 37 Rb | (2.25—)2.36 | 1 | 1.48 —1.49(—1.88) | 82 Pb | 1.74(—1.90) | 4 | 0.84 |
| 38 Sr | 1.95 | 2 | 1.13 —1.27(—1.45) | Pb | | 2 | (0.98—) 1.21 —1.32 |
| 39 Y | | 3 | 0.93 —1.06 | 83 Bi | (1.34—)1.46(—1.55) | 5 | 0.74 |
| 40 Zr | 1.60—1.62 | 4 | (0.68—) 0.80 —0.89 | 90 Th | 1.80—1.82 | 4 | 1.02 —1.10 |
| 41 Nb | 1.43(—1.50) | 5 | 0.69 — 0.70 | 92 U | | 4 | 0.97 —1.05 |
| Cb | | 4 | 0.67 —0.69 | —NII ₁ | | 1 | 1.42 —1.59 |

| Charge | Radius negative ion | Charge | Radius negative ion | Charge | Radius negative ion | Charge | Radius negative ion |
|--------|------------------------|--------|------------------------|--------|----------------------|--------|------------------------------|
| 1 H | —1 (1.27); 2.08 | 14 Si | —4 (1.98); 2.71 | 32 Ge | —4 2.72 | 50 Sn | —4 (2.15); 2.94 |
| 6 C | —4 2.60 | 15 P | —3 2.12 | 33 As | —3 2.22 | 51 Sb | —3 2.45 |
| 7 N | —3 1.71 | 16 S | —2 1.74— 1.84 | 34 Se | —2 1.91— 1.98 | 52 Te | —2 2.03 — 2.21 |
| 8 O | —2 1.32— 1.40 | 17 Cl | —1 1.81 | 35 Br | —1 1.95—1.96 | 53 I | —1 2.16 —2.20 |
| 9 F | —1 1.33— 1.36 | | | | | 82 Pb | —4 2.15 |

ELECTRONS, PROTONS, ATOMIC STRUCTURE

Free negative electron (corpuscle, J. J. Thomson).—Mass, spectroscopic (bound) 9.035×10^{-28} g; free, 8.994×10^{-28} g; atomic weight, 5.479 and 5.454×10^{-4} respectively, probably all electrical, due to inertia of self-induction. Theory shows that when speed of electron = 1/10 velocity of light, its mass should be appreciably dependent upon that speed. If m_0 be the mass for small velocity, m , the transverse mass for v , and v/c (velocity of light, c) = β then $m = m_0 (1 - \beta^2)^{-\frac{1}{2}}$ (Lorentz, Einstein).

| | | | | | | | | | | |
|-----------|---------|-------|------|-------|-------|-------|-------|-------|-------|-------|
| β , | 0.01 | 0.10 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| m/m_0 , | 1.00005 | 1.005 | 1.02 | 1.048 | 1.091 | 1.155 | 1.250 | 1.400 | 1.667 | 2.294 |

Radium ejects electrons with 3/10 to 98/100 of c . m , due to charge = $2E^2/3a$, where E = charge, a , radius, whence radius of electron is 2×10^{-13} cm = 1/50,000 atomic radius. Cf. (radius earth/radius Neptune's orbit) = 1/360,000. Collisions with α particles show diameter of electron must be less than 4×10^{-13} cm (Chadwick, Bieler, Philos. Mag., 1921).

Positive electron or proton.—Heavy, extraordinarily small, never found associated with mass less than that of the H atom; mass, 1.6609×10^{-24} g. Specific charge, 9579.7 abs-em-units \cdot g $^{-1}$. Ratio mass proton to mass electron, 1838 (spectroscopic), 1847 (deflection). If mass is all electrical, radius must be 1/2000 that of electron. No experimental evidence as with the latter since high enough speeds not available. Penetrability of atom by β particle (may penetrate 10,000 atomic systems before it happens to detach an electron) and α particle (8000 times more massive than negative electron, passes through 500,000 atoms without apparent deflection by nucleus more than 2 or 3 times) shows extreme minuteness. Upper limit of nucleus not larger than 10^{-12} cm for Au (heavy atom) and 10^{-13} cm for H (light atom) (Rutherford). Cf. (radius sun)/(radius Neptune's orbit) = 1/3000 but sun larger than planets. Hg atoms by billions may pass through thin-walled, highly-evacuated glass tube without impairing vacuum, therefore massive parts of atoms must be extremely small compared to volume of atom.

Rutherford atom.—Atoms of all elements are somewhat similarly built. At the center a charged nucleus of minute dimensions, responsible for most of the mass of the atom; this is surrounded by a distribution held in equilibrium by the force from the nucleus. Resultant nuclear charge = atomic or ordinal no., varies from 1 for H to 92 for U. These atomic nos. represent the number of planetary electrons which surround the nucleus. By the action of light, the electric charge, bombardment by α particles, one or more of the planetary electrons may be driven away from the nucleus; by X rays or the swift β rays some of the more strongly bound may be removed. New electrons are generally soon captured to replace these. The nucleus is much more stable and when disrupted (radio-active changes, bombardment with α particles) shows no tendency to revert to original state.

Moseley (Philos. Mag., 26, 1912: 27, 1914) photographed and analyzed X-ray spectra, showing their exact similarity in structure from element to element, differing only in frequencies, the square roots of the frequencies forming an arithmetical progression from element to element. Moseley's series of increasing X-ray frequencies is with one or two

ELECTRONS, PROTONS, ATOMIC STRUCTURE

exceptions that of increasing atomic weights, and these exceptions are less anomalous for the X-ray series than for the atomic-weight series. It seems plausible that there are 92 elements (from H to U) built up by the addition of some electrical element. Moseley assigned successive integers to this series (see Table 598) known now as atomic numbers.

Moseley's discovery may be expressed in the form

$$n_1/n_2 = E_1/E_2 \text{ or } \lambda_2/\lambda_1 = E_1^2/E_2^2$$

where E is the nuclear charge and λ the wave length. Substituting for the highest frequency line of W, $\lambda_2 = 0.167 \times 10^{-8} \text{ cm}$ (Hull), $E_2 = 74 = N_w$, and $E_1 = 1$, then $\lambda_1 =$ highest possible frequency by element which has one + electron; $\lambda_1 = 91.4 \text{ m}\mu$. Now the H ultra-violet series highest frequency line = $91.2 \text{ m}\mu$ (Lyman); i. e., this ultra-violet line of H is nothing but its K X-ray line. Similarly, it seems equally certain that the ordinary Balmer series of H (head at $365 \text{ m}\mu$) is its L X-ray series and Paschen's infra-red series its M X-ray series.

The application of Newton's law to Moseley's law leads to $E_1/E_2 = a_2/a_1$, where the a 's are the radii of the inmost — electronic orbits, i. e., the radii of these orbits are inversely proportional to the central charges or atomic numbers.

There are other negative electrons on the nucleus with corresponding + charges to make the atom neutral electrically. The negative nuclear charges may serve to hold the positive ones together. He, atomic no. = 2, has two free + charges, on nucleus; the nucleus has 4 + protons held together by 2 — electrons with 2 — electrons outside nucleus. H has one + proton and one — electron.

If the — electron is designated as e (charge — 1, mass negligible) and the + proton as p (charge + 1, mass 1 except in H) then the formula for the nucleus of any element from He to U may be written as $(p_2e)_N(p_e)_n$ where N is the atomic number and n has values from 0 to 54. If n be taken as — 1, then H may be included. (Masson, Philos. Mag., 41, 1921.) If brackets are used to designate the nucleus then the complete element becomes $[(p_2e)_N(p_e)_n]e_N$. In the formation of ions only the part exterior to the brackets is affected. For the α -transformation (emission of + charged He nucleus) $2(p_2e) = (p_2e)_2\uparrow$, the subchemical equation may be written $[(p_2e)_N(p_e)_n]e_N = [(p_2e)_N - 2(p_e)_n]e_N + (p_2e)_2\uparrow$ (He nucleus); the new elements upon discharge of its — charge becomes $[(p_2e)_N - 2(p_e)_n]e_N - 2$ showing the characteristic α -ray change with the atomic weight lowered by 2 and the mass by 4. The β -ray $2(p_e) = (p_2e) + e\uparrow$ gives the equation

$$[(p_2e)_N(p_e)_n]e_N = [(p_2e)_N + 1(p_e)_{n-2} + e\uparrow$$

mass unchanged and forms the singly — charged ion of an isobar.

From the emission of nuclear α particles, $2(p_2e) = p_4e_2$, it seems probable that the nuclei are compounds of He and I nuclei. By the bombardment of the nuclei of atoms up to atomic number 40 with α particles Rutherford has obtained H but only where H and He nuclei should both occur in the nucleus (Bo, N, Fl, Na, Al, P, see Table 638). Harkins has

TABLE 603(A) (*concluded*).—Electrons, Protons, Atomic Structure

developed this idea (Journ. Franklin Inst., 194, 213 et seq., 1922) and shown the much greater frequency in nature of the even-atomic numbered elements (97.6 per cent in stony meteorites, 99.2 Fe meteorites, 85.6 lithosphere, 5 unknown elements all odd, even radioactive most stable). Elements below atomic number 30 make up 99.99 per cent of all meteorites, 99.85 igneous rocks, 99.95 shale, 99.95 sandstones, 99.85 lithosphere. The stability of the He nucleus may be judged by the energy set free in the formation of He from H. According to "relativity" $1 \text{ g-mass} = 9 \times 10^{20} \text{ ergs}$ ($E = mc^2$). The change of mass involved in the formation of 1 g-atom of He (4,000 g) from 4 g-atoms of H_2 ($4 \times 1.0078 \text{ g}$) $= 2.81 \times 10^{19} \text{ ergs} = 6.71 \times 10^{11} \text{ calories}$. 1 lb. H_2 changed to He equals heat from 10,000 tons coal. The nuclei of light even numbered atoms (most abundant isotope) up to Fe (26) almost wholly of He nuclei. To a 1st approximation the α particle behaves in collision like an elastic oblate spheroid, semi-axes, 8×10^{-12} and $4 \times 10^{-13} \text{ cm}$ (Chadwick, Bieler, Philos. Mag. 1921).

TABLE 603(B).—Atomic Structure, Bohr Atom

Bohr atom.—Bohr postulated electrons rotating in circular nonradiating orbits about a central body according to the laws of celestial mechanics and its consequent energy relations. He added the idea that these electrons could jump between different orbits emitting light of a frequency ν which depended upon the relationship $E_2 - E_1 = h\nu$ where the E 's denote the energies (according to classical conceptions) in the two orbits and h , Planck's "quantum of action" of the nature of a moment of momentum. In going from one possible orbit to another the moment of momentum of the electron *must* progress by steps, each a multiple of $h/2\pi$. Balmer's formula is consistent with such a process: $\nu = N(1/n_1^2 - 1/n_2^2)$ where ν is the frequency, N , a constant, and n_1 for the visible series (Balmer's) has the value 2, n_2 , the successive integral values, 3, 4, 5, ...; 33 lines in the Balmer series have been observed in stars where orbits of greater radius are possible (small gas density) than in the laboratory (12 lines). With $n_1 = 1$, n_2 , 2, 3, 4, ..., Lyman's ultra-violet series results; $n_1 = 3$, n_2 , 4, 5, 6, ..., Paschen's infra-red series; $n_1 = 4$, n_2 , 5, 6, 7, ..., Brackett's series of even greater wave lengths.

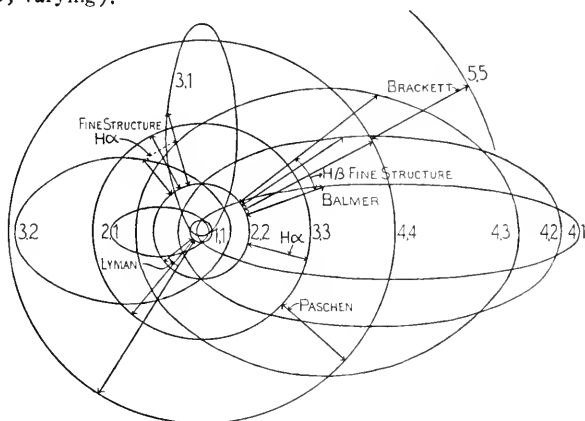
No mechanism was described to show how the energy of rotation was transferred into energy of radiation nor why only certain orbits could be occupied. He evidently used non-radiating orbits at variance with Maxwell's equations.

Two independent predictions from these assumptions were verified: the predicted and observed values of Rydberg's constant within $\frac{1}{2}\%$ and the differences in ν for the H and the He + lines due to the 4-fold mass of the He + nucleus.

Relativistic considerations.—Sommerfeld (1916) applied Einstein's relativity considerations together with the variation of mass with the speed of the revolving electrons and brought further support to the idea of orbits through prediction and the verification of the "fine structure of spectrum lines." Bohr considered only circular orbits in which the speed of rotation is constant, but elliptical orbits are possible with the same $h/2\pi$ as the circular and in them the speeds of revolution of the electrons change in different portions of the orbit as with classical mechanics but these speeds are such that a relativity

TABLE 603(B) (continued).—Atomic Structure, Bohr Atom

correction to the mass is necessary. Their quantization brought another quantum number; the so-called total quantum number, n , now becomes the sum of two since both the radii (r) and azimuth (ϕ) of the electron vary. The orbit is usually designated by two quantum numbers, the total, n , and the azimuthal (ϕ) viz.: 1.1, 2.3 (p orbit, circular), 2.1 (s orbit, elliptical), 3.3, 3.2, 3.1. . . . The following figure illustrates the first four sets of orbits of the hydrogen atom. The table indicates the modes of the quantum numbers (a_2 radius inner orbit, a , b , varying).



| nk | total n | azim. k | radial n_r | a/a_2 | b/a_1 |
|------|--------------|--------------|-----------------|---------|---------|
| 1.1 | 1 | 1 | 0 | 1 | 1 |
| 2.1 | 2 | 1 | 1 | 4 | 2 |
| 2.2 | 2 | 2 | 0 | 4 | 4 |
| 3.1 | 3 | 1 | 2 | 9 | 3 |
| 3.2 | 3 | 2 | 1 | 9 | 6 |
| 3.3 | 3 | 3 | 0 | 9 | 9 |

The resonance potentials for the circular orbits are (hydrogen atom):

| | | | | | | | | |
|-----------------------|-------|-------|--------|--------|--------|--------|------|-------------|
| 1.1 orbit to → | 2.2 | 3.3 | 4.4 | 5.5 | 6.6 | 7.7 | | ∞ |
| Volts observed | 10.15 | 12.05 | 12.70 | 13.00 | 13.17 | 13.27 | | 13.54 |
| λ Lyman series, μ | .1216 | .1026 | .0972 | .0950 | | | | .0912 μ |
| " Balmer 2.2 orbit | | .6563 | .4861 | .4340 | .4102 | .3970 | | .3646 μ |
| " Paschen 3.3 orbit | | | 1.8756 | 1.2821 | 1.0939 | 1.0052 | | .8203 μ |
| " Brackett 4.4 orbit | | | | 4.05 | 2.63 | 2.16 | | 1.46 μ |

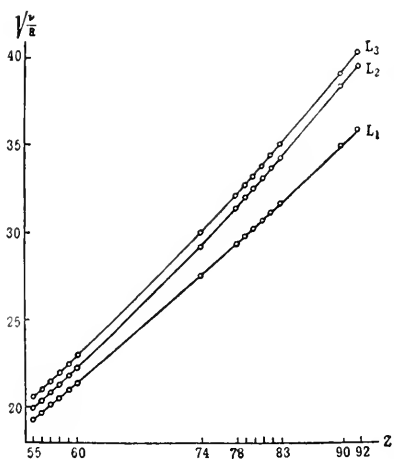
The remarkable prediction and consequent observation of the "fine-structure of spectrum lines resulted from this postulate." Thus all the lines of the Balmer series, consisting of jumps into the state of total quantum 2, possessing 2 orbits, a circle and an ellipse, should show a fine structure due to energy differences of these circular and elliptical orbits. Approximately they should be all doublet lines of wave length predictable from laws of orbital mechanics. The separations should be .365 cm^{-1} ; actually .36 cm^{-1} (Houston) was found. The separation should vary as the 4th power atomic no. Paschen (1916) actually found for He^+ , $16 \times .365 \text{ cm}^{-1}$. Further remarkable results came from Epstein's (Ann. Phys., 50, 489, 1916) work on the Stark effect and the prediction of the separation of the so-called L doublets of X-ray spectra. If actually a relativity doublet, one must multiply the H separation by 71 millions (92^4); also checked with experiment.

Inner quantum numbers.¹—It became necessary (1920, Sommerfeld, Ann. Phys., 63, 221, 1920) to account for further fine structure. e. g.: In X rays the L orbits or levels correspond to $n=2$, permitting only two different orbits, 2.2 (circle) and 2.1 (ellipse); but lines of 3 close wave lengths were observed—two being the regular expected doublet whose frequency varies with z^2 as expected. These two levels are indicated by the two diverging lines, L_2 , L_3 in the following figure.

¹ Millikan, Proc. Amer. Philos. Soc., 66, 211, 1927, from which much of the accompanying description is condensed.

TABLE 603(B) (continued).—Bohr Atom

The third level L_1 is seen to follow an entirely different law: it runs parallel to L_2 .



Bohr and Sommerfeld introduced the idea of two orbits of the same shape but different orientations, something different in the central field giving these orbits slightly different energies. A so-called *inner* quantum number, J , was introduced. The difference in the frequencies of the familiar doublets in Li was supposed due to jumps to a common orbit (s orbit) from 2 orbits differing only in the "inner" quantum number, i. e., orbits of different orientations but same shapes, in this case circles, or 2.2 orbits, known as the $p_{1/2}$ orbits. The s orbit into which the 2 electrons jumped to form the Li doublet was the third possible of total quantum 2, the 2.1 orbit. The two circular (p orbits) differed slightly in frequency, but the changes from either p to the s orbit was too large for the relativity effect. Bohr (Ann.

Phys., 71, 228, 1923) suggested that the anomaly was due to the penetration of orbits of outer electrons within the field of action of inner orbits.

TABLE 603(C).—The Spinning Electron and Summary

The spinning electron.—A disconcerting element existed in that the difference of energy between two circular $p_{1/2}$ orbits varied with the atomic number precisely as demanded by the relativity consideration, though it could not be due to relativity since the $p_{1/2}$ orbits had no difference in shape but only of orientation. A new conception by Uhlenbeck and Goudsmit (Nature, 117, 264, 1926) came to the rescue assuming that every electron rotates upon its axis. Two possible directions of spin are assumed 180° apart, but the moment of momentum is assumed always the same, exactly $\frac{1}{2}$ unit or $\frac{1}{2} h/2\pi$. This introduces exactly the right amount of energy difference between the $p_{1/2}$ circular orbits. It is superposed upon the relativity effect, making the fine structure (even in H and He+ without inner electronic orbits) somewhat more complex.

In the case of each individual electron there are four moments of momentum—four elements to describe an electron's orbital motion:

(1) The size of its orbit—the total moment of momentum characterized by its total quantum number n (Bohr) fixing the major axis of orbit.

(2) The azimuthal quantum number, k , which with a given n or major axis, fixes the shape (minor axis). It has been found expedient to reduce by unity all values of k heretofore assigned. Since we are not ready to discard entirely the old interpretation, this reduced value of k is for convenience denoted by a new letter, l , so that $l = k - 1$. Thus for an s orbit $l = 0$; p orbit, 1; d orbit, 2; etc.

(3) The projection of the moment of momentum l upon any fixed direction, which, in considering the Zeeman effect is the direction of the external magnetic field, is quantized (m_l). The projection fixes the orientation in space. The significance that this projection is quantized is that only certain definite orientations are possible (Stern, Gerlach experiments).

(4) The projection of the moment of momentum of spin upon this fixed direction is designated by the symbol m_s . In each atom only two possible directions of spin 180° apart are taken so that m_s determines in what direction the electron is spinning. m_l and m_s are usually called magnetic quantum numbers because of their use in connection with magnetic fields.

(Most of the above is abbreviated from Millikan, Proc. Amer. Philos. Soc., 66, 211, 1927.)

ENERGY OF BINDING OF AN ELECTRON—NEUTRAL ATOMS

(Adapted from paper by Henry Norris Russell, *Astrophys. Journ.*, 70, 1929.)

The electrons in an atom, neutral or ionized, are bound in different states (a preferable term to "orbits"). The more firmly bound inner ones which form parts of the completed shells concern the spectroscopy of X rays but not of ordinary light. The two following tables give a study of the energy of binding of an electron, in different atoms, in the same state, the state characterized by the same total and azimuthal quantum numbers, denoted in Bohr's notation by $1s, 2s, 3s, \dots$; $2p, 3p, 4p, \dots$; $3d, 4d, \dots$; $4f, \dots$, or more commonly at present, $1s, 2s, 3s, \dots$; $2p, 3p, 4p, \dots$; $3d, 4d, \dots$; $4f, \dots$. The energy in volts is given required to remove an electron in the given state from the atom or liberated when it returns. Among the energy levels resulting from different space quantizations of the same electronic configuration, that with the greatest binding energy is given regardless of the multiplicity. Most values are derived from spectrum series and are fully reliable; those in (), two decimals, are extrapolations from series formulae and should be substantially correct; those in [], one decimal and in [] are interpolated and should be accurate to 0, to 0.2 v.

| El. | 1s | 2s | 2p | 3s | 3p | 3d | 4s | 4p | 4d | 5s | 5p | 5d |
|-----|-------|------|--------|-------|--------|--------|-------|--------|-------|--------|------|-------|
| H | 13.54 | 3.38 | 3.38 | 1.50 | 1.50 | 1.50 | 0.81 | 0.81 | 0.81 | 0.54 | 0.54 | 0.54 |
| He | 24.48 | 4.75 | 3.61 | 1.86 | 1.57 | 1.51 | .99 | .87 | .85 | .61 | .56 | .54 |
| Li | | 5.36 | 3.40 | 2.01 | 1.55 | 1.51 | 1.05 | .87 | .85 | .64 | .55 | .54 |
| Be | | 9.29 | 6.57 | 2.86 | | 1.62 | 1.32 | | .90 | .76 | | .57 |
| B | | | 8.28 | 3.34 | | 1.52 | 1.49 | | .87 | | | .57 |
| C | | | 11.22 | 3.78 | 2.42 | 1.57 | | 1.19 | | | | |
| N | | | 14.50 | 4.20 | 2.78 | 1.55 | 1.69 | | .87 | .93 | | .56 |
| O | | | 13.56 | 4.45 | 2.86 | 1.52 | 1.77 | 1.32 | .86 | .95 | | .55 |
| F | | | [17.3] | (4.7) | (3.0) | | | | | | | |
| Ne | | | 21.47 | 4.93 | 3.17 | 1.53 | 1.86 | 1.41 | .86 | 1.00 | .80 | .55 |
| Na | | | | 5.11 | 3.02 | 1.51 | 1.94 | 1.38 | .85 | 1.02 | .79 | .54 |
| Mg | | | | 7.61 | 4.92 | 1.88 | 2.52 | 1.70 | 1.05 | 1.21 | .92 | .66 |
| Al | | | | | 5.95 | 1.95 | 2.83 | 1.89 | 1.15 | 1.31 | .99 | .75 |
| Si | | | | | 8.14 | | 3.08 | | 1.16 | 1.37 | | |
| P | | | | | [10.5] | | (3.5) | | | | | |
| S | | | | | 10.31 | (1.98) | 3.82 | 2.48 | 1.06 | (1.59) | 1.19 | .65 |
| Cl | | | | | [12.9] | | (3.9) | [2.6] | | | | |
| A | | | | | 15.69 | (1.93) | 4.19 | 2.84 | 1.06 | 1.69 | 1.29 | .65 |
| K | | | | | | 1.65 | 4.33 | 2.72 | .94 | 1.72 | 1.27 | .59 |
| Ca | | | | | | 3.57 | 6.09 | 4.21 | 1.42 | 2.19 | 1.57 | .81 |
| Sc | | | | | | 5.13 | 6.57 | 4.59 | 1.66 | 2.40 | | |
| Ti | | | | | | 5.95 | 6.80 | 4.76 | 1.60 | 2.32 | | |
| V | | | | | | 6.68 | 7.04 | 4.92 | | 2.35 | | |
| Cr | | | | | | 8.24 | 7.28 | 5.05 | | 2.43 | | |
| Mn | | | | | | 5.76 | 7.40 | 5.09 | 1.64 | 2.54 | | |
| Fe | | | | | | 6.98 | 7.83 | 5.45 | 1.63 | 2.55 | | |
| Co | | | | | | 7.82 | 8.25 | 5.33 | | 2.62 | | |
| Ni | | | | | | 8.63 | 8.65 | 5.25 | 1.65 | 2.55 | | |
| Cu | | | | | | 10.41 | 9.02 | 5.58 | 1.65 | 2.69 | | |
| Zn | | | | | | | 9.36 | 5.30 | 1.66 | 2.72 | 1.80 | .89 |
| Ga | | | | | | | | 5.98 | 1.68 | 2.92 | 1.89 | .94 |
| Ge | | | | | | | | 7.80 | 1.87 | 3.26 | | 1.04 |
| As | | | | | | | | [9.6] | | (3.4) | | |
| Se | | | | | | | | [9.4] | (1.9) | (3.4) | | (0.8) |
| Br | | | | | | | | [11.4] | | (3.6) | | |
| Kr | | | | | | | | [13.9] | | (3.9) | | |
| Rb | | | | | | | | | 1.76 | 4.13 | 2.60 | .88 |
| Sr | | | | | | | | | 3.42 | 5.65 | 3.82 | 1.34 |
| Yt | | | | | | | | | 5.04 | 6.40 | 4.55 | 1.61 |

ENERGY OF BINDING OF AN ELECTRON—SINGLY IONIZED ATOMS

(Adapted from Henry Norris Russell, *Astrophys. Journ.*, 70, 1929.)

This table companions the preceding one. A number of entries have been derived in various ways and may be in error by .5 volt; Li +, 3-4 v. The lines of a diagram made from the data of these two tables, with atomic numbers as abscissae and energy of binding as ordinates, a separate line for each state, are strikingly similar. The familiar "displacement law" applies not only to the multiplicities present in the spectrum, but also to the energy relations—the spark spectrum for any element resembling in both respects that of the arc of the preceding element.

The energy of binding, for a given state, increases with the atomic number. For the s states the increase is steady; for the p and d states it is interrupted by fluctuations remarkably similar.

The increase of energy is most rapid (1) when electrons of a given type are building up a complete shell; (2) when s electrons are being added. The fluctuations are most conspicuous when a shell is half full (half of the 6p electrons in N, P, As, O⁺, S⁺, and of the 10d electrons in Cr, Mn⁺).

Energy of Binding of an Electron—Singly Ionized Atoms

| El. | 1s | 2s | 2p | 3s | 3p | 3d | 4s | 4p | 4d | 5s | 5p | 5d |
|----------------------|-------|-------|--------|--------|--------|--------|--------|--------|------|------|------|------|
| He ⁺ | 54.16 | 13.54 | 13.54 | 6.02 | 6.02 | 6.02 | 3.38 | 3.38 | 3.38 | 2.16 | 2.16 | 2.16 |
| Li ⁺ (80) | | 16.58 | 14.70 | 6.83 | 6.24 | 6.03 | 3.72 | 3.48 | 3.39 | 2.33 | 2.22 | 2.17 |
| Be ⁺ | | 18.13 | 14.18 | 7.25 | 6.27 | 6.03 | 3.88 | 3.47 | 3.40 | 2.41 | 2.21 | 2.17 |
| B ⁺ | | 23 | 20.41 | 9.00 | 7.27 | 6.43 | 4.52 | | 3.56 | | | |
| C ⁺ | | | 24.28 | 9.90 | 8.01 | 6.31 | 4.87 | 4.22 | 3.52 | 2.85 | | 2.24 |
| N ⁺ | | | 29.50 | 11.10 | 8.93 | 6.45 | 5.22 | | 3.54 | 3.04 | | |
| O ⁺ | | | 34.94 | 12.09 | 9.76 | 6.37 | 5.44 | | | 3.10 | | |
| F ⁺ | | | [34.9] | (13.1) | | | | | | | | |
| Ne ⁺ | | | 40.89 | 13.74 | 10.40 | 6.33 | 5.98 | | | | | |
| Na ⁺ | | | 47.02 | 14.31 | 10.83 | 6.20 | 6.18 | | | | | |
| Mg ⁺ | | | | 14.97 | 10.56 | 6.13 | 6.33 | 5.01 | 3.34 | 3.51 | 2.94 | 2.20 |
| Al ⁺ | | | | 18.74 | 14.12 | 8.19 | 7.48 | 5.73 | 5.15 | 3.92 | 3.22 | 3.34 |
| Si ⁺ | | | | | 16.27 | 6.46 | 8.24 | 6.25 | 3.80 | 4.18 | 3.44 | 2.40 |
| P ⁺ | | | | | 19.81 | 6.95 | 9.11 | 7.08 | 4.07 | 4.58 | | |
| S ⁺ | | | | | 23.32 | 9.70 | 9.80 | 7.51 | 4.54 | 4.75 | | |
| Cl ⁺ | | | | | [23.9] | 10.25 | 10.56 | 7.98 | 4.79 | 5.08 | | |
| A ⁺ | | | | | 27.62 | 11.23 | 11.00 | 8.42 | 4.90 | 5.16 | | |
| K ⁺ | | | | | 31.68 | 11.50 | 11.62 | 9.07 | 5.43 | 5.08 | | |
| Ca ⁺ | | | | | | 10.14 | 11.82 | 8.72 | 4.80 | 5.37 | 4.35 | 2.84 |
| Sc ⁺ | | | | | | 12.19 | 12.80 | 9.58 | 5.40 | 5.68 | | |
| Ti ⁺ | | | | | | 13.45 | 13.60 | 9.98 | 5.55 | 5.90 | | |
| V ⁺ | | | | | | (14.7) | (14.4) | (10.3) | | | | |
| Cr ⁺ | | | | | | (16.6) | (15.1) | (10.7) | | | | |
| Mn ⁺ | | | | | | 13.93 | 15.70 | 10.91 | 5.85 | 6.50 | | |
| Fe ⁺ | | | | | | (16.3) | (16.5) | (11.7) | | | | |
| Co ⁺ | | | | | | (17.2) | (16.8) | (11.7) | | | | |
| Ni ⁺ | | | | | | 18.19 | 17.15 | 11.75 | | 7.20 | | |
| Cu ⁺ | | | | | | 20.34 | 17.62 | 12.13 | | 6.99 | | |
| Zn ⁺ | | | | | | | 17.89 | 11.79 | 5.92 | 6.97 | 5.40 | 3.35 |
| Ga ⁺ | | | | | | | (18.8) | 14.00 | 5.68 | 7.14 | | |
| Ge ⁺ | | | | | | | | 15.98 | 6.00 | 8.28 | 6.21 | 3.62 |

FIRST IONIZATION POTENTIALS OF THE ELEMENTS

(Russell, Astrophys. Journ., 70, 1929; Mt. Wilson Contr. 383.)

In discussing the relative strength of the arc and enhanced lines a knowledge of ionization potentials is necessary. These are implicitly contained in Tables 604 and 605. Generally the energy difference between the normal states of the neutral atom and ion is required; complications arise in the Fe group. Table 604 gives the energy difference between the 4s state of the ion ($d^{n-2}s$) and the various states of the neutral atom, of which we must evidently choose the lowest, whether it be $4s(d^{n-2}s^2)$ or $3d(d^{n-1}s)$. Sometimes the $3d(d^{n-1})$ state of the ion is the lowest, and the values of Table 604 must be corrected. For the 2nd ionizations no such complication arises. Both tables include heavier elements for which data are at hand. Each is divided into two sections, corresponding to the "building on" of shells of s and d, or of p electrons. He, Be, Mg are put on line with Zn, Cd, Hg, because their spectra resemble those of the latter much more closely than those for Ca, Sr, Ba. The line below La marks the position of the rare earths, where 14 4f electrons are added which are listed separately.

While each shell of outer electrons is being completed, the ionization potential increases (minor irregularities occur for space quantization or interchange of s and d configurations. Maximum occurs when a shell is filled). The drop after the filling of an s shell in Be and Mg is between 1 and 2 volts; after completion of the combined s and d shells in Zn, Cd, Hg, it is 3 or 4 volts, while that following the completion of a p shell in the inert gases is much greater—8 to 16 volts. For the 2nd ionization, these discontinuities are greater in absolute value, but are a smaller fraction of the potentials themselves. (Continued on next page.)

First Ionization Potentials of the Elements

| | | | | | | | | | | | | | |
|----|-------|----|--------|----|--------|----|--------|----|--------|----|-------|----|-----|
| H | 13.59 | Li | 5.36 | Na | 5.11 | K | 4.33 | Rb | 4.13 | Cs | 3.86 | Ce | 6.9 |
| | | | | | | Ca | 6.09 | Sr | 5.65 | Ba | 5.19 | Pr | 5.8 |
| | | | | | | Sc | 6.57 | Yt | 6.5 | La | 5.5 | Nd | 6.3 |
| | | | | | | Ti | 6.80 | Zr | .. | Hf | .. | Il | .. |
| | | | | | | V | 6.76 | Cb | .. | Ta | .. | Sa | 6.6 |
| | | | | | | Cr | 6.74 | Mo | 7.35 | W | 8.1 | Eu | .. |
| | | | | | | Mn | 7.40 | Ma | .. | Re | .. | Gd | 6.7 |
| | | | | | | Fe | 7.83 | Ru | 7.7 | Os | .. | Tb | 6.7 |
| | | | | | | Co | 7.81 | Rh | 7.7 | Ir | .. | Dy | 6.8 |
| | | | | | | Ni | 7.64 | Pd | 8.28 | Pt | 9.2 | Ho | .. |
| | | | | | | Cu | 7.69 | Ag | 7.33 | Au | 9.20 | Er | .. |
| | | | | | | Zn | 9.36 | Cd | 8.95 | Hg | 10.39 | Tu | .. |
| He | 24.48 | Be | 9.29 | Mg | 7.61 | | | | | | | | |
| | | B | 8.28 | Al | 5.95 | Ga | 5.98 | In | 5.76 | Tl | 6.08 | Yb | 7.1 |
| | | C | 11.22 | Si | 8.14 | Ge | 7.89 | Sn | 7.37 | Pb | 7.38 | Lu | .. |
| | | N | 14.50 | P | [10.5] | As | [9.6] | Sb | 8.35 | Bi | 7.25 | | |
| | | O | 13.56 | S | 10.31 | Se | [9.4] | Te | [8.7] | Po | .. | | |
| | | F | [17.3] | Cl | [12.8] | Br | [11.4] | I | [10.2] | .. | .. | | |
| | | Ne | 21.47 | A | 15.69 | Kr | [13.9] | Xe | [12.1] | Rn | .. | | |

SECOND IONIZATION POTENTIALS OF THE ELEMENTS

(Russell, *Astrophys. Journ.*, 70, 1929, Mt. Wilson Contr. 383.)

(Continued from previous page)

The general character of the spectra of most of the heavier elements can be deduced from Tables 604 and 605. For the 2nd long period (Rb-Xe) the ionization potentials are nearly the same as for homologous elements in the first, but average a little lower. The same is true, in general, regarding the other energy levels, so that the arc and spark spectra of these elements show high- and low-excitation lines in the same regions for those of the first long period, but on the whole, a little farther to the red.

At the start of the next period, we find the lowest-known ionization potentials (Cs and Ba + for the second stage), which remain lower than in other periods until the rare-earth group begins. In these elements the outer electrons are two 6s, one 5d, and from one to 14 4f electrons, the ionization potential slowly rising as the 4f group is built up. For the earlier members, the lines of the ionized atom are the main features of the arc spectrum; those of the neutral atom are best brought out in the furnace; first ionization potentials are very low. The strong lines of the first spark spectrum shift towards the violet with increasing atomic numbers, practically proving that the second ionization potential also increases. The number of atomic-energy states should be much greater among the rare earths than for other elements. Their spectra are very intricate.

The shell of 4f electrons completed, the ionization potential ceases to have any important effect on the properties of the elements; note their chemical behavior and what is known of their spectra (Hf+, W). A considerable fall in the ionization potential should occur between the last rare earth, Lu, and Hf, and a gradual rise to Au and Hg. For Au and Hg ionization is more difficult than for the homologous elements in the preceding periods.

Second Ionization Potentials

| | | | | | | | | | | | | | |
|-----------------|-------|-----------------|--------|-----------------|--------|-----------------|--------|-----------------|-------|-----------------|-------|-----------------|------|
| He ⁺ | 54.16 | Be ⁺ | 18.13 | Mg ⁺ | 14.97 | Ca ⁺ | 11.82 | Sr ⁺ | 10.98 | Ba ⁺ | 9.96 | Ra ⁺ | 10.2 |
| | | | | | | Sc ⁺ | 12.80 | Yt ⁺ | 12.3 | La ⁺ | .. | Ac ⁺ | .. |
| | | | | | | Ti ⁺ | 13.60 | Zr ⁺ | .. | Hf ⁺ | .. | Th ⁺ | .. |
| | | | | | | V ⁺ | (14.7) | Cb ⁺ | .. | Ta ⁺ | .. | Pa ⁺ | .. |
| | | | | | | Cr ⁺ | (16.6) | Mo ⁺ | .. | W ⁺ | .. | U ⁺ | .. |
| | | | | | | Mn ⁺ | 15.70 | Ma ⁺ | .. | Re ⁺ | .. | | |
| | | | | | | Fe ⁺ | (16.5) | Ru ⁺ | .. | Os ⁺ | .. | | |
| | | | | | | Co ⁺ | (17.2) | Rh ⁺ | .. | Ir ⁺ | .. | | |
| | | | | | | Ni ⁺ | 18.19 | Pd ⁺ | 19.8 | Pt ⁺ | .. | | |
| | | | | | | Cu ⁺ | 20.34 | Ag ⁺ | 21.9 | Au ⁺ | .. | | |
| | | | | | | Zn ⁺ | 17.89 | Cd ⁺ | 16.82 | Hg ⁺ | 18.9 | | |
| | | | | | | Ga ⁺ | (18.8) | In ⁺ | .. | Tl ⁺ | 20.0 | | |
| Li ⁺ | (80) | B ⁺ | (23) | Al ⁺ | 18.74 | | | | | | | | |
| | | C ⁺ | 24.28 | Si ⁺ | 16.27 | Ge ⁺ | 15.98 | Sn ⁺ | 14.5 | Pb ⁺ | 14.96 | | |
| | | N ⁺ | 29.50 | P ⁺ | 19.81 | As ⁺ | .. | Sb ⁺ | .. | Bi ⁺ | .. | | |
| | | O ⁺ | 34.94 | S ⁺ | 23.32 | Se ⁺ | .. | Te ⁺ | .. | Po ⁺ | .. | | |
| | | F ⁺ | [34.9] | Cl ⁺ | [23.9] | Br ⁺ | .. | I ⁺ | .. | .. | .. | | |
| | | Ne ⁺ | 40.89 | A ⁺ | 27.62 | Kr ⁺ | 26.4 | Xe ⁺ | .. | Rn ⁺ | .. | | |
| | | Na ⁺ | 47.02 | K ⁺ | 31.68 | Rb ⁺ | .. | Cs ⁺ | .. | .. | .. | | |

TABLE 608.—Radiation Units

Radio, meter Radiation, micron Colorimetry, millimicron Spectroscopy, Angstrom X rays, milliangstrom γ rays, microangstrom

| Units | | Powers-of-10 equivalent of units listed in column 1 | | | | | | | |
|--------------------|-----------------|---|-----------|--------------|---------------|-----------------|-------------------|------------|------------|
| Name | Symbol | μ | $m\mu$ | \AA | $m\text{\AA}$ | $\mu\text{\AA}$ | C.G.S. unit cm | mm | m |
| Micron..... | μ | 1 | 10^3 | 10^4 | 10^7 | 10^{10} | 10^{-4} | 10^{-3} | 10^{-6} |
| Millimicron..... | $m\mu$ | 10^{-3} | 1 | 10 | 10^4 | 10^7 | 10^{-7} | 10^{-6} | 10^{-9} |
| Angstrom..... | \AA | 10^{-4} | 10^{-1} | 1 | 10^3 | 10^6 | 10^{-8} | 10^{-7} | 10^{-10} |
| Milliangstrom..... | $m\text{\AA}$ | 10^{-7} | 10^{-4} | 10^{-3} | 1 | 10^3 | 10^{-11} | 10^{-10} | 10^{-13} |
| Microangstrom..... | $\mu\text{\AA}$ | 10^{-10} | 10^{-7} | 10^{-6} | 10^{-3} | 1 | 10^{-14} | 10^{-13} | 10^{-16} |

TABLE 609.—Spectrum Ranges of Various Radiations

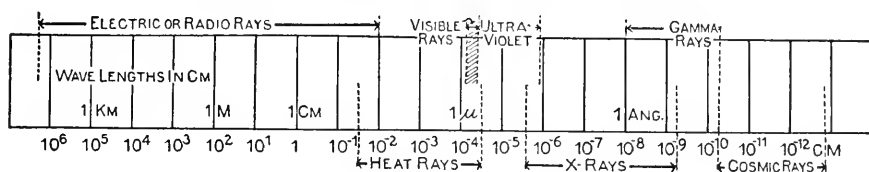


TABLE 610.—The Mechanical Effects of Radiation

(Jeans, Nature, 118, 1926, taken from Bull. 80, Nat. Res. Council, 1931.)

| Wave lengths, cm | Nature of radiation | Effect on atom | Temperature (degrees absolute) | Where found |
|--|-----------------------------|---|--|---------------------------------|
| 7500×10^{-8} 3750×10^{-8} | Visible light | Disturbs outermost electrons. | $\begin{cases} 3880 \\ \text{to} \\ 7700 \end{cases}$ | Stellar atmospheres. |
| 250×10^{-8} 10^{-8} | X rays | Disturb inner electrons. | $\begin{cases} 115,000 \\ \text{to} \\ 29,000,000 \end{cases}$ | Stellar interiors. |
| 5×10^{-9} 10^{-9} | Soft γ rays | Strip off all or nearly all electrons. | $\begin{cases} 58,000,000 \\ \text{to} \\ 290,000,000 \end{cases}$ | Central regions of dense stars. |
| 4×10^{-10} | γ rays of <i>RaB</i> | Disturb nuclear arrangement. | 720,000,000 | ? |
| 5×10^{-11} | Hardest γ rays | | 58×10^8 | |
| 4.5×10^{-12} | ? | Building of He atom out of H. | 64×10^9 | |
| 2×10^{-12} | Highly penetrating | Disintegrates nuclei. | 15×10^{10} | |
| 1.3×10^{-13} | ? | Annihilation or creation of proton and accompanying electron. | 22×10^{11} | |

NORMAL SERIES RELATIONS IN ATOMIC SPECTRA

(From manuscript by Henry Norris Russell, 1932.)

Every spectral line is believed to be emitted (or absorbed) in connection with the transition of an atom between two definite (quantized) states, of different energy-content—the frequency of the emitted or absorbed radiation being exactly proportional to the change of energy. The wave number (or frequency) of the line may therefore be expressed as the difference of two *spectroscopic terms* which measure, in suitable units, the energies of the initial and final states. It is customary to use in place of true frequency (sec^{-1}) the wave number (cm^{-1}), i. e., the number of waves in one centimeter in a vacuum. All quantities of the nature of frequency or energy are most conveniently expressed in cm^{-1} units. The multiplication of such values by c ($= 2.99796 \times 10^{10} \text{ cm. sec}^{-1}$) gives the true frequency in sec^{-1} and by hc ($= 1.9658 \times 10^{-16} \text{ erg cm}$) gives the true energy in ergs. Combinations between these terms occur according to definite laws, which enable us to classify them into systems, each containing a number of series of terms, which are usually multiple. The energy is often measured in “electron volts,” one of which $= 8106 \text{ cm}^{-1}$.

Terms, and the corresponding energies, may be measured either *upward* from the lowest energy state of the atom (in a given degree of ionization), or *downward* from a series limit (see below).

Series of terms are found in many spectra which satisfy the relation

$$y = s^2 R / (n + x)^2$$

Here y is the term-value, measured *downward* from the appropriate limit; $s = 1, 2, 3, \dots$ for neutral, singly, doubly, ionized atoms; R is the Rydberg constant, and n a “running” integer, which changes by 1 from one member of the series to the next. The “residual” x is often nearly constant (Rydberg’s formula). Ritz’s formula $x = \mu + ay$ (μ, a , constants) is usually a good approximation though not rigorous.

In the simplest spectra (e. g., Na, Ca^+) all the series have the same limit (corresponding to an isolated lowest energy state of the atom in its next higher degree of ionization) and long series of terms are known. But in most spectra there are many limits, corresponding to different states of the more highly ionized atom: few members of any given series are observed, and these perturb one another so that the Ritz formula no longer holds good.¹ The interpretation of these spectra depends upon the combination relations, formulated mainly by Sommerfeld and Landé, and the relations between electron configurations and term structure which have been put into definitive form by Hund.² These relations may be summarized as follows:

(a) The terms (or energy levels) of any given atom fall into two main groups of different *parity* (odd and even). Transitions producing spectral lines normally occur only between an odd and an even term. Those between terms of the same parity are “forbidden” but may occur under exceptional circumstances (as in gaseous nebulae).

(b) Terms of the same parity fall into *systems*—singlets, doublets, triplets, etc., characterized by the multiplicity R —the maximum number of components which a term may possess.

(c) In each system are found terms of various types denoted by the letters S, P, D, F, G, H, I. . . . The number of components increases along the series 1, 3, 5, but stops short at the maximum R (whether odd or even) characteristic of the system. The successive terms of a given series are always of the same multiplicity, type, and parity: but other terms of the same sort may be interpolated among them.

¹ Compare Shenstone and Russell, Phys. Rev., 39, 415, 1932.

² Linienspektren der Elemente, 1927.

NORMAL SERIES RELATIONS IN ATOMIC SPECTRA (continued)

(d) The components of a term are characterized by *inner quantum numbers* J , and the terms themselves by quantum numbers L , according to the following scheme.

TABLE 612.—Inner Quantum Numbers

| Type | L | Values of J for | | | | | |
|------|---|-----------------|-------------------------------|----------|---|-----------|---|
| | | Singlets | Doublers | Triplets | Quartets | Quintets | Septets |
| S | 0 | 0 | $\frac{1}{2}$ | 1 | $1\frac{1}{2}$ | 2 | $2\frac{1}{2}$ |
| P | 1 | 1 | $\frac{1}{2}$ $1\frac{1}{2}$ | 0 1 2 | $\frac{1}{2}$ $1\frac{1}{2}$ $2\frac{1}{2}$ | 1 2 3 | $1\frac{1}{2}$ $2\frac{1}{2}$ $3\frac{1}{2}$ |
| D | 2 | 2 | $1\frac{1}{2}$ $2\frac{1}{2}$ | 1 2 3 | $\frac{1}{2}$ $1\frac{1}{2}$ $2\frac{1}{2}$ $3\frac{1}{2}$ | 0 1 2 3 4 | $\frac{1}{2}$ $1\frac{1}{2}$ $2\frac{1}{2}$ $3\frac{1}{2}$ $4\frac{1}{2}$ |
| F | 3 | 3 | $2\frac{1}{2}$ $3\frac{1}{2}$ | 2 3 4 | $1\frac{1}{2}$ $2\frac{1}{2}$ $3\frac{1}{2}$ $4\frac{1}{2}$ | 1 2 3 4 5 | $\frac{1}{2}$ $1\frac{1}{2}$ $2\frac{1}{2}$ $3\frac{1}{2}$ $4\frac{1}{2}$ $5\frac{1}{2}$ |
| G | 4 | 4 | $3\frac{1}{2}$ $4\frac{1}{2}$ | 3 4 5 | $2\frac{1}{2}$ $3\frac{1}{2}$ $4\frac{1}{2}$ $5\frac{1}{2}$ | 2 3 4 5 6 | $1\frac{1}{2}$ $2\frac{1}{2}$ $3\frac{1}{2}$ $4\frac{1}{2}$ $5\frac{1}{2}$ $6\frac{1}{2}$ |

Line-producing combinations occur only between components for which the difference ΔJ is 0 or ± 1 . The combination of two multiple terms thus gives rise to a group of lines called a *multiplet*.

(e) In such a group the lines for which $\Delta J = \Delta L$ are the strongest (often called the diagonal lines) and the line for which the J 's are largest is the strongest of these. These intensity relations (which have been calculated in detail) are of great practical importance. The successive separations of the components of a multiple term are normally proportional to the larger value of J involved: (Landé's interval rule). The factor of proportionality is different for different terms. It increases rapidly with the atomic number Z , and is roughly proportional to Z^2 for similar elements, such as Ca, Sr, Ba. The character of the *Zeeman effect* for any line is completely defined by the numbers R , L , J , for the two levels involved. It is usually possible to work backward from a completely resolved Zeeman pattern and find the nature of the terms involved—a great aid in the analysis of complex spectra.

(f) In the simplest spectra, all the terms for which L is even or odd are themselves even or odd, so that $\Delta L = \pm 1$ for all lines. But in complex spectra all values of L appear among both odd and even terms, and transitions for which $\Delta L = 0$ also give strong multiplets. Transitions for which $\Delta L = \pm 2$, and a few for which it is ± 3 , are known, but usually give faint lines. Lines for $\Delta J = \pm 2$ are however extremely rare (except in strong magnetic fields).

(g) In arc spectra—that is, the spectra of neutral atoms—the multiplicities of the various systems are always even if the atomic number is odd, and vice versa, so that odd and even multiplicities *alternate*. The spectrum of a singly ionized atom is similar in general structure to that of the element of next preceding atomic number; of a doubly ionized atom to the element preceding this, and so on (the *displacement law*). In consequence the alternation of odd and even multiplicities is found for successive ionizations of the same element.

(h) The maximum multiplicity in arc spectra is 2 for elements in which there is but one electron outside "completed shells" (Li, Na, K, Rb, Cs; also B, Al, Ga, In, Tl). From these elements it increases by steps of a unit till the "shell" is half completed and then diminishes in the same way—the maximum values being 5 for O, S, Se (Te) and 8 for Mn, (Ma) Re. (Parentheses denote predictions for incompletely analyzed spectra.) In the rare earths it probably rises to 11. When the maximum multiplicity increases with

NORMAL SERIES RELATIONS IN ATOMIC SPECTRA (*continued*)

increasing atomic number the spectroscopic terms have the components with small J -values the lowest. Beyond the maximum they are "inverted" with the large J 's low. The higher the maximum multiplicity the greater, generally speaking, is the complexity of the spectrum. The terms of lowest energy are even in all arc spectra except those of B, N, F, and their homologues, and of some of the rare earths.

(i) *Inter-system combinations* between terms of different multiplicities are common when $\Delta R = 2$, and a few are known for which $\Delta R = 4$. They are faint for elements of small atomic number, but often strong when this is large. Deviations from the interval and intensity rules, and the usual rules for the Zeeman effect, also become great in this case. In extreme instances classification by term-types is hardly practicable, though parity and inner-quantum number remain definite.

(j) Arc lines originating in the lowest energy-level in the atom are strong at low temperatures, and usually easily reversed, and are strengthened in the sun-spot spectrum; while those arising from high levels do not reverse, are produced only at higher temperatures, and are little affected, or even weakened, in the spots. The gradation of these properties follows the energy-levels so closely that the temperature classification of the lines ranks with the frequency-differences and the Zeeman effect as a fundamental guide in the interpretation of many-lined spectra.

The *raies ultimes*, which are the last to disappear when the quantity of the element is diminished, are strong lines arising from the lowest level (or occasionally the next).

Resonance lines are those corresponding to the transition from the lowest level to the next lowest with which it can combine. Intersystem combinations, which are usually faint in the arc and spark, very rarely appear as *raies ultimes*, although they are often very strong in the furnace, and important resonance lines.

In spark spectra, lines arising from the lowest levels are strong in the arc, sometimes appear in the furnace, and tend to reverse in the spark, while those from high levels are faint in the arc (if present) and are usually diffuse in the spark.

TABLE 613.—Spectroscopic Notation

Until recently great diversity has prevailed, but an informal committee of American spectroscopists, after extensive correspondence with a large number of workers here and abroad, have suggested a notation¹ which has been generally adopted.

The successive spectra of an element are denoted by Roman numerals, e. g., Ti I, Ti II, Ti III for the spectra of neutral, singly, and doubly ionized titanium. (Lines of Rb IX have been identified.)

The type of term is denoted by letters, corresponding to the quantum numbers L of Hund's theory as follows:

| Letter | S | P | D | F | G | H | I | K | L | M |
|--------|---|---|---|---|---|---|---|---|---|---|
| L | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |

(Values of L greater than 6 have not yet been met with, but are anticipated among the rare earths.)

The multiplicity is denoted by a superscript at the left 1, 2 . . . for singlet, doublet terms. The inner quantum number is used as a subscript at the right, and the parity indicated by superscript ° at the right for odd terms . . . e. g., 'P_{2½}° read "quartet P odd 2½".

¹ Phys. Rev., 33, 900, 1929.

NORMAL SERIES RELATIONS IN ATOMIC SPECTRA (continued)

Terms of the same sort are distinguished by prefixing a lower case letter— a^3D , b^3D , etc. Lines are represented as the difference of two terms—the lower one coming first, e.g., $a^3D_2 - y^3F_2^\circ$.

It is recommended that the lowest terms in the spectrum, and others of the same type, multiplicity, and parity be lettered a, b, c—beginning with the lowest. Terms of the opposite parity should be lettered z, y, x—beginning with the lowest. In this way all resonance lines will be designated as $a(\) - z(\)^\circ$.

In most spectra there is a group of low metastable terms of the same parity as the lowest term, separated by a considerable interval from higher terms of the same parity. The letters a, b, c, d should be reserved for the low terms and the high terms should begin uniformly with e.

In a good many spectra, energy levels have been detected whose reality is proved by their combinations, but which can not (at present) be fitted definitely into the scheme of multiple terms. Such levels are to be denoted by Arabic numbers (beginning at the lowest level). It can always be told whether such a level is odd or even, and the inner quantum number can usually, and the multiplicity sometimes be assigned. The corresponding indices are then added to the number, e.g., $^{423}_{1/2}^\circ$.

This notation suffices for the formal description of even the most complex spectra. A further analysis giving the electron configurations responsible for each term should be made so far as possible. Following Hund the individual electrons in an atom may be defined by two quantum numbers, "azimuthal" l and "total" n . The latter is denoted by a numerical prefix, the former by the letters s, p, d, ... as follows:

TABLE 614.—Comparison Azimuthal and Bohr's Quantum Numbers

| Letter | s | p | d | f |
|-------------------------------|---|---|---|---|
| Azimuthal quantum number..... | l | 1 | 2 | 3 |
| Bohr's quantum number..... | k | 1 | 2 | 3 |

A 6d electron (for example) has $n=6$, $l=2$. This is exactly equivalent to Bohr's notation 6_{d} —the subscript by the value of k . Similarly $4p=4_{\text{p}}$, $5s=5_{\text{s}}$. (Note that $n \geq l+1$.)

The spin of the electron s , being always $\frac{1}{2}$, need not be specified.

The number of electrons of a given type in an atom is represented by an exponent, e.g., $3d^5$.

The quantities s and l are vectors, of the dimensions of angular momentum. By space quantization they combine to give the vectors S , L , and J which define the spectroscopic properties of the energy levels. The multiplicity $R=S+1$. The details are discussed in Hund's book. The total quantum numbers n are not vectors and do not give a resultant.

A complete specification of an electron configuration would include all the inner electrons—the normal state of iron, for example is $1s^2 2s^2 2p^6 3s^2 3p^6 3d^6 4s^2$. For ordinary spectroscopic purposes the complete shells may be omitted, reducing the foregoing to $3d^6 4s^2$. For brevity the total quantum numbers may be omitted when their values are the lowest which the electron can have without belonging to already complete shells. For example, for spectra from K I to Zn I, and Ca II to Ga II, these electrons are $4s$, $4p$, $3d$, $4f$. The normal state of Fe I is then represented by $d^6 s^2 {}^5D_4$ and that of O II by $s^2 p^3 {}^4S_{3/2}$.

Odd and even terms are those in which the sum of the l 's for all electrons is odd or even; i.e., in which the number of p or f electrons together is odd or even. Completed shells always give an even sum and may be disregarded.

NORMAL SERIES RELATIONS IN ATOMIC SPECTRA (concluded)

Series of terms arise from configurations in which one electron, keeping the same value of l , has successively higher values of n , the total quantum number. A configuration such as $3d4s4p$ theoretically belongs therefore to three different series in which either the d , the s , or the p electron takes higher total quantum numbers. In practice this complication is rare as there is almost always one electron which is more easily detached than the others, and is therefore the one to take the higher quantum numbers and give the series. An electron whose total quantum number is higher than those of the electrons discussed in the last section may always be regarded as the most easily detached, as may also one belonging to a group which is not represented in the configurations giving the low terms of the spectrum.

The limiting configuration (i.e., the one obtained by the removal of the electron which takes successively higher values of n to give the series) usually gives multiple terms. Each separate level of these terms is the limit of certain sets of the individual levels of the multiple terms converging to the limit. The configuration of the limit is to be represented as above, followed in parentheses by the notation for the particular type of term which is the limit for the series under consideration, than by the "running" electron, then by the notation for the term (or particular level) given by the whole configuration. For instance the s^2p^3 configuration of O II gives $^4S^\circ$, $^2D^\circ$ and $^2P^\circ$ terms. If we add to this one np electron to get terms of O I the $^4S^\circ$ term gives 5P and 3P , the $^2D^\circ$ gives 3P , 3D , 3F , 1P , 1D , 1F and the $^2P^\circ$ gives 3S , 3P , 3D , 1S , 1P , 1D terms. Thus, theoretically, the s^2p^3np configuration gives three 3P terms, two 3D terms, two 1P terms and two 1D terms. For distinguishing between them it is most convenient to use the notation suggested above. The three P terms would be written $s^2p^3(^4S^\circ)np^3P$, $s^2p^3(^2D^\circ)np^3P$, and $s^2p^3(^2P^\circ)np^3P$.

The notation here described may be considerably simplified for many of the simpler spectra. The abbreviations employed should in all cases be clearly explained by the author.

TABLE 615.—Comparison of Notations

Among the earlier systems of notation which are frequently met with are the following:

| | | | | | |
|------------------|----|----|----|----|----|
| Even terms | S | P' | D | F' | G |
| Odd terms | S' | P | D' | F | G' |

| Adopted notation | Fowler | Paschen-Götze |
|---|----------------------|-------------------|
| 1S_0 | S | S |
| 1P_1 | P | P |
| 1D_2 | D | D |
| 1F_3 | F | F |
| $^2S_{\frac{1}{2}}$ | α | S |
| $^2P_{\frac{1}{2}}$ $^2P_{\frac{3}{2}}$ | π_1 π_2 | p_1 p_2 |
| $^2D_{\frac{3}{2}}$ $^2D_{\frac{5}{2}}$ | δ_1 δ' | d_1 d_2 |
| $^2F_{\frac{3}{2}}$ $^2F_{\frac{5}{2}}$ | ϕ_1 ϕ' | f_1 f_2 |
| 3S_1 | S | s |
| 3P_2 3P_1 3P_0 | p_1 p_2 p_3 | p_1 p_2 p_3 |
| 3D_3 3D_2 3D_1 | d d' d'' | d_1 d_2 d_3 |
| 3F_4 3F_3 3F_2 | f f' f'' | f_1 f_2 f_3 |

As regards the total quantum numbers Fowler usually designates the lowest members of the series by $1s$, $1p$, $2d$, $3f$ and Paschen-Götze by $1s$, $2p$, $3d$, etc.

The current notation uses Bohr's values which differ from element to element: thus the lowest term in Li is 2^2S , in Na 3^2S , in K 4^2S , in Rb 5^2S , and in Cs 6^2S .

ULTIMATE SPECTRUM LINES AND RAIES ULTIMES*

(See p. 508 for explanation.)

(Selected by permission from I. C. T., 5, 322, Meggers.)

| | | | | | | | | |
|-----------|----------------|---------------|-------|----------------|-------------------------------|-------|----------------|-------------------|
| A I | 6965.43 | s_6-p_2 | Cr I | 5204.54 | $^5S_2-^5P_1$ | La II | 4123.23 | $^3D_2-^3F_3$ |
| | 7067.22 | s_6-p_3 | | 5206.04 | $^5S_2-^5P_2$ | Li I | 3232.67 | $^2S_1-^2P_{1,2}$ |
| | 7503.87 | s_2-p_1 | | 5208.43 | $^5S_2-^5P_3$ | | 6707.86 | $^2S_1-^2P_{1,2}$ |
| Ag I | 3280.67 | $^2S_1-^2P_2$ | Cs I | 4555.3 | $^2S_1-^2P_2$ | Lu I | 4518.54 | |
| | 3382.89 | $^2S_1-^2P_1$ | | 4593.2 | $^2S_1-^2P_1$ | Lu II | 3397.02 | |
| Al I | 3082.16 | $^2P_1-^2D_2$ | Cu I | 3247.55 | $^2S_1-^2P_2$ | | 3472.49 | |
| | 3092.72 | $^2P_2-^2D_3$ | | 3273.96 | $^2S_1-^2P_1$ | | 3554.43 | |
| | 3092.85 | $^2P_2-^2D_2$ | Dy I | 4000.50 | | Mg I | 3829.36 | $^3P_0-^3D_1$ |
| | 3944.03 | $^2P_1-^2S_1$ | | 4046.00 | | | 3832.31 | $^3P_1-^3D_2$ |
| | 3961.54 | $^2P_2-^2S_1$ | | 4077.98 | | | 3838.29 | $^3P_2-^3D_3$ |
| B II | 3452.33 | — | | 4167.99 | | Mn I | 4030.76 | $^6S_3-^6P_4$ |
| Ba I | 5424.63 | $^3P_2-^3D_3$ | | 4211.74 | | | 4033.07 | $^6S_3-^6P_3$ |
| | 5519.11 | $^3P_1-^3D_2$ | Er I | 3499.12 | | | 4034.49 | $^6S_3-^6P_2$ |
| | 5535.53 | $^1S_0-^1P_1$ | | 3692.65 | | Mo I | 3798.26 | $^5S_2-^5P_3$ |
| | 5777.7 | $^3P_0-^3D_1$ | | 3906.34 | | | 3864.12 | $^5S_2-^5P_3$ |
| Ba II | 4554.04 | $^2S_1-^2P_2$ | Eu I | 4129.72 | | | 3902.96 | $^5S_2-^5P_1$ |
| | 4934.09 | $^2S_1-^2P_1$ | | 4205.03 | | N I | 4099.96 | $^2P_1-^2D_2$ |
| Be I | 3321.01 | $^3P_0-^3S_1$ | F I | 6856.01 | $^4P_3-^4D_4$ | | 4109.94 | $^2P_2-^2D_3$ |
| | 3321.09 | $^3P_1-^3S_1$ | | 6902.46 | $^4P_2-^4D_3$ | N II | 5666.6 | $^3P_1-^3D_2$ |
| | 3321.35 | $^3P_2-^3S_1$ | Fe I | 3719.94 | $^5D_4-^5F_5$ | | 5675.9 | $^3P_0-^3D_1$ |
| Be II | 3130.42 | $^2S_1-^2P_2$ | | 3737.14 | $^5D_3-^5F_4$ | | 5679.5 | $^3P_2-^3D_3$ |
| | 3131.06 | $^2S_1-^2P_1$ | | 3745.56 | $^5D_2-^5F_3$ | N III | 4097.3 | $^2P_1-^2S_1$ |
| Bi I | 3067.73 | $^4S_2-^4P_1$ | | 3748.26 | $^5D_1-^5F_2$ | | 4103.4 | $^2P_2-^2S_1$ |
| Br II (?) | 4704.83 | — | | 3745.90 | $^5D_0-^5F_1$ | Na I | 3302.34 | $^2S_1-^2P_2$ |
| | 4785.48 | — | Ga I | 4033.01 | $^2P_1-^2S_1$ | | 3302.94 | $^2S_1-^2P_1$ |
| | 4816.72 | — | | 4172.05 | $^2P_2-^2S_1$ | | 5889.97 | $^2S_1-^2P_2$ |
| C II | 4267.02 | $^2D_2-^2F_3$ | Gd I | 3646.19 | | | 5895.93 | $^2S_1-^2P_1$ |
| | 4267.27 | $^2D_3-^2F_4$ | | 3768.40 | | Nd I | 3951.15 | |
| Ca I | 4226.73 | $^1S_0-^1P_1$ | Ge I | 3039.08 | $^1D_2-^1P_1$ | | 4177.34 | |
| | 4454.78 | $^3P_0-^3D_1$ | | 3269.49 | $^1D_2-^3P_1$ | | 4303.61 | |
| | 4455.88 | $^3P_1-^3D_2$ | | 4226.61 | $^1S_0-^1P_1$ | Ne I | 5400.56 | s_4-p_1 |
| | 4456.62 | $^3P_2-^3D_3$ | H I | 6562.79 | $R(\frac{1}{2}-\frac{1}{2})$ | | 5832.49 | s_2-p_1 |
| Ca II | 3933.67 | $^2S_1-^2P_2$ | | 4861.33 | $R(\frac{1}{2}-\frac{1}{2})$ | | 6402.25 | s_6-p_1 |
| | 3968.48 | $^2S_1-^2P_1$ | He I | 3888.64 | $^3S_1-^3P_2$ | Ni I | 3414.77 | $^3D_3-^3F_4$ |
| Cb I | 4058.97 | $^6D_5-^6F_6$ | | 5875.63 | $^3P_2-^3D_3$ | | 3492.97 | $^3D_2-^3P_1$ |
| | 4079.73 | $^6D_4-^6F_5$ | He II | 4685.81 | $4R(\frac{1}{2}-\frac{1}{2})$ | | 3515.06 | $^3D_2-^3F_3$ |
| | 4100.97 | $^6D_3-^6F_4$ | Hf I | 3072.88 | | | 3524.54 | $^3D_3-^3P_2$ |
| | 4123.85 | $^6D_2-^6F_3$ | | 4093.17 | | Os I | 3262.30 | |
| | 4137.13 | $^6D_1-^6F_2$ | Hf II | 3134.72 | | | 3267.94 | |
| Cb II | 3094.19 | $^5F_5-^5G_6$ | Hg I | 3650.15 | $^3P_2-^3D_3$ | | 3301.56 | |
| | 3130.78 | $^5F_4-^5G_5$ | | 3654.83 | $^3P_1-^3D_2$ | | 3752.54 | |
| | 3163.37 | $^5F_3-^5G_4$ | | 3662.88 | $^3P_0-^3D_1$ | | 3782.20 | |
| | 3194.95 | $^5F_2-^5G_3$ | Ho I | 3748.19 | | Pb I | 3639.58 | $^3P_1-^3P_1^1$ |
| | 3225.47 | $^5F_1-^5G_2$ | | 3891.02 | | | 3683.47 | $^3P_1-^3P_1^0$ |
| Cd I | 3403.65 | $^3P_0-^3D_1$ | I I | 5161.2 | | | 4057.83 | $^3P_2-^3P_1^1$ |
| | 3466.20 | $^3P_1-^3D_2$ | | 5464.6 | | Pd I | 3404.59 | $^3D_3-^3F_4$ |
| | 3610.51 | $^3P_2-^3D_3$ | In I | 4101.76 | $^2P_1-^2S_1$ | | 3421.23 | $^3D_2-^3D_1^1$ |
| Ce II | 4012.40 | | | 4511.31 | $^2P_2-^2S_1$ | | 3516.95 | $^3D_2-^3P_1$ |
| | 4040.76 | | Ir I | 3220.79 | | | 3609.55 | $^3D_2-^3F_3$ |
| | 4165.61 | | | 3437.05 | | | 3634.68 | $^3D_3-^3P_2$ |
| | 4186.60 | | | 3513.67 | | Pr I | 4062.83 | |
| Cl I | 4794.5 | | K I | 4044.16 | $^2S_1-^2P_2$ | | 4179.43 | |
| | 4810.0 | | | 4047.22 | $^2S_1-^2P_1$ | | 4189.52 | |
| | 4819.4 | | Kr I | 5570.29 | | Pt I | 3064.71 | $^3D_3-^3P_2$ |
| Co I | 3453.51 | $^4F_5-^4G_6$ | | 5870.92 | | Ra I | 4825.94 | $^1S_0-^1P_1$ |
| | 3465.79 | $^4F_5-^4G_6$ | La I | 5455.11 | $^2D_3-^2D_1^3$ | | 3814.44 | $^2S_1-^2P_2$ |
| | 3529.81 | $^4F_4-^4G_5$ | | 5930.59 | $^2D_3-^2F_4$ | Ra II | 4682.20 | $^2S_1-^2P_1$ |
| Cr I | 4254.34 | $^7S_3-^7P_4$ | | 6249.92 | $^4F_5-^4G_6$ | | 4201.81 | $^2S_1-^2P_2$ |
| | 4274.80 | $^7S_3-^7P_3$ | La II | 3949.10 | $^3D_3-^3F_4$ | Rb I | 4215.58 | $^2S_1-^2P_1$ |
| | 4289.73 | $^7S_3-^7P_2$ | | 4077.35 | $^3D_1-^3F_2$ | | | |

* Printed in bold-face type.

ULTIMATE SPECTRUM LINES AND RAIES ULTIMES *

(Selected by permission from I. C. T., 5, 322, Meggers.)

Raies Ultimes.—The strongest lines of any element (the last to disappear when the quantity present is diminished) usually arise from transitions from the lowest level to middle levels of the same multiplicity and belonging to the same family. Among the various lines in a multiplet, that involving the highest inner quantum number is the most persistent; among transitions to terms of the same family, the term of the greatest azimuthal quantum number has the advantage; and the larger multiplicities are preferred to the smaller. In a few cases, the combination of these influences causes a line originating from a level a little above the lowest to be the most persistent of all.

| | | | | | | | | |
|-------|----------------|---------------|-------|----------------|-------------|-------|----------------|-------------|
| Rh I | 3323.10 | $4F_5-4G_5$ | Ta I | 3311.14 | | V I | 3102.30 | $5F_4-5G_5$ |
| | 3396.82 | $4F_5-4F_1^1$ | | 3318.85 | | | 3110.71 | $5F_3-5G_4$ |
| | 3434.90 | $4F_5-4G_6$ | | 3406.65 | | | 3118.38 | $5F_2-5G_3$ |
| | 3657.99 | $4F_4-4D_3$ | Tb I | 3509.18 | | | 3125.29 | $5F_1-5G_2$ |
| | 3692.35 | $4F_5-4D_4$ | | 3561.75 | | W I | 4008.76 | $7S_3-7P_4$ |
| Ru I | 3436.74 | $5F_4-5G_5$ | | 3848.76 | | | 4294.62 | $7S_3-X_2$ |
| | 3498.95 | $5F_6-5G_6$ | | 3874.19 | | | 4302.12 | $7S_3-5P_3$ |
| | 3596.17 | $5F_3-5G_4$ | Th I | 3538.75 | | W II | 3613.79 | |
| S I | 4694.2 | $5S_2-5P_3$ | | 3601.05 | | Xe I | 4500.98 | |
| | 4695.5 | $5S_2-5P_2$ | | 4019.14 | | | 4624.28 | |
| | 4696.3 | $5S_2-5P_1$ | Th II | 3290.59 | | | 4671.23 | |
| Sa I | 4390.87 | | Ti I | 3635.47 | $3F_2-3G_3$ | Yt I | 4643.69 | $2D_2-2F_3$ |
| | 4424.35 | | | 3642.68 | $3F_3-3G_4$ | | 4674.84 | $2D_3-2F_4$ |
| | 4434.34 | | | 3653.49 | $3F_4-3G_5$ | Yt II | 3710.30 | $3D_3-3F_4$ |
| Sb I | 3232.52 | $2P_1^1-2P_1$ | | 4981.73 | $5F_5-5G_6$ | | 3774.33 | $3D_2-3F_3$ |
| | 3267.48 | $2P_1^1-2P_1$ | | 4991.07 | $5F_4-5G_5$ | | 3788.69 | $3D_1-3F_2$ |
| Sc I | 3907.49 | $2D_2-2F_3$ | | 4999.51 | $5F_3-5G_4$ | Yb I | 3289.37 | |
| | 3911.81 | $2D_3-2F_4$ | | 5007.21 | $5F_2-5G_3$ | | 3694.20 | |
| Sc II | 3613.83 | $3D_3-3F_4$ | | 5014.25 | $5F_1-5G_2$ | | 3988.01 | |
| | 3630.75 | $3D_2-3F_3$ | Ti II | 3349.03 | $4F_5-4G_6$ | Zn I | 3282.32 | $3P_0-3D_1$ |
| | 3642.81 | $3D_1-3F_2$ | | 3361.22 | $4F_4-4G_5$ | | 3302.6 | $3P_1-3D_2$ |
| Se I | 4730.9 | $5S_2-5P_3$ | | 3372.80 | $4F_3-4G_4$ | | 3344.5 | $3P_2-3D_3$ |
| | 4739.1 | $5S_2-5P_2$ | | 3383.77 | $4F_2-4G_3$ | Zr I | 3519.61 | $3F_4-3G_5$ |
| | 4742.3 | $5S_2-5P_1$ | Tl I | 3775.73 | $2P_1-2S_1$ | | 3547.69 | $3F_3-3G_4$ |
| | | | | 5350.47 | $2P_2-2S_1$ | | 3601.19 | $3F_2-3G_3$ |
| Si I | 3905.52 | $1S_0-1P_1$ | Tu I | 3462.21 | | | 4687.80 | $5F_6-5G_6$ |
| Sn I | 3009.14 | $3P_1-3P_1^1$ | | 3761.34 | | | 4710.08 | $5F_4-5G_5$ |
| | 3034.12 | $3P_1-3P_1^1$ | | 3761.91 | | | 4739.48 | $5F_3-5G_4$ |
| | 3175.05 | $3P_2-3P_1^1$ | | 3761.91 | | | 4772.31 | $5F_2-5G_3$ |
| | 3262.33 | $1D_2-1P_1$ | U I | 3552.20 | | | 4815.62 | $5F_1-5G_2$ |
| | 4524.74 | $1S_0-1P_1$ | | 3672.59 | | Zr II | 3391.98 | $4F_5-4G_6$ |
| Sr I | 4607.34 | $1S_0-1P_1$ | | 4241.68 | | | 3438.23 | $4F_4-4G_5$ |
| | 4832.07 | $3P_2-3D_3$ | V I | 3183.42 | $4F_3-4G_4$ | | 3496.21 | $4F_3-4G_4$ |
| | 4872.48 | $3P_1-3D_2$ | | 3183.96 | $4F_4-4G_5$ | | 3572.47 | $4F_2-4G_3$ |
| | 4962.25 | $3P_0-3D_1$ | | 3184.00 | $4F_2-4G_3$ | | | |
| Sr II | 4077.71 | $2S_1-2P_2$ | | 3185.41 | $4F_5-4G_6$ | | | |
| | 4215.52 | $2S_1-2P_1$ | | | | | | |

* Printed in bold-face type.

TABLE 618
PERSISTENT LINES, SPARK SPECTRA
 (Taken from Russell, *Astrophys. Journ.*, 70, II, 1929.)
Wave Lengths in I. A.

| He ⁺ | 303.8 | Be ⁺ | *3130.42 | Mg ⁺ | *2795.52 | Ca ⁺ Sc ⁺ | *3933.66 *3613.84 *3383.76 *3093.10 *2835.64 *2576.12 *2382.04 *2378.62 2216.47 2247.00 2061.96 1414.4 | Sr ⁺ Yt ⁺ | *4077.71 *3710.30 *3391.96 *3094.20 *2816.16 | Ba ⁺ La ⁺ | *4554.04 *3949.10 *2773.37† | Ra ⁺ Ac ⁺ | 3814.43 | ² S ₁ - ² P ₂ ³ D ₃ - ³ F ₄ ⁴ F ₅ - ⁴ G ₆ ⁵ F ₅ - ⁵ G ₆ ⁶ D ₅ - ⁶ F ₆ ⁷ S ₃ - ⁷ P ₁ ⁶ D ₅ - ⁶ F ₆ ⁵ F ₅ - ⁵ G ₆ ⁴ F ₅ - ⁴ G ₆ ³ D ₃ - ³ P ₂ ² S ₁ - ² P ₂ ¹ S ₀ - ¹ P ₁ |
|-----------------|--------|--|---|--|--|---|---|---|---|---|---|---|---|--|
| | | | | | | Ti ⁺ V ⁺ Cr ⁺ | *3383.76 *3093.10 *2835.64 | Zr ⁺ Cb ⁺ Mo ⁺ | *3391.96 *3094.20 *2816.16 | Hf ⁺ Ta ⁺ W ⁺ | *2773.37† | Th ⁺ Pa ⁺ U ⁺ | | |
| | | | | | | Mn ⁺ Fe ⁺ Co ⁺ Ni ⁺ Cu ⁺ Zn ⁺ Ga ⁺ | *2576.12 *2382.04 *2378.62 2216.47 2247.00 2061.96 1414.4 | Ma ⁺ Ru ⁺ Rh ⁺ Pd ⁺ Ag ⁺ Cd ⁺ In ⁺ | 2296.53 *2437.81 *2265.04 1586.4 | Re ⁺ Os ⁺ Ir ⁺ Pt ⁺ Au ⁺ Hg ⁺ Tl ⁺ | 2082.06 1942.3 1321.8 | | | |
| Li ⁺ | (192)‡ | B ⁺ | 1362.46 | Al ⁺ | 1670.98 | | | | | | | | | |
| | | C ⁺ N ⁺ O ⁺ F ⁺ Ne ⁺ Na ⁺ | 858.56 1085.70 834.46 606.81 460.72 376.34 | Si ⁺ P ⁺ S ⁺ Cl ⁺ A ⁺ K ⁺ | 1533.55 1542.29 1259.53 1071.03 919.69 612.61 | Ge ⁺ As ⁺ Se ⁺ Br ⁺ Kr ⁺ Rb ⁺ | 1649.27 886.29 | Sn ⁺ Sb ⁺ Te ⁺ I ⁺ Xe ⁺ Cs ⁺ | 1900.05 | Pb ⁺ Bi ⁺ Po ⁺ Rn ⁺ .. | *2203.5 | ² P ₂ - ² S ₁ ³ P _{1/2} - ³ D ₃ ¹ ⁴ S ₂ - ⁴ P ₃ ³ P ₂ - ³ P ₃ ² P ₂ - ² P ₁ ¹ S ₀ - ¹ P ₁ | | |

* Recorded by De Gramont (C. R., 171, 1105, 1920) or Meggers and Kless (Journ. Opt. Soc. Amer., 12, 417, 1926) as *raies ultimes*, which actually have been observed to persist in the manner supposed.

† See note for *Hf* in Table 617.

‡ Not yet observed; estimated by extrapolation of series.

TABLE 619.—Resonance Lines

(LaPorte, Meggers, Journ. Opt. Soc. Amer., 11, 462, 1925.)

An electron jump which involves the lowest term and gives rise to the line of greatest wave length, i. e., the first transition which is connected with emission and requires the least energy for excitation, in spectra where there is no metastable level lying close to the lowest term gives a resonance line.

| Z | Element | Arc | | Spark | |
|----|---------|--------------------------------|------------------|-------------------|-----------|
| | | Terms | λ | Terms | λ |
| 19 | K | $^2S_1 - ^2P_2$ | 7664.94 | | |
| 37 | Rb | | 7800.29 | | |
| 20 | Ca | $1S_0 - ^3P_1$ | 6572.78 | $^2S_1 - ^2P_2$ | 3933.66 |
| 38 | Sr | | 6892.62 | | 4077.71 |
| 21 | Sc | $(^2D_3 - ^4F_4)$ | >6413 | $^3D_3 - ^3F_4$ | 3613.86 |
| 39 | Y | | >6933 | | 3710.30 |
| 22 | Ti | $^3F_4 - ^5G_5$ | 6295.30 | $^4F_5 - ^4G_6$ | 3349.41 |
| 40 | Zr | | ? | | 3391.96 |
| 23 | V | $^4F_5 - ^6D_4, ^6G_6?$ | 5632.47 | $^5F_5 - ^5G_6$ | 3093.10 |
| 41 | Cb | | ? | | 3094.20 |
| 24 | Cr | $^7S_3 - ^7P_4$ | 4254.34 | $^6D_3 - ^6F_6$ | 2835.64 |
| 42 | Mo | | 3798.26 | | 2816.16 |
| 25 | Mn | $^6S_3 - ^8P_4$ | 5394.68 | $^7S_2 - ^7P_4$ | 2576.12 |
| 43 | ... | | | | |
| 26 | Fe | $^5D_4 - ^7\bar{D}_5, ^7F_5$ | 5166.29; 4375.93 | $^6D_3 - ^6F_6$ | 2382.04 |
| 44 | Ru | | ? | | ? |
| 27 | Co | $^4F_5 - ^6F_6, ^6G_6$ | ? | $(^5F_5 - ^5G_6)$ | 2388.93 |
| 45 | Rh | | ? | | ? |
| 28 | Ni | $(^3F_4 - ^5\bar{F}_5, ^5G_5)$ | ? | $(^4F_5 - ^4G_6)$ | 2416 16 |
| 46 | Pd | | ? | | ? |

TABLE 620.—Electron Impacts in Gases

(Langmuir, Jones, Rev. Mod. Phys., 2, 233, 1930.)

Probabilities that an electron, while going through gas at 1 mm pressure, 20°C, will collide inelastically, P_k , elastically, P_e , so as to produce 1st excited state, P_r , or so as to ionize P_i :

| Gas | Volts | P_k | P_e | P_r | P_i | Gas | Volts | P_k | P_e | P_r | P_i |
|-----|-------|-------|-------|-------|-------|-----|-------|-------|-------|-------|-------|
| He | 50 | 7.7 | 2.1 | 2.8 | 0.9 | Hg | 30 | 48.0 | 33.3 | 17.3 | 13.6 |
| | 100 | 6.0 | 1.5 | .7 | 1.6 | | 50 | 49.1 | 29.5 | 14.7 | 10.9 |
| Ne | 75 | 9.3 | 1.1 | 1.5 | 1.8 | | 100 | 50.3 | 25.9 | 16.7 | 21.7 |
| | 100 | 9.2 | .9 | 1.3 | 2.4 | | 250 | 32.0 | 21.3 | 6.7 | 20.4 |
| A | 30 | 19.1 | 24.1 | 5.9 | 4.7 | H | 100 | 9.2 | 5.3 | 3.5 | 3.9 |
| | 50 | 18.4 | 20.8 | 1.9 | 9.5 | | 250 | 7.2 | 6.3 | 2.1 | 3.6 |
| | 100 | 18.7 | 14.5 | 1.7 | 11.4 | N | 75 | 20.2 | 14.9 | 5.3 | 9.3 |
| | 150 | 18.4 | 12.8 | 2.7 | 11.4 | | 100 | 16.2 | 10.4 | 4.8 | 10.3 |

TABLE 621.—Average Life for Various Quantum States of Excited Atoms

Theoretical values of ionized helium (Maxwell, Sugiura, Stack.)

| Levels | Average Life $T(n, l)$ (sec.) | Mean av. life $T(n)$, (sec.) |
|-----------------------|--|----------------------------------|
| 2n, 2l | 1.02×10^{-10} | 1.36×10^{-10} |
| 3n, 3l, 32 | $1.01 \times 10^{-8}, 3.38 \times 10^{-10}, 9.93 \times 10^{-10}$ | 6.4 |
| 4n, 4l, 42, 43 | 1.46 " 7.89 " 2.32 $\times 10^{-9}, 4.66 \times 10^{-9}$ | 2.13 $\times 10^{-9}$ |
| 5n, 5l, 52, 53, 54 | 2.2 " 1.49 $\times 10^{-9}, 4.33 \times 10^{-9}, 8.73 \times 10^{-9}, 1.45 \times 10^{-8}$ | 5.4 $\times 10^{-9}$ |
| 6n, 6l, 62, 63, —, 65 | 3.3 " 2.44 " 7.20 " 1.47 $\times 10^{-8}, —, 3.91$ | 1.18 $\times 10^{-8}$ |
| 7n, 7l, 72, 73, —, 76 | 5.0 " 3.65 " 1.18 $\times 10^{-9}, 2.4 \times 10^{-8}, —, 8.80$ | 2.24 $\times 10^{-8}$ |

The values for H are 16 \times those for He (Sugiura, 1927, 1929). It is to be noted that the average life is longer for progressively higher quantum states.

Maxwell 1931 obtains $1.1 \pm 0.2 \times 10^{-8}$ sec. for av. life 6th quantum state (cf. 1.18×10^{-8}) given above. Maxwell's qualitative observation on first four lines of 4686 He + series, $4 > 3, 5 > 3, 6 > 3, 7 > 3$, show definitely the longer life for higher quantum states.

Poole (Phys. Rev., 33, 22, 1929) metastable Hg atom (Z^2P_0), max. time 4.2×10^4 sec. (6.8 mm).

See Ann. Phys., 83, 294, 1927, for early summary, including following:

O spark, 467, 459 $\mu\mu$, 1.53×10^{-8} sec. Ca spark 3933 Å, 3968 Å, 0.65×10^{-8} sec.

O arc, 6158, 4368 Å, 14.9 " Ca arc 4226 Å, 3.4 "

Koenig, Ellett. (Phys. Rev., 39, 576, 1932) give for 2^3P_1 state Cd, 2.5×10^{-6} sec.

MOLECULAR CONSTANTS OF DIATOMIC MOLECULES

(From manuscript by E. D. McAlister, 1932.)

Energy levels for molecules can be evaluated from their spectra, just as for atoms. *Widely spaced levels* in molecules correspond roughly to those known for atoms, are similarly designated (see "Notation for Spectra of Diatomic Molecules," R. S. Mulliken, Phys. Rev., 36, 611, 1930) and are said to be related to the *electronic* configuration. A *system* of bands arise from transitions from one (often multiple) electronic configuration to another.

Diatomic molecules have two other sets of levels in addition to the electronic. One is due to the energy of mutual *vibration* of the two nuclei and the other to the energy of rotation of the molecule as a whole. A distinct set of vibrational levels is associated with each electronic state. The energy difference corresponding to each level of such a set from that of the associated electronic state is obtained (approximately) by giving successive positive integral values to n in the expression $n(\omega_0 - \omega_0 \times n + \dots)$; x a positive constant. The frequency of vibration (ω) is obtained by differentiating this with respect to n ; $\omega = \omega_0(1 - 2xn + \dots)$. At the lowest level where the amplitude and energy of vibration are vanishingly small, $n=0$ and $\omega = \omega_0$. A transition from one vibrational level to another gives rise to a *single band*.

A distinct set of rotational levels is associated with each vibrational level. The presence of large numbers of these closely spaced rotational levels gives rise to the many individual lines of the band. The rotational energy, relative to the associated vibrational level is given (approximately) by $Bm^2(1 - m^2u^2 + \dots)$; where $u = \frac{2B_0}{\omega_0}$ and m is a parameter which is zero for zero rotation. Usually $BI = h/8\pi^2c = 27.70 \times 10^{-40}$ g. cm, where I = moment of inertia of the molecule about an axis through its center of mass and perpendicular to the line joining its nuclei. For multiple levels this relation is not accurately true. I varies with the vibrational energy, and becomes I_0 when it is *zero*; the corresponding nuclear separation is $\gamma_0 = \sqrt{I_0/\mu}$ where $\mu = \frac{m_1m_2m_3}{(m_1 + m_2)}$. m_0 = mass of an atom of unit atomic weight = 1.650×10^{-24} g. m_1, m_2 are the atomic weights of the two atoms composing the molecule.

The heat of dissociation is $D^v = \int_0^{n_0} \omega dn$, where n_0 is the value of n for $\omega=0$. If the bands can be experimentally followed to $\omega=0$, D^v can be determined from spectroscopic data. Usually this cannot be done but Birge and Sponer (Phys. Rev., 28, 259, 1926) have found that, for the normal state of certain types of molecules, fairly trustworthy values of D^v can be obtained by assuming $\omega = \omega_0(1 - 2 \times n)$ throughout the range $n=0$ to $n=n_0$; then $D = \omega_0^2/4\omega_0x$. In the accompanying table D is D^v plus the electronic energy for the particular state in question. Each horizontal line in the table is for one electronic state. The second column labelled energy (volts) is the electronic energy above the normal level which is assumed to have zero electronic energy. The heat of dissociation is tabulated in the same units which is the number of volts potential change an electron must undergo in order to acquire the corresponding energy. One electron volt per molecule = 2.306×10^4 g - cal.₁₅ per g-mole = 8100 cm⁻¹ per molecule. The data in the table are taken from compilations by Birge, Nat. Res. Council Bull. 57, "Molecular Spectra in Gases" and Mulliken, Phys. Rev., 32, 206, 1928, and *ibid.*, 33, 738, 1929, and are calculated with the "old mechanics" formulae.

MOLECULAR CONSTANTS OF DIATOMIC MOLECULES

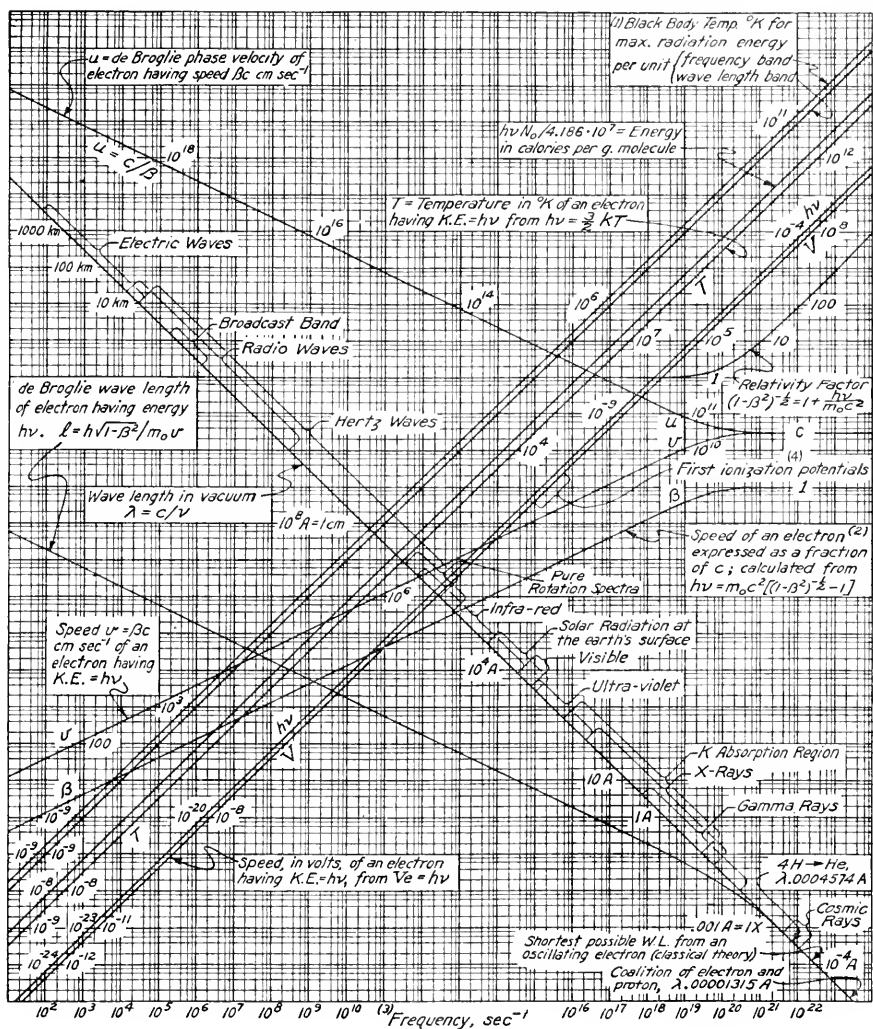
| Molecule | Energy (volts) | γ_0 (cm $\times 10^8$) | I_0 (g cm ² $\times 10^{40}$) | ω_0 (cm ⁻¹) | $\omega_0 V$ (cm ⁻¹) | D^v (volts) | D (volts) | State |
|-------------------|-------------------|-----------------------------------|--|-----------------------------------|-------------------------------------|------------------|----------------|-------------|
| Ag H | 0 | 1.630 | 4.38 | (1690) | | | | 1Σ |
| | 3.69 | 1.665 | 4.57 | (1490) | | | | 1Σ |
| Al H | 0 | 1.658 | 4.41 | (1625) | | | | 1Σ |
| | 2.90 | 1.690 | 4.58 | (1082) | | | | 1π |
| | 5.51 | 1.65 | | (1326) | | | | 1Σ |
| Au H | 0 | 1.54 | 3.93 | 2249.4 | 34.0 | 4.59 | 4.59 | 1Σ |
| | 3.37 | 1.69 | 4.74 | 1630 | 79 | 1.04 | 4.41 | 1Σ |
| | 4.72 | 1.71 | | (1548) | | | | 1Σ |
| Be F | 0 | | | 1253 | 10.2 | 4.8 | 4.8 | 2Σ |
| | 4.10 | | | 1156 | 8.4 | 4.9 | 9 | 2π |
| Be H | 0 | 1.35 | | 2026 | | | | 2Σ |
| | 2.48 | 1.34 | | 2053 | | | | 2π |
| Be O | 0 | 1.33 | | 1465 | 12.7 | 6.4 | 6.4 | 1Σ |
| | 2.62 | 1.36 | | 1354 | 8.9 | 5.2 | 7.8 | 1Σ |
| B ¹⁰ O | 0 | 1.21 | 15.68 | 1874 | 11.7 | 9.3 | 9.3 | 2Σ |
| | 2.91 | 1.36 | 20.03 | 1249 | 10.6 | 4.6 | 7.5 | $2\Sigma_i$ |
| | 5.30 | 1.31 | 18.53 | 1270 | 10.1 | 5.0 | 10.3 | 2Σ |
| C ₂ | 0 | 1.31 | 17.03 | 1630 | 11.7 | 7.0 | 7.0 | 3π |
| | 2.39 | 1.27 | 15.84 | 1773 | 19.4 | 6.4 | 8.8 | 3π |
| Cd H | 0 | 1.776 | 5.201 | (1374) | | | | 2Σ |
| | 2.75, 2.88 | 1.674 | 4.65, 4.59 | | | | | $2\pi_n$ |
| C H | 0 | 1.13 | 1.95 | (2806) | | | | $2\pi_n$ |
| | 2.86 | 1.11 | 1.90 | (2851) | | | | $2\Sigma_i$ |
| | 3.18 | 1.20 | 2.21 | (< 2806) | | | | 2Σ |
| C N | 0 | 1.17 | 14.65 | 2056 | 13.8 | 9.5 | 9.5 | 2Σ |
| | 1.78 | 1.23 | | 1729 | 13.5 | 6.8 | 8.6 | $2\pi_i$ |
| | 3.18 | 1.15 | 14.14 | 2144 | 21.3 | 6.7 | 9.9 | 2Σ |
| C O | 0 | 1.15 | 14.9 | 2155 | 12.7 | 11.2 | 11.2 | 1Σ |
| | 5.98 | | | 1725 | 14.5 | 6.4 | 12.4 | 3π |
| | 7.14 | | | 1173 | 9 | 4.6 | 11.9 | 3Σ |
| | 7.99 | 1.24 | 17.31 | 1499 | 17.2 | 4.0 | 12.0 | 1π |
| | 10.35 | | | (2214) | | | | 3Σ |
| | 10.73 | 1.12 | 14.26 | 2132 | 50 | 2.8 | 13.5 | 1Σ |
| | 11.35 | | | (2133) | | | | 1Σ |
| | 11.46 | | | (2134) | | | | 1Σ |
| | 12.30 | | | 1914 | 19.8 | .6 | 12.9 | 1π |
| CO + | 14.2 | 1.11 | 14.05 | 2197 | 15.2 | 9.8 | 9.8 | 2Σ |
| | 16.7 | 1.25 | 17.7 | 1550 | 14.1 | 7.1 | 9.6 | $2\pi_i$ |
| | 19.8 | 1.17 | 15.4 | 1698 | 24.3 | 3.7 | 9.3 | 2Σ |

MOLECULAR CONSTANTS OF DIATOMIC MOLECULES

| Molecule | Energy (volts) | γ_0 ($\text{cm} \times 10^3$) | I_0 ($\text{g cm}^2 \times 10^{40}$) | ω_0 (cm^{-1}) | $\omega_0 X$ (cm^{-1}) | Dv (volts) | D (volts) | State |
|------------------|-------------------|---|---|------------------------------------|--------------------------------------|-----------------|----------------|--------------|
| Cu H | 0 | 1.471 | 3.544 | 1903.7 | 37.36 | 3.02 | 3.02 | 1Σ |
| | 2.88 | 1.582 | 4.097 | 1655.7 | 44.63 | 1.89 | 4.77 | 1Σ |
| | 5.51 | 1.50 | | | | | | 1π |
| H ₂ | 0 | .76 | .480 | 4262 | 113.5 | 4.42 | 4.42 | 1Σ |
| | 11.12 | 1.55 | 1.99 | 1325 | 15.9 | | | 1Σ |
| | 11.70 | .97 | .78 | 2390 | 73 | | | 3π |
| He ₂ | 0 | | | | | | | 1Σ |
| | 20.3 | 1.052 | 3.650 | (1731.8) | | | | 1Σ |
| | 20.6 | 1.047 | 3.62 | (1790.1) | | | | 1Σ |
| | 20.9 | 1.071 | 3.784 | | | | | 1π |
| Hg H | 0 | 1.763 | 5.143 | 1308 | 104 | .369 | .369 | 2Σ |
| | 3.08 | 1.593 | { 4.22 } | 2025.7 | (1938.7) | 2.90 | 6.46 | { $2\pi_n$ } |
| | 3.56 | | { 4.18 } | | 43.8 | | | |
| | 4.18 | | | | (1940) | | | |
| Mg H | 0 | 1.74 | 4.86 | 1462.2 | 31.25 | 2.12 | 2.12 | 2Σ |
| | 2.38 | 1.70 | 4.62 | 1568.7 | 34.75 | 2.18 | 4.56 | $2\pi_n$ |
| | 5.09 | 1.70 | | (1622) | | | | 2π |
| | | | | | | | | |
| N ₂ | 0 | | | 2345 | 14.4 | 11.7 | 11.7 | 1Σ |
| | 8.18 | | | 1446 | 13.9 | 3.7 | 11.9 | 3Σ |
| | 8.50 | | | 1679 | 13.8 | 5.7 | 14.2 | 1π |
| | 9.35 | 1.21 | 16.98 | 1718 | 14.4 | 5.3 | 14.6 | $3\pi_n$ |
| | 13.00 | 1.15 | 15.24 | 2019 | 26.0 | 1.6 | 14.6 | $3\pi_n$ |
| N ₂ + | 16.9 | 1.12 | 14.41 | 2187 | 16.3 | 9.1 | 9.1 | 2Σ |
| | 20.1 | 1.08 | 13.35 | 2392 | 22.8 | 8 | 11 | 2Σ |
| NH | 0 | 1.08 | 1.81 | | | | | 3Σ |
| | 3.67 | 1.08+ | | | | | | 3π |
| NO | 0 | 1.15 | 16.29 | 1892 | 14.4 | 7.9 | 7.9 | $2\pi_n$ |
| | 5.45 | 1.07 | 14.05 | 2352 | 13 | 14 | 19 | 2Σ |
| | 5.60 | 1.42 | 24.80 | 1030 | 7.5 | 4.4 | 10 | $2\pi_n$ |
| | 6.45 | | | (2347) | | | | 2Σ |
| | 6.58 | | | 2324 | 27 | 6.2 | 13 | |
| NO+ | 9.4 | | | | | | | 1Σ |
| | 21 | | | | | | | 3Σ |
| | 22 | | | | | | | $\pi(?)$ |
| O ₂ | 0 | 1.21 | 19.2 | 1565 | 11.4 | 5.1 | 5.1 | 3Σ |
| | 1.62 | 1.23 | 19.8 | 1415 | 11.9 | | | 1Σ |
| | 6.09 | 1.61 | 34.22 | 708 | 12.4 | | | 3Σ |
| O ₂ + | 13.5 | | | 1926 | 16.5 | 6.9 | 6.9 | $2\pi_n$ |
| | 18.7 | | | 855 | 13.7 | | | $2\pi_n$ |
| | 18.7 | | | 1026 | 11.1 | | | $\pi(?)$ |
| | 20.8 | | | 1180 | 17.8 | | | $\Sigma(?)$ |
| O H | 0 | .979 | 1.500 | (3568.4) | | 5.4 | 5.4 | $2\pi_i$ |
| | 4.00 | 1.022 | 1.634 | 3084.7 | 97.8 | 3.0 | 7.0 | 2Σ |
| Zn H | 0 | 1.608 | 4.234 | (1552) | | | | 2Σ |
| | 2.87 | 1.522 | 3.78 | | | | | $2\pi_n$ |

TABLE 624

VARIOUS ATOMIC AND SPECTRUM FUNCTIONS



1. In black body unpolarized radiation the energy transmitted per sec per sq cm per unit solid angle per unit frequency band is, by Planck's radiation formula, $K_\nu = (h\nu^3/c^2) \cdot (e^{h\nu/kT} - 1)^{-1}$; per unit wave-length band it is $E_\lambda = (hc^2/\lambda^5) \cdot (e^{hc/\lambda kT} - 1)^{-1}$. The values $h\nu/kT = 2.82144 = a$ and $hc/\lambda kT = 4.96511 = b$ make K_ν and E_λ take their maximum values, whence the temperature of the radiation that has its maximum K_ν or E_λ at a particular frequency or wave length can easily be computed.

2. Electron speed $\div 1846^{1/2} =$ speed of a proton having the same energy, with negligible error at low energies. This holds to within 0.1% up to $v = 3 \times 10^{10}$, but becomes 1.8% low at $v = 3 \times 10^{10}$, 12% low at $v = 3 \times 10^{10}$, and should not be used at all for higher frequencies. For convenience, $.6368 \div 1846^{1/2} = .01622$; $20.89 \div 1846^{1/2} = .4863$; $66.07 \div 1846^{1/2} = 1.538$; $.2203 \div 1846^{1/2} = .005129$

3. Frequency is used as the fundamental quantity with Birge's values (Physical Review Supplement 1, 1, July 1929) of the physical constants, and the final calculation rounded off to four figures.

to four figures.

Speed of light, $c = 2.99796 \times 10^{10}$ cm sec⁻¹

Electronic charge, $e = 4.770 \times 10^{-10}$ abs esu

Electronic mass (by deflection), $m_0 = 9.94 \times 10^{-28}$ g

Planck's constant, $h = 6.547 \times 10^{-27}$ erg sec

Molecular gas constant, $k = 1.3708_9 \times 10^{-16}$ erg deg⁻¹

299.796 abs volts = 1 abs esu of potential

1 l calorie, $J_{15} = 4.1852$ abs joules

Avogadro's number, $N_0 = 6.064 \times 10^{23}$ mole⁻¹

Atomic weight of helium = 4.0022

Atomic weight of hydrogen = 1.00777

4. Corresponding to "first ionization potentials," Cs 3.88 V, He 24.48 V.

Compiled by W. Edwards Deming
Drawn by Mrs. C. Sherry
Revised, August 1929

U. S. Department of Agriculture
Bureau of Chemistry & Soils
Washington, D. C.

TABLE 625
RADIOACTIVITY

INTRODUCTION. THE URANIUM FAMILY

(References: Kovarik, McKeehan, Nat. Res. Council, Bull. 51 (reprint 1929); Andrade, Structure of the atom, 3rd ed., 1926; Rutherford, Radiations from radioactive substances, 1930; Kohlrausch, Radioaktivität, 1929; Radioactive constants of 1930, Report International Radium-Standards Commission, Rev. Mod. Phys., 3, 427, 1931.)

Certain elements (about 40) of high atomic weight (also slightly K and Rb) are unstable in that they spontaneously change to elements of lower atomic weight with the production of heat and the emission of α , β , or γ rays. Radioactivity is an additive property of the atom, dependent only on the particular element and not on the chemical compound into which this element enters nor on the physical conditions controlling ordinary reactions—temperature, whether solid, gaseous or liquid, etc. The lives of these elements vary from 10^{10} yrs. to 10^{-11} sec. (See Table 625.)

TABLE 625.—The Uranium Family, T , λ , τ

At. Wt. = atomic weight; P. No. = proton number; At. No. = atomic number; yr = years; d = days; h = hours; m = minutes; s = seconds; T = half-period; τ = average life; λ = decay constant.

| | | T | λ | τ | Rays and end product |
|--|--|--|--|---|---|
| Uranium I | UI | $4.4 \cdot 10^9 \text{ yr}$ $1.4 \cdot 10^{17} \text{ s}$ | $1.6 \cdot 10^{-10} \text{ yr}^{-1}$ $5.0 \cdot 10^{-18} \text{ s}^{-1}$ | $6.3 \cdot 10^9 \text{ yr}$ $2.0 \cdot 10^{17} \text{ s}$ | α , UX ₁ |
| | At. Wt. 238.14 At. No. 92 P. No. 238 | | | | |
| Uranium X ₁ | UX ₁ | 24.5d $2.12 \cdot 10^6 \text{ s}$ 23.8d $2.06 \cdot 10^6 \text{ s}$ 1.14m 68.4s | $2.83 \cdot 10^{-2} \text{ d}^{-1}$ $3.28 \cdot 10^{-7} \text{ s}^{-1}$ $2.90 \cdot 10^{-2} \text{ d}^{-1}$ $3.37 \cdot 10^{-7} \text{ s}^{-1}$ 0.61 m^{-1} $1.01 \cdot 10^{-2} \text{ s}^{-1}$ | 35.4d $3.05 \cdot 10^6 \text{ s}$ 34.4d* $2.97 \cdot 10^6 \text{ s}^*$ 1.64m 98.7s | β , UX ₂ .9965 UZ .0035 |
| | At. No. 90 P. No. 234 | | | | |
| Uranium X ₂ (Brevium) ca 99.65% | UX ₂ | | | | β , UII |
| | At. Wt. — At. No. 91 P. No. 234 | | | | |
| Uranium Z ca 0.35% | UZ | 6.7h $2.4 \cdot 10^4 \text{ s}$ | 0.103 h^{-1} $2.87 \cdot 10^{-5} \text{ s}^{-1}$ | 9.7h $3.5 \cdot 10^4 \text{ s}$ | β , UII |
| | At. No. 91 P. No. 234 | | | | |
| Uranium II | UII | $3 \cdot 10^5 \text{ yr}$ $9.4 \cdot 10^{12} \text{ s}$ | $2.3 \cdot 10^{-6} \text{ yr}^{-1}$ $7.4 \cdot 10^{-14} \text{ s}^{-1}$ | $4.3 \cdot 10^5 \text{ yr}$ $1.4 \cdot 10^{13} \text{ s}$ | α , Io .970 UY .030 |
| | At. No. 92 P. No. 234 | | | | |
| Uranium Y ca 3% | UY | 24.6h 1.03d $8.88 \cdot 10^4 \text{ s}$ | $2.82 \cdot 10^{-2} \text{ h}^{-1}$ 0.675 d^{-1} $7.81 \cdot 10^{-6} \text{ s}^{-1}$ | 35.5h 1.48d $1.28 \cdot 10^5 \text{ s}$ | β , Ac. |
| | At. No. 90 P. No. 231 or 230 | | | | |

* Earlier values still in use.

Notes on Decay Constants: For U₁ the calculation is based on Z = no. of α particles from 1 g Ra per sec. = 3.70×10^{10} ; $\text{Ra/U} = 3.40 \times 10^{-7}$; Avogadro's No. = 6.064×10^{23} ; no account is taken of the branching Ac series. The values given are for T and τ , upper, for λ lower limits.

For UX₁, the lowest value $T = 23.8$ is mentioned as well as the one preferred by the Commission.

UII. The adoption of 3×10^5 yr. is recommended.

ThC'. Mme. Curie has recently calculated λ = about 10^9 sec^{-1} . (Geiger-Nuttall Law). In view of the uncertainty of the values, $T < 10^{-6}$ sec. has been proposed.

AcC". 150 curves give $T = 4.71$ min., 9, $T = 4.76$ min. Both values are given.

RADIOACTIVITY

IONIUM—RADIUM FAMILY T, λ , τ

(Taken from 1930 Report International Radium Standards Commission, Rev. Mod. Phys., 3, 427, 1931.)

| | | T | λ | τ | Rays and end product |
|----------------------------|-----------------|--------------------------------|--------------------------------------|--------------------------------|---|
| Ionium | Io | $8.3 \cdot 10^4 \text{ yr}$ | $8.3 \cdot 10^{-6} \text{ yr}^{-1}$ | $1.2 \cdot 10^5 \text{ yr}$ | α , Ra |
| | At. No. 90 | $2.6 \cdot 10^{12} \text{ s}$ | $2.6 \cdot 10^{-13} \text{ s}^{-1}$ | $3.8 \cdot 10^{12} \text{ s}$ | |
| | P. No. 230 | | | | |
| Radium | Ra | 1590 yr | $4.36 \cdot 10^{-4} \text{ yr}^{-1}$ | 2295 yr | α , Rn |
| | At. No. 88 | $5.02 \cdot 10^{10} \text{ s}$ | $1.38 \cdot 10^{-11} \text{ s}^{-1}$ | $7.24 \cdot 10^{10} \text{ s}$ | |
| | P. No. 226 | | | | |
| Radon | Rn | 3.825d | 0.1812 d^{-1} | 5.518d* | α , RaA |
| | At. No. 86 | $3.305 \cdot 10^5 \text{ s}$ | $2.097 \cdot 10^{-6} \text{ s}^{-1}$ | $4.768 \cdot 10^5 \text{ s}^*$ | |
| | P. No. 222 | 3.823d | 0.1813 d^{-1} | 5.515d* | |
| Radium A | RaA | $3.303 \cdot 10^5 \text{ s}$ | $2.098 \cdot 10^6 \text{ s}^{-1}$ | $4.765 \cdot 10^5 \text{ s}^*$ | α , RaB |
| | At. No. 84 | 3.05m | 0.227 m^{-1} | 4.40m | |
| | P. No. 218 | 183s | $3.78 \cdot 10^{-3} \text{ s}^{-1}$ | 264s | |
| Radium B | RaB | 26.8m | $2.59 \cdot 10^{-2} \text{ m}^{-1}$ | 38.7m | β , RaC |
| | At. No. 82 | $1.61 \cdot 10^3 \text{ s}$ | $4.31 \cdot 10^{-4} \text{ s}^{-1}$ | $2.32 \cdot 10^3 \text{ s}$ | |
| | P. No. 214 | | | | |
| Radium C | RaC | 19.7m | $3.51 \cdot 10^{-2} \text{ m}^{-1}$ | 28.5m | β , α , .9996 RaC' .0004 RaC'' |
| | At. No. 83 | $1.18 \cdot 10^3 \text{ s}$ | $5.86 \cdot 10^{-4} \text{ s}^{-1}$ | $1.17 \cdot 10^3 \text{ s}$ | |
| | P. No. 214 | | | | |
| Radium C' | RaC' | ca 10^{-6} s | 10^6 s^{-1} | 10^{-6} s | α , RaD |
| | At. No. 84 | | | | |
| | P. No. 214 | | | | |
| Radium C'' | RaC'' | 1.32m | 0.525 m^{-1} | 1.9m | β , RaD |
| | At. No. 81 | 79.2s | $8.7 \cdot 10^{-3} \text{ s}^{-1}$ | 115s | |
| | P. No. 210 | | | | |
| Radium D | RaD | 22yr | 0.0315 yr^{-1} | 31.7yr | β , RaE |
| | At. No. 82 | $6.94 \cdot 10^8 \text{ s}$ | $1.00 \cdot 10^{-9} \text{ s}^{-1}$ | $1.00 \cdot 10^9 \text{ s}$ | |
| | P. No. 210 | | | | |
| Radium E | RaE | 4.9d | 0.141 d^{-1} | 7.07d* | β , RaF |
| | At. No. 83 | $4.26 \cdot 10^5 \text{ s}$ | $1.63 \cdot 10^{-6} \text{ s}^{-1}$ | $6.13 \cdot 10^5 \text{ s}^*$ | |
| | P. No. 210 | 5.0d | 0.139 d^{-1} | 7.2d* | |
| Radium F | | $4.32 \cdot 10^5 \text{ s}$ | $1.61 \cdot 10^{-6} \text{ s}^{-1}$ | $6.22 \cdot 10^5 \text{ s}^*$ | α , RaG |
| | RaF(Po) | 140d | $4.95 \cdot 10^{-3} \text{ d}^{-1}$ | 202d | |
| | At. No. 84 | $1.21 \cdot 10^7 \text{ s}$ | $5.73 \cdot 10^{-8} \text{ s}^{-1}$ | $1.75 \cdot 10^7 \text{ s}$ | |
| Polonium | P. No. 210 | | | | |
| Radium G (Uranium lead) | RaG | | | | |
| | At. Wt. 206.016 | | | | |
| | At. No. 82 | | | | |
| | P. No. 206 | | | | |

* Earlier values still in use.

TABLE 627
RADIOACTIVITY
ACTINIUM FAMILY

(Taken from 1930 Report International Radium Standards Commission, Rev. Mod. Phys., 3, 427, 1931.)

| | | <i>T</i> | λ | τ | Rays and end product |
|---|---|---|--|--|--|
| Actinium Uranium Uranium Y (see Uranium Family) | AcU | ca 10^8 to 10^9 yr | | | |
| Protactinium | Pa At. No. 91 P. No. 231 | $3.2 \cdot 10^4$ yr $1.01 \cdot 10^{12}$ s | $2.17 \cdot 10^{-5}$ yr $^{-1}$ $6.86 \cdot 10^{-13}$ s $^{-1}$ | $4.6 \cdot 10^4$ yr $1.46 \cdot 10^{12}$ s | α , Ac |
| Actinium | Ac At. No. 89 P. No. 227 | 13.5yr $4.23 \cdot 10^8$ s 20yr $6.3 \cdot 10^8$ s | $5.15 \cdot 10^{-2}$ yr $^{-1}$ $1.63 \cdot 10^{-9}$ s $^{-1}$ $3.4 \cdot 10^{-2}$ yr $^{-1}$ $1.1 \cdot 10^{-9}$ s $^{-1}$ | 19.4yr $6.12 \cdot 10^8$ s 29yr* $9.2 \cdot 10^8$ s* | β , RaAc |
| Radio-actinium | RaAc At. No. 90 P. No. 227 | 18.9d $1.63 \cdot 10^6$ s | $3.66 \cdot 10^{-2}$ d $^{-1}$ $4.24 \cdot 10^{-7}$ s $^{-1}$ | 27.3d $2.36 \cdot 10^6$ s | α , AcX |
| Actinium X | AcX At. No. 88 P. No. 223 | 11.2d $9.7 \cdot 10^5$ s 11.4d $9.85 \cdot 10^5$ s | $6.17 \cdot 10^{-2}$ d $^{-1}$ $7.14 \cdot 10^{-7}$ s $^{-1}$ $6.08 \cdot 10^{-2}$ d $^{-1}$ $7.06 \cdot 10^{-7}$ s $^{-1}$ | 16.2d* $1.40 \cdot 10^6$ s* 16.4d* $1.42 \cdot 10^6$ s* | α , An |
| Actinon | An At. No. 86 P. No. 219 | 3.92s | 0.177 s $^{-1}$ | 5.66s | α , AcA |
| Actinium A | AcA At. No. 84 P. No. 215 | $2 \cdot 10^{-3}$ s | 374 s $^{-1}$ | $2.88 \cdot 10^{-3}$ s | α , AcB |
| Actinium B | AcB At. No. 82 P. No. 211 | 36.0m $2.16 \cdot 10^3$ s | $1.93 \cdot 10^{-2}$ m $^{-1}$ $3.21 \cdot 10^{-4}$ s $^{-1}$ | 51.9m $3.12 \cdot 10^3$ s | β , AcC |
| Actinium C | AcC At. No. 83 P. No. 211 | 2.16m 130s | 0.321 m $^{-1}$ $5.35 \cdot 10^{-3}$ s $^{-1}$ | 3.12m 187s | α , β , .9984 AcC" .0016 AcC' |
| Actinium C' | AcC' At. No. 84 P. No. 211 | $ca 5 \cdot 10^{-3}$ s | $ca 140$ s $^{-1}$ | $ca 7 \cdot 10^{-3}$ s | α , AcD |
| 0.32% Actinium C'' | AcC'' At. No. 81 P. No. 207 | 4.76m 286s 4.71m 283s | 0.145 m $^{-1}$ $2.43 \cdot 10^{-3}$ s $^{-1}$ 0.146 m $^{-1}$ $2.44 \cdot 10^{-3}$ s $^{-1}$ | 6.87m* 412s* 6.83m* 410s | β , AcD |
| Actinium D Actinium Lead Pb207 | AcD At. Wt. 207.016 (?) At. No. 82 P. No. 207 | | | | |

* Earlier values still in use.

THORIUM FAMILY: POTASSIUM, RUBIDIUM

| | | T | λ | τ | Rays and end product |
|-----------------------|--|---|---|---|---|
| Thorium | Th At. Wt. 232.12 At. No. 90 P. No. 232 | $1.8 \cdot 10^{10}$ yr $5.6 \cdot 10^{17}$ s | $4.0 \cdot 10^{-11}$ yr $^{-1}$ $1.2 \cdot 10^{-18}$ s $^{-1}$ | $2.5 \cdot 10^{10}$ yr $8.0 \cdot 10^{17}$ s | α , MsTh ₁ |
| Mesothorium 1 | MsTh ₁ At. No. 88 P. No. 228 | 6.7yr $2.1 \cdot 10^8$ s | 0.103 yr $^{-1}$ $3.26 \cdot 10^{-9}$ s $^{-1}$ | 9.7yr $3.05 \cdot 10^8$ s | β , MsTh ₂ |
| Mesothorium 2 | MsTh ₂ At. No. 89 P. No. 228 | 6.13h $2.21 \cdot 10^4$ s | 0.113 h $^{-1}$ $3.14 \cdot 10^{-5}$ s $^{-1}$ | 8.84h $3.18 \cdot 10^4$ s | β , RdTh |
| Radiothorium | RdTh At. No. 90 P. No. 228 | 1.90yr $6.0 \cdot 10^7$ s | 0.365 yr $^{-1}$ $1.16 \cdot 10^{-8}$ s $^{-1}$ | 2.74yr $8.65 \cdot 10^7$ s | α , ThX |
| Thorium X | ThX At. No. 88 P. No. 224 | 3.64d $3.14 \cdot 10^5$ s | 0.190 d $^{-1}$ $2.20 \cdot 10^{-6}$ s $^{-1}$ | 5.25d $4.54 \cdot 10^5$ s | α , Tn |
| Thoron | Tn At. No. 86 P. No. 220 | 54.5s | $1.27 \cdot 10^{-2}$ s $^{-1}$ | 78.7s | α , ThA |
| Thorium A | ThA At. No. 84 P. No. 216 | 0.14s | 4.95 s $^{-1}$ | 0.20s | α , ThB |
| Thorium B | ThB At. No. 82 P. No. 212 | 10.6h $3.82 \cdot 10^4$ s | $6.54 \cdot 10^{-2}$ h $^{-1}$ $1.82 \cdot 10^{-5}$ s $^{-1}$ | 15.3h $5.51 \cdot 10^4$ s | β , ThC |
| Thorium C | ThC At. No. 83 P. No. 212 | 60.5m $3.63 \cdot 10^3$ s | $1.15 \cdot 10^{-2}$ m $^{-1}$ $1.91 \cdot 10^{-4}$ s $^{-1}$ | 87.3m $5.24 \cdot 10^3$ s | β , α , .65ThC' .35ThC" |
| Thorium C' | ThC' At. No. 84 P. No. 212 | 10^{-9} s(?) < 10^{-6} s | 10^9 s $^{-1}$ (?) > 10^6 s $^{-1}$ | 10^{-9} s(?) < 10^{-6} s | α , ThD |
| Thorium C" | ThC" At. No. 81 P. No. 208 | 3.1m 186s | $2.24 \cdot 10^{-1}$ m $^{-1}$ $3.73 \cdot 10^{-3}$ s $^{-1}$ | 4.47m 286.3s | β , ThD |
| Thorium D | ThD At. No. 82 P. No. 208 | | | | |
| Thorium lead Pb208 | At. Wt. 208.016 (?) At. No. 82 P. No. 208 | | | | |

Potassium (K19) and rubidium (Rb37) emit β rays; the β -ray activity of rubidium is 1/15 that of uranium; T is about 10^{11} years. Cesium (55Ce) has been found to have an activity less than 1/90 of potassium. Hoffman considers neither sodium nor cesium radioactive. Be, av. period 10^{11} years, (Langer, Raitt, 1933).

NOTE—The following data is from Holmes, Lawson, Nature, 117, 620, 1926:

| | U _r | Th | K | Rb |
|---|---------------------------|---------------------------|-----------------------|-----------------------|
| N , atoms per g..... | | | 15.5×10^{21} | 7.09×10^{21} |
| T , half-value period, years.. | | | 15×10^{11} | 1×10^{11} |
| λ , disintegration constant, years $^{-1}$ | | | 4.6×10^{-13} | 69×10^{-13} |
| No. atoms disintegrating per years, $n\lambda$ | | | 7.1×10^9 | 49×10^9 |
| Kinetic energy, E ergs per β ray..... | | | 7.30×10^{-7} | 2.04×10^{-7} |
| Energy per g, per year, $nE/(4.19 \times 10^7)$ cal..... | (7900×10^{-4}) | (2300×10^{-4}) | 1.24×10^{-4} | 2.38×10^{-4} |

RADIOACTIVITY UNITS

(Taken from 1930 Report International Radium Standards Commission, Rev. Mod. Phys., 3, 427, 1931.)

Radium content is expressed in g or mg of radium, regardless of its chemical combination. It is always desirable to know the total weight and nature of the compound.

Radon (radium emanation).—A curie: Quantity of Rn in equilibrium with 1 g Ra. One curie Rn has a vol. 0.66 mm³ at 0° C 760 mm. One curie (Rn without decay products) can with complete utilization of the α -particles keep by its ionization of air a saturation current of 2.75×10^6 e.s.u. (0.92 milliampere).

Sub-units: Millicurie, microcurie, milli-microcurie (10^{-9}).

Eman. = 10^{-10} curie per l (10^{-13} curie/cm³)—concentration unit used for Rn content of the atmosphere.

Mache Unit (M. E.): Concentration unit referred to the Rn content of 1 l, = quantity Rn/l which without decay products and with complete utilization of the α particles can maintain by its ionization of air a saturation current of 10^{-3} e.s.u. One M. E. corresponds to 3.64×10^{-10} curie/liter = 3.64 eman.

It is recommended that the curie be extended to include the equilibrium of any decay product of radium, specifying the element as 1 curie Rn. The unit quantity of any radioactive element may be expressed in terms of the mass equivalent to 1 g Ra with respect to the effect of the rays as to the number of atoms decaying per sec., e.g., 1 mg Ra equivalent is that amount of an element whose number of atoms decaying per sec. equals that of 1 mg Ra (3.7×10^7 atoms/sec.).

Polonium.—"1 curie Po" = amount equiv. to 1 g Ra emitting 3.7×10^{10} α particles per sec. = quantity in radioactive equilibrium with 1 g Ra = 2.24×10^{-4} g Po.

That quantity of Po whose α radiation directed to one side only is fully utilized to ionize air and which can support a current of 1 e.s.u. corresponds to 1.68×10^{-10} g Po or 0.75×10^{-6} curie Po. 1 curie Po would, in the utilization of its rays in all directions, support a saturation current in air of 2.66×10^{-6} e.s.u., 1 microcurie (one-sided radiation) = 1.33 e.s.u.

Mesothorium.—"1 mg MsTh" usually signifies that γ -ray equivalent of 1 mg Ra-RaC, compared after absorption by 5 mm of lead. (This definition is inexact and open to criticism.)

All determinations of content of Ra, Ru, Ms, Th, Po, etc., must be dated. (Condensed from Report of the International Radium Standards Commission, Rev. Mod. Phys., 1931.)

TABLE 633
RADIOACTIVITY

α Particles: Range, Velocity, Ionization

RaC' (84 RaII) taken as standard: $V_{std} = 1.922 \times 10^9$ cm/sec.

(Table taken from Report International Radium Standards Commission, 1930,
Rev. Mod. Phys., 1931.)

As an α particle passes through matter, energy is dissipated, principally in ionization; its velocity diminishes. Ultimately the α particle can not be detected. Rutherford was able to detect by their scintillations, α particles of velocity $0.15 V_s$ and Blackett in his study of cloud-tracks of RaC' α rays found tracks corresponding to a velocity greater than $0.04 V_s$. When the kinetic energy becomes equal to that of an electron fallen a p.d. of 13.5 volts, then an α particle should not produce even a single pair of ions.

When α particles encounter successive thin layers nearly the same number emerge as enter up to a certain thickness. Beyond, the number transmitted decreases rapidly with small increments in the thickness. If the ionization in a thin layer of gas at increasing distance is plotted against distance, the decrease from max. ionization is rapid, the ionization descending nearly to zero along a steeply sloping line, becoming asymptotic to the distance axis. Marsden-Perkins have defined the range as the abscissa of the point where the straight line portion of the curve, produced, intersects the distance axis.

For the discussion of ranges see especially Rosenblum, C. R., 190, 1124, 1930, and Rutherford, Chadwick, Ellis, "Radiations from Radioactive Substances," 1930, pages 82 et seq. and 86. For two decimal places the relation $v^2 = aR$ gives sufficient accuracy for normal ranges. The basic value for ion production of α particles is that for RaC'; $K = 2.2 \times 10^6$. For the velocity of α particles from ThC, Rutherford, Chadwick, Ellis chose 1.701, while Mmes. Curie and Joliet-Curie propose 1.698×10^9 cm/sec.

Ranges, Velocities and Ion Productions

In the Table for R , v , k (range, velocity, ion production) the directly observed values are denoted by +. The calculation of the other values for v and k was made by using the basic values denoted ++.

RANGES AT 0° C AND 760 MM HG IN AIR (R_0); AT 15° C (R_{15}). VELOCITY (v) AND ION PRODUCTION (k)

| | Ranges at 0° | Ranges at 15° | Velocity | Ion production |
|------|-------------------|----------------|-------------------------|-------------------|
| UI | 2.53 | 2.67 | $1.40 \cdot 10^9$ | $1.16 \cdot 10^6$ |
| | 2.59 | 2.73 | 1.41 | (1.18) |
| UII | 2.96 | 3.12 | 1.47 | 1.29+ |
| | 3.11 | 3.28 | 1.50 | (1.33) |
| Io | 3.03 | 3.19 | 1.48 | 1.31 |
| Ra | 3.21 | 3.39 | 1.51 | 1.36+ |
| Rn | 3.91 | 4.12 | 1.61 | 1.55 |
| RaA | 4.48 | 4.72 | 1.69 | 1.70 |
| RaC | 3.9 | 4.1 | 1.61 | 1.55 |
| RaC' | 6.600++ (6.58) | 6.96 (6.94) | 1.922++ | 2.20++ |
| Po | 3.67 (3.72) | 3.87 (3.92) | 1.593+ (1.58) (1.59) | 1.49 (1.50) |
| Pa | 3.48 | 3.67 | 1.55 | 1.44 |
| RdAc | 4.43 | 4.68 | 1.68 | 1.69 |
| | and 4.77 | 4.34 | 1.64 | 1.67 |
| AcX | 4.14 | 4.37 | 1.65 | 1.61 |
| An | 5.49 | 5.79 | 1.81 | 1.95 |
| AcA | 6.24 | 6.58 | 1.89 | 2.12 |
| AcC | 5.22 | 5.51 | 1.78 | 1.88 |
| | and 4.82 | 5.09 | 1.73 | 1.79 |
| AcC' | (6.2)? | (6.5)? | (1.9)? | ca 2 |
| Th | 2.5 | 2.6 | 1.39 | 1.15 |
| RdTh | 3.81 | 4.02 | 1.60 | 1.53 |
| ThX | 4.13 | 4.35 | 1.64 | 1.61 |
| Tn | 4.80 | 5.06 | 1.73 | 1.78 |
| ThA | 5.39 | 5.68 | 1.80 | 1.92 |
| ThC | 4.53 | 4.78 | (1.698) | 1.71 |
| | 4.47 | 4.72 | (1.703) 1.701+ | 1.70 |
| ThC' | 8.17 | 8.62 | 2.052+ | 2.54 |

RADIOACTIVITY. α PARTICLESTABLE 634.—Relative Ranges of α Particles of RaF in Gases

All values are at n. t. p.; the accepted value for the α particle in air is 3.721 cm and the following values are merely relative. (After van der Merwe.)

| Gas..... | Air | H ₂ | H ₂ O | CH ₄ | N ₂ | CO | O ₂ | N ₂ O ₃ | CO ₂ | SO ₂ | CH ₃ Br |
|----------------------------|------|----------------|------------------|-----------------|----------------|------|----------------|-------------------------------|-----------------|-----------------|--------------------|
| Range, cm..... | 3.58 | 16.28 | | 3.96 | 3.62 | 3.51 | 3.32 | 3.26 | 2.36 | 1.97 | 1.76 |
| Molec. stopping power..... | 1.00 | .22 | .77 | .91 | .99 | 1.02 | 1.08 | 1.11 | 1.52 | 1.82 | 2.04 |

TABLE 635.—Relative Ranges of α Particles of RaC' in Solid Elements

(After Rausch von Traubenberg.)

| Element... | Li | Mg | Al | Ca | Fe | Ni | Cu | Zn | Ag | Cd | Sn | Pt | Au | Tl | Pb |
|-----------------------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| cm $\times 10^{-3}$. | 12.9 | 5.8 | 4.1 | 7.9 | 1.9 | 1.8 | 1.8 | 2.3 | 1.9 | 2.4 | 2.9 | 1.3 | 1.4 | 2.3 | 2.4 |

TABLE 635 (a).—Long-Range α Particles. Relative Numbers

Scintillations at abnormally great distances from thorium active deposit were first observed by Rutherford-Wood. The range in air of the particles producing these was 11.3 cm and it was shown by Rutherford that their mass was that of helium atoms, i. e., that they were α particles. It now appears certain that some of the particles of long range must have been H nuclei from Hydrogen or its compounds or protons from artificial disintegration.

| | | | |
|---------------------------|-------------------|------------|--------------|
| RaC' (84 RaII) Range..... | 7.0 cm, 1 000 000 | 9.3 cm, 20 | 11.2 cm, 70 |
| ThC' (84 ThII)..... | 8.6 cm, 1 000 000 | 9.5 cm, 70 | 11.5 cm, 200 |

TABLE 636.—Atomic Stopping Powers, S , for α Particles of RaC', Z , Atomic Number

(After Rausch von Traubenberg.)

The ability of atoms and molecules to stop α particles or, more briefly, their stopping power, was first investigated by Bragg, and, more recently, by others. The atomic stopping power for elements may be given by the formula $S = R_{0\rho_0 A}/R\rho A_0$, where R_0 , ρ_0 , A_0 are the range, density and atomic weight for the standard and R , ρ , A , the corresponding quantities for the element considered. The stopping power therefore varies inversely as the range and the density but directly as the atomic weight.

| | Z | S | $SZ^{-2/3}$ | | Z | S | $SZ^{-2/3}$ | | Z | S | $SZ^{-2/3}$ |
|----|-----|-------|-------------|----|-----|------|-------------|----|-----|------|-------------|
| H | 1 | 0.200 | 0.20 | Si | 14 | 1.23 | 0.21 | Ag | 47 | 2.74 | 0.21 |
| He | 2 | .380 | .24 | Cl | 17 | 1.76 | .27 | Cd | 48 | 2.75 | .21 |
| Li | 3 | .519 | .25 | A | 18 | 1.80 | .26 | Sn | 50 | 2.86 | .21 |
| Be | 4 | .750 | .30 | Ca | 20 | 1.69 | .23 | I | 53 | 3.55 | .25 |
| C | 6 | .864 | .28 | Fe | 26 | 1.96 | .22 | Pt | 78 | 3.64 | .20 |
| N | 7 | .939 | .26 | Ni | 28 | 1.89 | .21 | Au | 79 | 3.73 | .20 |
| O | 8 | 1.00 | .25 | Cu | 29 | 2.00 | .21 | Tl | 81 | 3.76 | .20 |
| Mg | 12 | 1.23 | .24 | Zn | 30 | 2.05 | .21 | Pb | 82 | 3.86 | .21 |
| Al | 13 | 1.27 | .23 | Br | 35 | 2.51 | .23 | | | | |

TABLE 637.—Atomic Stopping Powers of Molecules for the α Particles of RaC' (84RaII) Relative to that of the Oxygen Atom

(After Rausch von Traubenberg, Philipp.)

| Molecule..... | CO | CO ₂ | CH ₃ Br | CH ₃ I | Cl ₂ | HCl | NH ₃ | H ₂ O (liquid) |
|---------------------|------|-----------------|--------------------|-------------------|-----------------|------|-----------------|---------------------------|
| Stopping power..... | 1.85 | 2.78 | 3.93 | 4.97 | 3.51 | 1.92 | 1.46 | 1.53 |

TABLE 638
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H PARTICLES

Marsden first observed the long-range particles due to the impact of α particles on matter, now known to be H particles, i.e., hydrogen nuclei or protons set in motion by α rays. Rutherford made a thorough study of this phenomenon, measured the ranges in H_2 of H particles due to α particles of various speeds, counted the relative number of α and H particles by the scintillation method; measured the magnetic and electrostatic deflection of the H particles and proved them to be hydrogen nuclei (protons) in motion. He was able to produce them by bombardment of substances rich in H_2 . When the α particles have a 7 cm air range, the H particles have a maximum air range of 29 cm.

H Particles from Atomic Nuclei Bombarded by α Particles from RaC'

(Taken from Kovarik, McKeehan, Nat. Res. Council Bull. 51, 1925.)

RANGES IN CM IN AIR AT 15° C IN DIRECTIONS INCLINED TO THE α RAYS

| At. No. | Nucleus | | Inclination | | | Ref., Remarks |
|---------|---------|------------|-------------|------------|------|------------------|
| | Symbol | At. Wt. | 0° | 90° | 180° | |
| 3 | Li | 6, 7 | | 10 | | 1, (2, doubtful) |
| 4 | Be | 9 | | 18 | | 1, (2, doubtful) |
| 5 | B | 10, 11 | 58 | | 38 | 3 |
| 6 | C | 12 | | 6 | | 1, (2, none) |
| 7 | N | 14 | 40 | | 18 | 3 |
| 9 | F | 19 | 65 | | 48 | 3 |
| 10 | Ne | 20, 22 | | 16 | | 2, very few |
| 11 | Na | 23 | 58 | | 36 | 3 |
| 12 | Mg | 24, 25, 26 | | 13 (18-30) | | 1, (2, very few) |
| 13 | Al | 27 | 90 | | 67 | 4 |
| 14 | Si | 28, 29, 30 | | 12 (18-30) | | 1, (2, very few) |
| 15 | P | 31 | 65 | | 49 | 3 |
| 16 | S | 32 | | 18-30 | | 2, very few |
| 17 | Cl | 35, 37, 39 | | 18-30 | | 2, very few |
| 18 | A | 36, 40 | | 18-30 | | 2, very few |
| 19 | K | 39, 41 | | 18-30 | | 2, very few |

¹ Kirsch-Pettersson, 1924. ² Rutherford-Chadwick, 1924. ³ Rutherford-Chadwick, 1922.

⁴ Rutherford-Chadwick, 1921.

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TABLE 639.—Relative Total Ionization by α Rays in Various Gases

(After Bragg, Taylor, Laby, Hess-Hornyak.)

| Gas | Mean relative total ionization | Gas | Mean relative total ionization | Gas | Mean relative total ionization |
|------------------|--------------------------------|----------------------------------|--------------------------------|----------------------------------|--------------------------------|
| Air | 100 | C ₂ H ₄ | 122 | CH ₄ | 117.3 |
| H ₂ | 99.5 | C ₂ H ₆ | 130 | CH ₄ O | 122 |
| N ₂ | 96.3 | C ₅ H ₁₂ | 134.8 | C ₂ H ₂ | 126.5 |
| O ₂ | 112 | C ₂ H ₆ O | 123 | CH ₃ I | 133 |
| CO | 101.5 | C ₄ H ₁₀ O | 132.3 | C ₂ H ₅ I | 128 |
| CO ₂ | 107 | C ₆ H ₆ | 129 | CHCl ₃ | 129 |
| NH ₃ | 90 | C ₂ H ₄ O | 105 | C ₂ H ₅ Cl | 129.5 |
| N ₂ O | 102 | HBr | 129 | CCl ₄ | 132 |
| CS ₂ | 137.5 | HI | 129 | CH ₃ Br | 132 |
| SO ₂ | 103 | HCl | 129 | | |

TABLE 640.—Delta Rays

Delta rays are electronic rays (β rays) produced by bombarding a substance with α particles, an ionization of a comparatively infrequent type. δ rays are of various velocities, some corresponding to a few volts; others have a velocity, 3×10^9 cm/sec. (2400 volts); the number of δ rays produced by bombarding metals is of the order of 8 to 10 per α particle.

The existence of swift δ rays in hydrogen gas has been proved by Bumstead (cloud-track method). From the wide column of droplets (α -ray track) there are short, narrow tracks nearly at right angles. Wilson obtained similar δ -ray tracks in air near the beginning of the α -ray tracks. These experiments show that some δ rays are capable of ionizing air along a path of considerable length. Bianu (ionization method) was able to show that δ rays ionize the gas and determined the velocity of the swiftest δ rays as 2.9×10^9 cm/sec. This velocity corresponds to 2400 volts. C. T. R. Wilson suggests that the δ rays may be due to expulsion of electrons from inner orbits of the bombarded atoms, which would agree with Kapitza's observation that the average energy lost by an α particle in producing a pair of ions is greater at high velocities than at low. Bianu shows that the number of low-speed δ rays produced is 40 times as great as the number of high-speed δ rays and that each α ray from RaF produces, on the average, 10 of the more numerous class. His work also shows the δ -ray emission to be independent of the nature of the metal bombarded, an observation in agreement with earlier investigations. The usual explanation offered for the production of δ rays is that an α particle entering a substance loses energy in ionization and that some of the electrons liberated possess speeds which enable them to escape.

TABLE 641.—Heating Effect of Radium and Its Emanation

(Rutherford and Robinson, Philosophical Magazine, 25, p. 312, 1913.)

| Heating effect in gram-calories per hour per gram radium. | | | | |
|---|----------------|---------------|----------------|--------|
| | α rays. | β rays. | γ rays. | Total. |
| Radium | 25.1 | — | — | 25.1 |
| Emanation | 28.6 | — | — | 28.6 |
| Radium A | 30.5 | — | — | 30.5 |
| Radium B + C | 39.4 | 4.7 | 6.4 | 50.5 |
| Totals | 123.6 | 4.7 | 6.4 | 134.7 |

Other determinations: Hess, Wien. Ber. 121, p. 1, 1912, Radium (alone) 25.2 cal. per hour per gram. Meyer and Hess, Wien. Ber. 121, p. 603, 1912, Radium in equilibrium, 132.3 gram. cal. per hour per gram. See also, Callendar, Phys. Soc. Proceed. 23, p. 1, 1910; Schweidler and Hess, Ion. 1, p. 161, 1909; Angström, Phys. ZS. 6, 685, 1905, etc.

RADIOACTIVITY

BETA RAYS

β rays are negatively charged particles (electrons) of the same nature as other electrons. It seems settled that the β particle is emitted first; the γ ray is emitted from the atom resulting after the disintegration of the nucleus caused by the emission of the β particle. In emitting β rays (random in direction) the original element is shifted one place to a next higher atomic number. Therefore one emitted electron is nuclear. Recent work proves some to be extra-nuclear. The velocity of the β particles is such that it is necessary in dealing with them to consider the Lorentz-Einstein equation, $m = m_0 (1 - \beta^2)^{-1/2}$; m_0 being the mass of a very slowly moving electron, β , the ratio of the velocity of the particle to that of light, V_0 .

The β and γ rays are best designated by their spectra. A complete compilation of these would be beyond the scope of these tables. See Kovarik and McKeehan, Nat. Res. Council, Bull. 51, 1929; or Rutherford, Chadwick, Ellis, radiations from radioactive substances.

The absorption coefficients (μ) are not precisely defined by the relation $I = I_0 e^{-\mu x}$, but they are of great value in practical work and for the rapid diagnosis of a radioactive substance. It appears desirable to include them and to give also the limits of velocity of the β -ray spectra.

| Substance | Type of decay | μ cm ⁻¹ Al | μ/ρ | D cm Al | Magnetic spectrum velocity limits in 10 ¹⁰ cm/sec. | Remarks * | Accompanying γ rays |
|-------------------|------------------|------------------------------|------------|------------|---|-----------|----------------------------|
| UX ₁ | β | 460 | 170 | 0.0015 | 1.44-1.74 | 3L, 1B | No nuclear |
| UX ₂ | β | 18 | 6.75 | .038 | 2.46-2.88 | 2B | Weak nuclear |
| UZ | β | 270 | 100 | .0026 | ? | ? | ? |
| | | to | to | to | | | |
| | | 36 | 13.5 | .019 | | | |
| Ra | α | 312 | 116 | .00222 | 1.56-2.04 | 3L | 1 nuclear line |
| RaB | β | 890 | 330 | .00078 | 1.08-2.47 | 31L | 9 nuclear lines |
| | | 80 | 29.5 | .0087 | | | |
| | | 13 | 4.84 | .053 | | | |
| RaC + C" | $\alpha + \beta$ | 50 | 18.5 | .0139 | 1.14-2.96 | 63L | 11 nuclear lines |
| | | 13 | 4.84 | .053 | | | |
| RaD | β | 5500 | 2037 | .000126 | .96-1.20 | 5L | 1 nuclear line |
| RaE | β | 45.5 | 16.9 | .0152 | 2.05-2.84 | 1B | Weak nuclear |
| UY | β | ca 300 | 110 | .0023 | ? | ? | ? |
| Pa | α | 126 | 47 | .0055 | 1.47-2.35 | 12L | 3 nuclear lines |
| Ac | β | ? | ? | ? | ? | | |
| RdAc | α | 175 | 65 | .004 | .66-2.3 | 49L | 10 lines |
| AcX | α | ? | ? | ? | .88-2.22 | 21L | 5 lines |
| AcB | β | ca 1000 | 370 | .0007 | 1.49 | 1L? | |
| AcC + C" | $\alpha + \beta$ | 29 | 10.7 | .024 | 2.25-2.56 | 8L | 3 nuclear lines |
| MsTh ₁ | β | ? | ? | ? | ? | ? | ? |
| MsTh ₂ | β | 40 | 14.8 | .018 | 1.09-2.90 | 31L | 8 lines |
| | | to | to | to | | | |
| | | 20 | 7.4 | .034 | | | |
| RdTh | α | 420 | 150 | .0017 | 1.19-1.53 | 6L | 2 lines |
| ThB | β | 153 | 57 | .0045 | 1.88-2.99 | 5L | 2 nuclear lines |
| ThC | $\alpha + \beta$ | 14.4 | 5.35 | .048 | | | |
| ThC" | β | 21.6 | 8.0 | .032 | .91-2.87 | 37L | 11 nuclear lines |
| K | β | 74 | 27.4 | .0094 | | | Weak |
| | | 49 | 18 | .014 | | | |
| Rb | β | 700 | 260 | .001 | | | |
| | | 190 | 70 | .0037 | | | |
| | | 900 | 333 | .0077 | | | |

* B = band, L = line. Bands originate in the primary (nuclear) rays; lines in the photo-electrons of the gamma rays.

μ/ρ is the mass absorption coefficient (ρ = density); D is the thickness in which the radiation is reduced to half value and = 0.69315 μ . All data refer to aluminum as the absorbing material.

RADIOACTIVITY

WORK OF EXTRACTION OF BETA PARTICLES

(After Bohr-Coster. Taken from Kovarik, McKeehan, Nat. Res. Council Bull. 51, 1929.)

Works of extraction V_i in volts $\times 10^5$; $V_i = E(T/R)$; they have been interpolated assuming linear-variation of $(T/R)^{\frac{1}{2}}$ with z in values given. In computing V_i , $\log_{10} E = 6.13129 - 10$; values not depending on interpolation italicized. M values, average of M_I and M_V ; to get M_I add, M_V , subtract correction term. Similarly with N, mean of N_I and N_{VII} ; O, mean of O_I and O_V .

| Atomic No. | Levels | | | | | | |
|---------------|---------------|---------------|---------------|---------------|-------------------------|------------------------|------------------------|
| | K | L_I | L_{II} | L_{III} | M | N | O |
| 92 | <i>1.1469</i> | <i>0.2169</i> | <i>0.2088</i> | <i>0.1711</i> | <i>0.0453</i> ± 100 | <i>0.0090</i> ± 54 | <i>0.0022</i> ± 14 |
| 91 | <i>1.1195</i> | <i>0.2106</i> | <i>0.2025</i> | <i>0.1666</i> | <i>0.0438</i> ± 96 | <i>0.0086</i> ± 52 | |
| 90 | <i>1.0922</i> | <i>0.2043</i> | <i>0.1964</i> | <i>0.1624</i> | <i>0.0424</i> ± 93 | <i>0.0082</i> ± 50 | |
| 89 | <i>1.0636</i> | <i>0.1981</i> | <i>0.1905</i> | <i>0.1582</i> | <i>0.0410</i> ± 90 | <i>0.0078</i> ± 48 | |
| 88 | <i>1.0353</i> | <i>0.1921</i> | <i>0.1846</i> | <i>0.1540</i> | <i>0.0396</i> ± 86 | <i>0.0074</i> ± 47 | |
| 87 | <i>1.0073</i> | <i>0.1862</i> | <i>0.1789</i> | <i>0.1499</i> | <i>0.0382</i> ± 83 | <i>0.0071</i> ± 45 | |
| 86 | <i>0.9797</i> | <i>0.1804</i> | <i>0.1733</i> | <i>0.1458</i> | <i>0.0368</i> ± 80 | <i>0.0067</i> ± 44 | |
| 85 | <i>0.9525</i> | <i>0.1746</i> | <i>0.1677</i> | <i>0.1418</i> | <i>0.0354</i> ± 77 | <i>0.0064</i> ± 42 | |
| 84 | <i>0.9257</i> | <i>0.1690</i> | <i>0.1622</i> | <i>0.1378</i> | <i>0.0342</i> ± 74 | <i>0.0060</i> ± 41 | |
| 83 | <i>0.8993</i> | <i>0.1634</i> | <i>0.1569</i> | <i>0.1339</i> | <i>0.0330</i> ± 70 | <i>0.0057</i> ± 39 | |
| 82 | <i>0.8744</i> | <i>0.1582</i> | <i>0.1518</i> | <i>0.1330</i> | <i>0.0316</i> ± 68 | <i>0.0052</i> ± 37 | <i>0.0008</i> ± 6 |
| 81 | <i>0.8509</i> | <i>0.1532</i> | <i>0.1467</i> | <i>0.1263</i> | <i>0.0305</i> ± 66 | <i>0.0049</i> ± 36 | <i>0.0008</i> ± 6 |
| 80 | <i>0.8275</i> | <i>0.1481</i> | <i>0.1419</i> | <i>0.1226</i> | <i>0.0293</i> ± 63 | <i>0.0046</i> ± 35 | |
| 79 | <i>0.8037</i> | <i>0.1434</i> | <i>0.1372</i> | <i>0.1189</i> | <i>0.0282</i> ± 60 | <i>0.0043</i> ± 34 | <i>0.0006</i> ± 5 |
| 78 | <i>0.7798</i> | <i>0.1389</i> | <i>0.1324</i> | <i>0.1153</i> | <i>0.0270</i> ± 58 | <i>0.0039</i> ± 32 | <i>0.0006</i> ± 5 |

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TABLE 644.—Effective Range of Beta Particles from RaE in a Few Elements

(After Gray-Douglas. Taken from Kovarik, McKeehan, Nat. Res. Council Bull. 51, 1929.)

| Element | C | Al | Cu | Sn | Pb |
|--|------|------|------|------|------|
| Effective range, g/cm ² | .474 | .460 | .432 | .395 | .354 |

TABLE 645.—Absorption of Characteristic Beta Particles in Air and CO₂

(After Kovarik.)

| Source | Air | | CO ₂ | |
|--|---------------------|----------------------------------|---------------------|----------------------------------|
| | μcm^{-1} | $(\mu/\rho)\text{cm}^2/\text{g}$ | μcm^{-1} | $(\mu/\rho)\text{cm}^2/\text{g}$ |
| UX ₁ | 0.12 | 100 | 0.23 | 126. |
| UX ₂ | 0.0065 | 5.43 | 0.0114 | 6.26 |
| UX ₁ } UX ₂ } | 0.0047 (Friman) | | | |
| RaD | 0.097 | 81 | 0.183 | 101. |
| | 0.64 | 535 | 1.69 | 930. |
| RaE | 0.0152 | 12.70 | 0.0207 | 16.31 |
| AcB | 0.31 | 260 | | |
| AcC } AcC'' } | 0.0091 | 7.60 | 0.0175 | 9.62 |
| ThB | 0.090 | 75 | 0.142 | 78. |
| ThC } ThC'' } | 0.0068 | 5.68 | 0.0129 | 7.08 |

RADIOACTIVITY

GAMMA RAYS

γ rays are extremely penetrating, nondeviable by electric and magnetic fields, produce ionization of gases, act on the photographic plate, excite phosphorescence. Like X rays, they are similar to light. γ rays are merely X rays produced in the radioactive atoms. The reflection of X rays and γ rays from crystals leaves no doubt that the wave theory of light is applicable. There are to be solved the same problems, as indicated by Bragg for the corpuscular theory of X rays. The same difficulties exist as in the case of visible radiation. Theoretical investigations on γ rays, based on the electromagnetic theory, lead to conclusions not very different from those of a corpuscular theory.

Emission of gamma rays.—The number of γ rays per sec. from RaB and RaC in equilibrium with 1 g of Ra, is 1.43×10^{10} and 1.49×10^{10} (Hess-Lawson). The mean value obtained by Kovarik for the number of γ rays per sec. from Ra(B + C) in equilibrium with 1 g of Ra was 7.28×10^{10} , which is nearly (within 2%) one γ ray per atom disintegrating. The random emission in time of penetrating γ rays from radium has been proved.

Energy and wave length of gamma rays.—The energies and wave lengths of γ rays have been obtained variously; much further research is required. The direct experimental determination of γ -ray wave lengths by reflection from a crystal (NaCl) was first made by Rutherford-Andrade for the γ rays of RaB and RaC. Both surface planes and internal planes were utilized. They showed that certain strong lines of the RaB γ -ray spectrum are identical with characteristic X rays (L series) of nonradioactive lead. The shortest wave length measured was that of a γ ray of RaC reflected at a grazing angle of $44'$ having a wave length of about 70 X.U. ($1 \text{ X.U.} = 10^{-13} \text{ cm} = 10^{-3} \text{ A.U.}$). The counting method was applied by Kovarik to high frequency γ rays of RaC reflected from calcite. The shortest measured wave length was about 28 X.U.

The determination of γ -ray wave lengths from mass absorption is made on the supposition that the relation between mass absorption and wave length found for X rays may be applied to γ rays. For X rays, outside regions of selective absorption, $\mu/\rho = k\lambda^n$ where λ is the wave length and n has a value 2.5 to 3. Rutherford found that as the mass absorption coefficient, μ/ρ , of γ rays approaches the order of magnitude of the mass scattering coefficient τ/ρ , it varies more slowly with λ , probably as the first power; from his X-ray data he concluded that the very penetrating γ rays have most probably a wave length between 20 and 7 X.U. Minna Lang applied her work on the absorption of hard X rays to the γ rays of all known radio-elements and found that many are probably characteristic X rays (K, L, and M series).

The energies of γ rays have been obtained also by measuring the energy of β rays "excited" by them in various elements. The velocity of the β particles emitted by the γ rays from the atom of any element depends upon the frequency of the γ rays and upon the work necessary to separate the emitted electron from the rest of the atom. The photoelectric equation $E = h\nu - W$, is applicable. (E is the energy of the "excited" β ray measured outside the atom, ν is the frequency of the exciting γ rays and W is the work of separation.) The energy E is the value of Hr in magnetic deflection experiments, the work W , the energy corresponding to the appropriate absorption edge in the X-ray spectrum of the atom in the electronic structure of which the β ray arises. The work of separation W will have different values for different energy levels in the same atom and different values for the same energy level in different atoms. The soft γ rays of RaB are the L-series X rays of Pb. Some of the γ rays of radio-elements belong to the K, L, M, or other series of X rays of the atoms concerned in the β -ray disintegration considered. Evidently, some of the γ rays are of extra-nuclear source. The most penetrating γ rays can not be so accounted for and must therefore be of nuclear origin.

Connection between gamma rays and beta rays (or alpha rays).—The more recent work has established: (1) some of the β rays are of photoelectric origin (extranuclear) "excited" by the γ rays; (2) some of the γ rays originate in rearrangements of electrons in the same part of the atom (ordinary X-ray types); (3) the change in nuclear charge requires some β rays in disintegration to be of nuclear origin; (4) some of the γ rays, all of the very penetrating rays, are of nuclear origin. The principal point in dispute is whether emission of nuclear β rays precedes or follows the emission of nuclear γ rays.

TABLE 647
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GAMMA RAYS

Nuclear analysis.—Analysis of nuclear γ rays show evidence for energy levels in the nucleus analogous to those in the extra-nuclear structure as found by X-ray analysis. When instability arises in the nucleus an electron occupying a level of higher energy falls to a level of less energy, the excess energy being emitted as a γ ray; since several changes of this kind are possible, γ rays of several different but definite frequencies may be emitted from this nucleus; further, different groups of frequencies may be emitted from different individual nuclei. Some of the γ rays cause (photo-electric) emission of electrons from various extra-nuclear levels, thus producing the β -ray lines in the β -ray spectrum, and rearrangement of the extra-nuclear electrons produces the γ rays which correspond in frequency to characteristic X rays. The nuclear electron finally arrives in a stationary state in which it is not permanently stable and it flies out from the nucleus. The nuclear electrons, one per atom disintegrating, thus leave the atom with different energies and form the continuous β -ray spectrum.

The absorption of γ rays by gases has not been studied at all exhaustively. Chadwick investigated the absorption of the γ rays from radium, i.e., from RaC, in air and in CO₂ by varying the gas pressure, and in air by varying the distance from the source. Hess made measurements in air by varying the distance. Chadwick's value for μ in air, reduced to atmospheric pressure and 15° C, is $6.0 \times 10^{-5}/\text{cm}$ and Hess' value is 4.47×10^{-5} cm.

Ahmad and Ahmad-Stoner find that the absorption coefficient per atom can be expressed as the sum of two terms, $aZ + bZ^4$, which corresponds to a similar expression for the absorption of X rays, $aZ + \beta\lambda^3Z^4$, the first term representing scattering and the second term true absorption.

Ionization by gamma rays.—With the development of the theory of atomic structure by study of X rays and γ rays, of ionizing potentials, and by applications of the quantum theory, views on ionization by γ rays have become more definite. When an X ray or a γ ray traverses matter its energy $h\nu$ may be absorbed ($h\nu = E + W$), an electron requiring energy W to remove it from the atom being ejected with residual kinetic energy E . Such an electron has generally been called a secondary β ray. It in turn may react with another atom, losing energy equivalent at least to the ionizing potential of a particular energy level in the atom ionized, repeating the process until its energy is dissipated, and leaving electrons and positive ions in its trail. Each of the ejected tertiary electrons if possessing sufficient energy, loses energy in the same manner.

Moseley-Robinson's values for the total number of pairs of ions produced per sec. in air at n.p.t. by γ rays from quantities of RaB and RaC in equilibrium with 1 g of Ra are 0.84×10^{14} and 11.34×10^{14} , respectively. From Chadwick's value for the coefficient of absorption in air the mean "range" is $1/\mu = 1.6 \times 10^4$ cm. This gives as a mean value 7.5×10^{10} pairs of ions/sec./cm of path in air for all the penetrating γ rays from 1 g of radium in equilibrium, and, taking one γ ray per atom of RaB and RaC disintegrating (Kovarik), this means about one pair of ions per cm of path in air for each penetrating γ ray.

RADIOACTIVITY

GAMMA RAYS

It is evident from the quantum relation, $h\nu = E + W$, that γ rays of given frequency will cause the emission of β particles of definite velocities, one for each energy level that can be ionized, from an atom of a given element (including all its isotopes). This has been proved experimentally and has been used in determining the energy of the exciting γ rays. A discussion of the subject of photoelectron emission by X rays has been given by A. H. Compton.

When γ rays pass through thin layers the β radiation leaving the layer on the side where the X ray beam emerges is more intense than that on the side where the X ray beam is incident. The asymmetry of this β radiation was more marked for light atoms than for heavy atoms; also for hard than for soft γ rays.

Scattering of gamma rays.—When γ rays are incident on matter γ rays may be detected on all sides of the piece as if emitted by it. γ rays so re-radiated were called "secondary" γ rays. These secondary γ rays appear to be really a mixture of two types: (1) scattered primary γ rays; (2) fluorescent or characteristic X rays produced in the atoms of the secondary radiator by high velocity electrons liberated photoelectrically by the primary γ rays.

Ishino's values of the mass scattering coefficient for Al, Fe, and Pb are respectively, 0.045, 0.042, and 0.034 (cm^2/gm). The softening of the "secondary" γ rays is undoubtedly due to (1) the production of fluorescent radiation which may be in part (Compton) similar to the general "white" radiation emitted by an X-ray tube, and (2) a modification of the true primary scattered radiation. The scattering of γ rays by thin sheets indicates that the scattering per atom is nearly proportional to the atomic number, and that each electron appears therefore to act as an independent center for scattering whether it is one of a small number of electrons (Al) or one of a larger number (Pb). The scattered radiation on the emergent side is greater in amount than that on the incident side.

Comparison of gamma-ray sources.—The relative ionizing powers of different types of γ radiation need to be known if the quantity of any γ -ray emitter is to be determined by comparison with a radium standard. The amount of MsTh_2 in equilibrium with 1 g of Th, e.g., one month after separation of MsTh_1 , gives a γ -ray ionization equivalent to that from 0.524×10^{-7} g Ra in equilibrium with its γ -ray products. The amount of ThC'' in equilibrium with 1 g Th gives a γ -ray ionization equivalent to that from 0.956×10^{-7} g Ra in equilibrium with its γ -ray products. Since MsTh_1 and Ra are isotopes, chemical separation is impossible, and since the γ rays compared are of nearly the same quality the detection and estimation of mesothorium impurities in radium by γ -ray measurements (usually used for standardization) is somewhat difficult. Hahn and Bothe have shown how to distinguish between these materials by absorption experiments. Mme. Curie has shown that the ratio of the total heating effect to the γ -ray activity is also characteristic of the proportion of mesothorium in a mixture of the two.

RADIOACTIVITY

ABSORPTION OF CHARACTERISTIC GAMMA RAYS

| Source and type of decay | Level assumed | In Aluminum | | | In Lead | | |
|---------------------------|---------------|----------------------|---------------------------|-----------------------------------|----------------------|---------------------------|-----------------------------------|
| | | Half value thickness | Absorption coefficient | Mass absorption coefficient | Half value thickness | Absorption coefficient | Mass absorption coefficient |
| | | <i>D</i> cm | μ cm ⁻¹ | μ/ρ cm ² /gm | <i>D</i> cm | μ cm ⁻¹ | μ/ρ cm ² /gm |
| UX ₁ β | L | 0.029 | 24 | 8.9 | | | |
| | K | .99 | .70 | .26 | 0.30 | 2.3 | 0.20 |
| UX ₂ β | * | 4.95 | .140 | .052 | .96 | .72 | .064 |
| Io α | M | .00064 | 1088 | 400 | | | |
| | L | .0307 | 22.7 | 8.35 | | | |
| | K | 1.7 | .41 | .15 | | | |
| Ra α | M | .0020 | 354 | 130 | | | |
| | L | .043 | 16.3 | 6 | | | |
| | * | 2.6 | .27 | .1 | | | |
| RaB β | M | .0030 | 230 | 85 | .015 | 46 | 4.1 |
| | L | .0173 | 40 | 15 | .15 | 4.6 | .41 |
| | K | 1.22 | .57 | .21 | .46 | 1.5 | .13 |
| RaC + C'' | | .0030 | 230 | 85 | .015 | 46 | 4.1 |
| α , β | | .0173 | 40 | 15 | .15 | 4.6 | .41 |
| | * | 3 | .230 | .085 | .46 | 1.496 | .132 |
| | * | 5.46 | .127 | .047 | 1.30 | .535 | .047 |
| RaD β | L | .0154 | 45 | 16.7 | | | |
| | K | .70 | 1.17 | .37 | | | |
| RaE β | | .0154 | 45 | 16.7 | | | |
| | * | .70 | .99 | .37 | | | |
| | * | 2.79 | .25 | .092 | | | |
| RaF β | M | .00120 | 2700 | 215 | | | |
| | L | | 46 | | | | |
| RdAC α | L | .28 | 25 | 9.3 | | | |
| | * | 3.65 | .190 | .070 | | | |
| AcB β | M | .0058 | 120 | 44 | | | |
| | L | .022 | 31 | 11.5 | | | |
| | K | 1.54 | .45 | .167 | | | |
| AcC'' β | * | 3.50 | .198 | .073 | | | |
| MsTh ₂ β | L | .027 | 26 | 9.6 | .061 | 11.3 | 1.00 |
| | * | 6.0 | .116 | .043 | .25 | 2.8 | .25 |
| | * | | | | .99 | .70 | .062 |
| RdTh | | | | | small | great | great |
| ThB β | M | .0043 | 160 | 59 | | | |
| | L | .022 | 32 | 11.9 | | | |
| | K | 1.9 | .36 | .133 | | | |
| ThC'' β | * | 7.2 | .096 | .036 | 1.5 | .46 | .041 |

Potassium, β rays, μ_{Fe} , 0.19; μ_{Pb} , 0.14; μ_{Al} , 0.065, * 0.14*.

* Nucleus.

RADIOACTIVITY

TABLE 650.—Characteristic Gamma-Ray Wave Lengths and Energies Estimated from Absorption and Scattering

(Taken from Kovarik, McKeehan, Nat. Res. Council Bull., 51, 1929.)

| Source | λ cm $\times 10^{-11}$ | Energy | | Reference |
|-------------------------|-----------------------------------|---------------------|-----------------------|-------------------------|
| | | volts $\times 10^5$ | ergs $\times 10^{-7}$ | |
| UX ₁ 90 UI | 903 | 0.137 | 0.217 | Lang, '21 |
| | 220 | .562 | .894 | |
| UX ₂ 91 U | 115 | 1.069 | 1.701 | " |
| Io 90 Ra | 4140 | .030 | .047 | " |
| | 880 | .140 | .223 | " |
| | 176 | .699 | 1.112 | " |
| Ra 88 Ra | 2640 | .047 | .074 | " |
| | 771 | .160 | .260 | " |
| | 150 | .822 | 1.308 | " |
| RaB 82 RaI | 2230 | .055 | .088 | " |
| | 1110 | .111 | .177 | " |
| | 202 | .610 | .970 | " |
| RaC 83 RaI | 141 | .877 | 1.395 | " |
| | 111 | 1.112 | 1.769 | " |
| | 27.5 | 4.483 | 7.135 | Compton, '21 |
| | 20 | 6.165 | 9.810 | Owen-Fleming, Fage, '24 |
| | 17 | 7.252 | 11.54 | Ahmad, '24 |
| RaD 82 RaII | 1160 | .106 | .169 | Lang, '21 |
| | 1063 | .116 | .184 | O, F, F, '24 |
| | 252 | .489 | .778 | Lang, '21 |
| | 290 | .425 | .677 | Meitner, '22 |
| RaF 84 RaIII | 3230 | .038 | .061 | Lang, '21 |
| RdAc 90 Ac | 918 | .134 | .214 | " |
| | 130 | .946 | 1.506 | " |
| AcB 82 AcI | 1720 | .072 | .114 | " |
| | 1000 | .123 | .192 | " |
| | 184 | .670 | 1.066 | " |
| AcC'' 81 Ac | 132 | .931 | 1.481 | " |
| MsTh ₂ 89 Th | 932 | .132 | .210 | " |
| | 107 | 1.153 | 1.834 | " |
| ThB 82 ThI | 1930 | .064 | .102 | " |
| | 1010 | .122 | .194 | " |
| | 168 | .733 | 1.166 | " |
| ThC'' 83 Th | 99 | 1.243 | 1.978 | " |

TABLE 651.—Nuclear Energy Deduced from Gamma-Ray Spectra

(Kovarik, McKeehan, Nat. Res. Council Bull., 51, 1925.)

| Nucleus | Energy of level volts $\times 10^5$ | No. of γ rays accounted for (each counted twice) | Nucleus | Energy of level volts $\times 10^5$ | No. of γ rays accounted for (each counted twice) |
|---------|--|--|---------|--|--|
| RaB | 0 | 4 | TnC'' | 0 | 7 |
| | .537 | 6 | | .41 | 5 |
| | .625 (0.628) | 4 | | .56 | 2 |
| | 2.571 (2.572) | 4 | | 2.28 | 2 |
| | 2.942 | 3 | | 2.48 | 4 |
| | 4.048 | 3 | | 2.54 | 3 |
| RaC | 5.31 | 4 | | 2.74 | 3 |
| | 0 | 2 | | 5.11 | 5 |
| | .59 | 4 | | 9.02 | 3 |
| | .70 | 1 | | | |
| | 3.07 | 2 | | | |
| | 3.30 | 2 | | | |
| | 4.45 | 1 | | | |

Ellis, Skinner, 1924; values in 3rd column of TnC'' supplied by Kovarik, McKeehan.

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GAMMA-RAY WAVE LENGTHS AND ENERGIES MEASURED BY CRYSTAL REFLECTION

(Taken from Kovarik, McKeehan, Nat. Res. Council Bull., 51, 1929.)

PART 1
Reflection from (100) Planes of Rock Salt ($d = 2.814 \times 10^{-8}$ cm)

| Source | θ | λ cm $\times 10^{-11}$ | Energy volts $\times 10^5$ | Energy ergs $\times 10^{-7}$ | Int. | Ref. |
|------------|-----------------|-----------------------------------|-------------------------------|---------------------------------|------|------|
| RaB 82 RaI | $14^\circ-02'$ | 1365 | 0.0903 | 0.1437 | m. | I |
| | $13^\circ-52'$ | 1349 | .0914 | .1455 | m. | I |
| | $13^\circ-31'$ | 1315 | .0937 | .1492 | w. | I |
| | $13^\circ-14'$ | 1288 | .0957 | .1523 | w. | I |
| | $13^\circ-00'$ | 1266 | .0974 | .1550 | w. | I |
| | $12^\circ-31'$ | 1220 | .1011 | .1609 | w. | I |
| | $12^\circ-16'$ | 1196 | .1031 | .1641 | m. | I |
| | $12^\circ-03'$ | 1175 | .1049 | .1670 | s. | I |
| | $11^\circ-42'$ | 1141 | .1080 | .1719 | m. | I |
| | $11^\circ-17'$ | 1101 | .1120 | .1782 | w. | I |
| | $11^\circ-00'$ | 1074 | .1148 | .1827 | w. | I |
| | $10^\circ-48'$ | 1055 | .1169 | .1860 | w. | I |
| | $10^\circ-32'$ | 1029 | .1198 | .1907 | m. | I |
| | $10^\circ-18'$ | 1006 | .1225 | .1950 | m. | I |
| | $10^\circ-03'$ | 982 | .1255 | .1998 | s. | I |
| | $9^\circ-45'$ | 953 | .1294 | .206 | m. | I |
| | $9^\circ-23'$ | 918 | .1344 | .214 | w. | I |
| | $8^\circ-43'$ | 853 | .1446 | .230 | m. | I |
| | $8^\circ-34'$ | 838 | .1471 | .234 | m. | I |
| | $8^\circ-16'$ | 809 | .1524 | .242 | m. | I |
| | $8^\circ-06'$ | 793 | .1555 | .247 | m. | I |
| | $4^\circ-22'$ | 428 | .288 | .458 | | 2, 3 |
| | $4^\circ-00'$ | 393 | .314 | .500 | | 2, 3 |
| | $3^\circ-18'$ | 324 | .381 | .606 | | 2, 3 |
| | $3^\circ-00'$ | 294 | .419 | .666 | | 2, 3 |
| | $2^\circ-40'$ | 262 | .471 | .749 | | 2, 3 |
| | $2^\circ-28'$ | 242 | .509 | .810 | | 2, 3 |
| | $2^\circ-20'$ | 229 | .538 | .856 | | 2, 3 |
| | $2^\circ-00'$ | 196.4 | .628 | .999 | | 2, 3 |
| | $\{1^\circ-43'$ | 168.6 | .731 | 1.164 | | 2, 3 |
| | $\{1^\circ-37'$ | 158.8 | .776 | 1.236 | | 2, 3 |
| | $1^\circ-24'$ | 137.5 | .897 | 1.427 | | 2, 3 |
| RaC 83 RaI | $1^\circ-10'$ | 114.6 | 1.076 | 1.712 | | 2, 3 |
| | $1^\circ-00'$ | 98.2 | 1.255 | 1.998 | | 2, 3 |
| | $0^\circ-43'$ | 70.4 | 1.752 | 2.79 | | 2, 3 |

PART 2
Reflection from (111) Planes of Calcite ($d = 3.028 \times 10^{-8}$ cm)

| | | | | | | |
|------------|-----------------|------|-------|-------|---|------|
| RaC 83 RaI | $0^\circ-41'$ | 72.2 | 1.707 | 2.716 | 4 | Note |
| | $0^\circ-37.5'$ | 66.1 | 1.866 | 2.772 | 4 | |
| | $0^\circ-33'$ | 58.1 | 2.121 | 3.375 | 4 | Note |
| | $0^\circ-27.5'$ | 48.4 | 2.545 | 4.050 | 4 | |
| | $0^\circ-21'$ | 37 | 3.333 | 5.304 | 4 | |
| | $0^\circ-16'$ | 28.1 | 4.374 | 6.961 | 4 | |

NOTE.—Possibly second order.

References: 1 Rutherford-Andrade (s. strong, m. medium, w. weak), '14.

2 Rutherford-Andrade, '14.

3 Rutherford, '14.

4 Kovarik, '22.

RADIOACTIVITY

QUANTITIES IN RADIOACTIVE EQUILIBRIUM

(Taken from 1930 Report International Radium Standards Commission, Rev. Mod. Phys., 3, 427, 1931.)

| | | T | M (mass units) for Ra = 1 | for U1 = 1 |
|---------------------------------------|-------------------|---|---|---------------------------|
| 99.65% .35% 3% | UI | $1.39 \cdot 10^{17} \text{s}$ | $2.94 \cdot 10^6$ | 1.00 |
| | UX ₁ | $2.12 \cdot 10^6$ | $4.4 \cdot 10^{-5}$ | $1.5 \cdot 10^{-11}$ |
| | | $(2.06) 10^6$ | $(4.3) \cdot 10^{-5}$ | |
| | UX ₂ | 68.4 | $1.4 \cdot 10^{-9}$ | $5 \cdot 10^{-16}$ |
| | UZ | $2.4 \cdot 10^4$ | $1.7 \cdot 10^{-8}$ | $6 \cdot 10^{-16}$ |
| | UII | $9.4 \cdot 10^{12}$ | $2.0 \cdot 10^2$ | $6.7 \cdot 10^{-5}$ |
| | UY | $8.88 \cdot 10^4$ | $5.6 \cdot 10^{-8}$ | $1.9 \cdot 10^{-14}$ |
| 97% 99.96% .04% | Io | $2.6 \cdot 10^{12} \text{s}$ | 52.7 | |
| | Ra | $5.02 \cdot 10^{10}$ | 1.00 | |
| | Rn | $3.303 \cdot 10^3$ | $6.47 \cdot 10^{-6}$ | |
| | RaA | 183 | $3.52 \cdot 10^{-9}$ | |
| | RaB | $1.61 \cdot 10^3$ | $3.04 \cdot 10^{-8}$ | |
| | RaC | $1.18 \cdot 10$ | $2.23 \cdot 10^{-8}$ | |
| | RaC' | ca 10^{-6} | ca $2 \cdot 10^{-19}$ | |
| | RaC'' | 79.2 | $6 \cdot 10^{-13}$ | |
| | RaD | $6.94 \cdot 10^8$ | $1.28 \cdot 10^{-2}$ | |
| | RaE | $4.26 \cdot 10^5$ (4.9d) | $7.9 \cdot 10^{-6}$ | |
| | Po = RaF | $4.32 \cdot 10^5$ (5.0d) $1.21 \cdot 10^7$ | $8.0 \cdot 10^{-6}$ $2.24 \cdot 10^{-4}$ | |
| for Ra = 1 and 3% branching fraction | | | | |
| .32% 99.68% | Pa | $1.01 \cdot 10^{12} \text{s}$ | .62 | |
| | Ac | $4.23 \cdot 10^8$ | $2.5 \cdot 10^{-4}$ | |
| | | $(6.3 \cdot 10^8 = 20 \text{ yr})$ | $(3.7 \cdot 10^{-4})$ | |
| | RdAc | $1.63 \cdot 10^6$ | $9.8 \cdot 10^{-7}$ | |
| | AcX | $9.7 \cdot 10^5$ | $5.8 \cdot 10^{-7}$ | |
| | An | 3.92 | $2.27 \cdot 10^{-12}$ | |
| | AcA | $2 \cdot 10^{-3}$ | $1.14 \cdot 10^{-15}$ | |
| | AcB | $2.16 \cdot 10^{-3}$ | $1.21 \cdot 10^{-9}$ | |
| | AcC | 130 | $7.2 \cdot 10^{-11}$ | |
| | AcC' | ca 10^{-3} | ca $2 \cdot 10^{-18}$ | |
| | AcC'' | 286 | $1.57 \cdot 10^{-10}$ | |
| | | (283) | $1.55 \cdot 10^{-10}$ | |
| | | | for Th = 1 | for MsTh ₁ = 1 |
| 65% 35% | Th | $5.6 \cdot 10^{17} \text{s}$ | 1.00 | $2.7 \cdot 10^9$ |
| | MsTh ₁ | $2.1 \cdot 10^8$ | $3.68 \cdot 10^{-10}$ | 1.00 |
| | MsTh ₂ | $2.21 \cdot 10^4$ | $3.88 \cdot 10^{-14}$ | $1.05 \cdot 10^{-4}$ |
| | RdTh | $6.0 \cdot 10^7$ | $1.05 \cdot 10^{-10}$ | .286 |
| | ThX | $3.14 \cdot 10^5$ | $5.41 \cdot 10^{-13}$ | $1.47 \cdot 10^{-3}$ |
| | Tn | 54.5 | $9.23 \cdot 10^{-17}$ | $2.50 \cdot 10^{-7}$ |
| | ThA | .14 | $2.32 \cdot 10^{-19}$ | $6.31 \cdot 10^{-10}$ |
| | ThB | $3.82 \cdot 10^4$ | $6.23 \cdot 10^{-14}$ | $1.69 \cdot 10^{-4}$ |
| | ThC | $3.63 \cdot 10^3$ | $5.92 \cdot 10^{-15}$ | $1.61 \cdot 10^{-5}$ |
| | ThC' | ca 10^{-9} | ca $3 \cdot 10^{-27}$ | ca $3 \cdot 10^{-18}$ |
| | | or 10^{-6} | 10^{-14} | $3 \cdot 10^{-15}$ |
| | ThC'' | 186 | $1.04 \cdot 10^{-16}$ | $2.83 \cdot 10^{-7}$ |

TABLE 654

CATHODE RAYS

Prepared by W. W. Nicholas, Bur. Standards

Cathode rays are swiftly moving electrons, and thus are of the same nature as β rays (see tables on radioactivity, pages 526 to 528). They are produced in gas discharge tubes. At comparatively low pressures the cathode rays thus produced have a nearly uniform velocity. Free electrons are emitted from hot bodies (Table 667), especially if the heated substance is coated with barium, calcium, or strontium oxide (Wehnelt cathode). These electrons can be given any desired speed if the heated substance (usually in the form of a wire) be enclosed in an evacuated tube and the difference of potential (I') applied between the wire (cathode) and another electrode (anode, anticathode, or target). The speed (v) of the cathode rays, expressed as a fractional part (β) of the speed of light ($\beta = v/c$, where c is the speed of light), when they have fallen through the entire potential difference, is given by the formula (corrected for the relativity change of mass)

$$V = 508.1 \{ (1 - \beta^2)^{\frac{1}{2}} - 1 \}$$

where V is in absolute kilovolts. The equivalent power series,

$$I' = 254.0 \{ \beta^2 + (\frac{3}{4})\beta^4 + (\frac{5}{8})\beta^6 + (\frac{35}{16})\beta^8 \dots \},$$

is useful for calculations at low and intermediate speeds (error is about 1% for $\beta = 0.60$, using terms given here). A tabulation of the corresponding values of I' (absolute kilovolts) and β follows. An electron speed of 0.2 cm/sec. is spoken of, e.g., as a 10.5 kilovolt electron, or as having an equivalent voltage of 10.5 kv.

| β | V | β | V | β | V | β | V | β | V |
|---------|--------|---------|-------|---------|-------|---------|-------|---------|-------|
| 0.02 | 0.1017 | 0.22 | 12.76 | 0.42 | 51.77 | 0.62 | 130.5 | 0.82 | 370.6 |
| .04 | .4070 | .24 | 15.30 | .44 | 57.71 | .64 | 153.2 | .84 | 428.3 |
| .06 | .9170 | .26 | 18.10 | .46 | 64.13 | .66 | 168.2 | .86 | 487.6 |
| .08 | 1.634 | .28 | 21.17 | .48 | 71.08 | .68 | 184.9 | .88 | 561.6 |
| .10 | 2.560 | .30 | 24.53 | .50 | 78.60 | .70 | 203.4 | .90 | 657.5 |
| .12 | 3.699 | .32 | 28.20 | .52 | 86.75 | .72 | 224.1 | .92 | 788.3 |
| .14 | 5.054 | .34 | 32.19 | .54 | 95.58 | .74 | 247.3 | .94 | 981.1 |
| .16 | 6.631 | .36 | 36.51 | .56 | 105.2 | .76 | 273.7 | .96 | 1307 |
| .18 | 8.436 | .38 | 41.20 | .58 | 115.6 | .78 | 303.8 | .98 | 2045 |
| .20 | 10.48 | .40 | 46.28 | .60 | 127.0 | .80 | 338.7 | | |

Cathode rays whose direction of motion is perpendicular to the direction of a uniform magnetic field (H) describe a circular path of radius (r) according to the formula (corrected for relativity change of mass of electron)

$$Hr = 1695 \{ \beta(1 - \beta^2)^{\frac{1}{2}} \}$$

where H is expressed in gauss and r in cm.

When they impinge on matter, cathode rays are deflected from their original direction of motion. These deflections grade all the way from 180° "reflections" to the "diffusion" corresponding to deflections through very small angles. The large-angle deflections are ordinarily comparatively infrequent. However, when the substance struck by the cathode rays is crystalline, certain directions may be preferred by the deflections. Here the beam of cathode rays behaves as though it consisted of a train of waves of wave length $\lambda_c = 0.02428/\beta$, where λ_c is in Angstroms. The preferred directions for the "reflected" cathode ray beams may be calculated from the Bragg formula (see Siegbahn's "X-ray Spectroscopy"). The simple Bragg formula is quite limited in application here, however, since refraction in the crystal is very appreciable for the cathode ray beams. In general, the cathode rays which have been deflected by matter will have lost speed, but the rays which have undergone these "preferred" deflections remain of the same speed as the primary cathode beam.

Cathode rays lose speed on penetrating matter. The losses of speed by individual cathode particles grade from complete stoppage to no loss of speed. The majority of the cathode particles, however, lose speed according to the relation (Thomas-Whiddington-Bohr law)

$$\beta_0^4 - \beta^4 = ax$$

where β_0 is the initial speed, and β the speed after traversing a path length x in the material (x to be measured in cm along the actual curved path), and a is a constant roughly equal to 6.5ρ where ρ is the density of the material in g/cm^3 . A convenient form for the expression is the following. Note that the two forms are not equivalent except at very low speeds (experiment has not yet decided between the two):

$$V_0^2 - V^2 = bx$$

where V_0 and V are the initial and final "equivalent voltages" (see above) of the cathode rays, in kv, and b is a constant roughly equal to $40 \times 10^3\rho$. A tabulation of experimental values of a and b for various materials follows:

RÖNTGEN RAYS (X RAYS)

TABLE 655.—Constants for Cathode-Ray Speeds in Matter

| Material | <i>a</i> | <i>b</i> |
|------------------------------|----------|--------------------|
| Beryllium | 12. | 0.75×10^6 |
| Aluminum | 17. | 1.1 " |
| Copper | 56. | 3.6 " |
| Silver | 66. | 4.2 " |
| Gold | 138. | 9.0 " |
| Moist air, 76 cm, 18° C..... | 0.0062 | 0.44×10^3 |

TABLE 656.—X-Ray Emission

X Rays are generated whenever and wherever swiftly moving electrons (cathode rays) strike matter. This process occurs in gas discharge tubes at moderately low pressures (about 0.001 to 0.01 mm Hg); the gas-filled X-ray tube is based on this principle. The Coolidge tube, in which the gas pressure is so low (less than 10^{-4} mm Hg) as not to play a part, is superior for most purposes: the electrons, supplied by a hot filament incorporated in the cathode, are given a high velocity by the application of a high potential (as high as 300,000 v, in certain types); these cathode rays are directed against an area ("focal spot") on the anode ("target," "anticathode") where the X rays are generated.

These X rays are of two types: continuous spectrum rays ("heterogeneous," "general," or "white" radiation) and characteristic rays (line spectra).

Continuous spectrum X rays are a direct result of the acceleration of the cathode rays due to their close contacts with the atoms of the anticathode. The spectrum energy distribution of this radiation, from a tube whose electrodes are maintained at a constant potential difference (I'), is described very roughly by the formula (for a more accurate type of formula, see the I.C.T. vol. 6)

$$J_\nu d\nu = C(\nu_0 - \nu)e^{-c/\nu^2} d\nu \quad \nu \leq \nu_0 \quad (1)$$

for an energy-frequency graph, or by

$$J_\lambda d\lambda = (K/\lambda^2) \left\{ 1/\lambda_0 - 1/\lambda \right\} e^{-k\lambda^2} d\lambda \quad \lambda \geq \lambda_0 \quad (2)$$

for an energy-wave length graph. In these two formulae, J_ν or J_λ is the energy between frequencies, ν and $\nu + d\nu$, or wave lengths λ and $\lambda + d\lambda$, respectively, c , the base of natural logarithms, and ν_0 and λ_0 the highest frequency and shortest wave length, respectively of the spectrum ("high frequency limit," "short wave-length limit," "spectrum limit"). For X rays generated inside the anticathode c and k are zero; this simplifies the formulae, the exponential term becoming unity. For the X ray obtained outside the tube, c and k have values, estimates of which are tabulated in Table 660. The factor, c or k , determines the energy of the X rays; the convenient way to evaluate this energy is, instead of assigning numerical values to c or k , to evaluate E_1 and I_1 (Table 660). ν_0 and λ_0 depend only on the voltage (I'), the relations being:

$$\lambda_0 = 12.336/I' \quad (3)$$

$$\nu_0 = 243.0 \times 10^{15} I' \quad (4)$$

(λ and λ_0 are expressed throughout this section in Angstrom units, 10^{-8} cm, and ν and ν_0 are in sec^{-1} , and I' is in kilovolts absolute.)

The energy of the continuous spectrum X rays, E_1 , produced in the anticathode ordinarily comprises a major fraction of the total X-ray energy generated; the energy of the characteristic rays, E_2 , comprises the minor fraction. ($E_1 + E_2$) is only an exceedingly small fraction of the electrical energy, E_3 , supplied to the tube. E_1/E_3 is called the efficiency of production of continuous spectrum X rays, and is closely represented by the formula

$$E_1/E_3 = ZI' \times 13 \times 10^{-7},$$

where Z is the atomic number of the material of the anticathode, and I' is expressed in kilovolts. On account of losses by absorption in the anticathode and in the walls of the tube only a small part of this energy generated inside the anticathode gets outside the tube. Table 660 supplies some numerical values of this "usable" energy, for tubes similar to the standard commercial types.

Characteristic X rays result from the ionization of atoms, either (1) by direct cathode ray impact, or (2) by absorption of X rays. In the anticathode of an X-ray tube both these processes occur. With a silver anticathode, for example, at any voltage between 35 and 80 kv, process (1) accounts for about 65% of the energy of the characteristic rays.

RÖNTGEN RAYS (X RAYS)

EMISSION LINES AND CRITICAL ABSORPTION LIMITS

(in Angstroms)

The characteristic rays group themselves naturally into several groups, K, L, M, etc.; for any given element the lines in one group differ from each other in wave length by amounts which are small compared with the differences between separate groups. The wave lengths of the characteristic rays vary only with the material of the anticathode; these wave lengths, for some of the more prominent lines are given in the table below.

λ_a is the wave length of the critical absorption limit associated with the emission lines listed in the same subgroup. Taken by permission from Compton, "X-rays and Electrons."

| Atomic number, Element | K | | | | | L | Group |
|------------------------------|----------------|------------|-----------|------------|------------|----------------|-----------|
| | K | | | | | L ₁ | Sub-group |
| | λ_a | γ_1 | β_1 | α_1 | α_2 | λ_a | |
| 1 H | 911.76 | | | | | | 1 H |
| 2 He | 524 | | | | | | 2 He |
| 3 Li | 235 | | | | | 2500 | 3 Li |
| 4 Be | 133 | | | | | 1360 | 4 Be |
| 5 B | 84 | | | | | 580 | 5 B |
| 6 C | 49.3 | | | | | 380 | 6 C |
| 7 N | 36.5 | | | | | 300 | 7 N |
| 8 O | 24.6 | | | | | 250 | 8 O |
| 9 F | 18.6 | | | | | 210 | 9 F |
| 10 Ne | 14.5 | | absent | 18.37 | | 180 | 10 Ne |
| 11 Na | | | 11.591 | 11.8836 | | 146 | 11 Na |
| 12 Mg | <i>9.5112*</i> | | 9.5345 | 9.86775 | | 117 | 12 Mg |
| 13 Al | <i>7.9470</i> | | 7.9405 | 8.31940 | | 101 | 13 Al |
| 14 Si | | | 6.7393 | 7.10917 | | 84 | 14 Si |
| 15 P | <i>5.7580</i> | | 5.7890 | 6.14171 | | 69 | 15 P |
| 16 S | <i>5.0123</i> | | 5.0213 | 5.36090 | 5.36375 | 56 | 16 S |
| 17 Cl | <i>4.3844</i> | | 4.3946 | 4.71821 | 4.72136 | 46 | 17 Cl |
| 18 A | <i>3.8657</i> | | | | | 37 | 18 A |
| 19 K | <i>3.4345</i> | | 3.44680 | 3.73368 | 3.73706 | 33.1 | 19 K |
| 20 Ca | <i>3.0633</i> | | 3.08343 | 3.35169 | 3.35495 | 28.9 | 20 Ca |
| 21 Sc | <i>2.7517</i> | | 2.77394 | 3.02503 | 3.02840 | 25.4 | 21 Sc |
| 22 Ti | <i>2.4937</i> | 2.4937 | 2.50808 | 2.74317 | 2.74681 | 22.5 | 22 Ti |
| 23 Va | <i>2.2653</i> | 2.2646 | 2.27972 | 2.49835 | 2.50213 | 20.0 | 23 Va |
| 24 Cr | <i>2.0648</i> | 2.0670 | 2.08045 | 2.28484 | 2.28895 | 17.7 | 24 Cr |
| 25 Mn | <i>1.8803</i> | 1.8932 | 1.90591 | 2.09732 | | 16.0 | 25 Mn |
| 26 Fe | <i>1.7377</i> | 1.7406 | 1.75272 | 1.93230 | 1.93651 | 14.6 | 26 Fe |

* The values in italics are observed values. Other critical absorption limits are computed or interpolated.

RÖNTGEN RAYS (X RAYS)
EMISSION LINES AND CRITICAL ABSORPTION LIMITS
(in Angstroms)

| Atomic number, Element | K | | | | | L | Group |
|------------------------------|-------------|------------|-----------|------------|------------|----------------|-----------|
| | K | | | | | L ₁ | Sub-group |
| | λ_a | γ_1 | β_1 | α_1 | α_2 | λ_a | |
| 24 Cr | 2.0648 | 2.0670 | 2.08045 | 2.28484 | 2.28895 | 17.7 | 24 Cr |
| 25 Mn | 1.8893 | 1.8932 | 1.90591 | 2.09732 | ... | 16.0 | 25 Mn |
| 26 Fe | 1.7377 | 1.7406 | 1.75272 | 1.93230 | 1.93651 | 14.6 | 26 Fe |
| 27 Co | 1.6018 | 1.6054 | 1.61713 | 1.78528 | 1.78956 | 13.2 | 27 Co |
| 28 Ni | 1.4890 | 1.4854 | 1.49703 | 1.65461 | 1.65854 | 12.1 | 28 Ni |
| 29 Cu | 1.3785 | 1.3780 | 1.38933 | 1.53730 | 1.54116 | 11.0 | 29 Cu |
| 30 Zn | 1.2903 | 1.28097 | 1.29260 | 1.43206 | 1.43587 | ... | 30 Zn |
| 31 Ga | 1.1902 | ... | 1.20591 | 1.33785 | 1.34161 | ... | 31 Ga |
| 32 Ge | 1.1146 | 1.11463 | 1.12671 | 1.25130 | 1.25521 | ... | 32 Ge |
| 33 As | 1.0435 | 1.04290 | 1.05518 | 1.17344 | 1.17741 | ... | 33 As |
| 34 Se | .9790 | .99792 | .99027 | 1.10241 | 1.10642 | ... | 34 Se |
| 35 Br | .9179 | .91827 | .93085 | 1.03756 | 1.04160 | ... | 35 Br |
| 37 Rb | .8143 | .81484 | .82703 | .92360 | .92772 | ... | 37 Rb |
| 38 Sr | .7693 | .76917 | .78151 | .87360 | .87754 | ... | 38 Sr |
| 39 Y | .7235 | .72663 | .73932 | .82700 | .83118 | ... | 39 Y |
| 40 Zr | .6872 | .68835 | .70048 | .78429 | .78850 | ... | 40 Zr |
| 41 Nb | .6503 | .65255 | .66449 | .74457 | .74882 | ... | 41 Nb |
| 42 Mo | .6184 | .61969 | .63124 | .70780 | .71208 | 4.303 | 42 Mo |
| 44 Ru | .5584 | .56048 | .57143 | .64181 | .64615 | ... | 44 Ru |
| 45 Rh | .5330 | .53313 | .54470 | .61201 | .61637 | 3.598 | 45 Rh |
| 46 Pd | .5057 | .50963 | .51972 | .58419 | .58858 | ... | 46 Pd |
| 47 Ag | .4850 | .48607 | .49630 | .55821 | .56264 | 3.2605 | 47 Ag |
| 48 Cd | .4632 | .46438 | .47428 | .53386 | .53829 | ... | 48 Cd |
| 49 In | .4434 | .44409 | .45373 | .51103 | .51546 | ... | 49 In |
| 50 Sn | .4242 | .42485 | .43439 | .48948 | .49396 | ... | 50 Sn |
| 51 Sb | .4005 | .40711 | .41624 | .46933 | .47386 | 2.6327 | 51 Sb |
| 52 Te | .3806 | .39035 | .39924 | .45037 | .45491 | 2.5026 | 52 Te |
| 53 I | .3737 | .37483 | .38341 | .43249 | .43703 | 2.3819 | 53 I |
| 55 Cs | .3444 | ... | .352 | .398 | .402 | 2.1605 | 55 Cs |
| 56 Ba | .3307 | ... | .343 | .388 | .393 | 2.0602 | 56 Ba |
| 57 La | .3186 | ... | .329 | .372 | .376 | 1.971 | 57 La |
| 58 Ce | .3005 | ... | .314 | .355 | .360 | 1.887 | 58 Ce |
| 59 Pr | .2949 | ... | .301 | .342 | .347 | 1.808 | 59 Pr |
| 60 Nd | .2840 | ... | .292 | .330 | .335 | 1.736 | 60 Nd |
| 62 Sm | .2640 | ... | ... | ... | ... | 1.598 | 62 Sm |
| 63 Eu | .2545 | ... | ... | ... | ... | 1.537 | 63 Eu |
| 64 Gd | .2459 | ... | ... | ... | ... | 1.477 | 64 Gd |
| 65 Tb | .2376 | ... | ... | ... | ... | 1.419 | 65 Tb |
| 66 Dy | .2301 | ... | ... | ... | ... | 1.367 | 66 Dy |
| 67 Ho | .2216 | ... | ... | ... | ... | 1.316 | 67 Ho |
| 68 Er | ... | ... | ... | ... | ... | 1.270 | 68 Er |
| 69 Tu | .2085 | ... | ... | ... | ... | 1.220 | 69 Tu |
| 70 Yb | .2010 | ... | ... | ... | ... | 1.177 | 70 Yb |
| 71 Cp | .1951 | ... | ... | ... | ... | 1.137 | 71 Cp |
| 72 Hf | .1901 | ... | ... | ... | ... | 1.098 | 72 Hf |
| 73 Ta | .1836 | .18452 | .18991 | .21488 | .21973 | 1.060 | 73 Ta |
| 74 W | .1781 | .17898 | .18422 | .20862 | .21345 | 1.024 | 74 W |
| 76 Os | .168 | .16875 | .17361 | .19645 | .20131 | ... | 76 Os |
| 77 Ir | ... | .16376 | .16850 | .19065 | .19550 | ... | 77 Ir |
| 78 Pt | .1578 | .15887 | .16370 | .18523 | .19004 | .8921 | 78 Pt |
| 79 Au | .1524 | .15426 | .15902 | .17996 | .18483 | .8613 | 79 Au |
| 80 Hg | .1479 | ... | ... | ... | ... | .8335 | 80 Hg |
| 81 Tl | .1427 | .14539 | .15011 | .16980 | .17466 | .8055 | 81 Tl |
| 82 Pb | .1385 | .14125 | .14606 | .16516 | .17004 | .7803 | 82 Pb |
| 83 Bi | .1346 | ... | .14205 | .16041 | .16525 | .7565 | 83 Bi |
| 90 Th | .1127 | ... | ... | ... | ... | .6044 | 90 Th |
| 92 U | .1075 | .10842 | .11187 | .12640 | .13095 | .5685 | 92 U |

RÖNTGEN RAYS (X RAYS)

EMISSION LINES AND CRITICAL ABSORPTION LIMITS (IN ÅNGSTRÖMS)

| Atomic number, Element | L (continued) | | | | | | | Group |
|------------------------------|-----------------|------------|-----------|------------------|------------|------------|-----------|-----------|
| | L _{II} | | | L _{III} | | | | Sub-group |
| | λ_a | γ_1 | β_1 | λ_a | α_1 | α_2 | β_2 | |
| 24 Cr | 21.2 | | 21.35 | 21.6 | | 21.69 | | 24 Cr |
| 25 Mn | 18.7 | | 19.17 | 19.0 | | 19.48 | | 25 Mn |
| 26 Fe | 17.1 | | 17.27 | 17.5 | | 17.60 | | 26 Fe |
| 27 Co | 15.3 | | | 15.2 | | | | 27 Co |
| 28 Ni | 14.6 | | | 14.9 | | | | 28 Ni |
| 29 Cu | 12.8 | | | 13.1 | | 13.309 | | 29 Cu |
| 30 Zn | | | 11.951 | | | 12.222 | | 30 Zn |
| 31 Ga | | | | | | | | 31 Ga |
| 32 Ge | | | | | | 10.413 | | 32 Ge |
| 33 As | | | 9.3940 | | | 9.6503 | | 33 As |
| 34 Se | | | 8.7172 | | | 8.9706 | | 34 Se |
| 35 Br | | | 8.1076 | | | 8.3566 | | 35 Br |
| 37 Rb | | | 7.0604 | | | 7.3027 | | 37 Rb |
| 38 Sr | | | | | | 6.8478 | | 38 Sr |
| 39 Y | | | | | | 6.4349 | | 39 Y |
| 40 Zr | 5.386 | 5.3730 | 5.8228 | 5.577 | | 6.0559 | 5.5734 | 40 Zr |
| 41 Nb | 5.027 | 5.0241 | 5.4796 | 5.228 | 5.7113 | 5.717 | 5.2253 | 41 Nb |
| 42 Mo | 4.702 | 4.7111 | 5.1658 | 4.897 | 5.3943 | 5.400 | 4.9092 | 42 Mo |
| 44 Ru | | 4.17282 | 4.61100 | | 4.83567 | 4.84367 | 4.3619 | 44 Ru |
| 45 Rh | 3.940 | 3.9357 | 4.1221 | 4.128 | 4.58778 | 4.59556 | 4.1221 | 45 Rh |
| 46 Pd | | 3.71636 | 4.13730 | | 4.35850 | 4.36660 | 3.9007 | 46 Pd |
| 47 Ag | 3.2005 | 3.51485 | 3.92664 | 3.6844 | 4.14564 | 4.15382 | 3.69383 | 47 Ag |
| 48 Cd | | 3.32800 | 3.73008 | | 3.94782 | 3.95636 | 3.5064 | 48 Cd |
| 49 In | | 3.15529 | 3.54783 | | 3.76367 | 3.77242 | 3.3312 | 49 In |
| 50 Sn | | 2.99493 | 3.37792 | | 3.59218 | 3.60108 | 3.1679 | 50 Sn |
| 51 Sb | 2.8310 | 2.84507 | 3.21836 | 2.9945 | 3.43177 | 3.44075 | 3.0166 | 51 Sb |
| 52 Te | 2.6837 | 2.70647 | 3.06997 | 2.8470 | 3.28199 | 3.29100 | 2.8761 | 52 Te |
| 53 I | 2.5483 | 2.57748 | 2.93093 | 2.7124 | 3.14166 | 3.15087 | 2.74608 | 53 I |
| 55 Cs | 2.3073 | 2.34252 | 2.67784 | 2.4678 | 2.88610 | 2.89560 | 2.5064 | 55 Cs |
| 56 Ba | 2.1995 | 2.23660 | 2.56224 | 2.3577 | 2.76964 | 2.77904 | 2.3993 | 56 Ba |
| 57 La | 2.068 | 2.13720 | 2.45330 | 2.250 | 2.65968 | 2.66893 | 2.2980 | 57 La |
| 58 Ce | 2.007 | 2.04433 | 2.35100 | 2.158 | 2.55600 | 2.56511 | 2.2041 | 58 Ce |
| 59 Pr | 1.920 | 1.95681 | 2.25390 | 2.072 | 2.45770 | 2.46763 | 2.1148 | 59 Pr |
| 60 Nd | 1.842 | 1.87383 | 2.16221 | 1.902 | 2.36531 | 2.37563 | 2.0314 | 60 Nd |
| 62 Sm | 1.692 | 1.72309 | 1.99357 | 1.841 | 2.19501 | 2.20568 | 1.8781 | 62 Sm |
| 63 Eu | 1.624 | 1.6543 | 1.91631 | 1.773 | 2.11633 | 2.12733 | 1.8082 | 63 Eu |
| 64 Gd | 1.560 | 1.55863 | 1.84246 | 1.709 | 2.04193 | 2.05262 | 1.7419 | 64 Gd |
| 65 Tb | 1.499 | 1.5266 | 1.77268 | 1.646 | 1.97149 | 1.98231 | 1.6790 | 65 Tb |
| 66 Dy | 1.442 | 1.4697 | 1.70658 | 1.588 | 1.90460 | 1.91564 | 1.6198 | 66 Dy |
| 67 Ho | 1.387 | 1.4142 | 1.64350 | 1.532 | 1.84098 | 1.85206 | 1.5637 | 67 Ho |
| 68 Er | 1.335 | 1.3623 | 1.58344 | 1.480 | 1.78040 | 1.79140 | 1.5106 | 68 Er |
| 69 Tm | 1.287 | 1.3127 | 1.5268 | 1.431 | 1.7228 | 1.7339 | 1.4602 | 69 Tm |
| 70 Yb | 1.240 | 1.2648 | 1.4725 | 1.383 | 1.66779 | 1.6789 | 1.4128 | 70 Yb |
| 71 Cp | 1.195 | 1.2203 | 1.4207 | 1.339 | 1.61551 | 1.62636 | 1.3672 | 71 Cp |
| 72 Hf | 1.152 | 1.1765 | 1.3711 | 1.294 | 1.56607 | 1.57704 | 1.3235 | 72 Hf |
| 73 Ta | 1.111 | 1.13471 | 1.32354 | 1.251 | 1.51825 | 1.5294 | 1.2810 | 73 Ta |
| 74 W | 1.0726 | 1.09553 | 1.27917 | 1.2136 | 1.47348 | 1.48452 | 1.24191 | 74 W |
| 76 Os | | 1.02247 | 1.19459 | | 1.38816 | 1.3982 | 1.16838 | 76 Os |
| 77 Ir | | .98841 | 1.15495 | | 1.34834 | 1.35939 | 1.13287 | 77 Ir |
| 78 Pt | .9321 | .95545 | 1.11722 | 1.0704 | 1.31008 | 1.32121 | 1.09950 | 78 Pt |
| 79 Au | .9011 | .92437 | 1.08093 | 1.0393 | 1.27355 | 1.28489 | 1.06775 | 79 Au |
| 80 Hg | .8700 | .8935 | 1.0458 | 1.0067 | 1.2385 | 1.2497 | | 80 Hg |
| 81 Tl | .8415 | .86529 | 1.01266 | .9776 | 1.20471 | 1.21603 | 1.00786 | 81 Tl |
| 82 Pb | .8133 | .83708 | .97990 | .9497 | 1.17202 | 1.18352 | .97990 | 82 Pb |
| 83 Bi | .7874 | .81065 | .94930 | .9216 | 1.14115 | 1.1533 | .95293 | 83 Bi |
| 90 Th | .6286 | .65103 | .76259 | .7506 | .95342 | .96524 | .79108 | 90 Th |
| 92 U | .5918 | .61283 | .71807 | .7214 | .90833 | .92014 | .75268 | 92 U |

RÖNTGEN RAYS (X RAYS)

TABLE 657 (Concluded).—Emission Lines and Critical Absorption Limits
(in Angstroms)

λ_a is the wave length of the critical absorption limit associated with the emission lines listed in the same subgroup. The italicized values are observed; other critical absorption limits are computed or interpolated.

| Atomic number, Element | M | | | | | | | | | Group | |
|------------------------|----------------|-----------------|------------------|----------|-----------------|---------|----------------|------------|------------|-----------|--|
| | M _I | M _{II} | M _{III} | | M _{IV} | | M _V | | | Sub-group | |
| | λ_a | λ_a | λ_a | γ | λ_a | β | λ_a | α_1 | α_2 | | |
| 13 Al | 1100 | 2300 | ... | ... | ... | ... | ... | ... | ... | 13 Al | |
| 25 Mn | 79 | 190 | ... | ... | ... | ... | ... | ... | ... | 25 Mn | |
| 42 Mo | 24.2 | 29.9 | 30.7 | ... | 52.4 | ... | 53.0 | ... | ... | 42 Mo | |
| 52 Te | 12.2 | 14.16 | 15.07 | ... | 21.11 | ... | 21.45 | ... | ... | 52 Te | |
| 66 Dy | 6.042 | 6.699 | 7.731 | ... | 9.28 | 9.323 | 9.54 | ... | ... | 66 Dy | |
| 67 Ho | 5.797 | 6.403 | 7.068 | ... | 8.85 | 8.943 | 9.12 | ... | 9.150 | 67 Ho | |
| 68 Er | 5.567 | 6.190 | 6.897 | ... | 8.50 | 8.573 | 8.75 | ... | 8.783 | 68 Er | |
| 70 Yb | 5.151 | 5.621 | 6.254 | ... | 7.83 | 7.891 | 8.08 | 8.011 | 8.125 | 70 Yb | |
| 71 Lu | 4.963 | 5.427 | 6.067 | ... | 7.542 | 7.582 | 7.78 | 7.803 | 7.820 | 71 Lu | |
| 72 Hf | 4.746 | 5.216 | 5.864 | ... | 7.19 | 7.286 | 7.42 | ... | 7.521 | 72 Hf | |
| 73 Ta | 4.557 | 5.038 | 5.674 | 6.301 | 6.87 | 7.001 | 7.10 | ... | 7.238 | 73 Ta | |
| 74 W | 4.392 | 4.827 | 5.447 | 6.085 | 6.617 | 6.745 | 6.845 | 6.952 | 6.973 | 74 W | |
| 76 Os | ... | ... | ... | 5.672 | ... | 6.256 | ... | 6.459 | 6.481 | 76 Os | |
| 77 Ir | ... | ... | ... | 5.484 | ... | 6.030 | ... | 6.223 | 6.250 | 77 Ir | |
| 78 Pt | 3.746 | 4.083 | 4.700 | 5.303 | 5.618 | 5.820 | 5.830 | 6.026 | 6.041 | 78 Pt | |
| 79 Au | 3.605 | 3.895 | 4.518 | 5.131 | 5.386 | 5.619 | 5.594 | 5.812 | 5.831 | 79 Au | |
| 81 Tl | 3.329 | 3.597 | 4.160 | 4.806 | 4.934 | 5.233 | 5.157 | 5.427 | 5.443 | 81 Tl | |
| 82 Pb | 3.213 | 3.477 | 4.035 | 4.666 | 4.786 | 5.065 | 4.982 | 5.250 | 5.273 | 82 Pb | |
| 83 Bi | 3.081 | 3.333 | 3.894 | 4.513 | 4.569 | 4.894 | 4.762 | 5.078 | 5.107 | 83 Bi | |
| 90 Th | 2.388 | 2.571 | 3.058 | 3.657 | 3.552 | 3.931 | 3.721 | 4.097 | 4.129 | 90 Th | |
| 92 U | 2.228 | 2.385 | 2.873 | 3.472 | 3.326 | 3.709 | 3.491 | 3.885 | 3.901 | 92 U | |

TABLE 658.—Probabilities of Ionization in K and L Shells

An atom ionized, in the K shell, say, by one of the two processes described, can either (a) radiate a quantum of K characteristic radiation, or it can (b) convert an equivalent amount of energy into an ionization (with photoelectric emission) of its own outer shells L, M, etc. (compound photoelectric effect). The probability (u) of occurrence of process (a) subsequent to the ionization of an atom depends on the atom, and on the particular shell ionized. Some numerical values for the probability u are given in the table below.

Values in parentheses are comparatively uncertain.

Ionization in the K shell

| Element | A | Cr | Fe | Co | Ni | Cu | Zn | Se | Br | Kr | Sr | Mo | Ag | I | Xe |
|---------|-----|-----|-----|-------|-----|-----|-----|-----|-----|-------|-----|-----|-------|-------|-------|
| u | .07 | .23 | .28 | (.39) | .36 | .38 | .41 | .54 | .56 | (.51) | .62 | .68 | (.86) | (.75) | (.71) |

Ionization in the L shell

| Element | Kr | Xe |
|---------|-------|-------|
| u | (.13) | (.25) |

RÖNTGEN RAYS (X RAYS)

TABLE 659.—Energy and Efficiency of Production of Characteristic X Rays

The energy, E_2 , of the characteristic rays, as produced inside the anticathode for a given tube and a given type of characteristic ray, varies with the material of the anticathode and the voltage applied to the tube. The rays in a particular subgroup (see Table 657) do not appear at all until a certain critical voltage, V_0 , is reached, then all the rays of the subgroup appear at once. V_0 is given by the formula: $V_0 = 12.336/\lambda_a$, where V_0 is in absolute kilovolts and λ_a in Angstroms. In Table 657 values of λ_a associated with the various subgroups of emission lines are tabulated to the left of the particular lines with which they are associated.

The efficiency of production of the characteristic rays, which may be taken as E_2/E_3 , is given roughly by the formula:

$$E_2/E_3 = G[(V - V_0)^2/V] \quad V > V_0$$

where G is a constant whose dependence on the anticathode material and type of characteristic ray has not yet been broadly investigated. For a silver anticathode and a tube voltage of 50 kv, E_2/E_3 for the K rays is about 0.48×10^{-3} . Due to losses by absorption in the anticathode and walls of the tube only a part of the energy generated in the anticathode reaches the outside of the tube. The following table supplies some estimates of this "usable" energy for tubes similar to the standard commercial types. I_2 , which is a measure of the useful characteristic ray energy, varies with voltage in a different manner than E_2 , on account of the variation with voltage of the absorption in the anticathode. For $V_0 < V < 2V_0$, I_2 is roughly proportional to $(V - V_0)^n$, where n is usually between $3/2$ and 2 ; but at higher voltages some measurements indicate that I_2 increases more slowly with voltage, approaching a limiting value in the neighborhood of $V = 6V_0$.

The relative intensities of the lines in a particular subgroup are independent of voltage for a given element; the variation from element to element is often negligible over long ranges of atomic number. In the K series, and at least for atomic numbers greater than 30, about $5/6$ of the energy is contained in the two α lines; of these two, α_1 is the more intense in the ratio $2:1$. In the L series of tungsten, at 22.75 kv, the ratio of the intensities $\alpha_1:\alpha_2$ is $10:1$; $\beta_1:\beta_2:\beta_3:\beta_4$ have relative intensities $100:55:15:1$; and $\gamma_1:\gamma_2:\gamma_3:\gamma_4$ have $100:14:18:6$.

TABLE 660.—Energy and Quality of Emission X Rays

| Type of tube (anticathode) | V kv | i ma | E_1 ergs/sec. | c sec. ⁻³ | k Å ³ | $(E_2)_K$ ergs/sec. | I_1 | I_2 |
|----------------------------|-----------|-----------|--------------------|---------------------------|-----------------------|------------------------|--------------------------------------|-------|
| | | | | | | | at one m erg/sec. cm ² | |
| Tungsten | 40 | 1.0 | 1.23×10^6 | 0.15×10^{57} | 5.5 | | 2.2 | 0 |
| " | 69 | " | 3.66 " | .17 " | 6.3 | | 10 | 0 |
| " | 100 | " | 7.20 " | .20 " | 7.4 | | 22.5 | 7.3 |
| " | 150 | " | 17.3 " | .25 " | 9.2 | | 50 | 24.2 |
| Silver | 50 | | | | | $.24 \times 10^6$ | | |

NOTE: V is the constant direct current potential difference maintained across the terminals of the tube. For varying voltages (as with a tube supplied directly from a transformer, or with a mechanical rectifier), where V is the peak voltage and i is the average current as read by a milliammeter, all the values tabulated are decreased by an extent dependent on the voltage and current wave forms for the particular outfit used, and therefore difficult to specify here. i is the milliamperage tube current for tubes of the Coolidge type, but not for gas-filled tubes, where there are complicating factors. E_1 is the energy converted per sec., inside the anticathode, into continuous spectrum X rays. $(E_2)_K$ is a similar quantity for the K characteristic rays.

TABLE 660 (continued).—Energy and Quality of Emission X Rays

I_1 is the intensity in the continuous X rays obtained outside the tube at a distance of 1 meter from the focal spot, supposing no filtration other than the unavoidable filtration due to the walls of the tube (assumed equivalent to 1.23 mm of Al), anticathode, etc. For practical purposes, until more thorough data is at hand, I_1 may be assumed proportional to the atomic number of the material of the anticathode. It is expressed in ergs per sec. falling on a 1 cm² surface perpendicular to the X-ray beam. The orientation of the tube is supposed to be the usual one, with X rays taken off perpendicular to the cathode stream, and target face inclined at 45°. I_2 is a similar quantity for the K characteristic rays.

c and k are quantities contained in p. 537, which describe the spectrum distribution of the intensity I_1 .

E_1 and E_2 are probably within 5% and 10%, respectively, of their correct values. I_1 and I_2 depend on the tube walls, the roughness of the target surface, etc., and on such accounts an estimate of accuracy is difficult to make; for a smooth target surface, inclined at 45°, and tube walls of 0.7 mm soda glass, the above values of I_1 and I_2 are probably correct to within 20%.

TABLE 661.—X-Ray Spectroscopy

When an X-ray beam is incident on a crystal in such a manner as to make a glancing angle θ with certain sets of parallel planes within the crystal (adjacent planes, containing large numbers of atoms, for best efficiency), these planes having an interplane spacing d , components of the beam of wave lengths λ , $\lambda/2$, $\lambda/3$, . . . λ/n will be diffracted (or "reflected") according to the relation (Bragg law): $\lambda = 2d \sin \theta$. The angle between the directions of the original beam and the deviated beam is 2θ . Refraction in the crystal would introduce an additional factor in the above formula, but the effect is negligible for all ordinary work.

Values for d , the "lattice constant," for some of the commonly used crystals are tabulated below.

TABLE 662.—Lattice Constants of Crystals

| Crystal | Surface | d in Angstroms at 18° C |
|--|---------------|------------------------------|
| Carborundum | (111) | 2.49 |
| Rock salt | Cleavage face | 2.814 |
| Calcite | Cleavage face | 3.029 |
| Quartz | Prism face | 4.247 |
| Gypsum | Cleavage face | 7.577 |
| K ₄ FeCN ₆ | (100) | 8.408 |
| Mica | Cleavage face | 9.993 |
| Sugar | (100) | 10.57 |
| Al ₂ O ₃ | (100) | 11.23 |

For an extensive tabulation of X-ray data on crystals see the I. C. T., vol. 1.

TABLE 663.—Absorption and Scattering of X Rays; Fluorescence

A beam of X rays loses energy as it traverses matter. For monochromatic rays, this loss of energy is given by the formula: $I/I_0 = e^{-\mu x}$ where I_0 and I represent respectively incident and emergent intensities of a parallel beam normal to a plate of absorbing material of thickness x , e is the base of natural logarithms, and μ is a constant depending only on the wave length of the x rays and the material of the plate.

For the most used range (wave lengths 0.1 to 1.4 Angstroms, and atomic numbers greater than 5; outside this range there are systematic deviations from the formulae) μ is approximated to about 5% or better by the formulae: (See next page.)

RÖNTGEN RAYS (X RAYS)

TABLE 663 (continued).—Absorption and Scattering of X Rays; Fluorescence

$$\begin{aligned}\mu/\rho &= (1/A) (0.0136Z^4\lambda^3 + 0.32Z) & \lambda < \lambda_k \\ \mu/\rho &= (1/A) (0.0020Z^4\lambda^3 + 0.32Z) & \lambda_k < \lambda < \lambda_{L_1}\end{aligned}$$

ρ is the density, Z , the atomic no., A , the atomic weight of the material of the plate, λ , the wave length of the X rays, Angstrom units; x is in cm. Values for λ_k and λ_{L_1} , wave lengths at which materials have "critical absorption discontinuities," are listed in Table 657 under "X-ray Emission" as λ_0 . Numerical values for μ/ρ , the "mass absorption coefficient," (A. H. Compton "X-rays and Electrons") are given in Table 665.

The first term in the brackets represents energy losses from "fluorescent," or "true," absorption; this first appears as energy of ionization of atoms and of photoelectrons. The ionized atoms then either emit characteristic X rays or use their energy for the photoelectric process; the quantitative relations between these are described in Table 660 under "X-ray Emission."

The second term is the energy lost by the X-ray beam by scattering. Except for the (usually small) amount of energy which goes into the production of "recoil electrons," it remains as X-ray energy which is simply redistributed as to direction of propagation, being radiated in all directions from the plate. The scattered radiation is of two parts, an "unmodified" (or "unshifted") part, and a "modified" (or "shifted") part. The former has the wave length of the original beam. The wave length of the modified part is longer ("Compton shift") than that of the original beam by an amount $\delta\lambda$ which varies with ϕ , the angle between the direction of the primary beam (of wave length λ), and the direction of that portion of the modified rays of wave length $\lambda + \delta\lambda$. The relation between $\delta\lambda$ and ϕ is $\delta\lambda$ (Angstrom units) = $0.02428(1 - \cos \phi)$.

TABLE 664.—X-Ray Absorption and Chemical Combination

The wave lengths of the critical absorption limits of an element depend, to a very small extent, on the chemical combination of the "absorbing" element. The K absorption limit for phosphorus follows for various chemical combinations: R stands for any one of several metals.

Wave lengths, λ , in Angstroms

| | λ | $\Delta\lambda$ | | λ | $\Delta\lambda$ |
|-------------------------------|-----------|-----------------|-------------------------------|-----------|-----------------|
| (RO) ₃ PO..... | 5.7507 | | (RN) ₃ PO..... | 5.7565 | 0.0058 |
| (RO) ₂ HPO..... | 5.7541 | 0.0034 | (RC) ₃ PS..... | 5.7632 | .0125 |
| (RO)H ₂ PO..... | 5.7575 | .0068 | RO(RC)(H)PO..... | 5.7581 | .0074 |
| (RO) ₂ (RC)PO..... | 5.7551 | .0044 | (RO) ₃ P..... | 5.7599 | .0092 |
| (RO)(RC) ₂ PO..... | 5.7591 | .0084 | (RC) ₃ P..... | 5.7676 | .0169 |
| (RC) ₃ PO..... | 5.7604 | .0097 | (RO)Cl ₂ P..... | 5.7602 | .0095 |
| (RC) ₃ POR..... | 5.7630 | .0123 | (RC) ₃ P,CuCl..... | 5.7645 | .0138 |
| (RN)(Cl) ₂ PO..... | 5.7588 | .0081 | (RO) ₃ P,CuCl..... | 5.7589 | .0082 |
| (RN)(RO)(Cl)PO..... | 5.7559 | .0052 | P (violet)..... | 5.7714 | .0207 |
| (RN)(RO) ₂ PO..... | 5.7512 | .0005 | P (black)..... | 5.7715 | .0208 |
| (RN) ₂ (RO)PO..... | 5.7541 | .0034 | P (white)..... | 5.7769 | .0262 |

There result some conclusions probably of general application: ($\Delta\lambda$) in its value for some particular compound, depends only on what atoms are directly attached to the absorbing atom (e.g., the phosphorus limit (RO)₃P does not depend on what metal is used for R). $\Delta\lambda$ depends on the *kind* of atom directly attached (compare (RO)₃P with (RC)₃P) and on the *number* of these atoms (compare (RO)₃P with (RO)₃PO). If any addition (any kind of atom) is made to a given set of atoms directly attached to the absorbing one, the limit is shifted toward a shorter λ (cf., (RC)₃P with (RC)₃PO). Further, the wave length for the element when uncombined is usually greater than when attached chemically to other atoms (true for all of 11 elements investigated except sulphur). A variation of wave length is also usually shown for allotropic modifications of an element.

MASS ABSORPTION COEFFICIENTS (μ/ρ)

| Atomic number, Element | Wave lengths in Angstroms | | | | | | | | | | | |
|------------------------------|---------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | 0.017 | 0.057 | 0.080 | 0.100 | 0.125 | 0.150 | 0.175 | 0.200 | 0.250 | 0.300 | 0.350 | 0.400 |
| 1 H | 0.117 | ... | ... | ... | 0.3 | 0.4 | 0.4 | 0.4 | 0.39 | 0.42 | 0.44 | 0.45 |
| 3 Li | ... | ... | ... | ... | ... | ... | ... | ... | ... | .172 | .188 | .208 |
| 6 C | .060 | ... | 0.140 | 0.146 | .152 | .160 | .162 | .170 | .184 | .197 | .216 | .240 |
| 7 N | ... | ... | ... | ... | ... | .163 | .171 | .177 | .193 | .224 | .251 | ... |
| 8 O | .059 | ... | ... | ... | .146 | .163 | .174 | .183 | .208 | .240 | .285 | .338 |
| 12 Mg | .057 | ... | ... | ... | .162 | .175 | .202 | .232 | .311 | .430 | .612 | .875 |
| 13 Al | .058 | 0.07 | .143 | .164 | .178 | .201 | .231 | .269 | .370 | .531 | .756 | 1.05 |
| 16 S | .058 | ... | .152 | .190 | .204 | .272 | .333 | .42 | .63 | .93 | 1.32 | 1.78 |
| 26 Fe | .058 | .08 | .232 | .265 | .399 | .572 | .79 | 1.07 | 1.93 | 3.18 | 4.94 | 7.17 |
| 27 Co | ... | ... | ... | ... | .42 | .60 | .84 | 1.17 | 2.12 | 3.52 | ... | ... |
| 28 Ni | .059 | ... | .261 | .328 | .475 | .68 | 1.00 | 1.40 | 2.50 | 4.10 | 6.22 | ... |
| 29 Cu | .057 | ... | .263 | .323 | .49 | .77 | 1.10 | 1.53 | 2.75 | 4.47 | 6.91 | 10.1 |
| 30 Zn | .057 | ... | .305 | .38 | .60 | .92 | 1.28 | 1.77 | 3.15 | 5.10 | 7.90 | 11.6 |
| 42 Mo | ... | ... | ... | ... | 1.35 | 1.96 | 2.83 | 4.02 | 7.42 | 12.7 | 19.1 | 26.7 |
| 47 Ag | .056 | ... | .72 | 1.13 | 1.67 | 2.63 | 3.76 | 5.75 | 11.1 | 18.0 | 27.0 | 38.4 |
| 50 Sn | .056 | .18 | .78 | 1.16 | 2.00 | 3.00 | 4.35 | 6.30 | 12.1 | ... | ... | ... |
| 74 W | ... | ... | 2.35 | 3.40 | 5.42 | 8.10 | 2.92 | 3.20 | 5.60 | 8.60 | 13.2 | 19.8 |
| 78 Pt | .068 | ... | 2.46 | 3.69 | 5.70 | 4.30 | 3.04 | 4.16 | 7.32 | 11.5 | 17.0 | 24.5 |
| 79 Au | ... | ... | 2.39 | 3.64 | 5.37 | 3.60 | 3.09 | 4.28 | 7.65 | ... | ... | ... |
| 82 Pb | .068 | .50 | 2.47 | 3.78 | 4.32 | 2.0 | 2.93 | 4.62 | 8.46 | 13.9 | 21.9 | 32.7 |
| 83 Bi | .070 | ... | 2.44 | 3.78 | 3.8 | 2.44 | 3.59 | 5.10 | 9.3 | 14.8 | 22.8 | ... |
| 90 Th | .081 | ... | ... | 3.88 | 1.85 | 2.69 | 2.87 | 5.47 | 9.67 | ... | ... | ... |
| ↓ K limit | | | | | | | | | | | | |
| | 0.500 | 0.600 | 0.700 | 0.800 | 0.900 | 1.00 | 1.10 | 1.32 | 1.40 | 1.76 | 2.25 | |
| 1 H | 0.45 | 0.44 | 0.51 | 0.57 | 0.63 | ... | ... | ... | ... | ... | ... | |
| 3 Li | .245 | .306 | .403 | ... | ... | ... | ... | ... | ... | ... | ... | |
| 6 C | .310 | .412 | .540 | .72 | 1.00 | 1.30 | 2.1 | 3.5 | 4.0 | 7.8 | 15 | |
| 8 O | .498 | .746 | 1.10 | 1.55 | 2.12 | 2.87 | ... | ... | ... | ... | ... | |
| 12 Mg | 1.56 | ... | ... | ... | ... | ... | 16 | ... | 35 | 63 | 126 | |
| 13 Al | 1.91 | 3.18 | 5.00 | 7.50 | 10.3 | 13.8 | 20.0 | 31.5 | 38 | 74 | 140 | |
| 16 S | ... | 5.9 | 9.5 | ... | ... | ... | ... | ... | ... | ... | ... | |
| 26 Fe | 14.3 | 23.3 | 36.3 | 51.7 | 69.6 | 95 | 126 | 220 | 270 | 60 | 104 | |
| 28 Ni | 18 | 30 | 45.0 | ... | 82 | 118 | 159 | 253 | 288 | 69 | 135 | |
| 29 Cu | 18.8 | 31.6 | 49.2 | ... | 97 | 133 | 181 | 265 | 40 | 75 | 143 | |
| 30 Zn | 22.2 | 37.2 | 57.0 | ... | 107 | 152 | 188 | 40 | 48 | 91 | 170 | |
| 42 Mo | 48.6 | 80.7 | 18.8 | 27.2 | 37.5 | 51 | ... | ... | ... | ... | ... | |
| 46 Pd | 60 | 17.0 | ... | ... | ... | ... | ... | ... | ... | ... | ... | |
| 47 Ag | 11.0 | 18.7 | 25.6 | ... | 57 | 75 | 92 | 155 | 176 | 320 | 590 | |
| 50 Sn | 13.1 | 21.6 | 31 | ... | 65 | 87 | 115 | 198 | 223 | 400 | 725 | |
| 74 W | 38.0 | 65.0 | ... | ... | ... | ... | ... | 113 | 141 | ... | ... | |
| 78 Pt | 45.5 | 75.5 | 112 | ... | 158 | 165 | 92 | 145 | 161 | 282 | 520 | |
| 79 Au | 51 | 77 | 116 | ... | 154 | 110 | 98 | 148 | 173 | 300 | 500 | |
| 82 Pb | 59.3 | 91 | 133 | ... | 140 | 77 | 100 | 166 | 185 | 340 | ... | |
| ↓ L limit | | | | | | | | | | | | |
| → L limit | | | | | | | | | | | | |

PHOTOGRAPHIC EFFECTS OF X RAYS

X rays affect a photographic plate (or film) in much the same way as does light, except that that part, D_x , of the photographic density which is due to the radiation depends on radiation intensity, I , and the time of exposure, t , in a simpler way. The relation for monochromatic X rays is

$$D_x \equiv D - D_0 = k(1 - e^{-aIt}), \quad 0 < D < 4 \quad (1)$$

where e is the base of natural logarithms, and k and a are constant for a given plate and given X-ray wave length. D and D_0 are the photographic densities of the exposed and unexposed parts of the plate. These densities are measurable with a photometer, photographic density being defined as the common logarithm of the reciprocal of the transmission T , i.e., density $\equiv \log_{10}(1/T)$, where T is the ratio (transmitted light)/(incident light) for a beam of light normal to the developed plate.

The limits of applicability of formula (1) probably depend on the characteristics of the plate used and on the development, as well as on the wave length of the X rays. Experimental tests indicate that the relation holds within a few per cent up to a density of at least 4, for X-ray plates, if the plate is fully developed and if the wave length of the X rays is between 0.4 and 1.1 Angstroms. Effects due to intermittency, and to the failure of the reciprocity law are negligible in the X-ray region.

SMITHSONIAN TABLES

NOTE: The phenomena of electron emission, photoelectric effect and contact (Volta) potential treated in the following tables are extremely sensitive to surface condition of the metal. The most consistent observations have been made in high vacua with freshly cut metal surfaces. (See Dushman, Rev. Mod. Phys., 2, 381, 1930.)

TABLE 667.—Electron Emission from Hot Solid Elementary Substances

(Most of the following is taken from Dushman, loc. cit., 1930.)

Among the free electrons within a metal some may have velocities great enough to escape the surface attraction. The number reaching the surface with velocities above this critical velocity $= N = (RT/2\pi M)^{1/2} e^{-w/rt}$ where N = no. of electrons/cm³ of metal, R the gas constant (83.14×10^6 erg-dyne), T , the absolute temperature, M , the atomic weight of an electron (.000545, $O = 16$), w the work done when a gram-molecule of electrons (6.06×10^{23} electrons or 96,500 coulombs) escape. It seems probable that this work is done against the attraction of the electron's own induced image in the surface of the conductor. When a sufficiently high + field is applied to escaping electrons so that none return to the conductor, then the saturation current has been found to follow the equation

$$i = a \sqrt{T} e^{-b_0/T} \text{ (Richardson's equation)}$$

assuming N and W constant with T . This is equivalent to the equation for N just given. The equation

$$I = AT^2 e^{-b_0/T} \text{ (Laue's equation)}$$

is just as valid theoretically and Dushman (Phys. Rev., 21, 623, 1923) considers A should be a universal constant (60.2 amp./cm²/deg.²/and b_0 dependent upon the emitter. The data is not accurate enough to distinguish between the two formulas. b or b_0 is a measure of the latent heat of evaporation of the electrons, i. e., the energy needed to get the electrons through the surface. While used in °K. in the above equation, it is customary to express it in volts by the relation $b_0 k = \phi_0 e$ where k = Boltzmann's constant, e , the electronic charge, and ϕ_0 is known as the work function, whence

$$\phi_0 = 8.62 \times 10^{-5} b_0 \text{ (volts)}$$

The experimental values of A do not seem to be independent of the substance.

| Element | $b \times 10^{-4}$ | A | $b_0 \times 10^{-4}$ | ϕ_0 | I_T | T | |
|---------|--------------------|-------------------|----------------------|----------|-----------------------|------|----------------|
| Mo | 5.26 | 60.2 | 5.15 | 4.44 | 1.6×10^{-3} | 2000 | Dushman, 1925 |
| Pt | ... | 1.7×10^4 | 7.25 | 6.27 | 9.2×10^{-10} | 1600 | DuBridge, 1928 |
| Ta | 4.98 | 60.2 | 4.72 | 4.07 | 1.38×10^{-2} | 2000 | Dushman, 1925 |
| Tn | ... | 60.2 | 3.89 | 3.35 | 4×10^{-3} | 1600 | Zwicker, 1925 |
| W | ... | 60.2 | 5.240 | 4.52 | 1×10^{-3} | 2000 | Average |
| Zr | ... | 330 | 4.79 | 4.13 | 8×10^{-5} | 1600 | Zwicker, 1929 |

(Above table of best authenticated values is from Dushman, loc. cit., p. 394, 1930. His table contains values for C, Ca, Cs, Hf, Ni. See also I.C.T.)

TABLE 668.—Electron Emission from Thorium-Coated Filaments (Monomolecular), $f(\theta)$

Values given for Dushman with W filaments coated with monomolecular films of thorium. $\theta = (b_0 - b_w)/(b_{Th} - b_w)$ where b_0 , b_{Th} and b_w represent values of b_0 in the emission equation for partly covered, completely covered, and pure tungsten surface.

I_0 and ϕ_0 refer to 1900°.

| | | | | |
|-----------------|------------------|---------------------|--------------------|----------------------|
| $\theta = 1.00$ | $A_\theta = 3.0$ | $b_\theta = 30.500$ | $I_\theta = 1.166$ | $\Phi_\theta = 2.63$ |
| 0.95 | 1.50 | 31.460 | 0.349 | 2.71 |
| .72 | 3.74 | 36.570 | .0594 | 3.15 |
| .43 | 10.86 | 42.840 | .0004 | 3.69 |
| .25 | 15.81 | 47.050 | .0010 | 4.06 |

TABLE 669.—Emission Current, I , Emission Efficiency I/W , Diffusion, D , I_0 for Zero Field, Completely Activated Surface, Th on W

| T | I (amp./cm ²) | I/W (amp./watt) | D (cm ² /sec.) | E (atoms/sec./cm ²) | I_0 |
|-------|-----------------------------|-----------------------|-----------------------------|-----------------------------------|----------------------|
| 1000° | 1.73×10^{-7} | 2.87×10^{-7} | | | 8.0×10^{-9} |
| 1200 | 3.95×10^{-5} | 2.38×10^{-5} | | | 5.3×10^{-6} |
| 1400 | 2.03×10^{-3} | 5.30×10^{-4} | 2.4×10^{-15} | 0.445 | 5.4×10^{-4} |
| 1500 | 1.00×10^{-2} | 1.81×10^{-3} | 2.2×10^{-14} | 58.5 | 3.5×10^{-3} |
| 1600 | 4.06×10^{-2} | 5.24×10^{-3} | 1.6×10^{-13} | 4.2×10^3 | 1.8×10^{-2} |
| 1700 | 1.40×10^{-1} | 1.32×10^{-2} | 9.2×10^{-12} | 1.8×10^5 | 7.9×10^{-3} |
| 1800 | $4.28 \times "$ | 3.09×10^{-2} | 4.3×10^{-12} | 5.2×10^5 | 2.9×10^{-1} |
| 1900 | 1.164 | 6.24×10^{-2} | 1.7×10^{-11} | 1.0×10^8 | 9.5×10^{-1} |
| 2000 | 2.864 | 1.19×10^{-1} | 5.9×10^{-11} | 1.5×10^9 | 2.8 |

TABLE 670.—Electron Emission from Other Than Th-Coated Filaments

Monatomic films of other rare earths (and alkaline earth metals absorbed on tungsten and molybdenum). D cm²/sec.⁻¹ for $T = 2000$. Q_D , heat of diffusion (g cal./g-atom), E , the rate of evaporation in atoms/cm²sec. at 2000° K. A , b_0 refer to formulas on page 547.

| Emitter | A | b_0 | $D \times 10^{11}$ | Q_D | $E \times 10^9$ |
|-------------|-----|---------|--------------------|---------|-----------------|
| Ce-W | 8.0 | 31,500. | 95. | 83,000 | 1450 |
| La-W | 8.0 | 31,500. | | | |
| U-W | 3.2 | 33,000. | 1.3 | 100,000 | > Th |
| Yt-W | 7.0 | 31,300. | 324. | 78,000 | 68. |
| Zr-W | 5.0 | 36,500. | 1820. | 62,000 | |
| Th-W | 3.0 | 30,500. | 5.9 | 94,000 | 1.53 |
| Th-Mo | 1.5 | 30,000. | 102000. | 52,000 | 5400. |

TABLE 671.—Photoelectric Effect

A negatively charged body loses its charge under the influence of ultra-violet light because of the escape of negative electrons freed by the absorption of the energy of the light. The light must have a wave length shorter than some limiting value λ_0 characteristic of the metal. The emission of these electrons, unlike that from hot bodies, is independent of the temperature. The relation between the maximum velocity v of the expelled electron and the frequency ν of the light is $(\frac{1}{2})mv^2 = h\nu - P$ (Einstein's equation) where h is Planck's constant (6.58×10^{-27} erg. sec.); $h\nu$ sometimes taken as the energy of a "quanta," P , the work which must be done by the electron in overcoming surface forces. $(\frac{1}{2})mv^2$ is the maximum kinetic energy the electron may have after escape. Richardson identifies the P of Einstein's formula with the ϕ of electron emission of the preceding table. The minimum frequency ν_0 (corresponding to maximum wave length λ_0) at which the photoelectric effect can be observed is determined by $h\nu = P$. P applies to a single electron, whereas ϕ applies to one coulomb (6.062×10^{23} electrons); therefore $\phi = NP = .00399\nu_0$ ergs. $\phi = (12.4 \times 10^{-5})\lambda_0$ volts. See Millikan, Proc. Nat. Acad. 2, 78, 1916; Phys. Rev. 7, 355, 1916; 4, 73, 1914; Hennings, Phys. Rev. 4, 228, 1914.

TABLE 672.—Contact (volta) Potentials

| | Pt | Fe | Cu | Au | Ag | Al | Mg | Zn | Pb | Sn |
|--------------------------------|-------|--------------|-------|-------|-------|------|------|-------|------|-------|
| SiO ₂ ... | +2.22 | +1.99 | +1.60 | +1.60 | +1.42 | +.93 | +.93 | +.45 | +.16 | -.30 |
| Glass .. | +1.15 | +1.15 | +0.58 | +0.58 | +0.58 | +.14 | +.14 | -.29 | -.60 | -1.14 |
| | | | | Cu | Cr | Ta | Mo | Ni | | |
| W | | | | +.08 | +.11 | -.38 | -.21 | -.17 | | |
| SiO ₂ , Glass | | Polodnik, Z. | Phys. | | | 66, | 619, | 1930. | | |
| W | | Kosters, " | " | | | 66, | 807, | 1930. | | |

(This Table Supplements Table 677.)

| | | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 3 Li | 3.00 | 13 Al | 2.70 | 25 Mn | 2.95† | 36 Kr | 2.35* | 54 Xe | 2.70* |
| 4 Gl | 2.30 | 14 Si | 2.35 | 26 Fe | 2.80 | 37 Rb | 4.50 | 55 Cs | 4.75 |
| 6 C | 1.54 | 16 S | 2.05 | 27 Co | 2.75 | 38 Sr | 3.90 | 56 Ba | 4.20 |
| 7 N | 1.30 | 17 Cl | 2.10 | 28 Ni | 2.70 | 47 Ag | 3.55 | 81 Tl | 4.50 |
| 8 O | 1.30 | 18 A | 2.05* | 29 Cu | 2.75 | 48 Cd | 3.20 | 82 Pb | 3.80 |
| 9 F | 1.35 | 19 K | 4.15 | 30 Zn | 2.65 | 50 Sn | 2.80 | 83 Bi | 2.96 |
| 10 Ne | 1.30* | 20 Ca | 3.40 | 33 As | 2.52 | 51 Sb | 2.80 | | |
| 11 Na | 3.55 | 22 Ti | 2.80 | 34 Se | 2.35 | 52 Te | 2.65 | | |
| 12 Mg | 2.85 | 24 Cr | 2.80† | 35 Br | 2.38 | 53 I | 2.80 | | |

* Outer electron shell.

† Cr, "electronegative," 2.35; Mn., ditto, 2.35.

Broughall (Phil. Mag. 41, p. 872, 1921) computes in the same units from Van der Waal's constant "b" the diameters of He, N, A, Kr, and X as 2.3, 2.6, 2.9, 3.1, and 3.4. These inert elements correspond to Langmuir's completely filled successive electron shells. The corresponding atomic numbers are 2, 10, 18, 36 and 54. For Langmuir's theory see J. Am. Ch. Soc., p. 868, 1919, Science 54, p. 59, 1921.

TABLE 672.—Contact (Volta) Potentials

There has been considerable controversy over the reality and nature of the contact differences of potential between two metals. At present, due to the studies of Langmuir, there is a decided tendency to believe that this Volta difference of potential is an intrinsic property of metals closely allied to the phenomena just given in Tables 667 to 671 and that the discrepancies among different observers have been caused by the same disturbing surface conditions. The following values of the contact potentials with silver and the relative photo-sensitiveness of a few of the metals are from Henning, *Phys. Rev.* 4, 228, 1914. The values are for freshly cut surfaces in vacuo. Freshly cut surfaces are more electro-positive and grow more electro-negative with age. That the observed initial velocities of emission of electrons from freshly cut surfaces are nearly the same for all metals suggests that the more electro-positive a metal is the greater the actual velocity of emission of electrons from its surface.

| | Ag | Cu | Fe | Brass | Sn | Zn | Al | Mg |
|-----------------------------------|----|-----|-----|-------|-----|-----|-----|------|
| Contact potential with Ag..... | 0 | .05 | .10 | .21 | .27 | .50 | .99 | 1.42 |
| Relative photo-sensitiveness..... | 50 | 60 | 65 | 45 | 70 | 80 | 500 | 1000 |

From the equation $w = RT \log(N_A/N_B)$, where w is the work necessary per gram-molecule when electrons pass through a surface barrier separating concentrations N_A and N_B of electrons, it can be shown (Langmuir, *Tr. Am. Electro. Soc.* 29, 142, 1916, *et seq.*) that the Volta potential difference between two metals should be

$$v_1 - v_2 = \frac{I}{F} \{w_2 - w_1 + RT \log(N_A/N_B)\} = \frac{w_2 - w_1}{F} = \phi_2 - \phi_1$$

(see Table 671 for significance of symbols), since the number of free electrons in different metals per unit volume is so nearly the same that $RT \log(N_A/N_B)$ may be neglected. The contact potentials may thus be calculated from photo-electric phenomena (see Table 671 for references). They are independent of the temperature. The following table gives a summary of values of ϕ in volts obtained from the various phenomena where an electron is torn from the attraction of some surface. In the case of ionization potentials the work necessary to take an electron from an atom of metal vapor is only approximately equal to that needed to separate it from a solid metal surface.

TABLE 673.—(a) The Electron Affinity of the Elements, in Volts

| Metal. | Contact. (Henning.) | Thermionic. (Langmuir.) | Photo- electric and contact. (Millikan.) | Photo- electric. (Richardson) | Miscel- laneous. | Single- line spectra. | Adjusted mean. |
|-----------------|------------------------|----------------------------|---|-------------------------------------|---------------------|-----------------------------|-------------------|
| Tungsten..... | — | 4.52 | — | — | — | — | 4.52 |
| Platinum..... | — | — | — | 4.3 | 4.45 | — | 4.4 ² |
| Tantalum..... | — | 4.31 | — | — | — | — | 4.3 |
| Molybdenum..... | — | 4.31 | — | — | — | — | 4.3 |
| Carbon..... | — | 4.14 | — | — | — | — | 4.1 |
| Silver..... | 4.05 | — | — | — | — | — | 4.1 |
| Copper..... | (4.0) | — | — | 4.1 | — | — | 4.0 |
| Bismuth..... | — | — | — | 3.7 | — | — | 3.7 |
| Tin..... | 3.78 | — | — | 3.5 | — | — | 3.8 |
| Iron..... | 3.86 | 3.2 ² | — | — | — | — | 3.7 |
| Zinc..... | 3.46 | — | — | 3.4 | — | 4.04 | 3.4 |
| Thorium..... | — | 3.36 | — | — | — | — | 3.4 |
| Aluminum..... | 3.06 | — | — | 2.8 | — | — | 3.0 |
| Magnesium..... | 2.63 | — | — | 3.2 | — | 4.35 | 2.7 |
| Titanium..... | — | 2.4 ² | — | — | — | — | 2.4 |
| Lithium..... | — | — | 2.35 | — | — | 1.85 | 2.35 |
| Sodium..... | — | — | 1.82 | 2.1 | — | 2.11 | 1.82 |

(b) It should not be assumed that all the emf of an electrolytic cell is contact emf. Its emf varies with the electrolyte, whereas the contact emf is an intrinsic property of a metal. There must be an emf between the two electrodes of such a cell dependent upon the concentration of the electrolyte used. The following table gives in its first line the electrode potential e_h of the corresponding metals (in solutions of their salts containing normal ion concentration) on assumption of no contact emf at the junction of the metals. The second line, $\phi - e_h = 3.7$ volts, gives an idea of the electrode potentials (arbitrary zero) exclusive of contact emf.

| Metal | Ag | Cu | Bi | Sn | Fe | Zn | Mg | Li | Na |
|--------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| e_h | +0.80 | +0.34 | +0.20 | -0.10 | -0.43 | -0.76 | -1.55 | -3.03 | -2.73 |
| $\phi - e_h = 3.7$ | -0.40 | +0.04 | +0.20 | -0.20 | -0.43 | -0.40 | -0.55 | -1.05 | -0.85 |

TABLE 674.—Molecular Velocities

The probability of a molecular velocity x is $(4/\sqrt{\pi})x^2e^{-x^2}$, the most probable velocity being taken as unity. The number of molecules at any instant of speed greater than c is $2N(hm/\pi)^{1/2} \left\{ \int_c^\infty e^{-hmc^2} dc + ce^{-hmc^2} \right\}$ (see table), where N is the total number of molecules. The mean velocity G (sq. rt. of mean sq.) is proportional to the mean kinetic energy and the pressure which the molecules exert on the walls of the vessel and is equal to $15,800 \sqrt{T/m}$ cm/sec, where T is the absolute temperature and m the molecular weight. The most probable velocity is denoted by W , the average arithmetical velocity by Ω .

$$G = W \sqrt{3/2} = 1.225W; \quad \Omega = W \sqrt{4/\pi} = 1.128W; \quad G = \Omega \sqrt{3\pi/8} = 1.086\Omega.$$

The number of molecules striking unit area of inclosing wall is $(1/4)N\Omega$ (Meyer's equation), where N is the number of molecules per unit volume; the mass of gas striking is $(1/4)\rho\Omega$ where ρ is the density of the gas. For air at normal pressure and room temperature (20°C) this is about $14 \text{ g/cm}^2 \text{ sec}$. See Langmuir, Phys. Rev. 2, 1013 (vapor pressure of W) and J. Amer. Ch. Soc. 37, 1915 (Chemical Reactions at Low Pressures), for fertile applications of these latter equations. The following table is based on Kinetic Theory of Gases, Dushman, Gen. Elec. Rev. 18, 1915, and Jeans, Dynamical Theory of Gases, 1916.

| Gas. | Molecular weight. | Sq. rt. mean sq. $G \times 10^{-2}$ cm/sec. | | | Arithmetical average velocity, $\Omega \times 10^{-2}$ cm/sec. | | | | | | | |
|----------------------|-------------------|--|------|------|---|------|------|------|-------|-------|-------|-------|
| | | 273° | 293° | 373° | 223° | 273° | 293° | 373° | 1000° | 1500° | 2000° | 6000° |
| Air..... | 28.96 | 485 | 502 | 567 | 404 | 447 | 463 | 522 | 855 | 1047 | 1200 | 2094 |
| Ammonia..... | 17.02 | 633 | 655 | 740 | 527 | 583 | 604 | 681 | 1115 | 1367 | 1577 | 2734 |
| Argon..... | 39.88 | 413 | 428 | 483 | 344 | 381 | 395 | 445 | 729 | 892 | 1030 | 1784 |
| Carbon monoxide..... | 28.00 | 403 | 511 | 576 | 410 | 454 | 471 | 531 | 870 | 1065 | 1230 | 2130 |
| Carbon dioxide..... | 44.00 | 393 | 408 | 459 | 327 | 362 | 376 | 434 | 694 | 850 | 981 | 1700 |
| Helium..... | 4.00 | 1311 | 1358 | 1533 | 1002 | 1208 | 1252 | 1412 | 2300 | 2840 | 3270 | 5680 |
| Hydrogen..... | 2.01 | 1838 | 1904 | 2140 | 1534 | 1696 | 1755 | 1980 | 3241 | 3970 | 4583 | 7940 |
| Krypton..... | 82.92 | 286 | 296 | 335 | 238 | 263 | 272 | 308 | 502 | 618 | 712 | 1236 |
| Mercury..... | 200.6 | 184 | 191 | 215 | 154 | 170 | 176 | 199 | 325 | 398 | 459 | 796 |
| Molybdenum..... | 96.0 | — | — | — | — | — | — | — | 469 | 575 | 664 | 1150 |
| Neon..... | 20.2 | 584 | 605 | 683 | 486 | 538 | 557 | 629 | 1030 | 1260 | 1460 | 2520 |
| Nitrogen..... | 28.02 | 403 | 511 | 577 | 410 | 454 | 471 | 531 | 860 | 1064 | 1220 | 2128 |
| Oxygen..... | 32.00 | 461 | 478 | 530 | 384 | 425 | 440 | 497 | 813 | 996 | 1150 | 1992 |
| Tungsten..... | 184.0 | — | — | — | — | — | — | — | 339 | 416 | 480 | 832 |
| Water vapor..... | 18.02 | 615 | 637 | 720 | 512 | 566 | 587 | 662 | 1084 | 1317 | 1533 | 2634 |
| Xenon..... | 130.2 | 228 | 236 | 267 | 190 | 210 | 218 | 246 | 400 | 493 | 570 | 986 |

Free electron, molecular weight = $1/1835$ when $H = 1$; $G = 1.114 \times 10^7$ at 0°C and $\Omega = 1.026 \times 10^7$ at 0°C .

TABLE 675.—Molecular Free Paths, Collision Frequencies, and Diameters

The following table gives the average free path L derived from Boltzmann's formula $\mu/(.3502\rho\Omega)$, μ being the viscosity, ρ the density, and from Meyer's formula $\mu/(.3007\rho\Omega)$. Experimental values (Verh. d. Phys. Ges. 14, 596, 1912; 15, 373, 1913) agree better with Meyer's values, although many prefer Boltzmann's formula. As the pressure decreases, the free path increases, at one bar (ordinary incandescent lamp) becoming 5 to 10 cm. The diameters may be determined from L by Sutherland's equation $\{1.02/\sqrt{2\pi NL}(1+C/T)\}^{1/2}$, N being the number of molecules per unit vol. and C Sutherland's constant; from van der Waal's b , $\{3b/2NV\pi\}^{1/2}$; from the heat conductivity k , the specific heat at constant volume c_v , $\{146\rho Gc_v/Nk\}^{1/2}$ (Laby and Kaye); a superior limit from the maximum density in solid and liquid states (Jeans, Sutherland, 1916) and an inferior limit from the dielectric constant D , $\{(D-1)/\pi N\}^{1/2}$, or the index of refraction n , $\{(n^2-1)/2\pi N\}^{1/2}$. The table is derived principally from Dushman, l.c.

| Gas. | $L \times 10^6$ (cm) Average free path.* | | | Collision frequency. $\frac{\Omega}{L}$ $\times 10^{-6}$ 20°C^* | $10^8 \times$ Molecular diameters (cm): | | | | |
|----------------------|---|---------------------|-----------------------------------|---|---|----------------------------------|---------------------------------------|---------------------------|--------------------|
| | Boltzmann. | | Meyer. 20°C | | From L (vis- cosity) μ | From van der Waal's b | From heat conduct- ivity k | Limiting | |
| | 0°C | 20°C | | | | | | Max. density ρ | Min. D or n |
| Ammonia..... | 5.02 | 6.60 | 5.83 | 9150 | 2.97 | 3.08 | — | — | — |
| Argon..... | 8.98 | 9.88 | 8.73 | 4000 | 2.88 | 2.94 | 2.86 | 2.87 | 2.66 |
| Carbon monoxide..... | 8.46 | 9.23 | 8.16 | 5100 | 3.19 | 3.12 | — | 3.27 | 2.74 |
| Carbon dioxide..... | 5.56 | 6.15 | 5.44 | 6120 | 3.34 | 3.23 | 3.40 | 3.35 | 2.90 |
| Helium..... | 25.25 | 27.45 | 33.10 | 4540 | 1.60 | 2.65 | 2.30 | 1.98 | 1.02 |
| Hydrogen..... | 16.00 | 17.44 | 15.40 | 10060 | 2.40 | 2.34 | 2.32 | 2.40 | 2.17 |
| Krypton..... | 9.5 | — | — | — | — | (3.69) | 3.14 | 3.35 | (2.70) |
| Mercury..... | — | (14.70) | (13.0) | — | — | 3.01 | — | — | — |
| Nitrogen..... | 8.50 | 9.29 | 8.21 | 5070 | 3.15 | 3.15 | 3.53 | 3.23 | 2.95 |
| Oxygen..... | 9.05 | 9.93 | 8.78 | 4430 | 2.98 | 2.92 | — | 2.90 | 2.71 |
| Xenon..... | 5.6 | — | — | — | — | 4.02 | 3.42 | 3.55 | (3.18) |

* Pressure = 10^6 bars = 10^6 dynes \div cm^2 = 75 cm Hg.

TABLE 676.—Cross-Sections and Lengths of Some Organic Molecules

According to Langmuir (J. Am. Ch. Soc. 38, 2221, 1916) in solids and liquids every atom is chemically combined to adjacent atoms. In most inorganic substances the identity of the molecule is generally lost, but in organic compounds a more permanent existence of the molecule probably occurs. When oil spreads over water evidence points to a layer a molecule thick and that the molecules are not spheres. Were they spheres and an attraction existed between them and the water, they would be dissolved instead of spreading over the surface. The presence of the $-\text{COOH}$, $-\text{CO}$ or $-\text{OH}$ groups generally renders an organic substance soluble in water, whereas the hydrocarbon chain decreases the solubility. When an oil is placed on water the $-\text{COOH}$ groups are attracted to the water and the hydrocarbon chains repelled but attracted to each other. The process leads the oil over the surface until all the $-\text{COOH}$ groups are in contact if possible. Pure hydrocarbon oils will not spread over water. Benzene will not mix with water. When a limited amount of oil is present the spreading ceases when all the water-attracted groups are in contact with water. If weight w of oil spreads over water surface A , the area covered by each molecule is AM/wN where M is the molecular weight of the oil ($O = 16$), N , Avogadro's constant. The vertical length of a molecule $l = M/apN = W/pA$ where p is the oil density and a the horizontal area of the molecule.

| Substance. | Cross section in $\text{cm}^2 \times 10^{16}$ | l in cm (length) $\times 10^8$ | Substance. | Cross section in $\text{cm}^2 \times 10^{16}$ | l in cm (length) $\times 10^8$ |
|--|---|----------------------------------|--|---|----------------------------------|
| Palmitic acid $\text{C}_{15}\text{H}_{31}\text{COOH}$ | 24 | 19.6 | Cetyl alcohol $\text{C}_{16}\text{H}_{33}\text{OH}$ | 21 | 21.9 |
| Stearic acid $\text{C}_{17}\text{H}_{35}\text{COOH}$ | 24 | 21.8 | Myrcyl alcohol $\text{C}_{30}\text{H}_{61}\text{OH}$ | 29 | 35.2 |
| Cerotic acid $\text{C}_{22}\text{H}_{45}\text{COOH}$ | 25 | 29.0 | Cetyl palmitate $\text{C}_{15}\text{H}_{31}\text{COOC}_{16}\text{H}_{33}$ | 21 | 44.0 |
| Oleic acid $\text{C}_{17}\text{H}_{33}\text{COOH}$ | 48 | 10.8 | Tristearin $(\text{C}_{18}\text{H}_{35}\text{O}_2)_3\text{C}_3\text{H}_5$ | 69 | 23.7 |
| Linoleic acid $\text{C}_{17}\text{H}_{31}\text{COOH}$ | 47 | 10.7 | Trielaidin $(\text{C}_{18}\text{H}_{33}\text{O}_2)_3\text{C}_3\text{H}_5$ | 137 | 11.9 |
| Linolenic acid $\text{C}_{17}\text{H}_{29}\text{COOH}$ | 66 | 7.6 | Triolein $(\text{C}_{18}\text{H}_{33}\text{O}_2)_3\text{C}_3\text{H}_5$ | 145 | 11.2 |
| Ricinoleic acid $\text{C}_{17}\text{H}_{33}(\text{OH})\text{COOH}$ | 90 | 5.8 | Castor oil $(\text{C}_{17}\text{H}_{33}(\text{OH})\text{COO})_3\text{C}_3\text{H}_5$ | 280 | 5.7 |
| | | | Linseed oil $(\text{C}_{17}\text{H}_{31}\text{COO})_3\text{C}_3\text{H}_5$ | 143 | 11.0 |

TABLE 677.—Size of Diffracting Units in Crystals ¶

The use of crystals for the analysis of X-rays leads to estimates of the relative sizes of molecular magnitudes. The diffraction phenomenon is here not a surface one, as with gratings, but one of interference of radiations reflected from the regularly spaced atomic units in the crystals, the units fitting into the lattice framework of the crystal. In cubical crystals {100} this framework is built of three mutually perpendicular equidistant planes whose distance apart in crystallographic parlance is d_{100} . This method of analysis from the nature of the diffraction pattern leads also to a knowledge of the structure of the various atoms of the crystal. See Bragg and Bragg, X-rays and Crystal Structure, 1918.

| Crystal. | Elementary diffracting element. | Side of cube. | Molecules or atoms in unit cube. |
|------------------------|---------------------------------|--------------------------|----------------------------------|
| KCl..... | Face-centered cube * | 6.28×10^{-8} cm | 4 molecules |
| NaCl..... | " " " " † | 5.628×10^{-8} | " |
| ZnS..... | " " " " ‡ | 5.43×10^{-8} | " |
| CaF ₂ | " " " " § | 5.46×10^{-8} | " |
| FeS ₂ | " " " " § | 5.38×10^{-8} | " |
| Fe..... | Body-centered cube | 2.86×10^{-8} | 2 atoms |
| Al..... | Face-centered cube | 4.05×10^{-8} | 4 " |
| Na..... | Body-centered cube | 4.30×10^{-8} | 2 " |
| Ni..... | " " " " | 2.76×10^{-8} | 2 " |
| "..... | Face-centered cube | 3.52×10^{-8} | 4 " |

* Each atom is so nearly equal in diffracting power (atomic weight) in KCl that the apparent unit diffracting element is a cube (simple) of $\frac{1}{2}$ this size. † Elementary body-centered cube. — atom at each corner, one in center; e.g., Fe, Ni (in part), Na, Li. ‡ Elementary face-centered cube, — atom at each corner, one in center of each face; e.g., Cu, Ag, Au, Pb, Al, Ni (in part), etc. Simple cubic lattice, — atom in each corner. Double face-centered cubic or diamond lattice — C (diamond); Si, Sb, Bi, As, Te.

† Diamond lattice. ‡ Cubic-holohedral. § Cubic-pyritohedral.

Metals taken from Hull, Phys. Rev. 10, p. 661, 1917

¶ See page 543 for best values of calcite and rock-salt grating spaces.

Note: — (Hull, Science 52, 227, 1920). Ca, face-centered cube, side 5.56 \AA , each atom 12 neighbors 3.93 \AA distant. Ti, centered cube, cf. Fe, side 3.14 \AA , 8 neighbors 2.72 \AA . Zn, 6 nearest neighbors in own plane, 2.67 \AA , 3 above, 3 below, 2.92 \AA . Cd, cf. Zn, 2.98 \AA , 3.30 \AA . In, face-centered tetragonal, 4 nearest 3.24 \AA , 4 above, 4 below, 3.33 \AA . Ru, cf. Zn, 2.69 \AA , 2.61 \AA . Pd, face-centered cube, side 3.92 \AA , 12 neighbors. 2.77 \AA . Ta, centered cube, side 3.27 \AA , 8 neighbors 2.83 \AA . Ir, face-centered cube, side 3.80 \AA , 12 neighbors, 2.69 \AA ($A = 10^{-8} \text{ cm}$).

Note: — (Bragg, Phil. Mag. 40, 169, 1920). Crystals empirically considered as tangent spheres of diameter in table, atom at center of sphere. When lattice known allows estimation of dimensions of crystal unit. Table foot of page 548 (atomic numbers, elements, diameter in Angstroms, 10^{-8} cm).

IONIC MOBILITIES AND DIFFUSIONS

The process of ionization is the removal of an electron from a neutral molecule, the molecule thus acquiring a resultant + charge and becoming a + ion. The negative carriers in all gases at high pressures, except inert gases, consist for the most part of carriers with approximately the same mobilities as the + ions. The negative electrons must, therefore, change initially to ions by union with neutral molecules.

The mobility, U , of an ion is its velocity in cm/sec. for an electrical field of one volt per cm. The rates of diffusion, D , are given in cm^2/sec . $U = DP/N\epsilon$, where P is the pressure, N , the number of molecules per unit volume of a gas and ϵ the electronic charge.

Nature of the gas and the mobilities: (1) The mobilities are approximately proportional to the inverse sq. rts. of the molecular weights of the permanent gases; better yet when the proportionality is divided by the 3th root of the dielectric constant minus unity; (2) The ratio $U + / U -$ seems to be greater than unity in all the more electro-negative gases.

Mobilities of Gaseous Mixtures: Three types: (1) Inert gases have high mobilities; small traces of electro-negative gases make values normal. (2) Mixed gases: lowering of mobilities is greater than would be expected from simple law of mixture. (3) Abnormal changes produced by addition of small quantities of electro-negative gases:

| | | | |
|---|--------------|------------|----------------|
| e.g.: normal mobility | $U + = 1.37$ | $U - 1.80$ | Wellisch, Pr. |
| 6 mm $\text{C}_2\text{H}_5\text{Br}$ gave | 1.37 | 1.80 | Roy. Soc. 82A, |
| 6 mm $\text{C}_2\text{H}_5\text{I}$ " | 1.37 | 1.80 | p. 500, 1909. |
| 10 mm $\text{C}_2\text{H}_5\text{OH}$ " | 0.91 | 1.10 | |
| 9 mm $\text{C}_2\text{H}_5\text{O}$ " | 1.15 | 1.37 | |

Temperature Coefficient of Mobility: There is no decided change with the temperature.

Pressure Coefficient of Mobility: Mobility varies inversely with the pressure in air from 100 to 1/10 atmosphere for - ion, to 1/1000, for + ion; below 1/10 atmosphere all observers agree that the negative ion in air increases abnormally rapidly.

Free Electrons: In pure He, Ar, and N, the negative carriers have a high mobility and are, in part at any rate, free electrons; electrons become appreciable in air at 10 cm pressure.

TABLE 678.—Ionic Mobilities

| Dry gas. | Mobilities. | | $K - 1$ | Observer. | Dry gas. | Mobilities. | | $K - 1$ | Observer. |
|---------------------|-------------|------|---------|-----------|----------------------|-------------|------|---------|-----------|
| | + | - | | | | + | - | | |
| H..... | 6.70 | 7.95 | .000273 | Zeleny | Nitrous oxide..... | 0.82 | 0.90 | .00107 | Wellisch |
| He..... | 5.00 | 6.31 | .000074 | Franck | Ethyl alcohol..... | 0.34 | 0.27 | .00040 | " |
| Ar..... | 1.37 | — | .000105 | " | CCl_4 | 0.30 | 0.31 | .00126 | " |
| N..... | 1.27 | — | .000590 | " | Ethyl chloride..... | 0.33 | 0.31 | .01550 | " |
| O..... | 1.30 | 1.80 | .000540 | Zeleny | Ethyl ether..... | 0.29 | 0.31 | .00742 | " |
| CO_2 | 0.81 | 0.85 | .000900 | Wellisch | Methyl bromide..... | 0.29 | 0.28 | .01460 | " |
| NH_3 | 0.74 | 0.80 | .00770 | " | Ethyl formate..... | 0.30 | 0.31 | .00870 | " |
| Air..... | 1.40 | 1.78 | .000590 | Mean | Ethyl iodide..... | 0.17 | 0.16 | — | " |

Franck, *Jahr. d. Rad. u. Elek.* 6, p. 2, 1912; Wellisch, *Pr. Roy. Soc. 82A*, p. 500, 1909. The following values are from Yen, *Pr. Nat. Acad.* 4, 19 8.

| | H_2 | N_2 | Air | SO_2 | C_2H_{12} | $\text{C}_2\text{H}_6\text{O}$ | $\text{C}_2\text{H}_5\text{O}$ | $\text{C}_2\text{H}_5\text{Cl}$ | CH_3I | $\text{C}_2\text{H}_5\text{I}$ |
|-------------|--------------|--------------|------|---------------|---------------------------|--------------------------------|--------------------------------|---------------------------------|-----------------------|--------------------------------|
| $U +$ | 5.54 | 1.30 | 1.37 | .412 | .385 | .363 | .397 | .304 | .216 | 1.81 |
| $U -$ | 8.45 | 1.80 | 1.81 | .414 | .451 | .373 | .331 | .317 | .220 | 1.81 |
| $U - / U +$ | 1.53 | 1.38 | 1.34 | 1.00 | 1.17 | 1.03 | 1.07 | 1.04 | 1.05 | 1.00 |

TABLE 679.—Diffusion Coefficients

The following table gives the observed and computed ($D = 300UP/N\epsilon$ = very nearly $0.0236U$) values of the diffusion coefficients. The diffusion coefficients are given for some neutral molecules as actually determined for some gases into gases of nearly equal molecular weight. Table taken from Loeb, "The Nature of the Gaseous Ion," *J. Franklin Inst.* 184, p. 775, 1917.

| Gas, diffusing. | Gas diffused into | D molecules. | $U +$ | $D +$ for ions. | |
|---------------------------------------|----------------------|----------------|-------|-----------------|-----------|
| | | | | Computed. | Observed. |
| Ar..... | He | 0.706 | 5.00 | 1.20 | — |
| H_2 | N_2 | .739 | 6.02 | 0.143 | 0.123 |
| Air..... | O_2 | .178 | 1.35 | 0.0319 | 0.028 |
| O_2 | N_2 | .171 | 1.27 | .0200 | .025 |
| CO_2 | N_2O | 1.5-1.0 | .82 | .0193 | .023 * |
| CO | CO | 1.31 | .81 | .0193 | — |
| $\text{C}_2\text{H}_5\text{OH}$ | CO_2 | 0.0693 | .34 | .00805 | — |
| Air..... | Ethyl acetate | .093 | .30 † | .0071 | — |
| H_2O | Air | .246 | 1.35 | .0319 | — |
| NH_3 | NH_3 | 1.00 ‡ | 0.74 | .0174 | — |

* CO_2 into CO_2 . † Ethyl formate. ‡ Estimated.

COLLOIDS

TABLE 680.—General Properties of Colloids

For methods of preparing colloids, see The Physical Properties of Colloidal Solutions, Burton, 1916; for general properties, see Outlines of Colloidal Chemistry, Journ. Franklin Inst. 185, p. 1, 1918 (contains bibliography).

The colloidal phase is conditioned by sufficiently fine division (1×10^{-4} to 10^{-7} cm). Colloids are suspensions (in gas, liquid, solid) of masses of small size capable of indefinite suspension; suspensions in water, alcohol, benzole, glycerine, are called hydrosols, alcosols, benzosols, glycerosols, respectively. The suspended mass is called the disperse phase, the medium the dispersion medium.

Colloids fall into 3 quite definite classes: 1st, those consisting of extremely finely divided particles (Cu, Au, Ag, etc.) capable of more or less indefinite suspension against gravity, in equilibrium of somewhat the same aspect as the gases of the atmosphere, depending as in the Brownian movement upon the bombardment of the molecules of the medium; 2nd, those resisting precipitation (hemoglobin, etc.) probably because of charged nuclei and which may be coagulated and precipitated by the neutralization of the charges; 3rd, colloidal as distinguished from the crystalloidal condition, the colloid being very slowly diffusible and incapable (unlike crystalloids) of penetrating membranes (gelatine, silicic acid, caramel, glue, white of egg, gum, etc.).

| | | |
|--|---|--------------------------|
| | Lyophile, marked affinity between two phases. | c.f., hydrophile. |
| | Lyophobe, " " absent. | c.f., hydrophobe. |
| Smallest particle of Au observed by Zsigmody (ultramicroscope) | | 1.7×10^{-7} cm. |
| " " visible in ordinary microscope about | | 2.5×10^{-5} cm. |
| " " " " ultramicroscope, with electric arc | | 15×10^{-7} cm. |
| " " " " " with direct sunlight | | 1×10^{-7} cm. |

Viscosity of Lyophile Sols

| | | | |
|--------------|-----------------------|--------------|-------|
| Gelatine | 20° C., concentration | 1, viscosity | 0.021 |
| Silicic acid | " " " | 1.00, " | 0.016 |
| " " | " " " | 2.00, " | 0.035 |

TABLE 681.—Molecular Weights of Colloids

| Determined from diffusion | | Determined from freezing point | | Particle wt. Svedberg | |
|---------------------------|-------|--------------------------------|-------|-----------------------|-------|
| Gum arabic | 1750 | Glycogen (162)* | 1625 | Egg albumen | 34500 |
| Tannic acid (322)* | 2730 | Tungstic acid (250)* | 1750 | Hemoglobin | 68100 |
| Egg albumen | 7420 | Gum | 1800 | Phycocorbin | 20800 |
| Caramel | 13200 | Albumose | 2400 | | |
| (Due to Graham) | | Ferric hydrate (107)* | 6000 | | |
| | | Egg albumen | 14000 | | |
| | | Starch (162)* | 25000 | | |

* Formula weight.

TABLE 682.—Brownian Movement

The Brownian movement is a microscopically observed agitation of colloidal particles. It is caused by the bombardment of them by the molecules of the medium and may be used to determine the value of Avogadro's number. Perrin, Chaudesaignes, Ehrenhaft and De Broglie found, respectively, 70, 64, 63 and 64×10^{23} as the value of this constant. The following table indicates the size and the dependence of this movement on the magnitude of the particles.

| Material. | Diameter $\times 10^5$ cm | Medium. | Temp. ° C | Velocity $\times 10^2$ cm/sec. | Observer. |
|-----------------|------------------------------|---------|--------------|--------------------------------------|--------------------------|
| Dust particles | 2.0 | Water | — | none | Zsigmody |
| Gold | 0.35 | " | 20° | 200. | " |
| Gold | 0.1 | " | " | 280. | " |
| Gold | 0.06 | " | " | 700. | " |
| Platinum | 4 to .5 | Acetone | 18 | 3900. | Svedberg, 1906-9 |
| Platinum | " | Water | 20 | 3200. | " |
| Rubber emulsion | 10. | " | 17 | 124. | Henri, 1908 |
| Mastic | 10. | " | 20° | 1.55 | Perrin, Dabrowski, 1909. |
| Gamboge | 4.5 | " | 20 | 2.4 | Chaudesaignes, 1908. |
| " | 2.13 | " | " | 3.4 | " |

The movement varies inversely as the size of the particles; in water, particles of diameter greater than 4μ show no perceptible movement; when smaller than $.1\mu$, lively movement begins, while at 10μ the trajectories amount up to 20μ .

COLLOIDS

TABLE 683.—Adsorption of Gas by Finely Divided Particles

Fine division means great surface per unit weight. All substances tend to adsorb gas at surface, the more the higher the pressure and the lower the temperature. Since different gases vary in this adsorption, fractional separation is possible. Pt black can absorb 100 vols. H_2 , 800 vols. O_2 , Pd 3000 vols. H_2 . In gas analysis Pd, heated to 100° , is used to remove H_2 (higher temperature used for faster adsorption, will take more at lower temperature). Pt can dissolve several vols. of H_2 , Pd, nearly 100 at ordinary temperatures; but it seems probable that the bulk of the 100 vols. of H_2 taken by Pt and the 3000 by Pd must be adsorbed. In 1848 Rose found the density 21 to 22 for Pt foil, but 26 for precipitated Pt.

The film of adsorbed air entirely changes the behavior of very small particles. They flow like a liquid (cf. fog). With substances like carbon black as little as 5 per cent of the bulk is C; a liter of C black may contain 2.5 liters of air. Mitscherlich calculated that when CO_2 at atmospheric pressure, $12^\circ C$, is adsorbed by boxwood charcoal, it occupies 1/56 original vol. Apparent densities of gases adsorbed at low temperatures by coconut charcoal are of the same order (sometimes greater) as liquids.

cm^3 of Gas Adsorbed by a cm^3 of Synthetic Charcoal (corrected to $0^\circ C$, 76 cm^2) (Hempel and Vater).

| $^\circ C$ | H_2 | Ar | N_2 | O_2 | CO | CO_2 | NO | N_2O |
|--------------|--------|----------|----------|----------|--------|--------|--------|--------|
| $+20^\circ$ | 7.3 | 12.6 | 21.0 | 25.4 | 26.8 | 83.8 | 103.6 | 100.4 |
| -20° | 10.5 | 92.6 | 107.4 | 122.4 | 139.4 | 568.4 | 231.3 | 330.1 |
| -185° | 284.7 | — | 632.2 | — | 607.0 | — | — | — |
| | CH_4 | C_2H_6 | C_2H_4 | C_2H_2 | NH_3 | H_2S | Cl_2 | SO_2 |
| $+20^\circ$ | 41.7 | 110.1 | 130.2 | 135.8 | 197.0 | 213.0 | 304.5 | 337.8 |
| -78° | 174.3 | 275.5 | 360.7 | 488.5 | — | — | — | — |

cm^3 of Gas Adsorbed by a cm^3 of Coconut Charcoal (corrected to $0^\circ C$, 76 cm) (Dewar).

| $^\circ C$ | He | H_2 | N_2 | O_2 | CO | Ar |
|--------------|----|-------|-------|-------|-----|-----|
| 0° | 2 | 4 | 15 | 18 | 21 | 12 |
| -185° | 15 | 135 | 155 | 230 | 190 | 175 |

See Langmuir, J. Am. Ch. Soc. 40, 1361, 1918; Richardson, 39, 1829, 1916.

TABLE 684.—Heats of Adsorption

| Adsorber. | Amylene. | Water. | Acetone. | Methyl alcohol. | Ethyl alcohol. | Aniline. | Amyl alcohol. | Ethyl ether. | Chloroform. | Benzene. | Carbon disulphide. | Carbon tetrachloride. | Hexane. |
|------------------|----------|--------|----------|-----------------|----------------|----------|---------------|--------------|-------------|----------|--------------------|-----------------------|---------|
| Fuller's earth * | 57.1 | 30.2 | 27.3 | 21.8 | 17.2 | 13.4 | 10.9 | 10.5 | 8.4 | 4.6 | 4.6 | 4.2 | 3.9 |
| Bone charcoal * | — | 18.5 | 19.3 | 17.6 | 16.5 | — | 10.6 | — | 14.0 | 11.1 | 8.4 | 13.9 | 8.9 |
| Kaolin * | 78.8 | — | — | 27.6 | 24.5 | — | 20.4 | — | 15.7 | 9.9 | 9.9 | 9.4 | 7.2 |
| Fuller's earth † | — | .683 | .684 | .679 | — | — | — | — | .611 | .610 | .621 | .625 | — |

* Small calories liberated when 1 g of the adsorbent is added to a relatively large quantity of the liquid.

† Volume adsorbed from saturated vapor by 1 g of fuller's earth.

Gurvich, J. Russ. Phys. Ch. Soc. 47, 805, 1915.

TABLE 685.—Molecular Heats of Adsorption and Liquefaction (Favre)

| Adsorber. | Gas. | Molecular heats of | | Adsorber. | Gas. | Molecular heats of | |
|-----------------|--------|--------------------|---------------|----------------|--------|--------------------|---------------|
| | | adsorption. | liquefaction. | | | adsorption. | liquefaction. |
| Platinum | H_2 | 46200 | — | Charcoal | SO_2 | 10000-10900 | 5600 |
| Palladium | H_2 | 18000 | — | " | HCl | 9200-10200 | (3600) |
| Charcoal | NH_3 | 5000-8500 | (5000) | " | HBr | 15200-15800 | (4000) |
| " | CO_2 | 6800-7800 | 6250 | " | HI | 21000-23000 | (4400) |
| " | N_2O | 7100-10900 | 4400 | | | | |

TABLE 686.—Transmission of Solar Radiation by Earth's Atmosphere

(Kimball, Monthly Weath. Rev., 56, 393, 1928; 58, 43, 1930.)

Upper curves give transmission (sea-level) by the general scattering by dust-free moist air summed over all wave lengths (w = precipitable water in beam); lower curves, the added fractional depletion in the selectively absorbing water-vapor bands. No allowance is indicated for dust. (See also Table 767.)

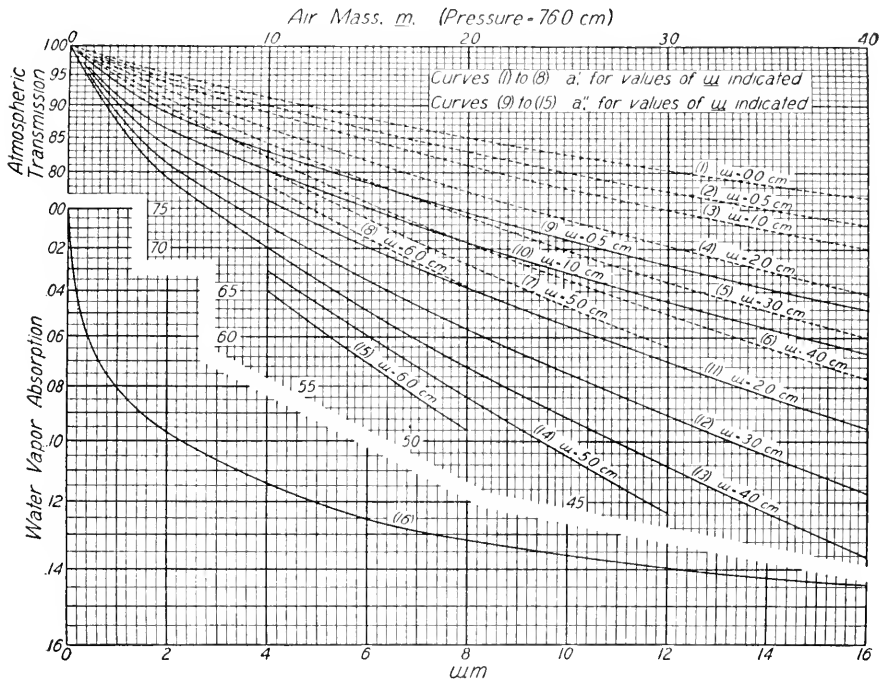


TABLE 687.—Ultra-Violet Solar Radiation at Earth's Surface

Average ultra-violet solar radiation of wave lengths <313 $m\mu$ on the clearest days in Washington during 1930-31. Data in g-cal./ cm^2 /min. $\times 10^5$ (Coblentz, Stair, Bur. Standards Journ. Research, 6, 971, 1931).

| | 1930: | | | | | | | | | | | | 1931: | |
|---------|-------|------|------|------|-----|------|------|------|-------|------|------|------|-------|------|
| | Jan. | Feb. | Mar. | Apr. | May | June | July | Aug. | Sept. | Oct. | Nov. | Dec. | Jan. | Feb. |
| 9 a. m. | 0 | 3 | 12 | 22 | 35 | 41 | 42 | 41 | 33 | 16 | 2 | 0 | 0 | 1 |
| 10 " | 11 | 24 | 37 | 49 | 58 | 63 | 63 | 59 | 50 | 35 | 21 | 11 | 11 | 29 |
| 11 " | 23 | 37 | 49 | 60 | 70 | 76 | 76 | 71 | 61 | 48 | 32 | 19 | 22 | 42 |
| 12 noon | 30 | 43 | 57 | 67 | 76 | 82 | 81 | 76 | 66 | 53 | 38 | 22 | 30 | 51 |

0.0008 cal./ cm^2 /min. = 56 microwatts. Data are also given for greater elevations. At high elevations the spectrum quality of the u.-v. region is richer in the shorter wave lengths than at sea-level; but owing to sky-scattering, the total amount of u.-v. light less than 313 $m\mu$ at sea-level, on the clearest days, is almost as large as at high elevations.

RELATIVE INTENSITY OF SOLAR RADIATION

TABLE 688.—Mean intensity J for 24 hours of solar radiation on a horizontal surface at the top of the atmosphere and the solar radiation A , in terms of the solar radiation, A_0 , at earth's mean distance from the sun.

| Date. | Motion of the sun in longi- tude. | RELATIVE MEAN VERTICAL INTENSITY $\left(\frac{J}{A_0}\right)$. | | | | | | | | | | $\frac{A}{A_0}$. |
|----------|---|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------------------|
| | | LATITUDE NORTH. | | | | | | | | | | |
| | | 0° | 10° | 20° | 30° | 40° | 50° | 60° | 70° | 80° | 90° | |
| Jan. 1 | 0.99 | 0.303 | 0.265 | 0.220 | 0.169 | 0.117 | 0.066 | 0.018 | | | | 1.0335 |
| Feb. 1 | 31.54 | .312 | .282 | .244 | .200 | .150 | .100 | .048 | 0.006 | | | 1.0288 |
| Mar. 1 | 59.14 | .320 | .303 | .279 | .245 | .204 | .158 | .108 | .056 | 0.013 | | 1.0173 |
| Apr. 1 | 89.70 | .317 | .319 | .312 | .295 | .269 | .235 | .195 | .148 | .101 | 0.082 | 1.0009 |
| May 1 | 119.29 | .303 | .318 | .330 | .329 | .320 | .302 | .278 | .253 | .255 | .259 | 0.9841 |
| June 1 | 149.82 | .287 | .315 | .334 | .345 | .349 | .345 | .337 | .344 | .300 | .306 | 0.9714 |
| July 1 | 179.39 | .283 | .312 | .333 | .347 | .352 | .351 | .345 | .356 | .373 | .379 | 0.9666 |
| Aug. 1 | 209.94 | .294 | .316 | .330 | .334 | .330 | .318 | .300 | .282 | .295 | .300 | 0.9709 |
| Sept. 1 | 240.50 | .310 | .318 | .316 | .305 | .285 | .256 | .220 | .180 | .139 | .140 | 0.9828 |
| Oct. 1 | 270.07 | .317 | .308 | .289 | .261 | .225 | .183 | .135 | .084 | .065 | | 0.9995 |
| Nov. 1 | 300.63 | .312 | .286 | .251 | .211 | .164 | .114 | .063 | .018 | | | 1.0164 |
| Dec. 1 | 330.19 | .304 | .267 | .224 | .175 | .124 | .072 | .024 | | | | 1.0288 |
| Year.... | | 0.305 | 0.301 | 0.289 | 0.268 | 0.241 | 0.209 | 0.173 | 0.144 | 0.133 | 0.126 | |

Average annual solar energy received per square dekameter of horizontal surface in kilowatt hours. U. S.: Lincoln, 160,906; Mt. Weather, 148,824; Washington, 145,403; New York, 106,460; Chicago, 97,856. Other countries: Toronto, 139,523; Johannesburg, 175,696; Davos Platz, 174,043; So. Kensington, 78,569; Stockholm, 79,267. (Kimball, Monthly Weather Rev., Apr. 1927.)

TABLE 689.—Mean Monthly and Yearly Temperatures

Mean temperatures of a few selected American stations, also of a station of very high, two of very low temperature, and one of very great and one of very small range of temperature.

| | Jan. | Feb. | Mar. | Apr. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
|--------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1 Hebron-Rama (Labr.) | -20.7 | -20.9 | -15.6 | -6.9 | +0.2 | +4.5 | +7.6 | +8.0 | +4.5 | -0.8 | -6.2 | -16.2 | -5.2 |
| 2 Winnipeg (Canada) | -21.6 | -18.8 | -11.0 | +1.9 | +10.9 | +17.1 | +18.9 | +17.6 | +11.6 | +4.1 | -7.6 | -15.7 | +0.6 |
| 3 Montreal | -10.9 | -9.1 | -4.3 | +4.8 | +12.6 | +18.3 | +20.5 | +19.3 | +14.7 | +7.8 | -0.2 | -7.1 | +5.5 |
| 4 Boston | -2.8 | -2.2 | +1.2 | +7.3 | +13.6 | +19.1 | +21.8 | +20.6 | +16.9 | +11.1 | +4.8 | -0.5 | +9.2 |
| 5 Chicago | -4.8 | -2.9 | +1.2 | +7.9 | +13.4 | +19.7 | +22.2 | +21.6 | +17.9 | +11.1 | +3.6 | -1.5 | +9.1 |
| 6 Denver | -2.1 | +0.1 | +3.8 | +8.3 | +13.6 | +19.1 | +21.2 | +21.2 | +16.6 | +10.3 | +3.3 | 0.0 | +9.7 |
| 7 Washington | +0.7 | +2.1 | +5.2 | +11.7 | +17.7 | +22.9 | +24.9 | +23.7 | +19.9 | +13.4 | +6.9 | +2.3 | +12.6 |
| 8 Pikes Peak | -16.4 | -15.6 | -13.4 | -10.4 | -5.1 | +0.4 | +4.5 | +3.6 | -0.3 | -5.8 | -11.8 | -14.4 | -7.1 |
| 9 St. Louis | -0.8 | +1.7 | +6.2 | +13.4 | +18.8 | +24.0 | +26.0 | +24.9 | +20.8 | +14.2 | +6.4 | +2.0 | +13.1 |
| 10 San Francisco | +10.1 | +10.9 | +12.0 | +12.6 | +13.7 | +14.7 | +14.6 | +14.8 | +15.8 | +15.2 | +13.5 | +10.8 | +13.2 |
| 11 Yuma | +12.3 | +14.9 | +18.1 | +21.0 | +25.1 | +29.4 | +33.1 | +32.6 | +29.1 | +22.8 | +16.6 | +13.3 | +22.3 |
| 12 New Orleans | +12.1 | +14.5 | +16.7 | +20.6 | +23.7 | +26.8 | +27.9 | +27.5 | +25.7 | +21.0 | +15.9 | +13.1 | +20.4 |
| 13 Massaua | +25.6 | +26.0 | +27.1 | +29.0 | +31.1 | +33.5 | +34.8 | +34.7 | +33.3 | +31.7 | +29.0 | +27.0 | +30.3 |
| 14 Ft. Conger (Greenl'd) | -39.0 | -40.1 | -33.5 | -25.3 | -10.0 | +0.4 | +2.8 | +1.0 | -9.0 | -22.7 | -30.9 | -33.4 | -20.6 |
| 15 Werchojansk | -51.0 | -45.3 | -32.5 | -13.7 | +2.0 | +12.3 | +15.5 | +10.1 | +2.5 | -15.0 | -37.8 | -47.0 | -16.7 |
| 16 Batavia | +25.3 | +25.4 | +25.8 | +26.3 | +26.4 | +26.0 | +25.7 | +25.9 | +26.3 | +26.4 | +26.2 | +25.6 | +25.9 |

Lat., Long., Alt. respectively: (1) +58°5, 63°0 W., —; (2) +49.9, 97.1 W, 233m.; (3) +45.5, 73.6 W, 57m.; (4) +42.3, 71.1 W, 38m.; (5) +41.9, 87.6 W, 251m.; (6) +39.7, 105.0 W, 1613m.; (7) +38.9, 77.0 W, 34m.; (8) +38.8, 105.0 W, 4308m.; (9) +38.6, 90.2 W, 173m.; (10) +37.8, 122.5 W, 47m.; (11) +32.7, 114.6 W, 43m.; (12) +30.0, 90.1 W, 16m.; (13) +15.6, 37.5 E, 9m.; (14) +81.7, 64.7 W., —; (15) +67.6, 133.8 E, 140m.; (16) -6.2, 106.8 E, 7m.

Taken from Hann's Lehrbuch der Meteorologie, 2nd edition, which see for further data.

Note: Highest recorded temperature in world = 57° C in Death Valley, California, July 10, 1913.
Lowest recorded temperature in world = -68° C at Verkhoyansk, Feb. 1892.

TABLE 690.—Temperature Variation over Earth's Surface (Hann)

| Latitude. | Temperatures ° C | | | | | | Mean ocean temp. | Land surface % |
|------------|------------------|-------|---------|-------|---------|--------|------------------|----------------|
| | Jan. | Apr. | July. | Oct. | Year. | Range. | | |
| North pole | -41.0 | -28.0 | -1.0 | -24.0 | -22.7 | 40.0 | -1.7 | — |
| +80° | -32.2 | -22.7 | +2.0 | -19.1 | -17.1 | 34.2 | -1.7 | 20 |
| 70° | -26.3 | -14.0 | 7.3 | -9.3 | -10.7 | 33.6 | +0.7 | 53 |
| 60° | -16.1 | -2.8 | 14.1 | +0.3 | -1.1 | 30.2 | 4.8 | 61 |
| 50° | -7.2 | +5.2 | 17.9 | 6.9 | +5.8 | 25.1 | 7.9 | 58 |
| 40° | +5.5 | 13.1 | 24.0 | 15.7 | 14.1 | 18.5 | 14.1 | 45 |
| 30° | 14.7 | 20.1 | 27.3 | 21.8 | 20.4 | 12.6 | 21.3 | 43.5 |
| +10° | 21.9 | 25.2 | 28.0 | 26.4 | 25.3 | 6.1 | 25.4 | 31.5 |
| Equator | 25.8 | 27.2 | 27.0 | 26.9 | 26.8 | 1.4 | 27.2 | 24 |
| -10° | 20.5 | 26.6 | 25.7 | 26.5 | 26.3 | 0.9 | 27.1 | 22 |
| 20° | 20.4 | 25.9 | 23.0 | 25.7 | 25.5 | 3.4 | 25.8 | 20 |
| 30° | 25.3 | 24.0 | 19.8 | 22.8 | 23.0 | 5.5 | 24.0 | 24 |
| 40° | 21.6 | 18.7 | 14.5 | 18.0 | 18.4 | 7.1 | 19.5 | 20 |
| 50° | 15.4 | 12.5 | 8.8 | 11.7 | 11.9 | 6.6 | 13.3 | 4 |
| 60° | 8.4 | 5.4 | 3.0 | 4.8 | 5.4 | 5.4 | +6.4 | 2 |
| 70° | 3.2 | — | -9.3 | — | -3.2 | 12.5 | 0.0 | 0 |
| 80° | -1.2 | — | -21.0 | — | -12.0 | 19.8 | -1.3 | 71 |
| South pole | (-4.3) | — | (-28.7) | — | (-20.6) | (24.4) | — | 100 |
| | (-6.0) | — | (-33.0) | — | (-25.0) | (27.0) | — | (100) |

TABLE 691.—Temperature Variation with Depth (Land and Ocean)

Table illustrates temperature changes underground at moderate depths due to surface warming (read from plot for Tiflis, *Lehrbuch der Meteorologie*, Hann and Süring, 1915). Below 20-30 m (nearer the surface in tropics) there is no annual variation. Increase downwards at greater depths, 0.03 ° C per m (1° per 35 m) l.c. At Pittsburgh, 1524 m, 49.4°, 0.0204 per m; Oberschlesien, 2003 m, 70°, 0.0204 per m; or W. Virginia, 2200 m, 70°, 0.034° per m (Van Orstrand). Mean value outflow heat from earth's center, 0.00000172 g-cal/cm²/sec. or 54 g-cal/cm²/year (39 Laby). Open ocean temperatures: Greatest mean annual range (Schott) 40° N, 4.2° C; 30° S, 5.1°; but 10° N, only 2.2°; 50° S, 2.0°. Mean surface temp. whole ocean (Krümmel) 17.4°; all depths, 3.9°. Below 1 km nearly isothermal with depth. In tropics, surface 28°; at 183 m, 11°. 80° all water less than 4.4°. Deep-sea (bottom) temps. range -0.5° to +2.6°. Soundings in S. Atlantic: 0 km, 18.9°; .25 km, 15°; .5 km, 8.3°; 1 km, 3.3°; 3 km, 1.7°; 4.5 km, 0.0°.

| Depth, m | Temperature, centigrade. | | | | | | | | | | | |
|----------|--------------------------|------|------|------|------|-------|-------|------|-------|------|------|------|
| | Jan. | Feb. | Mar. | Apr. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. |
| 0 | 1 | 4 | 10 | 14 | 21 | 29 | 32 | 32 | 24 | 16 | 9 | 4 |
| 0.5 | 4 | 4 | 9 | 13 | 18 | 23 | 26 | 28 | 24 | 18 | 12 | 6 |
| 1.0 | 6 | 6 | 8 | 12 | 15 | 20 | 24 | 26 | 23 | 18 | 14 | 10 |
| 1.5 | 9 | 8 | 9 | 11 | 14 | 18 | 21 | 23 | 22 | 18 | 15 | 12 |
| 2.0 | 11 | 10 | 10 | 11 | 13 | 16 | 19 | 21 | 21 | 18 | 16 | 14 |
| 3.0 | 14 | 12 | 12 | 11 | 13 | 14 | 16 | 17 | 18 | 18 | 17 | 15 |
| 4.0 | 15 | 13 | 12 | 12 | 12 | 13 | 14 | 16 | 16 | 17 | 17 | 16 |
| 5.0 | 15 | 14 | 13 | 13 | 13 | 13 | 14 | 14 | 15 | 16 | 16 | 16 |
| 6.0 | 15 | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 15 | 15 | 15 |

TABLES 692-694

THE EARTH'S ATMOSPHERE

TABLE 692.—Miscellaneous Data. Variation with Latitude

Optical ev. lence of atmosphere's extent: twilight 63 km, luminous clouds 83, meteors 200, aurora 44-360. Jeans computes a density at 170 km of 2×10^{18} molecules per cm^3 , nearly all H (5% He); at 810 km, 3×10^{10} molecules per cm^3 almost all H. When in equilibrium, each gas forms an atmosphere whose density decrease with altitude is independent of the other components (Dalton's law, H_2O vapor does not). The lighter the gas, the smaller the decrease rate. A homogeneous atmosphere, 76 cm pressure at sea-level, of sea-level density, would be 7991 m high. Average sea-level barometer is 74 cm; corresponding homogeneous atmosphere (truncated cone) 7790 m, weighs (base, m^2) 10,120 kg; this times earth's area is 52×10^{14} metric tons or 10^{-6} of earth's mass. The percentage by vol. and the partial pressures of the dry-air components at sea-level are: N_2 , 78.03, 593.02 mm; O_2 , 20.99, 159.52; A, 0.94, 7.144; CO_2 , 0.03, 0.228; H_2 , 0.01, 0.076; Ne, 0.0012, 0.009; He, 0.0004, 0.003 (Hann). The following table gives the variation of the mean composition of moist air with the latitude (Hann).

| | | | | | |
|--------------|--------------------|--------------------|--------|---------------------------|--------------------|
| Equator..... | N_2 75.99 | O_2 20.44 | A 0.92 | H_2O 2.63 | CO_2 0.02 |
| 50° N..... | 77.32 | 20.80 | 0.94 | 0.92 | 0.02 |
| 70° N..... | 77.87 | 20.94 | 0.94 | 0.22 | 0.03 |

TABLE 693.—Variation of Percentage Composition with Altitude (Humphreys)

Computed on assumptions: sea-level temperature 11° C; temperature uniformly decreasing 6° per km up to 11 km, from there constant with elevation at -55°. J. Franklin Inst. 184, p. 388, 1917.

| Height, km | Argon. | Nitrogen. | Water vapor. | Oxygen. | Carbon dioxide. | Hydrogen. | Helium. | Total pressure, mm |
|------------|--------|-----------|--------------|---------|-----------------|-----------|---------|--------------------|
| 140 | — | 0.01 | — | — | — | 99.15 | 0.84 | 0.0010 |
| 120 | — | 0.10 | — | — | — | 98.74 | 1.07 | 0.0052 |
| 100 | — | 2.95 | 0.05 | 0.11 | — | 95.58 | 1.31 | 0.0007 |
| 80 | — | 32.18 | 0.17 | 1.85 | — | 64.70 | 1.10 | 0.0123 |
| 60 | 0.03 | 81.22 | 0.45 | 7.69 | — | 10.68 | 0.23 | 0.0935 |
| 50 | 0.12 | 86.78 | 0.10 | 10.17 | — | 2.70 | 0.07 | 0.403 |
| 40 | 0.22 | 86.42 | 0.06 | 12.61 | — | 0.67 | 0.02 | 1.84 |
| 30 | 0.35 | 84.26 | 0.03 | 15.18 | 0.01 | 0.16 | 0.01 | 8.63 |
| 20 | 0.59 | 81.24 | 0.02 | 18.10 | 0.01 | 0.04 | — | 40.99 |
| 15 | 0.77 | 79.52 | 0.01 | 19.66 | 0.02 | 0.02 | — | 89.66 |
| 11 | 0.94 | 78.02 | 0.01 | 20.99 | 0.03 | 0.01 | — | 168.00 |
| 5 | 0.94 | 77.80 | 0.18 | 20.95 | 0.03 | 0.01 | — | 495. |
| 0 | 0.93 | 77.08 | 1.20 | 20.75 | 0.03 | 0.01 | — | 760. |

TABLE 694.—Variation of Temperature, Pressure and Density with Altitude

Average data from sounding balloon flights (65 for summer, 52 for winter data) made at Trappes (near Paris), Uccle (near Brussels), Strassburg and Munich. Compiled by Humphreys, 16 to 20 m chiefly extrapolated.

| Elevation, km | Summer. | | | Winter. | | |
|---------------|-----------|---------------------|--|-----------|---------------------|--|
| | Temp. ° C | Pressure, mm of Hg. | Density, dry air, g/cm^3 | Temp. ° C | Pressure, mm of Hg. | Density, dry air, g/cm^3 |
| 20.0 | -51.0 | 44.1 | 0.000092 | -57.0 | 39.5 | 0.000085 |
| 19.0 | -51.0 | 51.5 | 0.00108 | -57.0 | 46.3 | 0.00100 |
| 18.0 | -51.0 | 60.0 | 0.00126 | -57.0 | 54.2 | 0.00117 |
| 17.0 | -51.0 | 70.0 | 0.00146 | -57.0 | 63.5 | 0.00137 |
| 16.0 | -51.0 | 81.7 | 0.00171 | -57.0 | 74.0 | 0.00160 |
| 15.0 | -51.0 | 95.3 | 0.00199 | -57.0 | 87.1 | 0.00187 |
| 14.0 | -51.0 | 111.1 | 0.00232 | -57.0 | 102.1 | 0.00220 |
| 13.0 | -51.0 | 129.6 | 0.00270 | -57.0 | 119.5 | 0.00257 |
| 12.0 | -51.0 | 151.2 | 0.00316 | -57.0 | 140.0 | 0.00301 |
| 11.0 | -49.5 | 176.2 | 0.00366 | -57.0 | 164.0 | 0.00353 |
| 10.0 | -45.5 | 205.1 | 0.00419 | -54.5 | 192.0 | 0.00408 |
| 9.0 | -37.8 | 237.8 | 0.00470 | -49.5 | 224.1 | 0.00466 |
| 8.0 | -29.7 | 274.3 | 0.00524 | -43.0 | 260.6 | 0.00526 |
| 7.0 | -22.1 | 314.9 | 0.00583 | -35.4 | 301.6 | 0.00590 |
| 6.0 | -15.1 | 360.2 | 0.00649 | -28.1 | 347.5 | 0.00659 |
| 5.0 | -8.9 | 410.6 | 0.00722 | -21.2 | 398.7 | 0.00735 |
| 4.0 | -3.0 | 466.6 | 0.00803 | -15.0 | 455.9 | 0.00821 |
| 3.0 | +2.4 | 528.9 | 0.00892 | -9.3 | 519.7 | 0.00915 |
| 2.5 | +5.0 | 562.5 | 0.00942 | -6.7 | 554.3 | 0.00967 |
| 2.0 | +7.5 | 598.0 | 0.00990 | -4.7 | 590.8 | 0.01023 |
| 1.5 | +10.0 | 635.4 | 0.01043 | -3.0 | 629.6 | 0.01083 |
| 1.0 | +12.0 | 674.8 | 0.01100 | -1.3 | 670.6 | 0.01146 |
| 0.5 | +14.5 | 716.3 | 0.01157 | 0.0 | 714.0 | 0.01215 |
| 0.0 | +15.7 | 760.0 | 0.01223 | +0.7 | 760.0 | 0.01290 |

760 mm = 29.921 in. = 1013.3 millibars. 1 mm = 1.33322387 millibars. 1 bar = 1,000,000 dynes; this value, sanctioned by International Meteorological Conferences, is 1,000,000 times that sometimes used by physicists.

SMITHSONIAN TABLES.

THE EARTH'S ATMOSPHERE

Standard Atmosphere

A standard atmosphere is defined by an altitude-temperature-pressure relation. It is an aeronautic necessity in evaluating the performance of airplanes and for the calibration of instruments. The following standard has been officially adopted by the Army Air Corps, Bureau of Standards, National Advisory Committee for Aeronautics, and the Weather Bureau. However, in the evaluation of flights made to break international records, the Fédération Aéronautique Internationale Standard Atmosphere is used. The altitude-temperature assumption is a slight modification of that proposed by Toussaint and closely approximates the average observed values of air temperature at all altitudes at latitude 40° in the United States. Adapted from M 78 (Brombacher) published by the Bur. Standards. The formulae defining this standard atmosphere follow:

Z = standard altitude. Z_{55} = altitude lower limit isothermal layer.

T = absolute temperature of air at altitude Z .

T_0 = standard sea-level temperature, 288° absolute, 15° C.

T_m = mean absolute temperature of air column below altitude Z .

T_{m55} = ditto for Z_{55} , 251.378° absolute.

p = air pressure at altitude Z . p_0 , standard sea-level pressure, 760 mm.

ρ = density air at altitude Z . ρ_0 , ditto sea-level, 1.2255 kg/m^3 .

$Z = (KT_m/T_0) \log_{10}(p_0/p)$. K is 19,413.3 for Z in meters, or 63,691.8 in feet.

$\rho = \rho_0(p/p_0)^{(T_0/T)}$.

- (1) Up to the isothermal layer (below 10,769 m):

$T = 288 - aZ$. $T_m = aZ / \log_e [T_0 / (T_0 - aZ)]$.

$a = 0.0065000$ for Z in meters; 0.0019812 in feet.

- (2) At the lower limit of the isothermal layer (10,769 m):

$T = 218^\circ$ absolute or -55°C . $Z_{55} = 35,322$ feet or 10,769 meters.

- (3) In the isothermal layer (above 10,769 meters):

$T_m = Z / [Z_{55}/T_{m55} + (Z - Z_{55})/218]$.

(See Nat. Adv. Comm. Aeronautics Techn. Rep., Nos. 147, 218, and 246 of the committee for further data and complete tables.)

| Altitude | | Pressure | | Density | | Temperature °C | Mean temperature °C |
|----------|-------|----------|--------|-------------------|----------------------|-------------------|------------------------|
| Meters | Feet | mm Hg | in Hg | kg/m ³ | lb./ft. ³ | | |
| 0 | 0 | 760.0 | 29.921 | 1.2255 | 0.07650 | 15.0 | 15.0 |
| 1000 | 3281 | 674.1 | 26.54 | 1.1120 | .06942 | 8.5 | 11.7 |
| 2000 | 6562 | 596.2 | 23.47 | 1.0068 | .06286 | + 2.0 | 8.4 |
| 3000 | 9842 | 525.8 | 20.70 | .9094 | .05678 | - 4.5 | 5.1 |
| 4000 | 13123 | 462.3 | 18.20 | .8193 | .05115 | -11.0 | + 1.8 |
| 5000 | 16404 | 405.1 | 15.95 | .7363 | .04597 | -17.5 | - 1.6 |
| 6000 | 19685 | 353.8 | 13.93 | .6598 | .04119 | -24.0 | - 5.0 |
| 7000 | 22966 | 307.9 | 12.12 | .5896 | .03681 | -30.5 | - 8.4 |
| 8000 | 26247 | 266.9 | 10.51 | .5252 | .03279 | -37.0 | -11.9 |
| 9000 | 29528 | 230.4 | 9.07 | .4664 | .02912 | -43.5 | -15.4 |
| 10000 | 32808 | 198.2 | 7.80 | .4127 | .02577 | -50.0 | -18.9 |
| 11000 | 36089 | 169.7 | 6.68 | .3614 | .02256 | -55.0 | -22.4 |
| 12000 | 39370 | 145.0 | 5.71 | .3090 | .01929 | -55.0 | -25.5 |
| 13000 | 42651 | 124.0 | 4.88 | .2642 | .01649 | -55.0 | -28.1 |
| 14000 | 45932 | 106.0 | 4.17 | .2259 | .01410 | -55.0 | -30.2 |
| 15000 | 49212 | 90.6 | 3.57 | .1931 | .01206 | -55.0 | -32.0 |
| 0 | 0 | 760.0 | 29.921 | 1.2255 | .07651 | 15.0 | 15.0 |
| 1524 | 5000 | 632.3 | 24.89 | 1.0559 | .06592 | + 5.1 | 10.0 |
| 3048 | 10000 | 522.6 | 20.58 | .9048 | .05649 | - 4.8 | + 5.0 |
| 4572 | 15000 | 428.8 | 16.88 | .7711 | .04814 | -14.7 | - .1 |
| 6096 | 20000 | 349.1 | 13.75 | .6527 | .04075 | -24.6 | - 5.3 |
| 7620 | 25000 | 281.9 | 11.10 | .5489 | .03427 | -34.5 | -10.5 |
| 9144 | 30000 | 225.6 | 8.88 | .4583 | .02861 | -44.4 | -15.9 |
| 10668 | 35000 | 178.7 | 7.04 | .3795 | .02369 | -54.3 | -21.3 |
| 12192 | 40000 | 140.7 | 5.54 | .2998 | .01872 | -55.0 | -26.0 |
| 13716 | 45000 | 110.8 | 4.36 | .2361 | .01474 | -55.0 | -29.6 |
| 15240 | 50000 | 87.3 | 3.44 | .1860 | .01161 | -55.0 | -32.4 |

The following condensed tables (Maris, Terr. Mag. and Atmosph. Elec., 33, 233, 1928) of the upper atmosphere of the earth result from attempts at including further factors than usually considered. They should be taken as tentative because of approximate theory and ignorance of much necessary data for the discussion. Meteors, reflection of sound and radio waves, the aurora, ozone, ionization, and optical phenomena continually give us further probes into the upper air. The gases are uniformly mixed below a height of roughly 100 km; above 150 km each gas is in equilibrium with its own partial pressure; between these heights there is for each gas a transition from uniform mixture with the air to equilibrium with its own partial pressure at a height which depends on the temperature and previous wind currents of the atmosphere, but which averages about 110 km. Apparently above 300 km the atmosphere can not be assumed in equilibrium; the percentage of very high-energy molecules is far higher than indicated by a Maxwellian curve for thermal equilibrium.

TABLE 696.—Pressure in Dynes/cm², Summer and Winter, Day and Night (Maris)

| Altitude Km | Pressure = $p \times 10^6$ dynes/cm ² | | | | | | | | | | | | | | | | | |
|----------------|--|-----|----------------|-----|--------|-----|-----------------|-----|--------|-----|--------|-----|----------------|-----|-------------------------------|-----|---------------------|-----|
| | N ₂ | | O ₂ | | A | | CO ₂ | | Kr | | He | | H ₂ | | Totals | | | |
| | | | | | | | | | | | | | | | N ₂ H ₂ | | with H ₂ | |
| | ρ | n | ρ | n | ρ | n | ρ | n | ρ | n | ρ | n | ρ | n | ρ | n | ρ | n |
| Summer day | | | | | | | | | | | | | | | | | | |
| 0 | 79 | 4 | 22 | 4 | 96 | 2 | 30 | 1 | 98 | -2 | 40 | -1 | 11 | 1 | 10 | 5 | 10 | 5 |
| 40 | 32 | 2 | 85 | 1 | 39 | 0 | 72 | -1 | 39 | -4 | 16 | -3 | 41 | -2 | 40 | 2 | 41 | 2 |
| 100 | 61 | -1 | 16 | -1 | 74 | -3 | 24 | -4 | 76 | -7 | 31 | -6 | 78 | -5 | 78 | -1 | 78 | -1 |
| 200 | 11 | -4 | 17 | -5 | 23 | -7 | 38 | -9 | 53 | -15 | 18 | -8 | 31 | -7 | 13 | -4 | 13 | -4 |
| 300 | 33 | -8 | 14 | -9 | 17 | -12 | 03 | -15 | 89 | -26 | 56 | -9 | 17 | -7 | 40 | -8 | 21 | -7 |
| Summer night | | | | | | | | | | | | | | | | | | |
| 0 | 79 | 4 | 22 | 4 | 96 | 2 | 30 | 1 | 98 | -2 | 40 | -1 | 11 | 1 | 10 | 5 | 10 | 5 |
| 40 | 23 | 2 | 62 | 1 | 28 | 0 | 89 | -2 | 29 | -4 | 12 | -3 | 30 | -2 | 30 | 2 | 30 | 2 |
| 100 | 39 | -2 | 10 | -2 | 48 | -4 | 15 | -5 | 48 | -8 | 20 | -7 | 50 | -6 | 50 | -2 | 50 | 2 |
| 200 | 48 | -8 | 21 | -9 | 56 | -12 | 19 | -14 | 34 | -25 | 58 | -9 | 15 | -7 | 56 | -8 | 21 | -6 |
| 300 | 73 | -14 | 52 | -16 | 54 | -20 | 16 | -23 | 27 | -42 | 88 | -10 | 58 | -8 | 88 | -10 | 59 | -8 |
| Winter day | | | | | | | | | | | | | | | | | | |
| 0 | 79 | 4 | 22 | 4 | 96 | 2 | 30 | 1 | 98 | -2 | 40 | -1 | 11 | 1 | 10 | 5 | 10 | 5 |
| 40 | 22 | 2 | 60 | 1 | 27 | 0 | 86 | -2 | 28 | -4 | 12 | -3 | 29 | -2 | 29 | 2 | 29 | 2 |
| 100 | 70 | -2 | 19 | -2 | 85 | -4 | 27 | -5 | 86 | -8 | 36 | -7 | 80 | -6 | 89 | -2 | 64 | -3 |
| 200 | 24 | -7 | 14 | -8 | 46 | -11 | 24 | -13 | 26 | -23 | 64 | -9 | 17 | -7 | 26 | -7 | 73 | -8 |
| 300 | 12 | -12 | 12 | -14 | 12 | -18 | 12 | -21 | 51 | -39 | 16 | -9 | 71 | -8 | 16 | -9 | 30 | -8 |
| Winter night | | | | | | | | | | | | | | | | | | |
| 0 | 79 | 4 | 22 | 4 | 96 | 2 | 30 | 1 | 98 | -2 | 40 | -1 | 11 | 1 | 11 | 5 | 10 | 5 |
| 40 | 16 | 2 | 60 | 1 | 19 | 0 | 60 | -2 | 20 | -4 | 80 | -4 | 11 | -2 | 20 | 2 | 20 | 2 |
| 100 | 20 | -2 | 53 | -3 | 24 | -4 | 76 | -6 | 25 | -8 | 10 | -7 | 25 | -6 | 25 | -2 | 13 | -3 |
| 200 | 12 | -8 | 57 | -10 | 58 | -13 | 32 | -15 | 17 | -26 | 62 | -9 | 12 | -7 | 19 | -8 | 14 | -7 |
| 300 | 11 | -14 | 86 | -17 | 18 | -21 | 14 | -24 | 40 | -44 | 87 | -10 | 30 | -8 | 87 | -10 | 30 | -8 |

TABLE 697.—Molecular Densities in Atmosphere (Maris)

| Altitude Km | Number of molecules per cm ³ | | | | | | | | | | | | | | | | | |
|----------------|---|----------|----------------|----------|----------|----------|-----------------|----------|----------|----------|----------|----------|----------|----------|-------------------|----------|---------------------|----------|
| | N ₂ | | O ₂ | | A | | CO ₂ | | Kr | | He | | H | | Totals | | | |
| | | | | | | | | | | | | | | | No H ₂ | | with H ₂ | |
| | <i>p</i> | <i>n</i> | <i>p</i> | <i>n</i> | <i>p</i> | <i>n</i> | <i>p</i> | <i>n</i> | <i>p</i> | <i>n</i> | <i>p</i> | <i>n</i> | <i>p</i> | <i>n</i> | <i>p</i> | <i>n</i> | <i>p</i> | <i>n</i> |
| Summer day | | | | | | | | | | | | | | | | | | |
| 40 | 84 | 15 | 23 | 15 | 10 | 14 | 32 | 12 | 10 | 10 | 43 | 10 | 11 | 12 | 11 | 16 | 11 | 16 |
| 80 | 80 | 13 | 22 | 13 | 96 | 11 | 30 | 10 | 10 | 8 | 41 | 8 | 10 | 10 | 10 | 14 | 10 | 14 |
| 100 | 12 | 13 | 32 | 12 | 15 | 11 | 46 | 9 | 15 | 7 | 63 | 7 | 16 | 9 | 16 | 13 | 16 | 13 |
| 200 | 22 | 9 | 32 | 8 | 45 | 6 | 75 | 4 | 10 | -1 | 35 | 5 | 61 | 6 | 25 | 9 | 25 | 9 |
| 300 | 64 | 5 | 28 | 4 | 33 | 1 | 18 | -1 | 16 | -12 | 11 | 5 | 34 | 6 | 77 | 5 | 41 | 6 |
| Summer night | | | | | | | | | | | | | | | | | | |
| 40 | 73 | 15 | 20 | 15 | 89 | 13 | 28 | 12 | 91 | 9 | 38 | 10 | 94 | 11 | 94 | 15 | 94 | 15 |
| 80 | 22 | 13 | 59 | 12 | 27 | 11 | 84 | 9 | 27 | 7 | 14 | 8 | 28 | 9 | 28 | 13 | 28 | 13 |
| 100 | 12 | 12 | 33 | 11 | 15 | 10 | 48 | 8 | 15 | 6 | 63 | 6 | 16 | 8 | 16 | 12 | 16 | 12 |
| 200 | 15 | 6 | 66 | 4 | 21 | 2 | 49 | -1 | 11 | -10 | 18 | 5 | 48 | 6 | 18 | 6 | 66 | 6 |
| 300 | 23 | 0 | 17 | -2 | 17 | -6 | 52 | -10 | 86 | -20 | 28 | 4 | 18 | 6 | 28 | 4 | 19 | 6 |
| Winter day | | | | | | | | | | | | | | | | | | |
| 40 | 67 | 15 | 18 | 15 | 82 | 13 | 26 | 12 | 84 | 9 | 34 | 10 | 86 | 11 | 86 | 15 | 86 | 15 |
| 80 | 29 | 13 | 78 | 12 | 35 | 11 | 11 | 10 | 36 | 7 | 15 | 8 | 37 | 9 | 37 | 13 | 37 | 13 |
| 100 | 20 | 12 | 54 | 11 | 25 | 10 | 78 | 8 | 26 | 6 | 10 | 7 | 26 | 8 | 26 | 12 | 26 | 12 |
| 200 | 60 | 6 | 39 | 5 | 13 | 3 | 71 | 0 | 75 | -10 | 18 | 5 | 49 | 6 | 74 | 6 | 12 | 7 |
| 300 | 36 | 1 | 34 | -1 | 35 | -5 | 35 | -8 | 15 | -25 | 45 | 4 | 21 | 6 | 45 | 4 | 21 | 6 |
| Winter night | | | | | | | | | | | | | | | | | | |
| 40 | 51 | 15 | 14 | 15 | 62 | 13 | 20 | 11 | 63 | 9 | 26 | 10 | 65 | 11 | 65 | 15 | 65 | 15 |
| 80 | 14 | 13 | 34 | 12 | 15 | 11 | 48 | 9 | 16 | 7 | 65 | 7 | 16 | 9 | 17 | 13 | 17 | 13 |
| 100 | 65 | 11 | 17 | 11 | 79 | 9 | 25 | 8 | 81 | 5 | 33 | 6 | 83 | 7 | 83 | 11 | 83 | 11 |
| 200 | 39 | 5 | 19 | 4 | 19 | 1 | 10 | -1 | 57 | -13 | 20 | 5 | 39 | 6 | 61 | 5 | 45 | 6 |
| 300 | 36 | -1 | 28 | -3 | 58 | -8 | 46 | -11 | 13 | -30 | 23 | 4 | 13 | 6 | 23 | 4 | 13 | 6 |

TABLE 698.—Geopotential, Dynamic Heights

The "geopotential" or "gravity potential" of a point is its potential energy relative to sea-level of a unit-mass situated at the point.

In comparisons of vertical positions in dynamical meteorology, advantages result by giving the heights above sea-level in terms of the potential energy possessed by a unit-mass at these positions. The use of geopotential for heights is better realized in that surfaces of equal geopotential are identical with horizontal or level surfaces, and, due to the geographical variation of gravity, are not surfaces equally distant from sea-level.

Heights measured thus are called "dynamic heights." Defined more precisely, geopotential is

$$\Gamma = - \int_0^h g \, dh \quad (1)$$

where Γ = geopotential in absolute units, g = acceleration of gravity in meters, h = geometric height above sea-level in meters.

Γ has the dimensional formula [$L^2 T^{-2}$], and is expressed in absolute units, the "geodesic meter" when g is expressed in m/sec.², and h in meters. The derived unit adopted by the Commission Internationale de la Haute Atmosphère is the "dynamic meter" H_d , $10 \text{ m}^2/\text{sec}^2$, after Prof. V. Bjerknes¹. Then H_d = dynamic height (geopotential in dynamic meters) is

$$H_d = - (1/10) \int_0^h g \, dh \quad (2)$$

Helmert's equation (3) is substituted in (2),

$$g = - (g_\phi - 0.00003086 h), \text{ where,} \quad (3)$$

$g_\phi = g$ at latitude ϕ sea-level, below given point (in m/sec.²), g = acceleration of gravity at point in m/sec.², h = geometric height of point above sea-level in meters. (2) may then be integrated, giving

$$H_d = [g_\phi/10]h - 1.543 \times 10^{-7} h^2. \quad (4)$$

The following table results from (4) using g_ϕ computed from the U. S. Coast and Geodetic Survey formula:

$$g_\phi = 9.78039 (1 + 0.005294 \sin^2 \phi - 0.000007 \sin^2 2 \phi)$$

Neglecting the h^2 term, $H_d = 0.98 h$, approximately, whence, $h = 1.02 H_d$, approximately; substituting this in (4) for the h^2 term we have $h = (10/g_\phi)H_d + (10/g_\phi)(1.543)(1.02)^2 10^{-7} H_d^2$. For simplification, 9.8062, the mean value of g at lat. 45° and sea-level is substituted for g_ϕ in the second term and then approximately,

$$h = (10/g_\phi)H_d + 1.637 \times 10^{-7} H_d^2 \quad (5)$$

Table 699 is computed from (5) and values of g obtained as before.

References: Dynamical Meteorology and Hydrography, V. Bjerknes and collaborators, Carnegie Institution, 1910; Avant-propos of the C. R. des Jours internationaux 1923, Commission internationale de la haute atmosphère, 1927, Secretary of the commission, c/o Royal Meteorological Society, London.

TABLE 699.—Equivalents, in Geodynamic Kilometers, of Geometric Heights in Kilometers for Various Latitudes

| Geometric hts. in km | Latitude (degrees) Geodynamic heights | | | | | | | | | |
|-------------------------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | 0° | 10° | 20° | 30° | 40° | 50° | 60° | 70° | 80° | 90° |
| 30 | 29.202 | 29.207 | 29.220 | 29.241 | 29.266 | 29.293 | 29.318 | 29.339 | 29.353 | 29.358 |
| 25 | 24.354 | 24.358 | 24.370 | 24.387 | 24.408 | 24.430 | 24.451 | 24.469 | 24.480 | 24.484 |
| 20 | 19.499 | 19.502 | 19.511 | 19.525 | 19.542 | 19.560 | 19.576 | 19.590 | 19.600 | 19.603 |
| 15 | 14.636 | 14.638 | 14.645 | 14.655 | 14.668 | 14.681 | 14.694 | 14.704 | 14.711 | 14.713 |
| 10 | 9.765 | 9.767 | 9.771 | 9.778 | 9.786 | 9.795 | 9.804 | 9.811 | 9.815 | 9.817 |
| 5 | 4.886 | 4.887 | 4.889 | 4.892 | 4.897 | 4.901 | 4.906 | 4.909 | 4.911 | 4.912 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

TABLE 700.—Equivalents, in Geometric Kilometers, of Dynamic Heights in Geodynamic Kilometers for Various Latitudes

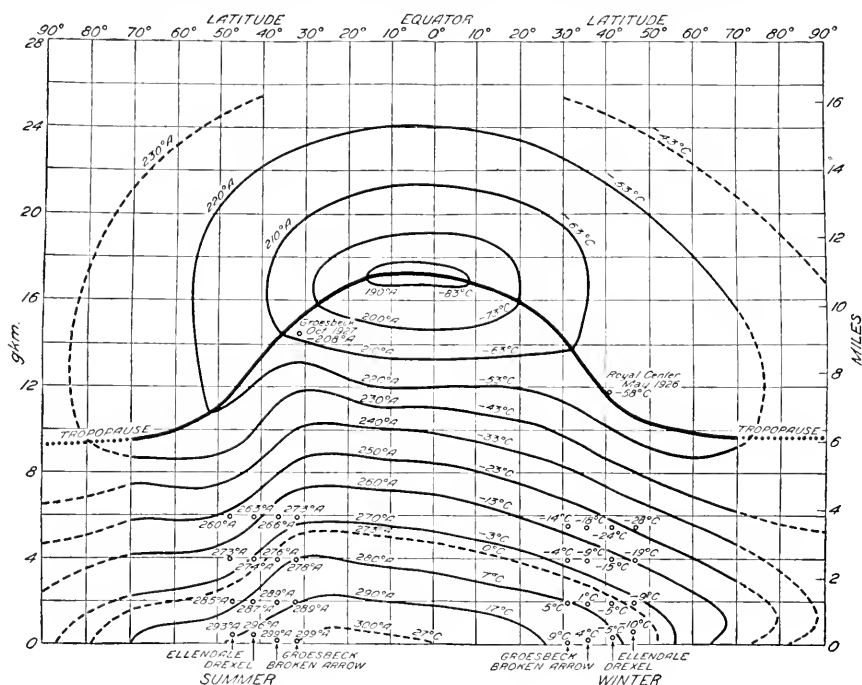
| Dynamic hts. Geodynamic km | Latitude (degrees) Geometric heights | | | | | | | | | |
|-------------------------------------|---|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | 0° | 10° | 20° | 30° | 40° | 50° | 60° | 70° | 80° | 90° |
| 30 | 30.820 | 30.815 | 30.801 | 30.780 | 30.754 | 30.726 | 30.699 | 30.677 | 30.663 | 30.658 |
| 25 | 25.663 | 25.659 | 25.647 | 25.629 | 25.608 | 25.584 | 25.562 | 25.544 | 25.532 | 25.528 |
| 20 | 20.515 | 20.512 | 20.503 | 20.488 | 20.470 | 20.452 | 20.434 | 20.420 | 20.411 | 20.407 |
| 15 | 15.373 | 15.371 | 15.364 | 15.354 | 15.340 | 15.325 | 15.313 | 15.302 | 15.295 | 15.293 |
| 10 | 10.241 | 10.239 | 10.234 | 10.227 | 10.218 | 10.209 | 10.200 | 10.193 | 10.189 | 10.187 |
| 5 | 5.116 | 5.115 | 5.113 | 5.109 | 5.105 | 5.101 | 5.096 | 5.092 | 5.090 | 5.089 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

THE EARTH'S ATMOSPHERE

TABLE 701.—Temperature Variation of Lower 25 Km with Latitude and Altitude, Northern Hemisphere (Ramanathan)

From figure adapted from Nature (Ramanathan, 123, 834, 1929) by Samuels (Monthly Weath. Rev., 57, 382, 1929). *gkm*, at right of figure indicates geodynamic kilometers (see Tables 698-700 for geodynamic kilometers). The tropopause is the boundary between the lower stratosphere and the upper troposphere. There have been incorporated by Samuels as indicated at the bottom of the plot certain values observed at aerological stations in the United States. The agreement is good. The differences are probably due to greater extremes found in continental America. The broken lines are based on few observations and are mainly conjectural. It is to be noted that:

(1) The stratosphere is not isothermal over any particular place; above a certain level there is a tendency for the temperature to increase with height. (2) The coldest air over the earth, about 185°K ,* lies at the height of some 17 *gkm* over the equator, a flat ring surrounded by rings of warmer air. (3) The tropopause surface has a relatively steep slope toward the pole between latitudes 30° and 50° in summer, 25° and 45° in winter. (4) The ring of lowest temperature is displaced towards the summer hemisphere. (5) There is a ridge of high temperature in the tropopause between latitudes 20° and 40°N , in summer corresponding to the ridge of high pressure at 8 km over these latitudes.

**TABLE 702.**—Seasonal Variation of Tropopause at Agra and Batavia

| | Jan. | Feb. | Mar. | Apr. | May | June | July | Aug. | Sept. | Oct. | Nov. | Dec. |
|-------------|------|------|------|------|-----|------|------|------|-------|------|------|------|
| Batavia °K. | 184 | 185 | 186 | 187 | 188 | 192 | 193 | 194 | 193 | 190 | 187 | 184 |
| Agra | 203 | 203 | 203 | 203 | 200 | 195 | 193 | 193 | 193 | 194 | 200 | 204 |

TABLE 703.—Seasonal Variation Height of Tropopause over Batavia (km)

(Bemmelen, Proc. Roy. Acad. Amsterdam, 20., 1313.)

| Jan. | Feb. | Mar. | Apr. | May | June | July | Aug. | Sept. | Oct. | Nov. | Dec. |
|------|------|------|------|------|------|------|------|-------|------|------|------|
| 17.8 | 17.6 | 17.3 | 17.0 | 16.5 | 16.2 | 16.0 | 16.5 | 17.0 | 17.4 | 17.6 | 17.7 |

* In the Figure, °A is used equivalent to °K.

THE EARTH'S ATMOSPHERE

TABLE 704.—Atmospheric Ozone

This table shows the variation of atmospheric ozone (layer about 40 to 50 km above the earth's surface), with latitude and time of the year, from measures in long-wave portions of Hartley ultra-violet band 0.230 to 0.310 μ , by Doctor Dobson and his associates (Proc. Roy. Soc. 110A, 660, 1926 and 122A, 456, 1929); prepared partly from unpublished data. Measures are in cm of ozone at n. t. p. As only one year's observations are available for most stations these figures must be regarded as approximate.

| Latitude | Jan. | Mar. | May | July | Sept. | Nov. |
|----------|-------|-------|-------|-------|-------|-------|
| 60°N. | 0.305 | 0.350 | 0.330 | 0.285 | 0.250 | 0.255 |
| 40 N. | .260 | .280 | .270 | .250 | .225 | .220 |
| 20 N. | .205 | .220 | .225 | .220 | .205 | .200 |
| 0 | .190 | .195 | .200 | .205 | .205 | .200 |
| 20 S. | .210 | .205 | .210 | .215 | .220 | .220 |
| 40 S. | .240 | .230 | .250 | .290 | .310 | .280 |

Values are very steady from day to day in equatorial regions; in temperate latitudes large variations occur (up to 0.1 cm) which are apparently associated with meteorological conditions (Dobson).

TABLE 705.—Mean Free Path, Air Molecules

(Mavis, Terr. Mag., 1928-29.)

Values of mean free path, λ , of air molecules, at different heights, for the density conditions of Table 697, col. 9.

| Z | Summer | | Winter | |
|-----|-----------------------|-----------------------|-----------------------|-----------------------|
| | Day | Night | Day | Night |
| km | | | | |
| 0 | 6.32×10^{-6} | 6.32×10^{-6} | 6.04×10^{-6} | 6.04×10^{-6} |
| 20 | 8.52×10^{-5} | 8.48×10^{-5} | 8.75×10^{-5} | 1.09×10^{-4} |
| 40 | 1.50×10^{-3} | 1.72×10^{-3} | 1.88×10^{-3} | 2.48×10^{-3} |
| 60 | 1.63×10^{-2} | 3.19×10^{-2} | 2.90×10^{-2} | 5.02×10^{-2} |
| 80 | 1.57×10^{-1} | 5.76×10^{-1} | 4.36×10^{-1} | 9.41×10^{-1} |
| 100 | 1.04 | 1.02×10^1 | 6.24 | 1.95 |
| 120 | 6.29 | 1.51×10^2 | 8.70 | 3.81×10^2 |
| 140 | 3.66×10^1 | 2.56×10^3 | 1.15×10^3 | 7.10×10^3 |
| 160 | 2.11×10^2 | 4.21×10^4 | 1.47×10^4 | 1.21×10^5 |
| 180 | 1.20×10^3 | 6.47×10^5 | 1.83×10^5 | 2.22×10^6 |
| 200 | 6.52×10^3 | 9.09×10^6 | 2.17×10^6 | 2.65×10^7 |
| 300 | 2.10×10^7 | 1.67×10^9 | 1.03×10^9 | 2.06×10^9 |
| 400 | 1.29×10^9 | | | |

ACCELERATION OF GRAVITY

For Sea-Level and Different Altitudes

Calculated from U. S. Coast and Geodetic Survey formula, p. 134 of Special Publication No. 40 of that Bureau.

$$g = 9.78030 (1 + 0.005294 \sin^2 \phi - 0.000007 \sin^2 2\phi) \text{ m}$$

$$g = 32.08783 (1 + 0.005294 \sin^2 \phi - 0.000007 \sin^2 2\phi) \text{ ft.}$$

| Latitude ϕ | $\frac{g}{\text{cm/sec}^2}$ | $\log g$ | $\frac{g}{\text{ft./sec}^2}$ | Latitude ϕ | $\frac{g}{\text{cm/sec}^2}$ | $\log g$ | $\frac{g}{\text{ft./sec}^2}$ |
|--------------------|-----------------------------|-----------|------------------------------|--------------------|-----------------------------|-----------|------------------------------|
| 0° | 978.030 | 2.0003562 | 32.0878 | 50° | 981.071 | 2.9917004 | 32.1873 |
| 5 | .078 | .0003735 | .0891 | 51 | .159 | .9917394 | .1902 |
| 10 | .195 | .0004254 | .0929 | 52 | .247 | .9917784 | .1931 |
| 12 | .262 | .0004552 | .0951 | 53 | .336 | .9918177 | .1960 |
| 14 | .340 | .0004898 | .0977 | 54 | .422 | .9918558 | .1988 |
| 15 | 978.381 | 2.0005094 | 32.0991 | 55 | 981.507 | 2.9918931 | 32.2016 |
| 16 | .430 | .0005298 | .1007 | 56 | .502 | .9919310 | .2044 |
| 17 | .480 | .0005520 | .1023 | 57 | .675 | .9919677 | .2071 |
| 18 | .532 | .0005750 | .1040 | 58 | .757 | .9920040 | .2098 |
| 19 | .585 | .0005985 | .1057 | 59 | .839 | .9920403 | .2125 |
| 20 | 978.641 | 2.0006234 | 32.1076 | 60 | 981.918 | 2.9920752 | 32.2151 |
| 21 | .701 | .0006500 | .1095 | 61 | .995 | .9921073 | .2176 |
| 22 | .763 | .0006775 | .1116 | 62 | 982.070 | .9921424 | .2201 |
| 23 | .825 | .0007050 | .1136 | 63 | .145 | .9921756 | .2225 |
| 24 | .892 | .0007348 | .1158 | 64 | .218 | .9922079 | .2249 |
| 25 | 978.960 | 2.0007649 | 32.1180 | 65 | 982.288 | 2.9922388 | 32.2272 |
| 26 | 979.030 | .0007960 | .1203 | 66 | .350 | .9922689 | .2295 |
| 27 | .101 | .0008275 | .1227 | 67 | .422 | .9922981 | .2316 |
| 28 | .175 | .0008603 | .1251 | 68 | .487 | .9923268 | .2338 |
| 29 | .251 | .0008940 | .1276 | 69 | .549 | .9923542 | .2358 |
| 30 | 979.329 | 2.0009286 | 32.1302 | 70 | 982.608 | 2.9923803 | 32.2377 |
| 31 | .407 | .0009632 | .1327 | 71 | .665 | .9924055 | .2396 |
| 32 | .487 | .0009987 | .1353 | 72 | .720 | .9924298 | .2414 |
| 33 | .500 | .0010350 | .1380 | 73 | .772 | .9924528 | .2431 |
| 34 | .652 | .9910718 | .1407 | 74 | .822 | .9924740 | .2448 |
| 35 | 979.737 | 2.0011095 | 32.1435 | 75 | 982.868 | 2.9924952 | 32.2463 |
| 36 | .822 | .9911472 | .1463 | 76 | .912 | .9925147 | .2477 |
| 37 | .908 | .9911853 | .1491 | 77 | .954 | .9925332 | .2491 |
| 38 | .993 | .9912238 | .1520 | 78 | .992 | .9925500 | .2503 |
| 39 | 980.083 | .9912628 | .1549 | 79 | 983.027 | .9925655 | .2515 |
| 40 | 980.171 | 2.0013018 | 32.1578 | 80 | 983.059 | 2.9925706 | 32.2525 |
| 41 | .261 | .9913417 | .1607 | 81 | .089 | .9925920 | .2535 |
| 42 | .350 | .9913812 | .1636 | 82 | .115 | .9926043 | .2544 |
| 43 | .440 | .9914210 | .1666 | 83 | .139 | .9926140 | .2552 |
| 44 | .531 | .9914613 | .1696 | 84 | .160 | .9926242 | .2558 |
| 45 | 980.621 | 2.0015011 | 32.1725 | 85 | 983.178 | 2.9926321 | 32.2564 |
| 46 | .711 | .9915410 | .1755 | 86 | .191 | .9926379 | .2569 |
| 47 | .802 | .9915814 | .1785 | 87 | .203 | .9926432 | .2572 |
| 48 | .892 | .9916212 | .1814 | 88 | .211 | .9926467 | .2575 |
| 49 | .981 | .9916606 | .1844 | 90 | 983.217 | .9926494 | .2577 |

To reduce $\log g$ (cm. per sec. per sec.) to $\log g$ (ft. per sec. per sec.) add $\log 0.03280833 = 8.5159842 - 10$.

The standard value of gravity, used in barometer reductions, etc., is 980.663. It was adopted by the International Committee on Weights and Measures in 1901. It corresponds nearly to latitude 45° and sea-level.

FREE-AIR CORRECTION FOR ALTITUDE

—0.0003086 cm/sec²/m when altitude is in meters.—0.00003086 ft/sec²/ft when altitude is in feet.

| Altitude. | Correction. | Altitude. | Correction. |
|-----------|-----------------------------|-----------|--------------------------------|
| 200 m. | —0.0617 cm/sec ² | 200 ft. | —0.000617 ft./sec ² |
| 300 | .0926 | 300 | .000926 |
| 400 | .1234 | 400 | .001234 |
| 500 | .1543 | 500 | .001543 |
| 600 | .1852 | 600 | .001852 |
| 700 | .2160 | 700 | .002160 |
| 800 | .2469 | 800 | .002469 |
| 900 | .2777 | 900 | .002777 |

ACCELERATION OF GRAVITY, VARIOUS WORLD STATIONS

The following more recent gravity determinations (Potsdam System) serve to show the accuracy which may be assumed for the values in Table 706, except for the three stations in the Arctic Ocean. The error in the observed gravity is probably not greater than 0.010 cm/sec², as the observations were made with the half-second invariable pendulum, using modern methods.

In recent years the Coast and Geodetic Survey has corrected the computed value of gravity for the effect of material above sea-level, the deficiency of matter in the oceans, the deficiency of density in the material below sea-level under the continents and the excess of density in the earth's crust under the ocean, in addition to the reduction for elevation. Such corrections make the computed values agree more closely with those observed. See special publication No. 40 of the U. S. Coast and Geodetic Survey entitled, "Investigations of Gravity and Isostasy," by William Bowie, 1917; also Special Publication No. 10 of same bureau entitled, "Effect of Topography and Isostatic Compensation upon the Intensity of Gravity," by J. F. Hayford and William Bowie, 1912.

| Name. | Latitude. | Elevation, meters. | Gravity, cm/sec ² | | Refer- ence. |
|--|-----------|-----------------------|------------------------------|--------------------------|-----------------|
| | | | Observed. | Reduced to sea-level. | |
| Kodaikanal, India | 10° 14' | 2336 | 977.645 | 978.366 | 1 |
| Ootacamund, India | 11 25 | 2254 | 977.735 | 978.427 | 2 |
| Madras, India | 13 4 | 6 | 978.270 | 978.281 | 2 |
| Jamestown, St. Helena | 15 55 | 10 | 978.712 | 978.715 | 2 |
| Cuttack, India | 20 20 | 28 | 978.650 | 978.663 | 2 |
| Amraoti, India | 20 56 | 342 | 978.609 | 978.714 | 2 |
| Jubbulpur, India | 23 0 | 447 | 978.710 | 978.856 | 2 |
| Gaya, India | 24 48 | 110 | 978.834 | 978.018 | 2 |
| Siliguri, India | 26 42 | 118 | 978.887 | 978.023 | 2 |
| Kuhria, India | 28 14 | 108 | 979.082 | 979.143 | 2 |
| Galveston, Texas | 29 18 | 3 | 979.272 | 979.273 | 2 |
| Rajpur, India | 30 24 | 1012 | 979.002 | 979.313 | 2 |
| Alexandria, La. | 31 19 | 24 | 979.420 | 979.436 | 2 |
| St. Georges, Bermuda | 32 21 | 2 | 979.806 | 979.807 | 2 |
| McCormick, S. C. | 33 55 | 163 | 979.624 | 979.674 | 2 |
| Shamrock, Texas | 35 13 | 708 | 979.577 | 979.795 | 2 |
| Cloudland, Tenn. | 36 6 | 1890 | 979.383 | 979.966 | 2 |
| Mount Hamilton, Cal. | 37 20 | 1282 | 979.660 | 980.056 | 2 |
| Kala-i-Chumb, Turkestan | 38 27 | 1345 | 979.462 | 979.877 | 2 |
| Denver, Col. | 39 41 | 1638 | 979.600 | 980.114 | 2 |
| Hachinohe, Japan | 40 31 | 21 | 980.350 | 980.365 | 2 |
| Chicago, Ill. | 41 47 | 182 | 980.278 | 980.334 | 2 |
| Albany, N. Y. | 42 39 | 61 | 980.344 | 980.363 | 2 |
| Florence, Italy | 43 45 | 184 | 980.401 | 980.548 | 2 |
| Minneapolis, Minn. | 44 59 | 256 | 980.597 | 980.676 | 2 |
| Simplan Hospice, Switzerland | 46 15 | 1998 | 980.202 | 980.819 | 2 |
| Fort Kent, Me. | 47 15 | 100 | 980.765 | 980.814 | 2 |
| Sandpoint, Idaho | 48 16 | 637 | 980.650 | 980.877 | 2 |
| Medicine Hat, Canada | 50 2 | 604 | 980.865 | 981.070 | 2 |
| Field, Canada | 51 24 | 1239 | 980.745 | 981.127 | 2 |
| Magleby, Denmark | 54 47 | 14 | 981.502 | 981.506 | 1 |
| Copenhagen, Denmark | 55 41 | 14 | 981.559 | 981.563 | 1 |
| St. Paul Island, Alaska | 57 7 | 10 | 981.726 | 981.729 | 2 |
| Fredericksvarn, Norway | 59 0 | 10 | 981.874 | 981.877 | 1 |
| Christiania, Norway | 59 55 | 28 | 981.027 | 981.936 | 1 |
| Ashe Inlet, Hudson Strait | 62 33 | 15 | 982.105 | 982.110 | 3 |
| St. Michael, Alaska | 63 28 | 1 | 982.192 | 982.192 | 2 |
| Hatnarfjörðr, Iceland | 64 3 | 4 | 982.266 | 982.267 | 1 |
| Niantilik, Cumberland Sound | 64 54 | 7 | 982.273 | 982.275 | 3 |
| Glaesibaer, Iceland | 65 46 | 10 | 982.342 | 982.345 | 1 |
| Sorvagen, Norway | 67 54 | 19 | 982.622 | 982.628 | 2 |
| Umanak, Greenland | 70 40 | 10 | 982.590 | 982.593 | 3 |
| Danes Island, Spitzbergen | 79 46 | 3 | 983.078 | 983.079 | 1 |
| Arctic Sea | 84 12 | 0 | 983.190 | 983.190 | 1 |
| Arctic Sea | 84 52 | 0 | 983.174 | 983.174 | 1 |
| Arctic Sea | 85 55 | 0 | 983.155 | 983.155 | 1 |

References: (1) Report 16th General Conference International Geodetic Association, London and Cambridge, 1909, 3d Vol. by Dr. E. Borrass, 1911; (2) U. S. Coast and Geodetic Survey, Special Publ. No. 40; (3) U. S. Coast and Geodetic Survey, Report for 1897, Appendix 6.*

* For references (2) and (3), values were derived from comparative experiments with invariable pendulums, the value for Washington being taken as 980.112. For the latter, Appendix 5 of the Coast and Geodetic Survey Report for 1901, and pages 25 and 241 of the 3d vol. by Dr. E. Borrass in 1911 of the Report of the 16th General Conference of the Intern. Geodetic Association, London and Cambridge, 1909. As a result of the adjustment of the net of gravity base stations throughout the world by the Central Bureau of the Intern. Geodetic Association, the value of the Washington base station was changed to 980.112.

ACCELERATION OF GRAVITY (g) IN THE UNITED STATES

The following table is abridged from one for 219 stations given on pp. 50 to 52, Special Publication No. 40, U. S. Coast and Geodetic Survey. The observed values depend on relative determinations and on adopted value of 980.112 for Washington (Coast and Geodetic Survey Office, see footnote, Table 707). There are also given terms necessary in reducing the theoretical value (Table 565) to the proper elevation (free-air) and to allow for topography and isostatic compensation by the Hayford method (see introductory note to Table 707).

To a certain extent, the greater the bulk of material below any station, the less its average density. This phenomenon is known as isostatic compensation. The depth below sea-level to which this compensation extends is about 96 km. Below this depth any mass element is subject to equal (fluid) pressure from all directions.

| Station. | Latitude. | Longitude. | Elevation, meters. | Observed g cm/sec ² | Correction. | |
|------------------------------------|-----------|------------|-----------------------|--|-----------------------------------|--|
| | | | | | Elevation, cm/sec ² | Topography and compensation, cm/sec ² |
| Key West, Fla..... | 24° 33.6' | 81° 48.4' | 1 | 978.970 | 0.000 | +0.035 |
| New Orleans, La..... | 29 57.0 | 90 4.2 | 2 | 979.324 | -.001 | +0.013 |
| Austin, Tex. university..... | 30 17.2 | 97 44.2 | 180 | 979.283 | -.058 | -.001 |
| El Paso, Tex..... | 31 46.3 | 106 29.0 | 1146 | 979.124 | -.354 | +0.001 |
| Yuma, Ariz..... | 32 43.3 | 114 37.0 | 54 | 979.529 | -.017 | -.010 |
| Charleston, S. C..... | 32 47.2 | 79 50.0 | 6 | 979.546 | -.002 | +0.016 |
| Birmingham, Ala..... | 33 30.8 | 86 48.8 | 179 | 979.536 | -.055 | +0.011 |
| Arkansas City, Ark..... | 33 36.5 | 91 12.2 | 44 | 979.600 | -.014 | +0.005 |
| Atlanta, Ga. capitol..... | 33 45.0 | 84 23.3 | 324 | 979.524 | -.100 | +0.014 |
| Beaufort, N. C..... | 34 43.1 | 76 39.8 | 1 | 979.729 | -.000 | +0.036 |
| Little Rock, Ark..... | 34 45.0 | 92 16.4 | 80 | 979.721 | -.027 | +0.001 |
| Memphis, Tenn..... | 35 8.8 | 90 3.3 | 80 | 979.740 | -.025 | +0.002 |
| Charlotte, N. C..... | 35 13.8 | 80 50.8 | 228 | 979.727 | -.070 | +0.015 |
| Las Vegas, N. Mex..... | 35 35.8 | 105 12.1 | 1060 | 979.204 | -.605 | +0.017 |
| Knoxville, Tenn..... | 35 57.7 | 83 55.5 | 280 | 979.712 | -.086 | -.001 |
| Grand Canyon, Ariz..... | 36 5.3 | 112 6.8 | 849 | 979.463 | -.262 | -.096 |
| Coudland, Tenn..... | 36 6.2 | 82 7.9 | 1800 | 979.383 | -.583 | +0.130 |
| Mount Hamilton, Cal., Obs'y | 37 20.4 | 121 38.6 | 1282 | 979.660 | -.396 | +0.120 |
| Richmond, Va..... | 37 32.2 | 77 26.1 | 30 | 979.900 | -.009 | +0.010 |
| San Francisco, Cal..... | 37 47.5 | 122 25.7 | 114 | 979.905 | -.035 | +0.045 |
| St. Louis, Mo., university..... | 38 38.0 | 90 12.2 | 154 | 980.001 | -.048 | +0.001 |
| Pike's Peak, Col..... | 38 50.3 | 105 2.0 | 4293 | 978.954 | -1.325 | +0.187 |
| Colorado Springs, Col..... | 38 50.7 | 104 49.0 | 1841 | 979.490 | -.568 | -.007 |
| Washington, D. C., Bur. St. ds. | 38 56.3 | 77 4.0 | 103 | 980.095 | -.032 | +0.012 |
| Wallace, Kans..... | 38 54.7 | 101 35.4 | 1005 | 979.755 | -.310 | .000 |
| Green River, Utah..... | 38 50.4 | 110 9.9 | 1243 | 979.636 | -.384 | -.043 |
| Cincinnati, Ohio, obs'y..... | 39 8.3 | 84 25.3 | 245 | 980.004 | -.076 | +0.002 |
| Baltimore, Md., university..... | 39 17.8 | 76 37.3 | 30 | 980.097 | -.009 | +0.006 |
| Terre Haute, Ind..... | 39 28.7 | 87 23.8 | 151 | 980.072 | -.047 | +0.001 |
| Denver, Col., university obs'y | 39 40.6 | 104 50.9 | 1638 | 979.609 | -.505 | -.015 |
| Philadelphia, Pa., university..... | 39 57.1 | 75 11.7 | 16 | 980.196 | -.005 | +0.009 |
| Wheeling, W. Va..... | 40 4.0 | 80 43.4 | 205 | 980.085 | -.063 | -.003 |
| Princeton, N. J..... | 40 21.0 | 74 39.5 | 64 | 980.178 | -.020 | +0.013 |
| Pittsburg, Pa..... | 40 27.4 | 80 0.6 | 235 | 980.118 | -.073 | .000 |
| Salt Lake City, Utah..... | 40 46.1 | 111 53.8 | 1322 | 979.803 | -.408 | -.041 |
| New York, N. Y., university..... | 40 48.5 | 73 57.7 | 38 | 980.207 | -.012 | +0.011 |
| Winnemucca, Nev..... | 40 58.4 | 117 43.8 | 1311 | 979.844 | -.404 | -.004 |
| Cleveland, Ohio..... | 41 30.4 | 81 30.6 | 210 | 980.211 | -.065 | .000 |
| Chicago, Ill., university..... | 41 47.4 | 87 30.1 | 182 | 980.278 | -.056 | +0.007 |
| Worcester, Mass..... | 42 16.5 | 71 48.5 | 170 | 980.324 | -.052 | +0.018 |
| Cambridge, Mass. observatory | 42 22.8 | 71 7.8 | 14 | 980.398 | -.004 | +0.010 |
| Ithaca, N. Y., university..... | 42 27.1 | 76 29.0 | 247 | 980.300 | -.076 | +0.005 |
| Fort Dodge, Iowa..... | 42 30.8 | 94 11.4 | 340 | 980.311 | -.105 | +0.002 |
| Grand Rapids, Mich..... | 42 58.0 | 85 40.8 | 236 | 980.372 | -.073 | +0.003 |
| Madison, Wis., university..... | 43 4.6 | 89 24.0 | 270 | 980.305 | -.083 | +0.003 |
| Boise, Idaho..... | 43 37.2 | 116 12.3 | 821 | 980.212 | -.253 | -.042 |
| Mitchell, S. Dak. university..... | 43 41.8 | 98 1.8 | 408 | 980.375 | -.120 | -.006 |
| Lancaster, N. H..... | 44 29.5 | 71 34.3 | 261 | 980.486 | -.081 | +0.007 |
| Grand Canyon, Wyo..... | 44 43.3 | 110 29.7 | 2386 | 979.809 | -.736 | +0.038 |
| Minneapolis, Minn..... | 44 58.7 | 93 13.9 | 256 | 980.597 | -.079 | -.005 |
| Calais, Me..... | 45 11.2 | 67 16.9 | 38 | 980.631 | -.012 | +0.010 |
| Miles City, Mont..... | 46 24.2 | 105 50.5 | 718 | 980.539 | -.222 | -.020 |
| Seattle, Wash. university..... | 47 39.6 | 122 18.3 | 58 | 980.733 | -.018 | -.020 |
| Pembina, N. Dak..... | 48 58.1 | 97 14.9 | 243 | 980.917 | -.075 | -.009 |

SOME PLACES OF ANOMALOUS GRAVITY

With their longitudes, latitudes, and heights above sea-level

(See Borrass, Verh. 16 allgem. Konferenz der Intern. Erdmessung, Berlin, 1911, 1914. The departures are from the values of gravity normally expected from Table 706.)

| Longitude east of Greenwich | Latitude | Altitude above sea-level m | Gravity cm/sec. ² | Departure from value of table | Place |
|-----------------------------------|----------|-------------------------------------|---------------------------------|--|------------------|
| 14 59.9 | 37 44.3 | 2943 | 979.350 | +287 | Etna |
| - 5 43.8 | -15 55.4 | 10 | 978.682 | +260 | St. Helena |
| -157 51.8 | 21 18.1 | 4 | 978.960 | +243 | Honolulu |
| 0 8 | 42 55.8 | 2877 | 979.779 | +233 | Pic du Midi |
| - 16 14.4 | 28 28.1 | 11 | 979.431 | +223 | Santa Cruz |
| 6 52 | 45 50 | 4807 | 979.401 | +188 | Mont Blanc |
| 77 27.9 | 10 13.8 | 2346 | 977.645 | +164 | Kodaikanal |
| - 61 4.5 | 14 36.0 | 4 | 978.520 | +155 | Fort de France |
| - 25 20.6 | 37 44.2 | 19 | 980.118 | +152 | Ponta Delgada |
| 10 37 | 51 48.0 | 1140 | 981.015 | +136 | |
| 15 4.7 | 37 30.2 | 43 | 980.065 | +127 | Catania |
| 13 56.6 | 40 44.5 | 35 | 980.348 | +122 | Ischia |
| 15 44.6 | 50 44.2 | 1604 | 980.761 | +119 | Schneekoppe |
| - 75 50.8 | 20 .8 | 4 | 978.756 | +115 | Santiago de Cuba |
| - 78 50.0 | - 0 14.0 | 2825 | 977.281 | +114 | Quito |
| 141 19 | 40 16 | 104 | 980.270 | +107 | Fukuoka |
| -121 38.7 | 37 20.4 | 1282 | 979.648 | +106 | Lick Observatory |
| 140 52 | 38 15 | 33 | 980.109 | +103 | |
| 15 33.4 | 38 11.5 | 5 | 980.111 | +102 | Messina |
| 10 23 | 63 25.9 | 37 | 982.114 | - 53 | |
| 6 52 | 45 55 | 1050 | 980.323 | - 57 | |
| 35 11.5 | 47 48.5 | 49 | 980.802 | - 58 | |
| 9 11.5 | 45 28.0 | 176 | 980.562 | - 58 | Milan-Brera |
| 69 17.7 | 41 19.5 | 478 | 980.082 | - 59 | Tashkent |
| 68 15.3 | 58 11.4 | 56 | 981.697 | - 59 | Tobolsk |
| 78 3.2 | 30 19.5 | 683 | 979.065 | - 77 | Dehra-Dun |
| 11 24.1 | 47 16.2 | 576 | 980.570 | - 78 | Innsbruck |
| 48 18.5 | 42 3.1 | -26 | 980.280 | - 83 | Derbent |
| 115 15.4 | -31 57.2 | 58 | 979.378 | - 88 | Perth |
| 12 2.8 | 44 13.5 | 26 | 980.441 | -102 | Forli |
| 77 54.0 | 29 52.3 | 264 | 979.131 | -106 | Roorkee |
| -122 20.1 | 47 36.6 | 74 | 980.726 | -108 | Seattle |
| 11 21.3 | 44 29.8 | 51 | 980.450 | -110 | Bologna |
| 88 44.2 | 26 31.3 | 82 | 978.924 | -118 | |

TABLE 710.—Length of Seconds Pendulum at Sea-Level and for Different Latitudes

| | Length in cm | Log. | Length in inches. | Log. | | Length in cm | Log. | Length in inches. | Log. |
|----|-----------------|----------|-------------------------|----------|----|-----------------|----------|-------------------------|----------|
| 0 | 99.0961 | 1.996056 | 39.0141 | 1.591222 | 50 | 99.4033 | 1.997401 | 39.1351 | 1.592566 |
| 5 | .1000 | .996074 | .0157 | .591239 | 55 | .4475 | .997594 | .1525 | .592760 |
| 10 | .1119 | .996126 | .0204 | .591292 | 60 | .4891 | .997776 | .1689 | .592941 |
| 15 | .1310 | .996210 | .0279 | .591375 | 65 | .5266 | .997939 | .1830 | .593104 |
| 20 | .1571 | .996324 | .0382 | .591490 | 70 | .5590 | .998081 | .1964 | .593246 |
| 25 | 99.1894 | 1.996465 | 39.0509 | 1.591631 | 75 | 99.5854 | 1.998196 | 39.2068 | 1.593361 |
| 30 | .2268 | .996629 | .0656 | .591794 | 80 | .6047 | .998280 | .2144 | .593446 |
| 35 | .2681 | .996810 | .0819 | .591976 | 85 | .6168 | .998332 | .2191 | .593498 |
| 40 | .3121 | .997002 | .0992 | .592168 | 90 | .6207 | .998350 | .2207 | .593515 |
| 45 | .3577 | .997201 | .1171 | .592367 | — | — | — | — | — |

Calculated from Table 706 by the formula $l = g/\pi^2$. For each 100 ft. of elevation subtract 0.000953 cm or 0.000375 in. or 0.000313 ft. This table could also have been computed by either of the following formulae derived from the gravity formula at the top of Table 706.

$l = 0.990961(1 + 0.005294 \sin^2 \phi - 0.000007 \sin^2 2\phi)$ meters

$l = 0.990961 + 0.005246 \sin^2 \phi - 0.000007 \sin^2 2\phi$ meters

$l = 39.014135(1 + 0.005294 \sin^2 \phi - 0.000007 \sin^2 2\phi)$ inches

$l = 39.014135 + 0.206535 \sin^2 \phi - 0.000276 \sin^2 2\phi$ inches

TABLE 711.—Miscellaneous Geodetic Data

(Replaced by Table 716)

SMITHSONIAN TABLES.

TABLE 712.—Miscellaneous Geographical Data (see page 650)

(The data on this page were compiled by R. W. Goranson, Geophysical Laboratory, Carnegie Institution, 1930.)

Land area, 148,847,000 km²; Ocean area, 361,254,000 km².

Mean elevation land above sea-level, 825 m.

Mean depth oceans, 3,680 m.

Highest known mountain, Mt. Everest, India, 87° E., 28° N., 8840 meters.

Greatest known sea-depths: Mindanao deep 10,430 meters, <10° N., 127° E.; Puerto Rico deep 8,525 meters, 19°35' N., 67°43' W.

Thermal gradient: Not well-known; from Van Orstrand's data average is 30°C per km depth but may be very different; variations observed are from 9 (Johannesburg, S. Africa) to 54 (Queensland) degrees C per km depth. Max. depth measured, 2,286 m.

TABLE 713.—Densities and Pressures of Earth's Interior

| Depth | Density | Pressure | Rock type |
|-------|-----------------------|--------------------------------------|------------------|
| 0 km | 2.7 g/cm ³ | | Granitic |
| 10 | 2.7 | $0.0027 \times 10^6 \text{ kg/cm}^2$ | |
| 30 | 3.0 | .0067 | Basaltic |
| 60 | 3.4 | .0171 | Peridotitic |
| 120 | 3.5 | .0381 | |
| 400 | 3.75 | .131 | |
| 800 | 4.0 | .30 | |
| 1200 | 4.25 | .47 | |
| 1700 | 4.4 | .68 | |
| 2000 | 5.8 | .84 | |
| 2450 | 7.25 | 1.135 | |
| 2900 | 9.0 | 1.5 | Transition layer |
| 3200 | 9.6 | 1.7 | |
| 4800 | 10.25 | 2.8 | Ni-Fe core |
| 6370 | 10.7 | 3.1 | |

(Below 800 km, due to Adams, Williamson.)

TABLE 714.—Velocities of Earthquake Waves

V_p is the velocity in km/sec. of the primary or condensational wave, V_s , of the secondary or distortional wave. Turner speaks of them as the *push* and *shake* waves.

| Layer: | V_p , km/sec. | V_s , km/sec. |
|--|---|-----------------|
| 0 to 20 ± 10 km depth, depending on locality | 5.4 to 5.6, depending on locality. May reach 6.1 | 3.2 ± 0.3 |
| 20 ± 10 to 45 ± 10 km depth, depending on locality | 6.25 to 6.75*, depending on locality | 3.5 ± 0.3* |
| Between 45 ± 10 and 2900 km depth: | | |
| 45 ± 10 | 8.0 ± 0.1 | 4.4 ± 0.2 |
| 1300 | 12.5 ± .1 | 6.9 ± .2 |
| 2400 | 13.5 ± .1 | 7.5 ± .2 |
| <2900 | 13.5 ± .1 | 7.4 ± .2 |
| Core, 2700 to 6370 km (center): | | |
| >2900 | 8.7 ± .2 | 7 |
| 6000 | 10.9 ± .2 | ? |

* B. Gutenberg, H. Jeffreys, K. Suda, A. and S. Mohorovicic, V. Conrad.

TABLE 715.—Elastic Constants of Earth's Interior

| Depth km | Bulk modulus $\times 10^{-12}$ dynes/cm ² | Rigidity $\times 10^{-12}$ dynes/cm ² | Depth km | Bulk modulus $\times 10^{-12}$ dynes/cm ² | Rigidity $\times 10^{-12}$ dynes/cm ² |
|----------|--|--|----------|--|--|
| 0 | 0.415 | 0.26 | 1200 | 3.6 ± 0.3 | 2.2 ± 0.3 |
| 0-20 | .5 ± 0.05 | .3 ± 0.5 | 1700 | 4.2 ± .3 | 2.7 ± .3 |
| 20-45 | .7 ± .1 | .4 ± .1 | 2850 | 8 ± 2 | 4.0 ± 1.0 |
| 45-120 | 1.4 ± .2 | .6 ± .1 | 2900 | 7 ± 1 ? | Smaller than at surface, perhaps zero. |
| 120-400 | 1.6 ± .2 | 1.0 ± .2 | 6370 | 12 ± 10 ? | |

MISCELLANEOUS GEOPHYSICAL DATA

Equatorial radius of earth, a , 6,378,388 m \pm 18.

Ellipticity, flattening, $(a-b)/a$, 1/297 or 0.003,367,003,4.

(Adopted at International Geodetic and Geophysical Union, 1924.)

Polar radius, b , 6,356,911.946 m.

Square of the eccentricity, e^2 , or $(a^2 - b^2)/a^2$, 0.006,722,670,0.

Quadrant of equator, 10,019,148.4 m; ditto of meridian, 10,002,288.3 m.

Area of ellipsoid, 510,100,934 km²; volume of ditto, 1,083,319,780,000 km³.

Radius of sphere having same area, 6,371,227.7 m.

Radius of sphere having same volume, 6,371,221.3 m.

Difference between geographical latitude, Φ , and geocentric latitude: Φ' .

$$\Phi - \Phi' = 695''.6635 \sin 2\Phi - 1''.1731 \sin 4\Phi + 0''.0026 \sin 6\Phi$$

$$= 695''.6635 \sin 2\Phi' + 1''.1731 \sin 4\Phi' + 0''.0026 \sin 6\Phi'$$

Newtonian constant of gravitation, G , $(6.664 \pm 0.002) \times 10^{-8}$ dyne cm²g⁻² (Heyl).

Mean density of the earth, 5.522 (Lambert).

Continental surface density of the earth, 2.67. } (Harkness.)

Mean density outer 10 miles of crust, 2.40.

Rigidity, μ , 8.6×10^{11} c.g.s. units.

Viscosity, 10.9×10^{16} c.g.s. units (comparable to steel). } Michelson, Astrophys. Journ., 39, 105, 1914.

Moments of inertia of the earth, the principal moments being taken as A , B , and C , and C the greatest (De Sitter, 1924):

$$A = B = 0.33235 \times Ea^2 \quad C = 0.33344 \times Ea^2 \quad C - A = 0.0010921 \times Ea^2$$

$$(C - A)/C = 0.0032774, \text{ from precession.}$$

Mass of the earth $= E = 5.983 \times 10^{24}$ kg; a = equatorial semidiameter.

Formulae for theoretical gravity at the surface of the ellipsoid (which is assumed to be an equipotential surface):

$$\gamma = \gamma_e (1 + 0.005288 \sin^2 \Phi - 0.000006 \sin^2 2\Phi) \text{ cm/sec}^2.$$

$$= \gamma_{45} (1 + 0.002637 \cos^2 \Phi + 0.000006 \cos^2 2\Phi) \text{ cm/sec}^2.$$

$$\gamma_e = \text{sea-level gravity at equator } \gamma_{45} = \text{sea-level gravity at lat. } 45^\circ$$

$$= 978.038 \text{ cm/sec}^2. \text{ Bowie} \quad = 980.621 \text{ cm/sec}^2. \text{ Bowie}$$

$$.052 \quad \text{Helmert} \quad .629 \quad \text{Helmert}$$

$$.052 \quad \text{Heiskanen} \quad .630 \quad \text{Heiskanen}$$

There is a systematic difference between gravity determinations over land or over sea, the latter being greater; this leads Bowie to favor a value of $978.52 \pm .008$ for the value above.

This systematic difference has led to the formula:

$g = 978.052 \{ 1 + 0.005288 \sin^2 \phi - 0.000006 \sin^2 2\phi + 0.000023 \cos^2 \phi \cos 2(\lambda + 5^\circ) \}$, where λ = east longitude. This longitude term has appeared to be indicated by the results of several observers.—Clarke, 1878, Helmert, 1915, and Heiskanen, 1928. It could be taken as indicating that the earth had three unequal axes.

Mean linear velocity of the earth in its orbit, 29.77 km/sec.

Mean linear velocity of rotation of earth at equator, 0.465 km/sec.

Rotational energy lost by tidal friction, 1.1×10^{19} erg/sec. (Jeffreys).

Angular velocity of rotation, 7.2921×10^{-6} radians/mean-solar-second.

Rotational energy, 2.160×10^{36} ergs/sec.

(See Lambert, Science, 63, 242, Mar, 5, 1926; Journ. Wash. Acad. Sci., 18, 571, 1928.)

TABLE 717.—Age of Earth, Moon, and Strata

(See The Earth, by Jeffreys, 1929.)

The age of the earth is probably from $(1.3 \text{ to } 3) \times 10^9$ years (radioactive data). Its liquefaction was probably complete within 5000 years, solidification within 15,000 years from start. The age of the earth's crust may be taken as roughly 2000 million years.

AGES OF GEOLOGIC STRATA

| | | | |
|-------------------------|------------------|-------------------------|--------------------|
| Late Oligocene | 37,000,000 yrs. | Late pre-Cambrian (?) . | 587,000,000 yrs. |
| " Cretaceous (?)... | 59,000,000 " | Upper pre-Cambrian .. | 640,000,000 " |
| Permian-Carboniferous . | 204,000,000 " | Middle pre-Cambrian .. | 987,000,000 to |
| Permian to Devonian... | 239,000,000 to | | 1,087,000,000 yrs. |
| | 374,000,000 yrs. | Lower pre-Cambrian .. | 1,257,000,000 " |

Note (Science 73 (Suppl.), 10, Mar. 13, 1931): An age of the earth of at least 2,000,000,000 years was adopted by a committee (Kovarik, Holmes, Knopf, Brown, Lane) appointed by the National Research Council; the age of the oldest rock, a uranite from Sinyaya Palo, Carelia, Russia, 1,852,000,000.

TABLE 718(a).—Geologic Age Determinations Based on the Lead Method

(Knopf, Nat. Res. Council Bull. 80, 1931.)

| Geologic age. | Mineral. | Locality. | Age (Millions of years) | |
|--|----------------|-----------------|--------------------------------------|--------------------------------------|
| | | | Based on $T_u = 4.56 \times 10^9$ | Based on $T_u = 4.56 \times 10^9$ |
| | | | $T_{Th} = 1.28 \times 10^{10}$ | $T_{Th} = 1.65 \times 10^{10}$ |
| Paleozoic; Devonian or Carboniferous. | Thorite | Norway | 224 | 310 |
| Latest Cambrian | Kolm | Sweden | 450 | |
| Pre-Cambrian | Bröggerite .. | Norway | 915 | 910 |
| Pre-Cambrian | Cleveite | Norway | 967 | 964 |
| Pre-Cambrian | Cleveite | Norway | 986 | 995 |
| Pre-Cambrian | Uraninite ... | S. Dakota | 1,465 | 1,462 |
| Pre-Cambrian | Uraninite ... | Russia | 1,852 | 1,852 |

TABLE 718(b).—The Age of the Earth

(Taken from Nat. Res. Council Bull. 80, 1931.)

Radioactive disintegration presents the only reliable measure. No trace of a beginning can yet be found. " The oldest rocks have everywhere been made from preexisting and therefore still older materials of which no other relics now survive. . . . The earth is older than the oldest granitic intrusion. It is impossible with the data available to know whether the highest reliable lead ratio so far obtained (Keystone uraninite, Black Hills, S. Dak.) represents the oldest granitic rocks. Accepting a ratio of 0.216 as an index of its age this is 1460 million years old. Before the oldest granites were intruded into the crust at least one cycle of denudation and sedimentation occurred indicated by the rocks into which the granites were injected. To the 1460 we should add perhaps 140, giving as the age some 1600 million years, as indicated by above mean. An upper limit assuming all rock lead of radioactive origin is 1600 million. The estimate of the total life of the earth (Russell, Holmes, loc. cit. p. 8) is some 3000 million years.

Strata accumulated: Max. since beginning of Cambrian from America data—260,000 ft.; 111,000 of this deposited during Paleozoic time, 86 are Mesozoic, 61,000 during Cenozoic.

TABLE 719

GEOCHEMICAL DATA

Eighty-three chemical elements (86 including Po, Ac and Ux_2) are found on the earth. Besides the eight occurring uncombined as gases, 23 may be found native, Sb, As, Bi, C, Cu, Au, Ir, Fe, Pb?, Hg, Ni, Os, Pd, Pt, Rh, Ru, Se, Ag, S, Ta?, Te, Sn?, Zn?. Combined the elements form about 1000 known mineral species. Rocks are in general aggregates of these species. Some few (e. g., quartzite, limestone, etc.) consist of one specie. We have some knowledge of the earth to a depth of 10 miles. This portion may be divided into three parts: the innermost of crystalline or plutonic rocks, the middle, of sedimentary or fragmentary rocks, the outer of clays, gravels, etc. 93% of it is solid matter, 7% liquid, and the atmosphere amounts by weight to 0.05% of it. Besides the 9 major constituents of igneous rock (see 7th col. of table) 3 are notable by their almost universal occurrence, TiO_2 , P_2O_5 , and MnO . Bo, Gl, and Sc are also widely distributed.

The density of the earth as a whole is 5.52 (Burgess); continental surface, 2.67 and outer 10 miles of crust, 2.46 (Harkness). Computed from average chemical composition: outer ten miles as a whole, 2.77; northern continents 2.73; southern, 2.70; Atlantic basin, 2.83; Pacific basin, 2.88.

Data of Geochemistry, Clarke, Bul. 616, U. S. Geological Survey, 1916; Washington, J. Franklin. Inst. 190, p. 757, 1920.

AVERAGE COMPOSITION OF KNOWN TERRESTRIAL MATTER.

| Atomic number and element. | Average composition. | | | Igneous rocks. | Average composition of lithosphere. | | | | | |
|----------------------------|----------------------|-----------------|-------------------------------|----------------|-------------------------------------|--------------------|-----------|------------------|------------------|-------------------|
| | Lithosphere, 93% | Hydrosphere, 7% | Average including atmosphere. | | Compound. | Igneous rocks, 95% | Shale, 4% | Sandstone, 0.75% | Limestone, 0.25% | Weighted average. |
| 8 O | 47.33 | 85.79 | 46.43 | 47.29 | SiO_2 | 59.09 | 58.10 | 78.33 | 5.19 | 59.77 |
| 14 Si | 27.74 | — | 27.77 | 28.02 | Al_2O_3 | 15.35 | 15.40 | 4.77 | 0.81 | 14.89 |
| 13 Al | 7.85 | — | 8.14 | 7.96 | Fe_2O_3 | 3.08 | 4.02 | 1.07 | 0.54 | 2.60 |
| 26 Fe | 4.50 | — | 5.12 | 4.56 | FeO | 3.80 | 2.45 | .30 | — | 3.39 |
| 20 Ca | 3.47 | 0.05 | 3.63 | 3.47 | MgO | 3.49 | 2.44 | 1.16 | 7.80 | 3.74 |
| 12 Mg | 2.24 | 0.14 | 2.09 | 2.29 | CaO | 5.08 | 3.11 | 5.50 | 42.57 | 4.86 |
| 11 Na | 2.46 | 1.14 | 2.85 | 2.50 | Na_2O | 3.84 | 1.30 | .45 | .05 | 3.25 |
| 19 K | 2.46 | 0.04 | 2.60 | 2.47 | K_2O | 3.13 | 3.24 | 1.31 | .33 | 2.98 |
| 1 H | 0.22 | 10.67 | 0.127 | 0.16 | H_2O | 1.14 | 5.00 | 1.63 | .77 | 2.02 |
| 22 Ti | 0.46 | — | .629 | .46 | TiO_2 | 1.05 | .65 | .25 | .06 | .77 |
| 6 C | .19 | 0.002 | .027 | .13 | ZrO_2 | 0.039 | — | — | — | .02 |
| 17 Cl | .06 | 2.07 | .055 | .063 | CO_2 | .102 | 2.63 | 5.03 | 41.54 | .70 |
| 35 Br | — | 0.008 | — | — | P_2O_5 | .30 | .17 | .08 | .04 | .28 |
| 15 P | .12 | — | .130 | .13 | S | .053 | — | — | .09 | .10 |
| 16 S | .12 | .09 | .052 | .103 | SO_3 | — | .64 | .07 | .05 | .03 |
| 56 Ba | .08 | — | .048 | .092 | Cl | .056 | — | — | .02 | .06 |
| 25 Mn | .08 | — | .096 | .078 | F | .078 | — | — | — | .09 |
| 38 Sr | .02 | — | .018 | .033 | BaO | .055 | .05 | .05 | — | .09 |
| 7 N | — | — | — | — | SrO | .022 | — | — | — | .04 |
| 9 F | .10 | — | .077 | .10 | MnO | .125 | — | — | .05 | .09 |
| etc. | .50 | — | .111 | .091 | NiO | .025 | — | — | — | .025 |
| | | | | | Cr_2O_3 | .056 | — | — | — | .05 |
| | | | | | V_2O_5 | .032 | — | — | — | .025 |
| | | | | | Li_2O | .007 | — | — | — | .01 |
| | | | | | C | — | .80 | — | — | .03 |

AVERAGE COMPOSITION OF METEORITES: The following figures give in succession the element, atomic number (bracketed), and the percentage amount in stony meteorites (Merrill, Mem. Nat. Acad. Sc. 14, p. 28, 1916). The "iron" meteorites contain a much larger percentage of iron and nickel, but there is a tendency to believe that with such meteorites the composition is altered by the volatilization or burning up of the other material in passing through the air. Note the greater abundance of elements of even atomic number (97.2 per cent).

| | | | | | | | |
|---------|-------|---------|-------|---------|-------|---------|-------|
| O (8) | 36.53 | Fe (26) | 23.32 | Si (14) | 18.03 | Mg (12) | 13.60 |
| S (16) | 1.80 | Ca (20) | 1.72 | Al (13) | 1.53 | Ni (28) | 1.52 |
| Na (11) | 1.64 | Cr (24) | 0.32 | Mn (25) | 0.23 | K (19) | 0.17 |
| C (6) | 0.15 | Co (27) | 0.12 | Ti (22) | 0.11 | P (15) | 0.11 |
| H (1) | 0.09 | Cu (29) | 0.01 | Cl (17) | 0.09 | V (23) | tr. |
| Ru (44) | tr. | Pd (46) | tr. | Pt (78) | tr. | Ir (77) | tr. |

THE EARTH'S ROTATION: ITS VARIATION

(Jeffreys, *The Earth*, Macmillan, 1929. Imes, *Changes in the Length of the Day*, Scientia, 42, 69, 1927; Brown, *Nature*, 119, 200, 1927; Journ. Roy. Astron. Soc. Canada, 24, 177, 1930.)

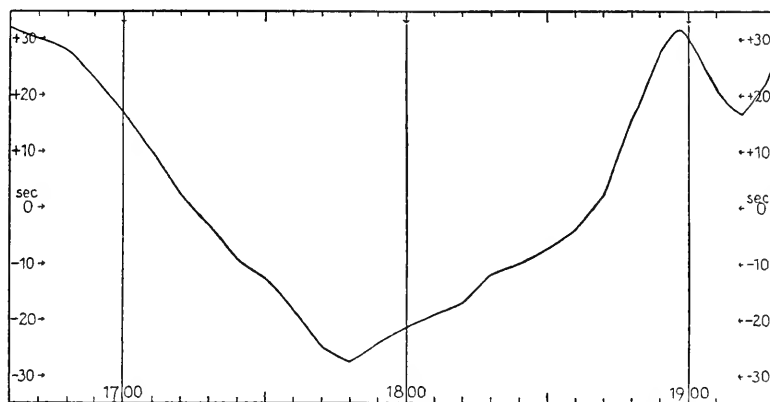
From eclipses, occultations, Fotheringham (M. N., 81, 104, 1920) deduces as the best value of the apparent solar acceleration $3.0''/(\text{century})^2$; lunar $21.6''/(\text{century})^2$. Lunar theory predicts $12.2''/(\text{century})^2$ leaving part attributable to tidal friction $9''/(\text{century})^2$.

Estimates of tidal friction losses (Jeffreys, *Philos. Trans. A* 221, 239, 1920):

| | | | | | |
|--------------|-------------------------------|---------------|-----------------------------|-------------|-------------------------------|
| Irish Sea | 0.6×10^{18} erg/sec. | So. China Sea | $- \times 10^{18}$ erg/sec. | Hudson Str. | 0.2×10^{18} erg/sec. |
| Eng. Channel | 1.1 " " | Okhotsk | 0.4 " " | Bay | — " " |
| North Sea | 1.7 " " | Bering | 15.0 " " | Fox Strait | 1.4 " " |
| Yellow Sea | 1.1 " " | Mallacca Str. | 1.1 " " | Bay Fundy | 0.4 " " |

Other contributions are small. Total for spring tides 22×10^{18} erg/sec. 1.1×10^{19} erg/sec. average, corresponding to about $7''$ secular acceleration per century per century. If Ω is earth's angular velocity of rotation, $d\Omega/dt = -2.5 \times 10^{-22}/\text{sec}^2$. $\Omega = 7.3 \times 10^{-5}/\text{sec}$. Ω changes by 10^{-5} of its amount in 3×10^{12} sec. or 10^5 years. The day *should* have lengthened by 1 sec. in 120,000 years.

The fluctuations in the earth's rate of rotation indicated by astronomical evidence are of a quite greater order of magnitude. Moreover the changes vary in sign whereas frictional effects should not. The observations come from deviations of the sun and moon from their gravitational orbits, the transits of Mercury, and eclipses of Jupiter's satellites. Changes in the speed of rotation of the earth rotation seem the only explanation. This may be due to shifts of matter within or on the earth. The following figure by Brown indicates that in 1928 the earth was about 25 sec. ahead of its average rotational motion during the last three centuries. The greatest apparent change is the loss or gain of one sec. in a whole year. (1 part in 30,000,000.)



IRREGULARITIES IN THE EARTH'S ROTATION DERIVED FROM THE MOON'S MOTION.

Tidal friction should make the earth rotate more slowly and the moon recede from the earth. The rate of dissipation of energy by friction is about 1.4×10^{19} erg/sec. The earth's rotation from this cause should have slowed by 4 hours during geologic time. The moon should continue to recede until its period of revolution and that of the earth's rotation are equal to 47 of our present days. The moon should then gradually approach the earth, ultimately coming within Roche's limit (about twice the earth's radius) breaking up possibly into a ring like Saturn's.

TABLE 721.—Tides, Sea-Level, Level Net

(Nat. Res. Council Bull. 78, 1931.)

Spring tides: When moon (new or full) is in line with sun (large).**Neap tide:** When moon is in quadrature with sun (small).

Generally two high and two low each day. Variation in heights of two high and two low = "diurnal inequality."

River type tide, steep short period graph for flood, more inclined and longer for ebb. Extreme case = "bore," tide rises so rapidly it assumes form of wall several feet high. Most famous bores, Tsientang Kiang, China; Turnagain Arm, Alaska; Severn and the Wye, England; Seine in France; Hoogly, India; Petitcodiac, Canada.

Mean sea-level (geodetic): The equipotential surface which the oceans would assume if undisturbed by the tides and effects of wind and weather. Starting with mean sea-level at any given initial point the geodesist can determine by precise spirit leveling, the equipotential surface.**Mean sea-level (geographic):** Determined by averaging actual tidal heights over a sufficient period. It is a local or geographic value. It is much disturbed by prevalent winds and local contours. Note difference between average of hourly readings (mean sea-level) and half-tide point (because of the shape of the tide height as related to time). On Atlantic coast $\frac{1}{2}$ tide level lies below mean by about 1/10 ft.; on Pacific above by 1/20 ft. Mean tide near rivers varies with rainfall. Nineteen years' observation used for full tide cycle. A fundamental level net has been connected with mean sea-level at Portland, Me., via Boston, Mass., Ft. Hamilton, N. Y., Sandy Hook and Atlantic City, N. J., Old Point Comfort and Norfolk, Va., Brunswick, Ga., Fernandina, St. Augustine, and Cedar Keys, Fla., Biloxi, Miss., Galveston, Tex., San Diego, San Pedro, San Francisco, Calif., Ft. Stevens, Oreg., and Seattle, Wash. The accuracy of high precision leveling is measured by the correction necessary to close circuits, about 0.00063 foot/mile. Mean sea-level differences:

Portland 16.94 cm higher than Ft. Hamilton.

Vancouver 10.28 cm higher than Seattle.

Galveston 24 cm higher than St. Augustine.

San Diego 40 cm higher than Galveston.

Fort Stevens 79 cm higher than San Diego.

Isthmus Panama, Pacific coast 20 cm higher than Atlantic.

Death Valley is 276 ft. (84.1 m) below sea-level, Mount Whitney 14,496 ft. (4418.4 m) above.

TABLE 722.—Magnetic and Electric Data for Sun and Earth

(Chapman, Cosmical magnetic phenomena, Nature, 124, 19, 1929.)

Sun's magnetic field too small to be measured by direct effects on earth; measured by Zeeman effect on spectrum lines.

Earth's magnetic axis inclined 12° to rotation axis.Sun's magnetic axis inclined 4° to rotation axis.

Polarity of both same relation to direction of rotation.

Earth's field rotates at same speed as nearly rigid earth.

Sun's field and magnetic axis rotate more slowly than solar surface (31, 26 days, respectively).

Earth: Polar intensity of field $\frac{2}{3}$ gauss.Sun: Estimated 50 gauss in reversing layer. Intense local fields frequent, 3000 gauss. The magnetic field of spots reverses each cycle (Proc. Astron. Soc. Pacific, 41, 136, 1929). The polarity of leading spot in a bipolar group in N. hemisphere is opposite that in the S. hemisphere—relationship reverses each new sun-spot cycle \therefore complete magnetic cycle is double sun-spot cycle.

Specific resistances: Earth

| | |
|------------------|------------------------|
| Heaviside layer, | 10^{10} |
| Dry earth, | 10^{15} to 10^{16} |
| Sea water, | 2×10^{10} |
| 200-600 m deep, | 3×10^{12} |

Sun

(Chapman loc. cit.)

| | |
|------------------|---|
| Reversing layer, | 3×10^{10} |
| Photosphere, | 10^8 , T , 10000° K. |
| Center, | 3×10^9 , T , 4×10^7 |

Drift currents in sun, + ions easterly.

Further characteristics of spots: (Milne, M. N. 90, 487, 1930; Russell.) Umbra (dark center), 800 (very small) to 80,000 km across: penumbra may reach 240,000 km. Generally short-lived. A few last several (3) rotations, very rarely 6; one in 1840, 18 months. Most occur in 2 belts 5° to 40° N. and S. latitudes, often occur in pairs (see above). Umbra temperature 4000° K. Evershed gives velocity of outburst from spot 2 km/sec.

TERRESTRIAL MAGNETISM

TABLE 723.—Magnetic Constants of the Earth

(Prepared by J. A. Fleming, Department of Terrestrial Magnetism, Carnegie Institution of Washington.)

If V be the magnetic potential of the earth, then

$$V/R = \sum c_m^n P_m^n \sin \phi \cos (m\lambda + a_m^n)$$

where R = earth's mean radius (6.37×10^8 cm), ϕ = latitude, λ = east longitude, n varies from 1 to ∞ , and m from 0 to n . The field-components of total intensity F designated, X positive towards geographic north, Y positive towards geographic east, and Z positive towards nadir, are

$$X = -(1/R) \left(\frac{\partial V}{\partial \phi} \right) = -\sum c_m^n (\partial P_m^n / \partial \phi) \cos (m\lambda + a_m^n)$$

$$Y = -(1/R \cos \phi) (\partial V / \partial \lambda) = (1/\cos \phi) \sum m c_m^n P_m^n \sin (m\lambda + a_m^n)$$

$$Z = -\sum (n+1) c_m^n P_m^n \cos (m\lambda + a_m^n)$$

L. A. Bauer (Terr. Mag., 28, 1-28, 1923) made an analysis based on the latest values of the magnetic elements, epoch 1922, between the parallels 60° N. and 60° S. He found the following for the uniform portion of the earth's X , Y , and Z magnetic systems:

| Quantity | Epoch 1922, c.g.s. units. | | |
|-----------|---------------------------|--------|----------|
| | X | Y | Z |
| M/R^3 | + .31626 | | + .30699 |
| M_p/R^3 | + .30992 | | + .30084 |
| M_e/R^3 | + .06303 | .06235 | + .06113 |

where M is the earth's moment, and M_p and M_e are its axial and equatorial components.

For the same date Bauer deduced the following values in magnetic units:

$$M = 8.04 \times 10^{25} \text{ c.g.s.} \quad M_p = 7.88 \times 10^{25} \text{ c.g.s.} \quad M_e = 1.60 \times 10^{25} \text{ c.g.s.}$$

The magnetic field of the earth approximates that of a uniformly magnetized sphere, its magnetic axis inclined to that of geographical rotation. The equivalent axis intercepts the northern hemisphere in latitude $78^\circ 32'$ N. and longitude $69^\circ 08'$ W.

The intensity of the earth's magnetic field above the surface may be expressed as a first approximation (according to Schmidt) by $F(1 - 3h/R)$ where h is the elevation and R the earth's radius; that is, for each 2 km the field diminishes by approximately 0.1 per cent while the direction is practically unchanged.

If the earth's magnetism were distributed uniformly throughout its volume, the average intensity of magnetization would be 0.074 c.g.s. The equivalent intensity of magnetization has been steadily diminishing during the past 80 years at the average annual rate of about 1/1,500 part.

A. Nippoldt (Veröff. Preus. Meteor. Inst., Berlin, no. 372, 137-143, 1930) gives the following positions based on observations:

TABLE 724.—North Magnetic Pole

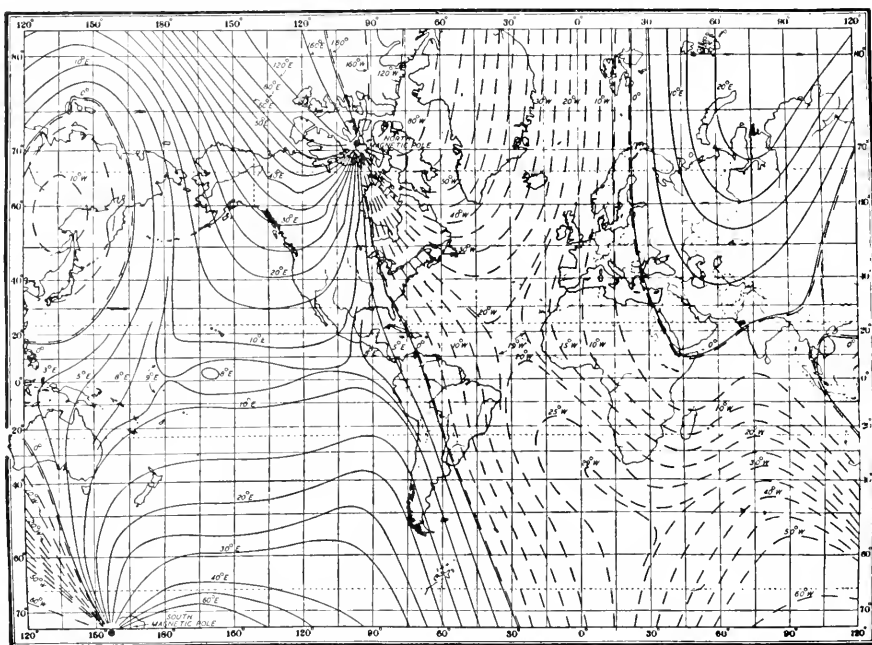
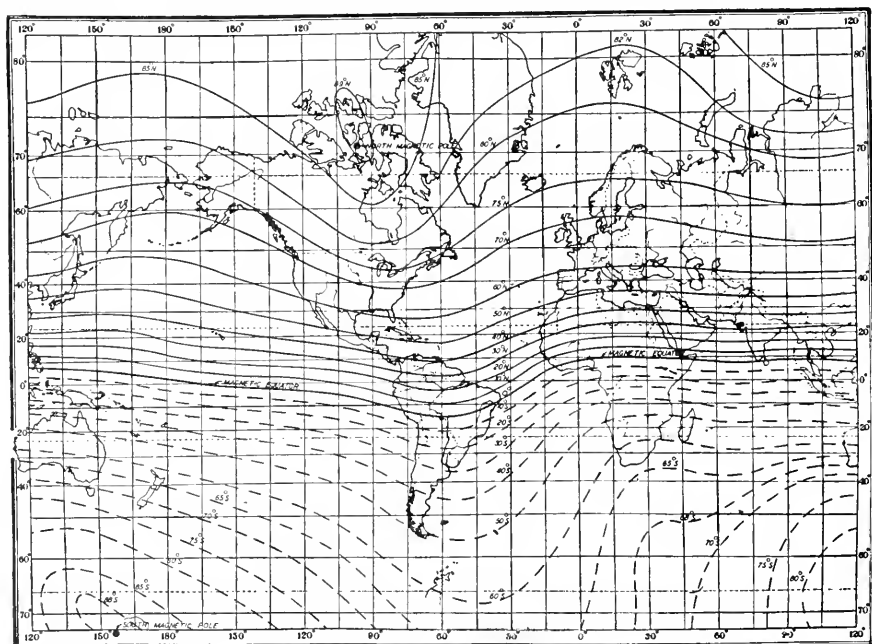
| Year. | Latitude. | | Longitude. | | Source. |
|-------|-----------|---------|------------|---------|----------|
| | $^\circ$ | $'$ | $^\circ$ | $'$ | |
| 1831 | 70 | 05.4 N. | 96 | 53.5 W. | Ross |
| 1903 | 70 | 30 N. | 95 | 30 W. | Amundsen |

TABLE 725.—South Magnetic Pole

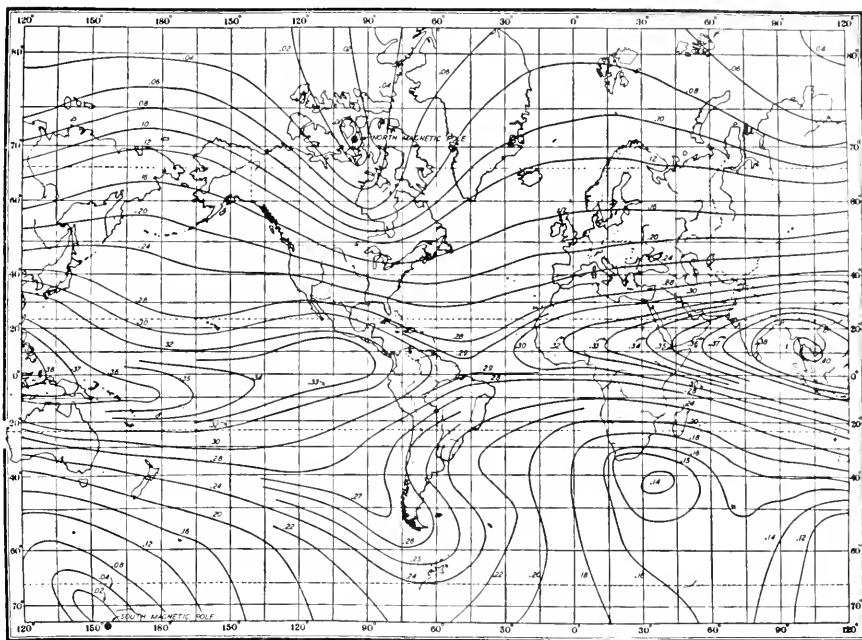
| Year. | Latitude. | | Longitude. | | Source. |
|-------|-----------|-------|------------|-------|----------------------------------|
| | $^\circ$ | $'$ | $^\circ$ | $'$ | |
| 1841 | 75 | 05 S. | 154 | 08 E. | Ross |
| 1903 | 72 | 41 S. | 156 | 25 E. | 1st British Antarctic expedition |
| 1909 | 72 | 25 S. | 154 | 00 E. | 2d British Antarctic expedition |

The magnetic poles are not diametrically opposite, each being approximately 2300 kilometers (Gutenberg, Lehrs. Geophys., 400, 1929) from the antipodes of the other. These poles are defined as the points at which magnetic lines of force are normal to the earth's surface, and are to be distinguished from the extremities of the magnetic axis derived from analysis.

TERRESTRIAL MAGNETISM

TABLE 726.—World Isogonic Lines, Epoch 1930 (Lines of Equal Declination (D))TABLE 727.—World Isoclinic Lines, Epoch 1930 (Lines of Equal Inclination (I)).
Solid Lines Indicate North End Dipping; Broken, South End Dipping

TERRESTRIAL MAGNETISM

TABLE 728.—World Isodynamic Lines, Epoch 1930 (Lines of Equal Horizontal Intensity (H))

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TABLE 730.—World Isoporic Lines for I (Lines of Equal Annual Change)
Approximate Epoch 1920-1925

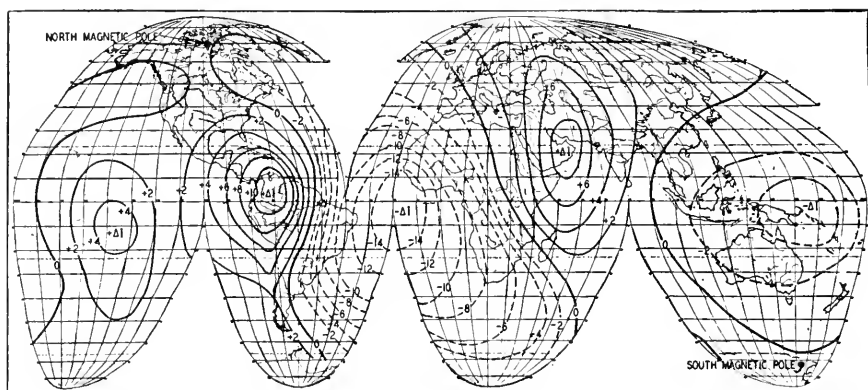
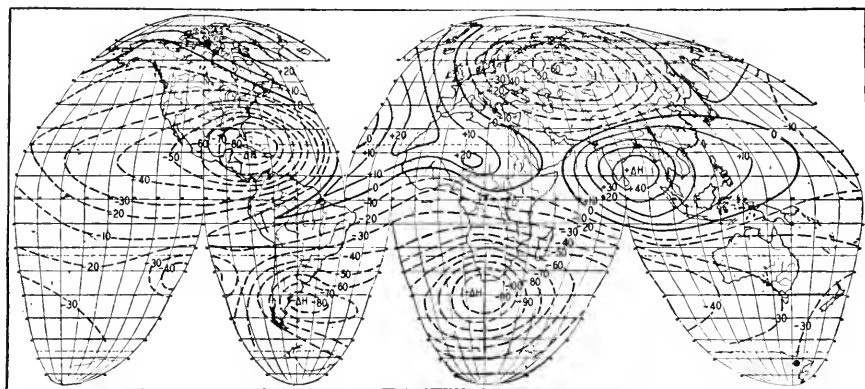


TABLE 731.—World Isoporic Lines for H (Lines of Equal Annual Change)
Approximate Epoch 1920-1925



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APPROXIMATE VALUES FOR ANNUAL RATES OF SECULAR CHANGE IN THE MAGNETIC ELEMENTS DECLINATION (D), INCLINATION (I), AND HORIZONTAL INTENSITY (H) FOR THE EPOCH 1925¹

(Because of the different intervals covered by available data and the known large accelerations in some parts, the values given for the annual secular-changes at intersections of parallels and meridians indicated are approximate except for those localities near magnetic observatories; in some cases there is great uncertainty and the values for these are enclosed in parentheses. The signs of the values given are in the algebraic sense for extrapolation considering east declination, north inclination, and horizontal intensity as positive and west declination and south inclination as negative.

TABLE 732.—Annual Change in Magnetic Declination (D)

| Latitude | Longitude east of Greenwich | | | | | | | | | | | | | | | | | |
|----------|-----------------------------|-----|-----|-----|-----|------|------|------|------|------|------|------|------|------|------|------|------|------|
| | 0° | 20° | 40° | 60° | 80° | 100° | 120° | 140° | 160° | 180° | 200° | 220° | 240° | 260° | 280° | 300° | 320° | 340° |
| 60° N. | +13 | +12 | +7 | 0 | -3 | -4 | -6 | -6 | -4 | -3 | 0 | 0 | -2 | -3 | 0 | +5 | +9 | +12 |
| 40° N. | +10 | +10 | +7 | 0 | -3 | -4 | -3 | -2 | -2 | 0 | +1 | 0 | -1 | -2 | -4 | -2 | +2 | +8 |
| 20° N. | +8 | +8 | +4 | -1 | -3 | -2 | -1 | -1 | 0 | 0 | +2 | +3 | +4 | +4 | +1 | -6 | -4 | +2 |
| 0 | +6 | +9 | +8 | -6 | -5 | -2 | 0 | +1 | +1 | +1 | +2 | +2 | +2 | +3 | 0 | -12 | -12 | -2 |
| 20° S. | +2 | +10 | +10 | -11 | -14 | -6 | +1 | +1 | +2 | +3 | +3 | +4 | +3 | +2 | -3 | -10 | -9 | -5 |
| 40° S. | 0 | +10 | +9 | -4 | -12 | -7 | 0 | +1 | +3 | +5 | +6 | +6 | +4 | +2 | -3 | -8 | -7 | -4 |
| 60° S. | +2 | +7 | +6 | +2 | 0 | -1 | -1 | +1 | +4 | +6 | +7 | +6 | +4 | +2 | +2 | -4 | -4 | -2 |

TABLE 733.—Annual Change in Magnetic Inclination (I)

| ° | ' | ' | ' | ' | ' | ' | ' | ' | ' | ' | ' | ' | ' | ' | ' | ' | ' | ' |
|--------|-----|----|----|----|----|----|----|----|----|----|------|------|------|------|------|----|-----|-----|
| 60° N. | +1 | +2 | +3 | +4 | +3 | +2 | +2 | +1 | +1 | +1 | 0 | 0 | 0 | 0 | -1 | -2 | -2 | 0 |
| 40° N. | -2 | +1 | +4 | +7 | +4 | +2 | +1 | 0 | 0 | -1 | -1 | 0 | +1 | +1 | +1 | 0 | -5 | -4 |
| 20° N. | -6 | -1 | +5 | +8 | +3 | 0 | -1 | -2 | -2 | -1 | +1 | +2 | +1 | +3 | +7 | +3 | -8 | -11 |
| 0 | -12 | -4 | +4 | +6 | +1 | -1 | -3 | -4 | -4 | -1 | +1 | +4 | +2 | +4 | +0 | +6 | -10 | -15 |
| 20° S. | -11 | -7 | -1 | +2 | +1 | -1 | -2 | -4 | -4 | -2 | 0 | +4 | +2 | +3 | +5 | 0 | -11 | -14 |
| 40° S. | -9 | -8 | -5 | -2 | +1 | 0 | -1 | -2 | -1 | -1 | 0 | +2 | +2 | +2 | +2 | -1 | -7 | -10 |
| 60° S. | -6 | -6 | -5 | -3 | 0 | 0 | 0 | 0 | -1 | 0 | (+1) | (+1) | (+1) | (+1) | (+2) | +1 | -2 | -4 |

TABLE 734.—Annual Change in Magnetic Horizontal Intensity (H)

| ° | γ | γ | γ | γ | γ | γ | γ | γ | γ | γ | γ | γ | γ | γ | γ | γ | γ | γ |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 60° N. | -10 | -30 | -45 | -60 | -50 | -40 | -25 | 0 | +10 | +10 | 0 | -10 | -10 | -5 | 0 | +10 | +20 | +5 |
| 40° N. | +5 | -10 | -25 | -35 | -35 | -20 | -10 | 0 | 0 | -10 | -15 | -20 | -25 | -30 | -40 | -25 | +5 | +25 |
| 20° N. | +10 | +15 | 0 | +5 | +35 | +30 | +15 | +10 | 0 | -20 | -30 | -35 | -45 | -60 | -90 | -60 | 0 | +20 |
| 0 | -25 | -15 | -10 | 0 | +25 | +25 | +10 | 0 | -10 | -10 | -15 | -25 | -30 | -35 | -25 | -5 | 0 | -15 |
| 20° S. | -55 | -70 | -50 | -40 | -30 | -20 | -25 | -25 | -25 | -20 | -15 | -15 | -15 | -20 | -20 | -25 | -30 | -40 |
| 40° S. | -95 | -110 | -95 | -70 | -50 | -45 | -35 | -30 | -30 | -25 | -20 | -25 | -25 | -30 | -50 | -85 | -70 | -70 |
| 60° S. | (-70) | (-80) | (-80) | (-70) | (-60) | (-35) | (-30) | (-30) | (-30) | -15 | -20 | -20 | -20 | -30 | -45 | -50 | -60 | -05 |

¹ Prepared by H. W. Fisk, of the Department of Terrestrial Magnetism, Carnegie Institution of Washington.

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TABLE 735.—World Isoporic Lines for Vertical Intensity (Lines of Equal Annual Change) Approximate Epoch 1920-1925

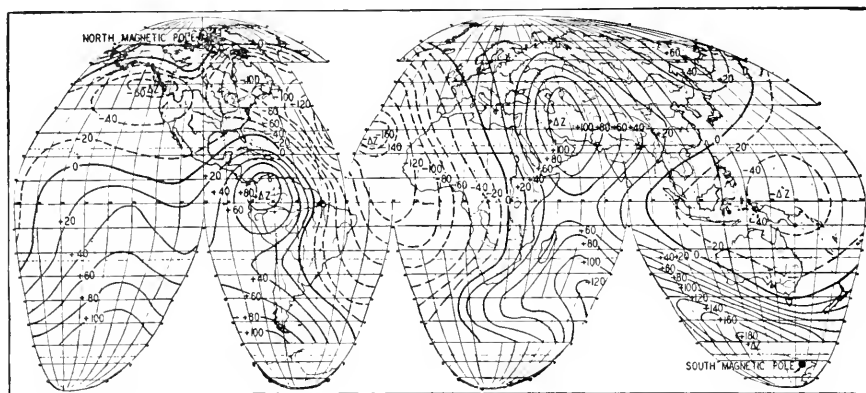
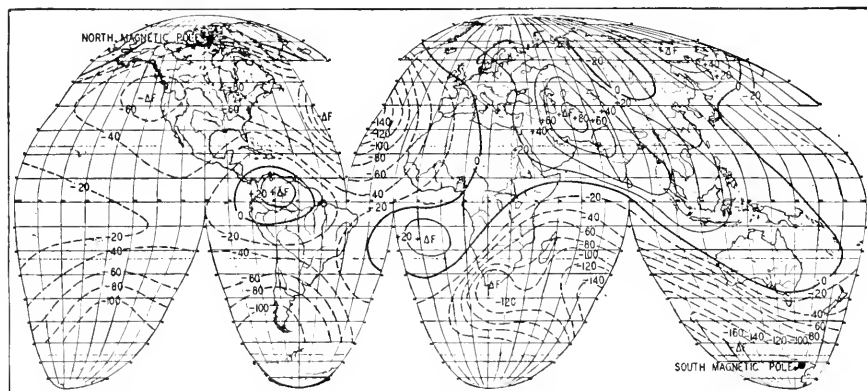


TABLE 736.—World Isoporic Lines for Total Intensity (Lines of Equal Annual Change) Approximate Epoch 1920-1925



MEAN ANNUAL VALUES OF MAGNETIC ELEMENTS AT OBSERVATORIES

In order to show the change of the annual rates of secular variation with geographical position and with time and the accelerations in those rates without unduly extending the tables, the values of the elements have been given for each fifth year beginning with 1900, and for consecutive years from 1925 or 1930. When the observatory was established subsequent to 1900, values obtained during the first year of the operation are given.

The lack of uniformity in the distribution of magnetic observatories should be taken into account. The satisfactory computation of the so-called magnetic constants of the earth, the investigation of the laws of secular variation and daily variation, the study of the manner of propagation of magnetic storms and their relation to other world-wide phenomena, require additional observatories in the southern hemisphere, specifically in Africa, and on favorably located islands in the southern Pacific and Atlantic oceans.

| Observatory | Latitude | Longitude | Year | Declination (D) | Inclination (I) | Intensity | |
|--------------------------------|----------------------|----------------------|-------------------|------------------------|-------------------------|---------------------|---------------------|
| | | | | | | Hor. (H) | Ver. (Z) |
| Matotchkin Shar Sodankylä | 73 16 N. 07 22 N. | 56 24 E. 26 39 E. | 1924 | 20 37.5 E. | 80 05.4 N. | C. R. S. .09491 | C. R. S. .54326 |
| | | | 1915 | 0 27.2 E. | 75 22.1 N. | .12853 | .49232 |
| | | | 1920 | 1 04.1 E. | 75 35.8 N. | .12638 | .49211 |
| | | | 1925 | 1 53.2 E. | 75 48.4 N. | .12440 | .49186 |
| | | | 1930 | 2 35.5 W. | 76 02.4 N. | .12228 | .49216 |
| Godhavn Lerwick | 05 15 N. 60 08 N. | 53 30 W. 1 11 W. | 1931 | 2 45.0 W. | 76 05.0 N. | .12188 | .49220 |
| | | | 1927 | 58 28.4 W. | 81 34.7 N. | .08259 | .55788 |
| | | | 1923 ^b | 15 44.5 W. | 72 33.6 N. | .14055 | .49650 |
| | | | 1925 ^b | 15 17.7 W. | 72 37.2 N. | .14021 | .49712 |
| | | | 1926 | 15 02.8 W. | 72 37.1 N. | .14018 | .49699 |
| Pavlovsk (Sloutzk) | 59 41 N. | 30 20 E. | 1930 | 14 11.2 W. | 72 41.6 N. | .14527 | .49624 |
| | | | 1931 | 13 59.6 W. | 72 42.3 N. | .14517 | .49623 |
| | | | 1900 | 0 37.6 E. | 70 37.4 N. | .16548 | .47959 |
| | | | 1905 | 0 59.8 E. | 70 36.1 N. | .16540 | .49975 |
| | | | 1910 | 1 30.0 E. | 70 41.9 N. | .16420 | .49882 |
| Lovö | 59 21 N. | 17 50 E. | 1915 | 2 06.8 E. | 70 54.9 N. | .16210 | .49850 |
| | | | 1920 | 2 42.7 E. | 71 11.2 N. | .15978 | .49807 |
| | | | 1925 | 3 25.3 E. | 71 27.1 N. | .15770 | .47900 |
| | | | 1927 | 3 42.6 E. | 71 34.8 N. | .15975 | .47068 |
| | | | 1928 | 3 50.2 E. | 71 38.6 N. | .15030 | .47106 |
| Sitka | 57 03 N. | 135 20 W. | 1929 | 3 57.4 E. | 71 42.3 N. | .15586 | .47145 |
| | | | 1928 | 3 18.6 W. | ... | .15917 | ... |
| | | | 1929 | 3 08.3 W. | 71 24.9 N. | .15584 | .49344 |
| | | | 1902 | 29 51.1 E. | 74 47.8 N. | .15441 | .50822 |
| | | | 1905 | 29 59.1 E. | 74 43.2 N. | .15494 | .50710 |
| Katharinenburg (Swerdlovsk) | 56 50 N. | 60 38 E. | 1910 | 30 16.4 E. | 74 32.2 N. | .15577 | .50312 |
| | | | 1915 | 30 23.2 E. | 74 26.5 N. | .15593 | .50608 |
| | | | 1920 | 30 28.2 E. | 74 22.1 N. | .15574 | .50662 |
| | | | 1925 | 30 27.0 E. | 74 22.0 N. | .15528 | .50501 |
| | | | 1928 | 30 20.0 E. | 74 22.4 N. | .15485 | .50537 |
| Rude Skov | 55 51 N. | 12 27 E. | 1920 | (30 17.7 E.) | (74 22.7 N.) | (.15465) | (.50307) |
| | | | 1930 | (30 15.6 E.) | (74 22.8 N.) | (.15448) | (.50253) |
| | | | 1931 | (30 13.1 E.) | (74 23.5 N.) | (.15434) | (.50190) |
| | | | 1900 | 10 04.0 E. | 70 40.3 N. | .17780 | .50718 |
| | | | 1905 | 10 27.2 E. | 70 48.3 N. | .17692 | .50810 |
| Kasan (Saimistsche) | 55 50 N. | 48 51 E. | 1910 | 10 48.7 E. | 71 00.7 N. | .17476 | .50786 |
| | | | 1915 | 11 02.6 E. | 71 21.2 N. | .17142 | .50797 |
| | | | 1920 | 11 01.9 E. | 71 42.1 N. | .16812 | .50843 |
| | | | 1925 | 11 01.0 E. | 72 03.0 N. | .16513 | .50974 |
| | | | 1927 | 10 59.5 E. | 72 12.2 N. | .16380 | .51053 |
| Eskdalemuir | 55 19 N. | 3 12 W. | 1929 | (10 57.2 E.) | (72 20.3 N.) | (.16285) | (.51145) |
| | | | 1907 | 9 48.4 W. | 68 44.0 N. | .17423 | .44765 |
| | | | 1910 | 9 27.1 W. | 68 45.0 N. | .17375 | .44638 |
| | | | 1915 | 8 42.7 W. | 68 50.6 N. | .17257 | .44591 |
| | | | 1920 | 7 55.6 W. | 68 59.6 N. | .17124 | .44506 |
| Koutchíno | 55 46 N. | 37 58 E. | 1925 | 6 57.7 W. | 60 07.2 N. | .17025 | .44031 |
| | | | 1930 | 6 00.4 W. | 60 10.0 N. | .17893 | .44747 |
| | | | 1931 | 5 50.4 W. | 60 20.5 N. | .17879 | .44717 |
| | | | 1915 ^b | 8 24.3 E. | 60 28.8 N. | .17820 | .47635 |
| | | | 1920 ^b | 8 30.6 E. ^c | 60 48.1 N. ^c | .17530 ^c | .47650 ^c |
| Eskdalemuir | 55 19 N. | 3 12 W. | 1925 | 8 57.0 E. | 70 12.2 N. | .17260 | .47951 |
| | | | 1930 | 9 06.8 E. | 70 36.3 N. | .16082 | .48238 |
| | | | 1931 | 9 07.3 E. | 70 39.1 N. | .16053 | .48279 |
| | | | 1926 | 6 25.9 E. | 68 51.1 N. | .17905 | .46442 |
| | | | 1927 | 6 36.1 E. | 68 59.5 N. | .17875 | .46545 |
| Eskdalemuir | 55 19 N. | 3 12 W. | 1908 ^d | 18 33.3 W. | 69 37.3 N. | .16830 | .45307 |
| | | | 1910 ^b | 18 23.3 W. | 69 37.8 N. | .16836 | .45343 |
| | | | 1915 | 17 35.9 W. | 69 36.9 N. | .16780 | .45173 |
| | | | 1920 | 16 49.7 W. | 69 39.5 N. | .16700 | .45062 |
| | | | 1925 | 15 48.4 W. | 69 39.3 N. | .16665 | .44943 |
| Eskdalemuir | 55 19 N. | 3 12 W. | 1930 | 14 47.1 W. | 69 43.2 N. | .16585 | .44881 |
| | | | 1931 | 14 38.4 W. | 69 43.7 N. | .16583 | .44898 |

^a See also tables for previous and intermediate years in Terr. Mag., 4, 135; 5, 128; 8, 7; 12, 175; 16, 200; 29, 131; 22, 169; 23, 191; 25, 179; 26, 147; 27, 157; 28, 140; 31, 27; 32, 27; 33, 95; and 35, 105. Unless otherwise indicated values are from continuous magnetograph records. Preliminary values, pending final reductions, are indicated by parentheses. Observatories marked by an asterisk (*) are in regions of local disturbance. ^b Values from absolute observations only. ^c No observations in February and March. ^d Absolute observations during June and July only.

MEAN ANNUAL VALUES OF MAGNETIC ELEMENTS AT OBSERVATORIES

| Observatory | Latitude | Longitude | Year | Declination (D) | Inclination (I) | Intensity | |
|-----------------------|----------|-----------|-------------------|-------------------------|-------------------------|---------------------------------|---------------------------------|
| | | | | | | Hor. (H) | Ver. (Z) |
| Meanook | 54 37 N. | 113 20 W. | 1916 ^e | 27 46.7 E. | 77 55.2 N. ^b | C. g. s. .12044 ^b | C. g. s. .60481 ^b |
| | | | 1920 | 27 38.6 E. | 77 53.6 N. ^b | .12923 ^b | .60246 ^b |
| | | | 1925 ^f | 27 10.7 E. | 77 53.8 N. ^b | .12852 ^b | .59934 ^b |
| | | | 1926 | 27 04.2 E. | 77 53.8 N. ^b | .12832 ^b | .59844 ^b |
| | | | 1928 | 26 48.5 E. | 77 54.6 N. ^b | .12790 | .59719 ^b |
| | | | 1930 | 26 39.2 E. | 77 56.1 N. ^b | .12755 | .59675 ^b |
| | | | 1900 | 18 10.9 W. | 68 50.3 N. ^b | .17312 | .44720 |
| | | | 1905 | 17 53.5 W. | 68 46.5 N. ^b | .17308 | .44718 |
| | | | 1910 | 17 20.0 W. | 68 42.2 N. ^b | .17407 | .44605 |
| | | | 1915 | 16 38.0 W. | 68 41.4 N. ^b | .17342 | .44457 |
| Stonyhurst | 53 51 N. | 2 28 W. | 1920 | 15 52.9 W. | 68 43.5 N. ^b | .17393 | .44433 |
| | | | 1925 | 14 53.4 W. | 68 42.2 N. ^b | .17203 | .44282 |
| | | | 1926 | 14 39.7 W. | 68 44.6 N. ^b | .17240 | .44316 |
| | | | 1927 | 14 26.5 W. | 68 43.5 N. ^b | .17231 | .44251 |
| | | | 1928 | 14 14.5 W. | 68 46.5 N. ^b | .17209 | .44310 |
| | | | 1929 | 14 03.1 W. | 68 46.2 N. ^b | .17201 | .44275 |
| | | | 1930 | 13 51.1 W. ^a | 68 47.8 N. ^b | .17190 ^a | .44271 ^b |
| | | | 1931 | 13 39.4 W. ^a | 68 47.3 N. ^b | .17181 ^a | .44271 ^b |
| | | | 1900 | 12 27.7 W. | 67 44.0 N. | .18095 | .44193 |
| | | | 1905 | 12 08.2 W. | 67 40.2 N. | .18169 | .44235 |
| Wilhelmshaven | 53 32 N. | 8 09 E. | 1910 | 11 37.0 W. | 67 30.5 N. | .18124 | .43773 |
| | | | 1911 | 11 28.2 W. | 67 30.7 N. ^b | .18110 | .43747 |
| | | | 1916 | 1 20.7 E. | 71 02.5 N. | .19396 | .50463 |
| | | | 1920 | 1 02.3 E. | 71 06.6 N. | .19277 | .50337 |
| | | | 1925 | 0 45.5 E. | 71 15.6 N. | .19070 | .50212 |
| | | | 1926 | 0 42.9 E. | 71 16.8 N. | .19025 | .50141 |
| | | | 1928 | 0 30.6 E. | 71 17.8 N. | .19061 | .50303 |
| | | | 1929 | 0 20.2 E. | 71 19.2 N. | .19038 | .50310 |
| | | | 1900 | 9 56.3 W. | 66 24.2 N. | .18844 | .43138 |
| | | | 1905 | 9 34.5 W. | 66 10.3 N. | .18879 | .43050 |
| Irkutsk* (Zouy) | 52 28 N. | 104 02 E. | 1910 | 9 02.9 W. | 66 10.7 N. | .18828 | .42948 |
| | | | 1915 | 8 17.1 W. | 66 25.1 N. | .18726 | .42899 |
| | | | 1920 | 7 29.4 W. | 66 33.5 N. | .18606 | .42912 |
| | | | 1925 | 6 33.0 W. | 66 39.7 N. | .18532 | .42951 |
| | | | 1926 | 6 20.6 W. | 66 42.6 N. | .18503 | .42982 |
| | | | 1927 | 6 09.1 W. | 66 44.0 N. | .18489 | .43012 |
| | | | 1928 | 5 58.2 W. | 66 45.8 N. | .18407 | .43010 |
| | | | 1929 | (5 47.8 W.) | (66 48.6 N.) | (.18442) | (.43049) |
| | | | 1908 | 9 19.2 W. | 66 16.2 N. | .18890 | .42974 |
| | | | 1910 | 9 04.3 W. | 66 16.6 N. | .18866 | .42933 |
| Potsdam | 52 23 N. | 13 04 E. | 1915 | 8 18.6 W. | 66 22.1 N. | .18765 | .42885 |
| | | | 1920 | 7 31.2 W. | 66 30.6 N. | .18645 | .42899 |
| | | | 1925 | 6 34.7 W. | 66 36.8 N. | .18570 | .42938 |
| | | | 1926 | 6 22.3 W. | 66 39.7 N. | .18539 | .42968 |
| | | | 1927 | 6 10.9 W. | 66 41.1 N. | .18526 | .42987 |
| | | | 1928 | 5 59.6 W. | 66 42.8 N. | .18505 | .42995 |
| | | | 1929 | 5 49.1 W. | 66 45.6 N. | .18480 | .43034 |
| | | | 1930 | 5 38.6 W. | 66 48.3 N. | .18456 | .43072 |
| | | | 1931 | (5 28.9 W.) | (66 49.8 N.) | (.18450) | (.43108) |
| | | | 1900 | 2 01.3 E. | 70 14.8 N. | .20129 | .56053 |
| Seddin | 52 17 N. | 13 01 E. | 1905 | 1 58.1 E. | 70 25.0 N. | .20011 | .56250 |
| | | | 1910 | 1 47.0 E. | 70 36.0 N. | .19824 | .56293 |
| | | | 1915 | 1 27.0 E. | 70 45.8 N. | .19621 | .56228 |
| | | | 1920 | 1 02.8 E. | 70 51.9 N. | .19458 | .56081 |
| | | | 1921 | 3 30.3 W. | 66 34.4 N. | .18712 | .43185 |
| | | | 1925 | 2 46.6 W. | 66 45.0 N. | .18620 | .43339 |
| | | | 1926 | 2 35.1 W. | 66 48.3 N. | .18584 | .43369 |
| | | | 1927 | 2 25.2 W. | 66 50.3 N. | .18563 | .43390 |
| | | | 1928 | 2 15.3 W. | 66 54.2 N. | .18536 | .43404 |
| | | | 1929 | 2 06.3 W. | 66 57.6 N. | .18507 | .43517 |
| Irkutsk (Old site) | 52 16 N. | 104 16 E. | 1930 | 1 49.1 W. | 67 03.2 N. | .18463 | .43608 |
| | | | 1900 | 13 50.6 W. | 66 57 N. | .18508 | .4349 |
| | | | 1905 | 13 28.5 W. | 66 48.5 N. | .18560 | .4332 |
| | | | 1910 | 12 58.2 W. | 66 46.5 N. | .18541 | .43208 |
| | | | 1915 | 12 12.5 W. | 66 48.0 N. | .18481 | .43117 |
| | | | 1920 | 11 24.2 W. | 66 51.8 N. | .18397 | .43056 |
| | | | 1925 | 10 25.4 W. | 66 53.5 N. | .18359 | .43026 |
| | | | 1926 | 10 13.1 W. | 66 55.5 N. | .18337 | .43040 |
| | | | 1927 | 10 01.0 W. | 66 55.9 N. | .18330 | .43041 |
| | | | 1928 | 9 48.8 W. | 66 57.4 N. | .18313 | .43053 |
| Swider ^b | 52 07 N. | 21 15 E. | 1929 | 9 37.3 W. | 66 58.6 N. | .18300 | .43063 |
| | | | 1930 | 9 26.3 W. | 67 00.4 N. | .18282 | .43084 |
| | | | 1931 | 9 15.7 W. | 67 00.8 N. | .18278 | .43089 |
| | | | | | | | |
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| De Bilt | 52 06 N. | 5 11 E. | | | | | |
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^e Last 4 months only. ^f No values in September. ^g 1915, New site at Zouy; values for 1915, 1920 determined from Zouy by applying corrections, *D*, +0°.5(E); *I*, -14°.7; *H*, +181°. ^b Built in 1914; World War prevented operation until 1921.

MEAN ANNUAL VALUES OF MAGNETIC ELEMENTS AT OBSERVATORIES

| Observatory | Latitude | Longitude | Year | Declination (D) | Inclination (I) | Intensity | |
|--|----------|-----------|-------------------|-------------------------|-------------------------|-----------|---------------------|
| | | | | | | Hor. (H) | Ver. (Z) |
| Valencia ^b (Cahirciveen) | 51 56 N. | 10 15 W. | 1900 | 21 30.0 W. | 68 29.6 N. | C. g. s. | C. g. s. |
| | | | 1905 | 21 10.4 W. | 68 19.2 N. | .17765 | .45082 |
| | | | 1910 | 20 44.6 W. | 68 13.0 N. | .17848 | .44893 |
| | | | 1915 | 20 03.8 W. | 68 07.9 N. ⁱ | .17892 | .44771 |
| | | | 1920 | 19 17.9 W. | 68 05.3 N. | .17869 | .44519 ⁱ |
| | | | 1925 | 18 22.4 W. | 68 00.0 N. | .17840 | .44353 |
| | | | 1930 | 17 27.6 W. | 67 59.8 N. | .17840 | .44177 |
| | | | 1931 | 17 16.8 W. | 67 58.7 N. | .17813 | .44081 |
| | | | | | | .17815 | .44048 |
| | | | 1900 | 12 47.2 W. | | | |
| | | | 1905 | 12 27.2 W. | | | |
| Bochum | 51 29 N. | 7 14 E. | 1910 | 11 56.4 W. | | | |
| | | | 1915 | 11 08.9 W. ^j | | | |
| | | | 1920 | 10 19.9 W. | | | |
| | | | 1925 | 9 25.9 W. | | | |
| | | | 1930 | 8 35.2 W. ^b | | | |
| | | | 1931 | 8 23.8 W. ^b | | | |
| | | | | | | | |
| Kew | 51 28 N. | 0 19 W. | 1900 | 16 52.7 W. | 67 11.8 N. | .18422 | .43818 |
| | | | 1905 | 16 32.9 W. | 67 03.8 N. | .18504 | .43727 |
| | | | 1910 | 16 03.2 W. | 66 58.7 N. | .18503 | .43546 |
| | | | 1915 | 15 18.4 W. | 66 56.6 N. | .18463 | .43376 |
| | | | 1920 | 14 31.0 W. | 66 57.9 N. | .18410 | .43297 |
| | | | 1924 | 13 45.1 W. | 66 56.5 N. | .18392 | .43205 |
| | | | | | | | |
| Greenwich ^k | 51 28 N. | 0 00 | 1900 | 16 29.0 W. | 67 08.8 N. | .1846 | .4380 |
| | | | 1905 | 16 09.9 W. | 66 56.3 N. | .1854 | .4355 |
| | | | 1910 | 15 41.2 W. | 66 52.8 N. | .1855 | .4344 |
| | | | 1915 | 14 56.5 W. | 66 52.0 N. | .1851 | .4333 |
| | | | 1920 | 14 08.6 W. | 66 53.6 N. | .18454 | .43249 |
| | | | 1925 | 13 09.9 W. | 66 51.4 N. | .18414 | .43080 |
| | | | 1925 ^l | 13 22.7 W. | 66 35.1 N. | .18597 | .42946 |
| | | | 1926 | 13 10.4 W. | 66 36.3 N. | .18581 | .42947 |
| | | | 1927 | 12 58.4 W. | 66 36.2 N. | .18575 | .42932 |
| | | | 1928 | 12 47.0 W. | 66 37.3 N. | .18564 | .42941 |
| Abinger | 51 11 N. | 0 23 W. | 1929 | 12 35.8 W. | 66 37.2 N. | .18555 | .42918 |
| | | | 1930 | 12 24.6 W. | 66 38.2 N. | .18542 | .42924 |
| | | | 1931 | 12 13.7 W. | 66 38.1 N. | .18544 | .42923 |
| | | | 1900 | 14 13.6 W. | 66 09.8 N. | .18952 | .42806 |
| | | | 1905 | 13 53.7 W. | 66 03.8 N. | .19069 | .42956 |
| | | | 1910 | 13 22.2 W. | 66 00.8 N. | .19028 | .42764 |
| | | | 1915 | 12 38.3 W. | 66 01.2 N. ^m | .18980 | .42690 ^m |
| Uccle | 50 48 N. | 4 21 E. | 1920 | 11 50.6 W. | 66 04.1 N. ^m | | |
| | | | 1925 | 10 52.7 W. | | | |
| | | | 1930 | 9 54.6 W. | | | |
| | | | 1901 | 8 13.6 W. ⁿ | | | |
| | | | 1905 | 7 55.0 W. | | | |
| | | | 1910 | 7 23.9 W. | | | |
| | | | 1915 | 6 37.8 W. | | | |
| | | | 1920 | 5 53.1 W. | | | |
| | | | 1925 | 4 54.3 W. | | | |
| | | | 1929 | 4 10.6 W. | | | |
| Beuthen | 50 21 N. | 18 55 E. | 1900 | 6 53.7 W. | | | |
| | | | 1905 | 6 27.9 W. | | | |
| | | | 1908 | 6 12.3 W. | | | |
| | | | 1925 | 3 37.8 W. | | | |
| Beuthen-Mikilow | 50 09 N. | 18 54 E. | 1926 | 3 26.7 W. | | | |
| | | | 1927 | 3 16.0 W. | | | |
| | | | 1928 | 3 06.2 W. | | | |
| | | | 1929 | 2 56.6 W. | | | |
| | | | 1930 | 2 46.7 W. | | | |
| | | | 1900 | 18 29.1 W. | 66 45.2 N. ^b | .18680 | .43507 ^b |
| Falmouth ^o | 50 09 N. | 5 05 W. | 1905 | 18 08.4 W. | 66 36.1 N. | .18740 | .43328 |
| | | | 1910 | 17 41.6 W. | 66 29.1 N. | .18802 | .43208 |
| | | | 1912 | 17 24.2 W. | 66 26.6 N. | .18799 | .43118 |
| | | | | | | | |
| Prague | 50 05 N. | 14 25 E. | 1902 | 8 57.6 W. | | .19903 | |
| | | | 1905 | 8 43.3 W. | | | |
| | | | 1910 | 8 09.6 W. | | | |
| | | | 1915 | 7 24.2 W. | | | |
| | | | 1920 | 6 35.6 W. | | | |
| | | | 1925 | 5 39.9 W. | | | |
| | | | 1926 | 5 27.7 W. | | | |
| Cracow | 50 04 N. | 19 58 E. | 1907 | 5 47.9 W. | | | |
| | | | 1910 | 5 27.4 W. | | | |
| | | | 1913 | 5 03.3 W. | 64 18.4 N. | | |
| | | | | | | | |

ⁱ 11 months, no observations in May. ^j Mean values from magnetograms at 8^h and 14^h daily; other values given are means of all hourly scalings. ^k Because of electric railway, superseded in 1926 by observatory at Abinger. ^l Means, 10 months, February to November. ^m Mean, 10 months, January to October. ⁿ Magnetograph for D only. ^o Discontinued in 1912.

MEAN ANNUAL VALUES OF MAGNETIC ELEMENTS AT OBSERVATORIES

| Observatory | Latitude | Longitude | Year | Declination (D) | Inclination (I) | Intensity | |
|----------------------------------|----------|-----------|-------------------|--------------------|--------------------|-----------|----------|
| | | | | | | Hor. (H) | Ver. (Z) |
| Val Joyeux | 48 40 N. | 2 01 E. | 1901 | 15 12.0 W. | 64 58.9 N. | C. g. s. | C. g. s. |
| | | | 1905 | 14 55.7 W. | 64 50.7 N. | .19680 | .42167 |
| | | | 1910 | 14 25.7 W. | 64 43.0 N. | .19728 | .42008 |
| | | | 1915 | 13 40.5 W. | 64 38.8 N. | .19738 | .41789 |
| | | | 1920 | 12 53.0 W. | 64 41.6 N. | .19715 | .41607 |
| | | | 1925 | 11 55.8 W. | 64 38.7 N. | .19666 | .41591 |
| | | | 1930 | 10 59.3 W. | 64 42.0 N. | .19650 | .41485 |
| | | | 1931 | 10 49.0 W. | 64 43.4 N. | .19631 | .41529 |
| | | | 1931 | 6 52.5 W. | 63 32.5 N. | .19636 | .41584 |
| | | | 1930 | 6 20.2 W. | 63 29.7 N. | .20314 | .40817 |
| Maisach | 48 12 N. | 11 15 E. | 1931 | 6 12.2 W. | 63 41.1 N. | .20279 | .40963 |
| | | | 1930 | 10 27.9 W. | 63 18.5 N. | .20288 | .41022 |
| | | | 1905 | 10 04.3 W. | 63 10.2 N. | .20610 | .40993 |
| Munich | 48 09 N. | 11 37 E. | 1910 | 9 31.5 W. | 63 08.4 N. | .20651 | .40828 |
| | | | 1915 | 8 49.3 W. | | .20638 | .40750 |
| | | | 1920 | 8 03.8 W. | | | |
| | | | 1925 | 7 06.7 W. | | | |
| | | | 1926 | 6 54.7 W. | | | |
| Ó-Gyalla (Pesth) | 47 53 N. | 18 12 E. | 1900 | 7 28.8 W. | | | |
| | | | 1905 | 7 03.0 W. | | .21151 | |
| | | | 1910 | 6 34.5 W. | 62 31.2 N. | .21082 | .40532 |
| | | | 1915 | 5 49.3 W. | | .20995 | |
| | | | 1918 | 5 21.1 W. | | .20917 | |
| Ó-Gyalla (Stara Dala) | 47 52 N. | 8 11 E. | 1924 | 4 18.6 W. | | | |
| | | | 1925 | 4 08.9 W. | | | |
| | | | 1926 | 3 57.2 W. | | | |
| | | | 1928 | 3 36.7 W. | | | |
| | | | 1930 | 3 18.8 W. | | | |
| Nantes ^p | 47 15 N. | 1 34 W. | 1923 | 13 23.5 W. | 63 45.8 N. | .20212 | .41009 |
| | | | 1924 | 13 11.6 W. | 63 41.6 N. | .20240 | .40940 |
| | | | 1925 | 12 59.6 W. | 63 39.0 N. | .20234 | .40850 |
| | | | 1926 | 12 48.2 W. | 63 40.3 N. | .20227 | .40876 |
| | | | 1928 | 12 23.6 W. | 63 41.2 N. | .20220 | .40886 |
| | | | 1930 | 12 04.6 W. | 63 43.3 N. | .20226 | .40965 |
| | | | 1931 | 11 54.6 W. | 63 43.3 N. | .20241 | .40995 |
| Otomari ^b | 46 30 N. | 142 46 E. | 1920 | 8 11.3 W. | | | |
| | | | 1925 | 8 25.9 W. | | | |
| | | | 1926 | 8 29.0 W. | | | |
| | | | 1927 | 8 30.8 W. | | | |
| | | | 1928 | 8 32.6 W. | | | |
| | | | 1929 | 8 34.8 W. | | | |
| | | | 1900 ^m | 4 29.9 W. | 62 18.0 N. | .21876 | .41659 |
| Odessa | 46 26 N. | 30 46 E. | 1910 | 3 35.9 W. | 62 26.9 N. | .21707 | .41606 |
| | | | 1925 | 1 36.4 W. | 63 18.9 N. | .21213 | .42206 |
| | | | 1900 | 9 25.8 W. | 60 15.9 N. | .22192 | .38852 |
| Pola | 44 52 N. | 13 51 E. | 1905 | 9 00.1 W. | 60 07.6 N. | .22227 | .38695 |
| | | | 1910 | 8 28.0 W. | 60 04.7 N. | .22194 | .38562 |
| | | | 1915 | 7 39.0 W. | 60 05.1 N. | .22166 | .38526 |
| | | | 1919 | 7 01.6 W. | 60 09.3 N. | .22111 | .38539 |
| | | | 1921 ^q | 6 38.6 W. | 60 10.3 N. | .22094 | .38537 |
| | | | 1922 | 6 28.0 W. | 60 12.8 N. | .22090 | .38591 |
| | | | 1900 | 5 28.8 W. | 74 31.6 N. | .16497 | .59594 |
| Agincourt | 43 47 N. | 79 16 W. | 1905 | 5 43.1 W. | 74 33.4 N. | .16411 | .59404 |
| | | | 1910 | 6 04.8 W. | 74 38.6 N. | .16248 | .59163 |
| | | | 1915 | 6 29.4 W. | 74 42.8 N. | .16034 | .58664 |
| | | | 1920 | 6 45.4 W. | 74 44.6 N. | .15865 | .58166 |
| | | | 1925 | 7 09.7 W. | 74 44.2 N. | .15727 | .57628 |
| | | | 1926 | 7 13.4 W. | 74 44.6 N. | .15692 | .57527 |
| | | | 1927 | 7 16.4 W. | 74 44.3 N. | .15664 | .57412 |
| | | | 1928 | 7 20.3 W. | 74 44.9 N. | .15628 | .57315 |
| | | | 1929 | 7 24.0 W. | 74 45.4 N. | .15586 | .57106 |
| | | | 1930 | 7 28.1 W. | 74 46.4 N. | .15544 | .57103 |
| Karsani (New site) | 41 50 N. | 44 42 E. | 1931 | 7 31.9 W. | 74 46.3 N. | .15520 | .57010 |
| | | | 1926 | 4 12.3 E. | 58 03.0 N. | .24604 | .39595 |
| | | | 1927 | 4 15.5 E. | 58 08.1 N. | .24673 | .39693 |
| | | | 1928 | 4 18.8 E. | 58 13.5 N. | .24646 | .39788 |
| | | | 1929 | 4 19.7 E. | 58 19.0 N. | .24627 | .39901 |
| Tiflis (Karsani, old site) | 41 43 N. | 44 48 E. | 1900 | 2 16.4 E. | 55 53.2 N. | .25594 | .37783 |
| | | | 1905 | 2 41.6 E. | 50 02.8 N. | .25451 | .37799 |
| | | | 1910 | 2 52.7 E. | 50 35.5 N. | .25343 | .37422 |
| | | | 1913 | 3 09.1 E. | 50 51.1 N. | .25217 | .37612 |

^p Electrical disturbances, especially in Z. ^q No observations during 1920 to August, 1921; values for 1921 are for four months, September to December.

MEAN ANNUAL VALUES OF MAGNETIC ELEMENTS AT OBSERVATORIES

| Observatory | Latitude | Longitude | Year | Declination (D) | Inclination (I) | Intensity | |
|--------------------------------|----------|-----------|-------------------|-------------------------|----------------------------|---------------------|---------------------|
| | | | | | | Hor. (H) | Ver. (Z) |
| Capodimonte (Naples) | 40 52 N. | 14 15 E. | 1900 | 9 10.2 W. | 56 23.8 N. | .24133 | .36318 |
| | | | 1905 | 8 45.3 W. | 56 15.0 N. | .24164 | .36164 |
| | | | 1910 | 8 13.0 W. | 56 11.9 N. | .24160 | .36088 |
| | | | 1922 | (6 25.7 W.) | (57 02.6 N.) | (.23705) | (.36563) |
| Ebro (Tortosa) | 40 49 N. | 0 31 E. | 1905 | 13 56.9 W. | 58 07.6 N. | .23230 | .37359 |
| | | | 1910 | 13 25.9 W. | 57 57.3 N. | .23251 | .37145 |
| | | | 1915 | 12 46.0 W. | 57 47.1 N. | .23277 | .36941 |
| | | | 1920 | 11 59.3 W. | 57 39.4 N. | .23291 | .36781 |
| | | | 1925 | 11 08.8 W. | 57 28.4 N. | .23367 | .36642 |
| | | | 1928 | 10 37.7 W. | 57 26.8 N. | .23386 | .36633 |
| | | | 1930 | 10 20.1 W. | 57 25.3 N. | .23401 | .36621 |
| | | | 1931 | 10 11.7 W. | 57 24.1 N. | .23415 | .36616 |
| Coimbra | 40 12 N. | 8 25 W. | 1900 | 17 20.1 W. | 59 24.3 N. | .22768 | .38506 |
| | | | 1905 | 17 01.5 W. | 59 06.4 N. | .22900 | .38273 |
| | | | 1910 | 16 34.5 W. | 58 50.1 N. | .22986 | .38006 |
| | | | 1915 | 15 57.5 W. | 58 34.7 N. | .23053 | .37734 |
| | | | 1920 | 15 21.5 W. | 58 22.8 N. | .23087 | .37496 |
| | | | 1925 | 14 38.2 W. | 58 13.0 N. | .23143 | .37368 |
| | | | 1930 ^b | 13 55.3 W. | 57 56.4 N. | .23179 | .37001 |
| | | | 1931 ^b | 13 45.5 W. | 57 52.2 N. | .23166 | .36931 |
| Baldwin ^r | 38 47 N. | 95 10 W. | 1901 | 8 21.9 E. | 68 34.5 N. | .21931 | .55800 |
| | | | 1905 | 8 27.6 E. | 68 43.0 N. | .21821 | .56016 |
| Cheltenham | 38 44 N. | 76 50 W. | 1900 ^a | 8 34.0 E. | 68 50.2 N. | .21644 | .55908 |
| | | | 1901 ^t | 5 05.0 W. | 70 21.5 N. | .20195 | .56586 |
| | | | 1905 | 5 17.8 W. | 70 25.4 N. | .20064 | .56418 |
| | | | 1910 | 5 41.4 W. | 70 35.4 N. | .19806 | .56209 |
| | | | 1915 | 6 04.0 W. | 70 46.8 N. | .19417 | .55604 |
| | | | 1920 | 6 18.5 W. | 70 55.4 N. | .19118 | .55285 |
| | | | 1925 | 6 39.4 W. | 71 06.2 N. | .18874 | .54824 |
| | | | 1930 | 6 55.9 W. | 71 08.0 N. | .18501 | .54402 |
| Athens | 37 59 N. | 23 42 E. | 1931 | (7 00.2 W.) | (71 09.3 N.) | (.18530) | (.54317) |
| | | | 1932 | (7 03.8 W.) | (71 11.2 N.) | (.18485) | (.54247) |
| | | | 1900 | 5 42.3 W. | 52 07.7 N. | .26003 | .33514 |
| | | | 1905 | 5 18.2 W. | 52 09.5 N. | .26140 | .33598 |
| San Miguel* (Ponta Delgada) | 37 46 N. | 25 39 W. | 1908 | 4 53.0 W. | 52 11.7 N. | .26197 | .33613 |
| | | | 1913 | 19 53.2 W. ^b | 60 40.5 N. ^b | .23059 ^b | .41283 ^b |
| | | | 1915 | 19 53.2 W. ^b | 60 49.5 N. ^b | .23059 ^b | .41282 ^b |
| | | | 1920 | 19 20.2 W. | 60 26.0 N. ^b | .23123 ^b | .40750 ^b |
| | | | 1925 | 18 56.5 W. | 60 03.0 N. ^b | .23256 ^b | .40378 ^b |
| | | | 1930 | 18 29.4 W. | 59 46.6 N. ^b | .23310 ^b | .40004 ^b |
| Zinsenh | 37 30 N. | 126 38 E. | 1931 | 18 23.1 W. | 59 41.1 N. ^b | .23351 ^b | .39936 ^b |
| | | | 1918 | 5 41.0 W. | | | |
| | | | 1926 | 5 57.8 W. | 53 09 N. | | |
| | | | 1927 | 5 59.1 W. | 53 08 N. | .29971 | |
| | | | 1928 | 6 00.8 W. | 53 13 N. | .29965 | |
| | | | 1929 | 6 02.4 W. | 53 16.1 N. | .29923 | .40099 |
| | | | 1930 | 6 03.8 W. | 53 08 N. | .29831 | |
| | | | 1931 | 6 03.0 W. | 53 12 N. | .29866 | |
| San Fernando | 36 28 N. | 6 12 W. | 1900 | 15 50.3 W. | 55 09.2 N. ^b | .24631 | .35378 |
| | | | 1905 | 15 40.3 W. | 54 54.2 N. ^b | .24702 | .35237 |
| | | | 1910 | 15 13.6 W. | 54 38.1 N. ^b | .24879 | .35053 |
| | | | 1915 | 14 36.0 W. | 54 10.1 N. ^b | .24978 | .34784 |
| | | | 1920 | 14 01.0 W. | 53 37.5 N. ^{b(?)} | .25021 | .33669(?) |
| | | | 1925 | 13 15.1 W. | 53 40.0 N. ^b | .25032 | .34035 |
| | | | 1930 | 12 32.8 W. | 53 20.9 N. ^b | .25072 | .33881 ^b |
| | | | 1931 | 12 25.9 W. | 53 27.0 N. ^b | .25106 | .33855 ^b |
| Kakioka ^u | 36 14 N. | 140 11 E. | 1913 | 5 10.1 W. | 49 30.0 N. | .29749 | .34851 |
| | | | 1914 | 5 12.9 W. | 49 20.8 N. | .29783 | .34868 |
| | | | 1915 | 5 15.6 W. | 49 31.3 N. | .29752 | .34863 |
| | | | 1916 | 5 17.6 W. | 49 31.7 N. | .29743 | .34859 |
| | | | 1924 | 5 31.6 W. | 49 29.5 N. | .29708 | .34774 |
| | | | 1925 | 5 34.4 W. | 49 27.8 N. | .29716 | .34749 |
| | | | 1926 | 5 36.6 W. | 49 27.7 N. | .29694 | .34721 |
| | | | 1928 | 5 40.5 W. | 49 27.0 N. | .29707 | .34721 |
| Tsingtao | 36 04 N. | 120 10 E. | 1930 | 5 42.4 W. | 49 27.9 N. | .29713 | .34746 |
| | | | 1916 | 4 04.7 W. | 52 07.1 N. | .30842 | .39644 |
| | | | 1920 | 4 12.9 W. | 52 07.0 N. | .30817 | .39610 |
| | | | 1925 | 4 22.6 W. | 52 05.9 N. | .30831 | .39603 |
| | | | 1930 | 4 32.8 W. | 52 06.8 N. | .30868 | .39673 |
| | | | 1931 | 4 32.1 W. | 52 05.1 N. | .30880 | .39646 |

^r Superseded by Tucson, October, 1909. ^a Means, 10 months, January to October. ^t Means, 6 months July to December. ^u Destroyed by earthquake, September 1, 1923; all records, January, 1917 to August, 1923, lost by fire.

MEAN ANNUAL VALUES OF MAGNETIC ELEMENTS AT OBSERVATORIES

| Observatory | Latitude | Longitude | Year | Declination (D) | Inclination (I) | Intensity | |
|--------------------------|----------|-----------|--------------------|--------------------------|---------------------------|-----------------------|-----------------------|
| | | | | | | Hor. (H) | Ver. (Z) |
| Tokyo ^v | 35 41 N. | 139 45 E. | 1900 | 4 33.7 W. | 49 00.7 N. | C. g. s. | C. g. s. |
| | | | 1905 | 4 46.2 W. | 48 56.1 N. | .29909 | .34421 |
| | | | 1910 | 4 58.2 W. | 49 07.3 N. | .29952 | .34376 |
| | | | 1912 | 5 03.4 W. | 48 53.7 N. | .30007 | .34668 |
| | | | 1910 | 5 03.4 W. | 48 53.7 N. | .29996 | .34379 |
| Tucson | 32 15 N. | 110 50 W. | 1910 | 13 25.8 E. | 59 19.6 N. | .27379 | .46160 |
| | | | 1915 | 13 42.5 E. | 59 24.7 N. | .27119 | .45879 |
| | | | 1920 | 13 48.0 E. | 59 27.6 N. | .26910 | .45610 |
| | | | 1925 | 13 45.2 E. | 59 30.3 N. | .26698 | .45334 |
| | | | 1930 | (13 47.7 E.) | (59 37.0 N.) | (.26432) | (.45081) |
| Lukiapang | 31 19 N. | 121 02 E. | 1931 | (13 49.5 E.) | (59 37.5 N.) | (.26398) | (.45038) |
| | | | 1900 | 2 58.6 W. | 45 34.8 N. | .33187 | .33879 |
| | | | 1910 | 3 01.1 W. | 45 34.3 N. | .33201 | .33883 |
| | | | 1915 | 3 13.2 W. | 45 32.1 N. | .33190 | .33839 |
| | | | 1920 | 3 21.4 W. | 45 30.7 N. | .33155 | .33773 |
| Zikawei ^w | 31 12 N. | 121 26 E. | 1925 ^b | 3 30.5 W. | 45 28.3 N. | .33160 | .33709 |
| | | | 1930 | (3 37.4 W.) ^b | (45 25.1 N.) ^b | (.33264) ^b | (.33753) ^b |
| | | | 1931 | (3 37.0 W.) ^b | (45 22.5 N.) ^b | (.33313) ^b | (.33751) ^b |
| | | | 1900 | 2 22.2 W. | 45 45.5 N. | .32859 | .33741 |
| | | | 1905 | 2 30.3 W. | 45 37.1 N. | .33009 | .33729 |
| Dehra-Dun | 30 19 N. | 78 03 E. | 1907 | 2 33.6 W. | 45 36.6 N. | .33056 | .33768 |
| | | | 1903 | 2 41.6 E. | 43 14 N. | .33430 | .31429 |
| | | | 1905 | 2 39.9 E. | 43 24.2 N. | .33383 | .31572 |
| | | | 1910 | 2 31.9 E. | 43 54.8 N. | .33257 | .32019 |
| | | | 1915 | 2 15.5 E. | 44 30.6 N. | .33083 ^x | .32522 ^x |
| Helwan | 29 52 N. | 31 20 E. | 1920 | 1 52.0 E. | 44 59.9 N. | .32951 | .32949 |
| | | | 1925 | 1 30.5 E. | 45 21.0 N. | .32948 | .33353 |
| | | | 1930 | 1 11.9 E. | 45 34.5 N. | .32963 | .33631 |
| | | | 1931 | (1 08.6 E.) | (45 35.9 N.) | (.33001) | (.33698) |
| | | | 1903 ^b | 3 21.4 W. | 40 31.2 N. | .30209 | .25819 |
| Taihokub | 25 02 N. | 121 31 E. | 1905 ^b | 3 12.7 W. | 40 36.2 N. | .30159 | .25852 |
| | | | 1910 | 2 41.5 W. | 40 40.5 N. | .30029 | .25806 |
| | | | 1915 | 2 03.0 W. | 40 54.8 N. | .30012 | .26009 |
| | | | 1920 | 1 23.7 W. | 41 12.8 N. | .29956 | .26236 |
| | | | 1925 | 0 44.8 W. | 41 25.7 N. | .29986 | .26463 |
| Barrackpore ^y | 22 46 N. | 88 22 E. | 1930 | (0 14.7 W.) ^b | (41 43.8 N.) ^b | (.30078) ^b | (.26827) ^b |
| | | | 1931 | (0 10.5 W.) ^b | (41 45.6 N.) ^b | (.30126) ^b | (.26898) ^b |
| | | | 1919 | 1 56.4 W. | | | |
| | | | 1920 | 1 57.5 W. | | | |
| | | | 1925 | 2 04.9 W. | | | |
| Au Taub. ^z | 22 27 N. | 114 03 E. | 1926 | 2 06.4 W. | | | |
| | | | 1927 | 2 07.6 W. | | | |
| | | | 1928 | 2 08.6 W. | | | |
| | | | 1929 | 2 08.6 W. | | | |
| | | | 1904 | 1 22.4 E. | 30 20.0 N. | .37224 | .21781 |
| Hong Kong ^{bb} | 22 18 N. | 114 10 E. | 1905 | 1 18.0 E. | 30 22.5 N. | .37242 | .21828 |
| | | | 1910 | 0 55.5 E. | 30 42.2 N. | .37320 | .22168 |
| | | | 1914 | 0 32.2 E. | 30 58.0 N. | .37493 | .22459 |
| | | | 1927 ^{aa} | 0 44.4 W. | | .37433 | |
| | | | 1928 | 0 43.1 W. | 30 38.8 N. | .37478 | .22207 |
| | | | 1929 | 0 43.5 W. | 30 38.7 N. | .37481 | .22206 |
| | | | 1930 | 0 43.6 W. | 30 37.3 N. | .37485 | .22187 |
| | | | 1931 | 0 43.3 W. | 30 34.4 N. | .37522 | .22164 |
| | | | 1900 | 0 18.5 E. | 31 24.7 N. | .36728 | .22430 |
| | | | 1905 | 0 08.9 E. | 31 06.6 N. | .36975 | .22317 |
| | | | 1910 | 0 00.4 E. | 30 58.8 N. | .37108 | .22279 |
| | | | 1915 | 0 11.7 W. | 30 52.2 N. | .37166 | .22217 |
| | | | 1920 | 0 20.7 W. | 30 46.4 N. | .37174 | .22137 |
| | | | 1925 | 0 30.2 W. | 30 41.0 N. | .37220 | .22085 |
| | | | 1926 | 0 32.6 W. | 30 41.6 N. | .37218 | .22002 |
| | | | 1927 | 0 34.7 W. | 30 39.1 N. | .37271 | .22085 |
| | | | 1928 | 0 33.3 W. | 30 36.3 N. | .37219 | .22016 |

^v, ^w Because of electric car disturbances, superseded in January, 1913, by Kakioka and in 1908 by Lukiapang, respectively. ^x New constants determined in 1914, used thereafter, gave for that year smaller values in *H* by 31γ and in *Z* by 31γ than those based on the constants previously used. ^y Observations discontinued Apr. 26, 1915. ^z New site of Hong Kong observatory. Corrections to reduce Au Tau values to the Hong Kong series from 1884 are +0.8 in *D* (i.e., west *D* is numerically less), -2.5 in *I*, -159γ in *H*, -101γ in *Z*. ^{aa} Means, 10 months, March to December. ^{bb} Original observing hut replaced in 1921; values from 1925 reduced to basis of original hut; superseded by Au Tau in 1927.

MEAN ANNUAL VALUES OF MAGNETIC ELEMENTS AT OBSERVATORIES

| Observatory | Latitude | Longitude | Year | Declination (D) | Inclination (I) | Intensity | |
|--|----------|-----------|--------------------|--------------------------|---------------------------|-----------------------|-----------------------|
| | | | | | | Hor. (H) | Ver. (Z) |
| | ° / | ° / | | ° / | ° / | C. G. S. | C. G. S. |
| Honolulu ^{ee} | 21 19 N. | 158 04 W. | 1902 | 9 10.1 E. | 40 14.5 N. | .29255 | .24758 |
| | | | 1905 | 9 21.7 E. | 40 05.8 N. | .29197 | .24583 |
| | | | 1910 | 9 20.7 E. | 39 47.2 N. | .29132 | .24259 |
| | | | 1915 | 9 41.6 E. | 39 20.1 N. | .29005 | .23897 |
| | | | 1920 | 9 53.2 E. | 39 25.1 N. | .28847 | .23711 |
| | | | 1925 | 10 01.9 E. | 39 25.4 N. | .28714 | .23606 |
| | | | 1930 | (10 04.4 E.) | (39 29.2 N.) | (.28542) | (.23516) |
| | | | 1931 | (10 04.3 E.) | (39 24.4 N.) | (.28551) | (.23458) |
| | | | 1932 | (10 05.0 E.) | (39 21.0 N.) | (.28545) | (.23405) |
| | | | 1910 ^b | 9 04.6 E. | | | |
| Teoloyucan | 10 45 N. | 99 11 W. | 1925 | 9 14.7 E. | | | |
| | | | 1926 | 9 18.1 E. | | | |
| | | | 1928 | 9 22.2 E. | 46 43.4 N. ^b | .31330 ^b | |
| | | | 1930 | 9 25.4 E. | 46 54.2 N. | .31199 | .33343 |
| | | | 1931 | (9 25.2 E.) ^b | (46 57.7 N.) ^b | (.31162) ^b | (.33375) ^b |
| Toungoo ^{dd} | 18 56 N. | 96 27 E. | 1905 | 0 48.4 E. | 22 58.3 N. | .38675 | .16394 |
| | | | 1910 | 0 24.0 E. | 23 02.1 N. | .38801 | .16498 |
| | | | 1915 | 0 03.1 W. | 23 07.2 N. | .39005 ^{ee} | .16653 ^{ee} |
| | | | 1920 | 0 23.7 W. | 23 07.7 N. | .39114 | .16707 |
| | | | 1921 | 0 20.8 W. | 23 07.0 N. | .39132 | .16704 |
| | | | 1922 | 0 29.7 W. | 23 07.2 N. | .39156 | .16717 |
| | | | 1923 ^{ff} | 0 31.9 W. | 23 06.1 N. | .39207 | .16725 |
| | | | 1900 | 0 24.5 E. | 21 22.4 N. | .37438 | .14652 |
| | | | 1905 | 0 14.0 E. | 21 58.5 N. | .37377 | .15083 |
| | | | 1904 | 1 09.4 E. | 22 54.7 N. | .36882 | .15588 |
| Colaba ^{gg} (Bombay) Alibag | 18 54 N. | 72 49 E. | 1905 | 1 06.5 E. | 23 01.6 N. | .36872 | .15671 |
| | | | 1910 | 0 57.7 E. | 23 39.6 N. ^{hh} | .36845 | .16143 ^{hh} |
| | | | 1915 | 0 40.6 E. | 24 21.1 N. | .36870 | .16688 |
| | | | 1920 | 0 20.2 E. | 24 54.7 N. | .36922 | .17147 |
| | | | 1925 | 0 03.4 E. | 25 18.5 N. | .37065 ⁱⁱ | .17527 ⁱⁱ |
| | | | 1930 | 0 08.0 W. | 25 30.6 N. | .37253 | .17777 |
| | | | 1931 | (0 10.5 W.) | (25 30.3 N.) | (.37323) | (.17806) |
| | | | 1927 ^{kk} | 4 21.0 W. | 52 10.6 N. | .27743 | .35737 |
| | | | 1928 | (4 35.6 W.) | (52 20.6 N.) | (.27644) | (.35824) |
| | | | 1929 | (4 41.9 W.) | (52 24.8 N.) | (.27551) | (.35795) |
| Vieques ^{ll} | 18 09 N. | 65 27 W. | 1930 | (4 59.5 W.) | (52 29.2 N.) | (.27403) | (.35813) |
| | | | 1931 | (4 58.8 W.) | (52 30.2 N.) | (.27451) | (.35780) |
| | | | 1903 ^{ll} | 1 23.2 W. | 49 10.0 N. | .29336 | .33046 |
| | | | 1905 | 1 38.3 W. | 49 17.0 N. | .29221 | .33952 |
| | | | 1910 | 2 20.6 W. | 49 52.0 N. | .28834 | .34202 |
| Antipolo | 14 36 N. | 121 10 E. | 1915 | 3 19.1 W. | 50 45.9 N. | .28279 | .34630 |
| | | | 1920 | 3 46.1 W. | 51 22.7 N. | .27827 | .34832 |
| | | | 1923 | 4 08.3 W. | 51 37.8 N. | .27632 | .34900 |
| | | | 1924 ^{ll} | 4 15.0 W. | 51 41.8 N. | .27571 | .34907 |
| | | | 1911 | 0 41.3 E. | 16 18.6 N. | .38072 | .11140 |
| | | | 1915 | 0 37.3 E. | 16 11.2 N. | .38005 | .11057 |
| | | | 1920 | 0 35.9 E. | 16 11.7 N. | .38100 | .11065 |
| | | | 1925 | 0 29.8 E. | 15 57.4 N. | .38211 | .10925 |
| | | | 1930 | (0 26.7 E.) ^b | (15 47.2 N.) ^b | (.38244) ^b | (.10812) ^b |
| | | | 1931 | (0 27.3 E.) ^b | (15 48.2 N.) ^b | (.38270) ^b | (.10832) ^b |
| Manila ^{mm} | 14 35 N. | 120 59 E. | 1900 | 0 52.1 E. | 16 15.0 N. | .38029 | .11005 |
| | | | 1904 | 0 51.4 E. | 16 00.2 N. | .38215 | .10960 |
| | | | 1903 | 0 23.4 W. | 3 05 N. | .37367 | .02013 |
| | | | 1905 | 0 31.9 W. | 3 16.7 N. | .37403 | .02142 |
| | | | 1910 | 0 55.0 W. | 3 45.2 N. | .37485 | .02459 |
| Kodaikanal ^{dd} | 10 14 N. | 77 28 E. | 1915 | 1 22.3 W. | 4 17.0 N. | .37614 ⁿⁿ | .02817 ⁿⁿ |
| | | | 1920 | 1 49.9 W. | 4 36.1 N. | .37787 | .03042 |
| | | | 1921 | 1 54.2 W. | 4 38.5 N. | .37832 | .03071 |
| | | | 1922 | 1 58.7 W. | 4 40.1 N. | .37878 | .03093 |
| | | | 1923 ^{ff} | 2 00.7 W. | 4 41.3 N. | .37950 | .03112 |

^{ee} 1913, change of earth inductors; the values with the inductor used previously appear to be 3'0 too high.
^{dd} Discontinued 1923. ^{ee} New constants determined in 1914, used thereafter, gave for that year smaller values in *H* by 18γ and in *Z* by 7γ than those based on the constants previously used. ^{ff} Means, 6 months, January to September. ^{gg} Superseded by Alibag in 1906. ^{hh} In 1909 an earth inductor replaced the Kew dip-circle; observations of 1909-11 appear to show that the old values of *I* are about 2' and of *Z* about 30γ too low. ⁱⁱ New 1923 constants make a change of -21γ and -10γ, respectively, necessary for values of *H* and *Z* given from 1904-22. ^{jj} Superseding Vieques Observatory. ^{kk} Five months means, January to May. ^{ll} Discontinued October 31, 1924; values for 1903, means for 9 months, April to December and those for 1924, 10 months, January to October. ^{mm} Superseded by Antipolo because of electric car disturbances. ⁿⁿ 1914, new constants, thereafter used, gave for that year larger values in *H* by 33γ and in *Z* by 3γ.

MEAN ANNUAL VALUES OF MAGNETIC ELEMENTS AT OBSERVATORIES

| Observatory | Latitude | Longitude | Year | Declination (D) | Inclination (I) | Intensity | |
|---------------------------------|----------|-----------|--------------------|-------------------------|------------------------------|----------------------|---------------------------|
| | | | | | | Hor. (H) | Ver. (Z) |
| | ° / | ° / | | ° / | ° / | C. G. S. | C. G. S. |
| Palau ^b | 7 20 N. | 134 29 E. | 1926 | 2 00.5 E. | | | |
| | | | 1927 | 2 00.2 E. | | | |
| | | | 1928 | 1 59.9 E. | | | |
| | | | 1929 | 1 59.8 E. | | | |
| Batavia- Buitenzorg | 6 11 S. | 106 49 E. | 1902 ^{oo} | 1 02.4 E. | 30 17.6 S. | .36717 | -.21450 |
| | | | 1905 | 0 55.0 E. | 30 39.7 S. | .36690 | -.21752 |
| | | | 1910 | 0 48.7 E. | 31 12.0 S. | .36660 | -.22202 |
| | | | 1915 | 0 46.1 E. | 31 33.6 S. | .36676 | -.22528 |
| | | | 1920 | 0 47.0 E. | 31 53.7 S. | .36706 | -.22809 |
| | | | 1925 | 0 53.2 E. | 32 06.0 S. | .36819 | -.23097 |
| | | | 1926 | 0 51.6 E. | 32 09.6 S. | .36826 | -.23154 |
| | | | 1927 ^b | 0 52.5 E. | 32 10.5 S. | .36853 | -.23185 |
| | | | 1928 | 0 53.0 E. | 32 14.9 S. | .36834 | -.23230 |
| | | | 1925 ^b | 7 59.1 E. | 1 01.5 N. | .29750 | .00532 |
| Huancayo | 12 03 S. | 75 20 W. | 1926 ^b | 7 55.5 E. | 1 09.8 N. | .29725 | .00604 |
| | | | 1927 ^b | 7 50.7 E. | 1 17.3 N. | .29737 | .00660 |
| | | | 1928 ^b | 7 47.2 E. | 1 25.8 N. | .29667 | .00741 |
| | | | 1929 ^b | 7 42.3 E. | 1 33.9 N. | .29675 | .00811 |
| Apia (Samoa) | 13 48 S. | 171 46 W. | 1930 | 7 36.5 E. | 1 42.7 N. | .29614 | .00885 |
| | | | 1905 | 9 37.0 E. | 29 11.8 S. | .35675 | -.19935 |
| | | | 1910 | 9 45.6 E. | 29 20.8 S. | .35550 | -.20110 |
| | | | 1915 | 9 57.0 E. | 29 52.8 S. | .35386 | -.20331 |
| | | | 1920 | 10 11.2 E. | 30 03.5 S. | .35273 | -.20413 |
| | | | 1925 | 10 22.8 E. | 30 07.9 S. | .35239 | -.20453 |
| | | | 1926 | 10 26.2 E. | 30 08.0 S. | .35228 | -.20449 |
| | | | 1927 | 10 29.5 E. | (30 07.0 S.) | .35223 | |
| | | | 1928 | 10 32.1 E. | | .35225 | -.20408 |
| | | | 1929 | 10 33.5 E. | | .35209 | -.20418 |
| Tananarive* ^b | 18 55 S. | 47 32 E. | 1930 | 10 34.2 E. | 30 07.9 S. | .35106 | -.20428 |
| | | | 1931 | 10 35.2 E. | 30 09.3 S. ^b | .35171 | -.20434 |
| | | | 1902 ^{pp} | 10 15.0 W. | 54 06.8 S. | .23168 | -.32021 |
| | | | 1903 | 10 07.0 W. | 54 06.5 S. | .23113 | -.31039 |
| | | | 1905 | 9 47.0 W. | 54 07.6 S. | .22940 | -.31721 |
| | | | 1910 | 9 01.3 W. | 53 58.9 S. | .22585 | -.31065 |
| | | | 1915 | 8 19.2 W. | 53 34.4 S. | .22417 | -.30376 |
| | | | 1916 | 8 14.0 W. | 53 32.8 S. | .22366 | -.30277 |
| | | | 1917 | 8 09.1 W. | 53 29.8 S. | .22306 | -.30141 |
| | | | 1918 | 8 04.2 W. | 53 23.6 S. | .22260 | -.29966 |
| Mauritius | 20 06 S. | 57 33 E. | 1910 | 8 04.6 W. | 53 21.2 S. | .22218 | -.29866 |
| | | | 1900 | 9 29.0 W. | 54 11.0 S. | .23826 | -.33015 |
| | | | 1905 | 9 11.3 W. | 53 55.5 S. | .23584 | -.32371 |
| | | | 1910 | 9 18.1 W. | 53 34.7 S. | .23327 | -.31615 |
| | | | 1915 | 9 41.1 W. ^{qq} | 53 00.2 S. ^{qq} | .23226 | -.30833 ^{qq} |
| | | | 1920 | 10 20.3 W. | 52 40.1 S. | .23093 | -.30278 |
| | | | 1925 | 11 09.6 W. | 52 31.0 S. | .22906 | -.29867 |
| | | | 1926 | 11 10.8 W. | 52 33.6 S. | .22852 | -.29849 |
| | | | 1927 | 11 32.0 W. | 52 28.8 S. ^{rr} (?) | .22804 | -.29701 ^{rr} (?) |
| | | | 1928 | 11 42.7 W. | 52 44.6 S. | .22768 | -.29934 |
| La Quiaca ^b | 22 07 S. | 65 35 W. | 1929 | 11 53.9 W. | 52 45.0 S. | .22732 | -.29893 |
| | | | 1930 | 12 05.5 W. | 52 39.6 S. | .22697 | -.29750 |
| | | | 1931 | (12 17.2 W.) | (52 38.3 S.) | (.22673) | (-.29606) |
| | | | 1920 | 6 03.3 E. | 12 39.6 S. | .26621 | -.05970 |
| Vassouras | 22 24 S. | 43 39 W. | 1925 | 5 20.1 E. | 12 28.2 S. | .26435 | -.05848 |
| | | | 1930 | 4 40.7 E. | 12 23.8 S. | .26266 | -.05774 |
| | | | 1931 | 4 31.7 E. | 12 22.8 S. | .26256 | -.05763 |
| | | | 1915 | 10 28.1 W. | 14 44.1 S. | .24700 | -.06496 |
| Rio de Janeiro ^{uu} | 22 55 S. | 43 11 W. | 1920 | 11 17.7 W. | 15 21.6 S. | .24494 | -.06728 |
| | | | 1925 | 12 03.5 W. | 16 15.6 S. | .24333 ^{ss} | -.07097 |
| | | | 1926 | 12 10.5 W. | 16 31.2 S. | .24293 | -.07205 |
| | | | 1927 | 12 10.6 W. | 16 39.7 S. | .24276 | -.07265 |
| | | | 1928 | 12 28.7 W. | 16 47.4 S. | .24221 ^{tt} | -.07398 |
| | | | 1900 | 7 55.7 W. | 13 17.1 S. | .2594 | -.0592 |
| | | | 1905 | 8 46.6 W. | 13 51.7 S. | .24777 | -.06098 |
| | | | 1910 | 9 49.0 W. | | | |

^{oo} Means, 6 months, July to December. ^{pp} Means, 8 months, May to December. ^{qq} The *D* values from 1912 to be decreased by 5'.1 for comparison with values in previous years; in 1914 an earth inductor replaced the dip circle on another pier and values are referred to dip-circle pier. ^{rr} Trouble experienced with galvanometer; earth inductor replaced by dip circle in 1928; the values of *I* and *Z* for 1927 are indicated as only approximate. ^{ss} No data in June, and only 4 days in May and 7 days in July. ^{tt} No data in January. ^{uu} Superseded about 1913 by Vassouras.

MEAN ANNUAL VALUES OF MAGNETIC ELEMENTS AT OBSERVATORIES

| Observatory | Latitude | Longitude | Year | Declination (D) | Inclination (I) | Intensity | |
|----------------------------|----------|-----------|--------------------|-------------------------|-----------------------------|---------------------|----------------------|
| | | | | | | Hor. (H) | Ver. (Z) |
| Watheroo | 30 10 S. | 115 52 E. | 1910 | 4 22.8 W. | 63 51.4 S. | c. g. s. 24925 | c. g. s. -50780 |
| | | | 1920 | 4 22.1 W. | 63 54.7 S. | 24889 | -50832 |
| | | | 1925 | 4 17.6 W. | 64 07.8 S. | 24719 | -50977 |
| | | | 1926 | 4 17.2 W. | 64 10.7 S. | 24681 | -51007 |
| | | | 1927 | 4 16.3 W. | 64 11.8 S. | 24671 | -51030 |
| | | | 1928 | 4 15.0 W. | 64 13.8 S. | 24656 | -51070 |
| | | | 1929 | 4 12.1 W. | 64 15.5 S. | 24646 | -51116 |
| | | | 1930 | 4 08.0 W. | 64 17.7 S. | 24634 | -51174 |
| | | | 1931 | 4 03.2 W. | 64 18.1 S. | 24646 | -51215 |
| | | | 1995 | 9 51.7 E. | 26 03.0 S. | 25804 | -12657 |
| Pilar | 31 40 S. | 63 53 W. | 1910 | 9 13.9 E. | 25 52.8 S. | 25694 | -12465 |
| | | | 1914 | 8 40.4 E. | 25 41.5 S. | 25597 | -12315 |
| | | | 1916 | 8 22.0 E. | 25 40.9 S. | 25495 | -12260 |
| | | | 1920 | 7 48.6 E. | 25 41.2 S. | 25297 | -12168 |
| | | | 1925 | 7 06.2 E. | 25 41.3 S. | 25012 | -12031 |
| | | | 1930 | 6 26.8 E. | 25 50.6 S. | 24695 | -11961 |
| | | | 1931 | 6 18.9 E. | 25 51.2 S. | 24661 | -11950 |
| | | | 1992 | 14 41.6 E. | 30 55.8 S. | | |
| | | | 1995 | 14 27.0 E. | 30 25.0 S. | | |
| | | | 1999 | 13 57.9 E. | 29 57.2 S. | | |
| Melbourne ^{b, vv} | 37 50 S. | 144 58 E. | 1916 | 8 06.7 E. | 67 48.0 S. | 22998 | -56397 |
| | | | 1919 | 8 01.0 E. | 67 53.8 S. | 22895 | -56374 |
| Toolangi | 37 32 S. | 145 28 E. | 1920 ^b | 8 00.8 E. | 67 55.1 S. | 22874 | -56384 |
| | | | 1925 | 8 10.4 E. | 67 44.5 S. | 22948 | -56071 |
| | | | 1930 ^b | 8 21.6 E. | 67 52.4 S. | 22851 | -56198 |
| | | | 1931 ^b | (8 24.5 E.) | (67 51.1 S.) | (22890) | (-56232) |
| Amberley | 43 10 S. | 172 44 E. | 1929 | 17 45.0 E. | 67 57.8 S. | 22305 | -55252 |
| | | | 1930 | 17 51.0 E. | 67 58.4 S. | 22351 | -55246 |
| Christchurch ^{ww} | 43 32 S. | 172 37 E. | 1902 | 16 15.1 E. | 67 40.8 S. | 22694 | -55277 |
| | | | 1905 | 16 25.4 E. | 67 45.8 S. | 22628 | -55348 |
| | | | 1910 | 16 37.5 E. | 67 54.8 S. | 22515 | -55485 |
| | | | 1914 | 16 44.8 E. | 67 59.8 S. | 22414 | -55465 |
| | | | 1917 | 16 53.0 E. | 68 04.8 S. | 22328 | -55486 |
| | | | 1920 | 17 01.7 E. | 68 09.2 S. | 22261 | -55525 |
| | | | 1925 | 17 21.1 E. | 68 14.2 S. | 22166 | -55522 |
| | | | 1930 | 17 48.3 E. | 68 18.3 S. | 22108 | -55570 |
| New Year's Island | 54 30 S. | 64 09 W. | 1902 ^{xx} | 15 57.3 E. | 50 13.8 S. | 27306 | -32808 |
| | | | 1905 | 15 45.7 E. | 50 06.6 S. | 27196 | -32536 |
| | | | 1910 | 15 26.3 E. | | 27040 | -32114 ^{xx} |
| | | | 1915 | 15 06.6 E. | 49 41.6 S. | 26821 | -31619 |
| Orcadas | 60 43 S. | 44 47 W. | 1916 | 15 02.4 E. | 49 39.4 S. | 26771 | -31520 |
| | | | 1905 | 5 16.6 E. ^{yy} | 54 31.0 S. ^{yy, b} | 25667 ^{zz} | |
| | | | 1909 | 4 56.6 E. | 54 27.4 S. ^b | 25436 | |
| | | | 1912 | 4 46.5 E. | 54 26.0 S. ^b | 25343 | -3544 ^b |

^{vv} Superseded in 1920 by Toolangi. ^{ww} January 1, 1923, the variation observatory was transferred to Amberley but all results subsequently are referred to basis of the old station at Christchurch. ^{xx} Means, 10 months, March to December in 1902 for all elements, and 9 months, January to September in 1910 for Z. ^{yy} Mean, 11 months, February to December. ^{zz} Mean, 10 months, March to December.

TABLE 738.—Bibliography

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SECULAR CHANGE OF MAGNETIC DECLINATION

Changes in the magnetic declination between 1820, or the date of the earliest observations, and 1930, based on tables in "Magnetic Declination in the United States in 1925" published by the U. S. Coast and Geodetic Survey (Special Publication No. 126) in 1926.

| State | Lat. | Long. | 1820 | 1830 | 1840 | 1850 | 1860 | 1870 | 1880 | 1890 | 1900 | 1910 | 1920 | 1930 |
|--------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| At sea | 44 | 68 | 12.2W | 13.0W | 13.8W | 14.6W | 15.4W | 15.8W | 16.2W | 16.5W | 16.8W | 17.5W | 18.3W | 19.1W |
| Me. | 46 | 68 | 14.8W | 15.0W | 16.4W | 17.3W | 18.0W | 18.5W | 18.9W | 19.0W | 19.3W | 20.0W | 20.7W | 21.3W |
| Canada | 48 | 68 | 17.6W | 18.5W | 19.4W | 20.2W | 21.0W | 21.5W | 21.8W | 21.9W | 22.1W | 22.7W | 23.2W | 23.8W |
| At sea | 40 | 72 | 5.0W | 5.5W | 6.2W | 6.6W | 7.0W | 8.2W | 8.7W | 9.2W | 9.7W | 10.6W | 11.3W | 12.2W |
| Conn. | 42 | 72 | 6.5W | 7.0W | 7.7W | 8.4W | 9.1W | 9.7W | 10.3W | 10.8W | 11.3W | 12.1W | 12.9W | 13.7W |
| N. H. | 44 | 72 | 8.3W | 8.0W | 9.6W | 10.4W | 11.1W | 11.7W | 12.3W | 12.7W | 13.2W | 14.0W | 14.8W | 15.7W |
| Canada | 46 | 72 | 10.0W | 11.5W | 12.2W | 13.0W | 13.7W | 14.3W | 15.0W | 15.3W | 15.8W | 16.6W | 17.3W | 18.0W |
| At sea | 34 | 76 | 1.2E | 0.6E | 0.4E | 0.2W | 0.8W | 1.4W | 2.0W | 2.6W | 3.1W | 3.7W | 4.2W | 4.6W |
| N. C. | 36 | 76 | 0.2E | 0.2W | 0.6W | 1.2W | 1.8W | 2.5W | 3.1W | 3.6W | 4.2W | 4.8W | 5.4W | 5.9W |
| Md. | 38 | 76 | 0.4W | 0.8W | 1.3W | 1.9W | 2.5W | 3.2W | 3.8W | 4.4W | 5.0W | 5.6W | 6.3W | 6.9W |
| Pa. | 40 | 76 | 1.6W | 2.0W | 2.5W | 3.1W | 3.7W | 4.4W | 5.0W | 5.6W | 6.2W | 7.0W | 7.6W | 8.4W |
| Pa. | 42 | 76 | 3.4W | 3.8W | 4.3W | 4.9W | 5.5W | 6.2W | 7.0W | 7.5W | 8.1W | 8.9W | 9.6W | 10.4W |
| N. Y. | 44 | 76 | 4.7W | 5.1W | 5.7W | 6.3W | 7.0W | 7.6W | 8.5W | 9.0W | 9.6W | 10.4W | 11.2W | 12.0W |
| At sea | 26 | 80 | 5.4E | 5.1E | 4.7E | 4.2E | 3.7E | 3.1E | 2.6E | 2.0E | 1.5E | 1.3E | 1.4E | 1.5E |
| At sea | 28 | 80 | 4.9E | 4.6E | 4.3E | 3.8E | 3.3E | 2.7E | 2.1E | 1.5E | 1.0E | 0.8E | 0.7E | 0.8E |
| At sea | 30 | 80 | 4.6E | 4.3E | 3.9E | 3.5E | 2.9E | 2.3E | 1.7E | 1.1E | 0.6E | 0.3E | 0.2E | 0.1E |
| At sea | 32 | 80 | 4.0E | 3.8E | 3.4E | 3.0E | 2.4E | 1.8E | 1.2E | 0.6E | 0.0 | 0.3W | 0.5W | 0.7W |
| S. C. | 34 | 80 | 3.7E | 3.4E | 3.1E | 2.6E | 2.0E | 1.4E | 0.8E | 0.2E | 0.4W | 0.8W | 1.1W | 1.4W |
| N. C. | 36 | 80 | 2.6E | 2.4E | 2.0E | 1.5E | 1.0E | 0.3E | 0.4W | 1.0W | 1.5W | 2.0W | 2.4W | 2.8W |
| Va. | 38 | 80 | 2.0E | 1.8E | 1.4E | 0.9E | 0.3E | 0.3W | 1.0W | 1.6W | 2.2W | 2.7W | 3.2W | 3.7W |
| Pa. | 40 | 80 | 0.9E | 0.7E | 0.3E | 0.2W | 0.8W | 1.4W | 2.1W | 2.8W | 3.4W | 4.0W | 4.5W | 5.1W |
| Pa. | 42 | 80 | 0.6E | 0.3E | 0.0 | 0.5W | 1.1W | 1.8W | 2.5W | 3.2W | 3.8W | 4.4W | 5.1W | 5.8W |
| Canada | 44 | 80 | 0.8W | 1.1W | 1.5W | 2.0W | 2.6W | 3.3W | 4.1W | 4.8W | 5.4W | 6.1W | 6.8W | 7.6W |
| Fla. | 30 | 84 | 6.2E | 6.1E | 5.9E | 5.5E | 5.0E | 4.5E | 3.9E | 3.2E | 2.8E | 2.7E | 2.8E | 2.9E |
| Ga. | 32 | 84 | 5.7E | 5.6E | 5.3E | 5.0E | 4.5E | 3.9E | 3.3E | 2.6E | 2.1E | 2.0E | 2.0E | 2.0E |
| Ga. | 34 | 84 | 5.3E | 5.2E | 4.9E | 4.5E | 4.0E | 3.4E | 2.8E | 2.1E | 1.6E | 1.4E | 1.3E | 1.2E |
| Tenn. | 36 | 84 | 4.0E | 3.9E | 3.6E | 3.2E | 2.7E | 2.1E | 1.4E | 0.8E | 0.2E | 0.0 | 0.2W | 0.5W |
| Ky. | 38 | 84 | 4.7E | 4.6E | 4.3E | 3.9E | 3.4E | 2.8E | 2.1E | 1.4E | 0.9E | 0.6E | 0.3E | 0.1W |
| Ohio | 40 | 84 | 4.3E | 4.2E | 3.8E | 3.4E | 2.9E | 2.4E | 1.7E | 1.0E | 0.4E | 0.0 | 0.4W | 0.6W |
| Mich. | 42 | 84 | 3.1E | 2.9E | 2.6E | 2.2E | 1.7E | 1.1E | 0.4E | 0.4W | 1.0W | 1.4W | 1.8W | 2.5W |
| Mich. | 44 | 84 | 2.8E | 2.6E | 2.3E | 1.9E | 1.4E | 0.8E | 0.0 | 0.8W | 1.4W | 1.8W | 2.4W | 3.1W |
| Mich. | 46 | 84 | 1.5E | 1.4E | 1.0E | 0.6E | 0.1E | 0.5W | 1.3W | 2.1W | 2.7W | 3.2W | 3.8W | 4.7W |
| Ala. | 30 | 88 | 7.3E | 7.3E | 7.2E | 7.0E | 6.6E | 6.1E | 5.6E | 4.9E | 4.5E | 4.6E | 4.9E | 5.1E |
| Ala. | 32 | 88 | 7.1E | 7.1E | 7.0E | 6.7E | 6.4E | 5.9E | 5.3E | 4.6E | 4.2E | 4.2E | 4.4E | 4.5E |
| Ala. | 34 | 88 | 7.4E | 7.4E | 7.2E | 7.0E | 6.6E | 6.1E | 5.5E | 4.8E | 4.3E | 4.3E | 4.4E | 4.4E |
| Tenn. | 36 | 88 | 7.2E | 7.2E | 7.1E | 6.8E | 6.4E | 5.9E | 5.2E | 4.6E | 4.1E | 4.0E | 4.0E | 3.8E |
| Ind. | 38 | 88 | 7.2E | 7.2E | 7.0E | 6.7E | 6.3E | 5.8E | 5.1E | 4.4E | 3.9E | 3.8E | 3.7E | 3.3E |
| Ill. | 40 | 88 | 6.6E | 6.6E | 6.7E | 6.4E | 6.0E | 5.5E | 4.8E | 4.1E | 3.6E | 3.4E | 3.2E | 2.7E |
| Ill. | 42 | 88 | 6.5E | 6.5E | 6.4E | 6.0E | 5.6E | 5.1E | 4.4E | 3.7E | 3.1E | 2.9E | 2.6E | 1.9E |
| Wis. | 44 | 88 | 6.3E | 6.3E | 6.2E | 5.8E | 5.4E | 4.9E | 4.2E | 3.4E | 2.8E | 2.5E | 2.1E | 1.4E |
| Mich. | 46 | 88 | 5.0E | 6.0E | 5.8E | 5.5E | 5.0E | 4.5E | 3.7E | 3.0E | 2.4E | 2.1E | 1.6E | 0.7E |
| Lake | 48 | 88 | 5.6E | 5.7E | 5.5E | 5.2E | 4.8E | 4.2E | 3.4E | 2.6E | 2.0E | 1.7E | 1.1E | 0.2E |
| La. | 30 | 92 | 8.3E | 8.5E | 8.5E | 8.4E | 8.1E | 7.8E | 7.2E | 6.7E | 6.3E | 6.6E | 7.0E | 7.2E |
| La. | 32 | 92 | 8.5E | 8.7E | 8.6E | 8.5E | 8.3E | 7.9E | 7.4E | 6.8E | 6.4E | 6.6E | 6.9E | 7.1E |
| Ark. | 34 | 92 | 8.8E | 8.6E | 8.6E | 8.8E | 8.5E | 8.1E | 7.6E | 7.0E | 6.6E | 6.7E | 6.9E | 6.9E |
| Ark. | 36 | 92 | 8.8E | 8.0E | 8.0E | 8.7E | 8.4E | 8.0E | 7.5E | 6.8E | 6.4E | 6.5E | 6.7E | 6.5E |
| Mo. | 38 | 92 | 9.0E | 9.2E | 9.1E | 9.0E | 8.6E | 8.2E | 7.7E | 7.0E | 6.5E | 6.6E | 6.6E | 6.4E |
| Mo. | 40 | 92 | 9.2E | 9.4E | 9.3E | 9.1E | 8.8E | 8.4E | 7.8E | 7.1E | 6.6E | 6.6E | 6.5E | 6.1E |
| Iowa | 42 | 92 | 9.5E | 9.7E | 9.7E | 9.5E | 9.2E | 8.7E | 8.1E | 7.4E | 6.9E | 6.8E | 6.6E | 6.0E |
| Minn. | 44 | 92 | 9.2E | 9.3E | 9.3E | 9.1E | 8.8E | 8.4E | 7.7E | 7.0E | 6.4E | 6.4E | 6.1E | 5.4E |
| Minn. | 46 | 92 | 9.1E | 9.2E | 9.2E | 9.0E | 8.7E | 8.3E | 7.6E | 6.8E | 6.3E | 6.3E | 5.9E | 5.1E |
| Minn. | 48 | 92 | 8.7E | 8.0E | 8.0E | 8.7E | 8.4E | 8.0E | 7.2E | 6.5E | 5.9E | 5.0E | 5.5E | 4.5E |
| At sea | 28 | 96 | 8.5E | 8.8E | 8.0E | 8.8E | 8.8E | 8.6E | 8.2E | 7.8E | 7.6E | 8.0E | 8.5E | 8.8E |
| Tex. | 30 | 96 | 9.0E | 9.2E | 9.3E | 9.3E | 9.2E | 9.0E | 8.6E | 8.1E | 7.0E | 8.3E | 8.7E | 8.0E |
| Tex. | 32 | 96 | 9.2E | 9.4E | 9.6E | 9.6E | 9.4E | 9.2E | 8.8E | 8.2E | 8.0E | 8.3E | 8.7E | 8.8E |
| Okla. | 34 | 96 | 9.6E | 9.8E | 9.9E | 9.9E | 9.8E | 9.5E | 9.1E | 8.6E | 8.2E | 8.5E | 8.8E | 8.8E |
| Okla. | 36 | 96 | 10.2E | 10.4E | 10.5E | 10.5E | 10.4E | 10.1E | 9.7E | 9.1E | 8.8E | 9.0E | 9.2E | 9.1E |
| Kans. | 38 | 96 | 11.1E | 11.3E | 11.4E | 11.4E | 11.2E | 11.0E | 10.5E | 9.9E | 9.5E | 9.8E | 9.9E | 9.6E |
| Kans. | 40 | 96 | 11.2E | 11.4E | 11.5E | 11.5E | 11.3E | 11.0E | 10.5E | 9.9E | 9.5E | 9.7E | 9.9E | 9.3E |
| Iowa | 42 | 96 | 11.5E | 11.7E | 11.8E | 11.8E | 11.6E | 11.3E | 10.8E | 10.1E | 9.7E | 9.8E | 9.8E | 9.2E |
| Minn. | 44 | 96 | 11.6E | 11.9E | 12.0E | 12.0E | 11.8E | 11.4E | 10.9E | 10.2E | 9.8E | 9.9E | 9.7E | 9.1E |
| Minn. | 46 | 96 | 12.4E | 12.7E | 12.8E | 12.7E | 12.5E | 12.2E | 11.6E | 10.9E | 10.5E | 10.6E | 10.4E | 9.6E |
| Minn. | 48 | 96 | 12.4E | 12.7E | 12.8E | 12.7E | 12.5E | 12.2E | 11.6E | 10.8E | 10.4E | 10.5E | 10.2E | 9.3E |

SECULAR CHANGE OF MAGNETIC DECLINATION

| State | Lat. | Long. | 1820 | 1830 | 1840 | 1850 | 1860 | 1870 | 1880 | 1890 | 1900 | 1910 | 1920 | 1930 |
|---------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Mexico | 28 | 100 | | 0.6E | 0.8E | 0.9E | 0.9E | 0.8E | 0.5E | 0.1E | 0.0E | 0.5E | 10.0E | 10.3E |
| Tex. | 30 | 100 | | 0.9E | 10.1E | 10.2E | 10.2E | 10.1E | 0.8E | 0.3E | 0.2E | 0.7E | 10.2E | 10.4E |
| Tex. | 32 | 100 | | 10.6E | 10.8E | 10.8E | 10.8E | 10.7E | 10.4E | 0.9E | 0.8E | 10.2E | 10.6E | 10.7E |
| Tex. | 34 | 100 | | 11.0E | 11.2E | 11.2E | 11.2E | 11.1E | 10.8E | 10.3E | 10.1E | 10.5E | 10.8E | 10.8E |
| Okl. | 36 | 100 | | 11.7E | 11.9E | 12.0E | 11.9E | 11.8E | 11.4E | 11.0E | 10.8E | 11.1E | 11.4E | 11.3E |
| Kans. | 38 | 100 | | 12.2E | 12.4E | 12.4E | 12.4E | 12.2E | 11.8E | 11.3E | 11.1E | 11.4E | 11.6E | 11.4E |
| Kans. | 40 | 100 | | 12.8E | 13.0E | 13.0E | 13.0E | 12.8E | 12.4E | 11.8E | 11.6E | 11.9E | 12.0E | 11.6E |
| Nebr. | 42 | 100 | | 13.1E | 13.3E | 13.3E | 13.2E | 13.1E | 12.6E | 12.1E | 11.8E | 12.0E | 12.1E | 11.6E |
| S. Dak. | 44 | 100 | | 14.2E | 14.4E | 14.4E | 14.3E | 14.1E | 13.7E | 13.0E | 12.8E | 13.0E | 13.0E | 12.4E |
| N. Dak. | 46 | 100 | | 15.0E | 15.2E | 15.3E | 15.2E | 15.0E | 14.5E | 13.9E | 13.5E | 13.8E | 13.7E | 13.0E |
| N. Dak. | 48 | 100 | | 15.6E | 15.8E | 15.8E | 15.8E | 15.5E | 15.0E | 14.4E | 14.0E | 14.3E | 14.1E | 13.3E |
| Tex. | 30 | 104 | | 10.6E | 10.8E | 11.0E | 11.1E | 11.1E | 10.9E | 10.5E | 10.5E | 11.0E | 11.5E | 11.7E |
| Tex. | 32 | 104 | | 11.3E | 11.6E | 11.7E | 11.8E | 11.8E | 11.6E | 11.2E | 11.1E | 11.6E | 12.0E | 12.1E |
| N. Mex. | 34 | 104 | | 12.0E | 12.2E | 12.4E | 12.5E | 12.5E | 12.2E | 11.8E | 11.7E | 12.2E | 12.6E | 12.6E |
| N. Mex. | 36 | 104 | | | | 13.1E | 13.2E | 13.2E | 13.0E | 12.5E | 12.4E | 12.9E | 13.2E | 13.1E |
| Colo. | 38 | 104 | | | | 13.7E | 13.8E | 13.8E | 13.5E | 13.0E | 12.9E | 13.4E | 13.6E | 13.4E |
| Colo. | 40 | 104 | | | | 14.4E | 14.5E | 14.5E | 14.2E | 13.7E | 13.6E | 14.0E | 14.2E | 13.8E |
| Nebr. | 42 | 104 | | | | 15.6E | 15.7E | 15.7E | 15.4E | 14.8E | 14.7E | 15.1E | 15.2E | 14.8E |
| S. Dak. | 44 | 104 | | | | 16.4E | 16.4E | 16.3E | 16.0E | 15.5E | 15.4E | 15.8E | 15.8E | 15.3E |
| N. Dak. | 46 | 104 | | | | 17.3E | 17.3E | 17.2E | 16.9E | 16.3E | 16.2E | 16.6E | 16.5E | 15.9E |
| N. Dak. | 48 | 104 | | | | 18.5E | 18.6E | 18.4E | 18.0E | 17.5E | 17.3E | 17.7E | 17.5E | 16.8E |
| Mexico | 30 | 108 | | | | 11.5E | 11.7E | 11.8E | 11.7E | 11.4E | 11.4E | 12.1E | 12.5E | 12.6E |
| N. Mex. | 32 | 108 | | | | 12.3E | 12.5E | 12.6E | 12.5E | 12.2E | 12.2E | 12.8E | 13.2E | 13.2E |
| N. Mex. | 34 | 108 | | | | 13.0E | 13.2E | 13.3E | 13.1E | 12.8E | 12.8E | 13.4E | 13.8E | 13.7E |
| N. Mex. | 36 | 108 | | | | 13.7E | 13.9E | 14.0E | 13.8E | 13.5E | 13.5E | 14.1E | 14.4E | 14.3E |
| Colo. | 38 | 108 | | | | 14.5E | 14.7E | 14.8E | 14.6E | 14.2E | 14.2E | 14.8E | 15.0E | 14.8E |
| Colo. | 40 | 108 | | | | 15.5E | 15.7E | 15.8E | 15.6E | 15.2E | 15.2E | 15.7E | 15.9E | 15.6E |
| Wyo. | 42 | 108 | | | | 16.4E | 16.6E | 16.7E | 16.4E | 16.1E | 16.1E | 16.6E | 16.7E | 16.3E |
| Wyo. | 44 | 108 | | | | 17.6E | 17.8E | 17.8E | 17.6E | 17.2E | 17.2E | 17.7E | 17.7E | 17.3E |
| Mont. | 46 | 108 | | | | 18.7E | 18.9E | 19.0E | 18.7E | 18.3E | 18.3E | 18.8E | 18.8E | 18.2E |
| Mont. | 48 | 108 | | | | 20.2E | 20.4E | 20.4E | 20.1E | 19.7E | 19.7E | 20.2E | 20.1E | 19.4E |
| Ariz. | 32 | 112 | | | | 12.6E | 12.9E | 13.1E | 13.1E | 12.9E | 13.0E | 13.8E | 14.2E | 14.2E |
| Ariz. | 34 | 112 | | | | 13.3E | 13.6E | 13.8E | 13.7E | 13.6E | 13.6E | 14.4E | 14.7E | 14.6E |
| Ariz. | 36 | 112 | | | | 14.1E | 14.4E | 14.6E | 14.5E | 14.3E | 14.4E | 15.1E | 15.4E | 15.3E |
| Utah | 38 | 112 | | | | 15.2E | 15.4E | 15.6E | 15.6E | 15.4E | 15.4E | 16.1E | 16.3E | 16.2E |
| Utah | 40 | 112 | | | | 16.3E | 16.6E | 16.8E | 16.7E | 16.5E | 16.6E | 17.2E | 17.4E | 17.1E |
| Idaho | 42 | 112 | | | | 17.4E | 17.7E | 17.9E | 17.8E | 17.6E | 17.7E | 18.2E | 18.4E | 18.1E |
| Idaho | 44 | 112 | | | | 18.5E | 18.8E | 19.0E | 18.8E | 18.6E | 18.7E | 19.3E | 19.4E | 19.0E |
| Mont. | 46 | 112 | | | | 19.4E | 19.8E | 19.9E | 19.8E | 19.5E | 19.6E | 20.2E | 20.2E | 19.8E |
| Mont. | 48 | 112 | | | | 21.0E | 21.3E | 21.5E | 21.3E | 21.0E | 21.1E | 21.7E | 21.7E | 21.2E |
| Mexico | 32 | 116 | 11.4E | 11.8E | 12.3E | 12.6E | 13.0E | 13.3E | 13.4E | 13.4E | 13.6E | 14.4E | 14.8E | 14.7E |
| Calif. | 34 | 116 | 12.3E | 12.8E | 13.2E | 13.5E | 13.9E | 14.2E | 14.3E | 14.2E | 14.4E | 15.2E | 15.6E | 15.5E |
| Calif. | 36 | 116 | 13.1E | 13.6E | 14.0E | 14.4E | 14.8E | 15.1E | 15.1E | 15.1E | 15.3E | 16.0E | 16.3E | 16.2E |
| Nev. | 38 | 116 | | | | 15.0E | 15.4E | 15.8E | 16.1E | 16.1E | 16.1E | 16.3E | 17.0E | 17.1E |
| Nev. | 40 | 116 | | | | 15.9E | 16.2E | 16.6E | 16.9E | 17.0E | 17.0E | 17.1E | 17.8E | 17.8E |
| Nev. | 42 | 116 | | | | 17.2E | 17.5E | 17.9E | 18.2E | 18.2E | 18.4E | 19.0E | 19.2E | 19.0E |
| Idaho | 44 | 116 | | | | 18.2E | 18.6E | 19.0E | 19.3E | 19.3E | 19.2E | 20.1E | 20.2E | 19.9E |
| Idaho | 46 | 116 | | | | 19.9E | 20.3E | 20.7E | 21.0E | 21.0E | 20.9E | 21.2E | 21.8E | 21.5E |
| Mont. | 48 | 116 | | | | 21.1E | 21.5E | 21.9E | 22.2E | 22.2E | 22.2E | 23.0E | 23.1E | 22.6E |
| At sea | 34 | 120 | 12.5E | 12.8E | 13.1E | 13.5E | 14.0E | 14.4E | 14.6E | 14.6E | 14.6E | 15.8E | 16.1E | 16.0E |
| Calif. | 36 | 120 | 13.5E | 13.8E | 14.2E | 14.6E | 15.0E | 15.4E | 15.6E | 15.6E | 15.9E | 16.8E | 17.1E | 16.9E |
| Calif. | 38 | 120 | 14.2E | 14.5E | 14.9E | 15.3E | 15.8E | 16.2E | 16.4E | 16.4E | 16.7E | 17.5E | 17.8E | 17.6E |
| Calif. | 40 | 120 | 15.3E | 15.7E | 16.0E | 16.5E | 17.0E | 17.4E | 17.5E | 17.6E | 17.8E | 18.6E | 18.8E | 18.6E |
| Calif. | 42 | 120 | 16.5E | 17.0E | 17.4E | 17.8E | 18.3E | 18.7E | 18.8E | 18.9E | 19.1E | 19.9E | 20.1E | 19.9E |
| Oreg. | 44 | 120 | 18.0E | 18.5E | 18.9E | 19.4E | 19.8E | 20.2E | 20.3E | 20.4E | 20.7E | 21.5E | 21.7E | 21.4E |
| Wash. | 46 | 120 | 18.9E | 19.4E | 19.9E | 20.3E | 20.8E | 21.2E | 21.3E | 21.4E | 21.7E | 22.4E | 22.6E | 22.2E |
| Wash. | 48 | 120 | 19.8E | 20.5E | 20.9E | 21.4E | 21.9E | 22.3E | 22.4E | 22.5E | 22.9E | 23.6E | 23.7E | 23.3E |
| At sea | 38 | 124 | 14.2E | 14.6E | 14.9E | 15.4E | 16.0E | 16.5E | 16.7E | 16.8E | 17.2E | 18.0E | 18.3E | 18.2E |
| Calif. | 40 | 124 | 15.3E | 15.6E | 16.0E | 16.5E | 17.1E | 17.6E | 17.8E | 17.9E | 18.3E | 19.1E | 19.4E | 19.2E |
| Calif. | 42 | 124 | 16.5E | 16.9E | 17.3E | 17.8E | 18.4E | 18.8E | 19.1E | 19.2E | 19.6E | 20.4E | 20.7E | 20.5E |
| Oreg. | 44 | 124 | 17.5E | 18.0E | 18.4E | 18.9E | 19.5E | 20.0E | 20.2E | 20.4E | 20.8E | 21.6E | 21.9E | 21.6E |
| Oreg. | 46 | 124 | 18.4E | 19.0E | 19.5E | 20.0E | 20.6E | 21.1E | 21.3E | 21.5E | 21.9E | 22.8E | 23.0E | 22.7E |
| Wash. | 48 | 124 | 19.5E | 20.2E | 20.6E | 21.2E | 21.8E | 22.3E | 22.5E | 22.8E | 23.2E | 24.0E | 24.2E | 23.8E |

TABLE 740.—Dip or Inclination, United States

This table gives for the epoch January 1, 1925, the values of the magnetic dip, I , corresponding to the longitudes west of Greenwich in the heading and the north latitudes in the first column.

| λ ϕ | 65° | 70° | 75° | 80° | 85° | 90° | 95° | 100° | 105° | 110° | 115° | 120° | 125° |
|---------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 19 | | | 51.5 | 50.6 | 49.6 | | | | | | | | |
| 21 | | | 53.8 | 53.0 | 52.1 | 50.9 | | | | | | | |
| 23 | | | 56.3 | 55.4 | 54.5 | 53.4 | 52.2 | 50.9 | 50.0 | | | | |
| 25 | | | 58.6 | 57.8 | 56.9 | 55.9 | 54.8 | 53.5 | 52.4 | 51.3 | 50.2 | | |
| 27 | | | 60.6 | 60.0 | 59.1 | 58.3 | 57.1 | 55.9 | 54.8 | 53.7 | 52.5 | 51.5 | |
| 29 | | 62.1 | 62.6 | 62.1 | 61.3 | 60.5 | 59.4 | 58.1 | 57.0 | 55.9 | 54.8 | 53.8 | |
| 31 | | 64.0 | 64.3 | 64.0 | 63.5 | 62.6 | 61.5 | 60.5 | 59.2 | 58.2 | 57.0 | 55.9 | |
| 33 | | 65.8 | 66.1 | 65.7 | 65.2 | 64.4 | 63.5 | 62.6 | 61.3 | 60.1 | 59.2 | 58.1 | |
| 35 | | 67.5 | 67.9 | 67.6 | 66.9 | 66.5 | 65.6 | 64.5 | 63.4 | 62.3 | 61.0 | 60.1 | |
| 37 | | 69.3 | 69.6 | 69.2 | 69.1 | 68.4 | 67.5 | 66.6 | 65.3 | 64.3 | 63.0 | 62.1 | |
| 39 | | 70.8 | 71.0 | 70.9 | 70.8 | 70.3 | 69.4 | 68.4 | 67.3 | 66.2 | 65.0 | 63.9 | 62.7 |
| 41 | | 72.2 | 72.5 | 72.7 | 72.4 | 71.9 | 71.1 | 70.2 | 69.0 | 68.0 | 66.7 | 65.6 | 64.3 |
| 43 | | 73.6 | 73.9 | 74.2 | 73.9 | 73.6 | 72.7 | 71.9 | 70.8 | 69.8 | 68.4 | 67.4 | 66.1 |
| 45 | | 74.7 | 75.3 | 75.6 | 75.6 | 75.2 | 74.5 | 73.6 | 72.6 | 71.3 | 70.2 | 69.0 | 67.8 |
| 47 | | 75.3 | 76.1 | 76.7 | 77.1 | 77.1 | 76.8 | 76.1 | 75.2 | 74.3 | 72.9 | 71.7 | 70.7 |
| 49 | | 76.3 | 77.2 | 77.9 | 78.4 | 78.6 | 77.7 | 76.8 | 75.8 | 74.6 | 73.2 | 72.0 | 70.9 |

TABLE 741.—Secular Change of Dip, United States

Values of the magnetic dip for places designated by the north latitudes and longitudes west of Greenwich in the first two columns for January 1, of the years in the heading. The degrees are given in the third column and the minutes in the succeeding columns.

| Latitude | Longitude | | 1855 | 1865 | 1875 | 1885 | 1895 | 1900 | 1905 | 1910 | 1915 | 1920 | 1925 |
|----------|-----------|-----|------|------|------|------|------|------|------|------|------|------|------|
| ° | ° | ° | ' | ' | ' | ' | ' | ' | ' | ' | ' | ' | ' |
| 25 | 80 | 55+ | 29 | 27 | 22 | 12 | 16 | 25 | 42 | 77 | 114 | 144 | 171 |
| 25 | 90 | 53+ | 17 | 23 | 34 | 40 | 34 | 44 | 73 | 106 | 136 | 157 | 177 |
| 25 | 100 | 51+ | 15 | 33 | 50 | 49 | 61 | 71 | 87 | 107 | 126 | 140 | 151 |
| 31 | 80 | 62+ | 45 | 43 | 37 | 22 | 18 | 23 | 35 | 57 | 81 | 101 | 120 |
| 31 | 90 | 60+ | 52 | 60 | 67 | 58 | 60 | 68 | 81 | 104 | 124 | 140 | 155 |
| 31 | 100 | 59+ | 01 | 15 | 26 | 22 | 28 | 36 | 48 | 62 | 74 | 83 | 91 |
| 31 | 110 | 57+ | 05 | 16 | 24 | 28 | 38 | 43 | 49 | 56 | 63 | 67 | 71 |
| 37 | 80 | 68+ | 60 | 55 | 49 | 31 | 20 | 21 | 27 | 39 | 53 | 65 | 75 |
| 37 | 90 | 67+ | 34 | 40 | 42 | 33 | 27 | 32 | 40 | 53 | 65 | 75 | 83 |
| 37 | 100 | 65+ | 45 | 54 | 61 | 55 | 56 | 61 | 70 | 79 | 86 | 91 | 95 |
| 37 | 110 | 63+ | .. | .. | 53 | 54 | 60 | 63 | 66 | 70 | 73 | 76 | 78 |
| 37 | 120 | 61+ | 52 | 54 | 57 | 61 | 69 | 67 | 64 | 64 | 63 | 65 | 66 |
| 43 | 70 | 73+ | 117 | 107 | 90 | 67 | 45 | 38 | 38 | 38 | 38 | 37 | 36 |
| 43 | 80 | 73+ | 106 | 100 | 92 | 73 | 55 | 52 | 54 | 59 | 65 | 68 | 70 |
| 43 | 90 | 73+ | 36 | 36 | 35 | 26 | 16 | 17 | 20 | 26 | 32 | 35 | 38 |
| 43 | 100 | 71+ | .. | .. | 48 | 41 | 37 | 39 | 43 | 47 | 50 | 53 | 55 |
| 43 | 110 | 69+ | .. | .. | 44 | 42 | 44 | 45 | 46 | 46 | 46 | 48 | 49 |
| 43 | 120 | 67+ | .. | .. | 26 | 29 | 33 | 29 | 26 | 24 | 22 | 22 | 22 |
| 47 | 70 | 76+ | 109 | 97 | 80 | 57 | 32 | 25 | 22 | 19 | 15 | 10 | 05 |
| 47 | 80 | 77+ | 66 | 60 | 50 | 31 | 11 | 07 | 06 | 06 | 07 | 06 | 04 |
| 49 | 90 | 78+ | 53 | 50 | 45 | 36 | 24 | 21 | 20 | 20 | 20 | 20 | 20 |
| 49 | 100 | 76+ | .. | .. | 62 | 55 | 49 | 48 | 47 | 46 | 45 | 45 | 46 |
| 49 | 110 | 74+ | .. | .. | 47 | 44 | 43 | 41 | 40 | 37 | 35 | 35 | 35 |
| 49 | 120 | 72+ | .. | .. | 18 | 19 | 19 | 15 | 11 | 06 | 02 | 01 | 00 |

TABLE 742.—Horizontal Magnetic Intensity, United States

This table gives for the epoch January 1, 1925, the horizontal intensity, H , expressed in c.g.s. units, corresponding to the longitudes in the heading and the latitudes in the first column.

| λ φ | 65° | 70° | 75° | 80° | 85° | 90° | 95° | 100° | 105° | 110° | 115° | 120° | 125° |
|------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 19 | | | .286 | .294 | .302 | .308 | .315 | .320 | | | | | |
| 21 | | | .280 | .286 | .294 | .301 | .307 | .312 | .313 | .313 | | | |
| 23 | | | .272 | .279 | .285 | .293 | .300 | .304 | .305 | .306 | | | |
| 25 | | | .263 | .270 | .276 | .282 | .290 | .295 | .297 | .298 | .298 | | |
| 27 | | | .254 | .260 | .267 | .273 | .280 | .286 | .289 | .291 | .292 | .292 | |
| 29 | | .240 | .244 | .249 | .257 | .264 | .270 | .276 | .280 | .283 | .284 | .285 | |
| 31 | | .230 | .234 | .238 | .245 | .253 | .260 | .266 | .271 | .274 | .276 | .277 | |
| 33 | | .220 | .223 | .227 | .234 | .241 | .248 | .254 | .260 | .264 | .268 | .268 | |
| 35 | | .209 | .211 | .215 | .223 | .228 | .235 | .242 | .247 | .252 | .256 | .258 | |
| 37 | | .197 | .198 | .202 | .208 | .214 | .222 | .227 | .235 | .240 | .245 | .249 | |
| 39 | | .186 | .187 | .190 | .193 | .200 | .207 | .215 | .223 | .228 | .235 | .239 | .242 |
| 41 | | .174 | .175 | .176 | .182 | .187 | .193 | .202 | .209 | .216 | .223 | .228 | .232 |
| 43 | .165 | .163 | .162 | .163 | .167 | .171 | .178 | .187 | .195 | .203 | .211 | .217 | .222 |
| 45 | .155 | .153 | .151 | .150 | .152 | .157 | .163 | .172 | .181 | .190 | .198 | .205 | .212 |
| 47 | .145 | .142 | .138 | .136 | .138 | .139 | .148 | .157 | .165 | .176 | .185 | .192 | .201 |
| 49 | .135 | .130 | .126 | .123 | .123 | .126 | .134 | .142 | .152 | .160 | .171 | .181 | .189 |

TABLE 743.—Secular Change of Horizontal Intensity, United States

Values of horizontal intensity in c.g.s. units for the places designated by the latitude and longitude in the first two columns for January 1 of the years in the heading.

| Lat. | Long. | 1855 | 1865 | 1875 | 1885 | 1895 | 1900 | 1905 | 1910 | 1915 | 1920 | 1925 |
|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| ° | ° | | | | | | | | | | | |
| 25 | 80 | .3064 | .3054 | .3034 | .3003 | .2968 | .2946 | .2916 | .2870 | .2805 | .2749 | .2704 |
| 25 | 90 | | | .3107 | .3087 | .3051 | .3026 | .3000 | .2962 | .2910 | .2863 | .2825 |
| 25 | 100 | | | .3188 | .3157 | .3125 | .3108 | .3086 | .3065 | .3017 | .2980 | .2950 |
| 31 | 80 | .2652 | .2650 | .2644 | .2624 | .2606 | .2591 | .2567 | .2526 | .2465 | .2419 | .2382 |
| 31 | 90 | .2817 | .2787 | .2752 | .2750 | .2728 | .2710 | .2687 | .2653 | .2603 | .2561 | .2527 |
| 31 | 100 | .2922 | .2887 | .2852 | .2838 | .2816 | .2802 | .2784 | .2755 | .2720 | .2688 | .2662 |
| 31 | 110 | .2963 | .2933 | .2903 | .2876 | .2855 | .2847 | .2832 | .2809 | .2784 | .2760 | .2738 |
| 37 | 80 | .2184 | .2187 | .2197 | .2189 | .2182 | .2177 | .2159 | .2130 | .2086 | .2049 | .2022 |
| 37 | 90 | .2332 | .2314 | .2292 | .2302 | .2292 | .2284 | .2266 | .2239 | .2198 | .2167 | .2142 |
| 37 | 100 | | | .2407 | .2403 | .2391 | .2383 | .2368 | .2345 | .2317 | .2292 | .2272 |
| 37 | 110 | | | .2519 | .2502 | .2488 | .2481 | .2471 | .2453 | .2433 | .2414 | .2396 |
| 37 | 120 | .2612 | .2602 | .2592 | .2573 | .2557 | .2553 | .2547 | .2536 | .2522 | .2506 | .2492 |
| 43 | 70 | .1612 | .1631 | .1654 | .1667 | .1682 | .1689 | .1692 | .1680 | .1662 | .1644 | .1632 |
| 43 | 80 | .1682 | .1682 | .1692 | .1710 | .1718 | .1718 | .1710 | .1693 | .1667 | .1647 | .1632 |
| 43 | 90 | | | .1792 | .1798 | .1794 | .1791 | .1783 | .1766 | .1741 | .1723 | .1708 |
| 43 | 100 | | | .1958 | .1956 | .1952 | .1949 | .1940 | .1924 | .1905 | .1888 | .1873 |
| 43 | 110 | | | .2110 | .2100 | .2092 | .2087 | .2082 | .2070 | .2057 | .2043 | .2029 |
| 43 | 120 | | | .2242 | .2242 | .2217 | .2215 | .2213 | .2206 | .2196 | .2183 | .2172 |
| 47 | 70 | .1365 | .1372 | .1381 | .1402 | .1424 | .1434 | .1444 | .1443 | .1432 | .1422 | .1415 |
| 47 | 80 | | .1367 | .1367 | .1387 | .1397 | .1402 | .1404 | .1394 | .1380 | .1369 | .1362 |
| 49 | 90 | | | .1280 | .1286 | .1291 | .1294 | .1295 | .1287 | .1276 | .1268 | .1262 |
| 49 | 100 | | | .1458 | .1458 | .1457 | .1458 | .1458 | .1450 | .1440 | .1431 | .1422 |
| 49 | 110 | | | .1639 | .1635 | .1631 | .1632 | .1632 | .1626 | .1618 | .1609 | .1600 |
| 49 | 120 | | | .1847 | .1838 | .1831 | .1832 | .1834 | .1831 | .1825 | .1816 | .1808 |

TABLE 744.—Total Magnetic Intensity, United States

This table gives for the epoch January 1, 1925, the values of total intensity, F , expressed in c.g.s. units, corresponding to the longitudes in the heading and the latitudes in the first column.

| λ ° | 65° | 70° | 75° | 80° | 85° | 90° | 95° | 100° | 105° | 110° | 115° | 120° | 125° |
|----------------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 19 | | | .460 | .463 | .465 | | | | | | | | |
| 21 | | | .474 | .475 | .477 | .478 | | | | | | | |
| 23 | | | .491 | .491 | .490 | .491 | .488 | .482 | .475 | | | | |
| 25 | | | .504 | .508 | .505 | .504 | .503 | .496 | .487 | .477 | .466 | | |
| 27 | | | .516 | .521 | .521 | .520 | .516 | .510 | .501 | .491 | .479 | .469 | |
| 29 | | .513 | .529 | .533 | .535 | .536 | .531 | .522 | .514 | .504 | .493 | .482 | |
| 31 | | .526 | .540 | .543 | .549 | .549 | .543 | .541 | .529 | .519 | .507 | .493 | |
| 33 | | .537 | .551 | .552 | .558 | .559 | .556 | .552 | .541 | .530 | .522 | .507 | |
| 35 | | .545 | .560 | .563 | .570 | .571 | .569 | .562 | .553 | .542 | .528 | .518 | |
| 37 | | .558 | .568 | .571 | .583 | .582 | .581 | .572 | .561 | .553 | .540 | .533 | |
| 39 | | .565 | .576 | .582 | .586 | .593 | .589 | .584 | .577 | .565 | .556 | .542 | .529 |
| 41 | | .569 | .583 | .589 | .601 | .602 | .596 | .598 | .584 | .577 | .564 | .551 | .536 |
| 43 | | .578 | .586 | .598 | .602 | .606 | .597 | .603 | .594 | .588 | .573 | .564 | .548 |
| 45 | .562 | .581 | .594 | .603 | .608 | .613 | .609 | .608 | .605 | .592 | .583 | .573 | .561 |
| 47 | .570 | .588 | .599 | .608 | .620 | .606 | .619 | .614 | .609 | .601 | .588 | .581 | .572 |
| 49 | .568 | .587 | .603 | .611 | .622 | .624 | .626 | .621 | .617 | .602 | .594 | .585 | .577 |

TABLE 745.—Secular Change of Total Intensity, United States

Values of total intensity in c.g.s. units for places designated by the latitudes and longitudes in the first two columns for January 1 of the years in the heading.

| Lat. | Long. | 1855 | 1865 | 1875 | 1885 | 1895 | 1900 | 1905 | 1910 | 1915 | 1920 | 1925 |
|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| ° | ° | | | | | | | | | | | |
| 25 | 80 | .5407 | .5385 | .5339 | .5262 | .5209 | .5190 | .5175 | .5170 | .5136 | .5102 | .5081 |
| 25 | 90 | | | .5232 | .5210 | .5137 | .5115 | .5131 | .5134 | .5107 | .5070 | .5045 |
| 25 | 100 | | | .5159 | .5107 | .5078 | .5069 | .5064 | .5051 | .5025 | .4990 | .4961 |
| 31 | 80 | .5792 | .5781 | .5749 | .5657 | .5606 | .5589 | .5575 | .5554 | .5496 | .5456 | .5434 |
| 31 | 90 | .5786 | .5749 | .5697 | .5666 | .5627 | .5613 | .5604 | .5602 | .5557 | .5516 | .5488 |
| 31 | 100 | .5676 | .5647 | .5608 | .5570 | .5543 | .5537 | .5535 | .5516 | .5479 | .5439 | .5409 |
| 31 | 110 | .5453 | .5424 | .5388 | .5348 | .5333 | .5330 | .5317 | .5291 | .5261 | .5225 | .5193 |
| 37 | 80 | .6094 | .6080 | .6080 | .5977 | .5910 | .5901 | .5878 | .5851 | .5790 | .5739 | .5707 |
| 37 | 90 | .6111 | .6089 | .6040 | .6028 | .5977 | .5977 | .5963 | .5947 | .5889 | .5848 | .5814 |
| 37 | 100 | | | .5922 | .5889 | .5863 | .5863 | .5860 | .5838 | .5795 | .5752 | .5717 |
| 37 | 110 | | | .5722 | .5687 | .5676 | .5670 | .5657 | .5629 | .5593 | .5560 | .5525 |
| 37 | 120 | .5539 | .5524 | .5512 | .5484 | .5474 | .5459 | .5437 | .5414 | .5381 | .5353 | .5326 |
| 43 | 70 | .6208 | .6214 | .6189 | .6091 | .6011 | .5994 | .6005 | .5962 | .5898 | .5828 | .5780 |
| 43 | 80 | .6402 | .6361 | .6345 | .6287 | .6201 | .6183 | .6166 | .6136 | .6079 | .6024 | .5981 |
| 43 | 90 | | | .6341 | .6306 | .6231 | .6227 | .6217 | .6194 | .6142 | .6097 | .6061 |
| 43 | 100 | | | .6269 | .6224 | .6190 | .6191 | .6184 | .6155 | .6110 | .6072 | .6034 |
| 43 | 110 | | | .6091 | .6053 | .6039 | .6030 | .6020 | .5985 | .5948 | .5917 | .5881 |
| 43 | 120 | | | .5842 | .5818 | .5806 | .5784 | .5767 | .5740 | .5706 | .5673 | .5644 |
| 47 | 70 | .6468 | .6398 | .6298 | .6209 | .6115 | .6106 | .6126 | .6100 | .6025 | .5947 | .5883 |
| 47 | 80 | | .6575 | .6486 | .6417 | .6298 | .6288 | .6289 | .6244 | .6189 | .6132 | .6085 |
| 49 | 90 | | | .6561 | .6506 | .6421 | .6408 | .6404 | .6364 | .6310 | .6270 | .6241 |
| 49 | 100 | | | .6498 | .6441 | .6389 | .6385 | .6377 | .6334 | .6283 | .6243 | .6212 |
| 49 | 110 | | | .6245 | .6209 | .6188 | .6178 | .6172 | .6129 | .6087 | .6053 | .6019 |
| 49 | 120 | | | .6075 | .6051 | .6028 | .6009 | .5994 | .5957 | .5916 | .5882 | .5851 |

TABLE 746.—Agonic Line, United States

The line of no declination (agonic line) is moving westward in the northern part of the country, but south of latitude 30° it is nearly stationary.

| Lat. N. | Longitudes of the agonic line for the years— | | | | | | | |
|------------|--|------|------|------|------|------|------|------|
| | 1800 | 1850 | 1875 | 1890 | 1905 | 1915 | 1920 | 1925 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 25 | | | | 75.5 | 76.1 | 77.4 | 77.4 | 77.1 |
| 30 | | | | 78.6 | 79.7 | 80.0 | 80.1 | 79.7 |
| 35 | | 76.7 | 79.0 | 79.9 | 81.7 | 82.7 | 82.8 | 83.0 |
| 6 | 75.2 | 77.3 | 79.7 | 80.5 | 82.8 | 84.4 | 84.5 | 84.4 |
| 7 | 76.3 | 77.7 | 80.6 | 82.2 | 83.5 | 84.0 | 84.0 | 84.0 |
| 8 | 76.7 | 78.3 | 81.3 | 82.6 | 83.6 | 84.1 | 84.1 | 84.0 |
| 9 | 76.9 | 78.7 | 81.6 | 82.2 | 83.6 | 83.9 | 84.0 | 84.2 |
| 40 | 77.0 | 79.3 | 81.6 | 82.7 | 84.0 | 84.3 | 84.5 | 84.6 |
| 1 | 77.9 | 80.4 | 81.8 | 82.8 | 84.6 | 85.1 | 85.2 | 85.2 |
| 2 | 79.1 | 81.0 | 82.6 | 83.7 | 84.8 | 85.3 | 85.4 | 85.8 |
| 3 | 79.4 | 81.2 | 83.1 | 84.3 | 85.0 | 85.4 | 85.6 | 85.8 |
| 4 | 79.8 | | 83.3 | 84.9 | 85.5 | 85.8 | 86.0 | 86.1 |
| 45 | | | 83.6 | 85.2 | 86.0 | 86.2 | 86.4 | 86.6 |
| 6 | | | 84.2 | 84.8 | 86.4 | 86.3 | 86.6 | 86.8 |
| 7 | | | 85.1 | 85.4 | 86.4 | 86.6 | 86.8 | 87.1 |
| 8 | | | 86.0 | 85.9 | 86.5 | 87.2 | 87.6 | 87.7 |
| 9 | | | 86.5 | 86.3 | 87.2 | 88.0 | 88.2 | 88.2 |

TABLE 747.—Mean Magnetic Character of Each Month in the Years 1906 to 1930*

Means derived from daily magnetic characters based upon the following scale; 0, no disturbance; 1, moderate disturbance, and 2, large disturbance.

| Year | Jan. | Feb. | Mar. | Apr. | May | June | July | Aug. | Sept. | Oct. | Nov. | Dec. | Year Mean |
|------|------|------|------|------|------|------|------|------|-------|------|------|------|-----------|
| 1906 | 0.45 | 0.90 | 0.68 | 0.63 | 0.58 | 0.56 | 0.69 | 0.63 | 0.79 | 0.59 | 0.55 | 0.71 | 0.65 |
| 1907 | .69 | .83 | .58 | .55 | .72 | .67 | .67 | .66 | .68 | .71 | .61 | .53 | .66 |
| 1908 | .64 | .71 | .87 | .68 | .82 | .66 | .49 | .77 | .89 | .53 | .60 | .47 | .68 |
| 1909 | .76 | .63 | .79 | .49 | .59 | .54 | .53 | .65 | .70 | .69 | .49 | .58 | .62 |
| 1910 | .58 | .71 | .81 | .68 | .72 | .53 | .55 | .81 | 80 | .96 | .77 | .76 | .72 |
| 1911 | .78 | .89 | .78 | .76 | .70 | .53 | .61 | .53 | .50 | .59 | .49 | .45 | .63 |
| 1912 | .42 | .49 | .45 | .45 | .47 | .47 | .41 | .49 | .47 | .46 | .45 | .43 | .46 |
| 1913 | .51 | .53 | .53 | .54 | .45 | .45 | .42 | .46 | .58 | .57 | .42 | .36 | .48 |
| 1914 | .46 | .50 | .62 | .50 | .37 | .52 | .61 | .61 | .53 | .64 | .60 | .46 | .54 |
| 1915 | .53 | .64 | .68 | .61 | .58 | .61 | .47 | .60 | .59 | .77 | .82 | .54 | .62 |
| 1916 | .61 | .56 | .86 | .68 | .75 | .67 | .62 | .75 | .75 | .76 | .83 | .65 | .71 |
| 1917 | .81 | .69 | .59 | .63 | .66 | .55 | .61 | .85 | .61 | .74 | .53 | .72 | .67 |
| 1918 | .63 | .78 | .73 | .79 | .68 | .56 | .69 | .77 | .88 | .85 | .87 | .88 | .76 |
| 1919 | .78 | .81 | .89 | .70 | .82 | .55 | .54 | .70 | .83 | .91 | .52 | .56 | .72 |
| 1920 | .62 | .52 | .78 | .65 | .57 | .43 | .51 | .61 | .87 | .65 | .58 | .65 | .62 |
| 1921 | .54 | .51 | .68 | .67 | .83 | .55 | .54 | .58 | .50 | .63 | .62 | .65 | .76 |
| 1922 | .65 | .74 | .79 | .75 | .57 | .62 | .66 | .71 | .69 | .68 | .47 | .42 | .65 |
| 1923 | .48 | .61 | .53 | .44 | .47 | .50 | .42 | .36 | .52 | .55 | .42 | .50 | .48 |
| 1924 | .64 | .56 | .64 | .43 | .54 | .64 | .55 | .41 | .67 | .52 | .54 | .40 | .54 |
| 1925 | .44 | .42 | .42 | .52 | .47 | .74 | .55 | .61 | .71 | .82 | .48 | .57 | .56 |
| 1926 | .84 | .85 | .85 | .75 | .60 | .53 | .49 | .50 | .75 | .67 | .46 | .54 | .65 |
| 1927 | .62 | .66 | .80 | .60 | .65 | .47 | .56 | .61 | .77 | .84 | .35 | .63 | .63 |
| 1928 | .44 | .62 | .48 | .52 | .75 | .72 | .72 | .56 | .75 | .83 | .65 | .54 | .63 |
| 1929 | .47 | .82 | .85 | .54 | .61 | .56 | .66 | .55 | .75 | .85 | .71 | .71 | .67 |
| 1930 | .65 | .49 | .35 | .38 | .37 | .29 | .22 | .25 | .32 | .34 | .36 | .26 | .37 |
| 1931 | .54 | .62 | .59 | .45 | .54 | .65 | .55 | .68 | .82 | .95 | .83 | .74 | .66 |

* Compiled from annual reviews of the "Caractère magnétique de chaque jour," prepared by the Royal Meteorological Institute of the Netherlands for the International Commission for Terrestrial Magnetism.

TABLE 748.—Elements and Constants of Atmospheric Electricity

(Prepared by O. H. Gish, Department of Terrestrial Magnetism, Carnegie Institution of Washington, 1930.)

The elements of atmospheric electricity show variations, both regular and irregular. Over land the irregular variations are very pronounced and the regular variations differ notably from place to place, in marked contrast to the corresponding characteristics over the ocean. Therefore, and because of the wider and more uniform geographical distribution of ocean observations, it seems best to give the greater weight to the ocean data when attempting to arrive at values characterizing world-wide conditions. Because of the wide variation from place to place in the means from land stations, due to local factors, a general mean of these is of questionable significance. Hence it seems better to indicate the extremes of station means in the case of elements for which the data are sufficiently abundant.

Certain disparities which will be found between these and other published tables [see references (2) and (21)] arise largely from the inclusion of more recent data. The references to authorities have been selected with a view to being helpful in following up the literature rather than to assigning due credit for the original investigations.

Of the atmospheric-electric elements the potential gradient has been the most extensively observed. The sign of the average gradient is everywhere such as to drive positive ions toward the earth. The periodic variations in this element are of great interest because of their apparent relation with cosmic phenomena. Thus the potential gradient apparently increases with increase in the Wolfer sun-spot numbers, varies throughout the year, the maxima in monthly means occur everywhere, with few exceptions, at the time of northern winter, and the corresponding minima occur at the time of northern summer. The diurnal variation observed over the oceans is everywhere in phase when considered on a common-time basis, except for a minor phase-shift that depends upon the season. This diurnal variation derived from observations made on the *Carnegie* during 1915 to 1921 is given by the Fourier expression¹ $\Delta P/P = 0.15 \sin(\theta + 186^\circ) + 0.03 \sin(2\theta + 237^\circ)$ where θ is reckoned at 15° per hour beginning at 0^h Greenwich mean civil time.

No general expression that will approximately characterize the diurnal variation over land can be given. There variations determined by local factors are apparently superimposed upon a variation of the same world-wide character as that found to prevail over the oceans [see reference (5)].

¹ From revised calculations in unpublished manuscript of the Department of Terrestrial Magnetism.

TABLE 749.—Atmospheric-Electric Data

| Element | Symbol | Means | Units | Variations | Author- ity |
|---|-----------------------------------|--|-------------------------------------|--|------------------------|
| Potential gradient..... | P | Land: 67 to 317 Sea: 128 Free air..... | volts/m " " | Range Per cent of mean Annual 22 to 145 Diurnal 35 to 120 Annual 13 Diurnal 35 Percentage of surface values at various altitudes 0 km 100 6 km 8 3 " 17 9 " 4 | 3 4, 5 1, 2 1 |
| Air-conductivity total..... | $\lambda = \lambda_+ + \lambda_-$ | Land: 1 to 5 Sea: 2.6 Free air..... | c.g.s.e. $\times 10^{-4}$ " " | Variations determined chiefly by local factors Variations small and chiefly irregular Ratio of value at various altitudes to that at surface 0 km 1 6 km 20 3 " 8 9 " 38 | 3, 6 1 7 |
| Ratio of positive to negative conductivity.. | λ_+/λ_- | Land: 1.12 Sea: 1.26 | | | 3, 6 1 |
| Air-earth current density..... | $i = \lambda P/30000$ | Land: 7.0 Sea: 11.0 | c.g.s.e. $\times 10^{-7}$ | | 3 1 |
| Density of small ions: Positive | n_+ | Land: 750 Sea: 600 | ions/cm ³ | | 3, 6 1 |
| Negative | n_- | Land: 650 Sea: 500 | " | | 3, 6 1 |
| | $(n_+ + n_-)/2$ | Free air..... | | Values at various altitudes 2 km 1300 4 " 1900 5 " 2300 | 10 |
| Ratio of positive to negative ionic density.. | $p = n_+/n_-$ | Land: 1.23 Sea: 1.23 | | | 3, 6 1 |

TABLE 749 (continued).—Atmospheric-Electric Data

| Element | Symbol | Means | Units | Authority |
|--------------------------------|--|---|--|---|
| Space-charge, over land | ρ $\rho = - \left(\frac{dP}{dh} / 1.2\pi \right) \times 10^{-10}$ (For h = height in km) | At surface:* - 2000 to + 1000 Free air: 0 to 3 km 3 to 6 6 to 9 | 10^{-10} c.g.s.e./cm ³ " " " | 3 |
| Mobility of small ions: | $k_+ = \lambda_+ / 300 en_+$ | | | |
| Positive | k_+ | Land: 0.9 Sea: 1.6 | cm/sec./volt/cm " | 3, 6 1 |
| Negative | k_- | Land: 1.0 Sea: 1.7 | " " | 3, 6 1 |
| Rate of formation of ion-pairs | q | Over land: Ra and Th products in air α rays 4.6 β rays 0.2 γ rays 0.15 Radioactive matter in the Earth's crust β rays 0.1 γ rays 3.0 Penetrating radiation 1.5 Total 9.55 At sea: Penetrating radiation 1.5 (?) 0.7 Total 2.2 | ions/cm ³ /sec. " " " " " " " " | 3, 6 8 |

* The sign and magnitude of surface values are exceedingly variable from place to place.

TABLE 750.—Ionic equilibrium in the atmosphere

Equilibrium for atmospheric ionization occurs when $q = \alpha n^2 + \eta_1 N_0 n + \eta_2 N n$, where n and N are the number of pairs of small and large ions, and N_0 the number of uncharged nuclei; α , η_1 , η_2 , are coefficients of recombination of small ions with small ions, with uncharged nuclei, and with large ions. If for both small and large ions the positive and negative are equally abundant, then $N_0/N = \eta_2/\eta_1 = 1.28$ [reference (12)]. When $n/N \ll 2\eta_2/\alpha$, the equilibrium-condition is expressed by $q = \beta n$; β is designated the diminution-constant; $1/\beta = \Theta$ is the "average life" of a small ion in air which contains an abundance of large ions; Θ varies inversely as N .

α : 1.55×10^{-6} cm³/sec. [see reference (11)]

η_1 : 5×10^{-6} " } [see references (8), (12), (13)]

η_2 : 6×10^{-6} " }

Θ : Over land,

Average, 30 sec.

Extremes, 10 to 60 sec. } [see reference (8)]

Over sea, 230 sec.

N : Over land, 500 to 50,000 ions/cm³ [see references (13), (14)]

Aitken nuclei, number per cm³:

Over open country, up to 10^5 [see reference (16)]

Over mid-ocean, about 800 [see reference (15)]

In free air,

Altitude 1 km 6,000 5 km 50 } see reference (17)
3 km 200 8.5 km about 5 }

TABLE 751.—Thunderstorm Electricity

| | |
|--|-------------------------|
| Quantity discharged by a lightning flash: 10 to 50 coulombs; average 20 coulombs. | } [see reference (18)]. |
| Energy of a lightning flash: 10^{17} ergs. | |
| Potential difference between discharge points: 10^9 volts. | |
| Potential gradient at earth's surface beneath a thundercloud: 10^4 volts/meter. (The charge producing this field more frequently negative than positive). | |
| Number of lightning discharges over entire earth each second: At least 100. | |
| Duration of lightning flash: More than 0.001 sec [see reference (19)]. | |

TABLE 752.—Charge on Rain and Snow

Specific net charge on precipitation:

| | |
|-----------------------------------|------------------------|
| Average, 0.5 c.g.s.e./gm. | } [see reference (3)]. |
| Maximum observed, 20 c.g.s.e./gm. | |

Specific charge on individual raindrops or snowflakes:

| | |
|------------------------------------|-------------------------|
| Rain, + 2.7 to - 3.2 c.g.s.e./gm. | } [see reference (20)]. |
| Snow, + 11.6 to - 8.1 c.g.s.e./gm. | |

References

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For current literature consult Journal of Terrestrial Magnetism and Atmospheric Electricity, Baltimore (vol. 38 in progress 1933), and Zeitschrift für Geophysik, Braunschweig.

TABLE 753.—Ionization in the Upper Atmosphere of the Earth

(Hulburt, Phys. Rev., 34, 1167, 1929; 35, 24, 1930; 37, 1, 1931.)

Each cm^3 of the upper atmosphere is assumed approximately electrically neutral. Above 60 km the ionization is assumed to be caused by solar ultra-violet light; below, by cosmic radiation. At any height z km above sea-level, let the numbers per cm^3 of singly-charged positive ions, negative ions and electrons be y_+ , y_- and y_e . Then $y_+ = y_- + y_e$, and since y_e is in general small compared to y_- , the values of y_+ and y_- are nearly equal. Above 60 km the positive ion densities y_+ are given in Table 754. The electron density y_e increases with z to a max. value $y_{e\text{ max}}$ at a height z_m ; $y_{e\text{ max}}$ and z_m are given in Table 754a. Above and below the max. y_e can not yet be estimated with certainty. The values for y_+ and $y_{e\text{ max}}$ may be correct within a factor of 2; a zero value means a small value. The tables are for average equinoctial conditions and solar quiescence, halfway between the periods of max. and min. solar activity. The values should be increased and reduced by roughly 25% to refer to epochs of max. and min. solar activity. During magnetic storms the ionization increases, being perhaps double the tabular values for a severe storm. In polar regions it is probably not greatly different from that for latitude 60° . The seasonal changes are small at the equator. In temperate latitudes for winter and summer use the values for latitudes about 20° higher and lower. Below 60 km the ionization due to cosmic radiation is independent of the latitude, hour of the day, solar activity, etc., and y is 8×10^2 , 1.6×10^3 , 1.9×10^3 , 2.2×10^3 , 2.9×10^3 , and 3.5×10^3 at 0, 10, 20, 30, 40, and 50 km.

TABLE 754.—Ion Density y_+ in the Upper Atmosphere

| | z | Geographic latitude. | | |
|--------------------|--------|----------------------|-------------------|-------------------|
| | | 0° | 40° | 60° |
| Noon | 200 km | 0 | 0 | 0 |
| | 190 | 4.7×10^9 | 4.0×10^9 | 0 |
| | 180 | 4.7×10^9 | 4.0×10^9 | 0 |
| | 170 | 4.7×10^9 | 4.0×10^9 | 3.1×10^9 |
| | 160 | 4.7×10^9 | 4.0×10^9 | 3.1×10^9 |
| | 150 | 4.7×10^9 | 4.0×10^9 | 3.1×10^9 |
| | 140 | 7.0×10^8 | 4.0×10^8 | 3.1×10^9 |
| | 130 | 2.3×10^8 | 1.4×10^8 | 3.1×10^9 |
| | 120 | 9.1×10^7 | 6.7×10^7 | 5.1×10^7 |
| | 110 | 3.6×10^7 | 2.7×10^7 | 2.3×10^7 |
| | 100 | 1.4×10^7 | 1.2×10^7 | 7.1×10^6 |
| | 90 | 5.8×10^6 | 5.4×10^6 | 2.7×10^6 |
| | 80 | 2.1×10^6 | 1.6×10^6 | 1.1×10^6 |
| 3 p. m. or 9 a. m. | 200 km | 0 | 0 | 0 |
| | 190 | 3.0×10^9 | 0 | 0 |
| | 180 | 3.0×10^9 | 2.8×10^9 | 0 |
| | 170 | 3.0×10^9 | 2.8×10^9 | 2.3×10^9 |
| | 160 | 3.0×10^9 | 2.8×10^9 | 2.3×10^9 |
| | 150 | 3.0×10^9 | 2.8×10^9 | 2.3×10^9 |
| | 140 | 2.8×10^8 | 2.8×10^8 | 2.3×10^9 |
| | 130 | 1.1×10^8 | 4.0×10^8 | 2.3×10^9 |
| | 120 | 4.6×10^7 | 1.0×10^8 | 1.1×10^8 |
| | 110 | 1.9×10^7 | 3.4×10^7 | 3.7×10^7 |
| | 100 | 9.1×10^6 | 1.2×10^7 | 1.1×10^7 |
| | 90 | 2.8×10^6 | 4.5×10^6 | 3.1×10^6 |
| | 80 | 1.2×10^6 | 1.8×10^6 | 1.0×10^6 |
| 6 p. m. or 6 a. m. | 150 km | 0 | 0 | 0 |
| | 140 | 1.7×10^9 | 0 | 0 |
| | 135 | 1.7×10^9 | 1.7×10^9 | 1.6×10^9 |
| | 130 | 1.7×10^9 | 1.7×10^9 | 1.6×10^9 |
| | 120 | 1.7×10^9 | 1.7×10^9 | 1.6×10^9 |
| | 115 | 1.7×10^9 | 1.7×10^9 | 1.6×10^9 |
| | 110 | 5.1×10^7 | 1.7×10^9 | 1.6×10^9 |
| | 100 | 1.3×10^7 | 1.9×10^7 | 1.4×10^7 |
| | 90 | 2.9×10^6 | 3.9×10^6 | 3.4×10^6 |
| | 80 | 8.0×10^5 | 8.4×10^5 | 8.1×10^5 |

TABLE 754 (continued).—Ion Density y_e in the Upper Atmosphere

| | z | Geographic latitude. | | |
|----------|--------|----------------------|-------------------|-------------------|
| | | 0° | 40° | 60° |
| 9 p. m. | 170 km | 0 | 0 | 0 |
| | 160 | 1.7×10^9 | 0 | 0 |
| | 150 | 1.7×10^9 | 0 | 0 |
| | 140 | 0 | 1.7×10^9 | 1.6×10^9 |
| | 130 | 0 | 1.7×10^9 | 1.6×10^9 |
| | 120 | 0 | 0 | 0 |
| | 115 | 5.2×10^7 | 0 | 0 |
| | 110 | 2.4×10^7 | 3.8×10^7 | 3.3×10^7 |
| | 100 | 5.9×10^6 | 1.0×10^7 | 9.2×10^6 |
| | 90 | 1.3×10^6 | 2.1×10^6 | 1.9×10^6 |
| | 80 | 3.8×10^5 | 5.1×10^5 | 4.6×10^5 |
| Midnight | 170 km | 0 | 0 | 0 |
| | 160 | 1.6×10^9 | 0 | 0 |
| | 150 | 1.6×10^9 | 0 | 0 |
| | 145 | 0 | 1.2×10^9 | 1.1×10^9 |
| | 135 | 0 | 1.2×10^9 | 1.1×10^9 |
| | 125 | 0 | 0 | 0 |
| | 115 | 3.4×10^7 | 0 | 0 |
| | 110 | 1.6×10^7 | 2.3×10^7 | 2.1×10^7 |
| | 100 | 3.6×10^6 | 2.3×10^6 | 6.5×10^6 |
| | 90 | 8.7×10^5 | 1.8×10^6 | 1.3×10^6 |
| | 80 | 4.6×10^5 | 3.7×10^5 | 3.1×10^5 |
| 3 a. m. | 170 km | 0 | 0 | 0 |
| | 160 | 1.5×10^9 | 0 | 0 |
| | 150 | 1.5×10^9 | 0 | 0 |
| | 145 | 0 | 1.0×10^9 | 9.0×10^8 |
| | 135 | 0 | 1.0×10^9 | 9.0×10^8 |
| | 125 | 0 | 0 | 0 |
| | 115 | 2.4×10^7 | 0 | 0 |
| | 110 | 1.0×10^7 | 1.5×10^7 | 1.4×10^7 |
| | 100 | 3.1×10^6 | 5.3×10^6 | 4.9×10^6 |
| | 90 | 5.5×10^5 | 1.1×10^6 | 9.4×10^5 |
| | 80 | 1.9×10^5 | 2.8×10^5 | 2.2×10^5 |

TABLE 754A.—Maximum Electron Density y_e Max. in the Upper Atmosphere

| | Geographic latitude | | | | | |
|----------|---------------------|-------------------------|--------|--------------------------|--------|--------------------------|
| | Z_m | 0° y_e max. | Z_m | 40° y_e max. | Z_m | 60° y_e max. |
| Noon | 195 km | 3.2×10^5 | 195 km | 2.4×10^5 | 175 km | 1.6×10^5 |
| 3 p. m. | 195 | 2.5×10^5 | 195 | 1.9×10^5 | 175 | 1.3×10^5 |
| 6 p. m. | 144 | 1.2×10^5 | 140 | 0.9×10^5 | 140 | 0.6×10^5 |
| 9 p. m. | 165 | 1.1×10^5 | 145 | 0.1×10^5 | 145 | 0 |
| Midnight | 165 | 1.0×10^5 | 145 | 0 | 145 | 0 |
| 3 a. m. | 165 | 0.8×10^5 | 145 | 0 | 145 | 0 |
| 6 a. m. | 144 | 1.0×10^5 | 140 | 0.8×10^5 | 140 | 0.5×10^5 |
| 9 a. m. | 195 | 2.0×10^5 | 195 | 1.5×10^5 | 175 | 1.0×10^5 |

TABLE 755

MISCELLANEOUS ASTRONOMICAL DATA

| | | | |
|---|---|---|--------------------------------|
| Tropical (ordinary) year | = | $\{ 365.24219879 - 0.0000000614 (t - 1900) \}$ | days. |
| Sidereal year | = | $\{ 365.25636042 + 0.000000011 (t - 1900) \}$ | days. |
| Anomalistic year | = | $\{ 365.25664134 + 0.0000000304 (t - 1900) \}$ | days. |
| Eclipse year | = | $\{ 346.620000 + 0.00000036 (t - 1900) \}$ | days. |
| Synodical (ordinary) month | = | $\{ 29.530588102 - 0.00000000294 (t - 1900) \}$ | days. |
| Sidereal month | = | $\{ 27.321660890 - 0.00000000252 (t - 1900) \}$ | days. |
| Sidereal day (ordinary, two successive transits of vernal equinox, might be called equinoctial day) | | $= 86164.09054$ | mean solar seconds. |
| | | $= 23$ h. 56 m. 4.09054 | mean solar time. |
| Two successive transits of same fixed star | | $= 86164.09966$ | mean solar seconds. |
| 1930, Julian Period | | $= 6643$. | |
| January 1, 1933, Julian-day number | | $= 2427074$. | See p. 603. |
| Solar parallax | | $= 8.7958'' \pm 0.002''$ (Weinberg). | |
| | | 8.807 ± 0.0027 (Hincks, Eros). | |
| | | 8.799 (Sampson, Jupiter satellites; Harvard observations). | |
| | | 8.80 Paris conference; $8.8032'' \pm 0.0013$.* | |
| Lunar parallax | | $= 3422.63'' = 57' 2.63''$ (Newcomb). | |
| " | | $= \pi = 3422.519'' \pm 0.009$ (De Sitter).* | |
| Mean distance earth to sun | | $= 149500000$ kilometers | $= 92900000$ miles. |
| Mean distance earth to moon | | $= 60.2678$ terrestrial radii. | |
| | | $= 384411$ kilometers | $= 238862$ miles. |
| Light traverses mean radius of earth's orbit in | | 498.7 | sec. |
| Velocity of light (mean value) in vacuo, | | 299796 ± 4 km/sec. | (Michelson). |
| Constant of aberration | | $= 20.4874'' \pm 0.005''$. | |
| | | 20.47 Paris conference (work of Doolittle and others indicates value not less than 20.51). | |
| Light year | | $= 9.5 \times 10^{12}$ kilometers | $= 5.9 \times 10^{12}$ miles. |
| Parsec, distance star whose parallax is 1 sec. | | $= 31 \times 10^{12}$ km | $= 19.2 \times 10^{12}$ miles. |
| General precession | | $= 50.2564'' + 0.000222 (t - 1900)''$ (Newcomb). | |
| General precession | | $50.2486'' \pm 0.0010$ (De Sitter, 1927). | |
| Planetary precession | | $= \lambda = 0.1228'' \pm 0.0012$ (De Sitter, 1927). | |
| Lunar-solar precession | | $= p' = 50.3714'' \pm 0.0016$ (De Sitter, 1927). | |
| | | Of this $0.0191''$, Einstein, orbital motion earth.* | |
| True lunar-solar precession | | $= p = 50.3523$, sun, moon, earth's attraction.* | |
| Obliquity of ecliptic | | $= 23^\circ 27' 8.26'' - 0.4684 (t - 1900)''$ (Newcomb). | |
| Constant of nutation | | $= 9.21''$ (Paris conference); $9.208'' \pm 0.003$.* | |
| Constant in long. | | $= \Delta\phi = (-17.234'' - .017''T) \sin \Omega$ Jackson, | |
| Constant in obliquity | | $= \Delta\epsilon = (+9.218 + .0000T) \cos \Omega$ M. N., 1930. | |
| | | Latter has relativity correction; T centuries from 1900. | |
| Gravitation constant | | $= (6.670 \pm 0.002) \times 10^{-8}$ dyne $\text{cm}^2 \text{g}^{-2}$ (Heyl, 1930). | |
| Eccentricity earth's orbit | | $= e = 0.01675104 - 0.0000004180 (t - 1900) - 0.000000000126 (t - 1900)^2$. | |
| Eccentricity moon's orbit | | $= e_2 = 0.05490056$ (Brown). | |
| Inclination moon's orbit | | $= I = 5^\circ 8' 43.5''$ (Brown). | |
| Delaunay's $\gamma = \sin \frac{1}{2}I$ | | $= 0.04488716$ (Brown). | |
| Lunar inequality of earth | | $= L = 6.454''$; 6.459 ± 0.005 .* | |
| Parallactic inequality moon | | $= Q = 124.785''$ (Brown). | |
| Mean sidereal motion of moon's node in 365.25 days | | $= -19^\circ 21' 19.3838'' + 0.001294 (t - 1900)''$. | |
| Pole of Milky Way | | $=$ R. A., 12 h. 48 m.; Dec., $+27^\circ$. See p. 604. | |
| d (lunar perigee) | | $= +6.386''$. | |
| d (lunar node) | | $= -5.977''$. | |

* De Sitter, Bull. Astron. Inst., Netherlands, 4, 57, 1927.

MISCELLANEOUS ASTRONOMICAL DATA AND FORMULAE

If δ = declination, t , hour angle measured west from meridian, h , altitude, ϕ , latitude and A , azimuth measured from S. point through W. Then

$$\left. \begin{aligned} \sin h &= \sin \phi \sin \delta + \cos \phi \cos \delta \cos t \\ \cos h \cos A &= -\cos \phi \sin \delta + \sin \phi \cos \delta \cos t \\ \cos h \sin A &= \cos \delta \sin t \end{aligned} \right\} \text{given } \delta, t, \phi$$

$$\left. \begin{aligned} \sin \delta &= \sin \phi \sin h - \cos \phi \cos h \cos A \\ \cos \delta \cos t &= \cos \phi \sin h + \sin \phi \cos h \cos A \\ \cos \delta \sin t &= \cos h \sin A \end{aligned} \right\} \text{given } h, A, \phi$$

Refraction.— r in (") = $[983 \times (\text{barometer in in.}) / (460 + t^\circ \text{ F.})] \tan Z$, where Z = zenith distance. Error $< 1''$, $Z < 75^\circ$, ordinary t and pressure.

Twilight.—Considered to end when 1st mag. star is visible in zenith. Lasts until sun is about 18° below horizon; lat. 40° , equivalent to about $1\frac{1}{2}$ to 2 hr.; latitude $> 50^\circ$, lasts until midnight.

Dip of horizon.—In minutes of arc = $\sqrt{\text{elevation in ft.}}$

Horizon.—Distance at sea is approximately, miles = $\sqrt{\frac{3}{2}h}$ in feet; no account taken of refraction, actual distance greater.

Date line.— 180° from meridian of Greenwich. Ships crossing it from the east, skip a day; going east, count same day twice.

Velocity, equatorial point on earth.—Because of rotation: 1000 mi./hr. = 1500 ft./sec. = 1600 km/m = 450 m/sec. In orbit: 18.5 mi./sec. = 30 km/sec.

Latitude variation.—Direction of axis of the earth in space is invariable but a variation in latitude is caused by a shift of the earth's body about this axis. There are two components, one, annual (narrow ellipse, varying in form and position, about 10 m long on the earth's surface) probably meteorological in origin; the other, circular, about 8 m in diameter, period 433 days, due to noncoincidence of axis of figure and of rotation.

Magnitudes.—(Apparent, m). The light of an average 1st magnitude star was found to be physically 100 times as intense as that of a 6th. $\sqrt[5]{100}$ or 2.512 has been adopted as the light ratio between two stars differing in magnitude by unity ($\log_{10} 0.400 = 2.512$). If l_m = approximate brightness of star of magnitude m , l_n of n , then, $l_n/l_m = (2.512)^{m-n}$ whence

$$m - n = 2.5 (\log l_n - \log l_m); \text{ if } l_0 = \text{brightness 0 mag. star } \log (\log m / \log_0) = -0.4 m.$$

Magnitudes.—("Absolute," M .) The "absolute" magnitude of a star is its magnitude reduced to a standard distance, 10 parsecs (Int. Astron. Union, 1922). $M - m = 2.5 (\log \text{amt. light rec'd}) / (\log \text{amt. if at unit distance}) = 5 \log p - 5 \log p_0$ where p , p_0 are observed parallax and that for standard distance; $p_0 = 0.1$. $M = m + 5 + 5 \log p$. β Orionis, $M = -5.5$ is brightest star.

Color index.—We have visual, photographic, and bolometric (radiometric) magnitudes. The zero of the photographic scale is taken so that both the photographic and visual scale coincide, on the average, for stars of spectrum class AO and $m = 5.5$ to 6.5. Difference of magnitudes on the two scales is the color index, photovisual is + for red, — for blue stars and may amount to + 2.0 mag.

Heat index.—Radiometric (heat or bolometric), zero taken to agree with Class AO, (radiometric — visual magnitude) = heat index, + for red stars.

Purkinje effect.—Two colored lights appearing equally bright at a certain brightness, when brightness decreased equally physically, the bluer appears brighter.

CALENDARS

TABLE 757.—Julian Day Calendar

Proposed by Scaliger, 1582. Days are numbered consecutively from Greenwich mean noon on January 1, 4713 B. C. Advantage: difference between two dates becomes merely difference between two Julian day numbers. As our civil and astronomical days begin at midnight, the numbers from the table must be increased by one after noon of date.

Julian Day No. = 2420000 + no. in table. Jan. 0, etc., at head of col. means Jan. 0 until noon, then Jan. 1, etc.

| Year | Jan. 0 | Feb. 0 | Mar. 0 | Apr. 0 | May 0 | June 0 | July 0 | Aug. 0 | Sept. 0 | Oct. 0 | Nov. 0 | Dec. 0 |
|-----------|--------|--------|--------|--------|-------|--------|--------|--------|---------|--------|--------|--------|
| 1920..... | 2324 | 2355 | 2384 | 2415 | 2445 | 2476 | 2506 | 2537 | 2568 | 2598 | 2629 | 2659 |
| 1921..... | 2690 | 2721 | 2749 | 2780 | 2810 | 2841 | 2871 | 2902 | 2933 | 2963 | 2994 | 3024 |
| 1922..... | 3055 | 3086 | 3114 | 3145 | 3175 | 3206 | 3236 | 3267 | 3298 | 3328 | 3359 | 3389 |
| 1923..... | 3420 | 3451 | 3479 | 3510 | 3540 | 3571 | 3601 | 3632 | 3663 | 3693 | 3724 | 3754 |
| 1924..... | 3785 | 3816 | 3845 | 3876 | 3906 | 3937 | 3967 | 3998 | 4029 | 4059 | 4090 | 4120 |
| 1925..... | 4151 | 4182 | 4210 | 4241 | 4271 | 4302 | 4332 | 4363 | 4394 | 4424 | 4455 | 4485 |
| 1926..... | 4516 | 4547 | 4575 | 4606 | 4636 | 4667 | 4697 | 4728 | 4759 | 4789 | 4820 | 4850 |
| 1927..... | 4881 | 4912 | 4940 | 4971 | 5001 | 5032 | 5062 | 5093 | 5124 | 5154 | 5185 | 5215 |
| 1928..... | 5246 | 5277 | 5306 | 5337 | 5367 | 5398 | 5428 | 5459 | 5490 | 5520 | 5551 | 5581 |
| 1929..... | 5612 | 5643 | 5671 | 5702 | 5732 | 5763 | 5793 | 5824 | 5855 | 5885 | 5916 | 5946 |
| 1930..... | 5977 | 6008 | 6036 | 6067 | 6097 | 6128 | 6158 | 6189 | 6220 | 6250 | 6281 | 6311 |
| 1931..... | 6342 | 6373 | 6401 | 6432 | 6462 | 6493 | 6523 | 6554 | 6585 | 6615 | 6646 | 6676 |
| 1932..... | 6707 | 6738 | 6767 | 6798 | 6828 | 6859 | 6889 | 6920 | 6951 | 6981 | 7012 | 7042 |
| 1933..... | 7073 | 7104 | 7132 | 7163 | 7193 | 7224 | 7254 | 7285 | 7316 | 7346 | 7377 | 7407 |
| 1934..... | 7438 | 7469 | 7497 | 7528 | 7558 | 7589 | 7619 | 7650 | 7681 | 7711 | 7742 | 7772 |
| 1935..... | 7803 | 7834 | 7862 | 7893 | 7923 | 7954 | 7984 | 8015 | 8046 | 8076 | 8107 | 8137 |
| 1936..... | 8168 | 8199 | 8228 | 8259 | 8289 | 8320 | 8350 | 8381 | 8412 | 8442 | 8473 | 8503 |
| 1937..... | 8534 | 8565 | 8593 | 8624 | 8654 | 8685 | 8715 | 8746 | 8777 | 8807 | 8838 | 8868 |
| 1938..... | 8899 | 8930 | 8958 | 8989 | 9019 | 9050 | 9080 | 9111 | 9142 | 9172 | 9203 | 9233 |
| 1939..... | 9264 | 9295 | 9323 | 9354 | 9384 | 9415 | 9445 | 9476 | 9507 | 9537 | 9568 | 9598 |
| 1940..... | 9629 | 9660 | 9688 | 9720 | 9750 | 9781 | 9811 | 9842 | 9873 | 9903 | 9934 | 9964 |

TABLE 758.—Perpetual Calendar

To find the calendar for any year, e.g., 1924, divide century part of year (19) by 4 and with the remainder (3) enter Dominical Letters table. Use line (3) of lower sections of table corresponding to value of remainder, taking the Dominical Letter corresponding to the column in upper parts of table containing the last two figures of the year in question (24). This being a leap year we find two letters (F) to be used with Jan. and Feb., (E) with the rest of the year. In the second part of the table this Dominical Letter indicates which schedule of week days is to be used with the month in question. E.g., Jan. 1, 1924, comes on Tuesday; July 4 on Friday.

| Year No. | { | 00 | 01 | 02 | 03 | 04 | 05 | 06 | 07 | 08 | 09 | 10 | 11 | 12 | 13 | 14 | 15 |
|------------------|----|------------------|----|----|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|----|
| | | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | |
| | | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | |
| | | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | |
| (1) | C | B | A | G | FE | D | C | B | AG | F | E | D | CB | A | G | F | |
| (2) | E | D | C | B | AG | F | E | D | CB | A | G | F | ED | C | B | A | |
| (3) | G | F | E | D | CB | A | G | F | ED | C | B | A | GF | E | D | C | |
| (4) | BA | G | F | E | DC | BA | C | A | FE | D | C | B | AG | E | D | C | |
| Year No. | { | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | | | |
| | | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | | | |
| | | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | | | |
| | | | | | | | | | | | | | | | | | |
| (1) | ED | C | B | A | GF | E | D | C | BA | G | F | E | DC | | | | |
| (2) | GF | E | D | C | BA | G | F | E | DC | B | A | G | FE | | | | |
| (3) | BA | G | F | E | DC | B | A | G | FE | D | C | B | AG | | | | |
| (4) | CB | A | G | F | ED | C | B | A | GF | E | D | C | BA | | | | |
| Month | | Dominical letter | | | | | | | | | | | | | | | |
| Jan., Oct. | | A | B | C | D | E | F | G | A | B | C | D | E | F | G | A | |
| Feb., Mar., Nov. | | D | E | F | G | A | B | C | D | E | F | G | A | B | C | D | |
| Apr., July | | G | A | B | C | D | E | F | G | A | B | C | D | E | F | G | |
| May | | C | D | E | F | G | A | B | C | D | E | F | G | A | B | C | |
| June | | E | F | G | A | B | C | D | E | F | G | A | B | C | D | E | |
| Aug. | | F | G | A | B | C | D | E | F | G | A | B | C | D | E | F | |
| Sept., Dec. | | A | B | C | D | E | F | G | A | B | C | D | E | F | G | A | |
| 1 | 8 | 15 | 22 | 29 | Sun. | Sat. | Fri. | Thurs. | Wed. | Tues. | Mon. | Sun. | Sat. | Fri. | Thurs. | Wed. | |
| 2 | 9 | 16 | 23 | 30 | Mon. | Sun. | Sat. | Fri. | Thurs. | Wed. | Tues. | Mon. | Sun. | Sat. | Fri. | Thurs. | |
| 3 | 10 | 17 | 24 | 31 | Tues. | Mon. | Sun. | Sat. | Fri. | Thurs. | Wed. | Tues. | Mon. | Sun. | Sat. | Fri. | |
| 4 | 11 | 18 | 25 | | Wed. | Tues. | Mon. | Sun. | Sat. | Fri. | Thurs. | Wed. | Tues. | Mon. | Sun. | Sat. | |
| 5 | 12 | 19 | 26 | | Thurs. | Wed. | Tues. | Mon. | Sun. | Sat. | Fri. | Thurs. | Wed. | Tues. | Mon. | Sun. | |
| 6 | 13 | 20 | 27 | | Fri. | Thurs. | Wed. | Tues. | Mon. | Sun. | Sat. | Fri. | Thurs. | Wed. | Tues. | Mon. | |
| 7 | 14 | 21 | 28 | | Sat. | Fri. | Thurs. | Wed. | Tues. | Mon. | Sun. | Sat. | Fri. | Thurs. | Wed. | Tues. | |

Month

Dominical letter

Jan., Oct.
Feb., Mar., Nov.
Apr., July
May
June
Aug.
Sept., Dec.

A
D
G
B
E
C
F

B
E
A
C
F
D
G

C
F
B
D
G
E
A

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F
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D

G
C
F
A
D
B
E

1 8 15 22 29
2 9 16 23 30
3 10 17 24 31
4 11 18 25
5 12 19 26
6 13 20 27
7 14 21 28

Sun.
Mon.
Tues.
Wed.
Thurs.
Fri.
Sat.

Sat.
Sun.
Mon.
Tues.
Wed.
Thurs.
Fri.

Fri.
Sat.
Sun.
Mon.
Tues.
Wed.
Thurs.

Thurs.
Fri.
Sat.
Sun.
Mon.
Tues.
Wed.

Wed.
Thurs.
Fri.
Sat.
Sun.
Mon.
Tues.

Tues.
Wed.
Thurs.
Fri.
Sat.
Sun.
Mon.

Mon.
Tues.
Wed.
Thurs.
Fri.
Sat.
Sun.

NOTE.—For general discussion of calendars, see British Nautical Almanac, p. 734 et seq., 1931.

RIGHT ASCENSION, DECLINATION INTO GALACTIC COORDINATES

Condensed from Tavole calcolate dal Emanuelli (1929), Secretario della Specola Vaticano. Galactic pole, R. A., 191.1° , dec. $+26.6^\circ$ (Newcomb, 1904). The zero point of the tables takes the longitude of the solar apex as 0° (R. A., 270° , dec., $+30^\circ$, 1900). To reduce the galactic longitude as reckoned from the intersection of the galactic plane with equator, add 23.6° to "Long."; as reckoned from α Cygni (proposed by Int. Astron. Union, 1925), add $+27.9$, 1900, ($+23.7$, 1930).

| R. A. Dec. | ^{0h} | | ^{1h} | | ^{2h} | | ^{3h} | | ^{4h} | |
|---------------|---------------|-------|---------------|-------|---------------|-------|---------------|-------|---------------|-------|
| | Long. | Lat. | Long. | Lat. | Long. | Lat. | Long. | Lat. | Long. | Lat. |
| +90 | 66.4 | +26.8 | 66.4 | +26.8 | 66.4 | +26.8 | 66.4 | +26.8 | 66.4 | +26.8 |
| +80 | 64.4 | +17.0 | 67.1 | +16.8 | 69.8 | +17.3 | 72.3 | +18.4 | 74.4 | +20.0 |
| +70 | 62.6 | +7.1 | 67.7 | +6.8 | 72.8 | +7.7 | 77.6 | +9.8 | 81.7 | +12.9 |
| +60 | 60.9 | -2.7 | 68.4 | -3.1 | 75.7 | -1.8 | 82.6 | +1.2 | 88.7 | +5.6 |
| +50 | 59.2 | -12.6 | 69.0 | -13.1 | 78.7 | -11.4 | 87.6 | -7.5 | 95.4 | -1.8 |
| +40 | 57.2 | -22.4 | 69.7 | -23.1 | 81.8 | -20.9 | 92.8 | -16.1 | 102.2 | -9.2 |
| +30 | 55.0 | -32.2 | 70.4 | -33.1 | 85.4 | -30.4 | 98.5 | -24.6 | 109.3 | -16.4 |
| +20 | 52.3 | -42.0 | 71.4 | -43.1 | 89.7 | -39.7 | 105.0 | -32.8 | 116.9 | -23.4 |
| +10 | 48.6 | -51.6 | 72.8 | -53.0 | 95.4 | -48.9 | 112.8 | -40.6 | 125.4 | -30.0 |
| 0 | 42.9 | -61.1 | 75.0 | -62.9 | 103.6 | -57.6 | 122.6 | -47.8 | 134.9 | -35.9 |
| -10 | 32.4 | -70.2 | 79.5 | -72.8 | 116.7 | -65.5 | 135.2 | -53.9 | 146.0 | -41.0 |
| -20 | 7.8 | -77.8 | 94.9 | -82.3 | 139.0 | -71.4 | 151.3 | -58.2 | 158.6 | -44.9 |
| -30 | 315.7 | -79.7 | 200.3 | -85.3 | 171.7 | -73.1 | 170.6 | -60.1 | 172.6 | -47.2 |
| -40 | 278.5 | -73.9 | 233.6 | -76.4 | 201.3 | -69.5 | 190.3 | -59.0 | 187.4 | -47.7 |
| -50 | 263.6 | -65.3 | 240.1 | -66.6 | 219.5 | -62.7 | 207.4 | -55.3 | 201.9 | -46.3 |
| -60 | 256.3 | -55.9 | 242.9 | -56.7 | 230.3 | -54.4 | 220.9 | -49.5 | 215.3 | -43.1 |
| -70 | 251.9 | -46.3 | 244.5 | -46.7 | 237.3 | -45.4 | 231.4 | -42.6 | 227.1 | -38.6 |
| -80 | 248.8 | -36.6 | 245.6 | -36.8 | 242.4 | -36.2 | 239.6 | -34.9 | 237.4 | -33.1 |
| -90 | 246.4 | -26.8 | 246.4 | -26.8 | 246.4 | -26.8 | 246.4 | -26.8 | 246.4 | -26.8 |

| R. A. Dec. | ^{5h} | | ^{6h} | | ^{7h} | | ^{8h} | | ^{9h} | |
|---------------|---------------|-------|---------------|-------|---------------|-------|---------------|-------|---------------|-------|
| | Long. | Lat. | Long. | Lat. | Long. | Lat. | Long. | Lat. | Long. | Lat. |
| +90 | 66.4 | +26.8 | 66.4 | +26.8 | 66.4 | +26.8 | 66.4 | +26.8 | 66.4 | +26.8 |
| +80 | 76.1 | +22.1 | 77.2 | +24.5 | 77.6 | +27.0 | 77.3 | +29.6 | 76.2 | +32.0 |
| +70 | 85.1 | +16.8 | 87.5 | +21.4 | 88.8 | +26.4 | 88.7 | +31.5 | 87.1 | +36.4 |
| +60 | 93.7 | +11.2 | 97.4 | +17.7 | 99.8 | +24.9 | 100.5 | +32.3 | 99.1 | +39.7 |
| +50 | 101.8 | +5.3 | 106.9 | +13.6 | 110.4 | +22.6 | 112.3 | +32.1 | 112.0 | +41.7 |
| +40 | 109.9 | -0.6 | 116.0 | +9.1 | 120.6 | +19.7 | 123.9 | +30.7 | 125.5 | +42.1 |
| +30 | 117.9 | -6.6 | 124.9 | +4.4 | 130.5 | +16.1 | 135.1 | +28.4 | 138.8 | +41.0 |
| +20 | 126.2 | -12.4 | 133.7 | -0.4 | 140.0 | +12.2 | 145.7 | +25.2 | 151.4 | +38.5 |
| +10 | 134.8 | -18.0 | 142.4 | -5.2 | 149.2 | +7.9 | 155.7 | +21.3 | 162.9 | +34.6 |
| 0 | 144.0 | -23.1 | 151.3 | -9.9 | 158.2 | +3.5 | 165.2 | +16.8 | 173.3 | +29.8 |
| -10 | 153.8 | -27.7 | 160.5 | -14.3 | 167.1 | -1.1 | 174.2 | +11.9 | 182.6 | +24.3 |
| -20 | 164.4 | -31.5 | 170.1 | -18.4 | 176.0 | -5.6 | 182.9 | +6.8 | 191.2 | +18.3 |
| -30 | 175.8 | -34.4 | 180.0 | -22.0 | 185.1 | -9.9 | 191.4 | +1.4 | 199.1 | +11.9 |
| -40 | 187.9 | -36.2 | 190.4 | -24.9 | 194.4 | -14.1 | 199.8 | -3.9 | 206.7 | +5.2 |
| -50 | 200.3 | -36.7 | 201.3 | -27.1 | 204.1 | -17.8 | 208.4 | -9.2 | 214.2 | -1.5 |
| -60 | 212.7 | -35.9 | 212.5 | -28.5 | 214.1 | -21.1 | 217.2 | -14.2 | 221.6 | -8.1 |
| -70 | 224.7 | -33.9 | 223.9 | -28.9 | 224.5 | -23.8 | 226.4 | -19.0 | 229.3 | -14.7 |
| -80 | 235.9 | -30.8 | 235.3 | -28.3 | 235.3 | -25.7 | 236.1 | -23.2 | 237.5 | -20.9 |
| -90 | 246.4 | -26.8 | 246.4 | -26.8 | 246.4 | -26.8 | 246.4 | -26.8 | 246.4 | -26.9 |

N. B.—The reductions for plus and minus 90° are independent of the right ascension and declination and respectively: $66^\circ.4$, $+26^\circ.8$ and $246^\circ.4$, $-26^\circ.9$. The Galactic pole has been variously taken: Newcomb 12^h44^m , $+26^\circ.6$; Gould, 12^h42^m , $+32^\circ$; Scarle, 12^h40^m , $+28^\circ$, for tables of conversion see Harvard Annals, 56, 1912; Kapteyn, 12^h41^m , $+27^\circ.3$; Van Rhijn, 12^h56^m , $+25^\circ$, for tables, see Gröningen Publications, 43, 1929.

RIGHT ASCENSION, DECLINATION INTO GALACTIC COORDINATES

| | 10 ^h | | 11 ^h | | 12 ^h | | 13 ^h | | 14 ^h | |
|-----|-----------------|-------|-----------------|-------|-----------------|-------|-----------------|-------|-----------------|-------|
| | Long. | Lat. | Long. | Lat. | Long. | Lat. | Long. | Lat. | Long. | Lat. |
| +80 | 74.3 | +34.1 | 71.8 | +35.7 | 68.8 | +36.6 | 65.6 | +36.8 | 62.4 | +36.2 |
| +70 | 83.7 | +40.8 | 78.6 | +44.3 | 71.9 | +46.3 | 64.5 | +46.7 | 57.3 | +45.4 |
| +60 | 95.0 | +46.6 | 87.5 | +52.3 | 76.3 | +55.9 | 62.9 | +56.7 | 50.3 | +54.4 |
| +50 | 108.6 | +51.1 | 100.1 | +59.4 | 83.6 | +65.3 | 60.1 | +66.6 | 39.5 | +62.7 |
| +40 | 124.5 | +53.6 | 118.4 | +64.7 | 98.5 | +73.9 | 53.6 | +76.4 | 21.3 | +69.5 |
| +30 | 141.4 | +53.9 | 142.3 | +66.9 | 135.7 | +79.7 | 20.3 | +85.3 | 351.7 | +73.1 |
| +20 | 157.7 | +51.8 | 166.7 | +65.1 | 187.8 | +77.8 | 274.9 | +82.3 | 319.0 | +71.4 |
| +10 | 171.9 | +47.8 | 185.8 | +60.2 | 212.4 | +70.2 | 259.5 | +72.8 | 296.7 | +65.5 |
| 0 | 183.7 | +42.3 | 199.0 | +53.3 | 222.9 | +61.1 | 255.0 | +62.9 | 283.6 | +57.6 |
| -10 | 193.5 | +35.7 | 208.4 | +45.3 | 228.6 | +51.6 | 252.8 | +53.0 | 275.4 | +48.9 |
| -20 | 201.7 | +28.5 | 215.3 | +36.8 | 232.3 | +42.0 | 251.4 | +43.0 | 269.7 | +39.7 |
| -30 | 208.9 | +20.9 | 220.9 | +27.9 | 235.0 | +32.2 | 250.4 | +33.1 | 265.4 | +30.4 |
| -40 | 215.3 | +13.0 | 225.5 | +18.9 | 237.2 | +22.4 | 249.7 | +23.1 | 261.8 | +20.9 |
| -50 | 221.3 | +5.0 | 229.7 | +9.8 | 239.2 | +12.6 | 249.0 | +13.1 | 258.7 | +11.4 |
| -60 | 227.2 | -3.1 | 233.7 | +0.6 | 240.9 | +2.7 | 248.4 | +3.1 | 255.7 | +1.8 |
| -70 | 233.2 | -11.2 | 237.7 | -8.6 | 242.6 | -7.1 | 247.7 | -6.8 | 252.8 | -7.7 |
| -80 | 239.5 | -19.1 | 241.8 | -17.7 | 244.4 | -17.0 | 247.1 | -16.8 | 249.8 | -17.3 |
| | 15 ^h | | 16 ^h | | 17 ^h | | 18 ^h | | 19 ^h | |
| +80 | 59.6 | +34.9 | 57.4 | +33.1 | 54.8 | +31.2 | 55.3 | +28.3 | 55.3 | +25.7 |
| +70 | 51.4 | +42.6 | 47.1 | +38.6 | 44.7 | +33.9 | 43.9 | +28.9 | 44.5 | +23.8 |
| +60 | 40.9 | +49.5 | 35.3 | +43.1 | 32.7 | +35.9 | 32.5 | +28.5 | 34.1 | +21.1 |
| +50 | 27.4 | +55.3 | 21.9 | +46.3 | 20.3 | +36.7 | 21.3 | +27.1 | 24.1 | +17.8 |
| +40 | 10.3 | +59.0 | 7.4 | +47.7 | 7.9 | +36.2 | 10.4 | +24.9 | 14.4 | +14.1 |
| +30 | 350.6 | +60.1 | 352.6 | +47.2 | 355.8 | +34.4 | 0.0 | +22.0 | 5.1 | +9.9 |
| +20 | 331.3 | +58.2 | 338.6 | +44.9 | 344.4 | +31.5 | 350.1 | +18.4 | 356.0 | +5.6 |
| +10 | 315.2 | +53.9 | 326.0 | +41.0 | 333.8 | +27.7 | 340.5 | +14.3 | 347.1 | +1.1 |
| 0 | 302.6 | +47.8 | 314.9 | +35.9 | 324.0 | +23.1 | 331.3 | +9.9 | 338.2 | -3.5 |
| -10 | 292.8 | +40.6 | 305.4 | +30.0 | 314.8 | +18.0 | 322.4 | +5.2 | 329.2 | -7.9 |
| -20 | 285.0 | +32.8 | 296.9 | +23.4 | 306.2 | +12.4 | 313.7 | +0.4 | 320.0 | -12.2 |
| -30 | 278.5 | +24.6 | 289.3 | +16.4 | 297.9 | +6.6 | 304.9 | -4.4 | 310.5 | -16.1 |
| -40 | 272.8 | +16.1 | 282.2 | +9.2 | 289.9 | +0.6 | 296.0 | -9.1 | 300.6 | -19.7 |
| -50 | 267.6 | +7.5 | 275.4 | +1.8 | 281.8 | -5.3 | 286.9 | -13.6 | 290.4 | -22.6 |
| -60 | 262.6 | -1.2 | 268.7 | -5.6 | 273.7 | -11.2 | 277.4 | -17.7 | 279.8 | -24.9 |
| -70 | 257.6 | -9.8 | 261.7 | -12.9 | 265.1 | -16.8 | 267.5 | -21.4 | 268.8 | -26.4 |
| -80 | 252.3 | -18.4 | 254.4 | -20.0 | 256.1 | -22.1 | 257.2 | -24.5 | 257.6 | -27.0 |
| | 20 ^h | | 21 ^h | | 22 ^h | | 23 ^h | | 24 ^h | |
| +80 | 56.1 | +23.2 | 57.5 | +20.9 | 59.5 | +19.1 | 61.8 | +17.7 | 64.4 | +17.0 |
| +70 | 46.4 | +19.0 | 49.3 | +14.7 | 53.2 | +11.2 | 57.7 | +8.6 | 62.6 | +7.1 |
| +60 | 37.2 | +14.2 | 41.6 | +8.1 | 47.2 | +3.1 | 53.7 | -0.6 | 60.9 | -2.7 |
| +50 | 28.4 | +9.2 | 34.2 | +1.5 | 41.3 | -5.0 | 49.7 | -9.8 | 59.2 | -12.6 |
| +40 | 19.8 | +3.9 | 26.7 | -5.2 | 35.3 | -13.0 | 45.5 | -18.9 | 57.2 | -22.4 |
| +30 | 11.4 | -1.4 | 19.1 | -11.9 | 28.9 | -20.9 | 40.9 | -27.9 | 55.0 | -32.2 |
| +20 | 2.9 | -6.8 | 11.2 | -18.3 | 21.7 | -28.5 | 35.3 | -36.8 | 52.3 | -42.0 |
| +10 | 354.2 | -11.9 | 2.6 | -24.3 | 13.5 | -35.7 | 28.4 | -45.3 | 48.6 | -51.6 |
| 0 | 345.2 | -16.8 | 353.3 | -29.8 | 3.7 | -42.3 | 19.0 | -53.3 | 42.9 | -61.1 |
| -10 | 335.7 | -21.3 | 342.9 | -34.6 | 351.9 | -47.8 | 5.8 | -60.2 | 32.4 | -70.2 |
| -20 | 325.7 | -25.2 | 331.4 | -38.5 | 337.7 | -51.8 | 346.7 | -65.1 | 7.8 | -77.8 |
| -30 | 315.1 | -28.4 | 318.8 | -41.0 | 321.4 | -53.9 | 322.3 | -66.9 | 315.7 | -79.7 |
| -40 | 303.9 | -30.7 | 305.5 | -42.1 | 304.5 | -53.6 | 298.4 | -64.7 | 278.5 | -73.9 |
| -50 | 292.3 | -32.1 | 292.0 | -41.7 | 288.6 | -51.1 | 280.1 | -59.4 | 263.6 | -65.3 |
| -60 | 280.5 | -32.3 | 279.1 | -39.7 | 275.0 | -46.6 | 267.5 | -52.3 | 256.3 | -55.9 |
| -70 | 268.7 | -31.5 | 267.1 | -36.4 | 263.7 | -40.8 | 258.6 | -44.3 | 251.9 | -46.3 |
| -80 | 257.3 | -29.6 | 256.2 | -32.0 | 254.3 | -34.1 | 251.8 | -35.7 | 248.8 | -36.6 |

TABLE 760.—Planetary Data

| Body | Reciprocals of masses | Mean distance from the sun, km | Sidereal period, Mean days | Inclination of orbit | Mean density, H ₂ O = 1 | Gravity at surface |
|--------------|-----------------------|--------------------------------|----------------------------|----------------------|------------------------------------|--------------------|
| Sun..... | 1 | | | | 1.42 | 28.0 |
| Mercury..... | 6000000 | 58 × 10 ⁶ | 87.97 | 7°.003 | 5.61 | .4 |
| Venus..... | 408000 | 108 " | 244.70 | 3.393 | 5.16 | .9 |
| Earth*..... | 329390 | 149 " | 365.26 | | 5.52 | 1.00 |
| Mars..... | 3093500 | 228 " | 686.98 | 1.850 | 3.95 | .4 |
| Jupiter..... | 1047.35 | 778 " | 4332.59 | 1.308 | 1.34 | 2.7 |
| Saturn..... | 3501.6 | 1426 " | 10759.20 | 2.492 | .69 | 1.2 |
| Uranus..... | 22869 | 2869 " | 30685.93 | .773 | 1.36 | 1.0 |
| Neptune..... | 19700 | 4495 " | 60187.64 | 1.778 | 1.30 | 1.0 |
| Pluto..... | | 5900 " | 908.85 | 17.1 | | |
| Moon..... | †81.45 | 38 × 10 ⁴ | 27.32 | 5.145 | 3.36 | .17 |

* Earth and moon. † Relative to earth. Inclination of axes: Sun 7°.25; Earth 23°.45; Mars 24°.6; Jupiter 3°.1; Saturn 26°.8; Neptune 27°.2. Others doubtful. Approximate rates of rotation: Sun 25½^d; Moon 27¼^d; Mercury 88^d; Venus 225^d; Mars 24^h 37^m; Jupiter 9^h 55^m; Saturn 10^h 14^m. Asteroids (planetoids): Sept. 28, 1931, 1183 had been numbered, inclination Pallas orbit 34° 43', Hidalgo 43°; c. Albert, 0.54; Hidalgo 0.65. Heaviest meteorite (So. Africa) 50 tons.

TABLE 761.—Satellites of the Solar System

| | Mean distance | Sidereal period | Diameter |
|--------------------------|---------------|--|----------|
| Earth's: Moon..... | 384,400 km | 27 ^d 7 ^h 43 ^m 11.5 ^s | 3476 km |
| Martian: Phobos..... | 9,380 | 0 7 39 13.85 | 15 ? |
| Deimos..... | 23,460 | 1 6 17 54.9 | 8 ? |
| Jovian: 5th..... | 181,200 | 0 11 57 22.70 | 160 ? |
| 1, Io..... | 421,300 | 1 18 27 33.51 | 3730 |
| 2, Europa..... | 670,500 | 3 13 13 42.05 | 3150 |
| 3, Ganymede..... | 1,069,300 | 7 3 42 33.35 | 5150 |
| 4, Callisto..... | 1,881,000 | 16 16 32 11.21 | 5180 |
| 6th..... | 11,450,000 | 250.68 d | 130 ? |
| 7th..... | 11,730,000 | 260.06 d | 40 ? |
| 8th..... | 23,500,000 | 738.9 d | 25 ? |
| 9th..... | 24,100,000 | 745.0 d | 25 ? |
| Saturnian: 7, Mimas..... | 185,700 | 0 22 37 5.25 | 650 ? |
| 6, Enceladus..... | 237,900 | 1 8 53 6.82 | 800 ? |
| 5, Tethys..... | 294,500 | 1 21 18 26.14 | 1300 ? |
| 4, Dione..... | 377,200 | 2 17 41 9.53 | 1200 ? |
| 2, Rhea..... | 526,700 | 4 12 25 12.23 | 1750 ? |
| 1, Titan..... | 1,220,000 | 15 22 41 26.82 | 4200 |
| 8, Hyperion..... | 1,480,000 | 21 6 38 24.0 | 500 ? |
| 3, Iapetus..... | 3,558,000 | 79 7 56 24.4 | 1800 ? |
| 9, Phoebe..... | 12,930,000 | 550.44 d | 250 ? |
| Uranian: 1, Ariel..... | 191,700 | 2 12 29 20.8 | 900 ? |
| 2, Umbriel..... | 267,000 | 4 3 27 36.7 | 700 ? |
| 3, Titania..... | 438,000 | 5 16 56 26.7 | 1700 ? |
| 4, Oberon..... | 586,000 | 13 11 7 3.5 | 1500 ? |
| Neptune's: 1..... | 354,000 | 5 21 2 38.1* | 5000 ? |

* Motion retrograde. Notes: Jovian: 1st 4 called Galilean; eccentricity 6, 7, 8, 9: 0.15, 0.21, 0.38, 0.25; masses 1, 2, 3, 4: 1.00, 0.65, 2.10, 0.58 of moon. 6, 7 orbits about 29° and 28° to Jupiter's; 8, 32° or more properly, 148°. 9, inclination of orbit 156° to planets. Saturnian: Hyperion, mass, 1.86 × moon; Phoebe, eccentricity 0.17; inclination 53° or 174°7'. Uranus: orbits inclined 82°.2 to ecliptic, in that plane revolve backward = 97°.8 to ecliptic and direct motion. Neptune: inclination, 40°. All other satellites are small eccentricity, mass and inclinations. The mass of Saturn's ring < 1/1000000 Saturn's mass.

TABLE 762.—Diameters of the Planets

From critical review by Rabe, *Astron. Nach.*, 234, 154, 1928. Solar parallax taken as 8".800, earth's radius 6738 km. Order of p.e. ± 0.04 for planets.

| Object | At distance | Diameter | | | Object | At distance | Diameter | | |
|-------------------|-------------|------------|--------|-----------|------------------|-------------|------------|--------|-----------|
| | | ap- parent | km | earth = 1 | | | ap- parent | km | earth = 1 |
| Mercury..... | 1.000 | 7".09 | 5140 | 0.403 | Saturn: Equat... | 9.539 | 17.44 | 120600 | 9.45 |
| Venus..... | " | 17.40 | 12620 | .989 | Polar..... | " | 15.77 | 109000 | 8.55 |
| Earth..... | " | 17.60 | 12756 | 1.000 | Outer ring..... | " | 40.29 | 278500 | 21.84 |
| Mars: Equat... | " | 9.47 | 6860 | .538 | Crepe ring..... | " | 20.83 | 144000 | 11.29 |
| Polar..... | " | 9.42 | 6820 | .535 | Uranus..... | 19.19 | 3.84 | 53400 | 4.19 |
| Jupiter: Equat... | 5.203 | 38.09 | 143600 | 11.26 | Neptune..... | 30.06 | 2.28 | 49700 | 3.89 |
| Polar..... | " | 35.76 | 134800 | 10.57 | | | | | |

TABLE 763.—Planetary and Satellite Distances as Connected by Bode's Law; Later Developments

It is notable that the planetary and satellite distances from their primaries approximately follow Bode's law or some modification thereof. Bode's law: Write a series of fours; to the 2nd add 3; to the 3rd, 3×2 or 6; to the 4th, 6×2 , or 12; etc., doubling the added number each time. Jeans states: "It is more than likely that Bode's law is a mere coincidence" (1929). Penniston (Science, 71, 513, 1930) suggests adding to the square of the integer the integer itself, thus assuming that the terms differ from the square of the integers by a progressively changing amount. See also Caswell, Science, 60, 384, 1929; Armellini, Scientia, 12, 1, 1918; 1, 1922.*

| System | Satellite | Relative distance | New law | Bode's law | Caswell's law | System | Satellite | Relative distance | New law | Bode's law | Caswell's law |
|---------|-----------|-------------------|---------|------------|---------------|--------|-----------|-------------------|---------|------------|---------------|
| Sun | Mercury | 3.87 | 3 | 4 | 3.82 | Saturn | Mimas | 10.0 | 10 | 10 | 10.6 |
| " | Venus | 7.23 | 6 | 7 | 6.80 | " | Enceladus | 12.8 | ... | ... | ... |
| " | Earth | 10.0 | 10 | 10 | 10.6 | " | Tethys | 15.8 | 15 | 16 | 15.3 |
| " | Mars | 15.2 | 15 | 16 | 15.3 | " | Dione | 20.3 | 21 | ... | 20.8 |
| " | Ceres | 27.7 | 28 | 28 | 27.2 | " | Rhea | 28.0 | 28 | 28 | 27.2 |
| " | Jupiter | 52.0 | 55 | 52 | 51.4 | " | Titan | 66.0 | 66 | 52 | 61.2 |
| " | Saturn | 95.3 | 91 | 100 | 95.6 | " | Themis | 78.1 | 78 | ... | 83.1 |
| " | Uranus | 191.0 | 190 | 196 | 187.0 | " | Hyperion | 79.0 | 78 | 100 | 83.1 |
| " | Neptune | 300.0 | 300 | ... | 310.0 | " | Iapetus | 190.0 | 190 | 196 | 187.0 |
| " | "Pluto" | ... | 406 | 388 | 408.0 | " | Phoebe | 698.0 | 703 | 772 | 712.0 |
| " | " | ... | 435 | 388 | 435.0 | Uranus | Ariel | 10.0 | 10 | 10 | 10.6 |
| Mars | Phobos | 1.00 | 1 | ... | 1.70? | " | Umbriel | 14.1 | 15 | 16 | 15.3 |
| " | Deimos | 3.22 | 3 | 4 | 3.82 | " | Titania | 22.8 | 21 | ... | 20.8 |
| Jupiter | V | 2.71 | 3 | 4 | 3.82 | " | Oberon | 30.4 | 28 | 28 | 27.2 |
| " | I | 6.27 | 6 | 7 | 6.80 | | | | | | |
| " | II | 10.0 | 10 | 10 | 10.6 | | | | | | |
| " | III | 15.8 | 15 | 16 | 15.3 | | | | | | |
| " | IV | 27.9 | 28 | 28 | 27.2 | | | | | | |
| " | V | 109.4 | 171 | ... | 170.0 | | | | | | |
| " | VII | 173.0 | 171 | 196 | 170.0 | | | | | | |
| " | VIII | 348.5 | 351 | ... | 357.0 | | | | | | |
| " | IX | 371.0 | 378 | 388 | 382.0 | | | | | | |

* See also Narlicker, Philos. Mag. 12, 67, 1931, with note by Larmor. Sir G. Darwin was inclined to regard Bode's Law a subject for serious discussion. See Turner, Blagg, M. N. R. A. S. 73, 414, 1913. See Pruett, Pop. Astron. 39, 360, 1931.

TABLE 764.—Albedos

The albedo, according to Bond, is defined as follows: "Let a sphere S be exposed to parallel light. Then its albedo is the ratio of the whole amount reflected from S to the whole amount of light incident on it." In the following table, m = the stellar magnitude at mean opposition; g = magnitude it would have at full phase and unit distance from earth and sun; σ = assumed mean semi-diameter at unit distance; p = ratio of observed brightness at full phase to that of a flat disk of same size and same position, illuminated and viewed normally and reflecting all the incident light according to Lambert's law; q depends on law of variation of light with phase; albedo = pq . Russell, Astrophys. Journ., 43, 173, 1916.

Albedo of the earth: A reduction of Very's observations by Russell gives 0.45 in close agreement with the recent value of Aldrich of 0.43 (see Aldrich, Smithsonian Misc. Coll., vol. 69, no. 10, 1919).

| Object | m | g | σ | p | q | Visual albedo | Color index | Photographic albedo |
|---------|--------|-------|----------|-------|-------|---------------|-------------|---------------------|
| Moon | -12.55 | +0.49 | 2.40'' | 0.105 | 0.604 | 0.073 | +1.18 | 0.051 |
| Mercury | -2.94 | - .88 | 3.45 | .164 | .42 | .069 | ... | ... |
| " | -2.12 | - .06 | 3.45 | .077 | .72 | .055 | ... | ... |
| Venus | -4.77 | -4.06 | 8.55 | .492 | 1.20 | .50 | + .78 | .60 |
| Mars | -1.85 | -1.36 | 4.67 | .139 | 1.11 | .154 | +1.38 | .009 |
| Jupiter | -2.20 | -8.09 | 95.23 | .375 | 1.5: | .50: | + .50 | .73: |
| Saturn | + .80 | -8.67 | 77.95 | .420 | 1.5: | .63: | +1.12 | .47: |
| Uranus | +5.74 | -6.08 | 36.0 | .42 | 1.5: | .63: | ... | ... |
| Neptune | +7.65 | -7.06 | 34.5 | .49 | 1.5: | .73: | ... | ... |

TABLE 765.—Equation of Time

The equation of time when + is to be added to the apparent solar time to give mean time. When the place is not on a standard meridian (75th, etc.) its difference in longitude in time from that meridian must be subtracted when east, added when west to get standard time (75th meridian time, etc.). The equation varies from year to year cyclically, and the figure following the \pm sign gives a rough idea of this variation.

| | Min. | Sec. | | Min. | Sec. | | Min. | Sec. | | Min. | Sec. |
|--------|------|-------------|--------|------|------------|---------|------|------------|--------|------|-------------|
| Jan. 1 | + 3 | 26 \pm 14 | Apr. 1 | +4 | 2 \pm 7 | July 1 | +3 | 31 \pm 5 | Oct. 1 | -10 | 12 \pm 8 |
| 15 | + 9 | 25 \pm 9 | 15 | +0 | 8 \pm 5 | 15 | +5 | 42 \pm 3 | 15 | -14 | 5 \pm 6 |
| Feb. 1 | +13 | 42 \pm 4 | May 1 | -2 | 54 \pm 3 | Aug. 1 | +6 | 9 \pm 3 | Nov. 1 | -16 | 10 \pm 2 |
| 15 | +14 | 20 \pm 2 | 15 | -3 | 49 \pm 1 | 15 | +4 | 24 \pm 5 | 15 | -15 | 22 \pm 4 |
| Mar. 1 | +12 | 34 \pm 4 | June 1 | -2 | 28 \pm 3 | Sept. 1 | +0 | 2 \pm 7 | Dec. 1 | -10 | 58 \pm 8 |
| 15 | + 9 | 9 \pm 6 | 15 | +0 | 8 \pm 4 | 15 | -4 | 41 \pm 9 | 15 | - 4 | 53 \pm 10 |

TABLES 766-769 SOLAR RADIATION

TABLE 766.—The Solar Constant

Solar constant (amount of energy falling at normal incidence on one square centimeter per minute on body at earth's mean distance) = 1.932 calories = mean 696 determinations 1902-12. Apparently subject to variations, usually within the range of 7 per cent, and occurring irregularly in periods of a week or ten days.

Computed effective temperature of the sun: from form of black-body curves, 6000° to 7000° Absolute; from λ_{max} = 2930 and $\text{max.} = 0.470\mu$, 6230°; from total radiation, $J = 76.8 \times 10^{-12} \times T^4$, 5830°.

TABLE 767.—Solar spectrum energy (arbitrary units) and its transmission by the earth's atmosphere.

Values computed from $e_m = e_0 a^m$, where e_m is the intensity of solar energy after transmission through a mass of air m ; m is unity when the sun is in the zenith, and approximately = sec. zenith distance for other positions (see table 778); e_0 = the energy which would have been observed had there been no absorbing atmosphere; a is the fractional amount observed when the sun is in the zenith.

| Wave length μ | Transmission coef- ficients, a | | | | Intensity Solar Energy Arbitrary | | | | | | | | | |
|----------------------|-----------------------------------|--|--|--|---|--|--|--|--|--|--|--|--|--|
|----------------------|-----------------------------------|--|--|--|---|--|--|--|--|--|--|--|--|--|

Transmission coefficients are for period when there was apparently no volcanic dust in the air.

* Possibly too high because of increased humidity towards noon.

† Altitude 4420 m.

TABLE 768.—The amount of Solar Radiation in different sections of the spectrum, ultra-violet, visual infra-red. Calories

| Wave length. | | | Mount Whitney. | | | | | Mount Wilson. | | | | Washington. | | | |
|--------------|-------|----------|----------------|------|------|------|------|---------------|------|------|------|-------------|------|-----|-----|
| μ | μ | | m=0 | m=1 | 2 | 3 | 4 | m=1 | 2 | 3 | 4 | m=1 | 2 | 3 | 4 |
| 0.00 | to | 0.45 | .31 | .25 | .19 | .16 | .13 | .23 | .16 | .12 | .09 | .13 | .06 | .04 | .02 |
| 0.45 | to | 0.70 | .71 | .67 | .62 | .58 | .54 | .65 | .57 | .51 | .45 | .53 | .40 | .30 | .24 |
| 0.70 | to | .80 | .91 | .87 | .85 | .82 | .80 | .69 | .68 | .66 | .63 | .69 | .62 | .57 | .53 |
| 0.00 | to | ∞ | 1.93 | 1.78 | 1.66 | 1.56 | 1.47 | 1.57 | 1.42 | 1.28 | 1.17 | 1.35 | 1.08 | .90 | .79 |

TABLE 769.—Distribution of intensity (Radiation) over the Solar Disk
(These observations extend over only a small portion of a sun-spot cycle.)

| Wave length. | μ 0.323 | μ 0.386 | μ 0.433 | μ 0.456 | μ 0.481 | μ 0.501 | μ 0.534 | μ 0.604 | μ 0.670 | μ 0.699 | μ 0.866 | μ 1.031 | μ 1.225 | μ 1.655 | μ 2.097 |
|------------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Fraction Radius. | | | | | | | | | | | | | | | |
| { 0.00 | 144 | 338 | 456 | 515 | 511 | 489 | 463 | 399 | 333 | 307 | 174 | 111 | 77.6 | 39.5 | 14.0 |
| { 0.40 | 128 | 312 | 423 | 486 | 483 | 463 | 440 | 382 | 320 | 295 | 169 | 108 | 75.7 | 38.9 | 13.8 |
| { 0.53 | 120 | 289 | 395 | 455 | 456 | 437 | 417 | 365 | 308 | 284 | 163 | 105.5 | 73.8 | 38.2 | 13.6 |
| { 0.65 | 112 | 267 | 368 | 428 | 430 | 414 | 396 | 348 | 295 | 273 | 159 | 103 | 72.2 | 37.6 | 13.4 |
| { 0.75 | 99 | 240 | 333 | 390 | 394 | 380 | 366 | 326 | 281 | 258 | 152 | 99 | 69.8 | 36.7 | 13.1 |
| { 0.825 | 86 | 214 | 296 | 351 | 358 | 347 | 337 | 304 | 262 | 243 | 145 | 94.5 | 67.1 | 35.7 | 12.8 |
| { 0.875 | 76 | 188 | 266 | 317 | 324 | 323 | 312 | 284 | 247 | 229 | 138 | 90.5 | 64.7 | 34.7 | 12.5 |
| { 0.92 | 64 | 163 | 233 | 277 | 290 | 286 | 281 | 259 | 227 | 212 | 130 | 86 | 61.6 | 33.6 | 12.2 |
| { 0.95 | 49 | 141 | 205 | 242 | 255 | 254 | 254 | 237 | 210 | 195 | 122 | 81 | 58.7 | 32.3 | 11.7 |

Taken from vols. II and III and unpublished data of the Astrophysical Observatory of the Smithsonian Institution. Schwartzchild and Villiger: Astrophysical Journal, 23, 1906.

TABLE 770.—The Solar Constant,* Decade Means (See Tables 771 and 772)

| Decade | 1918 | 1919 | 1920 | 1921 | 1922 | 1923 | 1924 | 1925 | 1926 | 1927 | 1928 | 1929 |
|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Jan. 1 | | 1.943 | 1.968 | 1.956 | 1.924 | 1.946 | 1.937 | 1.945 | 1.944 | 1.939 | 1.941 | 1.925 |
| 2 | | 1.948 | 1.967 | 1.953 | 1.946 | | 1.943 | 1.939 | 1.943 | 1.938 | 1.931 | 1.941 |
| 3 | | 1.938 | 1.959 | | 1.952 | | 1.944 | 1.947 | 1.933 | 1.931 | 1.942 | 1.939 |
| Feb. 1 | | 1.962 | 1.958 | | 1.911 | 1.934 | 1.938 | | 1.938 | 1.936 | 1.947 | 1.937 |
| 2 | | 1.951 | 1.954 | 1.952 | 1.947 | 1.951 | 1.943 | 1.951 | 1.939 | 1.946 | 1.941 | 1.925 |
| 3 | | 1.930 | 1.956 | 1.958 | 1.948 | 1.923 | 1.938 | 1.938 | 1.929 | | 1.934 | 1.925 |
| Mar. 1 | | 1.950 | 1.959 | 1.954 | 1.949 | 1.929 | 1.947 | 1.941 | 1.941 | | 1.950 | 1.932 |
| 2 | | 1.942 | 1.948 | 1.940 | 1.939 | 1.936 | 1.944 | 1.936 | 1.948 | 1.944 | 1.945 | 1.931 |
| 3 | | 1.931 | 1.932 | | 1.932 | 1.931 | 1.942 | 1.941 | 1.932 | 1.941 | 1.945 | 1.932 |
| Apr. 1 | | 1.943 | 1.948 | 1.951 | 1.930 | 1.934 | 1.942 | 1.945 | 1.927 | 1.941 | 1.946 | 1.932 |
| 2 | | 1.957 | 1.956 | 1.941 | 1.937 | 1.928 | 1.948 | 1.950 | 1.937 | 1.945 | 1.940 | 1.942 |
| 3 | | 1.961 | 1.952 | 1.934 | 1.925 | 1.934 | 1.947 | 1.946 | 1.939 | 1.945 | 1.940 | 1.938 |
| May 1 | | 1.953 | 1.950 | 1.946 | 1.924 | 1.934 | 1.944 | 1.946 | 1.937 | 1.947 | 1.943 | 1.936 |
| 2 | | 1.921 | 1.961 | 1.939 | 1.925 | 1.935 | 1.948 | 1.950 | 1.938 | 1.944 | 1.951 | 1.941 |
| 3 | | 1.945 | 1.950 | 1.941 | | 1.937 | 1.950 | 1.954 | 1.942 | 1.944 | 1.949 | 1.937 |
| June 1 | | 1.957 | 1.943 | 1.933 | 1.910 | 1.918 | 1.957 | 1.943 | 1.939 | 1.950 | 1.947 | 1.938 |
| 2 | | 1.938 | 1.934 | 1.936 | 1.913 | 1.934 | 1.956 | 1.943 | 1.946 | 1.943 | 1.948 | 1.932 |
| 3 | | 1.962 | 1.938 | 1.945 | 1.920 | 1.933 | 1.953 | 1.948 | 1.945 | 1.945 | 1.951 | 1.932 |
| July 1 | | 1.951 | 1.945 | 1.960 | 1.904 | 1.934 | 1.946 | 1.952 | 1.942 | 1.949 | 1.943 | 1.935 |
| 2 | | 1.961 | 1.940 | 1.957 | 1.913 | 1.928 | 1.951 | 1.954 | 1.949 | 1.942 | 1.942 | 1.931 |
| 3 | 1.921 | 1.950 | 1.951 | 1.953 | 1.918 | 1.944 | 1.942 | 1.947 | 1.944 | 1.946 | 1.940 | 1.935 |
| Aug. 1 | 1.955 | 1.961 | 1.930 | 1.944 | 1.919 | 1.942 | 1.950 | 1.949 | 1.945 | 1.942 | 1.943 | 1.931 |
| 2 | 1.945 | 1.942 | 1.927 | | 1.916 | 1.940 | 1.940 | 1.941 | 1.942 | 1.941 | 1.937 | 1.932 |
| 3 | 1.959 | 1.955 | 1.932 | | 1.921 | 1.941 | 1.933 | 1.942 | 1.942 | 1.941 | 1.932 | 1.930 |
| Sept. 1 | 1.942 | 1.938 | 1.951 | | | 1.948 | 1.941 | 1.956 | 1.942 | 1.940 | | 1.926 |
| 2 | 1.946 | 1.942 | 1.944 | | 1.931 | 1.947 | 1.950 | 1.946 | 1.940 | 1.942 | 1.938 | 1.928 |
| 3 | 1.944 | 1.937 | 1.944 | 1.969 | 1.916 | 1.945 | 1.946 | 1.950 | 1.943 | 1.950 | 1.921 | 1.929 |
| Oct. 1 | 1.951 | 1.947 | 1.942 | 1.959 | 1.926 | 1.942 | 1.953 | 1.942 | 1.938 | 1.945 | 1.930 | 1.928 |
| 2 | 1.930 | 1.949 | 1.950 | 1.969 | 1.929 | 1.944 | 1.949 | 1.949 | 1.937 | 1.944 | 1.935 | 1.934 |
| 3 | 1.933 | 1.960 | 1.943 | 1.966 | | 1.940 | 1.948 | 1.946 | 1.929 | 1.943 | 1.927 | 1.926 |
| Nov. 1 | 1.928 | 1.958 | 1.951 | 1.953 | 1.929 | 1.935 | 1.948 | 1.944 | 1.931 | 1.945 | 1.924 | 1.932 |
| 2 | 1.945 | 1.951 | 1.946 | 1.949 | 1.935 | 1.945 | 1.951 | 1.948 | 1.926 | 1.943 | 1.932 | 1.936 |
| 3 | 1.947 | 1.948 | 1.945 | 1.952 | 1.919 | 1.945 | 1.945 | 1.944 | 1.930 | 1.944 | 1.930 | 1.939 |
| Dec. 1 | 1.962 | 1.944 | 1.957 | 1.956 | 1.912 | 1.942 | 1.942 | 1.944 | 1.935 | 1.949 | 1.930 | 1.941 |
| 2 | 1.969 | 1.949 | 1.957 | 1.937 | 1.916 | 1.942 | 1.947 | 1.945 | 1.931 | 1.935 | 1.924 | 1.939 |
| 3 | 1.960 | 1.958 | 1.956 | | 1.912 | 1.921 | 1.939 | 1.946 | 1.935 | 1.939 | 1.927 | 1.940 |

TABLE 771.—The Solar Constant, Monthly and Yearly Means

| Month | 1918 | 1919 | 1920 | 1921 | 1922 | 1923 | 1924 | 1925 | 1926 | 1927 | 1928 | 1929 |
|-------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Jan. | | 1.943 | 1.964 | 1.955 | 1.948 | 1.946 | 1.942 | 1.943 | 1.941 | 1.938 | 1.940 | 1.938 |
| Feb. | | 1.949 | 1.956 | 1.956 | 1.943 | 1.930 | 1.939 | 1.943 | 1.938 | 1.943 | 1.943 | 1.929 |
| Mar. | | 1.941 | 1.945 | 1.949 | 1.938 | 1.932 | 1.945 | 1.939 | 1.939 | 1.942 | 1.946 | 1.931 |
| Apr. | | 1.953 | 1.952 | 1.944 | 1.931 | 1.932 | 1.946 | 1.947 | 1.934 | 1.944 | 1.942 | 1.937 |
| May | | 1.940 | 1.953 | 1.943 | 1.925 | 1.936 | 1.948 | 1.950 | 1.939 | 1.945 | 1.947 | 1.938 |
| June | | 1.955 | 1.939 | 1.939 | 1.914 | 1.928 | 1.956 | 1.945 | 1.944 | 1.946 | 1.948 | 1.934 |
| July | | 1.954 | 1.945 | 1.956 | 1.912 | 1.936 | 1.946 | 1.951 | 1.944 | 1.945 | 1.942 | 1.933 |
| Aug. | 1.954 | 1.953 | 1.930 | 1.944 | 1.919 | 1.941 | 1.940 | 1.945 | 1.944 | 1.941 | 1.937 | 1.931 |
| Sept. | 1.944 | 1.939 | 1.947 | 1.969 | 1.923 | 1.947 | 1.946 | 1.950 | 1.942 | 1.944 | 1.927 | 1.928 |
| Oct. | 1.939 | 1.953 | 1.944 | 1.962 | 1.927 | 1.942 | 1.949 | 1.946 | 1.934 | 1.944 | 1.930 | 1.929 |
| Nov. | 1.941 | 1.953 | 1.948 | 1.951 | 1.929 | 1.942 | 1.948 | 1.946 | 1.929 | 1.944 | 1.929 | 1.936 |
| Dec. | 1.962 | 1.950 | 1.957 | 1.953 | 1.915 | 1.933 | 1.942 | 1.945 | 1.932 | 1.942 | 1.926 | 1.940 |
| Yearly mean | | 1.949 | 1.948 | 1.952 | 1.927 | 1.937 | 1.946 | 1.946 | 1.938 | 1.943 | 1.938 | 1.934 |

* In calories/cm²/min. at earth's mean distance from sun (Smithsonian Astrophysical Observatory).

ATMOSPHERIC TRANSPARENCY AND SOLAR DATA

TABLE 775.—Transmission of Radiation Through Moist and Dry Air

This table gives the wave-length, λ ; a the transmission of radiation by dry air above Mount Wilson (altitude = 1730 m. barometer, 620 mm.) for a body in the zenith; finally a correction factor, a_w , due to such a quantity of aqueous vapor in the air that if condensed it would form a layer 1 cm. thick. Except in the bands of selective absorption due to the air, a agrees very closely with what would be expected from purely molecular scattering. a_w is very much smaller than would be correspondingly expected, due possibly to the formation of ions by the ultra-violet light from the sun. The transmission varies from day to day. However, values for clear days computed as follows agree within a per cent or two of those observed when the altitude of the place is such that the effect due to dust may be neglected, e. g. for altitudes greater than 1000 meters. If $B =$

the barometric pressure in mm., w , the amount of precipitable water in cm., then $a_B = a_w^{B/620}$. w is best determined spectroscopically (Astrophysical Journal, 35, p. 149, 1912, 37, p. 359, 1913) otherwise by formula derived from Hann, $w = 2.3e_w 10^{-22} h$, e_w being the vapor pressure in cm. at the station, h , the altitude in meters. See Table 449 for long-wave transmission.

| λ (μ) | .360 | .384 | .413 | .452 | .503 | .535 | .574 | .624 | .653 | .720 | .986 | 1.74 |
|---------------------|--------|------|------|------|------|------|------|------|------|------|------|------|
| a | (.660) | .713 | .783 | .840 | .885 | .898 | .905 | .929 | .938 | .970 | .986 | .990 |
| a_w | .950 | .960 | .965 | .967 | .977 | .980 | .974 | .978 | .985 | .988 | .990 | .990 |

Fowle, Astrophysical Journal, 38, 1913.

TABLE 776.—Brightness of (radiation from) Sky at Mt. Wilson (1730 m.) and Flint Island (sea-level)

| Zenith dist. of zone | | | | | | | | | | | | | |
|---|--------------|-------|-------|--------|--------|--------|--------|--------|--------|-------|-------|--|--|
| $10^6 \times$ mean ratio sky/sun | Mt. Wilson | . . . | 0-15° | 15-35° | 35-50° | 50-60° | 60-70° | 70-80° | 80-90° | - | Sun | | |
| | Flint Island | . . . | 1500* | 400 | 520 | 610 | 660 | 700 | 720 | - | - | | |
| | Mt. Wilson | . . . | 115 | 122 | 128 | 150 | 185 | 210 | 460 | - | - | | |
| Ditto \times area of zone | Mt. Wilson | . . . | 51.0 | 58.8 | 61.5 | 87.2 | 104.3 | 117.6 | 125.3 | - | 636 | | |
| | Flint Island | . . . | 3.9 | 17.9 | 22.5 | 21.4 | 29.2 | 35.3 | 80.0 | - | 210 | | |
| Altitude of sun | | | - | - | 5° | 15° | 25° | 35° | 47½° | 65° | 82½° | | |
| Sun's brightness, cal. per cm. ² per min. | | | - | - | .533 | .900 | 1.233 | 1.358 | 1.413 | 1.496 | 1.521 | | |
| Ditto on horizontal surface | | | - | - | .046 | .243 | .524 | .750 | 1.041 | 1.355 | 1.507 | | |
| Mean brightness on normal surface sky $\times 10^6$ /sun | | | - | - | .423 | .493 | .385 | .365 | .346 | .320 | .310 | | |
| Total sky radiation on horizontal cal. per cm. ² | | | - | - | .056 | .110 | .162 | .189 | .205 | .225 | .240 | | |
| per m. | | | - | - | .102 | .343 | .686 | .969 | 1.249 | 1.581 | 1.747 | | |
| Total sun + sky, ditto | | | - | - | .102 | .343 | .686 | .969 | 1.249 | 1.581 | 1.747 | | |

* Includes allowance for bright region near sun. For the dates upon which the observation of the upper portion of table were taken, the mean ratios of total radiation sky/sun, for equal angular areas, at normal incidence, at the island and on the mountain, respectively, were 636×10^{-8} and 210×10^{-8} , on a horizontal surface, 305×10^{-8} and 77×10^{-8} ; for the whole sky, at normal incidence, 0.37 and 0.20; on a horizontal surface 0.27 and 0.07. Annals of the Astrophysical Observatory of the Smithsonian Institution, vols. II and III, and unpublished researches (Abbot).

TABLE 777.—Relative Distribution in Normal Spectrum of Sunlight and Sky-light at Mount Wilson
Zenith distance about 50°.

| | μ | μ | μ | μ | μ | μ | C | D | b | F |
|----------------------------|-------|-------|-------|-------|-------|-------|-----|-----|-----|-----|
| Place in Spectrum | 0.422 | 0.457 | 0.491 | 0.566 | 0.614 | 0.660 | | | | |
| Intensity Sunlight | 186 | 232 | 227 | 211 | 191 | 166 | | | | |
| Intensity Sky-light | 1194 | 986 | 701 | 395 | 231 | 174 | | | | |
| Ratio at Mt. Wilson | 642 | 425 | 309 | 187 | 121 | 105 | 102 | 143 | 246 | 316 |
| Ratio computed by Rayleigh | - | - | - | - | - | - | 102 | 164 | 258 | 328 |
| Ratio observed by Rayleigh | - | - | - | - | - | - | 102 | 168 | 291 | 369 |

TABLE 778.—Air Masses

See Table 767 for definition. Besides values derived from the pure secant formula, the table contains those derived from various other more complex formula, taking into account the curvature of the earth, refraction, etc. The most recent is that of Bemporad.

| Zenith Dist. | 0° | 20° | 40° | 60° | 70° | 75° | 80° | 85° | 88° |
|--------------|------|-------|-------|-------|-------|-------|------|-------|------|
| Secant | 1.00 | 1.064 | 1.305 | 2.000 | 2.924 | 3.864 | 5.76 | 11.47 | 28.7 |
| Forbes | 1.00 | 1.065 | 1.306 | 1.995 | 2.902 | 3.809 | 5.57 | 10.22 | 18.9 |
| Bouguer | 1.00 | 1.064 | 1.305 | 1.990 | 2.900 | 3.805 | 5.56 | 10.20 | 19.0 |
| Laplace | 1.00 | - | - | 1.993 | 2.899 | - | 5.56 | 10.20 | 18.8 |
| Bemporad | 1.00 | - | - | 1.995 | 2.904 | - | 5.60 | 10.39 | 19.8 |

The Laplace and Bemporad values, Lindholm, Nova Acta R. Soc. Upsal. 3, 1913; the others, Radau's Actinometric, 1877.

TABLE 779
SOLAR DATA

58 Elements Known in the Sun's Atmosphere

Taken, with additions and corrections, from St. John's Revision of Rowland. Papers of Mount Wilson Observatory, vol. 3 (Carnegie Inst. Publ. 396, 1928).

| At. no., element | Atomic state | | | | | | | | Molecular state | |
|---------------------|--|--------------|--------|--------------|--------------|--------------|--------------|-------|------------------------|------------------|
| | Reversing layer. Chromosphere or spots.† | | | | | | | | Band lines | |
| | No. lines | Max. int. | Ele. + | No. lines | Max. int. | No. lines | Max. int. | Locus | Source | Locus |
| 1 H | 6 | 40 | | | | 30 | 100 | Chr | OH; NH; CH MgH; CaH | D, S Spots |
| 2 *He | 1 | 0 | † | | | 30 | 40 | Chr | | |
| 3 Li | | | | | | 1 | 4 | Spots | | |
| 4 Be | 2 | -3 | Be+ | 3 | 1 | | | | | |
| 5 B | | | | | | | | | | |
| 6 C | 9 | 0 | | | | | | | BO | Spots |
| 7 N | 1 | -2 | | | | | | | CN; CH; (C-) | D, S |
| 8 O | 5 | 2 | | | | | | | NH; CN | D, S |
| 11 Na | 22 | 30 | | | | | | | OH; TiO § | Spots |
| 12 Mg | 25 | 30 | Mg+ | 2 | 0 | | | | MgH | Spots |
| 13 Al | 8 | 20 | Al+? | 1 | -2 | | | | | |
| 14 Si | 22 | 12 | Si+ | 5 | 2 | | | | | |
| 16 S? | 3 | -1 | | | | | | | | |
| 19 K | 5 | 0 | | | | | | | | |
| 20 Ca | 115 | 15 | Ca+ | 12 | 200 | | | | CaH | Spots |
| 21 Sc | 74 | 2 | Sc+ | 71 | 5 | 5 | 2 | Spots | | |
| 22 Ti | 769 | 7 | Ti+ | 300 | 12 | 16 | 3 | Spots | TiO § | Spots |
| 23 V | 470 | 4 | V+ | 140 | 5 | 8 | 1 | Spots | | |
| 24 Cr | 859 | 5 | Cr+ | 168 | 5 | 1 | -1 | Spots | | |
| 25 Mn | 440 | 7 | Mn+ | 18 | 6 | | | | | |
| 26 Fe | 3157 | 40 | Fe+ | 131 | 6 | | | | | |
| 27 Co | 773 | 6 | Co+ | 10 | 0 | 2 | 0 | Spots | | |
| 28 Ni | 611 | 20 | Ni+ | 17 | 2 | | | | | |
| 29 Cu | 26 | 10 | | | | | | | | |
| 30 Zn | 10 | 3 | | | | | | | | |
| 31 Ga | 2 | -1 | | | | | | | | |
| 32 Ge | 5 | 0 | | | | | | | | |
| 37 Rb | | | | | | 2 | 1 | Spots | | |
| 38 Sr | 22 | -1 | Sr+ | 7 | 8 | 4 | -1 | Spots | | |
| 39 Y | 47 | 0 | Y+ | 69 | 3 | 4 | 5 | Spots | | |
| 40 Zr | 126 | -1 | Zr+ | 238 | 2 | 7 | 0 | Spots | | |
| 41 Cb? | 12 | -2 | Cb+ | 6 | -1 | | | | | |
| 42 Mo | 38 | -2 | Mo+ | 8 | 0 | | | | | |
| 44 Ru | 24 | 0 | | | | | | | | |
| 45 Rh | 20 | -2 | | | | | | | | |
| 46 Pd | 21 | 0 | | | | | | | | |
| 47 Ag | 2 | 0 | | | | | | | | |
| 48 Cd | 1 | -1 | | | | | | | | |
| 49 In | | | | | | 1 | -1 | Spots | | |
| 50 Sn? | 2 | -2 | | | | | | | | |
| 51 Sb | 3 | -3N | | | | | | | | |
| 55 Cs | 2 | 1 | | | | | | | | |
| 56 Ba | | | Ba+ | 9 | 8 | | | | | |
| 57 La | | | La+ | 100 | 1 | | | | | |
| 58 Ce | | | Ce+ | 249 | 0 | | | | | |
| 59 Pr | | | Pr+? | 18 | -1 | | | | | |
| 60 Nd | | | Nd+ | 107 | 0 | | | | | |
| 62 Sa | | | Sa+ | 67 | -1 | | | | | |
| 63 Eu | | | Eu+? | 5 | 1 | | | | | |
| 64 Gd | | | Gd+? | 15 | 0 | | | | | |
| 66 Dy | | | Dy+ | 12 | 0 | | | | | |
| 68 Er | | | Er+? | 2 | -1 | | | | | |
| 70 Yb | | | Yb+? | 2 | -1? | | | | | |
| 72 Hf | | | Hf+ | 12 | -1 | | | | | |
| 74 W | 6 | -2 | | | | | | | | |
| 78 Pt | 3 | 1 | | | | | | | | |
| 81 TI? | 2 | -2 | | | | | | | | |
| 82 Pb | 6 | -2 | | | | | | | | |

* λ 5875.618 He often present (absorption) over disturbed regions of disk. † λ 4685.81 He+1N, present in chromosphere. ‡ Only in chromosphere or spots. § Possibly TiO₂ in red. || Present in disk and spots.

Quantitative Estimates of Composition of Solar Atmosphere

(Taken from Russell, *Astrophys. Journ.*, 70, 11, 1929.)

In the *chromosphere* a deep layer of gases is held up by radiation pressure. The (gas) pressure, p , and density, d , increase slowly downwards as gravity gradually balances the radiation pressure. At the base p may be about 10^{-7} atmosphere. At lower levels is the *reversing layer* in which gravity is dominant, p increases rapidly, and temperature remains nearly constant at 5000° K., as long as the gases are transparent. When $p < 0.01$ atm. general absorption by electron collisions make gas hazy. Opacity gains greatly with p , passes rapidly to the *photosphere*. When opacity important, temperature rises (radiative equilibrium, Schwarzschild, Eddington). Observed photospheric temperature = mean value of the radiating layers (Russell, Stewart, *Astrophys. Journ.*, 59, 197, 1924).

The presence and absence of lines of different elements depends on the excitation potential. Almost all the elements for which this is less than 5 volts appear. There are very few other lines except the strong ones of H. The level of ionization in solar atmosphere is such that those of 8.3 volts are 50% ionized.

Na, Mg, Si, K, Ca, and Fe are 95% of the whole mass. Number of metallic atoms above cm^2 of surface = 8×10^{20} . 80% are ionized. Mean atomic weight = 32, total mass 42 mg/ cm^2 . Even atomic weights 10 times as abundant as odd. Heavy metals (Ba onwards) little less abundant than those beyond Sr. Hypothesis that heavy metals sink below photosphere thus not confirmed. Metals Na-Zn far most common. Most elements not appearing in the table would hardly be expected to show spectral lines under solar conditions.

Nonmetal abundance difficult to estimate. O is as abundant by weight as all metals together. Atmosphere = 60 H by vol., 2 He, 2 O, 1 of metallic vapors, 0.8, free electrons. Temperature of reversing layer = 5600° K.; pressure at its base 0.005 atm.

In the following table, S_0 = whole no. neutral atom/ cm^2 ; S_i , no. ionized; T , total no. both stages of ionization; Q , total mass/ cm^2 = $T \times \text{at. wt.}$; ::, indicate less accuracy; ?, origin doubtful.

| El. | log S_0 | log S_i | log T | log Q | El. | log S_0 | log S_i | log T | log Q | El. | log S_0 | log S_i | log T | log Q |
|-----|-----------|-----------|---------|---------|-----|-----------|-----------|---------|---------|----------------|-----------|-----------|---------|---------|
| H | 11.5:: | 5.7:: | 11.5:: | 11.5:: | Cu | 4.3 | 4.9 | 5.0 | 6.8 | Ce | | 2.4 | 2.4 | 4.6 |
| Li | -0.9 | 2.0: | 2.0: | 2.8: | Zn | 4.9 | 3.8 | 4.9 | 6.7 | Pr | | 0.6: | 0.6: | 2.8: |
| Be | 1.8 | 0.8 | 1.8 | 2.8 | Ga | 0.2: | 2.0: | 2.0: | 3.8: | Nd | | 2.0 | 2.0 | 4.2 |
| C | 7.4 | 4.4: | 7.4: | 8.5: | Ge | 2.5 | 2.8 | 3.0 | 4.9 | Sa | | 1.5 | 1.5 | 3.7 |
| N | 7.6? | 1.8? | 7.6? | 8.7? | As | 0.6 | -0.7? | 0.6? | 2.5 | Eu | | 1.4: | 1.4: | 3.6: |
| O | 9.0 | 3.3: | 9.0: | 10.2: | Rb | -2.5: | 1.7: | 1.7: | 3.6: | Gd | | 1.1: | 1.1: | 3.3: |
| Na | 4.0 | 7.2 | 7.2 | 8.6 | Sr | 0.6 | 3.3 | 3.3 | 5.2 | Dy | | 1.6: | 1.6: | 3.8: |
| Mg | 7.0 | 7.7 | 7.8 | 9.2 | Vt | 0.8 | 2.6 | 2.6 | 4.5 | Er | | 0.1: | 0.1: | 2.3: |
| Al | 4.6 | 6.4 | 6.4 | 7.8 | Zr | 0.9 | 2.5 | 2.5 | 4.5 | Hf | | 0.4 | 0.4 | 2.6 |
| Si | 7.0 | 7.0 | 7.3 | 8.8 | Cb | -0.2: | 1.0: | 1.0: | 3.0: | W | -0.1 | -0.1 | 0.2 | 2.5 |
| S | 5.7: | 3.4: | 5.7: | 7.2: | Mo | 0.5 | 1.4 | 1.4 | 1.4 | Ir | -0.5? | -0.5? | -0.2? | 2.1? |
| K | 2.8: | 6.8: | 6.8: | 8.4: | Ru | 1.0 | 1.6 | 1.7 | 3.7 | Pt | 1.5 | 1.0 | 1.6 | 3.9 |
| Ca | 4.6 | 6.7 | 6.7 | 8.3 | Rh | -0.3 | 0.5 | 0.5 | 2.5 | Tl | -0.8? | 1.4? | 1.4? | 3.7? |
| Sc | 1.9 | 3.6 | 3.6 | 5.3 | Pd | 0.6 | 0.9 | 1.1 | 3.1 | Pb | 0.2 | 1.2 | 1.2 | 3.5 |
| Ti | 3.6 | 5.2 | 5.2 | 6.9 | Ag | 0.0 | 1.0 | 1.0 | 3.0 | CN | 3.2 | | 3.2 | 4.6 |
| V | 1.9 | 5.0 | 5.0 | 6.7 | Cd | 2.1: | 1.6: | 2.2: | 4.2: | C ₂ | 1.3 | | 1.3 | 2.7 |
| Cr | 4.4 | 5.7 | 5.7 | 7.4 | In | -2.0: | 0.0: | 0.0: | 2.1: | CH | 3.0 | | 3.0 | 4.1 |
| Mn | 5.1 | 5.8 | 5.9 | 7.6 | Sn | 0.3? | 1.2? | 1.2? | 3.3? | NH | 2.1 | | 2.1 | 3.3 |
| Fe | 6.7 | 7.1 | 7.2 | 9.0 | Sb | 0.4: | 0.7: | 0.8: | 2.9: | OH | 3.0 | | 3.0 | 4.2 |
| Co | 5.1 | 5.4 | 5.6 | 7.4 | Ba | -0.2 | 3.3 | 3.3 | 5.4 | BO | 1.4 | | 1.4 | 2.8 |
| Ni | 5.7 | 5.7 | 6.0 | 7.8 | La | 0.7 | 1.8 | 1.8 | 3.9 | | | | | |

Comparison of above values with values of Payne by a very different process show good agreement except for H (Payne 12.9, Russell, 11.5, the latter uncertain) and K, (Payne 5.3, Russell 6.8; the former probably too low).

SOLAR DATA

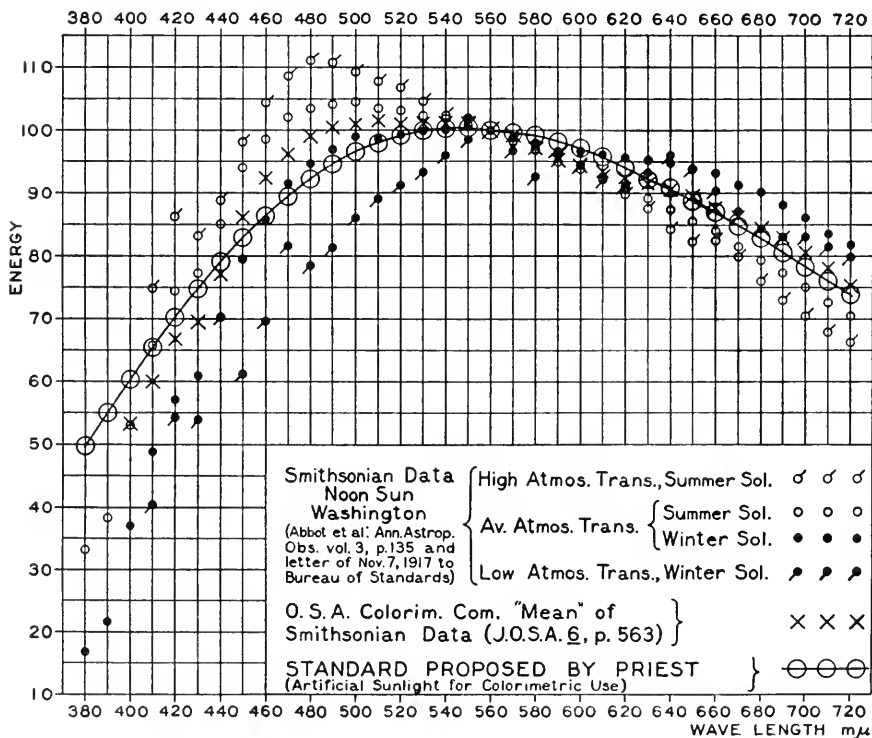
TABLE 781.—Abundance of Elements in Sun, Earth, and Meteorites

(Taken from Russell, *Astrophys. Journ.*, 70, 66, 1929.)

| El. | Sun | Earth | E-S | Meteorites | M-S | El. | Sun | Earth | E-S | Meteorites | M-S |
|-----|-------------------|-------|------|------------|------|-----|-------------------|-------|-------|------------|------|
| Na | 8.6 | 8.7 | +0.1 | 7.8 | -0.8 | Ni | 7.8 | 6.8 | -1.0 | 8.2 | +0.4 |
| Mg | 9.2 | 8.6 | -0.6 | 9.1 | -0.1 | Cu | 6.8 | 6.3 | -0.5 | 6.2 | -0.6 |
| Al | 7.8 | 9.2 | +1.4 | 8.2 | +0.4 | Zn | 6.7 | 5.9 | -0.8 | ... | ... |
| Si | 8.8 | 9.7 | +0.9 | 9.3 | +0.5 | H | 11.5 | 8.3 | -3.2 | 6.9 | -4.6 |
| K | 8.4: ¹ | 8.7 | +0.3 | 7.2 | -1.2 | C | 8.5 | 7.4 | -1.1 | 7.2 | -1.3 |
| Ca | 8.3 | 8.8 | +0.5 | 8.1 | -0.2 | N | 8.7? ² | 6.8 | -1.9? | ... | ... |
| Sc | 5.3 | 3.: | -2.: | ... | ... | O | 10.2 | 9.7 | -0.5 | 9.6 | -0.6 |
| Ti | 6.9 | 8.1 | +1.2 | 7.0 | +0.1 | F | ... | 6.8 | ... | ... | ... |
| V | 6.7 | 6.9 | +0.2 | ... | ... | P | ... | 7.4 | ... | 7.0 | ... |
| Cr | 7.4 | 7.1 | -0.3 | 7.5 | +0.1 | S | 7.2 | 7.3 | +0.1 | 8.3 | +1.1 |
| Mn | 7.6 | 7.3 | -0.3 | 7.3 | -0.3 | Cl | ... | 7.7 | ... | 6.9 | ... |
| Fe | 9.0 | 9.0 | 0.0 | 9.4 | +0.4 | | | | | | |
| Co | 7.4 | 5.8 | -1.6 | 7.1 | -0.3 | | | | | | |

¹ : indicates less accuracy.² ? indicates doubtful origin.

TABLE 782.—Abbot-Priest Solar Energy Curve (Sea-Level)



STELLAR DATA

TABLE 783.—Constellation Abbreviations (Astron. Union, 1922)

| | | | |
|---------------------|------------------|------------------|--------------------|
| Andromeda.....And | Circinus.....Cir | Lacerta.....Lac | Pisces Austr...PsA |
| Antlia.....Ant | Columba.....Col | Leo.....Leo | Puppis.....Pup |
| Apus.....Aps | Coma Beren. Com | Leo Minor...LMi | Pyxis.....Pyx |
| Aquarius.....Aqr | Corona Aust. CrA | Lepus.....Lep | Reticulum...Ret |
| Aquila.....Aql | Corona Bor. CrB | Libra.....Lib | Sagitta.....Sge |
| Ara.....Ara | Corvus.....Crv | Lupus.....Lup | Sagittarius...Sgr |
| Aries.....Ari | Crater.....Crt | Lynx.....Lyn | Scorpius.....Sco |
| Auriga.....Aur | Crux.....Cru | Lyra.....Lyr | Sculptor.....Scl |
| Boötes.....Boo | Cygnus.....Cyg | Mensa.....Men | Scutum.....Sct |
| Caelum.....Cae | Delphinus...Del | Microscopium.Mic | Serpens.....Ser |
| Camelopardalis. Cam | Dorado.....Dor | Monoceros...Mon | Sextans.....Sex |
| Cancer.....Cnc | Draco.....Dra | Musca.....Mus | Taurus.....Tau |
| Canes Venatici. CVn | Equuleus...Equ | Norma.....Nor | Telescopium. Tel |
| Canis Major...CMa | Eridanus...Eri | Octans.....Oct | Triangulum...Tri |
| " Minor...CMi | Fornax.....For | Ophiuchus...Oph | " Austr...TrA |
| Capricornus...Cap | Gemini.....Gem | Orion.....Ori | Tucana.....Tuc |
| Carina.....Car | Grus.....Gru | Pavo.....Pav | Ursa Major...UMa |
| Cassiopeia....Cas | Hercules...Her | Pegasus.....Peg | " Minor...UMi |
| Centaurus.....Cen | Horologium. Hor | Perseus.....Per | Vela.....Vel |
| Cepheus.....Cep | Hydra.....Hya | Phoenix.....Phe | Virgo.....Vir |
| Cetus.....Cet | Hydrus.....Hyi | Pictor.....Pic | Volans.....Vol |
| Chamaeleon...Cha | Indus.....Ind | Pisces.....Psc | Vulpecula...Vul |

TABLE 784.—Occurrence and Abundance of Elements in the Stars

(Shapley, 1931. Payne, Stellar atmosphere, 1925. I, II, III, IV denote the occurrence of the neutral, once, twice, and thrice ionized atom. For the sun see Tables 780 and 781.)

| At. no., element | State in star | Abundance | At. no., element | State in star | Abundance | At. no., element | State in star | At. no., element | State in star |
|------------------|---------------|-----------|------------------|---------------|-----------|------------------|---------------|------------------|---------------|
| 1 H | I | 12.9 | 18 A | ... | ... | 35 Br | ... | 52 Te | ... |
| 2 He | I II | 10.2 | 19 K | I II | 5.3 | 36 Kr | ... | 53 I | ... |
| 3 Li | I | 1.9 | 20 Ca | I II | 6.7 | 37 Rb | ... | 54 Xe | ... |
| 4 Be | " | ... | 21 Sc | I II | ... | 38 Sr | I II | 55 Cs | ... |
| 5 B | " | ... | 22 Ti | I II | 6.0 | 39 Y | I II | 56 Ba | II† |
| 6 C | I II III | 6.4 | 23 V | I II | 4.9 | 40 Zr | I II* | 57 La | II |
| 7 N | II III | ... | 24 Cr | I II | 5.8 | 41 Cb | ... | 58 Ce | II |
| 8 O | I II III | 8.0 | 25 Mn | I II | 6.5 | 42 Mo | ... | 59 Pr | ... |
| 9 F | ... | ... | 26 Fe | I II | 6.7 | 43 Ma | ... | 60 Nd | II |
| 10 Ne | ... | ... | 27 Co | I II | ... | 44 Ru | ... | 61 II | ... |
| 11 Na | I | 7.1 | 28 Ni | I II | ... | 45 Rh | ... | 62 Sa | ... |
| 12 Mg | I II | 7.5 | 29 Cu | I | ... | 46 Pd | ... | 63 Eu | II |
| 13 Al | I II III | 6.9 | 30 Zn | I | ... | 47 Ag | ... | 64 Gd | ... |
| 14 Si | I II III IV | 7.5 | 31 Ga | ... | ... | 48 Cd | I | 65 Tb | ... |
| 15 P | II ? III | ... | 32 Ge | ... | ... | 49 In | ... | 66 Dy | ... |
| 16 S | II III | ... | 33 As | ... | ... | 50 Sn | ... | 67 Ho | ... |
| 17 Cl | ... | ... | 34 Se | ... | ... | 51 Sb | ... | 68 Er | II ? |

Elements of higher atomic number than 68 have not been noted.

* Abundance 3.5. † Abundance, 3.0.

STELLAR SYSTEMS

(See Shapley, Harvard Reprint 68, 1931, Harvard Explorations, Science, 74, 207, 1931.)

The solar neighborhood distance of *50 light-years*, explored chiefly through the motions of nearby stars. A large majority are of less than solar luminosity, most below naked eye visibility. Only 40% of the stars known to be nearer than 16 light-years are brighter than the 6th magnitude. Exploring the solar neighborhood therefore involves a search for telescopic dwarf stars. Any body 1/100 of sun's mass within 1,000 astronomical units (.015 light year) would be detected by its disturbance on Neptune and Uranus even if invisible (Russell). Nearest known star is 4 light-years distant (Proxima centauri, $m = 11$, $M = 15.5$).

Region of brighter stars extending *500 light-years*. The great majority of naked-eye stars lie in this region, though some of unusually high intrinsic luminosity are farther away. It includes probably 500,000 telescopic stars. Studied by proper motions, trigonometric and spectroscopic parallaxes, and photometry.

The local system.—Its diameter is *several thousand light-years*. There is good but not incontrovertible evidence of a localized star cloud in our part of the galaxy. Its population is in the tens or hundreds of millions of stars. Shapley considers it may be comparable in dimensions and composition with Magellanic clouds or a typical spiral nebula. Investigated principally statistically by spectra, magnitudes, and positions, and explored by spectroscopic parallaxes, star counts, and structure of variable stars and galactic clusters.

The Milky Way with a radius much greater than *5000 light-years*. The stars within 5000 light-years of the sun are a trifling part of the galactic system outlined by the globular clusters and Milky Way clouds. The stars are so remote that proper motions and spectroscopic analyses hopelessly fail. Statistical counts are of some help in the nearer parts. But most of our knowledge comes from eclipsing binaries, long-period variables, and Cepheids. The period-luminosity relation for Cepheid variables is the key to practically all distances $>$ a few 1000 light-years.

The Clouds of Magellan, nearly *100,000 light-years* distant, nearest of all external galaxies and the most easily studied. Great advantage; all of its varied manifestations are seen at practically the same distance. These phenomena include gaseous nebulae, star clusters, giant and supergiant stars, some 1500 known Cepheids in the Larger Cloud. In this cloud 750 stars brighter than -5.0 abs. mag. and over 200,000 brighter than the 0.0 have been estimated. The following gives an indication of the classes of stars measured in and in front of the Larger Cloud and adjacent field.

| Class | O | B | A | F | G | K | M |
|------------------|---|----|----|-----|-----|-----|-----|
| Cloud | 8 | 28 | 66 | 153 | 771 | 768 | 385 |
| Field | 0 | 0 | 10 | 35 | 206 | 172 | 77 |
| Difference | 8 | 28 | 56 | 118 | 565 | 596 | 308 |

The Super-Galaxies, *1,000,000 to 100,000,000 light-years* distant. Composed of clusters of extra-galactic nebulae. The relative diameters and brightnesses have been determined for some of the super-galaxies. The most conspicuous is the Coma-Virgo cloud A, a stream of several hundred bright spiral, spheroidal, and irregular galaxies, about 10^7 light-years distant; its greatest length about $\frac{1}{2}$ this. One of the richest and most distinct super-galaxies is in Centaurus.

The Meta-Galaxy.—Great irregularity is found in the distribution of the objects exterior to our galaxy—perhaps partly due to obscuring clouds in our system but much attributable to aggregation of galaxies into super-systems and large indefinite streams. We find no evidence that we have approached the limits of a populated universe—no falling off in the number per cubic million light-years. The red-shift in the spectra of distant galaxies may be taken as an observational, relativistic indication of an expanding finite universe, "but so far as the present census of the meta-galaxy goes, the total number of galaxies and the radius of space may both be infinite" (Shapley).

TABLE 786.—Stellar Spectra and Related Characteristics

The spectra of almost all the stars can be arranged in a continuous sequence, the various types connected in a series of imperceptible gradations. With one unimportant exception, the sequence is linear. According to the now generally adopted Harvard system of classification, certain principal types of spectrum are designated by letters—O, B, A, F, G, K, M, R, S, N, P, and Q—and the intermediate types by suffixed numbers. A spectrum halfway between classes B and A is denoted B₅, while those differing slightly from Class A in the direction of Class B are called B8 or B₉. In Classes M and O the notation Ma, Mb, Mc, etc., is employed. Classes R and N apparently form a side chain branching from the main series near Class K.

The colors of the stars, the degree to which they are concentrated into the region of the sky, including the Milky Way, and the average magnitudes of their peculiar velocities in space, referred to the center of gravity of the naked-eye stars as a whole, all show important correlations with the spectral type. In the case of colors, the correlation is so close as to indicate that both spectrum and color depend almost entirely on the surface temperature of the stars. The correlation in the other two cases, though statistically important, is by no means as close.

Examples of all classes from O to M are found among the bright stars. The brightest star of Class N is of magnitude 5.3; the brightest of Class R, 7.0. About 1% show bright lines.

TABLE 787.—The Harvard Spectrum Classification

| Class | Principal spectral lines (dark unless otherwise stated) | Example | Number brighter than 6.25, mag. | Per cent in galactic region | Color index | Effective surface tempera- ture, K. | Mean peculiar velocity, km/sec. |
|-------|--|----------------------|--|--------------------------------------|----------------|--|--|
| O | Bright H lines, bright spark lines of He, N, O, C..... | γ Velorum | 20 | 100 | -0.3 | .. | .. |
| B | H, He, spark lines of N and O, a few spark lines of metals..... | ε Orionis | 696 | 82 | -0.30 | 20,000° | 6 |
| A | H series very strong, spark lines of metals. | Sirius | 1885 | 66 | 0.00 | 11,000° | 10 |
| F | H lines fainter. Spark and arc lines of metals | Canopus | 720 | 57 | +0.33 | 7,500° | 14 |
| G | Arc lines of metals, spark lines very faint..... | The sun | 609 | 58 | +0.70 | 5,000° | 15 |
| K | Arc lines of metals, spectrum faint in violet..... | Arcturus | 1719 | 56 | +1.12 | 4,200° | 17 |
| M | Bands of TiO ₂ , flame and arc lines of metals | Antares | 457 | 54 | +1.00 | 3,100° | 17 |
| R | Bands of carbon, flame and arc lines of metals..... | B. D. -10° 5057 | 0 | 63 | +1.7 | 3,000° | 15 |
| S | Bands ZrO ₂ , metal flame and arc lines; in Se, bright H and metallic lines of high excitation. Latter are always long period variables.... | η ₁ Gruis | 0 | .. | .. | 3,000°? | .. |
| N | Bands of carbon, bright lines, very little violet light.... | 19 Piscium | 8 | 87 | +2.5 | 2,300° | 13 |
| P | Isolated bright lines, gaseous nebulae.... | .. | .. | .. | .. | .. | .. |
| Q | Novae (see Russell, Dugan and Stewart, Astronomy, p. 780). | .. | .. | .. | .. | .. | .. |

Compiled mainly from the Harvard Annals. Temperatures based on the work of Wilsing and Scheiner (see also pp. 632-3). Radial velocities from Campbell. Data for classes R and N from Curtis and Rufus. The peculiar velocities are in the radial direction (towards or from the sun). The average velocities in space should be twice as great. The "galactic region" here means the zone between galactic latitudes $\pm 30^\circ$, and including half the area of the heavens, 96% of the stars of known spectra belong to classes A, F, G, K, 99.7% including B and M (Innes, 1910). Henry Draper Catalogue, 9 vols., 1918-24, with later volumes give positions, magnitudes and spectra of more than 225,000 stars. See also Catalogue of Bright Stars. Schlesinger, Yale Univ. Obs., 1930.

TABLE 788.—Values of Log (no. stars)/(sq. degree) Brighter Than Photographic Magnitude, *m*, at Stated Galactic Latitudes

| <i>m</i> | | | | | | | | | | Ratio nos. successive magnitudes | | | Ratio nos. at 0° to ± 90° | |
|----------|------|------|------|------|------|------|------|------|------|----------------------------------|-----|------|---------------------------|------|
| | +90° | +40° | +20° | +10° | 0° | -10° | -20° | -40° | -90° | +90° | 0° | -90° | +90° | -00° |
| 5.0 | 8.15 | 8.24 | 8.37 | 8.49 | 8.77 | 8.65 | 8.50 | 8.25 | 8.07 | | | | 4.1 | 5.0 |
| 6.0 | 8.59 | 8.72 | 8.85 | 8.95 | 9.22 | 9.10 | 8.94 | 8.71 | 8.62 | 2.8 | 2.8 | 3.5 | 4.3 | 4.0 |
| 7.0 | 9.02 | 9.18 | 9.31 | 9.41 | 9.64 | 9.51 | 9.35 | 9.16 | 9.08 | 2.7 | 2.6 | 2.9 | 4.1 | 3.6 |
| 8.0 | 9.44 | 9.62 | 9.77 | 9.87 | 0.09 | 9.93 | 9.79 | 9.60 | 9.50 | 2.6 | 2.8 | 2.6 | 4.5 | 3.9 |
| 9.0 | 9.86 | 0.05 | 0.21 | 0.33 | 0.55 | 0.37 | 0.23 | 0.04 | 9.92 | 2.6 | 2.9 | 2.6 | 4.9 | 4.3 |
| 10.0 | 0.25 | 0.47 | 0.65 | 0.77 | 1.02 | 0.82 | 0.67 | 0.47 | 0.32 | 2.5 | 3.0 | 2.5 | 5.9 | 5.0 |
| 11.0 | 0.63 | 0.87 | 1.08 | 1.21 | 1.49 | 1.26 | 1.11 | 0.89 | 0.72 | 2.4 | 3.0 | 2.5 | 7.2 | 5.9 |
| 12.0 | 1.01 | 1.26 | 1.50 | 1.64 | 1.95 | 1.70 | 1.54 | 1.29 | 1.12 | 2.4 | 2.9 | 2.5 | 8.7 | 6.8 |
| 13.0 | 1.38 | 1.63 | 1.90 | 2.05 | 2.39 | 2.14 | 1.95 | 1.68 | 1.48 | 2.3 | 2.8 | 2.3 | 10 | 8.1 |
| 14.0 | 1.70 | 1.97 | 2.28 | 2.45 | 2.82 | 2.57 | 2.34 | 2.03 | 1.78 | 2.1 | 2.7 | 2.0 | 13 | 11 |
| 15.0 | 1.98 | 2.30 | 2.66 | 2.85 | 3.22 | 2.99 | 2.72 | 2.34 | 2.02 | 1.9 | 2.5 | 1.7 | 17 | 16 |
| 16.0 | 2.26 | 2.61 | 3.02 | 3.25 | 3.60 | 3.39 | 3.07 | 2.64 | 2.26 | 1.9 | 2.4 | 1.7 | 22 | 22 |
| 17.0 | 2.53 | 2.90 | 3.36 | 3.64 | 3.96 | 3.76 | 3.40 | 2.92 | 2.48 | 1.9 | 2.3 | 1.7 | 27 | 30 |
| 18.0 | 2.79 | 3.15 | 3.67 | 3.97 | 4.32 | 4.10 | 3.68 | 3.18 | 2.70 | 1.8 | 2.3 | 1.7 | 34 | 42 |
| 19.0 | | | | | | | | | | 1.6 | 2.0 | | | |
| 20.0 | | | | | | | | | | 1.5 | 1.9 | | | |
| 21.0 | | | | | | | | | | 1.4 | 1.9 | | | |

Taken from Publ. Groningen, van Rhijn, 1929, which see for far more detailed values for both latitude and longitude. An excess of stars, especially S. of 0° latitude, between longitudes 240° and 60°, and a deficit elsewhere (Sears, Mt. Wilson Contributions, 301, 346, 347, also Publ. Astron. Soc. Pacific, 40, 303, 1928).

TABLE 789.—Numbers and Equivalent Light of the Stars

The total of starlight is a sensible but very small amount. This table by Chapman, shows that up to the 20th magnitude the total light emitted is equivalent to 687 1st-magnitude stars, equal to about the hundredth part of full moonlight. If all the remaining stars are included, following the formula, the equivalent addition would be only three more 1st-magnitude stars. The summation leaves off at a point where each additional magnitude is adding more stars than the last. But, according to the formula, between the 23d and 24th magnitudes there is a turning point, after which each new magnitude adds less than before. The actual counts have been carried so near this turning point that there is no reasonable doubt of its existence. Given its existence, the number of stars is probably finite, a conclusion open to very little doubt. Van Rhijn estimates the total number of stars at 30,000,000,000. Equivalent to 1440 stars of 1st visual magnitude in zenith, 1674 outside earth's atmosphere. Density of radiation = 0.8×10^{-13} erg/cm². Millikan's cosmic radiation density = 4×10^{-15} erg/cm².

| Magnitude, <i>m</i> | Number | Equivalent 1st mag. stars | Totals to magnitude, <i>m</i> | Magnitude, <i>m</i> | Number | Equivalent 1st mag. stars | Totals to magnitude, <i>m</i> |
|---------------------|------------|---------------------------|-------------------------------|---------------------------------|------------|---------------------------|-------------------------------|
| -1.6.... | Sirius | 11 | .. | 9.0-10.0.... | 174,000 | 69 | 380 |
| -0.9.... | α Carinae | 6 | .. | 10.0-11.0.... | 426,000 | 68 | 448 |
| 0.0.... | α Centauri | 2 | .. | 11.0-12.0.... | 961,000 | 60 | 508 |
| 0.0-1.0.... | 8 | 14 | 33 | 12.0-13.0.... | 2,020,000 | 51 | 559 |
| 1.0-2.0.... | 27 | 17 | 50 | 13.0-14.0.... | 3,960,000 | 40 | 599 |
| 2.0-3.0.... | 73 | 18 | 68 | 14.0-15.0.... | 7,820,000 | 31 | 630 |
| 3.0-4.0.... | 189 | 19 | 87 | 15.0-16.0.... | 14,040,000 | 22 | 652 |
| 4.0-5.0.... | 650 | 26 | 113 | 16.0-17.0.... | 25,400,000 | 16 | 668 |
| 5.0-6.0.... | 2,200 | 35 | 148 | 17.0-18.0.... | 38,400,000 | 10 | 678 |
| 6.0-7.0.... | 6,600 | 42 | 190 | 18.0-19.0.... | 54,600,000 | 6 | 684 |
| 7.0-8.0.... | 22,550 | 56 | 246 | 19.0-20.0.... | 76,000,000 | 3 | 687 |
| 8.0-9.0.... | 65,000 | 65 | 311 | All stars fainter than 20.0.... | .. | 3 | 690 |

Practically all the stars visible to the naked eye lie within 1000 parsecs of the sun, and most of them are more than 100 parsecs distant. In the vicinity of the sun, the majority of the stars lie within two or three hundred parsecs of the galactic plane; but along this plane the star-filled region extends far beyond 1000 parsecs in all directions, and may reach 30,000 parsecs in the great southern star clouds (Shapley).

TABLE 790.—The First-Magnitude Stars

| No. | Star | m Mag. | Spec- trum. | R.A. 1900 | Dec. 1900 | Annual proper motion, μ | P.A. of μ | π Parallax | Abs. mag. | Radial velocity km. |
|-----|-------------------------|-----------|----------------|----------------------------------|--------------|--------------------------------------|---------------------|-------------------|--------------|---------------------------|
| 1 | Achernar..... | 0.6 | B5 | 1 ^h 34.0 ^m | -57° 45' | 0.004" | 108° | +0.051" | -0.9 | .. |
| 2 | Aldebaran†..... | 1.1 | K5 | 4 30.2 | +16 18 | .203 | 160 | + .062 | -0.0 | +55.1 |
| 3 | Capella†..... | 0.2 | G | 5 9.3 | +45 54 | .437 | 168 | + .075 | -0.5 | +30.2 |
| 4 | Rigel*†..... | 0.3 | B8 | 5 9.7 | - 8 10 | .001 | 135 | + .007 | -5.5 | +22.6 |
| 5 | Betelgeuse†..... | 0.6-1.2 | Ma | 5 49.8 | + 7 23 | .020 | 74 | + .010 | -2.7 | +21.3 |
| 6 | Canopus..... | -0.9 | F | 6 21.7 | -52 38 | .018 | 56 | + .007 | -6.7 | +20.8 |
| 7 | Sirius*..... | -1.6 | A | 6 40.7 | -16 35 | 1.316 | 204 | + .376 | +1.2 | - 7.4 |
| 8 | Procyon*..... | 0.5 | F5 | 7 34.1 | + 5 20 | 1.242 | 214 | + .309 | +3.0 | - 3.5 |
| 9 | Pollux§..... | 1.2 | K8 | 7 39.2 | +28 16 | .625 | 204 | + .064 | +0.2 | + 3.9 |
| 10 | Regulus†..... | 1.3 | B8 | 10 3.0 | +12 27 | .247 | 209 | + .033 | -1.1 | - 9.1 |
| 11 | α Crucis*..... | 1.1 | B1 | 12 21.0 | -62 33 | .048 | 240 | + .047 | -0.5 | + 7.0 |
| 12 | β Crucis†..... | 1.5 | B1 | 12 41.9 | -59 9 | .050 | 240 | + .008 | -4.0 | +13.0 |
| 13 | Spica†..... | 1.2 | B2 | 13 19.0 | -10 38 | .055 | 229 | - .012 | .. | + 1.6 |
| 14 | β Centauri†..... | 0.0 | B1 | 13 56.8 | -59 53 | .041 | 216 | + .037 | -1.3 | - 7.0 |
| 15 | Arcturus..... | 0.2 | K | 14 11.1 | +19 42 | 2.282 | 209 | + .075 | -0.5 | - 3.9 |
| 16 | α Centauri*..... | 0.3 | G | 14 32.8 | -00 25 | 3.680 | 281 | + .759 | +4.7 | -21.6 |
| 17 | Antares†..... | 1.2 | Ma | 16 23.3 | -26 13 | .034 | 192 | + .020 | -1.5 | - 3.1 |
| 18 | Vega§..... | 0.1 | A | 18 33.6 | +38 41 | .346 | 36 | + .001 | -0.1 | -13.8 |
| 19 | Altair§..... | 0.9 | A5 | 19 45.9 | + 8 36 | .655 | 54 | + .214 | +2.5 | -33.0 |
| 20 | Deneb§..... | 1.3 | A2 | 20 38.0 | +44 55 | .001 | 180 | + .002 | -7.2 | - 4.0 |
| 21 | Fomalhaut..... | 1.3 | A3 | 22 52.1 | -30 9 | .365 | 117 | + .138 | +2.0 | + 6.7 |

* Visual binary. † Spectroscopic binary. ‡ Pair with common proper motion. § Wide pair probably optical

Mass relative to sun of (7) is 3.1; of (8), 1.5; of (16), 2.0. For description of types, see Table 787 or Annals of Harvard College Observatory, 28, p. 146, or more concisely 56, p. 66, and 61, p. 5. The light ratio between successive stellar magnitudes is $\sqrt[100]{10}$ or the number whose logarithm is 0.4000, viz., 2.512. The absolute magnitude of a star is its magnitude reduced to a distance corresponding to 0.1" parallax = $5 + 5 \log \pi$.

TABLE 791.—Stars Known to be Within Five Parsecs of the Sun

The number of stars (doubles counted as singles) per cubic parsec in the neighborhood of the sun has been estimated as 0.0451 (Kapteyn, Van Rhijn, Astron. Journ., 52, 32, 1920). This gives as expectation of 24 within 5 parsecs and 12 nearer than 4. The numbers actually known are 28 and 19. It seems improbable that we should already know practically all within these limits. (Van Maanen, Mt. Wilson, 1930.) See note bottom page 620.

See Luyten, Ann. Harvard Obs., 85, 1023, for stars within 10 parsecs.

| Star | Right Ascension 1900 | Declination 1900 | App. mag. | Parallax | Abs. mag. | Spectrum class | Proper motion |
|-----------------------------|----------------------------|---------------------|--------------|----------|--------------|-------------------|------------------|
| | h m | ° ' | | " | | | " |
| α Centauri..... | 14 32.8 | -60 25 | 0.33 | .763 | 4.74 | G6 | 3.66 |
| "..... | 14 32.8 | -60 25 | 1.70 | .763 | 6.11 | K4 | 3.66 |
| α | 14 32.8 | -60 25 | (10.5) | .763 | 14.9 | (M) | (3.66) |
| (Barnard's star)..... | 17 52.9 | + 4 28 | 9.07 | .538 | 13.32 | Mb | 10.30 |
| Wolf 359..... | 10 51.6 | + 7 37 | 13.5 | .407 | 16.5 | M4e | 4.84 |
| Lalande 21185..... | 10 57.9 | +36 38 | 7.60 | .380 | 10.5 | Ma | 4.77 |
| α Canis Majoris..... | 6 40.7 | -16 34 | 1.58 | .358 | 1.19 | A0 | 1.32 |
| "..... | 6 40.7 | -16 34 | 8.44 | .358 | 11.21 | (A) | 1.32 |
| Innes' star..... | 11 12.0 | -57 2 | (12) | .345 | 14.69 | .. | 2.69 |
| BD - 12°45'23..... | 16 24.8 | - 2 24 | 9.5 | .327 | 12.1 | M5 | 1.24 |
| α Canis Minoris..... | 7 34.1 | + 5 29 | 0.48 | .318 | 2.99 | F3 | 1.24 |
| "..... | 7 34.1 | + 5 29 | (12.5) | .318 | 15.0 | .. | 1.24 |
| ϵ Ceti..... | 1 39.4 | -16 28 | 3.05 | .318 | 6.16 | G7 | 1.92 |
| ζ 5h 243..... | 5 7.7 | -44 59 | 8.3 | .310 | 10.8 | K2 | 8.70 |
| 61 Cygni..... | 21 2.4 | +38 15 | 5.57 | .305 | 7.90 | K7 | 5.21 |
| "..... | 21 2.4 | +38 15 | 6.28 | .305 | 8.70 | K8 | 5.21 |
| ϵ Eridani..... | 3 28.2 | - 0 48 | 3.81 | .304 | 6.21 | K1 | .97 |
| Σ 2398..... | 18 41.8 | +50 29 | 0.33 | .293 | 11.7 | Mb | 2.28 |
| Σ | 18 41.8 | +50 29 | 10.01 | .293 | 12.4 | (M) | 2.28 |
| Σ | 21 55.7 | -57 12 | 4.74 | .280 | 7.08 | K5 | 4.67 |
| ϵ Indi..... | 0 12.5 | +43 27 | 7.98 | .277 | 10.19 | Ma | 2.85 |
| Groombr. 34..... | 0 12.5 | +43 27 | 11.05 | .277 | 13.26 | (M) | 2.85 |
| Krüger 60..... | 22 24.5 | +57 12 | 0.64 | .258 | 11.73 | Mb | .94 |
| "..... | 22 24.5 | +57 12 | 11.34 | .258 | 13.40 | (M) | .94 |
| Lacaille 9352..... | 22 59.4 | -36 26 | 7.44 | .256 | 9.48 | Ma | 7.02 |
| Van Maanen's star..... | 0 43.9 | + 4 55 | 12.34 | .256 | 14.38 | F0 | 3.01 |
| Lacaille 8760..... | 21 11.4 | -39 15 | 6.05 | .232 | 8.48 | Ma | 3.53 |
| Gou 32416..... | 23 59.5 | -37 51 | 8.5 | .220 | 10.2 | K5 | 6.11 |
| WB 10h 234..... | 10 14.2 | +20 22 | 9.2 | .217 | 10.9 | Mdp | .490 |
| Lalande 25372..... | 13 40.7 | +15 26 | 9.6 | .213 | 11.2 | Mb | 2.298 |
| Oe Arg 17415-6..... | 17 37.0 | +68 26 | 9.2 | .209 | 10.8 | Mb | 1.31 |
| Wolf 562..... | 15 14.2 | - 7 21 | 10.7 | .209 | 12.3 | M5 | 1.33 |
| Groombr. 1618..... | 10 5.3 | +49 58 | 6.82 | .208 | 8.41 | K6 | 1.451 |
| BD +43°4305..... | 22 42.5 | +43 48 | 9.5 | .208 | 11.1 | Me5 | .86 |
| α Eridani..... | 4 10.7 | - 7 49 | 4.48 | .200 | 6.0 | G5 | 4.082 |
| "..... | 4 10.7 | - 7 49 | 9.7 | .200 | 11.2 | A | 4.027 |
| α Aquilae..... | 19 45.9 | + 8 36 | 0.80 | .198 | 2.37 | A5 | .65 |
| Our sun..... | | | -26.72 | | + 4.85 | G0 | |

TABLES 792-795
SPECTROSCOPIC DATA

(Mostly derived by permission from Russell, Dugan, and Stewart, Astronomy, Ginn & Co., 1917.)

TABLE 792.—Percentage of Stars of Various Spectrum Classes
(Henry Draper Catalogue)

| Visual magnitude | B (B ₀ to B ₅) | A (B ₈ to A ₃) | F (A ₅ to F ₂) | G (F ₅ to G ₀) | K (G ₅ to K ₂) | M (K ₅ to M ₈) |
|-----------------------|--|--|--|--|--|--|
| Brighter than 2.24... | 28 | 28 | 7 | 10 | 15 | 12 |
| 2.25 to 3.24..... | 25 | 19 | 10 | 12 | 22 | 12 |
| 3.25 to 4.24..... | 16 | 22 | 7 | 12 | 35 | 8 |
| 4.25 to 5.24..... | 9 | 27 | 12 | 12 | 30 | 10 |
| 5.25 to 6.24..... | 5 | 38 | 13 | 10 | 28 | 6 |
| 6.25 to 7.24..... | 4 | 30 | 12 | 14 | 33 | 7 |
| 7.25 to 8.24..... | 2 | 26 | 11 | 16 | 37 | 8 |
| 8.25 to 9.24..... | 1 | 27 | 10 | 21 | 34 | 7 |
| Below 9.25 | 1 | 33 | 8 | 25 | 29 | 4 |
| All together | 2 | 29 | 9 | 21 | 33 | 6 |

Among 6000 brighter than 6.25 m only 20 are recorded at Harvard as Class O, 8 of N. The brightest stars of Class O are γ Velorum (2.22 m) and ζ Puppis (2.27 m); of Class N, 19 Piscium (5.30 m); only about 70 of Class R and 20 of S known. Brightest R, — 10°5057, (7.04 m); S, 2 Gruis (6.65 m).

TABLE 793.—Galactic Concentration of Various Spectrum Classes
(Henry Draper Catalogue)

| Above 7.0 mag. | B | A | F | G | K | M | All |
|------------------|------|------|------|------|------|------|-------|
| 40° to 90°..... | 0.2 | 6.6 | 3.0 | 3.4 | 10.2 | 1.5 | 24.9 |
| 0° | 10.8 | 21.1 | 5.1 | 5.1 | 15.1 | 3.9 | 61.1 |
| 7.0 to 8.25 mag. | | | | | | | |
| 40° to 90°..... | 0.1 | 6.6 | 9.5 | 16.4 | 32.8 | 6.1 | 71.5 |
| 0° | 18.9 | 75.8 | 13.6 | 20.9 | 53.9 | 13.6 | 196.7 |

Star density per 100 sq. degrees. O stars entirely confined to Milky Way. N stars also strong galactic concentration.

TABLE 794.—Distribution of Binaries as to Spectrum Class

| Brighter 8.75 mag. | No. | O—B8 | B9—A ₃ | A ₅ —F ₂ | F ₅ —G ₂ | G ₅ —K ₂ | K ₅ —M |
|-----------------------|-------|------|-------------------|--------------------------------|--------------------------------|--------------------------------|-------------------|
| All stars | 98675 | 5 | 24 | 11 | 19 | 35 | 8 |
| Visual pairs | 3939 | 4 | 32 | 14 | 28 | 21 | 1 |
| Eclipsing pairs | 132 | 18 | 58 | 12 | 8 | 3 | 1 |
| Visual orbits | 110 | 1 | 16 | 15 | 47 | 17 | 4 |

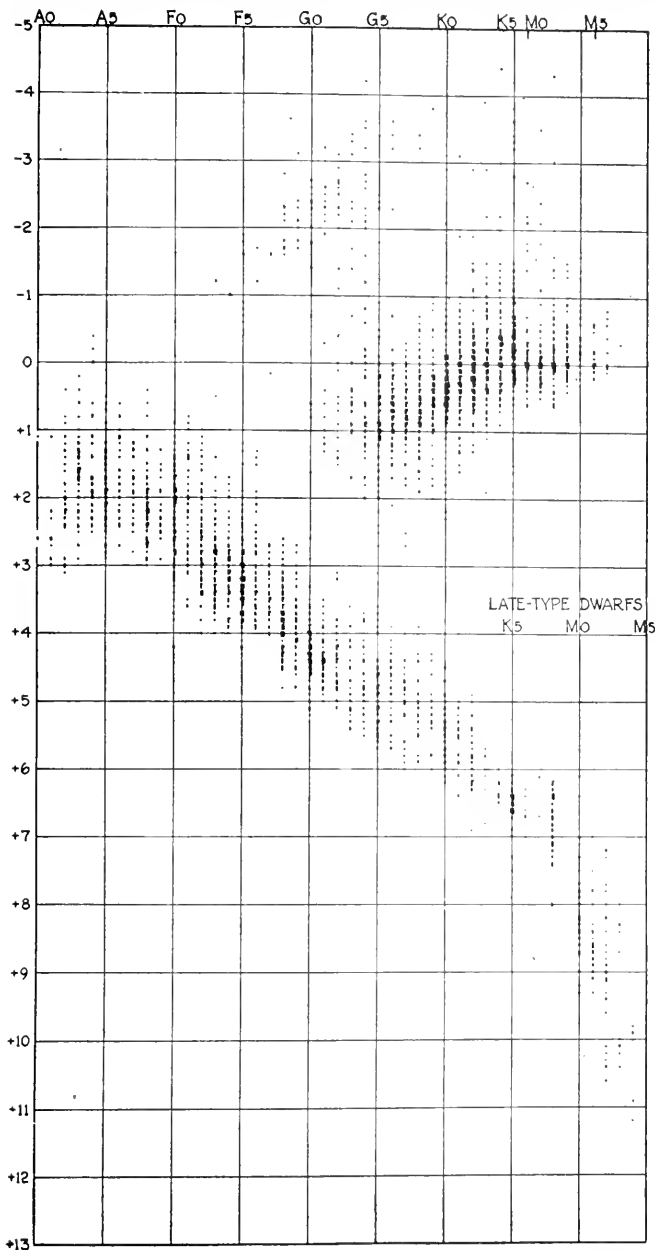
TABLE 795.—Masses of Spectroscopic Binaries, Sun = 1

| Class | O8 | B ₀ to B ₂ | B ₃ to B ₅ | B ₈ to A ₃ | A ₅ to F ₃ | F ₃ to G ₅ |
|-----------------------------------|-----|----------------------------------|----------------------------------|----------------------------------|----------------------------------|----------------------------------|
| No. of stars..... | 1 | 8 | 8 | 22 | 12 | 12 |
| Inferior limit $M_1 \sin^3 i$... | 75 | 12.2 | 4.9 | 2.3 | 1.4 | 1.2 |
| " " $M_2 \sin^3 i$... | 63 | 9.4 | 3.5 | 2.0 | 1.1 | 1.1 |
| Ratio | .84 | .77 | .71 | .87 | .79 | .89 |

NOTE.—16 Urs. Maj., spec. binary, F8 dwarf, RA 9^h 6^m, dec. + 61° 51', annual p. m. 0.032", $M + 4$, π 0.06, rad. veloc. — 15.0 km/sec. in about 10⁶ yrs will pass within 2 parsecs of sun. Barnard's star and α Centauri are only two stars known closer than 2 parsecs. They will pass the sun distant 1.1 and 0.93 parsecs. Kapteyn's star was distant 1.6 parsecs 10,000 years ago; 279 Sagittarii, 1.4 parsecs, 35,000 years hence. (Pop. Astron. 32, 324, 1924.)

RUSSELL DIAGRAM

Absolute magnitudes (ordinates) of 3,915 stars of different spectrum types (abscissae) determined by the spectroscopic method by Dr. W. S. Adams and his associates. (Courtesy of Mt. Wilson Observatory, 1932.)



The diagram shows the division of types G, and later, into giants (high luminosity stars) and dwarfs (low luminosity) with few or no intermediate stars. It resembles an inverted 7, and with the addition of much new material confirms fully that first drawn by Russell in 1913.

The stars may be divided into dwarfs, giants and supergiants. In each class the absolute magnitude progresses nearly linearly with spectral type except for the coolest stars; the direction of change is opposite for the dwarfs from that for the giants and supergiants. The luminosity of the dwarfs decreases regularly with advancing type (reduced surface temperature); it drops abruptly for the coolest. Among the giants and probably the supergiants the luminosity increases with decreasing temperature at least as far as the early subdivisions of type M.

The sequence of normal giants, conspicuous in types G, K, M, is almost missing for F5 and G0, the luminous stars of these latter types being supergiants. If this sequence is present in type A stars, they are intermingled with the dwarf sequence; the two sequences appear to cross in near type F0. If so, the more luminous stars of types

earlier than A should be those of the main dwarf series sequence. The tendency of both giants and dwarfs, especially giants, to group around definite values of absolute magnitude is remarkable. About 90 per cent of the K0 stars fall within limits of less than one magnitude. The hottest stars extend dwarf sequence up and to the left (Table 797). The white dwarfs belong to the lower left corner (Table 828), F to A, M 15 \pm .

(Strömberg, Mt. Wilson, Astrophys. Journ., 72, 111, 1930; 73, 40, 1931; 74, 110 and 342, 1931. See also Wilson, Astron. Journ., 41, 169, 1932.)

Statistical discussion of distribution of absolute magnitudes among the various spectrum groups. Figures marked** relate to supergiants,* normal giants,† dwarfs,*† normal giants and dwarfs, and refer to the groups of which the numbers thus marked are maxima. The subscripts are the percentages in the various groups. The first line of the table shows the number of stars used in the discussion for the column, but the figures in the columns are reduced so that the distribution is for 1000 stars in each group.

| Number | 124 | 246 | 152 | 351 | 416 | 558 | 622 | 601 | 1058 | 375 | 539 |
|-----------|----------------------------------|---------------------|---------------------|----------------------------------|---------------------|----------------------------------|----------------------------------|----------------------------------|----------------------------------|----------------------------------|---------------------|
| Abs. Mag. | B ₀ to B ₂ | B ₃ | B ₅ | B ₈ to B ₉ | A ₀ | A ₂ to A ₅ | F ₀ to F ₉ | G ₀ to G ₉ | K ₀ to K ₂ | K ₃ to K ₉ | M |
| -9.2 | 1 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. |
| 8.8 | 7 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. |
| 8.4 | 11 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. |
| 8.0 | 12 ₂ ** | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. |
| 7.6 | 9 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. |
| 7.2 | 5 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. |
| 6.8 | 0 | .. | .. | .. | .. | .. | .. | .. | .. | .. | .. |
| 6.4 | 0 | 3 | .. | .. | 3 | .. | .. | .. | .. | .. | .. |
| 6.0 | 2 | 8 ₂ ** | .. | .. | 7 | .. | .. | .. | .. | .. | .. |
| 5.6 | 14 ₁₈ ** | 4 | .. | .. | 8 ₄ ** | .. | .. | .. | 0 | 4 | 1 |
| 5.2 | 10 | 0 | .. | .. | 8 | .. | 2 | 3 | 0 | 10 | 12 |
| 4.8 | 2 | 17 | 8 | 4 | 6 | 1 | 3 | 9 | 0 | 14 | 24 |
| 4.4 | 38 | 43 | 32 | 17 | 3 | 8 | 6 | 14 | 2 | 15 ₇ ** | 28 ₉ ** |
| 4.0 | 80 | 53 ₁₈ ** | 50 ₁₇ ** | 33 | 0 | 19 | 14 | 22 | 8 | 13 | 23 |
| 3.6 | 116 | 53 | 50 | 38 ₁₈ ** | 0 | 28 | 18 ₉ ** | 27 | 14 | 11 | 4 |
| 3.2 | 230 | 16 | 26 | 32 | 0 | 32 ₁₅ ** | 15 | 27 ₁₉ ** | 20 | 8 | 0 |
| 2.8 | 262 ₈₀ ** | 0 | 2 | 22 | 0 | 29 | 13 | 25 | 25 | 12 | 0 |
| 2.4 | 107 | 16 | 4 | 6 | 0 | 22 | 16 | 31 | 26 ₁₄ ** | 21 | 2 |
| 2.0 | 39 | 120 | 103 | 0 | 0 | 9 | 3 | 27 | 23 | 33 | 26 |
| 1.6 | 13 | 228 | 232 ₈₃ * | 0 | 1 | 1 | 0 | 2 | 6 | 46 | 74 |
| 1.2 | 1 | 229 ₈₀ * | 219 | 22 | 5 | 0 | 0 | 0 | 10 | 66 | 116 |
| 0.8 | 4 | 125 | 131 | 210 | 13 | 0 | 0 | 0 | 23 | 111 | 148 |
| -0.4 | 20* | 64 | 86 | 248 ₈₈ * | 34 | 1 | 1 | 1 | 99 | 171 | 157 ₉₁ * |
| 0.0 | 13 | 19 | 37 | 206 | 167 | 34 | 23 | 88 | 235 | 185 ₉₀ * | 149 |
| +0.4 | 4 | 2 | 13 | 100 | 254 ₉₆ * | 132 | 56 | 238 ₄₉ * | 269 ₇₈ * | 112 | 135 |
| 0.8 | .. | .. | 6 | 43 | 249 | 189 | 91 | 133 | 111 | 58 | 62 |
| 1.2 | .. | .. | 1 | 17 | 162 | 192 ₈₅ *† | 120 ₄₅ * | 30 | 24 | 36 | 22 |
| 1.6 | .. | .. | .. | 2 | 53 | 160 | 109 | 10 | 17 | 25 | 5 |
| 2.0 | .. | .. | .. | .. | 22 | 98 | 46 | 32 | 14 | 15 | .. |
| 2.4 | .. | .. | .. | .. | 5 | 28 | 38 | 48 | 15 | 7 | .. |
| 2.8 | .. | .. | .. | .. | .. | 8 | 100 | 53 _{23,19} *† | 18 ₆ *† | 3 | .. |
| 3.2 | .. | .. | .. | .. | .. | 5 | 139 ₄₆ † | 50 | 14 | 0 | .. |
| 3.6 | .. | .. | .. | .. | .. | 3 | 111 | 38 | 4 | 0 | .. |
| 4.0 | .. | .. | .. | .. | .. | 1 | 52 | 36 | 0 | 0 | .. |
| 4.4 | .. | .. | .. | .. | .. | .. | 19 | 32 | 0 | 0 | .. |
| 4.8 | .. | .. | .. | .. | .. | .. | 5 | 18 | 0 | 0 | .. |
| 5.2 | .. | .. | .. | .. | .. | .. | 0 | 5 | 1 | 0 | .. |
| 5.4 | .. | .. | .. | .. | .. | .. | 0 | 1 | 3 | 2 | .. |
| 5.8 | .. | .. | .. | .. | .. | .. | .. | .. | 4 ₁ † | 3 | .. |
| 6.2 | .. | .. | .. | .. | .. | .. | .. | .. | 4 | 6 | .. |
| 6.6 | .. | .. | .. | .. | .. | .. | .. | .. | 1 | 7 ₂ † | .. |
| 7.0 | .. | .. | .. | .. | .. | .. | .. | .. | 0 | 5 | .. |
| 7.4 | .. | .. | .. | .. | .. | .. | .. | .. | 0 | 1 | .. |

Summary (mean abs. magnitude)

| Spectrum | No. stars | Super-giants | Bright giants | Normal giants | Faint giants | Dwarfs |
|---------------------------------|-----------|--------------|---------------|---------------|--------------|----------|
| Mo to M ₉ | 247 | -4.5(9) | | -0.2(91) | | |
| K ₃ " K ₉ | 378 | -4.5(7) | | -0.1(91) | | +6.7(2) |
| K ₀ " K ₂ | 1058 | | -2.5(14) | +0.3(78) | +2.7(7) | +6.1(1) |
| G ₀ " G ₉ | 601 | | -3.0(19) | +0.4(49) | +2.8(23) | +4.2(9) |
| F ₀ " F ₉ | 622 | | -3.0(9) | +1.2(25) | | +3.2(46) |
| A ₂ " A ₅ | 478 | | -3.2(15) | | | +1.2(85) |

The small percentage of dwarf stars is due to the fact that their apparent magnitudes in most cases are fainter than the set limit of 6.0.

TABLE 798.—Brightness of the Stars

Stellar magnitudes give the apparent brightness of the stars on a logarithmic scale,—a numerical increase of one magnitude corresponding to a decrease of the common logarithm of the light by 0.400, and a change of five magnitudes to a factor of 100. The brightest objects have negative stellar magnitudes. The visual magnitude of the Sun is -26.7 ; of the mean full Moon, -12.5 ; of Venus at her brightest, -4.3 ; of Jupiter, at opposition, -2.3 ; of Sirius, -1.6 ; of Vega, $+0.2$; of Polaris, $+2.1$. (The stellar magnitude of a standard candle 1 m distant is -14.18 .) The faintest stars visible with the naked eye on a clear dark night are of about the sixth magnitude (though a single luminous point as faint as the eighth magnitude can be seen on a perfectly black background). The faintest stars visible with a telescope of aperture d in. are approximately of magnitude $9 + 5 \log_{10} d$. The faintest photographed with the 100-inch reflector at Mt. Wilson are of about the 22nd magnitude. A standard candle, of the same color as the stars, would appear of magnitude $+0.8$ at a distance of one kilometer.

The actual luminosity (absolute magnitude) is the stellar magnitude which the star would have if placed at a distance of ten parsecs. The faintest star at present known (Lunes), a distant companion to α Centauri, has the (visual) absolute magnitude $+15.4$, and a luminosity 0.00006 that of the sun. The brightest so far definitely measured, β Orionis, has (Kapteyn) the abs. mag. -5.5 and a luminosity 13,000 times the sun's. Canopus, and some other stars, may be still brighter. Note 1931: S. Doradus abs. mag. probably > -8 .

The absolute magnitudes of 6 planetary nebulae average 0.1; average diameter, 4000 astronomical units (Solar system to Neptune = 60 astr. units), van Maanen, Proc. Nat. Acad. Sci. 4, p. 394, 1918.

TABLE 799.—Giant and Dwarf Stars

The stars of Class B are all bright, and nearly all above the absolute magnitude zero. Stars of comparable brightness occur in all the other spectral classes, but the inferior limit of brightness diminishes steadily for the "later" or redder types. The distribution of absolute magnitudes conforms to the superposition of two series, in each of which the individual stars of each spectral class range through one or two magnitudes on each side of the mean absolute magnitude. Absolute magnitude supergiants -2 to -8 ; giants roughly 0 to $+1$; dwarfs A, 1 to 2; F, 2 to 4; G, 4 to 6; K, 6 to 9; M, 0 to 11. The two series overlap in Classes A and F, are fairly well separated in Class K, and sharply so in Class M. Two very faint stars of Classes A and F fall into neither series.

The majority of the stars visible to the naked eye are giants since these, being brighter, can be seen at much greater distances. The greatest percentage of dwarf stars among those visible to the eye is found in Classes F and G. The dwarf stars of Classes K and M are actually much more numerous per unit of volume, but are so faint that few of the former, and none of the latter, are visible to the naked eye.

TABLE 800.—Masses and Densities

Stars differ less in mass than in any other characteristic. The most massive star known is the brighter component of the spectroscopic binary B.D. 6 1309, 86 times the sun's mass, 113 times its luminosity, and spectrum Oe. The smallest known mass is that of the faint component of the visual binary Krueger 60, whose mass is 0.15, and luminosity 0.0004 of the sun's, and spectrum M. Note: Plaskett notes giant double star 184 sun's mass.

The giant stars are in general more massive than the dwarfs. According to Russell (Publ. Astron. Soc. America, 3, 327, 1917) the mean values of Binary systems are:

| Spectrum | B2 | A0 | F5 giant | K5 giant | F2 dwarf | G2 dwarf | K8 dwarf |
|----------------------|----|-----|----------|----------|----------|----------|----------|
| Ratio of mass to Sun | 12 | 6.5 | 8 | 10 | 3.0 | 1.2 | 0.9 |

The densities can be determined only for eclipsing variables. Stars of Classes B and A have densities averaging about one tenth that of the sun and a relatively small range; Classes F to K show a wide range in density, from 1.8 times that of the sun (W Urs. Maj.) to 0.000002 (W Crucis).

The surface brightness probably diminishes by at least one magnitude for each step along the Harvard scale from B to M. It follows that the dwarf stars are, in general, closely comparable with the sun in diameter, while the stars of Classes B and A, though larger, rarely exceed ten times the sun's diameter. The redder giant stars must be much larger, and a few, such as Antares, may have diameters exceeding that of the earth's orbit. The densities of these stars must be exceedingly low.

Arranged in order of increasing density, the stars form a single sequence starting with the giant stars of Class M, proceeding up that series to Class B, and then down the dwarf series to Class M.

| Star | Type | Mag. | Diam. | Parallax | Mass | Density | Brightness | Diameter (km) |
|-------------------|------|-------|-------|----------|------|----------|------------|---------------|
| Antares | Map | 1.2 | "038 | "013 | 30. | .0000010 | 1600. | 440,000,000 |
| Betelgeuse | Ma | 0.0 | "044 | "018 | 30. | .0000012 | 1450. | 378,000,000 |
| α Hercules | Mb | 3.5 | "015 | "007 | 30. | .0000020 | 710. | 330,000,000 |
| Aldebaran | K5 | 1.5 | "027 | "075 | 10. | .00017 | 36. | 52,000,000 |
| Arcturus | K0 | 0.2 | "023 | "005 | 10. | .0007 | 78. | 37,000,000 |
| Rigel | B3 | 0.3 | "019 | "007 | 30. | .0012 | 13500. | 40,000,000 |
| Capella | G0 | 0.2 | "082 | "071 | 4.6 | .006 | 78. | 13,000,000 |
| Vega | A0 | 0.1 | "026 | "004 | 5. | .21 | 86. | 4,200,000 |
| Procyon | F5 | 0.5 | "057 | "370 | 2.5 | .02 | 26. | 2,300,000 |
| Our Sun | G | -26.5 | 960. | — | 1. | .00 | 5. | 2,300,000 |
| Krueger 60 | Mb | 0.3 | "0011 | "200 | 4.2 | 4.0 | 0.002 | 1,301,000 |
| Prox. Cent. | N | 11.0 | "0017 | "70 | .055 | 4.0 | .00006 | 580,000 |
| Barnard's | Mb | 0.7 | "0009 | "53 | .023 | 4.0 | .0004 | 333,000 |
| | | | | | | | | 249,000 |

Computed by Plaskett, Publ. Ast. Soc. Pac. 1922; Interferometer measurements, Antares, 0.024", 30,600,000 km; Betelgeuse, 0.047", 386,000,000 km. (1921).

TABLE 801.—Parallax and Mean Apparent Magnitude

(Reprinted by permission from Russell, Dugan, and Stewart, *Astronomy*, Ginn & Co., 1927.)

| Magnitude | Mean parallax | <i>m</i> | <i>p</i> | <i>m</i> | <i>p</i> |
|-----------|---------------|----------|----------|----------|----------|
| 1 | 0''.083 | 6 | 0''.0120 | 11 | 0''.0018 |
| 2 | .056 | 7 | .0082 | 12 | .0013 |
| 3 | .038 | 8 | .0056 | 13 | .0009 |
| 4 | .026 | 9 | .0039 | | |
| 5 | .018 | 10 | .0027 | | |

TABLE 802.—Spectrum Type and Mean Absolute Magnitude

(Trumpler, *Bull. Lick Obs.*, No. 420, 1930.)

| Mean absolute magnitude Dwarf branch | | | Mean absolute magnitude Giants | | | | |
|---|------|--------|-----------------------------------|------|--------|------|--------|
| Type | Vis. | Phtgr. | Type | Vis. | Phtgr. | Vis. | Phtgr. |
| O | -4.0 | -4.3 | A3 | +2.0 | +2.1 | | |
| B0 | -3.1 | -3.4 | A5 | +2.3 | +2.5 | | |
| B1 | -2.5 | -2.8 | F0 | +2.9 | +3.2 | +0.5 | +0.9 |
| B2 | -1.8 | -2.1 | F2 | +3.2 | +3.5 | | |
| B3 | -1.2 | -1.4 | F5 | +3.6 | +4.0 | + .5 | +1.0 |
| B5 | - .8 | -1.0 | F8 | +4.2 | +4.7 | | |
| B8 | - .2 | - .3 | G0 | +4.5 | +5.1 | + .5 | +1.2 |
| B9 | + .3 | + .3 | G5 | +5.0 | +5.7 | + .5 | +1.4 |
| A0 | + .9 | + .9 | K0 | +6.2 | +7.0 | + .5 | +1.6 |
| A2 | +1.7 | +1.7 | | | | | |

Based on Adams, Joy, Mt. Wilson Contr. 199, 244, 262; Lundmark, Publ. Astron. Soc. Pacific, 34, 1922; Malmquist, Meddel. Lund. II, 32, 1924; Hess, Seeliger Festschrift, p. 265, 1924.

TABLE 803.—Reduction of Visual to Bolometric Magnitude

Eddington (M. N. 177, 605) gives the corrections from visual to bolometric magnitudes for the cooler stars. For the hotter stars the data are not so certain. The values are to be added algebraically to the absolute visual magnitudes.

| | | | | | | | | | |
|----|-------|----|-------|-----|------|-----|------|-----|-------|
| O5 | -3.60 | A0 | -0.31 | F5 | 0.00 | gM5 | -1.5 | dK4 | -0.50 |
| O6 | -3.30 | A1 | -.27 | F6 | .00 | dG0 | -.01 | dK5 | -.60 |
| O7 | -2.90 | A2 | -.23 | F7 | -.02 | dG1 | -.02 | dK6 | -.71 |
| O8 | -2.50 | A3 | -.19 | F8 | -.03 | dG2 | -.02 | dK7 | -.82 |
| O9 | -2.10 | A4 | -.15 | F9 | -.05 | dG3 | -.02 | dK8 | -.93 |
| B0 | -1.80 | A5 | -.12 | gG0 | -.10 | dG4 | -.03 | dK9 | -1.05 |
| B1 | -1.65 | A6 | -.09 | gG2 | -.14 | dG5 | -.03 | dM0 | -1.17 |
| B2 | -1.50 | A7 | -.06 | gG5 | -.17 | dG6 | -.03 | dM2 | -1.30 |
| B3 | -1.35 | A8 | -.04 | gG6 | -.18 | dG7 | -.04 | dM3 | -1.43 |
| B4 | -1.20 | A9 | -.02 | gG7 | -.21 | dG8 | -.06 | dM4 | -1.56 |
| B5 | -1.00 | F0 | -.02 | gG8 | -.25 | dG9 | -.09 | dM5 | -1.71 |
| B6 | -.85 | F1 | -.01 | gK0 | -.39 | dK0 | -.14 | dM6 | -1.85 |
| B7 | -.65 | F2 | -.01 | gK3 | -.65 | dK1 | -.22 | dM7 | -2.05 |
| B8 | -.53 | F3 | .00 | gK4 | -.74 | dK2 | -.31 | dM8 | -2.30 |
| B9 | -.39 | F4 | .00 | gK5 | -.83 | dK3 | -.40 | dM9 | -2.59 |

TABLE 804.—Summary, Elements of Solar Motion (Campbell, 1928)

(Publ. Lick Obs., vol. 16, 1928.)

| | | | | |
|-----------------|-------------------------|-------------------------|---------------------|-----------------------------------|
| Charlier | $\alpha_0, 269.3^\circ$ | $\delta_0, +30.8^\circ$ | $v_0, 19.0$ km/sec. | 1986 r. v.; 4182 p. m.; 646 π |
| Strömberg | 272.1 | +29.5 | 20.6 | Space veloc. 1026, A6-M. |
| Wilson | 270.8 | +27.1 | 19.0 | 2748, 2395, r. v. and p. m. |
| Campbell, Moore | 270.58 | +29.24 | 19.65 | 2149 r. v. B-M stars |
| Mean | 270.70 | +29.16 | 19.55 | |

Dwarf stars decidedly higher space velocity than giants (Strömberg).

| | | | | |
|------------------|----------------------|------------|--------------------------------|------------|
| Class B (Oo5-B5) | $v_0 = 22.7$ km/sec. | $K = +4.9$ | $K (G5-K4) v_0 = 18.0$ km/sec. | $K = +0.3$ |
| A (B8-A3) | 18.6 | +1.7 | M (K5-Mb) | 22.1 |
| F (A5-F4) | 19.7 | +1.3 | B-M | 19.7 |
| G (F5-G4) | 18.6 | — .2 | | +1.26 |

Dwarfs appear only in classes F, G; remove 3 from G, $v_0 = 16.6$ km/sec.

TABLE 805.—Elements of Solar Motion (Charlier, 1926)

(Charlier, The motion and the distribution of the stars, Mem. Univ., California, vol. 7, 1926)

Radial velocities lead to conclusion stars are receding.
Galactic coordinates of apex.

| Type | No. stars | Galac. long. ° | Galac. lat. ° | Mag. | No. stars | Galac. long. ° | Galac. lat. ° |
|--------------|-----------|----------------|---------------|--------------|-----------|----------------|---------------|
| B stars..... | 694 | 26.7 | +17.3 | 5.0-5.9..... | 454 | 20 | +22 |
| A "..... | 1281 | 18.6 | +22.8 | 6.0-6.9..... | 1003 | 29 | +16 |
| F "..... | 508 | 17.8 | +20.4 | 7.0-7.9..... | 1239 | 55 | +17 |
| G "..... | 379 | 29.7 | +28.6 | 8.0-8.9..... | 811 | 37 | +24 |
| K "..... | 1135 | 37.7 | +17.8 | 8.6..... | 276 | 55 | +23 |
| M "..... | 190 | 31.5 | +20.6 | 11.1..... | 203 | 69 | +24 |

1986 (rad. v.), 646 (parallax stars); sun's velocity = 19.0 km/sec.

(4 astr. units/yr.). 1986 (rad. v.), 646 (par. stars), 4182 (p. m. stars) give as apex. Galac. long., $24^\circ.3$, latitude, $+22^\circ.44$; $\alpha = 269.3$, $\delta = +30^\circ.85$

TABLE 806.—Stars of Large Proper Motion

| Mag. | p. m. | spect. | | Mag. | p. m. | spect. |
|------------------------|-------|--------|-----|--------------------------------------|-------|---------|
| | | | " | | | " |
| Barnard's..... | 9.7 | 10.2 | M5 | O ₂ Eridani (triple)..... | 4.5 | 4.1 G5 |
| Kapteyn's..... | 9.2 | 8.8 | M0 | Wolf 489..... | 13 | 3.9 ... |
| Gr. 1830..... | 6.5 | 7.0 | G5 | Prox. Centauri..... | 10.5 | 3.8 M? |
| Lacaille 9352..... | 7.4 | 6.9 | M0 | μ Cassiopeiae..... | 5.3 | 3.8 G5 |
| Cordoba 32416..... | 8.3 | 6.1 | M3 | α Centauri (double)..... | 3 | 3.7 G0 |
| 61 Cygni (double)..... | 6.3 | 5.2 | K8 | Washington 5584 (double) | 8.9 | 3.7 G0 |
| Wolf 359..... | 13 | 4.8 | ... | Cordoba 29191..... | 6.6 | 3.5 M0 |
| Lalande 21185..... | 7.6 | 4.8 | M2 | ϵ Eridani..... | 4.3 | 3.2 G5 |

In case of multiple stars the magnitudes and spectra of the brightest star are indicated.

See Lick Obs. Bull. 344; Harvard Circular 283; also Luyten, Astronom. Journ. 42, 69, 1932. List of stars, p. m. > $0''.5$ annually. The following stars, Van Maanen's, $3''.01$, Ross 619, R. A. 8^h06^m , Dec. $+92^\circ$, annual p. m. $5''.40$, may be added to the above list.

TABLE 807.—Spectrum Class and Proper Motions

(Reprinted by permission from Russell, Dugan, and Stewart, *Astronomy*, Ginn & Co., 1927.)

| Limits of p. m. | O | B | A | F | G | K | M | N |
|--------------------------|-------|-------|-------|-------|-------|-------|-------|----|
| 0".00 to 0".02..... | 13 | 238 | 392 | 97 | 107 | 218 | 48 | 3 |
| 0 .02 to 0 .04..... | 6 | 164 | 533 | 115 | 91 | 327 | 54 | 4 |
| 0 .04 to 0 .10..... | 1 | 88 | 476 | 231 | 168 | 393 | 99 | 2 |
| 0 .10 to 0 .20..... | .. | .. | 160 | 245 | 70 | 242 | 27 | 1 |
| 0 .20 to 0 .45..... | .. | 1 | 31 | 168 | 56 | 88 | 8 | .. |
| 0 .45 to 0 .80..... | .. | .. | 1 | 46 | 20 | 23 | 1 | .. |
| 0 .80 to 2 .00..... | .. | .. | 1 | 12 | 19 | 13 | .. | .. |
| Over 2".00 | .. | .. | .. | 1 | 6 | 6 | .. | .. |
| Mean p. m.0".22 | 0".03 | 0".06 | 0".17 | 0".18 | 0".12 | 0".07 | 0".04 | |
| Percentage of stars with | | | | | | | | |
| $\mu > 0".20$ | 0 | 0.2 | 5 | 25 | 18 | 10 | 4 | 0 |

TABLE 808.—Equipartition of Energy in Stellar Motions

(Jeans, *Nature*, 122, 689, 1928.)

| Type. | Mean mass. | Mean velocity. | Mean energy. | Corresponding temperature. |
|------------|-----------------------|----------------------------|-----------------------|----------------------------|
| B3 | 10.8×10^{23} | 14.8×10^5 cm/sec. | 1.95×10^{46} | 1.0×10^{62} °K. |
| B8.5 | 12.9 " | 15.8 " | 1.62 " | 0.8 " |
| A0 | 12.1 " | 24.5 " | 3.63 " | 1.8 " |
| A2 | 10.0 " | 27.2 " | 3.72 " | 1.8 " |
| A5 | 8.0 " | 29.9 " | 3.55 " | 1.7 " |
| F0 | 5.0 " | 35.9 " | 3.24 " | 1.6 " |
| F5 | 3.1 " | 47.9 " | 3.55 " | 1.7 " |
| G0 | 2.0 " | 64.6 " | 4.07 " | 2.0 " |
| G5 | 1.5 " | 77.6 " | 4.57 " | 2.2 " |
| K0 | 1.4 " | 79.4 " | 4.27 " | 2.1 " |
| K5 | 1.2 " | 74.1 " | 3.39 " | 1.7 " |
| M0 | 1.2 " | 77.6 " | 3.55 " | 1.7 " |

"This equality of energy can be attributable only to the gravitational interaction of the stars. For if it were produced by any physical agency, such as pressure of radiation, bombardment by molecules, atoms, or high-speed electrons, this agency, as the last column shows, would have to be in thermodynamical equilibrium with matter at a temperature of the order of 2×10^{62} °K. Since no such temperatures are known the observed equality must be due to gravitational interactions over millions of years. Such evidence suggests a general age of the stars of 5 to 10 million-million years."

TABLE 809.—Stars of Large Space Velocity, Greater Than 300 km/sec.

| Right ascension and declination 1900 | App. magnitude | Parallax π | Apex of motion Right ascension and declination | Velocity km/sec. | Right ascension and declination 1900 | App. magnitude | Parallax π | Apex of motion Right ascension and declination | Velocity km/sec. |
|--------------------------------------|----------------|----------------|---|------------------|--------------------------------------|----------------|----------------|---|------------------|
| ° ° | | " | ° ° | | ° ° | | " | ° ° | |
| 8.5 + 2.6 | 7.4 | 0.007 | 100 +23 | 543 | 223.6 -21.6 | 8.5 | 0.009 | 145 -45 | 429 |
| 15.8 +61.0 | 7.8 | .015 | 149 -46 | 369 | 226.2 -16.0 | 9.9 | .034 | 189 -69 | 590 |
| 32.4 - 1.7 | 9.2 | .013 | 121 - 3 | 362 | 226.2 -15.9 | 9.4 | .034 | 187 -69 | 583 |
| 62.2 +22.1 | 8.9 | .008 | 97 - 4 | 448 | 227.1 +19.7 | 7.3 | .006 | 124 +24 | 509 |
| 72.8 +34.1 | 8.0 | .006 | 150 -11 | 465 | 234.4 -10.6 | 7.3 | .012 | 123 - 8 | 479 |
| 116.8 +30.9 | 8.2 | .040 | 257 -64 | 333 | 245.4 +19.1 | var. | .002 | 205 -69 | 409 |
| 127.3 -31.2 | 6.4 | .008 | 57 +27 | 786 | 246.9 +48.2 | 7.0 | .003 | 220 -42 | 482 |
| 128.6 + 6.1 | 7.8 | .002 | 213 -59 | 799 | 262.5 + 6.1 | 8.5 | .008 | 143 +37 | 395 |
| 135.4 +23.4 | {6.3 7.1} | .002 | 48 + 3 | 371 | 263.5 +18.6 | 9.1 | .002 | 167 -51 | 695 |
| 138.8 +34.8 | 3.3 | .002 | 49 + 6 | 501 | 264.1 +37.3 | 8.6 | .013 | 302 -35 | 364 |
| 145.9 +14.2 | 8.1 | .003 | 187 -50 | 787 | 304.4 -21.7 | 8.2 | .012 | 92 -41 | 480 |
| 153.6 +20.4 | 3.2 | .004 | 239 -27 | 420 | 308.6 +42.5 | 7.1 | .003 | 90 +44 | 306 |
| 176.8 +38.4 | 6.5 | .101 | 243 -49 | 346 | 314.8 + 2.6 | 8.1 | .003 | 228 -51 | 767 |
| 180.0 - 1.0 | 8.4 | .004 | 92 + 7 | 617 | 341.6 +13.4 | 8.0 | .005 | 78 +28 | 440 |
| 182.0 +10.6 | 8.0 | .005 | 256 -58 | 408 | 355.0 +29.0 | 8.9 | .009 | 80 + 6 | 466 |
| 192.0 -18.0 | 8.3 | .011 | 273 -67 | 418 | | | | | |
| 222.0 +19.2 | 8.0 | .002 | 55 +66 | 444 | | | | | |

This and the following table are taken from Katalog von 1937 absoluten Sternengeschwindigkeiten, Klumak, Hecht, Astron. Nachr. no. 5696-7, 238, 116, 1930. See also Wilson, Raymond, Astron. Journ. 40, 121, 1930, 4233 stars.

TABLE 810.—Stars of Small Space Velocity, 5 km/sec. or less

Same reference and designations as for preceding table.

| Right ascension and declination 1900 | App. magnitude | Parallax π | Apex of motion Right ascension and declination | Velocity km/sec. | Right ascension and declination 1900 | App. magnitude | Parallax π | Apex of motion Right ascension and declination | Velocity km/sec. |
|--------------------------------------|----------------|----------------|---|------------------|--------------------------------------|----------------|----------------|---|------------------|
| ° ° | | " | ° ° | | ° ° | | " | ° ° | |
| 8.7 +56.0 | 2.5 | 0.016 | 345 +34 | 5 | 185.2 +39.6 | 5.2 | 0.021 | 180 + 9 | 4 |
| 16.0 +35.1 | 2.4 | .045 | 95 -18 | 3 | 207.1 +18.4 | 5.7 | .010 | 126 + 7 | 4 |
| 18.1 -69.4 | 5.0 | .160 | 315 - 6 | 5 | 224.6 -24.9 | 3.4 | .025 | 193 +27 | 5 |
| 41.0 +26.9 | 3.7 | .031 | 299 -57 | 5 | 241.4 +45.2 | 4.3 | .014 | 41 +68 | 5 |
| 66.6 +42.8 | 6.8 | .018 | 306 -61 | 4 | 255.8 +54.6 | 5.8 | .044 | 157 +15 | 4 |
| 69.1 +22.8 | 4.3 | .008 | 12 +45 | 4 | 268.9 +16.8 | 4.7 | .011 | 125 -11 | 5 |
| 73.6 +60.3 | 4.2 | .004 | 284 + 9 | 5 | 274.1 +36.0 | 4.3 | .042 | 146 - 1 | 5 |
| 92.7 +46.4 | 6.5 | .035 | 243 -26 | 5 | 277.9 +52.3 | 5.4 | .007 | 197 -31 | 5 |
| 99.5 +25.2 | 3.2 | .007 | 230 +26 | 4 | 297.3 - 8.5 | 6.5 | .010 | 16 +50 | 3 |
| 110.2 -31.6 | 5.4 | .035 | 145 -14 | 5 | 297.4 + 8.2 | 4.9 | .038 | 0 -27 | 5 |
| 112.2 +56.0 | 6.0 | .013 | 238 - 6 | 4 | 299.3 +27.5 | 4.7 | .030 | 121 + 9 | 5 |
| 131.1 +33.7 | 6.2 | .038 | 274 +41 | 5 | 305.0 +31.9 | 4.6 | .016 | 353 +31 | 4 |
| 156.4 +81.0 | 6.6 | .005 | 271 -44 | 4 | 325.4 -16.6 | 3.0 | .114 | 245 - 2 | 3 |
| 183.6 +28.7 | 6.3 | .056 | 355 -76 | 5 | 349.0 +37.6 | 5.8 | .035 | 330 -56 | 5 |

TABLE 811.—Motions of the Stars

The individual stars are moving in all directions, but, for the average of considerable groups, there is evidence of a drift away from the point in the heavens towards which the sun is moving (solar apex). The best determinations of the solar motion, relative to the stars as a whole, are given in Table 804. In round numbers this motion of the sun may be taken as 20 km/sec. towards the point R. A. 18 h. o. m., Dec. $+30^{\circ}$.

After allowance is made for the solar motion, the motions of the stars in space, relative to the general mean, present marked peculiarities. If from an arbitrary origin a series of vectors are drawn, representing the velocities of the various stars, the ends of these vectors do not form a spherical cluster (as would occur if the motions of the stars were at random), but a decidedly elongated cluster, whose form can be approximately represented either by the superposition of two intermingling spherical clusters with different centers (Kapteyn's two-stream hypothesis) or by a single ellipsoidal cluster (Schwarzschild), the actual form, however, being more complicated than is indicated by either of these hypotheses. The direction of the longest axis of the cluster is known as that of preferential motion. The two opposite points in the heavens at the extremities of this axis are called the vertices. The components of velocity of the stars parallel to this axis average considerably larger than those parallel to any axis perpendicular to it.

The preferential motion varies greatly with spectral type, being practically absent in Class B, very strong in Class A, and somewhat less conspicuous in Classes F to M, on account of the greater mean velocities of these stars in all directions. The positions of the vertices are nearly the same for all.

Numerous investigators, from the more distant naked-eye stars, find substantially the same position for the vertex, the mean being R. A. 6 h. 6 m., Dec. $+9^{\circ}$. The nearer stars, of large proper motion, give a mean of 6 h. 12 m., $+25^{\circ}$. (See Strömberg's discussion, cited above.)

In addition to these general phenomena, there are numerous clusters of stars whose members possess almost exactly equal and parallel motions,—for example, the Pleiades, the Hyades, and certain large groups in Ursa Major, Scorpius, and Orion. The vertices, and the directions toward which these clusters are moving, are all in the plane of the galaxy.

The greatest known p. m. star is Barnard's 9th m. in Ophiuchus, $10.3''$ per year, position angle 356° , parallax $0.52''$, radial velocity about -117 km/sec.

The average radial velocity of the globular clusters is 100 km/sec. The globular clusters as a class are approaching the sun. The spiral nebulae are receding.

A general card catalogue of radial velocities is kept at the Lick Observatory. See Campbell, Radial velocities of 2600 stars, Lick Obs. Publ., vol. 16, 1928; of 741 stars, Adams, Joy, Strömberg, Sanford—Astroph. Journ. 70, 1929.

TABLE 812.—Known Stars of Radial Velocities Greater Than 100 km/sec.

| Star | Mag. | Spectrum class | R. A. h. m. | Dec. ° | Proper motion | Velocity km/sec. |
|-------------------------------|---------|----------------|----------------|--------|---------------|------------------|
| (1) RZ Lyrae..... | ... | ... | ... | ... | ... | +385 |
| (2) Washington 5583..... | 9.1 | G5 | ... | ... | 3.68 | +307 |
| (3) Washington 5584..... | 8.9 | G6 | ... | ... | 3.68 | +295 |
| (4) S Carinae..... | var. | Md | 10 06 | -61 4 | ... | +289 |
| (5) Kapteyn's star..... | 9.2 | Mo | ... | ... | 8.76 | +242 |
| (6) Van Maanen No. 2..... | 12.3 | dF3 | 0 45 | + 5 2 | 3.01 | +238 |
| (7) Cord. 5-243..... | ... | G-K | 5 8 | -45 59 | ... | +225 |
| (8) R Pictoris..... | var. | Md | 4 44 | -49 26 | ... | +207 |
| (9) A G Wash. 3498..... | 9.4 | A7 | 8 37 | -16 4 | .56 | +200 |
| (10) 41312 Boss 1511..... | 5.2 | G5 | 5 59 | -26 17 | ... | +184 |
| (11) ω Pavonis..... | 5.1 | K0 | 18 50 | -60 20 | ... | +181 |
| (12) Luyten 680..... | 10.8 | dGo | 21 52 | +32 17 | .73 | -178 |
| (13) BD +34° 2476..... | 9.3 | A3sp | 13 56 | +34 16 | .54 | -164 |
| (14) V Urs. Min..... | 7.5-8.7 | gM5 | 13 37 | +74 41 | ... | -158 |
| (15) BD +35° 3659..... | 9.5 | Fos | 19 28 | +36 1 | .56 | -172 |
| (16) BD +6° 2932..... | 9.5 | dG1 | 14 40 | + 6 9 | .93 | -139 |
| (17) AGC 27600..... | 5.3 | K5 | 20 5 | -36 21 | ... | -130 |
| (18) Barnard star..... | 9.7 | M5 | ... | ... | 10.25 | -117 |
| (19) μ Columbae..... | 5.2 | B2 | 5 42 | -32 21 | ... | +110 |
| (20) BD -3° 3746..... | 9.2 | dMo | 15 10 | - 3 32 | .69 | -106 |
| (21) β GC 10404 br..... | 8.5 | gK4 | 20 36 | +21 27 | ... | -106 |
| (22) Cin. 2750..... | 8 | dF9 | 21 9 | +23 51 | .46 | -103 |
| (23) 172 G Puppis..... | 5.4 | F8 | 7 42 | -33 59 | ... | +102 |
| (24) γ 31 Aquilae..... | 5.2 | G5 | 19 20 | +11 44 | ... | -101 |
| (25) Boss 4188..... | 5.4 | Ma | 16 22 | - 7 22 | ... | +101 |
| (26) δ Leporis..... | 3.9 | K0 | 5 47 | -20 53 | ... | +100 |

(Tables abridged by permission from Russell, Dugan, and Stewart, *Astronomy*, Ginn & Co., 1927.)

TABLE 813.—Visual Binary Stars

Burnham's General Catalogue, 1906, 3,665 pairs. Card catalogue kept by Aitken at Lick Observatory. Of stars brighter than 6.5 mag., one in 9 visual double. See also Aitken, *The binary stars*, McMurtrie, 1918, and New General Catalogue, Carnegie Institution, 1932; Innis, *Southern double star catalogue*, 1927.

e is eccentricity, a major axis in seconds of arc, A in astronomical units of orbit.

| Star | Magnitude | Spectra | Period | e | a | A | $m_1 + m_2$ | m_1, m_2 | Abs. mag. |
|---------------------|-----------|---------|---------------------|------|---------------------|------|-------------|------------|------------|
| α Aur..... | 0.8, 1.1 | G0, F5 | 0 ^h .285 | 0.01 | 0 ^h .054 | 0.85 | 7.5 | 4.2, 3.3 | -0.2, 0.1 |
| δ Equ..... | 5.2, 5.7 | F5 | 5.70 | .39 | 0.27 | 4.5 | 2.8 | | 4.1, 4.6 |
| α CMi..... | 0.5, 1.3 | F5 | 39.0 | .32 | 4.05 | 13.0 | 1.5 | 1.1, .4 | 3.0, 15.5 |
| α CMa..... | -1.6, 8.4 | A0, F0 | 50.0 | .60 | 7.57 | 20.4 | 3.4 | 2.44, .96 | 1.3, 11.3 |
| ξ UMa..... | 4.4, 4.9 | F9, G2 | 59.8 | .41 | 2.51 | 17 | 1.4 | 0.7, .7 | 5.2, 5.7 |
| α Cen..... | 0.3, 1.7 | G0, K5 | 78.8 | .51 | 17.65 | 23.3 | 2.04 | 1.10, .94 | 4.7, 6.1 |
| ξ Boo..... | 4.8, 6.7 | G6, K4 | 152.8 | .51 | 4.83 | 29 | 1.0 | .53, .47 | 5.9, 7.8 |
| α_2 Eri..... | 9.7, 11.4 | A0, M6 | 248 | .40 | 6.80 | 34 | 0.64 | .44, .20 | 11.4, 12.9 |
| α Gem..... | 2.0, 2.8 | A0, A0 | 306 | .56 | 6.06 | 80 | 5.5 | | 1.4, 2.2 |
| η Cas..... | 3.7, 7.4 | F8, K0 | 346 | .33 | 10.1 | 55 | 1.4 | .8, .6 | 5.0, 8.7 |

TABLE 814.—Spectroscopic Binary Stars

Stars so close not yet visually double. Discovered and studied through shift of spectrum lines (Doppler effect). i is inclination of orbit to "plane of sky," m , masses of components. The percentage with periods < 10 d: 71 for O and B stars; 64, A; 52, F-G; 16, K-M; periods > 100 d, percentages are 12, 6, 18, 61. See Lick Obs. Bull. No. 355.

| Star | App. mag. | Class | Period days | Eccentricity | Orbital velocity | $A \sin i$ 10 ⁶ km | $m_1 \sin^3 i$ $m_2 \sin^3 i$ | $\frac{m_2^2 \sin^3 i}{(m_1 + m_2)^2}$ | Abs. mag. |
|----------------------------|-----------|-------|-------------|--------------|------------------|----------------------------------|----------------------------------|--|------------|
| μ Sco..... | 3.1 | B3 | 1.45 | 0.05 | 480 | 9.5 | 16.5 | ... | -2.2, -1.8 |
| β Per..... | 2.1 | B8 | 2.87 | .004 | 44 | 1.73 | ... | 0.025 | -0.7 |
| "..... | .. | .. | 688 | .13 | 10 | 93 | ... | .070 | ... |
| α Gem B..... | 2.8 | A0 | 2.93 | .01 | 32 | 1.28 | ... | .0097 | ... |
| " A..... | 2.0 | A0 | 9.22 | .50 | 13.6 | 1.49 | ... | .0015 | ... |
| α Vir..... | 1.2 | B2 | 4.01 | .10 | 126, 208 | 6.9, 4.4 | 9.6, 5.8 | ... | -2.6, -2.2 |
| + 6 ^o 1309..... | 6.4 | O8 | 14.41 | .04 | 206, 247 | 41, 49 | 76, 63 | 13.2 | ... |
| ζ U MaA..... | 2.4 | A2 | 20.54 | .54 | 69 | 16.4 | 1.66 | .41 | 1.4 |
| α Aur..... | 0.2 | G0 | 104 | .01 | 26, 32 | 37, 46 | 1.2, 0.9 | .18 | ... |
| ξ U MaA..... | 4.4 | G0 | 665 | .41 | 7.0 | 58.3 | ... | .018 | ... |
| β Cap..... | 3.2 | G0 | 1375 | .44 | 22.2 | 377 | ... | 1.13 | ... |

TABLE 815.—Spectroscopic Eclipsing Binaries

Some 200 known. Last column, distance between center of two stars = radius of relative orbit. See Shapley Contr. 3, Princeton Univ. Obs.

| Name | Max. mag. | Sp. class | Period days | e | i | Radii sun = 1 | Density sun = 1 | Masses sun = 1 | 10 ⁶ km |
|------------------|-----------|-----------|-------------|------|-----------------|------------------|--|-------------------|--------------------|
| SW Lac.. | 8.6 | G2p | 0.32 | 0.78 | 73 ^o | 0.42, 0.46* | 1.6, 1.2 | | |
| WU Ma.. | 7.9 | G0 | .33 | .85 | 76 | .78, .78 | 2.1, 1.5 | 0.69, 0.49 | 1.53 |
| S Ant.... | 6.3 | F0 | .65 | .75 | 62 | 1.7, 1.3 | .31, .38 | .75, .42 | 2.30 |
| α Gem C. | 9.0 | M | .81 | ... | 86 | .58, .58 | 2.6, 2.6 | .52, .52 | 2.58 |
| ν Pup.... | 4.1 | B1p | 1.45 | .88 | 74 | 8.4, 7.7 | .04, .06 | 19, 19 | 8.83 |
| ω Her.... | 4.6 | B3 | 2.05 | .93 | 74 | 4.6, 5.4 | .09, .02 | 7.7, 2.9 | 10.3 |
| U Cep.... | 6.9 | A0 | 2.49 | .96 | 86 | .20, .32* | .14, .03 | | |
| β Pes.... | 2.3 | B8 | 2.87 | .99 | 82 | .21, .24* | .13, .03 | | 1.76† |
| TX Cas.. | 9.3 | B3 | 2.93 | .93 | 88 | .57, .30* | .006, .02 | | |
| β Aur.... | 2.1 | A0p | 3.96 | .99 | 77 | 2.8, 2.8 | .11, .11 | 2.4, 2.4 | 12.3 |
| RS Vul.. | 6.9 | B8 | 4.48 | .98 | 79 | 4.3, 5.6 | .06, .01 | 4.6, 1.4 | 14.5 |
| S Cnc.... | 8.2 | A0 | 9.48 | 1.0 | 85 | .10, .18* | .10, .01 | | |
| W Cru... | 8.7 | G0p | 198 | .91 | 76 | .61, .34* | (1.3 \times 10 ⁻⁶ , 3.1 \times 10 ⁻⁶) | | |
| RZ Oph.. | 9.7 | cG0 | 262 | ... | 87 | .53, .47* | .05, .15 | .001, .00003 | |

* Radii in terms of the relative orbit as unit. † Radius of relative orbit.

PERIODS OF KNOWN BINARY STARS WITHIN 10 PARSECS OF THE SUN

There is no reliable evidence (1930) for favored orientation of planes of double-star orbits. Kepler 3rd law gives (p , period in yrs.)² = (a , major axis, astr. units)³ / (M , in solar masses). There is an apparent statistical relation between eccentricity and period, viz.:

| | | | | | | | |
|--------------------|-----|-----|-----|-----|-----|-----|-----|
| Eccentricity..... | 3.0 | 3.5 | 4.0 | 4.5 | 5.0 | 5.5 | 6.0 |
| Period (logs)..... | .62 | .66 | .71 | .76 | .80 | .83 | .85 |

Using the mass-luminosity law (see p. 631) Luyten obtains: Log period in yrs. = 1.460 log d - 0.48 log (M , in solar air-masses) + 0.168 ± 0.35 where d is observed distance between stars at right angle to line of sight in astronomical units.

From the data of the following groups the median-mean log of the periods (median-geometrical mean of actual periods) is probably about 2.5 (a little more than 300 yrs.). Half of the binaries in space may be expected to have periods between the limits of 20 and 4000 yrs.

| Star | d | Paral- lax π | Mass sun = 1 | Log period | Period years | Star | d | Paral- lax π | Mass sun = 1 | Log period | Period years |
|---------------------------------|---|------------------------|-----------------------------------|------------------------------------|----------------------------|-----------------------|-------------------------|------------------------|--------------------|---------------|-----------------|
| β 733..... | 0.72 | 0.100 | 1.0 | 1.43 | 26.7 | α Cen AB.. | 7.02 | 0.757 | 2.04 | 1.90 | 80.1 |
| ζ Her (Σ 2084)... | 1.2 | .112 | 2.1 | 1.54 | 34.5 | 70 Oph.... | 6.56 | .194 | 1.7 | 1.94 | 87.7 |
| α CMi..... | 3 \pm | .307 | 1.6 | 1.60 | 40.2 | Brsb 13.... | 3.60 | .140 | .8 | 2.11 | 130.? |
| Mlb 4 AB..... | 1.26 | .140 | 1.1 | 1.62 | 42.2 | ξ Boo..... | 3.01 | .173 | 1.0 | 2.18 | 151 |
| μ Her BC..... | .74 | .107 | .90 | 1.63 | 43.0 | Δ 5 (p Eri) | 9.22 | .165 | 2.32 | 2.34 | 219 |
| Krü 60 AB..... | 1.36 | .258 | .45 | 1.65 | 44.3 | σ_2 Eri Bc.... | 4.52 | .200 | .64 | 2.39 | 248 |
| α CMa AB..... | 10.6 | .366 | 3.4 | 1.70 | 50.0 | η Cas..... | 8.14 | .180 | 1.4 | 2.71 | 508 |
| ξ UMa AB-CD.. | 1.61 | .145 | 1.4 | 1.78 | 59.9 | | | | | | |
| Spectroscopic binaries | δ Tri ξ UMa CD χ Drac | | log p : -1.57 -1.56 -0.11 | p : 0.0272 .027 \pm .769 | η Boo ξ UMa AB | | log p : +0.13 0.26 | p : 1.36 1.82 | | | |

| Star | d | Paral- lax π | d Astro- nomical units | Abs. magnitudes | Mass sun = 1 | Log period | Period years |
|------------------------------|-------|------------------------|-----------------------------------|-------------------------|--------------------|---------------|-----------------|
| Lac 353 CD..... | 1.2 | .11? | 11 \pm | 7.8, 8.8..... | 1.03 | 1.58 | 38 |
| Brs 5 (P 342y?)..... | 1.57 | .100 | 15.7 | 8.0, 8.0..... | 1.00 | 1.91 | 82 |
| Sh 243 AB..... | 4.3 | .174 | 24.8 | 6.5, 6.5..... | 1.36 | 2.14 | 138 |
| Millb 377..... | 2.3 | .115 | 20 | 10, 13..... | .51 | 2.31 | 204 |
| K Tuc AB (h3423)..... | 5.1 | .11? | 46 \pm | 5.2, 7.4..... | 1.50 | 2.51 | 324 |
| h 5173..... | 9 | .243 | 37 | 7.2, 13.2..... | .78 | 2.51 | 324 |
| Hu 1128..... | 5.0 | .104 | 48 | 5.6, 14..... | .99 | 2.62 | 417 |
| O Σ 547 AB..... | 4.8 | .100 | 48 | 9.3, 9.4..... | .77 | 2.68 | 480 |
| Σ 2398..... | 16 | .294 | 54.4 | 11.1, 11.7..... | .55 | 2.83 | 680 |
| Σ 1280..... | 5.2 | .100 | 52 | 8.7, 9.1..... | .86 | 2.70 | 500 |
| 61 Cyg (Σ 2758)..... | 21 | .300 | 70 | 8.0, 8.7..... | .95 | 2.87 | 740 |
| Sh 190..... | 14.2 | .181 | 78.8 | 7.1, 10.2..... | .94 | 2.95 | 890 |
| O Σ 539 AC..... | 7.8 | .095 | 87 | 7.3, 9.7..... | .95 | 3.01 | 1020 |
| Σ 1321..... | 19.4 | .163 | 119 | 9.1, 9.1..... | .84 | 3.24 | 1740 |
| Bo 187..... | 39 | .281 | 139 | 10.4, 13.0..... | .51 | 3.44 | 2700 |
| Mlb 4 AB-C..... | 31 | .144 | 215 | 11.1, + mass 1.1..... | 1.40 | 3.51 | 3200 |
| μ Her A-BC..... | 32 | .105 | 305 | 3.7, + mass 0.9..... | 2.20 | 3.64 | 4400 |
| O $_2$ Eri A-BC..... | 83 | .200 | 415 | 6.0, + mass 0.64..... | 1.38 | 3.92 | 8300 |
| γ Lep (HV 50)..... | 95 | .149 | 639 | 4.7, 7.3..... | 1.58 | 4.17 | 15000 |
| Chri 2448..... | 63.7 | .095 | 670 | 8.8, 10.5..... | .76 | 4.35 | 22000 |
| Lpz II 961..... | 150 | .142 | 1060 | 6.6, 12.2..... | .91 | 4.60 | 40000 |
| K Tuc-Lac 353 AB-CD.. | 319.4 | .11? | 2875 \pm | 5.2, 7.4, 7.8, 8.8..... | 2.53 | 5.02 | 105000 |
| ζ Ret..... | 310 | .1? | 3100 \pm | 5.2, 5.5..... | 1.8 | 5.13 | 135000 |
| O Σ 547 AB-C..... | 330 | .100 | 3300 | 9.3, 9.4, 10.2..... | 1.11 | 5.28 | 190000 |
| 36 Oph-30 Sco AB-C.... | 730 | .174 | 4200 | 6.5, 6.5, 7.8..... | 1.89 | 5.32 | 210000 |
| W-Ott 5811..... | 512 | .160 | 3210 | 10.2, 12.4..... | .56 | 5.41 | 260000 |
| α Cen AB-C..... | 6740 | .760 | 8860 | 15.5, + mass 2.04..... | 2.20 | 5.77 | 590000 |

Luyten, W. J. (Harvard College Obs., Proc. Nat. Acad. Sci., 10, 252, 257, 1930.

TABLE 817.—Masses and Absolute Magnitudes of Binary Stars

(Pitman, Astron. Journ. 39, 57, 1929.)

This paper contains a discussion of the orbits of 104 binary stars and of the relationship between stellar masses and luminosities (Eddington, M. N., March, 1924). In the following table of averages the magnitudes are visual. Values in blacker type are averages of greater weight. Six planetary nebulae give an average mass of 16.7, absolute magnitude 8.1.

| | Visual binaries | | | | Eclipsing binaries | | | | Spectroscopic binaries | | | |
|-------|-----------------|-------|-------|-------|--------------------|-------|-------|-------|------------------------|------|---------|-------|
| | Trig. | | Spec. | | Trig. | | Spec. | | Trig. | | Spec. | |
| | Mass | Mag. | Mass | Mag. | Mass | Mag. | Mass | Mag. | M. Mass | Mag. | M. Mass | Mag. |
| O-Bo | ... | ... | ... | ... | ... | ... | 70.1 | -4.26 | 17.4 | 2.39 | 85.0 | -4.36 |
| B1-B3 | ... | ... | ... | ... | ... | ... | 35.0 | -2.68 | 8.7 | 3.96 | 42.5 | -3.55 |
| B1-B3 | ... | ... | 12.9 | -1.14 | 20.87 | -0.24 | 15.24 | -1.54 | 15.5 | .64 | 9.91 | -1.73 |
| B1-B3 | ... | ... | 6.45 | -.27 | 10.44 | -.60 | 7.62 | -.81 | 7.75 | 1.29 | 5.22 | -.84 |
| B4-B8 | ... | ... | ... | ... | 7.87 | -.74 | 7.18 | -.04 | 1.58 | 2.72 | 11.21 | -.80 |
| B4-B8 | ... | ... | ... | ... | 3.94 | 1.26 | 3.59 | 1.04 | .79 | 3.50 | 5.37 | .25 |
| B9-A1 | 2.65 | 2.80 | 2.69 | 2.23 | 4.71 | -1.47 | 4.61 | .51 | 1.88 | .61 | 2.60 | .56 |
| B9-A1 | 1.52 | 3.25 | 1.51 | 2.94 | 2.37 | -.72 | 2.36 | 1.52 | .94 | 1.66 | 1.30 | 1.92 |
| A2-A6 | 6.76 | 1.54 | 5.47 | 1.16 | ... | ... | 4.29 | 1.30 | 3.20 | .12 | 2.52 | 1.42 |
| A2-A6 | 3.15 | 2.41 | 2.74 | 2.07 | ... | ... | 2.15 | 2.23 | 1.60 | 1.18 | 1.26 | 2.43 |
| A7-F2 | 3.57 | 2.25 | 5.17 | 1.88 | ... | ... | 1.17 | .53 | 2.95 | 3.89 | 1.73 | 1.26 |
| A7-F2 | 1.59 | 4.15 | 2.41 | 3.32 | ... | ... | .58 | 1.30 | 1.48 | 4.57 | .86 | 2.00 |
| F3-F7 | 2.44 | 3.26 | 2.12 | 3.15 | 2.90 | 4.82 | 2.76 | 2.21 | 2.02 | 2.67 | 2.56 | 2.23 |
| F3-F7 | 1.31 | 4.50 | 1.34 | 4.54 | 1.45 | 5.58 | 1.59 | 2.83 | 1.01 | 3.64 | 1.28 | 3.02 |
| Go-G2 | 2.11 | 3.76 | 2.22 | 3.70 | 1.26 | 5.60 | 1.26 | 5.13 | 2.01 | 4.34 | 2.12 | 2.37 |
| Go-G2 | 1.06 | 4.94 | 1.13 | 4.75 | .63 | 5.83 | 1.08 | 5.09 | 1.00 | 5.16 | 1.06 | 3.18 |
| G3-G9 | 4.75 | 4.91 | 2.71 | 4.92 | ... | ... | ... | ... | 1.38 | 4.82 | 1.38 | 4.50 |
| G3-G9 | 2.28 | 6.11 | 1.35 | 5.84 | ... | ... | ... | ... | .69 | 5.61 | .69 | 5.41 |
| K | 1.54 | 6.21 | 4.39 | 5.38 | ... | ... | ... | ... | ... | ... | ... | ... |
| K | .78 | 7.43 | 2.01 | 6.38 | ... | ... | 1.74 | 3.94 | ... | ... | ... | ... |
| M | .64 | 10.43 | 1.16 | 9.97 | 1.20 | 8.32 | 1.20 | 8.20 | ... | ... | ... | ... |
| M | .31 | 11.40 | .51 | 11.02 | .60 | 9.02 | .60 | 8.90 | ... | ... | ... | ... |

TABLE 818.—Mass-Luminosity Curve

(Prepared by Doctor Shapley, 1931.)

Masses are stated as logarithms of masses in terms of the sun's mass; the magnitudes absolute bolometric.

| Log mass | Abs. mag. | Log mass | Abs. mag. | Log mass | Abs. mag. |
|----------|-----------|----------|-----------|----------|-----------|
| 1.6 | -5.5: | 1.0 | -2.92 | 0.0 | + 4.41 |
| 1.4 | -4.6: | .8 | -1.97 | -0.2 | + 6.22 |
| 1.2 | -3.84 | .6 | -.74 | -0.4 | + 8.19 |
| ... | ... | .4 | +.72 | -0.6 | +10.20 |
| ... | ... | .2 | +2.57 | -0.8 | +12.29 |

Notes added in press.—(Aitken, M. N., 92, 596, 1932.) At least one star in every 18 to 9th mag. is a close visual double; 1 in 4 or 3, a spectroscopic binary; 1495 of latter known, surely physical doubles. Orbits known for 120 pairs.

| Spectrum | B | A | F | G | K | M | B | A | F | G | K | M | sun |
|----------------|---------------|------|------|-----|------|-----|-------------|-----|-----|-----|-----|-----|-----|
| % distribution | 1.7 | 21.4 | 15.3 | 33. | 15.6 | 1.4 | masses 10.6 | 5.2 | 2.6 | 2.4 | 2.2 | 0.6 | 1.0 |
| | Spectroscopic | | | | | | Visual | | | | | | |

| Periods | 2.7d | 7.6 | 14.1 | 30.6 | 102.5 | 3.2y | 16.8y | 37.1 | 73. | 138 | 274 | 2000 | 5000 |
|---------|------|-----|------|------|-------|------|-------|------|-----|-----|-----|------|------|
| e | .05 | .16 | .22 | .35 | .30 | .31 | .43 | .40 | .53 | .57 | .62 | .61 | .76 |

TABLE 819.—Stellar Radiation Measurements (Pettit, Nicholson, 1928)

Radiometric magnitude = apparent magnitude of an Ao star which will give same radiometric deflection. Heat index = visual - radiometric magnitudes. Heat index - color index = zero for Ao star. Water-cell-absorption is fraction of radiation eliminated by water-cell expressed in magnitudes.

Giants, F5-Mo, have greater heat indices than dwarfs of same classes. Red stars deviate from black-body conditions. The radiation received at earth's surface at Mount Wilson from star in zenith of zero radiometric magnitude, 17.1×10^{-12} cal./cm²/min. Radiometric magnitude Hefner lamp at 1 meter is -20.00; International candle is 1.11 Hefner unit = -20.11; its heat index is 5.82 mag. (1900°K.).

(All measures reduced to zenith at Mount Wilson, 2 reflections from fresh silver in telescope; rock-salt window over thermocouple.)

TABLE 820.—Spectrum Classes and Temperatures

| Spectral type | Observed | | Temperature | | | | |
|---------------|------------|-----------------------|-----------------------|-----------------------|-----------------------|--------------|-------------|
| | Heat index | Water-cell absorption | Heat index | | Water-cell absorption | Color index* | Ionization† |
| | | | λ 0.555 μ | λ 0.529 μ | | | |
| | Mag. | Mag. | | | | | |
| Bo..... | 0.05 | 0.20 | | | | 23000° | 20000 |
| B5..... | .01 | .23 | | | | 15000 | 15000 |
| Ao..... | .00 | .26 | | | | 11200 | 10000 |
| A5..... | .02 | .30 | | | 7500° | 8600 | 8400 |
| Fo..... | .15 | .36 | 6750° | 7300° | 6200 | 7400 | 7500 |
| F5..... | .30 | .41 | 5760 | 6160 | 5450 | 6500 | 7000 |
| gGo..... | .47 | .50 | 5000 | 5450 | 4700 | 5500 | 5600 |
| gG5..... | .65 | .60 | 4550 | 4870 | 4140 | 4700 | 5000 |
| gKo..... | .90 | .70 | 4020 | 4300 | 3750 | 4100 | 4000 |
| gK5..... | 1.57 | .93 | 3240 | 3480 | 3130 | 3300 | 3000 |
| gMo..... | 1.86 | 1.01 | 3030 | 3250 | 2980 | 3050 | 3000 |
| gM2..... | 2.2 | 1.14 | 2810 | 3000 | 2810 | | |
| gM4..... | 3.1 | 1.30 | 2400 | 2590 | 2550 | | |
| gM6..... | 4.2 | 1.46 | 2050 | 2200 | 2390 | | |
| gM8..... | 5.2 | 1.62 | 1780 | 2000 | 2250 | | |
| Me Max..... | 4.4 | 1.5 | 1990 | 2160 | 2350 | | |
| Me Min..... | 8.9 | 2.2 | | | 1830 | | |
| dGo..... | .32 | .42 | 5700 | 6100 | 5350 | 6000 | |
| dG5..... | .39 | .47 | 5350 | 5750 | 4920 | 5600 | |
| dKo..... | .55 | .54 | 4820 | 5100 | 4460 | 5100 | |
| dK5..... | 1.10 | .76 | 3720 | 3980 | 3550 | 4400 | |
| dMo..... | 1.40 | .87 | 3400 | 3650 | 3260 | 3400 | |
| dM2..... | 2.1 | 1.14 | 2870 | 3060 | 2780 | | |

* Russell, Dugan, and Stewart, *Astronomy*, 2, 734, 1927. † Payne, *Stellar atmospheres*, 1925.

NOTE—Hottest known stars 20,000 to 30,000 °K, O type, abs. mag. -4, masses 10-80 suns, (Plaskett).

TABLE 821.—Visual and Radiometric Magnitudes and Total Radiations

| Brightest stars— Visual magnitude | | | | Brightest stars— Radiometric magnitude | | | | Brightest stars— Total radiation reaching the solar system | |
|--------------------------------------|------|--------------|--------------|---|------|--------------|--------------|---|---|
| Star | Type | Vis. mag. | Rad. mag. | Star | Type | Rad. mag. | Vis. mag. | Star | Cal. cm ⁻² min ⁻¹ $\times 10^{12}$ |
| Sirius..... | A2s | -1.58 | -1.27 | Betelgeuse.. | M2 | -1.67 | +0.92 | Sirius..... | 145 |
| Canopus... | F3 | -.86 | -1.09 | Antares.... | M1 | -1.32 | +1.22 | Betelgeuse.. | 132 |
| α Centauri. | G6 | +.33 | -.08 | Sirius..... | A2s | -1.27 | -1.58 | Antares.... | 96 |
| | K4 | +1.70 | +.70 | Canopus... | F3 | -1.09 | -.86 | β Centauri. | 83 |
| Vega..... | A1s | +.14 | +.10 | γ Crucis.... | M3 | -1.0 | +1.61 | Canopus... | 77 |
| Capella.... | Go | +.21 | -.38 | Arcturus... | Ko | -.98 | +.24 | γ Crucis.... | 69 |
| Arcturus... | Ko | +.24 | -.98 | Aldebaran.. | K5 | -.60 | +1.06 | Arcturus... | 64 |
| Rigel..... | B8p | +.34 | +.23 | Capella.... | Go | -.38 | +.21 | Achernar.. | 51 |
| Procyon... | F3 | +.48 | +.22 | σ Ceti max.. | M6e | -.2 | +3.6 | Rigel..... | 50 |
| Achernar.. | B5 | +.60 | +.60 | α Centauri.. | G6 | -.08 | +.33 | Spica 33... | 48 |
| β Centauri. | B1 | +.86 | +.81 | | K4 | +.70 | +1.70 | | |

STELLAR RADIATION MEASUREMENTS

TABLE 822.—Energy Spectra of the Stars (Abbot, 1929)

Measures made with radiometer at the Coudé focus of the Mt. Wilson 100-inch reflecting telescope (arbitrary units). *Astrophys. Journ.*, 69, 293, 1929.

Stellar energy spectrum distribution; normal scale, outside the atmosphere.

| Object | Date | Place in wave lengths, microns | | | | | | | | |
|-------------------------|-----------------|--------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | 0.437 | 0.472 | 0.520 | 0.580 | 0.700 | 0.905 | 1.316 | 1.751 | 2.224 |
| β Orionis* | 13 [†] | 990 | 1140 | 584 | 233 | 89 | 21 | ... | ... | ... |
| α Lyrae..... | 26 | 1355 | 446 | 334 | 644 | 287 | 91 | 77 | 29 | ... |
| | 13 | 990 | 642 | 367 | 377 | 267 | 105 | 17 | ... | ... |
| α Cygni..... | 25 | ... | 502 | 434 | 455 | 277 | 121 | 86 | ... | ... |
| | 13 | ... | 363 | 267 | 266 | 297 | 206 | 172 | ... | ... |
| α Aquilae..... | 26 | 616 | 474 | 267 | 355 | 247 | 121 | 17 | ... | ... |
| α Canis Min..... | 13 | ... | 139 | 167 | 277 | 436 | 149 | 17 | ... | ... |
| α Persei..... | 26 | ... | ... | 234 | 189 | 267 | 231 | 159 | 43 | ... |
| | 13 | ... | ... | 184 | 244 | 228 | 177 | 73 | 38 | ... |
| γ Cygni..... | 13 | ... | 390 | 434 | 244 | 208 | 149 | 125 | 60 | 8 |
| α Aurigae..... | 25 | ... | 28 | 284 | 388 | 455 | 369 | 202 | 119 | 37 |
| Mars..... | 13 | ... | ... | 317 | 366 | 337 | 256 | 206 | 41 | ... |
| Jupiter..... | 26 | ... | ... | 134 | 178 | 238 | 241 | 95 | 6 | ... |
| β Ceti..... | 25 | ... | ... | ... | 155 | 297 | 263 | ... | 35 | ... |
| | 26 | ... | ... | ... | 166 | 198 | 298 | 116 | 43 | ... |
| γ Aquilae..... | 26 | ... | ... | ... | 33 | 109 | 199 | 168 | 93 | 10 |
| α Boötis..... | 25 | ... | ... | ... | 200 | 228 | 376 | 404 | 183 | 56 |
| α Tauri..... | 25 | ... | ... | ... | 255 | 238 | 461 | 456 | 345 | 124 |
| α Orionis..... | 25 | ... | ... | ... | 311 | 485 | 844 | 1010 | 597 | 172 |
| β Andromedae..... | 25 | ... | ... | ... | 189 | 228 | 312 | 189 | 104 | 65 |
| | 26 | ... | ... | ... | 155 | 257 | 177 | 202 | 104 | 29 |
| β Pegasi..... | 25 | ... | ... | ... | 89 | 218 | 241 | 176 | 145 | 80 |
| δ Sagittae..... | 25 | ... | ... | ... | 111 | 99 | 312 | 120 | 171 | 32 |
| | 26 | ... | ... | ... | 144 | 168 | 170 | 150 | 128 | 12 |
| α Herculis..... | 25 | ... | ... | ... | 233 | 406 | 369 | 417 | 348 | 83 |
| | 26 | ... | ... | ... | 166 | 257 | 334 | 387 | 342 | 163 |
| \circ Ceti..... | 25 | ... | ... | ... | 166 | 287 | 220 | 331 | 299 | 107 |
| | 26 | ... | ... | ... | 67 | 337 | 319 | 396 | 194 | 61 |
| | 13 | ... | ... | ... | 144 | 188 | 192 | 185 | 116 | 26 |

* Additional observations for β Orionis: 0.423 μ , 505; 0.454 μ , 738; 0.404 μ , 827.

[†] The dates refer to August 25, 26, and September 13, 1928, respectively.

TABLE 823.—Stellar Temperatures, Radiation, and Diameters

| Star | Absolute temperature °K | N^* Unit = 10^{-11} | Parallax | Sun's diameter = 1 [†] | | |
|------------------------|----------------------------|----------------------------|--------------|---------------------------------|----------------|---------|
| | | | | Radiometer | Interferometer | Russell |
| Sun..... | 6,000° | ... | ... | ... | ... | ... |
| β Orionis..... | 16,000 | 3.20 | 0".007 | 20 | ... | 28 |
| α Lyrae..... | 14,000 | 6.10 | .130 | 2 | ... | 3 |
| α Can. Maj..... | 11,000 | 6.60 | .370 | 1.2 | 2 | ... |
| α Can. Min..... | 8,000 | 1.24 | .315 | 1.1 | ... | 1.6 |
| α Aurigae..... | 5,800 | 2.20 | .071 | 13 | ... | 9 |
| α Tauri..... | 3,000 | 2.54 | .053 | 70 | 39 | ... |
| β Pegasi..... | 2,850 | 1.10 | .026 | 94 | 82 | ... |
| β Orionis..... | 2,600 | 7.90 | .017 | 510 | 280 | ... |
| α Herculis..... | 2,500 | 3.60 | .007 .013 | 900 480 | ... | 230 |

* Ratio of stellar to solar radiation outside earth's atmosphere.

[†] To express in kilometers, multiply by 1.42×10^6 ; to express in miles, multiply by 0.865×10^6 .

TABLE 824

VARIABLE STARS—GENERAL CHARACTERISTICS

(See Russell, Dugan, and Stewart, *Astronomy*, 1927; Ludendorff, Stratton, *Das Sternsystem*, Handb. Astrophys., 6, Berlin, 1928; Payne, *Stars of high luminosity*, Chap. 14, 1930.)

Perhaps 5% of all stars are variable; number known, over 5000. *Astronomische Gesellschaft* acts as central bureau; when a variable star is confirmed it there receives a definite designation, e.g., R. T. Persei. Most recent list *Astron. Nachr.*, 244, 82, 1931, contains 873 additional thus named variables. The Harvard College Observatory (Doctor Shapley, Cambridge, Mass.) keeps a record of variable-star data. A yearly list of stars with known periods is published by the Berlin-Babelsberg Observatory. Note added in press: 5826 in 1933 volume.

CLASSIFICATION

I. Periodic Variables.

- (1) Eclipsing variables: Generally B and A stars. Not true variables. See Table 815.
- (2) Short period: 100 to 10,000 sun's luminosity, large mass. Types B to M. Preferably F and G.
 - (a) Period range about $\frac{1}{2}$ day; about 10% of variables of regular period. Generally called *cluster variables*; quick rise in light, slow decline, visual range generally less than 1.5 mag.; photographic range averages 50% greater; $\frac{1}{2}$ day generally of class A; peculiar velocities average 70 km/sec.; variable radial velocity range small, proportional to range in mag. Max. of approach invariably near max. mag., max. of recession near min. mag. Galactic concentration small. Shortest period known (1932), 0.69746 days, 15 mag., range 1 mag. ($8^h 19^m 38^s$ R. A., $18^\circ 45'$ S. dec. van Gent).
 - (b) Periods 1 to 32+ days; 15% of regular variables. *Cepheids*. Much like (2a) but periods 4 d, class F5; 8 d, G0; 20 d, G5. Peculiar velocities average about 12 km/sec. Galactic concentration strong. About 120 known. Long-period Cepheids are among the brightest stars known, 20,000 times brightness of sun. The following table 825 is due to Shapley, 1931.
- (3) Long-period variables: Nearly all red stars 87% class M, 6% class N, 5% class S, a few G and K. α Ceti typical. Abs. mag. -2.0 (Oort, 1927); periods 100 to 150 d, $M = -2.3$; 250 to 340, $M = -1.1$; > 340 , $+0.3$ (Gerasimović, 1928). Periods often irregular, proper motions small ($0.03'' \pm$), radial velocities large (mean 35 km/sec.). For S Librae, 385 km/sec. Heat radiation diminishes by 1 or 2 mag. while light by 5 or so.

II. Irregular variables.

- (1) R V Tauri: Resembles Cepheids somewhat irregularly. 12 known (Gerasimović, 1929). 19 given by Ludendorff (1928).
- (2) R Coronae Borealis: About 11 known. Typical R. Cor. Bor. remains often for years of 6th mag.; then may rapidly drop 6 mag. for indefinite period then returns to original mag. Ludendorff gives 11.
- (3) U Geminorum (type): Normally faint but brighten up at irregular intervals to drop back to original magnitude. Some analogy to Novae. Ludendorff gives 20.
- (4) T Pyxidis: Resemble Novae. Ludendorff gives 5.

TABLE 825.—The Cepheid Period-Luminosity Curve

| Logarithm of period. | Mean spectrum.* | Absolute photographic magnitude.** | Absolute bolometric magnitude. |
|----------------------|-----------------|------------------------------------|--------------------------------|
| 0.0 | F 2.5 | — 0.31 | — 0.82 |
| 0.2 | F 5.5 | — 0.61 | — 1.25 |
| 0.4 | F 7.5 | — 0.93 | — 1.67 |
| 0.6 | G 0 | — 1.22 | — 2.16 |
| 0.8 | G 2 | — 1.53 | — 2.65 |
| 1.0 | G 4 | — 1.89 | — 3.15 |
| 1.2 | G 6 | — 2.26 | — 3.71 |
| 1.4 | G 8 | — 2.68 | — 4.34 |
| 1.6 | K 0.5 | — 3.19 | — 5.13 |
| 1.8 | K 2.5 | — 3.81 | — 6.11 |
| 2.0 | M 0 | — 4.60 | — 8.2: |

* Shapley, Harvard Bull., 861, 1928.

** Shapley, Harvard Monogr., 2, 1930.

TABLE 826.—Novae

Novae (temporary stars): Between 10 to 20 brighter than the 9th app. mag. occur in a year (Bailey). Numerous in spiral nebulae. More than 80 in Andromeda nebula (Hubble); 30 per year estimated. Mean parallax of five, 0.01"; abs. mag. + 8.5 to — 3.1 (Russell). Nova Aquilae, 1918, class A before outbreak; then appears as rapidly expanding gas 1700 to 2300 km/sec.; fades to Wolf-Rayet, class O (T Coronae Bor. changed finally to gM); gaseous envelope visible 1918 to 1926, reached diameter 16"; abs. mag. + 3 to — 8.8; distant 1200 light years. Nova Persei: Diffuse cloud faint light expanding 6' to 7' in 7 months. Six weeks later moved 35" to 65"—apparently due to illumination of dark nebulous matter near star by outgoing light (Russell). See Milne, Nature, 128, 715, 1931. If after outburst it has dwindled to previous magnitude but spectrum shows a higher temperature, then radius must have decreased, say 10-fold, and the density would be much greater (compare white dwarfs, Table 828).

TABLE 827.—Observed Maxima of Spectrum Lines in the Giant Sequence

(Shapley.)

| Line. | Atom | Ionization potential volts. | Excitation potential volts. | Maximum. | No. of effective atoms at max. per cm ² surface | Source. |
|-------|------|-----------------------------|-----------------------------|------------------|--|-----------------|
| 4340 | H | 13.54 | 10.15 | A ₀ | 4.2×10^{19} | Contour of line |
| | | | | F ₅ * | 1.9×10^{18} | Contour of line |
| 4026 | He | 24.41 | 20.81 | B _{1.5} | 1.6×10^{17} | Estimate |
| 4481 | Mg + | 14.97 | 8.83 | A ₃ | | Estimate |
| 3033 | Ca + | 11.82 | 0.0 | K ₂ | 2.4×10^{19} | Contour of line |
| | | | | G ₅ * | 2.4×10^{19} | Contour of line |
| 4444 | Ti + | 13.6 | 1.16 | F ₅ | 1.3×10^{17} | Line depth |
| 4416 | Fe + | 16.5 | 2.82 | F ₅ | 1.7×10^{17} | Line depth |
| 4215 | Sr + | 10.98 | 0.0 | K ₂ | 6.9×10^{17} | Line depth |
| 4554 | Ba + | 9.96 | 0.0 | Mo? | | Estimate |

* Data for the supergiant sequence.

TABLE 828.—High-Density Stars. White Dwarfs

| | Class | Visual abs. mag. | Density | Radius sun = 1 | Mass |
|---------------------------|-------|---------------------|----------------------------------|-------------------|-------|
| Sirius B | F | 11.3 | $0.5 \times 10^5 \text{ g/cm}^3$ | .034 | |
| α_2 Eridani B..... | A0 | 11.2 | 1.0×10^5 " | .019 | |
| Procyon B | .. | 16. | | ... | |
| Van Maanen's * | F | 14.3 | 4×10^5 | .007 | |

* Smallest star known, about the size of the earth.

TABLE 829.—Low-Density Stars. Giants

| | Class | Visual abs. mag. | Density | Radius sun = 1 | Mass sun = 1 |
|-------------------------|-------|---------------------|--------------------|-------------------|-----------------|
| α Scorpii A..... | cM0 | — 4.0 | 3×10^{-7} | 480 | (30) |
| α Orionis | cM0 | — 2.9 | 6×10^{-7} | 290 | (15) |
| β Pegasi | gM5 | — 1.4 | 2×10^{-6} | 170 | (9) |
| α Tauri | gK5 | — 0.1 | 2×10^{-5} | 60 | (4) |

(Taken by permission from Russell, Dugan, and Stewart, *Astronomy*, Ginn & Co., 1927.)

TABLE 830.—High-Temperature Stars. High-Luminosity Stars

(Plaskett, M. N. 90, 616, 1930. Payne, *Stars of high luminosity*, 1930. Pearce, *Pub. Dom. Astron. Obs.*, 3, 302, 1926.)

Draper Catalogue, 0.1% O; 0.3% B0 to B2; 1% B3-B5. Stars of highest temperature, greatest mass, highest luminosity, greatest distance from sun. Masses 5, O type, $43 \times \text{sun's}$; 10, B0 to B2, $15 \times \text{sun's}$; 12, B3, B5, $6 \times \text{sun's}$.

| Type. | Temp. | Surface brightness. | $M_v - M_b$ | M_v | Density. |
|-------|------------|------------------------|-------------|--------|----------|
| O5 | 35,000° K. | — 4.15 M | 3.61 M | ... | ... |
| O6 | 33,000 | — 4.10 | 3.41 | ... | ... |
| O7 | 31,000 | — 4.03 | 3.20 | ... | ... |
| | | | | — 3.84 | .049 |
| O8 | 29,000 | — 3.96 | 2.98 | ... | ... |
| O9 | 27,000 | — 3.88 | 2.76 | ... | ... |
| B0 | 25,000 | — 3.78 | 2.52 | — 3.16 | ... |
| B1 | 22,000 | — 3.61 | 2.13 | — 2.72 | .056 |
| B2 | 19,000 | — 3.38 | 1.73 | — 2.59 | ... |
| B3 | 16,000 | — 3.08 | 1.28 | — 1.44 | .071 |
| B5 | 14,000 | — 2.80 | 0.98 | — 1.86 | ... |

NOTE.—See Russell, *The Constitution of the Stars*, Science, 77, 65, 1933.

TABLE 831.—Properties and Classification of Star Clusters

Star clusters fall into two distinctly different types:

Globular: Typical, Messier 13; open, Messier 4; elongated, Messier 19. Have strong central condensations, rich in faint stars. Scattered widely in latitude, restricted in longitude. Many variables—nearly 900 in 45 clusters. Radial velocities > 100 km/sec. All distant $> 10,000$, $\frac{1}{2} > 100,000$ light-years. Very few new ones found—about 103 known. Very definitely part of galaxy. Although concentrated towards its plane, only 2 within 4° of it (cloud obstruction probably). Diameters about 35 parsecs. Many stars, tens and hundreds of thousands. Many giants and supergiants. Max. luminosity about -2.5 .

Galactic: Very varied: rich, M 11; irregular, M 35; nebulous, Pleiades, M 16; accidental, M 103. Almost exclusively in Milky Way, all longitudes; apparently no variables. Radial velocities rarely > 40 km/sec., generally less. Almost all $< 4,000$ light-years distant. Almost exclusively in galactic region devoid of globulars. Tens and hundreds, rarely thousands of stars. Hyades type, yellow stars as dominant as A type. Pleiades type, almost all B's and A's, on Russell's main branch.

TABLE 832.—Distribution of Open Star Clusters

(Trumpler, Bull. Lick Obs., no. 420, 1930. Contains classification in diameters, distances, and distribution of 334 open clusters.)

The plane of symmetry of open clusters is inclined 23° to the adopted galactic plane. Its pole lies at R. A. $12^h 50^m$, Dec. $27^\circ 7'$ (1900). Forms much flattened disklike system 1000 parsecs thick, diameter 10,000 parsecs.

| In galactic latitude. | | | | In plane \perp to plane of concentration. | |
|----------------------------|-------------------------------------|-------------------------------------|--------|---|--|
| Lat. | Long. 90° - 270° . | Long. 270° - 90° . | Total. | Mean distance parsecs. | No. per layer 100 parsecs thick. |
| -90° to -30° | 0 | 1 | 1 | -850 | 2 |
| -30 -20 | 3 | 0 | 3 | -750 | 0 |
| -20 -15 | 5 | 0 | 5 | -650 | 1 |
| -15 -10 | 8 | 4 | 12 | -550 | 2 |
| -10 -8 | 4 | 2 | 6 | -450 | 1 |
| -8 -6 | 3 | 8 | 11 | -350 | 5 |
| -6 -4 | 12 | 16 | 28 | -250 | 10 |
| -4 -2 | 19 | 38 | 57 | -150 | 38 |
| -2 0 | 34 | 28 | 62 | -50 | 113 |
| 0 $+2$ | 34 | 27 | 61 | $+50$ | 106 |
| $+2$ $+4$ | 27 | 10 | 37 | $+150$ | 29 |
| $+4$ $+6$ | 12 | 2 | 14 | $+250$ | 11 |
| $+6$ $+8$ | 9 | 5 | 14 | $+350$ | 6 |
| $+8$ $+10$ | 2 | 1 | 3 | $+450$ | 6 |
| $+10$ $+15$ | 7 | 3 | 10 | $+550$ | 1 |
| $+15$ $+20$ | 4 | 1 | 5 | $+650$ | 1 |
| $+20$ $+30$ | 1 | 1 | 2 | $+750$ | 1 |
| $+30$ $+90$ | 3 | 0 | 3 | $+750$ | 1 |
| Total | 187 | 147 | 334 | Total | 334 |

| In galactic longitude. | | | | In galactic plane. | | |
|------------------------|--------------------|---------------------------|-----|-------------------------|---------------------|--------------------------------------|
| Long. | In galactic No. | Long. | No. | Ring limits parsecs. | No. of clusters. | Density per 10^6 parsecs 2 . |
| 0° - 40° | 12 | 160° - 200° | 46 | 0-1000 | 88 | 28 |
| 40 -80 | 34 | 200 -240 | 41 | 1000-2000 | 108 | 12 |
| 80 -120 | 40 | 240 -280 | 51 | 2000-3000 | 77 | 5 |
| 120 -160 | 28 | 280 -320 | 41 | 3000-4000 | 38 (48) | 2 |
| | | 320 -360 | 41 | 4000-5000 | 16 (36) | 1 |
| | | | | > 5000 | 7 | |

TABLE 833.—Globular Star Clusters

Table contains those distant greater than 40,000 and less than 10,000 parsecs. For complete list see Shapley, Star clusters, p. 224, McGraw-Hill, 1930.

1 kiloparsec = 31×10^{15} km = 3×10^3 light-years. Proper motions:

M13, R.A. +0.0005", dec. +0.0008; M56, -0.0013, +0.0066; M2, +0.0082, +0.0026; Van Maanen, 1927

| N. G. C. | R. A. 1900 | | Dec. 1900 | ° | ' | Galactic | | Angular diam- eter ' | No. vari- ables | Distance kilo- parsecs |
|-------------------|---------------|------|--------------|----|---|------------|-----------|-------------------------------|-----------------------|------------------------------|
| | h | m | | | | Long. ° | Lat. ° | | | |
| 6397 (Δ366)..... | 17 | 32.7 | -53 | 37 | | 304.5 | -12.5 | 19.0 | 2 | 5.65 |
| 104 (47 Tuc.)... | 0 | 19.6 | -72 | 38 | | 272 | -45 | 23 | 7 | 6.8 |
| 5139 (ω Cen.).... | 13 | 20.8 | -46 | 47 | | 277 | +15 | 23 | 132 | 6.8 |
| 6656 (M22)..... | 18 | 30.3 | -24 | 0 | | 337 | -9 | 17.3 | 21 | 6.8 |
| 6121 (M4)..... | 16 | 17.5 | -26 | 17 | | 319 | +15 | 14.0 | 33 | 7.2 |
| 6752 (Δ295)..... | 19 | 2.0 | -60 | 8 | | 303 | -26.5 | 13.3 | 1 | 8.4 |
| 6809 (M55)..... | 19 | 33.7 | -31 | 10 | | 336 | -25 | 10.0 | 2 | 8.8 |
| 6541 (Δ473)..... | 18 | .8 | -43 | 44 | | 317 | -12 | 6.3 | 1 | 8.9 |
| 3201 (Δ445)..... | 10 | 13.5 | -45 | 54 | | 244 | +9 | 7.7 | 61 | 9.2 |
| 4372..... | 12 | 20.1 | -72 | 7 | | 269 | -10 | 12.0 | .. | 9.6 |
| 6205 (M13)..... | 16 | 38.1 | +36 | 39 | | 27 | +40 | 10.0 | 7 | 10.3 |
| 6342..... | 17 | 15.3 | -19 | 29 | | 333 | +8 | .5 | .. | 40 |
| 6528..... | 17 | 58.4 | -30 | 4 | | 328.5 | -5 | .5 | .. | 44.4 |
| 6325..... | 17 | 11.9 | -23 | 38 | | 327.5 | +6 | .7 | .. | 46 |
| 6864 (M75)..... | 20 | .2 | -22 | 12 | | 347 | -27 | 1.9 | 11 | 48.5 |
| 6356..... | 17 | 17.8 | -17 | 43 | | 334 | +9 | 1.7 | .. | 50 |
| 6440..... | 17 | 43 | -20 | 20 | | 335 | +2 | .7 | .. | 50 |
| 6453..... | 17 | 44.7 | -34 | 36 | | 322.5 | -5.5 | .7 | .. | 50 |
| 6517..... | 17 | 56.4 | -8 | 57 | | 347 | +6 | .4 | .. | 50 |
| 7006..... | 20 | 56.8 | +15 | 48 | | 32 | -21 | 1.1 | 11 | 56.8 |

TABLE 834.—Galactic Star Clusters

Selected as having the best determined distances from list of 248 clusters in Shapley, Star clusters, p. 228, McGraw-Hill, 1930.

1 kiloparsec = 31×10^{15} km = 3×10^3 light-years

| N. G. C. | R. A. 1900 | | Dec. 1900 | ° | ' | Galactic | | Diameter | | No. stars | Dis- tance kilo- parsecs |
|--------------|---------------|------|--------------|----|---|------------|-----------|-----------|----------------|--------------|-----------------------------------|
| | h | m | | | | Long. ° | Lat. ° | Ang. ' | Linear kps. | | |
| 663..... | 1 | 39.2 | +60 | 44 | | 98 | -0.4 | 11 | 2.5 | 80 | 0.79 |
| 869..... | 2 | 12 | +56 | 41 | | 102.5 | -3.1 | 36 | 26.3 | .. | |
| 884..... | 2 | 15.4 | +56 | 39 | | 103 | -3.1 | 36 | 26.3 | .. | 2.51 |
| Pleiades.... | 3 | 41 | +23 | 48 | | 134.5 | -22.3 | .. | 10: | .. | .15 |
| Hyades.... | 4 | 14 | +15 | 23 | | 147 | -22.6 | .. | 10: | .. | .04 |
| 1960..... | 5 | 29.5 | +34 | 4 | | 143 | +2.4 | 12 | 4 | 60 | 1.16 |
| 2099..... | 5 | 45.8 | +32 | 31 | | 145 | +4.5 | 20 | 8.4 | 150 | 1.45 |
| 2632..... | 8 | 34.3 | +20 | 20 | | 173.5 | +34 | .. | ... | .. | .18 |
| Mel III..... | 12 | 20 | +26 | 40 | | 200 | +85.4 | .. | ... | .. | .1 |
| 6705..... | 18 | 45.7 | -6 | 23 | | 355 | -4.2 | 10 | 3.6 | 200 | 1.25 |
| 7654..... | 23 | 19.8 | +61 | 3 | | 80.5 | +5 | 12 | 4.1 | 120 | 1.17 |

(Hubble, *Astrophys. Journ.*, 64, 321, 1926; *Contr. Mt. Wilson Obs.*, no. 324.)

| | | Symbol | e. g. |
|--|----------------------------|--------|--|
| I Galactic nebulae— | A Planetary | P | N.G.C. 7662 |
| | B Diffuse | D | |
| | (1) Predominantly luminous | DL | N.G.C. 6618 |
| | (2) “ “ “ obscure | DO | Barnard 92 |
| | (3) Conspicuously mixed | DL0 | N.G.C. 7023 |
| II Extra-galactic nebulae— | A Regular | | |
| | (1) Elliptical | EN | { N.G.C. 3379 E0 “ 221 E2 “ 4611 E5 “ 2117 E7 |
| | 1 to 7 shows ellipticity | | |
| | (2) Spirals | | |
| | (a) Normal spirals | S | |
| | (1) Early | Sa | N.G.C. 4594 |
| | (2) Intermediate | Sb | “ 2841 |
| | (3) Late | Sc | “ 5457 |
| | (b) Barred spirals | SB | |
| | (1) Early | SBa | N.G.C. 2859 |
| | (2) Intermediate | SBc | “ 3351 |
| | (3) Late | SBc | “ 7479 |
| | B Irregular | Irr | N.G.C. 4449 |
| Extra-galactic nebulae too faint to be classified, “Q” | | | |

(Russell, Dugan, and Stewart, *Astronomy*, 1927; Russell, Atkinson, *Nature*, 127, 661, 1931.)

Dark nebulae: Detected by obscuration of stars.

Diffuse " Irregular of outline and shape—probably owing their detection to reflected light from nearby stars.

Planetary " Roundish, sharply defined, almost always with a central star; less than 150 known. Gerasimović (1929) gives mean distance about 790 parsecs. The largest parallax is for N.G.C. 7283 in Aquarius, 12' in diameter. Russell gives mean parallax 0.008", mean diameter 54". Nuclear star absolute mag. + 7 to + 8 (Russell, Menzel), + 5 (Gerasimović). Classes O, Oe (ordinary isolated O type stars abs. mag. -4). Proper motion, mean of 9, 0.022"; av. radial veloc. ± 37 km/sec; 6 > 100 km/sec.

Zanstra gives temperatures 30,000 to 100,000° K. for 20 of these objects; radius perhaps 1/43 our sun's; density 100,000 g/cm², possibly, 10⁶ or 10⁷ g/cm². Apparently upper end of a white dwarf sequence probably parallel to main dwarf sequence, viz.:

| | | | | | | |
|------------------------------------|----|---------|-------------------|----------------|----|----|
| Planetary nuclei... M _v | 4 | Sp. = O | Sirius B..... | M _v | 10 | A5 |
| o Ceti B..... | 6 | BSe | Van Maanen's..... | 14.5 | F | |
| o ₂ Eridani B..... | 11 | AO | Wolf 489..... | 13 | G | |

Observed velocity of rotation 1.4 to 18, av. value 5.3 km/sec. at an apparent distance of 5.7" from center. Period of rotation must be large, 4,000 to 15,000 years.

(Van Maanen, Proc. Nat. Acad. Sci., 4, 324, 1918.)

| N.G.C. | Parallax | Magnitude | | Diameter | | |
|---|----------|-----------|--------|----------|-------------|-------------|
| | | App. m | Abs. M | Angular | Astr. units | Light-years |
| 2392 | +0.022 | +10.0 | + 6.7 | 46" | 2100 | 0.03 |
| 6720 | + .008 | +14.7 | + 9.2 | 80 | 10000 | .16 |
| 6804 | + .022 | +13.4 | +10.1 | 32 | 1450 | .02 |
| 6905 | + .015 | +14.5 | +10.4 | 47 | 3100 | .05 |
| 7008 | + .016 | +12.8 | + 8.8 | 95 | 5900 | .09 |
| 7662 | + .023 | +12.9 | + 9.7 | 31 | 1350 | .02 |
| Mean abs. mag. +9.1. Mean radial velocity 29 km/sec. (Campbell, Moore, Proc. Nat. Acad. Sci., 1, 496, 1915.) (Diameter Neptune = 60 astr. units.) | | | | | | |

TABLE 837.—Diffuse Galactic Nebulae, Dimensions

(Trumpler, Proc. Astron. Soc. Pacific 43, 255, 1931.)

| | Orion neb. | Pleiades | N.G.C. 2237 | 6514 | 6523 (Mes. 8) | 6611 (Mes. 16) |
|-----------------------|---------------|----------|----------------|------|------------------|-------------------|
| Distance parsecs..... | 540 | 150 | 1340 | 980 | 1090 | 2050 |
| Diameter (")..... | 50' | 360' | 60' | 23' | 35 × 55' | 20' |
| " parsecs..... | 8 | 16 | 23 | 6.5 | 11 × 17 | 12 |

TABLE 838.—Nongalactic Nebulae

(Hubble, Astrophys. Journ., 64, 1926.)

Some 400 considered. Distribution of magnitudes appears uniform throughout sequence. For each stage in the sequence the total magnitude (M_T) is related to the max. diameter (d) by the formula: $M_T = C - 5 \log d$. When minor diameter is used, C approx. constant throughout sequence ($C = 10.1$). Mean absolute visual magnitude -15.2 . The statistical expression for distance in parsecs is $\log D = 4.04 + 0.2 M_T$. Masses appear to be of the order of $2.6 \times 10^8 \times$ our sun's. Apparently nebulae as far as measured are distributed uniformly in space, one to 10^{17} parsecs³ or 1.5×10^{-31} in C.G.S. units.

Corresponding radius of curvature of the finite universe of general relativity is of order of 2.7×10^{10} parsecs, about 600 times the distance at which normal nebulae can be detected with the Mt. Wilson 100-inch reflector.

TABLE 839.—The Magellanic Clouds and N.G.C. 6822, Dimensions

(Hubble, Astrophys. Journ., 62, 409, 1925.)

| | | Large cloud | Small cloud | N.G.C. 6822 | |
|----------------------|-------|------------------------|-----------------------|-----------------------|--------------------------------|
| Angular size: | Total | 7.2° × 7.2°* | 3.6° × 3.6° | 20' × 10' | |
| | Core | 3.6° × 1.2° | 1.8° × 0.9° | 8' × 3' | |
| App. luminosity: | Total | 1.2 | 2.0† | 9.0 | phtg. mags. |
| | Core | 1.9 | 2.7 | 9.7 | " " |
| Surface brightness: | Core | 21.0 | 21.0 | 22.1 | mag./(") ² |
| Distance | | 34,500* | 31,600† | 214,000 | parsecs |
| Linear dimensions: | Total | 4,300§ | 2,000† | 1250 × 625 | " |
| | Core | 2150 × 715 | 1100 × 500 | 500 × 190 | " |
| Volume: | Total | 4.2 × 10 ¹⁰ | 4.2 × 10 ⁹ | 3.8 × 10 ⁸ | (parsecs) ³ |
| | Core | 9.2 × 10 ⁸ | 2.3 × 10 ⁸ | 1.7 × 10 ⁷ | " |
| Absolute luminosity: | Total | -16.5§ | -15.5 | -12.7 | phtg. mag. |
| | Core | -15.8 | -14.8 | -12.0 | " " |
| Mean density: | Total | -10.0 | 8.5 | 8.8 | abs. mag./parsecs ³ |
| | Core | 6.6 | 6.1 | 6.1 | " " |

* Harvard Coll. Obs. Circ. no. 268. † loc. cit. 255. ‡ loc. cit. 260. § Harvard Coll. Obs. Bull. no. 816.

MAGNITUDES, RADIAL VELOCITIES, AND DISTANCES OF EXTERNAL GALAXIES

The following table is due to Shapley (Proc. Nat. Acad. Sci., 15, 565, 1929). The velocities (mainly Slipher data) are from Hubble (loc. cit., 15, 169, 1929); the velocities are also given corrected for the sun's motion towards the apex A, 277° , D, $+36^{\circ}$, and a velocity of 280 km/sec. (Hubble, loc. cit.), i.e., corrected for "galactic rotation". Color indices are not very reliable but the mean values for various groups serve to indicate negligible absorption of light in space. Mean difference phtg.-vis. mag., $+0.23$; Hubble's 7619, the faintest, fastest, probably most remote, shows the largest color index, $+2.8$.

| Class | N.G.C. | R. A. 1900 h m | Dec. 1900 ° ' " | Radial velocity km/sec. | v_0 km/sec. | Apparent photo- graphic magnitude mean (Harvard) | Visual mag. Holetschek corrected | Distance in mega- parsecs (Hubble) |
|------------|--------|----------------------|-----------------------|-------------------------------|------------------|---|---|---|
| Peculiar.. | 205 | 0 35 | +41 8 | - 300 | - 195 | 11.2 | 10.0 | |
| E2..... | 221 | 0 37 | +40 19 | - 185 | - 85 | 8.7 | 8.8 | 0.275 |
| Sb..... | 224 | 0 37 | +40 43 | - 220 | - 120 | 6.0 | 5.0 | .275 |
| Sc..... | 278 | 0 46 | +47 1 | + 650 | + 760 | 11.7 | 12.0 | |
| Eo..... | 404 | 1 4 | +35 11 | - 25 | + 40 | 11.6 | 11.1 | |
| E4..... | 584 | 1 26 | - 7 23 | +1800 | +1725 | 11.8 | 10.9 | |
| Sc..... | 598 | 1 28 | +29 8 | - 70 | - 40 | 9.0 | 7.0 | .263 |
| SBa..... | 936 | 2 23 | - 1 36 | +1300 | +1185 | 11.2 | 11.1 | |
| SBa..... | 1023 | 2 34 | +38 38 | + 300 | + 310 | 11.2 | 10.2 | |
| Sb..... | 1068 | 2 38 | - 0 26 | + 920 | + 795 | 9.8 | 9.1 | 1.0 |
| E4..... | 1700 | 4 52 | - 5 1 | + 800 | + 580 | 12.1 | 12.5 | |
| | 2681 | 8 46 | +51 41 | + 700 | + 710 | 11.3 | 10.7 | |
| Sc..... | 2683 | 8 46 | +33 48 | + 400 | + 335 | 11.3 | 9.9 | |
| Sb..... | 2841 | 9 15 | +51 24 | + 600 | + 620 | 10.5 | 9.4 | |
| Sb..... | 3031 | 9 47 | +69 32 | - 30 | + 75 | 8.5 | 8.3 | .9 |
| Irreg..... | 3034 | 9 48 | +70 9 | + 290 | + 395 | 8.6 | 9.0 | |
| E7..... | 3115 | 10 0 | - 7 14 | + 600 | + 495 | 9.9 | 9.5 | |
| Sa..... | 3368 | 10 41 | +12 20 | + 940 | + 870 | 9.8 | 10.0 | |
| Eo..... | 3379 | 10 43 | +13 6 | + 810 | + 745 | 10.2 | 9.4 | |
| Sb..... | 3480 | 10 55 | +14 26 | + 600 | + 550 | 10.5 | 11.2 | |
| Sc..... | 3521 | 11 1 | + 0 30 | + 730 | + 635 | 9.8 | 10.1 | |
| Sb..... | 3623 | 11 14 | +13 39 | + 800 | + 765 | 9.8 | 9.9 | |
| Sb..... | 3627 | 11 15 | +13 33 | + 650 | + 590 | 10.0 | 9.1 | .9 |
| E7..... | 4111 | 12 2 | +43 38 | + 800 | + 895 | 11.0 | 10.1 | |
| Sb..... | 4151 | 12 5 | +39 58 | + 960 | +1050 | 10.9 | 12.0 | 1.7 |
| Irreg..... | 4214 | 12 11 | +36 53 | + 300 | + 385 | 10.6 | 11.3 | .8 |
| Sb..... | 4258 | 12 14 | +47 52 | + 500 | + 455 | 9.8 | 8.7 | 1.4 |
| E4..... | *4382 | 12 20 | +18 45 | + 500 | + 570 | 9.7 | 10.0 | |
| Irreg..... | 4449 | 12 23 | +44 39 | + 200 | + 230 | 9.5 | 9.5 | .63 |
| E1..... | *4472 | 12 25 | + 8 33 | + 850 | + 870 | 9.1 | 8.8 | |
| Eo..... | *4486 | 12 26 | +12 57 | + 800 | + 835 | 9.2 | 9.7 | |
| Sa..... | *4526 | 12 29 | + 8 15 | + 580 | + 600 | 10.3 | 11.1 | |
| Sb..... | 4565 | 12 31 | +26 33 | +1100 | +1175 | 10.4 | 11.0 | |
| Sa..... | 4594 | 12 35 | -11 4 | +1140 | +1115 | 9.4 | 9.1 | |
| E2..... | *4649 | 12 39 | +12 6 | +1090 | +1130 | 9.8 | 9.5 | |
| Sb..... | 4736 | 12 46 | +41 40 | + 290 | + 410 | 8.8 | 8.4 | .5 |
| Sb..... | 4826 | 12 52 | +22 13 | + 150 | + 230 | 9.3 | 9.0 | .9 |
| Sc..... | 5005 | 13 6 | +37 35 | + 900 | +1030 | 10.6 | 11.1 | |
| Sb..... | 5055 | 13 11 | +42 33 | + 450 | + 590 | 10.0 | 9.6 | 1.1 |
| Sc..... | 5194 | 13 26 | +47 43 | + 270 | + 450 | 8.3 | 7.4 | .5 |
| | 5195 | 13 26 | +47 47 | + 240 | + 410 | 10.5 | 8.9 | |
| Sc..... | 5236 | 13 31 | -29 21 | + 500 | + 470 | 8.8 | 10.4 | .9 |
| Sc..... | 5457 | 14 0 | +54 49 | + 200 | + 385 | 10.2 | 9.9 | .45 |
| Sa..... | 5866 | 15 4 | +56 9 | + 650 | + 865 | 11.2 | 11.7 | |
| | 6822 | 19 39 | -15 0 | - 130 | + 35 | 11.3 | | .214 |
| Sb..... | 7331 | 22 33 | +33 54 | + 500 | + 685 | 10.1 | 10.4 | 1.1 |
| E3..... | 7619 | 23 15 | + 7 39 | +3780 | +3910 | 14.6 | 11.8 | |

TABLE 841.—Extra-Galactic Nebulae, High Velocities

(Hubble, Humason, Astrophys. Journ., 74, 43, 1931.)

Velocity (km/sec.)=(Distance in parsecs)/1790

| Object. | Distance. | Mean velocity. | Notes. |
|--------------------|---------------------|----------------|---|
| Virgo cluster | 1.8 million parsecs | 890 km/sec. | Several nebulae, $12^{\circ} \times 11^{\circ}$ |
| Pegasus " | 7.25 | 3800 | $100 \pm$ nebulae |
| Pisces group | 7. | 4630 | 25 " |
| Cancer cluster ... | 9. | 4800 | 150 " |
| Perseus " | 11. | 5200 | 500 " |
| Coma " ... | 13.8 | 7360 | 800 " . |
| Urs. Maj. " ... | 21.4 | 11800 | 300 " |
| Leo " ... | 32. | 19600 | 300 " |

Extra-galactic nebulae.—(Analysis of 900 plates with 60- and 100-in. Mt. Wilson reflectors, Hubble, Science, 75, 24, 1931.) (1) None found in low galactic latitudes; avoidance zone irregular, 10° to 40° width—apparently due to known obscuring clouds in Taurus, Cassiopeia, Ophiuchus, etc. Inclined belt of bright B stars and diffuse nebulosity reaches highest latitude in Taurus and Ophiuchus. (2) Avoidance zone bordered by partial obscuration to -40° in general direction of center of galactic system (long. 330° to 340°): very limited in opposite direction (except in Taurus) long. 140° , lat. -35° to -40° . (3) Lat. $> 40^{\circ}$ (and in lower lat. towards anti-center) nebulae approx. uniform distribution log number per sq., degree = 2.375. Variation with exposure time indicates uniform distribution also in depth. (4) Appreciable absorption of light in extra-galactic space appears inadmissible. (5) Mean abs. phtg. mag. = 13.8. Density one neb./ 6×10^{-31} parsec³. Mean mass 5×10^6 sun's. Mean density in observable space 5×10^{-31} g/cm³. (6) It may be hazarded that clustered nebulae (in 1 hr. plates) may be expected one per square degree.

TABLE 842.—Rotation of Stars

Values derived for the components, in the line of sight, of the equatorial velocities of rotation for single stars, 0 to 250 km/sec. Assuming that the axes of the stars having the largest rotational velocities are at right angles to the line of sight, it appears that these stars are still stable. "Our analysis of the spectra of giants and dwarfs shows that all single stars belonging to the later spectrum classes show little rotation. On the other hand, a number of spectroscopic binaries of late type, such as W Urs. Maj. have a very rapid rotation. In fact, Adams and Joy have in a number of cases successfully predicted that stars of spectrum classes F or G showing diffuse lines are close spectroscopic binaries. It is probable that we have here a real difference in behavior: in the early spectrum types rapid axial rotation is observed in single stars about as frequently as in spectroscopic binaries; while in the later types rapid rotation occurs only in close binaries. This may have a bearing on the problem of the origin of double stars. (Struve-Elrey, M. N. 26, 91, 663, 1931.)

TABLE 843.—The Galaxy, its Center and Rotation

The center of the galaxy lies apparently among the dense clouds in Sagittarius 40,000 light-years (13,000 parsecs). About this center the sun revolves with a period of about 250,000,000 years, an orbital speed of 200–300 km/sec. Amount of matter within sun's orbit must have mass about 200 billion times our sun's. In following table based partly on Redman, M.N. 92, 113, 1931, r = mean distance in parsecs from center of objects. A = about .017 km/sec./parsec. l_0 longitude galactic center. The sun is about +33 parsecs from galactic plane (Gerasimovič, Luyten, Proc. Nat. Acad. Sci., 1927).

| Type | m | Approx. distance | No. objects | rA | l_0 | Source |
|--------------------------|------|------------------|-------------|-------|-------|---------------------------|
| (1) O-B2..... | 3.98 | 250 | 78 | 2.8 | 290° | Plaskett, Pearce |
| (2) B3-B5..... | 4.64 | 135 | 241 | 1.0 | 300 | " " |
| (3) B3-B5..... | 6.60 | 330 | 222 | 3.2 | 346 | " " |
| (4) A-G, $\mu < ".020 >$ | 5.3 | 180 | 122 | 7 | 345 | Oort, B.A.N., 1927 |
| (5) A-G, $\mu < ".020 >$ | 6.4 | 210 | 88 | 10 | 337 | " " " |
| (6) B8-B9..... | 5.1 | 160 | 250 | 2.1 | 334 | Lindblad, M.N., 1930 |
| (7) F-K, $\mu < ".040 >$ | 5.4 | 190 | 714 | 3.8 | 346 | " " " |
| (8) A, $\mu < ".040 >$ | 5.3 | 160 | 304 | 5.0 | 319 | " " " |
| (9) K..... | 7.3 | 230 | 392 | 1.9 | 17 | Redman, loc. cit., 1931 |
| (10) O-B5..... | ... | ... | 790 | 4.3 | 321 | Pearce, 1931 |
| (11) Interstellar Ca. } | ... | ... | 103 | 5.3* | 325 | Gerasimovič, Struve |
| (12) Same stars..... } | ... | ... | 103 | 12.0* | 330 | Astrophys. Journ., 1929 } |

* These values seem consistent on the supposition that the Ca is more or less evenly distributed between the stars and us, so that r for Ca should be $\frac{1}{2}$ that for the stars.

Lindblad (Scientia, 61, 325, 1932) gives a more recent summary of various workers. With Plaskett's $A = +0.0155$ km/sec./parsec, time of revolution = 200,000,000 years; $l_0 = 327^\circ$. With a linear speed of 275 km/sec, our distance to center is 9,400 parsecs (about 30,000 light-years). Total mass of stellar system = 16×10^{10} solar masses.

TABLE 844.—Transmission of Light Across Space; Theoretical

(Russell, Proc. Nat. Acad. Sci., 8, 115, 1922; Nature, 110, 81, 1922.)

Let radius of particle = r' , density, ρ , (random distribution); quantity of matter per unit vol. = d . The extinction of a beam of light will be e stellar magnitudes per unit distance where $e = 0.814 qd/\rho r$. q is a numerical factor independent of physical units, taking account of complications when $2r$ becomes near the wave length, λ , of the light; when $2r = 2$ or 3λ , q = sensibly unity. q increases for small particles to a max. 2.56, when circumference = $1.12 \times \lambda$; then rapidly decreases, = nearly $(14/3) \times 2\pi r/\lambda^4$ for particles less than $1/2$ this diameter. q/r is max. 2.42, when circumference = λ .

Clouds, same mean density, d , opacity reaches sharp max. when particles of this size, at the same time becomes selective ($1/\lambda^4$). Visual max. when $r = 0.086\rho$. A cloud of this size dust, (density 2.7), absorbs 1 magnitude if 1/86 mg./cm² regardless of cross section. If $1/2$ this or smaller, selective absorption almost as complete as for a gas. Best size particles for opaqueness also best for light pressure.

Rayleigh's formula for gas is $I = I_0 e^{-k}$

$$k = \frac{32\pi^3 (n-1)}{3N \lambda^4} \text{ where } n \text{ is the index of refraction, } N, \text{ Loschmidt's number.}$$

TABLE 845.—Transmission of Light Across Space; Observed Estimates

| | |
|------------------------------------|---|
| Kapteyn, 1904...0.0016 mag./parsec | Van Rhijn, 1928...0.000035* mag./parsec |
| Seeliger, 1911.... .0003 | Shalen, 1929..... .0005 |
| Halm, 1917..... .0030 | Lundmark, 1925... .00000007 |
| | Shapley, 1929..... .000000007 |

* Equivalent to 4.7×10^{-14} g/cm². Bull. Astron. Soc. of Netherlands, 4, 123, 1928. Eddington computed 0.00007 per 100 parsecs as scattering coefficient. For Ca Gerasimovič, 1929, obtained 1.1×10^{-22} as the scattering coefficient.

Absorption and space reddening in the Galaxy as shown by the colors of globular clusters. Stebbins, Proc. Nat. Acad. Sci. 19, 222, 1933.

TABLE 846.—Amount of Matter in Interstellar Space

(Eddington, Proc. Roy. Soc., A3, 424, 1926. Note also Table 848.)

Whether or not matter exists in space is important in estimating absolute magnitudes (Cepheids), and, as a resisting medium, for its dynamical effects.

Density at average point, 10^{-24} g/cm³ (Eddington, dynamical reasons, star velocities).

(Gerasimović, Struve, Gaseous substratum of galaxy, Astrophys. Journ., 69, 7, 1929.)

Interstellar density of Ca probably about $\rho_{Ca} = 3.6 \times 10^{-32}$ g/cm³

For all gases 10^{-26} "

Assuming matter of about atomic weight 20, doubly ionized so that there will be about one free electron per cm, then

Free path for ions, roughly 10^8 km, duration 1 year.

Free path for electrons, roughly 5.2×10^8 km, duration 10 days.

An ion encounters and deflects an electron once in 5 days.

Central density of typical diffuse nebula, estimated, 10^{-20} g/cm³. Hubble (Astrophys. Journ., 1926) estimates if all matter within 100 light-years uniformly distributed, density of order 10^{-31} g/cm³. Eddington (Nature, 128, 702, 1931), 10^{19} electrons and protons in universe.

TABLE 847.—Radii of Curvature of Space

Radius of curvature of the finite universe of general relativity is of the order of 2.7×10^{10} parsecs (Hubble, Astrophys. Journ., 64, 1926).

Radius of Curvature of de Sitterian space time:

| | | | | |
|-------------|-----------------------|----------------------------------|---------------------------------|---------|
| 460 stars | 3.63×10^{11} | astr. units = 5.74×10^6 | light-years = 1.8×10^6 | parsecs |
| 29 Cepheids | 3.0 | " | " | " |
| 35 O stars | 3.2 | " | " | " |

(Silberstein, Nature, 9, 50, 1930.)

TABLE 848.—Interstellar Gases (Calcium, Sodium)

Since excited atoms are exceedingly rare, the only strong absorption lines will be the principal lines. Na, Ca, and Ca + have principal lines in the observable spectrum. If we take a 12000° K. temperature for the interstellar medium, ionization potential may be taken as 20 volts = ψ_0 . For electrons of ionization potential ψ the fraction ionized is $x/(1-x) = e^{(\psi-\psi_0)/RT}$. For Na, $\psi = 5.1$ v. and 30.35 v., $T = 12000$, $RT = 10.3$ v.

whence

$$x/(1-x) = 2 \times 10^6 \text{ for 1st ionization; } 10^{-6} \text{ for 2nd ionization.}$$

Thus the Na + (which is undetectable) is but one part in 2,000,000 of Na. For Ca with ionization potential 6.1 and 11.8 v. we have nearly all Ca as Ca +, but one part in 3000 of Ca +, one in 2×10^6 of Ca.

Certain brighter stars show these lines of Ca (fewer those of Na), which when corrected for solar motion indicate a stationary (relative to sun) absorber, whereas other lines indicate a definite radial velocity for the star (Plaskett). Struve gives the following table indicating definitely the increase of this absorption with the distance:

| | | | | | | | |
|---------------|----------|-------------|-----|-----------------|----------|-------------|-----|
| 0-100 parsecs | 22 stars | K intensity | 2.1 | 400-600 parsecs | 30 stars | K intensity | 4.2 |
| 100-200 | 101 | | 2.2 | 600-800 | 26 | | 4.6 |
| 200-300 | 62 | | 3.1 | 800 | 33 | | 3.1 |
| 300-400 | 47 | | 3.3 | | | | |

Note.—Max. intensity K corresponds closely to outside boundary of local cluster (He B stars). The interstellar Ca apparently shares in the rotation of the galaxy (see Table 843).

Note added 1933.—Plaskett, Pearce consider best value of interstellar density of matter as 10^{-25} g/cm³.

TABLE 849.—Temperature of Interstellar Space

(Eddington, Proc. Roy. Soc., A3, 424, 1926.)

Total light from stars equivalent to 1000 1st (visual) mag. or heat from about 2000 (bolometric) 1st mag. stars. Star abs. mag. 1 radiates $36 \times \text{sun} = 1.37 \times 10^{35}$ erg/sec. At std. distance 10 parsecs (3.08×10^{19} cm) gives flow of 1.15×10^{-6} erg/cm²/sec. Energy density due to star app. bolometric mag. 1.0, is 3.8×10^{-10} erg/cm³ or energy of starlight $= 7.7 \times 10^{-13}$ erg/cm³. The effective temperature of space from Stefan's law is $3^{\circ}.2$ K.

In a region away from prepondering influence of a star a *black* body will take up a temperature $3^{\circ}.2$ K.; then its radiation will balance that which it absorbs. But if the receiving matter be a strongly selectively absorbing gas, higher temperatures may result. See Fabry., *Astrophys. Journ.*, 45, 264. Then the temperature will be governed by 4 considerations: (1) Line absorption (excitation of atoms); energy held about 10^{-8} sec. and then lost by reradiation. An atom meets an electron only once in 5 days. So negligible chance (10^{-10}) of thermal agitation by an encounter. (2) Scattering of free electrons; retards an electron 1 mm/sec./yr.—not cumulative and negligible. (3) Continuous absorption during encounters of electrons with atoms (orbit switches). (4) Photoelectric effect (ionization of atoms). Velocity depends on quality and not intensity of radiation. Forms an electron gas with temperature determined by the mean energy of expulsion. The temperature defined by the mean molecular speed is of the order $10,000^{\circ}$ K.*

The temperature of the electron gas will be the same in space as close to the star. The rate of production of electrons but not their speed will be diminished. The heat of the electrons will be continually renewed and the atoms will gradually be brought to the same temperature. This high temperature is a typical quantum effect.

* $15,000^{\circ}$ K. is considered a better value from more recent data. Plaskett, Pearce, The problems of the diffuse matter in the galaxy, *Publ. Dominion Astrophys. Obs.*, 5, 167, 1923.

TABLE 850.—Matter and Energy

(Donnan, *Nature*, 128, 290, 1931. Dushman, *Gen. Elec. Rev.*, 33, 327, 1930;Eddington, *Nature*, May 1, 1926.)

Jeans proposed the annihilation and transformation of an electron and a proton into radiation to account for the immense output of radiation from the stars. Einstein's special relativity theory gives as the energy corresponding to a mass of m grams of matter mc^2 ergs (c = velocity of light). If E = energy in ergs, then this transformed to matter $= E/c^2$ grams. The mass of a proton + electron $= 6.00 \times 10^{-23}$ g. Applying Einstein's development of Planck's quantum theory, then the coalescence of a proton and electron produces one quantum of monochromatic radiation (photon); and since $mc^2 = h\nu$, $\nu = 2.2 \times 10^{23}$ or $\lambda = 1.3 \times 10^{-13}$ cm. Formerly such short waves were not known but the discovery of cosmic rays shows their possibility.

Now the reaction $P + E \rightleftharpoons$ radiation can occur only under unusual conditions. Imagine a proton-electron gas, only photons of $\nu \geq 2.2 \times 10^{23}$ could change into a matter pair. Donnan shows that the black-body temperature of a *hohlraum* radiation necessary would be $2.2 \times 10^{12}^{\circ}$ K. By another method (equation for variation with the temperature of the

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equilibrium constant of an ideal gas reaction, $d \cdot \log K/dT = Q/RT^2$) he derives a T of 10^{12} °K. Milne yields another solution. If n = no. of protons (electrons) present per cm^3 at statistical equilibrium, then $n = 0.96 \times 10^{18} T^{\frac{1}{2}} \times 10^{-(2.35 \times 10^{12})/T}$.

| T | n/cm^3 | $\rho_m (\text{g}/\text{cm}^3)$ | $\rho_e (\text{g}/\text{cm}^3)$ |
|-----------|-----------------|---------------------------------|---------------------------------|
| 10^{10} | 10^{-202} | 1.65×10^{-226} | 0.85×10^5 |
| 10^{11} | 10^{11} | 1.65×10^{-15} | 0.85×10^9 |
| 10^{12} | 10^{61} | 1.34×10^{10} | 0.85×10^{13} |

We have the following picture: As T rises, molecules will be ionized and finally all dissociated to atoms; then the atoms become ionized with finally a proton-electron gas. At some very high temperature $P + E \rightarrow$ radiation sets in. Milne's equation shows that at $T = 10^{10}$ this reaction is practically complete. As T rises yet higher the birth of matter will commence and we see that $T = 10^{12}$, the equilibrium density of matter becomes equal to $1.34 \times 10^{10} \text{ g}/\text{cm}^3$. $T = 10^{12}$ corresponds to enormous densities for both matter and radiation. Enormous voltages (9×10^8 volts) may give the attainment of such reactions.

Compton effect.—X rays are supposed to consist of streams of energy quanta. While each quantum carries the energy equivalent to $h\nu$, one may also specify each of these photons (light units) by the momentum which, according to the theory of quanta, is equal to $h\nu/c$. When this photon collides with a free or loosely bound electron there is an interchange of both energy and momentum in accordance with the laws of conservation of energy and of momentum. Consequently the photon suffers a recoil in one direction with loss of momentum, while the electron moves off in another direction with added momentum. The decrease in momentum of the scattered X-ray photon corresponds to an increase in wave length. (Dushman, Gen. Elec. Rev., 33, 334, 1930.)

De Broglie phase waves.—De Broglie was led to the conception that associated with a particle of mass m_0 (rest mass, zero velocity) and velocity v , there is a wave motion of wave length given by

$$\lambda = h\sqrt{1 - v^2/c^2}/m_0v = h/m_0v$$

for small values of v ; c is the velocity of light. The theory of relativity gives as the total energy, E , of a particle of mass m_0

$$E = m_0c^2/\sqrt{1 - v^2/c^2} = mc^2$$

with m the mass for velocity v . According to the quantum theory, the frequency associated with E is given by E/h . Hence the phase velocity or velocity of the individual waves constituting the group is given by

$$u = \nu\lambda = mc^2/mv = c^2/v.$$

The value of h is $6.55 \times 10^{-27} \text{ erg}/\text{sec}$. For a mass of 1 g moving at 1 cm/sec. the associated wave length is $6.55 \times 10^{-27} \text{ cm}$ —too small to be measured at present. Wave lengths 10^{-10} to 10^{-7} cm are measurable with crystal lattices. With de Broglie's assumption we would expect corpuscular motion to exhibit phenomena like those associated with light waves under conditions where the momenta of the particles are of the order of magnitude

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$m\bar{v} = h/10^{-10}$ to $h/10^{-7}$; i.e., for $m\bar{v}$ ranging from 6.55×10^{-17} to 6.55×10^{-20} . According to kinetic theory a H_2 molecule ($m = 3.7 \times 10^{-24}$) has a \bar{v} of about 2×10^5 cm/sec. at room temperature. $m\bar{v}$ is then 6.6×10^{-19} , within the above-mentioned range. An electron falling through 100 volts acquires a \bar{v} of 5.9×10^8 cm/sec. and $m\bar{v} = 5.3 \times 10^{-19}$ and $\lambda = 1.24 \times 10^{-8}$ cm. For cathode rays of 25,000-volt velocity, λ comes out 0.75×10^{-9} cm, approximately. Several observers have found for diffracted electrons values of λ in accordance with De Broglie's relation. (Dushman, Gen. Elec. Rev., 33, 335, 1930.)

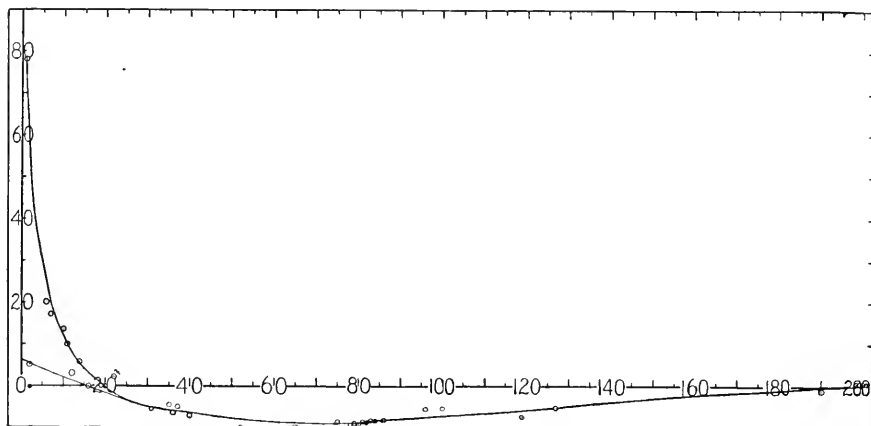
Neutrons.—Bothe and Becker (1930) bombarded various elements with Po α particles (range 3.9 cm in air, 76 cm, 0° C, initial kinetic energy 5.25×10^6 electron volts). Mg, Al, give trace of a resulting radiation, Li, Bo, Fe, notable effects, Be tremendous results—a very penetrating radiation. Joliot and Curie-Joliot (1931) detected it through 30 cm Pb. First considered photons but finally neutrons. Speed of neutrons from Be, 7 to 35×10^8 cm/sec. Curie and Joliot found two groups 29 and 38×10^8 cm/sec. Becker and Bothe found Be to eject 19 photons to 1 neutron. Mass of neutron = $B^{11} + He^4 - N^{14} = 1.0051 \pm 0.005$ (O = 16). (Darrow, Rev. Sci. Instr., 4, 58, 1933, contains bibliography.) May be considered element of atomic number 0; close combination of electron and proton. Effective collision radius 1.31×10^{-13} cm. (Rabi, Phys. Rev., 43, 828, 1933.)

Positron.—Positive electron (Anderson, 1932) + charge $< 2e$, probably exactly equal to e and a mass comparable to a free negative electron. Probably results from the disintegration of atomic nuclei (in Anderson's case by cosmic rays). Out of total of 25,000 exposures, 1,450 cosmic ray photographs were obtained: particles of + and - charge occur in about equal numbers. Energies range $> 10^6$ volts down to few million. Mass probably less than of proton. Anderson < 20 times mass of electron (Anderson, Science, 77, 494, 1933; Darrow, Rev. Sci. Instr., 4, 263, 1933, bibliography).

PACKING FRACTIONS (ASTON)

(See Table 596.)

A reason for the failure of the additive law within the nucleus in atom building is because the protons and electrons become so closely packed that their electromagnetic fields interfere and a certain fraction of the mass is destroyed and appears as an electromagnetic radiation. The greater this loss, the more stable is the resulting nucleus. A convenient and informative expression for this loss is the "packing fraction," the mean gain or loss of mass per proton when the nuclear packing is changed from that of oxygen to the atom under consideration. These are given in Table 596 as parts per 10,000, and their run is indicated in the following plot (ordinates). It is a measure of the forces binding together the protons and electrons of the nucleus. The abscissae are *mass* numbers. It is to be noted that the more stable (even *atomic* numbers) lie on the lower of the two lines drawn. (See Millikan, Phys. Rev., 32, 535, 1928, for the following use of this curve.)



Aston's curve indicates that only very heavy elements can evolve energy by disintegration and there are no abundant elements above at. wt. 80 (less than 1% of all matter).

The condition necessary that even a heavy atom may liberate energy through the emission of an α particle may be seen at once from Aston's curve. Such liberation can happen only where the curve is rising so rapidly with increasing atomic weight that

$$n\Delta y > 4 \times (0.00054 - y_n).$$

n is the at. wt. of the active atom, Δy , the difference in ordinate between $(n - 4)$ and n , y_n , the ordinate for the at. wt. n , and 0.00054 the value of y for He., i.e., it is the mass of the H nucleus within the α particle.

Therefore, not only very heavy atoms alone can disintegrate with the ejection of α rays and the evolution of energy, but we can compute the max. hardness, or penetrating power, of any radiations producible by radioactive disintegration.

When thorium, e.g., throws off an α particle ($n = 232$, $y_n = 0.00031$), the increase in the mass of the α particle per gram-atom, because it has escaped from the nucleus, is $4(0.00054 - 0.00031) = 0.00092$. The loss in mass of the residue of the Th atom $n\Delta y = 0.000034 \times 2.8 = 0.0007752$. Therefore the total loss in mass through the emission of the α ray is $0.000775 - 0.00092 = 0.00683$ grams per gram-atom. By Einstein's equation the energy available for emission from this loss of mass is $0.00683c^2$ ergs/g-atom. The total energy from each ejection of an α particle is this divided by the Avogadro number or 1.004×10^{-5} ergs. The highest speed α ray known to be given off from Ra has an energy of 8,800,000 volts (1.2×10^{-5} ergs). ThC' ejects in one instance an α ray with 14% more energy than this. Similarly the "upper limit" for the speed of a β ray ejected by any of the disintegration products of Th or Ra is 7,540,000 volts or again 1.2×10^{-5} ergs. Einstein's equation predicts quite within the limits of reliability of Aston's measurements of mass, the maximum energy available in the radioactive process.

TABLE 852.—Cosmic Rays

(Millikan, Cameron, Phys. Rev., 31, 921, 1928; 32, 533, 1928.)

The measurements on the absorption coefficients for the cosmic rays indicate a complex set of entering rays which may be analyzed into separate rays with mean absorption coefficients (μ) per meter of water of 0.02, 0.04, 0.08, and 0.30.

Formation of He nucleus from hydrogen: From Einstein's equation and Aston's curve (Table 851) the loss of mass in the formation in a single act of the nucleus of He from four + electrons and two - electrons is $4 \times 1.00778 - 4 \times 1.00054 = 0.029$ g/g-atom, and the radiant energy released each time this act occurs is

$$(0.029 \times 9 \times 10^{20}) / (6.062 \times 10^{23}) = 4.3 \times 10^{-5} \text{ ergs.}$$

$\nu = (4.3 \times 10^{-5}) / (6.547 \times 10^{-27}) = 6.57 \times 10^{-21}$, $\lambda = 0.00046$ A. From Dirac's relativity-quantum-mechanics formula $\mu = 0.30$ per meter H_2O .

Oxygen from hydrogen: $16 \times 0.00778 = 0.1245$ g/g-atom $\mu = 0.074$ per m H_2O .

Nitrogen " " 0.108 g/g-atom = 0.086.

Mean of these two corresponds to 0.08.

Silicon gives $\mu = 0.041$. Iron " $\mu = 0.019$.

So that the observed μ of the cosmic ray may correspond to the creation from hydrogen of He ($\mu = 30$), O (.08), Si (.04) and Fe (.02).

Cosmic rays (A. H. Compton, Phys. Rev., 43, 387, 1933).—Intensity vs. altitude curves indicate not only a rapid increase in ionization intensity with altitude but also that at each alt. the intensity is greater for high lat. than near the Equator. At sea-level the intens. at high lat. is 14% greater than at Equator; at 2000 m alt., 22%, at 4360 m, 33% greater. With arbitrary constants corresponding to 1.605 ions due to rays unaffected by the earth's magnetic field (neutral rays or electrons of energies $> 4 \times 10^{10}$ electron-volts), and a band of electrons approaching the earth with energies between 0.5×10^{10} and 1.3×10^{10} electron-volts reaching the earth at lat. $> 50^\circ$ and producing 0.235 ion, but failing to reach the earth at the Equator, Compton's observations will bear out the theory of Lemaitre and Vallarta (Phys. Rev., 42, 914, 1932). The extra component appearing at high lat. is more rapidly absorbed than the main body of rays. This would be anticipated if rays unaffected by earth's magnetic field were of electrons of greater energy; or a uniform background due to neutral rays such as photons, neutrons, or high speed neutral atoms. Average intensity lat. 0° to 22° , sea-level, 1.620 ± 0.006 ions per cm per sec.; lat. $> 48^\circ$, 1.839 ± 0.006 ions.

Cosmic rays (Millikan, État actuel de nos connaissances sur le lieu et la mode de production des Rayons Cosmiques, Congrès international d'Electricité, 1932; Phys. Rev., 43, 661, 1933; 43, 695, 1933; Science, 77, 494, 1933; 77, May 5, 1933).—Most distinctive results: (A) Ionization-altitude curve (to 18 km or 92% through the atmosphere) does not rise exponentially clear to top with apparent absorption coefficient about 0.6 per m H_2O (all observers get this, say 5 to 9 km) but shows a marked decrease 9 km to top (about 12 km), actually becoming concave downward. This is inconsistent with (1) incoming rays primarily of charged particles, (2) photons in complete equilibrium with their secondaries, (3) rays of the penetrating power of γ rays or rays between these and the least energetic cosmic rays. They show non-ionizing primary entering rays not yet in equilibrium with secondaries.

The rays show a rapid softening with altitude (essentially the same in temperate and equatorial latitudes); best interpreted by cosmic photon bands of widely differing penetrating powers as from the production of He, O, Si, Fe, etc. More than $\frac{2}{3}$ of the cosmic rays at 7.6 km have energy $< 350,000,000$ volts. Millikan considers that the "cosmic rays" found at low altitudes are secondaries formed in the earth's atmosphere by collisions of photons with air atoms. Anderson has caught the cosmic rays, which cannot themselves be photographed, in the act of smashing atoms, setting loose + and - charged particles. So all but a small fraction of the cosmic rays at sea-level are secondaries produced in the earth's atmosphere.

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(See Nat. Res. Council Bull. 85, 1932.)

TABLE 853.—Area of Ocean Depths (Littlehales)

Area of total water surface is about 365,500,000 km². (Land surface about 153,500,000 km².)

| Meters | 0-200 | 200-1000 | 1000-2000 | 2000-3000 | 3000-4000 | 4000-5000 | 5000-6000 | > 6000 |
|-----------------------------------|-------|----------|-----------|-----------|-----------|-----------|-----------|--------|
| km ² × 10 ⁶ | 30.60 | 16.40 | 18.05 | 36.45 | 79.01 | 112.72 | 66.88 | 5.38 |
| % | 8.4 | 4.4 | 4.9 | 9.9 | 21.7 | 30.8 | 18.4 | 1.5 |

The continental shelf dips gradually (depth contour about 200 m); then a steeper continental slope (talus), the seat of many deposit slips, seismic disturbances. Insular shelves and taluses, then troughs, trenches, basin deeps.

TABLE 854.—Oceanic Gradients

Ocean bottom gradients, Atlantic Ocean between Equator and 47° N. latitude.

| Zone, N. lat. | 0-10° | 10-20° | 20-25° | 25-30° | 30-35° | 35-40° | 40-47° |
|---------------|-------|--------|--------|--------|--------|--------|--------|
| Gradient | 20'.7 | 28'.7 | 28'.7 | 23'.9 | 24'.1 | 36'.2 | 37'.1 |

Island gradients often great; St. Helena, up to 40°; St. Paul (Atlantic Ocean), 62°. Gradients for volcanic and coral islands also great, generally in upper 300 m. Great Caldera of Santorin > 50°. S. of Cuba, 76° W., to depth 2625 m, 35° 30'. Compare Fujiyama, Japan, fine volcanic peak, 35°; 12° at base. Steep gradients (Alpine conditions) westward of British, French, Iberian coasts (av. angle 13° to 14°) and W. of continental slope of California (San Diego to Point Conception) 14° between 2000 and 4000 m isobaths.

TABLE 855.—Atlantic Ocean Basin. Areas and Depths (Littlehales)

| Depths, km | 0-2 | 2-4 | 4-6 | 6-8 | Over 8 | Total area |
|--|-------|-------|-------|------|--------|------------|
| Areas, 10 ⁶ km ² | 29.49 | 19.50 | 50.60 | 7.38 | 0.039 | 107.014900 |
| % of whole | 27.6 | 18.2 | 47.3 | 6.9 | 0.4 | 100 |

Remarkable feature: Mid-Atlantic Rise, of median course and continental extent, from Iceland to S. polar border; throughout its more than 13 km, the general rise of its crest is some 3 km above the basin bottom on each side. W. Atlantic trough 6 km deep over large area of N. portion; other troughs and basins of similar depth. European isolated depth of 6 km. Near Equator lessened depth, 1.9 km, and extension along Equator 34° to 15° W. long., cut by narrow gap 18° W., 4 to 5 km deep. Passage through gap leads to Brazilian basin, 7.4 km deep. Ridge < 1 km deep leads from Greenland (Iceland is a volcanic rise) to British Isles.

Greatest depths: 54° 30' S., 28° 30' W., 8.050 km; 19° 36' N., 66° 26' W., 8.351 km; 19° 35' N., 67° 43' W., 8.525 km; 19° 38' N., 68° 17' W., 8.198 km. See also page 651. Greatest depth in Mediterranean, 4,400 km at 35° 45' N., 21° 46' E.; Black Sea, entire central basin below 2 km; North Sea < 200 m throughout.

TABLE 856.—Indian Ocean Basin. Areas and Depths (Littlehales)

| Depths, km | 0-2 | 2-4 | 4-6 | Over 6 | Total area |
|--|-------|--------|--------|--------|------------|
| Areas, 10 ⁶ km ² | 8.192 | 18.569 | 44.569 | 4.656 | 75.986000 |
| % of whole | 10.8 | 24.4 | 58.7 | 6.1 | 100 |

Compared with Atlantic the bottom relief of the Indian Ocean is much simpler. 7 km deep 250 km S. of Java 10° 1' S., 108° 65' E. Persian Gulf, order of 0.09 km deep. Red Sea, about 2 km.

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(See Nat. Res. Council Bull., 85, 1932.)

TABLE 857.—Pacific Ocean Basin. Areas and Depths (Littlehales)

| | | | | | | |
|--|--------|--------|---------|--------|--------|------------|
| Depths, km | 0-2 | 2-4 | 4-6 | 6-8 | Over 8 | Total area |
| Areas, 10 ⁶ km ² | 18.580 | 31.632 | 115.593 | 11.426 | 0.521 | 177.752 |
| % of whole..... | 10.5 | 17.8 | 65.0 | 6.4 | 0.3 | 100 |

With much more steeply sloping shores on the E. and W., this ocean, with its Polynesian characteristics, presents a very irregular depth map. Along W. coasts of both N. and S. America steep slopes are remarkable, descending from great heights of Rocky Mts. and the Andes to depths of 4 km or more within short distances; off S. A., between 10° and 35° S., depths to 8 km near coast. All soundings > 8 km near land, off S. A., Aleutian Is., Kurile Is., Japan, etc. There are numerous isolated volcanic formations, *e. g.*, Hawaiian chain. The largest and deepest depressions are in the gigantic Pacific basin. Tuscarora deep, 8,513 km; 3 elongated tracts 45°, 38°, 31° lat. > 8 km for 38 km². Manchu deep, 31° N., 142° E., 9,435 km for 4 km²; Fleming deep, 23° 48' N., 144° 6' E., 8,650 km deep; Tonga deep, 23° 39' N., 175° 4' E., 9,184 km; Aleutian deep > 6 or 7 km near S. A., 25° 42' S., 71° 31' W., 7,635 km. These deeps are as a rule not associated with the pits of great basins but are nearer land.

Note: The Arctic basin is about $\frac{1}{2}$ of Atlantic Ocean in extent; greatest depths about 4 km. The Antarctic Ocean basin falls steeply from its continent to 2 km.

TABLE 858.—Physical Properties of Sea Water (Thompson)

Temperatures.—Tropical, surface up to 28° C, < 0° C at bottom. Northern Pacific, extreme variation < 6° throughout. Generally decreases with depth.

Pressure.—Atmospheric surface pressure generally neglected, called zero. Pressure is $f(\text{wt.}) = f(\text{temperature, chlorinity, compressibility, latitude})$. Gravity = $f(\text{latitude})$. Bjerknes (1909) proposed a "bar" as unit of pressure = that due to column of water 10 m high.

Concentration.—Dilute solution of several strong electrolytes. An ionizing medium better than distilled water; dielectric constant is greater. Composition much the same, varying mainly in dilution.

Salinity (s) is defined as the total amount of solid material in one kg of sea water when all the carbonates have been converted into oxides, the Br and I replaced by Cl and all organic matter completely oxidized. **Chlorinity** (Cl) = total amount chlorine in one kg when all the Br and I have been replaced by Cl. $S = 0.03 + 1.805 \text{ Cl}$. Thus chlorinity may be reduced to salinity (Knudsen, Hydrographical Tables, Copenhagen, 1901). The principal ions, chlorinity 19.374% are (Ditmar, 1884):

| | | | | | | | | | | |
|---------------|-----------------|------------------|------------------|----------------|--------------|-----------------|-------------------------------|-------------------------------|------------------------------|-------|
| Cations | Na ⁺ | Mg ⁺⁺ | Ca ⁺⁺ | K ⁺ | Anions | Ce ⁻ | SO ₄ ⁻⁻ | HCO ₃ ⁻ | CO ₃ ⁻ | Br- |
| g/kilo | 10.722 | 1.207 | 0.417 | 0.382 | g/kilo | 19.337 | 2.705 | 0.097 | 0.007 | 0.066 |
| moles/l | .4662 | .0533 | .0104 | .0098 | moles/l ... | .5453 | .0281 | .0016 | .0001 | .0008 |
| Totals: | | | 12.818 | g/kilo | Totals: | | 22.212 | g/kilo | | |
| | | | 0.5397 | moles/l | | | 0.5759 | moles/l | | |

For fresh water Ca⁺, HCO₃⁻, and CO₃⁻ predominate.

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(See Nat. Res. Council Bull., 85, 1932.)

TABLE 858 (continued).—Physical Properties of Sea Water (Thompson)

Adiabatic cooling for sea water, chlorinity 19.29‰, 2° C, when brought from various depths to the surface (Ekman, Schott, Amer. Hydrogr. 321, 1914):

| | | | | | | |
|---------------|------|------|------|------|------|-------|
| Depth, meters | 1000 | 2000 | 4000 | 6000 | 8000 | 10000 |
| Cooling, °C | 0.06 | .14 | .36 | .63 | .96 | 1.33 |

Color and transparency.—(See Atkins, Journ. Conseil, 1, 99, 1926.) Optically pure water becomes bluer with depth. Green tints due to suspended matter. A rough measure may be taken as the depth where a white immersed disk becomes just invisible; coastal water, 5 to 25 m, often 45 to 60 m. Max. record 66 m (Sargasso Sea).

Density taken as S_{20} , sp. gr. at 0° referred to distilled water at 4°. Density expressed as $\sigma_0 = (S_0 - 1)1000$. $\sigma_0 = -0.069 + 1.4708 \text{ Cl} - 0.00157 \text{ Cl}^2 + 0.0000398 \text{ Cl}^3$.

| | | | | | |
|------------------|--------|--------|--------|--------|--|
| Chlorinity | 5% | 10% | 15% | 20% | |
| Density | 5.45 | 10.90 | 20.35 | 25.81 | |
| " | 5.00 | 10.40 | 15.75 | 25.15 | |
| Max. density | 2.1 | +0.1 | -1.9 | -3.8 | |
| Freezes | 0.5 | -1.0 | -1.5 | -2.0 | |
| Conductivity | .0085 | .0160 | .0235 | .0305 | Reciprocal ohms |
| " | .0140 | .0265 | .0385 | .0500 | |
| Refractive index | 1.3358 | 1.3376 | 1.3394 | 1.3412 | |
| " | 1.3347 | 1.3364 | 1.3381 | 1.3397 | |
| Sp. heat | .9971 | .9954 | .9942 | .9930 | Atm. pressure |
| Conductivity | 1370. | 1356. | 1348. | 1341. | Thermal, all $\times 10^8$ |
| Surface tension | 77.3 | 77.5 | 77.7 | 77.85 | Dynes/cm |
| " | 73.7 | 73.9 | 74.1 | 74.3 | " " |
| Sp. viscosity | 1.015 | 1.030 | 1.045 | 1.060 | } Referred to dis- tilled H ₂ O, 1.00 at 0° C |
| " | .74 | .755 | .765 | .78 | |
| " | .57 | .58 | .59 | .605 | |

Velocity of sound: Chlorinity, 19.37‰; salinity, 35.00‰

| | | | | | | |
|-----------------|--------------|-------|------|------|------|------------|
| Depth, meters | 0 | 0 | 2000 | 4000 | 6000 | 8000 |
| Velocity m/sec. | [1630] 20° C | [1560 | 1590 | 1625 | 1660 | 1695] 0° C |

TABLE 859.—Chemical Composition of Sea Water (Thompson, Robinson)

Concentration as millimols or milligram atoms per kilogram

| | | | | | | | | | |
|----------|-------|-----------------|------|---------|-------|---------|--------|-------|-----------|
| Cl | 535.0 | CO ₂ | 2.25 | B | 0.037 | Cu | 0.002 | Zn | 0.00003 |
| Na | 454.0 | Br | .81 | Li | .015 | Ba | .0015 | H ion | .00001 |
| Sulphate | 82.88 | Sr | .15 | Nitrate | .014 | I | .00035 | Au | .00000025 |
| Mg | 52.29 | Al | .07? | Fe | .0036 | Ag | .0002 | | |
| Ca | 10.19 | F | .043 | Mn | .003? | Nitrite | .0001 | | |
| K | 9.6 | Si | .04 | P | .002 | As | .00004 | | |

OCEANOGRAPHY

(See Nat. Res. Council Bull. 85, 1932)

TABLE 860.—Waves of the Sea (Patton, Marmer)

Wave forms.—Progression of wave form across a stretch of water; actual cyclic movement (circular in deep water; elliptical, long axis horizontal, in shallow) of particle; there also may be a forward propagation of particles. Form of ocean wave, trochoid or prolate cycloid. If a = height of crest, b = depth of trough, both from undisturbed water level, h and l , the height and length of wave, then $a = (h/l) + 0.7854(h^2/l)$; $b = (h/2) - 0.7854(h^2/l)$ (Gaillard, 1904).

Wind waves in deep water are surface waves. Particle motions decrease rapidly with depth; halved for each $1/9$ l of depth. If height of wave = vertical distance between crest and trough, l , distance between consecutive same phases, v , velocity, p , period, $v = l/p$; $v = (g/2\pi)^{1/2}l$; g = gravity; $p = (2\pi/g)^{1/2}l = (2\pi/g)v$; $l = (g/2\pi)p^2 = (2\pi/g)v^2$.

Principal factors: Strength and duration of wind, fetch exposed to wind. Highest (hurricane) waves in open sea, about 15 m; may be higher through interference, etc., over 30 m. No fixed relation between l and h . Some observed ratios (Gaillard): h , 0.6 to 1.5 m, 30; 3 to 6 m, 20; > 9 m, 14. 150 m long not uncommon; some up to 300 m.

Swell.—As waves pass from disturbed area they degenerate to a gentle swell; not important in mid-ocean but may be dangerous to exposed coasts and harbors. Periods (Morocco coasts) 7 to 20 sec., height 0.45 to 4.5 m.

Waves in shallow water are considerably different. If depth of water greater than length of wave, water deep; less, shallow. Wave of translation (Russell, Rep. British Assoc., 8, 417, 1838; 14, 311, 1845).—All the water is above the undisturbed level; there is actual translation of the water particles; due to sudden addition of water, as with breaking of a wave.

Wave pressure may be as great as 3.3×10^6 dyne/cm².

Seismic waves: Lisbon tidal wave, 1755, 18.3 m; Krakatoa, 1883, 21 m at Telok Betong.

TABLES 861-863

TABLE 861.—Properties of Carboloy

(Hoyt, Hard metal carbides and cemented tungsten carbides, Trans. Amer. Inst. Metals, Inst. of Metals Division, p. 9, 1930.)

Carboloy is a cemented tungsten carbide, $WC + 13\% Co$. At. vol. of the C atoms indicates that they assume the structure of the diamond. Especially adapted to high-speed cutting tools—long life, great hardness and strength.

| | | | | | | |
|--|-------|-------|-------|-------|-------|-------|
| Per cent cobalt..... | 3 | 6 | 9 | 13 | 20 | 100 |
| Density, g/cm ³ | 15.04 | 14.82 | 14.56 | 14.10 | 12.54 | 8.62 |
| Rockwell A hardness, C scale, 60 kg. | | 90 | | 87 | | |
| Vicker Brinell number *..... | 1380a | 1450a | 1365a | 1255b | 755b | 280b |
| Elec. resistance, microms/cm ² , 20° C. | 21.3 | 21.1 | 22.3 | 19.6 | 29.2 | 9.84 |
| Ditto, temp coef., 20-30° C..... | .0047 | .0045 | .0043 | .0044 | .0038 | .0036 |
| * (a) 10 kg load. (b) 30 kg load. | | | | | | |

Carboloy:

Modulus of rupture, cross bending, 20° C, about 225000; 800° C, 183000; 850°, 170000; 900°, 141000 lb./in.².

Expansion coefficient per °C, 20 to 400° C, .000006

Thermal conductivity, watts/cm/°C, .65.

Specific heat, cal./g, .052.

Wiedermann-Franz constant (watts/ohm/°C) $\times 10^6$, 20° C, 12.2.

Hardness at high temp. Brinell, 1100° C, 36; 1300° C, 2.7.

| | | | | | | | |
|-------------------------------------|------|------|------|------|------|------|------|
| Magnetizing force, gilberts/cm..... | 100 | 200 | 300 | 500 | 700 | 900 | 1000 |
| Induction, kilogauss | 0.58 | 1.10 | 1.50 | 2.17 | 2.67 | 3.10 | 3.29 |

TABLE 862.—Properties of Dekhotinsky Cement

Dekhotinsky cement for air-tight joints. Sp. resistance 2×10^{13} ohm · cm and inductive capacity higher than of mica; adhesion great. For cementing glass and metals. Nitric, sulphuric, hydrochloric acids, bisulphide of carbon, benzene, gasoline, turpentine do not attack it. Very little affected by ether, chloroform, caustic alkalies, etc.

TABLE 863.—Properties of Fused Quartz (Vitreous Silica)

Fused quartz (vitreous silica). Can be used to a working temperature of 1000° C. Softens about 1400°, melts about 1756° C. Can be used intermittently to 1700° but above 1000° devitrification commences.

Thermal expansion low, .0000005 per °C up to 1000°.

Invar, .0000009.

Chemical pyrex, .0000032.

Jena glass 59, .0000057.

Expands on continued cooling to 80° C.

Specific gravity: clear fused, 2.21, translucent, 2.1.

Hardness, Moh's scale, fused, 4.9, crystal, 6.3.

Modulus of elasticity, 9,400,000 lbs./in.²

Tensile strength, 7,000 lbs./in.²

Compression strength, 190,000 lbs./in.²

Impermeability. Not porous to common gases at high T and ordinary pressures.

Helium diffuses through even at low T . Non-hygroscopic.

Transparent to radiation about .1850 to 1μ .

Thermal conductivity at 20° C .0024 for clear fused quartz, increases rapidly with rise in temperature.

Resistivity electrical, 5×10^{18} ohm · cm 25° C.

Dielectric constant, 100000 cycles, 25° C, 60% humidity = 4.4.

Most acids, neutral salts, refractory oxides, either no chemical action or less than with glass, Pt, or porcelain. Hot solutions and fusions of the caustic alkalies readily attack.

(Vitreous silica, Sosman, 1927; Fused quartz, Gen. Elec. Co., 1928.)

TABLE 864.—Properties of Phenol-Resinoid Products

| Quality | Pure hardened resinoid | Molded | | | Laminated | |
|--|-------------------------|------------------------|------------------------|------------------|---|-------------------------------|
| | | Wood floor filler | Fabric filler | Asbestos filler | Paper | Fabric |
| Molding qualities..... | none | excellent | good | fair | sheets, tubes, rods, etc. permanently infusible | |
| After molding..... | | permanently infusible | | | fair | fair |
| Machining..... | good | fair | fair | fair | none | none |
| Cold flow..... | none | none | none | none | opaque | opaque |
| Transparency..... | transparent translucent | opaque | opaque | opaque | opaque | opaque |
| Refractive index..... | 1.56-1.70 | opaque | opaque | opaque | opaque | opaque |
| Specific gravity..... | 1.2-1.3 | 1.3-1.4 | 1.3-1.4 | 1.8-2.0 | 1.3-1.4 | 1.3-1.4 |
| Tensile strength lb./in. ² | 5,000 to 11,000 | 6,000 to 12,000 | 6,000 to 12,000 | 3,500 to 5,000 | 8,000 to 20,000 | 8,000 to 12,000 |
| Fig. 8 test piece | negligible | negligible | negligible | negligible | negligible | negligible |
| Elongation..... | 10-25 | | | | | |
| Modulus of elasticity transverse lbs./in. ² | $\times 10^5$ | | | | | |
| Modulus of rupture transverse lbs./in. ² | 12,000 to 20,000 | 10,000 to 20,000 | 8,000 to 15,000 | 8,000 to 20,000 | flat or edge-wise 75,000 | flat or edge-wise 75,000 |
| Electrical resist. $\omega \cdot \text{cm}^3$ | 10^{10} to 10^{12} | 10^{10} to 10^{11} | 10^{10} to 10^{11} | 10^8 to 10^9 | to 30,000 10^{10} to 10^{11} | to 25,000 10^9 to 10^{10} |
| Breakdown volts,* V/mil. | 250-700 | 300-500 | 20-500 | 150-400† | 500-1300 | 200-500 |
| Power factor 10^6 cycles..... | 4.5 to 7 | 4.5 to 8 | 4.5 to 7 | 5 to 20 | 4.5 to 6 | 4.5 to 7 |
| Thermal conductivity..... | 3-4 | 4-6 | 4-6 | 12-20 | 5-8 | 5-8 |
| cal./sec. cm ² °C | $\times 10^{-4}$ | $\times 10^{-4}$ | $\times 10^{-4}$ | $\times 10^{-4}$ | $\times 10^{-4}$ | $\times 10^{-4}$ |
| Sp. heat..... | .33-.36 | | .30-.40 | | .30-.40 | |
| Burning..... | extremely low | | nonflammable | | extremely low | |

Instantaneous at 60 cycles. † Mica filler.

animal, vegetable, mineral oils, hydrocarbons, esters, ketones, no effect; alcohols, practically none; alkalis, slowly softened, strong, disintegrates; decomposed by strong nitric and sulphuric acids by hydrochloric and hydrofluoric which attack fillers. Withstands 250° F. (Data from Mory and Lor, Bakelite Corporation, 1920.)

TABLE 865.—High Vacuum Technique

References: Dunoyer, Vacuum practice, London, Bell and Sons, 1926; Newman, The production and measurement of low pressures, New York, Van Nostrand, 1925; Kaye, High vacuum, Longmans, Green & Co., 1927; Dushman, High vacuum, Gen. Elec. Rev., 1922; Goetz, Physik und Technik der Hochvakua, Vieweg und Sohn, Akt. Ges., Braunschweig, 1926; Langmuir, Phys. Rev., 2, 450, 1930; Zeitschr., 15, 516, 1914.

The following is taken from Dushman, Rev. Mod. Phys., 2, 381, 1930, whence the above references. Stop-cocks, greased joints, etc., should be avoided in connection with the exhaust and preparation of tubes containing cathodes for which electron emissivity are to be determined. While the evaporation of Ca, Ba, and alloys of rare-earth metals have been used. Ba cleans up practically all residual gases at ordinary temperatures, while Mg is ineffective for H₂ and Ca does not take up N to any great extent. Very low pressures may be obtained with a side tube containing charcoal (which has been well outgassed) immersed in liquid air. Care should be taken that the liquid air is maintained at constant level during the series of measurements.

PROPERTIES OF MALLEABLE CAST IRON

(From Proc. Amer. Soc. for Testing Materials, 31, pt. 2, 1931; Malleable Iron Research Institute.)

Malleable iron is the product produced by the annealing or graphitization of "white iron" castings in which all carbon should be present in the combined form, such that the final structure of the malleable casting consists of ferrite and free carbon (temper carbon) with practically no combined carbon as free cementite or pearlite. Where strength, ductility, machineability, and resistance to shock are important, malleable iron castings are of wide application.

Chemical composition: C 1.00 to 2.00; Si 0.60 to 1.10; Mn < .30; P < .2; S .06 to .15%.

Density: 7.15 to 7.45. Thermal expansion: 20°-400° C, about 0.000012 per °C.

Sp. Ht.: Mean 20°-100° C, 0.122 per g per °C; 20°-200°, 0.125; 20°-500°, 0.139; 20°-700°, 0.159.

Thermal conductivity: K_t , 50° C, 0.145 g. cal./sec./°C/cm; 100° C, 0.137; 200° C, 0.115.

Tensile strength: 54,000 lbs./in.²; range 45,000 to 63,000; yield point 36,000 lb./in.²

Elongation in 2 in. 18%. Modulus of elasticity in tension 25,000,000 lb./in.²

Compressive strength: Material flows indefinitely.

"Special" tensile 57,690; yield point 38,000; elongation 25% in 2 in.

Ultimate shearing strength 48,000 lb./in.²; yield point 23,000 lb./in.²; elasticity mod. 12,500,000 lb./in.²

Modulus rupture in torsion 58,000 lb./in.²; yield point in torsion 24,000 lb./in.²

Brinell hardness 115, range 100 to 140. Charpy impact value 7.75 ft. lb.

Note: If malleable iron is heated above its lower critical point (about 760° C), carbon redissolves and the character of the iron changes.

Resistivity: 28 to 37 microhms · cm³ $R_{100}/R_0 = 1.1$ $R_{500}/R_0 = 2.3$.

| | | | | | | | |
|---|------|------|------|-------|-------|-------|-------|
| Magnetizing force, H , gilberts/cm..... | 2.5 | 5 | 7.5 | 10 | 15 | 20 | 30 |
| Induction, B , gauss (mean)..... | 5800 | 7600 | 9200 | 10000 | 11000 | 11400 | 11900 |

Comparative machineability. Relative power required (means of planing, drilling, and milling):

| | | | | | |
|------------------------|----|-----------------------|----|--------------------------|-----|
| Dow metal, type E.... | 19 | Gun metal | 55 | Copper annealed | 131 |
| Bearing bronze | 36 | Cast iron | 60 | Tool steel 1.03% C... | 145 |
| Aluminum alloy no. 31. | 37 | Manganese bronze ... | 61 | Stainless Cr, iron, ann. | 158 |
| Red brass | 38 | Malleable cast iron.. | 70 | Monel metal | 165 |
| Sheet brass | 41 | Unleaded brass | 85 | Nickel "A" | 193 |

DEFINITIONS OF UNITS

ACTIVITY. Power or rate of doing work; unit, the watt.*

AMPERE. Unit of electrical current. The international ampere, "which is one-tenth of the unit of current of the c.g.s. system of electromagnetic units, and which is represented sufficiently well for practical use by the unvarying current which, when passed through a solution of nitrate of silver in water, and in accordance with accompanying specifications, deposits silver at the rate of 0.00111800 of a gram per second."

The ampere = 1 coulomb per second = 1 volt through 1 ohm = 10^{-1} e.m.u. = 3×10^9 e.s.u.

Amperes = volts/ohms = watts/volts = (watts/ohms) $^{\frac{1}{2}}$.

Amperes \times volts = amperes $^2 \times$ ohms = watts.

ANGSTROM. Unit of wave length = 10^{-10} meter.

ASTRONOMICAL UNIT. Mean distance earth to sun, 149,500,000 km.

ATMOSPHERE. Unit of pressure.

English normal = 14.7 pounds per sq. in. = 29.929 in. = 760.18 mm Hg. 32° F.

French " = 760 mm of Hg. 0° C = 29.922 in. = 14.70 lbs. per sq. in.

AVOGADRO NUMBER. Number of molecules per mole 6.064×10^{23} mole $^{-1}$.

BAR. International unit of pressure 10^6 dyne/cm 2 , g = 980.616 cm/sec 2 .

BARYE. c.g.s. pressure unit, one dyne/cm 2 .

BRITISH THERMAL UNIT. Heat required to raise one pound of water at its temperature of maximum density, 1° F. = 252 gram-calories.

CALORIE. Small calorie = gram-calorie = therm = quantity of heat required to raise one gram of water at its maximum density, one degree Centigrade.

Large calorie = kilogram-calorie = 1000 small calories = one kilogram of water raised one degree Centigrade at the temperature of maximum density.

For conversion factors see page 251.

CANDLE, INTERNATIONAL. The international unit of candlepower maintained jointly by national laboratories of England, France and United States of America.

CARAT. The diamond carat standard in U. S. = 200 milligrams. Old standard = 205.3 milligrams = 3.168 grains.

The gold carat: pure gold is 24 carats; a carat is $1/24$ part.

CIRCULAR AREA. The square of the diameter = $1.2733 \times$ true area.

True area = $0.785398 \times$ circular area.

CIRCULAR INCH. Area of circle one inch in diameter.

COULOMB. Unit of quantity. The international coulomb is the quantity of electricity transferred by a current of one international ampere in one second = 10^{-1} e.m.u. = 3×10^9 e.s.u.

Coulombs = (volts-seconds)/ohms = amperes \times seconds.

CUBIT = 18 inches.

DALTON. Unit of mass, $1/16$ mass of oxygen atom. 1.65×10^{-24} g.

DAY. Mean solar day = 1440 minutes = 86400 seconds = 1.0027379 sidereal day.

Sidereal day = 86164.10 mean solar seconds.

DIGIT. $\frac{3}{4}$ inch; $1/12$ the apparent diameter of the sun or moon.

DIOPTER. Unit of "power" of a lens. The number of diopters = the reciprocal of the focal length in meters.

DYNE. c.g.s. unit of force = that force which acting for one second on one gram produces a velocity of one cm per sec. = $1g \div$ gravity acceleration in cm/sec./sec.

Dynes = wt. in g \times acceleration of gravity in cm/sec./sec.

ELECTROCHEMICAL EQUIVALENT is the ratio of the mass in grams deposited in an electrolytic cell by an electrical current to the quantity of electricity.

DEFINITIONS OF UNITS

FOOT-POUND. The work which will raise one pound one foot high.

For conversion factors *see* page 251.

FOOT-POUNDALS. The English unit of work = foot-pounds/g.

For conversion factors *see* page 251.

EQUATION OF TIME. Excess of mean time over true time.

ERG. c.g.s. unit of work and energy = one dyne acting through one centimeter.

For conversion factors *see* page 251.

FLUIDITY. Reciprocal of viscosity.

g. The acceleration produced by gravity.

GAUSS. A unit of intensity of magnetic field = 1 e.m.u. = $\frac{1}{3} \times 10^{-10}$ e.s.u.

GRAM. *See* page 6.

GRAM-CENTIMETER. The gravitation unit of work = g. ergs.

GRAM-MOLECULE = x grams where x = molecular weight of substance.

GRAVITATION CONSTANT = G in formula $G \frac{m_1 m_2}{r^2} = 666.4 \times 10^{-10}$ dyne \cdot cm² \cdot g⁻².

HEAT OF THE ELECTRIC CURRENT generated in a metallic circuit without self-induction is proportional to the quantity of electricity which has passed in coulombs multiplied by the fall of potential in volts, or is equal to (coulombs \times volts)/4.181 in small calories.

The heat in small or gram-calories per second = (amperes² \times ohms)/4.181 = volts²/ (ohms \times 4.181) = (volts \times amperes)/4.181 = watts/4.181.

HEAT. Absolute zero of heat = -273.18° C.

HEFNER UNIT. Photometric standard; *see* page 334.

HENRY. Unit of induction. It is "the induction in a circuit when the electromotive force induced in this circuit is one international volt, while the inducing current varies at the rate of one ampere per second" = 10^9 e.m.u. = $1/9 \times 10^{-11}$ e.s.u.

HORSEPOWER. The English and American horsepower is defined by some authorities as 550 foot-pounds per second and by others as 746 watts. The continental horsepower is defined by some authorities as 75 kilogrammeters per second and by others as 736 watts. *See* page 251.

JOULE. Unit of work = 10^7 ergs. For electrical Joule *see* page xlv.

Joules = (volts² \times seconds)/ohms = watts \times seconds = amperes² \times ohms \times sec.

For conversion factors *see* page 251.

JOULE'S EQUIVALENT. The mechanical equivalent of heat. *See* page 86.

KILODYNE. 1000 dynes. About 1 gram.

KINETIC ENERGY in ergs = grams \times (cm/sec.)²/2.

LITER. *See* page 6.

LOSCHMIDT NUMBER. Number of molecules per unit vol. ideal gas at 0° C and normal pressure, 2.705×10^{19} cm⁻³.

LUMEN. Unit of flux of light-candles divided by solid angles.

MEGABAR. Unit of pressure = 1,000,000 bars = 0.987 atmospheres.

MEGADYNE. One million dynes. About one kilogram.

METER. *See* page 6.

METER CANDLE. The intensity of lumination due to standard candle distant one meter.

MHO. The unit of electrical conductivity. It is the reciprocal of the ohm.

MICRO. A prefix indicating the millionth part.

MICROFARAD. One-millionth of a farad, the ordinary measure of electrostatic capacity.

MICRON. (μ) = one-millionth of a meter.

MIL. One-thousandth of an inch.

MILE. *See* pages 5, 6.

MILE, NAUTICAL or GEOGRAPHICAL = 6080.204 feet.

MILLI-. A prefix denoting the thousandth part.

MOLE. Mass equal to molecular weight of substance.

DEFINITIONS OF UNITS

- MONTH. The anomalistic month = time of revolution of the moon from one perigee to another = 27.55460 days.
- The nodical month = draconitic month = time of revolution from a node to the same node again = 27.21222 days.
- The sidereal month = the time of revolution referred to the stars = 27.32166 days (mean value), but varies by about three hours on account of the eccentricity of the orbit and "perturbations."
- The synodic month = the revolution from one new moon to another = 29.5306 days (mean value) = the ordinary month. It varies by about 13 hours.
- OHM. Unit of electrical resistance. The international ohm is based upon the ohm equal to 10^9 units of resistance of the c.g.s. system of electromagnetic units, and "is represented by the resistance offered to an unvarying electric current by a column of mercury, at the temperature of melting ice, 14.4521 grams in mass, of a constant cross section and of the length of 106.3 centimeters" = 10^9 e.m.u. = $1/9 \times 10^{11}$ e.s.u.
- International ohm = 1.01367 B. A. ohms = 1.06292 Siemens' ohms.
- B. A. ohm = 0.98651 international ohms.
- Siemens' ohm = 0.94080 international ohms.
- PARSEC. Distance of star whose parallax is 1".
- PENTANE CANDLE. Photometric standard. *See* page 334.
- $\pi = \pi$ = ratio of the circumference of a circle to the diameter = 3.14159265359.
- POUNDAL. The British unit of force. The force which will in one second impart a velocity of one foot per second to a mass of one pound.
- RADIAN = $180^\circ/\pi = 57.29578^\circ = 57^\circ 17' 45'' = 206265''$.
- REAMUR. Thermometric scale. $0^\circ \text{C} = 0^\circ \text{R}$. $100^\circ \text{C} = 80^\circ \text{R}$.
- SECOHM. A unit of self-induction = 1 second \times 1 ohm.
- SLUG. Unit of mass. Mass acquiring acceleration 1 ft./sec.² when continuously acted upon by 1 lb. wt.
- SLUG. (Metric) ditto accel. 1 m/sec.², 1 kg weight.
- TENTH-METER. 10^{-10} meter = 1 Angstrom.
- THERM = small calorie = (obsolete).
- THERMAL UNIT, BRITISH = the quantity of heat required to warm one pound of water at its temperature of maximum density one degree Fahrenheit = 252 gram-calories.
- VOLT. The unit of electromotive force (e.m.f.). The international volt is "the electromotive force that, steadily applied to a conductor whose resistance is one international ohm, will produce a current of one international ampere. The value of the e.m.f. of the Weston Normal cell is taken as 1.0183 international volts at $20^\circ \text{C} = 10^8$ e.m.u. = $1/300$ e.s.u. *See* page 80.
- VOLT-AMPERE. Equivalent to Watt/Power factor.
- WATT. The unit of electrical power = 10^7 units of power in the c.g.s. system. It is represented sufficiently well for practical use by the work done at the rate of one Joule per second.
- Watts = volts \times amperes = amperes² \times ohms = volts²/ohms (direct current or alternating current with no phase difference).
- For conversion factors *see* page 251.
- Watts \times seconds = Joules.
- WEBER. A name formerly given to the coulomb.
- WORK in ergs = dynes \times cm. Kinetic energy in ergs = grams \times (cm/sec.)²/2.
- YEAR. *See* page 601.
- Anomalistic year = 365 days, 6 hours, 13 minutes, 48 seconds.
- Sidereal " = 365 " 6 " 9 " 9.314 "
- Ordinary " = 365 " 5 " 48 " 46 + "
- Tropical " same as the ordinary year.

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* Phenomenon too complex for insertion in book. See J. J. and G. P. Thomson, Conductivity of electricity through gases, 1928; K. T. Compton and Langmuir, Electrical discharge in gases, Rev. Mod. Phys., 2, 123, 1930.

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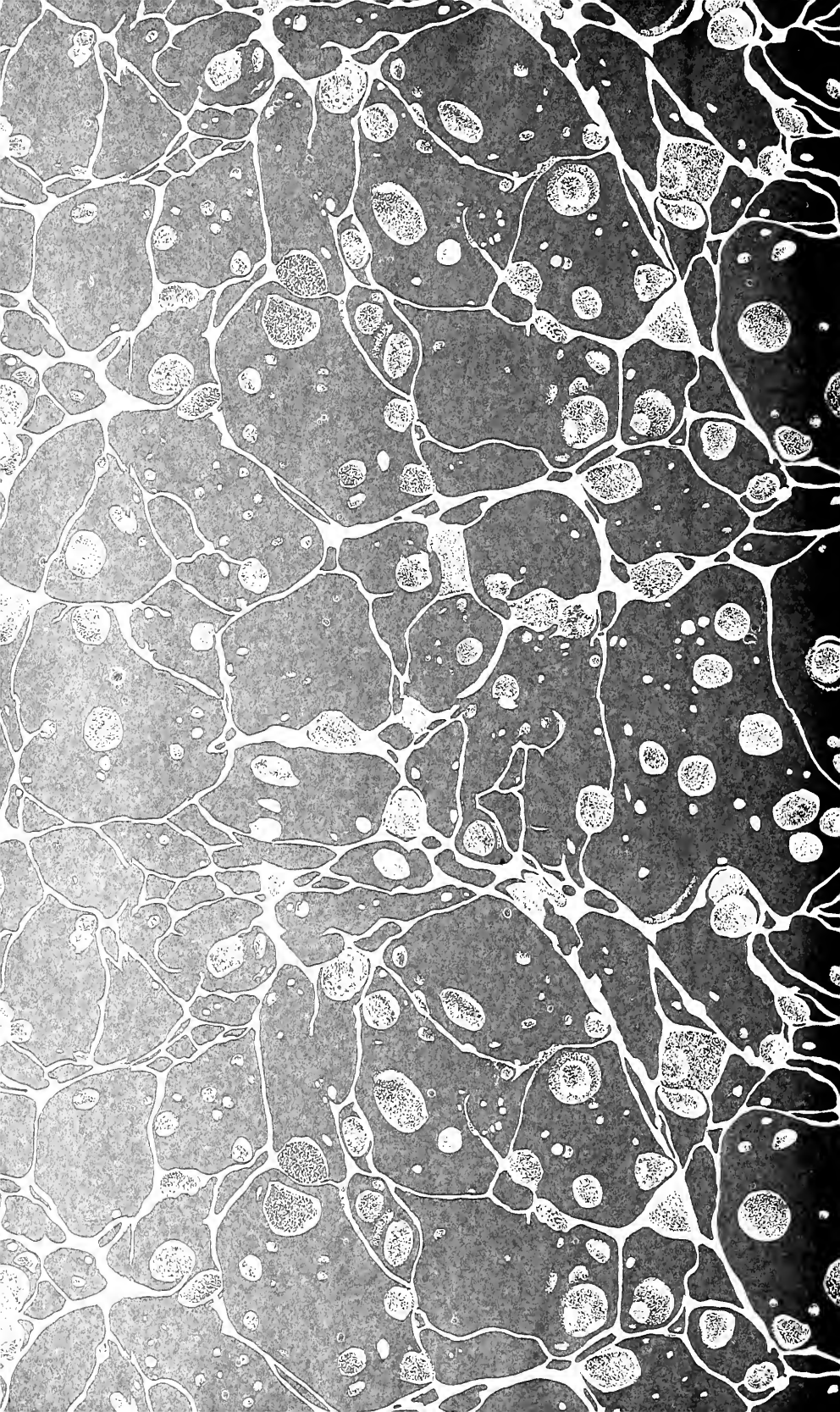
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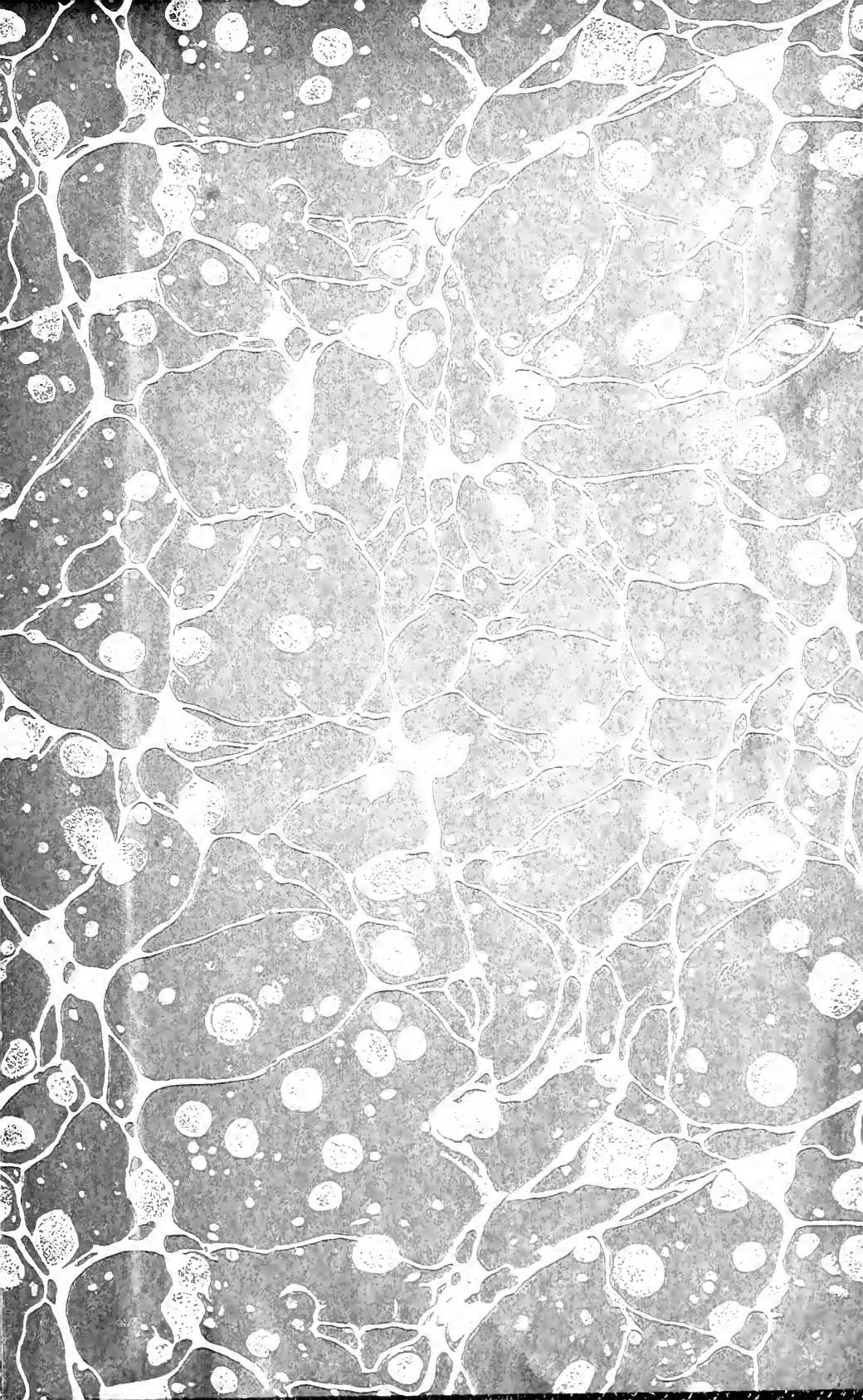
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